APPENDIX G: DESIGN GEOTECHNICAL DATA



DRAFT GEOTECHNICAL STUDY MISSISSIPPI RIVER LONG DISTANCE SEDIMENT PIPELINE (BA-43 EB) MISSISSIPPI RIVER TO BARATARIA WATERWAY LDNR RSIQ NO. 2503-08-22 JEFFERSON PARISH, LOUISIANA

MOFFATT & NICHOL BATON ROUGE, LOUISIANA



FUGRO CONSULTANTS, INC.



Report No. 04.55084005 - DRAFT November 29, 2011 4233 Rhoda Drive Baton Rouge, Louisiana 70816 Tel. (225) 292-5084 Fax: (225) 292-8084

MOFFATT & NICHOL

One American Place, Suite 800 301 Main Street Baton Rouge, LA 70825

Attention: Mr. Jonathan Hird, P.E.

Draft Geotechnical Study

Mississippi River Long Distance Sediment Pipeline (BA-43B)

Mississippi River to Barataria Waterway

LDNR RSIQ No. 25503-08-22

Jefferson Parish, Louisiana

Fugro Consultants, Inc. (Fugro) is pleased to present this draft report of our geotechnical services for the above referenced project. Our services were performed in general accordance with our Proposal No. 5508-4005 dated July 13, 2011. We submitted a data report discussing our field and laboratory operations for the Phase I borings and CPTs on September 23, 2011 and preliminary recommendations based on the borings and CPTs for both Phase I and Phase II on October 28, 2011. Moffatt and Nichol provided comments subsequent to our preliminary recommendations that we have incorporated into this draft report.

This report includes a comprehensive discussion of our field and lab operations as well as a discussion of our engineering analyses and recommendations. We appreciate the opportunity to be of service to Moffatt and Nichol. Please call if you have any questions or comments concerning this draft report, or when we may be of further assistance.

Sincerely,

FUGRO CONSULTANTS, INC.

Jennifer E. Aguettant, P.E. Engineering Supervisor

Eric R. Marx, P.E. Branch Manager

Copies Submitted: (1) Addressee

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CONTENTS

		<u>Page</u>
1.0	INTRODUCTION	
	1.2 Scope of Services	1
2.0	REVIEW OF EXISTING INFORMATION	3
	2.1 Eustis Engineering Company, Inc. Report 2.2 URS Corporation Report 2.3 BA-39 Data	3
3.0	FIELD EXPLORATION	5
	3.1 Drilling Methods and Boring/CPT Locations	6
	3.3 Cone Penetration Testing	
	3.5 Borehole and CPT Completion	
4.0	LABORATORY TESTING	9
	4.1 Classificatino Testing	9
	4.2 Undrained Shear Strength	
	4.3 One-Dimensional Consolidation Testing	
5 0	GENERALIZED SUBSURFACE CONDITIONS	
5.0	5.1 Soils Reach 1	
	5.1 Soils Reach 1	
	5.3 Soils Reach 3	
	5.4 Design Soil Strength Parameters	.13
	5.5 Design Soil Compressibility	.14
6.0	PROJECT FEATURES	.17
	6.1 Containment Dikes	
	6.2 Pipeline Access Corridor and Adjacent Marsh Apron Fill Area	
	6.3 Additional Marsh Creation Fill Area	
7.0	SETTLEMENT ANALYSES	_
	7.1 Settlement Models	
	7.2 Settlement Analyses of the Pipeline Corridor and Containment Dikes7.3 Settlement of the Marsh Creation Areas	
8 N	SLOPE STABILITY ANALYSES	
5.0	8.1 Material Properties	
	8.2 Stability Models	





8.3 Slope Stability Analysis Results	30
9.0 CONSTRUCTION RECOMMENDATIONS	32
9.1 Containment Dikes	32
9.2 Pipeline Corridor and Marsh Creation Fill Material	
9.3 Additional Construction Considerations	
ILLUSTRATIONS	
	<u>Plate</u>
Plan of Borings and CPTs	1
Boring Logs	. 2 through 19
Key to Terms and Symbols used on the Boring Logs	20a and 20b
Grain Size Distributions	la through 21f
Generalized Subsurface Profile – Soils Reach 1 – Cross-Section A-A	22
Generalized Subsurface Profile - Soils Reach 2, North-South - Cross-Section B-B	23
Generalized Subsurface Profile – Soils Reach 2, East-West – Cross-Section C-C	24
Generalized Subsurface Profile – Soils Reach 3 – Cross-Section D-D	25
Locations of BA-39 Settlement Plates	26
Generalized Subsurface Profile – BA-39 – Cross-Section E-E	27
Design Strength and Unit Weight Parameters – Soils Reach 1	28
Design Strength and Unit Weight Parameters – Soils Reach 2	29
Design Strength and Unit Weight Parameters – Soils Reach 3	30
Time Rate of Settlement – Pipeline Corridor – Lower-Bound Mudline Elevations	31
Time Rate of Settlement – Pipeline Corridor – Upper-Bound Mudline Elevations	32
Time Rate of Settlement – Pipeline Corridor – Soils Reach 1 Borrow Excavation	33
Time Rate of Settlement – Containment Dikes – Lower-Bound Mudline Elevations.	34
Time Rate of Settlement – Containment Dikes –Upper-Bound Mudline Elevations	35
Time Rate of Settlement – Marsh Creation Area	36
Slope Stability – Soils Reach 1 – Containment Dike	37





APPENDICES

Summary of Test Results	Appendix A
One-Dimensional Consolidation Test Results	Appendix E
Cone Penetration Test Logs	Appendix C
Subsurface Information Obtained by Others	Appendix D
Typical Cross-sections Provided by Moffatt and Nichol	Appendix E





1.0 INTRODUCTION

1.1 Project Description

Over the last 100 years, the rate of land lost has increased rapidly in the Barataria Basin. One of the major factors has been the construction of levees on the Mississippi River and other natural channels, preventing the yearly deposition of soil as the river flooded and changed courses. Other contributing factors to land loss include manmade pipeline canals, subsidence, sea level rise, shoreline erosion, and saltwater intrusion.

The objective of this project is to obtain renewable sediment sources and provide an adequate corridor that supports equipment mobilization for long-distance conveyance of Mississippi River sediments to wetland creation projects in the Central Barataria Basin in Plaquemines, Jefferson, and Lafourche Parishes. A site vicinity map for the project is included on Plate 1. Our geotechnical study was concentrated on the proposed pipeline corridor alignment between the back levee and Barataria Waterway.

Two options were being considered for the pipeline alignment at the start of our study. The first option, designated the "Option A" alignment, follows a natural ridge immediately south of Chenier Traverse Bayou from the back levee to Bayou DuPont. The second option, designated the "Option B" alignment, follows an existing oil and gas channel that crosses the BA-39 Project area and then turns southwest towards Bayou Dupont. The alignments for Options A and B meet south of Bayou DuPont. After the completion of our field investigation, Option B was removed from consideration.

Moffatt and Nichol, the design engineer for the project, requested that we perform a geotechnical study within the project boundaries to assess subsurface conditions and provide geotechnical recommendations to the project team. Our findings are included herein.

1.2 Scope Of Services

The purposes of our geotechnical study were: 1) to explore and evaluate the subsurface soil conditions at the site, and 2) to provide geotechnical recommendations to assist the design team in developing plans and specifications for the sediment pipeline corridor. The scope of this study included the following:

- reviewing existing topographic and geotechnical information in the vicinity of the project to develop an exploration program
- drilling soil borings and performing Cone Penetration Test (CPT) soundings to evaluate subsurface conditions;





- performing field and laboratory tests on select soil samples to assess pertinent engineering soil properties;
- performing engineering analyses to estimate settlement, factors of safety against slope stability failures and ultimate bearing capacity due to the placement of marsh creation fill and containment dike material;
- preparing a report summarizing our findings and geotechnical recommendations.

Environmental assessments, compliance with state and federal regulatory requirements, and/or environmental analyses including those associated with mold, fungi, and other biologic agents were beyond the scope of this study. A geologic fault study was also beyond the scope of this study.

1.3 Applicability of Report

The explorations and analyses for this study were selected or developed based on our understanding of the project as described previously and in later sections of this report. If there are differences in project location or design features as we understand them, or if the locations or design features change, we should be authorized to review the changes and, if necessary, modify our conclusions and recommendations. The observations, conclusions, and recommendations presented in this report may not apply to locations not explored by our borings and CPTs or areas outside the project boundaries.

We have prepared this report exclusively for Moffatt and Nichol and the Louisiana Office of Coastal Protection and Restoration (OCPR) to guide the geotechnical aspects of the Long Distance Sediment Pipeline Project. We have conducted this study using the standard level of care and diligence normally practiced by recognized engineering firms now performing similar services under similar circumstances. We intend for this report, including all illustrations, to be used in its entirety. This report should be made available for information only and not as a warranty of subsurface conditions.





2.0 REVIEW OF EXISTING INFORMATION

Moffatt and Nichol provided reports of geotechnical studies performed by others in the vicinity of the Long Distance Sediment Pipeline project. In addition, survey data and construction observations from the recently constructed BA-39 marsh creation area was provided. The data was used to develop a field exploration program that would supplement the available subsurface information. In addition, the information was used as a guide to calibrate engineering analyses based on the performance of recently constructed marsh. We have provided a brief discussion of the contents of this available information in the following sections.

2.1 Eustis Engineering Company, Inc. Report (Project No. 19183, dated September 13, 2006)

Eustis Engineering Company, Inc. (Eustis) conducted a geotechnical investigation within the area of BA-39 and also in a potential borrow source area within the Mississippi River. BA-39 is located within the northeast portion of the alignment of the Long Distance Sediment Pipeline project. Eustis performed 3 soil borings along the Mississippi River bank in a potential borrow source area and 5 soil borings within the BA-39 area. The Eustis boring locations within BA-39 are shown on the Plan of Borings and CPTs on Plate 1. The boring logs from the Eustis report along with their plan of borings are presented in Appendix D.

Eustis performed settlement analyses of the containment dikes constructed to contain the marsh fill material as it is placed and the marsh fill material itself, in addition to the settlement of the underlying subsoils.

2.2 URS Corporation Report (Project No. 19228956, dated July 23, 2009)

URS Corporation (URS) conducted a geotechnical investigation within the BA-48 area adjacent to Bayou DuPont. The location of Bayou DuPont is shown on the Plan of Borings and CPTs on Plate 1. URS performed 9 soil borings within the BA-48 area. The URS soil boring locations within BA-48 are shown within the Plan of Borings and CPTS on Plate 1. The boring logs from the URS report are presented in Appendix D.

URS performed settlement analyses of the containment dikes and the marsh fill material. In addition, they also performed slope stability analyses of the containment dikes to evaluate stable side slopes.





2.3 BA-39 Data

The BA-39 marsh creation area was constructed between November 2009 and April 2010. The BA-39 marsh fill area is located in the northeast portion of the project location as shown on the Plan of Borings and CPTs on Plate 1. Sand was pumped from the Mississippi River to the BA-39 area to create the marsh.

Five settlement plates were placed on the natural mudline prior to the placement of the fill material. The locations of the settlement plates are shown on Plate 26. The elevations of the settlement plates were surveyed every one to two weeks during the construction process between November 1, 2009 and April 25, 2010. Moffatt and Nichol also provided information related to the end of construction of each cell within BA-39. Based on the settlement plate survey data and the dates of the end of construction of each cell, the underlying soils appear to have consolidated between 0.2-to 1-ft during the construction of BA-39.

Moffatt and Nichol also provided post-construction topographic survey information of the ground surface after completion of BA-39. The last date of the post-construction survey provided by Moffatt and Nichol was in April 2010. In April 2010, the ground surface within BA-39 appeared to be between El. +2.0 and El. +2.5. John Chance Land Surveys, Inc., a Fugro company, obtained recent topographic information within the BA-39 area on October 10, 2011, for LDNR Contract No. 2503-11-65, Task No. 9. Based on the recent topographic data, the current elevation within BA-39 is on the order of El. +1.6-ft to El. +1.8-ft. Using the topographic data provided by Moffatt and Nichol and John Chance Land Surveys, Inc., total settlement experienced by the sand fill material and the underlying soils is on the order of 0.2-ft to 0.9-ft between April 2010 and October 10, 2011. This information was used to calibrate our settlement analyses discussed later.





3.0 FIELD EXPLORATION

Based on a review of the existing survey and geotechnical information in Section 2.0, we developed a field exploration program to supplement the available data and obtain enough subsurface information suitable for design. Our field activities are discussed in this section. We have included discussions of drilling methods and boring/CPT locations, soil sampling methods, Cone Penetration Testing, water depth observations, and borehole and CPT completion.

3.1 Drilling Methods and Boring/CPT Locations

Our overall field exploration program consisted of a total of 10 soil borings to a depth of approximately 40 ft each below the mudline and 8 soil borings to a depth of approximately 60 ft each below the mudline. In addition, we also performed 10 Cone Penetration Tests (CPT) to a depth of approximately 40 ft each below the mudline, 5 CPTs to a depth of approximately 60 ft each below the mudline and 9 CPTs to a depth of approximately 10 ft each below the mudline.

The borings and CPTs were performed between August 17 and September 14, 2011. The borings and CPTs were performed in a marsh environment west of the Backwater Levee, east of the Barataria Waterway, and south of The Pen. The soil borings were drilled using our skid drilling equipment mounted to a marsh buggy using wet-rotary drilling techniques.

The approximate boring locations are presented in the Plan of Borings and CPTs on Plate 1. The soil boring locations were selected by Fugro and Moffatt and Nichol. Moffatt and Nichol provided proposed coordinates of the boring locations. T. Baker Smith staked the borings in the field prior to our drill crew's mobilization. It should be noted that location boring and CPT location 17 was moved approximately 1,000 ft to the east of its original location due to shallow pipelines in the vicinity that our drilling equipment would have to cross to access the original location. A list of the boring/CPT locations in each Phase and their depths is presented in the following table.

<u>Location</u>	Boring Depth	CPT Depth
1		40-ft
2		40-ft
3	60-ft	60-ft
4		40-ft
5	40-ft	
6		40-ft
7	60-ft	60-ft
8		40-ft
9	40-ft	
10		40-ft





Location	Boring	СРТ
11	40-ft	<u></u>
12	40-ft	
13	40-ft	
14		40-ft
15	40-ft	
16		40-ft
17	60-ft	60-ft
18	40-ft	
19	40-ft	
26	60-ft	60-ft
27		40-ft
28	60-ft	60-ft
29		40-ft
30		10-ft
32		10-ft
34		10-ft
35		10-ft
36		10-ft
37		10-ft
38	60-ft	
39		10-ft
40	40-ft	
41	60-ft	
42	40-ft	
43	60-ft	

We have presented the boring logs on Plates 2 through 19. A key to the terms and symbols used on our boring logs is presented on Plates 20a and 20b.

3.2 Soil Sampling Methods

Soil samples were generally taken at about 2-ft intervals to a depth of about 20-ft. Below the depth of continuous sampling, soil samples were taken at 5-ft intervals to the completion depth of the borings as indicated on the boring logs. Undisturbed samples of cohesive soils were obtained by hydraulically pushing a 3-inch-diameter, thin-walled tube a distance of about 24-inches. Our field procedure for cohesive soil sampling was conducted in general accordance with the *Standard Practice for Thin-Walled Tube Sampling of Soils* (ASTM D 1587). The thin-walled tubes were capped and sealed in the field and then transported back to our laboratory in the vertical position.





The samples were extruded in our laboratory and visually classified by one of our senior geotechnical personnel.

Our field procedure for sampling granular soils was conducted in general accordance with the *Standard Method for Penetration Test and Split-Barrel Sampling of Soils* (ASTM D 1586). Granular soil samples were obtained using the Standard Penetration Test (SPT) as described on Plate 20b. A manual hammer was used to obtain the hammer blows for each SPT. Our geotechnical personnel recorded the hammer blows for each sampling interval. The uncorrected SPT N-values are recorded on the boring logs. The soil samples obtained from the split-barrel sampler were visually classified and packaged for transportation to our laboratory.

3.3 Cone Penetration Testing

The CPT soundings were conducted using our skid-mounted CPT unit mounted on a marsh buggy that uses the weight of the marsh buggy to push a cylindrical steel probe into the ground. We obtained CPT data by pushing a series of cylindrical rods with an instrumented probe at the base into the soil at a constant rate¹. The probe consists of a cone tip element and a side friction sleeve element. Continuous measurements of penetration resistance at the cone tip and friction on the friction sleeve were recorded during the penetration. Continuous measurements of pore pressure were also made and recorded. CPT field data were saved on computer diskettes for further data reduction in the office.

The location of the CPTs can be found on the Plan of Borings and CPTs located on Plate 1. The CPT results will be correlated with the results of our borings.

The CPT logs are presented in Appendix C. A key identifying the terms and symbols used on the CPT logs and the generalized classification chart utilized for data reduction of the test results are also presented at the beginning of Appendix C.

3.4 Water Depth Observations

The soil borings and CPTs were performed in a marsh environment. Most of the boring/CPT locations were performed in the water; however, some were performed above the water level on the marsh. The approximate depth to the mudline for the exploration locations below the water surface at the time of our field operations varied between about 1.1- to 4.0-ft. The approximate depth of water at the boring/CPT locations is presented on the boring/CPT logs.

It should be noted that the water depth measurements are intended for the purpose of the geotechnical investigation only, and are not corrected for tidal or other variations. If utilized for



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¹ Jean Louis Briaud and Jerome Miran, <u>The Cone Penetrometer Test</u>, Report to the Federal Highway Administration, Report No. FHWA-SA-91-043, February 1992.



other purposes, the water depth measurements should be adjusted to account for meteorological tide and datum corrections.

3.5 Borehole and CPT Completion

The borings and CPTs for this study were backfilled upon completion with cement-bentonite grout. We grouted the boreholes from the bottom up. When grout returned to the surface, we topped off each borehole by pouring grout from the surface.





4.0 LABORATORY TESTING

The laboratory-testing program for this study was directed toward evaluating the classification properties, undrained shear strength, and compressibility characteristics of the subsurface soils. Our laboratory tests were performed in general accordance with the appropriate ASTM standards as tabulated in this section.

4.1 Classification Tests

The classification tests included tests for natural moisture content, liquid and plastic limits (collectively termed Atterberg Limits), particle size distribution, percent passing a single sieve, and organic content. These tests aid in classifying the soils and are used to correlate the results of other tests performed on samples taken from different borings and/or different depths. The results of the classification tests are presented on the boring logs on Plates 2 through 19. The particle size analyses are presented on Plates 21a through 21f.

4.2 Undrained Shear Strength Tests

We measured the undrained shear strength of select undisturbed samples of cohesive soils by performing undisturbed and remolded miniature vane shear tests and undisturbed unconsolidated-undrained triaxial compression tests. Miniature vane shear tests were generally performed on each cohesive sample prior to extrusion. Natural moisture contents and dry unit weights were determined as routine portions of the compression tests. The results of the undisturbed shear strength tests are presented on the boring logs on Plates 2 through 19. The results of the undisturbed and remolded shear strength tests are presented in the Summary of Test Results in Appendix A.

4.3 One-Dimensional Consolidation Testing

We measured the compressibility characteristics of the soils along the proposed ridge alignment by performing 27 incremental one-dimensional consolidation tests. Undisturbed soil samples from various soil borings were selected at depths ranging from 3-ft to 54-ft below existing grade for consolidation testing. Natural moisture contents and dry unit weights were determined as routine portions of the consolidation tests. The consolidation test reports are presented in Appendix B. A summary of the consolidation test results is presented in the table on the following page.





Summary of Consolidation Test Results

Boring No.	Depth (ft)	e ₀	Сс	Cr	σ' _v (tsf)	σ' _p (tsf)	OCR
B-3	15.0	1.11	0.30	0.07	0.33	0.44	1.3
B-3	29.0	1.80	0.68	0.12	0.60	0.64	1.1
B-5	7.0	1.77	0.53	0.12	0.18	0.23	1.3
B-5	19.0	0.99	0.14	0.02	0.50	0.68	1.4
B-7	3.0	3.13	1.87	0.23	0.03	0.03	1.0
B-7	29.0	2.14	1.12	0.19	0.51	0.70	1.4
B-9	3.0	6.07	1.95	0.32	0.03	0.03	1.0
B-11	9.0	6.83	2.24	0.43	0.03	0.06	2.0
B-12	7.0	7.07	2.68	0.43	0.03	0.03	1.0
B-13	17.0	2.63	0.66	0.13	0.15	0.15	1.0
B-15	5.0	0.90	0.18	0.02	0.11	0.45	4.1
B-15	24.0	2.59	1.26	0.26	0.60	1.00	1.7
B-17	17.0	1.00	0.22	0.03	0.45	0.95	2.1
B-17	54.0	1.62	0.60	0.11	1.40	1.40	1.0
B-18	7.0	1.73	0.58	0.15	0.05	0.40	8.0
B-19	7.0	1.27	0.26	0.03	0.08	0.14	1.8
B-26	7.0	3.01	0.93	0.29	0.08	0.18	2.3
B-28	7.0	1.74	0.39	0.03	0.09	0.09	1.0
B-28	13.0	2.19	0.70	0.16	0.21	0.17	0.8
B-28	54.0	1.40	0.57	0.12	1.20	1.35	1.1
B-38	3.0	3.23	1.21	0.25	0.03	0.03	1.0
B-38	19.0	1.51	0.35	0.05	0.35	0.40	1.1
B-40	13.0	2.49	0.76	0.12	0.14	0.14	1.0
B-41	24.0	1.71	0.47	0.09	0.25	0.40	1.6
B-42	11.0	5.50	2.60	0.34	0.07	0.07	1.0
B-43	3.0	4.85	1.16	0.25	0.03	0.03	1.0
B-43	19.0	4.15	1.15	0.28	0.20	0.20	1.0

 e_0 = initial void ratio

 σ'_{v} = effective overburden pressure

 C_c = compression index

 $\sigma^{\prime}_{\ p}$ = effective preconsolidation pressure

 C_r = recompression index

OCR = overconsolidation ratio





4.4 Summary of Laboratory Testing

The laboratory tests were conducted in accordance with the procedures described in the table below. The results of our laboratory tests are presented on the boring logs on Plates 2 through 19 and also in the Summary of Test Results in Appendix A.

Type of Test	Test Designation
Moisture Content	ASTM D 2216
Atterberg Limits	ASTM D 4318
Particle Size Distribution	ASTM D 6913
Material Finer than a No. 200 Sieve	ASTM D 1140
Organic Content	ASTM D 2974
Miniature Vane Shear (undisturbed and remolded)	ASTM D 4648
Unconsolidated-Undrained Triaxial Compression	ASTM D 2850
One-Dimensional Consolidation	ASTM D 2435





5.0 GENERALIZED SUBSURFACE CONDITIONS

The generalized subsurface soil conditions based on the results of our soil borings and Cone Penetration Test soundings are discussed in the following sections. Soil borings and CPTs within each soils reach were grouped based on similarities in stratigraphy and undrained shear strength. In summary, three distinct profiles were delineated along the alignment. The three soil profiles were designated Soils Reach 1, 2 and 3. The borings and CPTs included in each soils reach are defined in the table below.

Soils Reach	<u>Borings</u>	<u>CPTs</u>
1	B-3, B-5, B-7, B-38, and B-40	CPT-1, CPT-2, CPT-3, CPT-4, CPT-6,
		CPT-7, CPT-8, CPT-30, and CPT-39
2	B-9, B-11, B-12, B-13, B-19, B- 26, B-28, B-41, and B-42	CPT-10, CPT-26, CPT-27, CPT-28, and CPT-29
3	B-15, B-17, B-18, and B-43	CPT-14, CPT-16, and CPT-17

5.1 Soils Reach 1

Soils Reach 1 includes the portion of the pipeline alignment extending west of the backwater levee and east of Bayou DuPont and south of the Chenier Traverse Bayou as depicted on the Plan of Borings and CPTs. A generalized cross-section of the borings and CPTs included in Soils Reach 1 is presented on Plate 22.

Based on our field observations and the results of our laboratory testing and CPT interpretation, we classified the subsurface soils as mostly cohesive. Sand was found in the upper 3- to 7-ft of Borings B-3 and B-5 and CPT-1, CPT-2, CPT-3, CPT-4, CPT-30, and CPT-39. At CPT-6 and CPT-32, little to no sand fill was detected. We have assumed the sand to be fill material that was placed during the construction of BA-39. Based on grain size distributions performed on samples of the sand material obtained from Borings B-3 and B-5, the fill material is composed of poorly graded sand (SP).

The native soils beneath the sand fill consist primarily of fat and lean clay materials with organic clays and peat within the upper 4- to 5-ft. A layer of silty sand was encountered between El. -30-ft- and -40-ft in Boring B-38.





5.2 Soils Reach 2

Soils Reach 2 was designated to be the portion of the pipeline alignment extending south of Bayou DuPont and a portion of the Option B pipeline alignment as shown on the Plan of Borings and CPTs. The boring and CPT locations included in Soils Reach 2 are B-9, CPT-10, B-11, B-12, B-13, B/CPT-26, CPT-27, B/CPT-28, CPT-29, B-41, B-42, and B-19. Boring B-19 is actually located closer to Soils Reach 3; however, the soil conditions and strength parameters encountered in Boring B-19 are more similar to the borings included in Soils Reach 2. Therefore Boring B-19 was included in our analyses for Soils Reach 2. A generalized cross-section of the borings and CPTs included in Soils Reach 2 is presented on Plates 23 and 24.

Based on our field observations and the results of our laboratory testing and CPT interpretation, we would classify the subsurface soils as mostly cohesive material. The soils consist mostly of fat and lean clays with organic clay and peat found within the upper 4- to 14-ft of our soil borings. Silty sand was encountered in Boring B-9 between El. -26-ft and -41-ft and in Boring B-28 between El. -31-ft and -41-ft. Sand pockets were also observed in Boring B-26 between El. -41-ft and -48-ft. CPT-26, CPT-27, and CPT-28 also indicated sand between El. -29-ft and -50-ft.

5.3 Soils Reach 3

Soils Reach 3 was designated to be the portion of the pipeline alignment extending to the west of Boring B-13, as shown on the Plan of Borings and CPTs. The boring and CPT locations included in Soils Reach 3 are CPT-14, B-15, CPT-16, B/CPT-17, B-18, B-19, and B-43. A generalized cross-section of the borings and CPTs included in Soils Reach 3 is presented on Plate 25.

Based on our field observations and the results of our laboratory testing and CPT interpretation, we would classify the subsurface soils as mostly cohesive material. The soils consist mostly of fat and lean clays. Organic clay and peat were observed within the upper 4- to 7-ft of Borings B-18 and B-43, which were located to the north of the proposed pipeline alignment. The rest of the borings in Soils Reach 3 indicated more lean clay as compared to the borings in Soils Reaches 1 and 2.

5.4 Design Soil Strength Parameters

Design undrained shear strength and unit weight profiles were developed for each soils reach based upon the results of the laboratory tests performed on samples from the soil borings along with cone penetration tests (CPT).

For the CPT data, site correlations have indicated that dividing the CPT tip resistance by a Nc factor of 20 correlates well with unconsolidated undrained triaxial shear tests. Therefore, combined plots of undrained shear strength versus elevation based on a Nc factor of 20 are presented on the design shear strength plots. Results of laboratory shear strength tests and unit





weights from undisturbed borings performed for this study are plotted for the various soils reaches on Plates 28 through 30.

5.5 Design Soil Compressibility Parameters

Soil compressibility parameters for design were developed using the 27 consolidation tests performed for this study. The results of the consolidation tests are discussed in Section 4.3. After reviewing the consolidation data, we determined in our analyses that the soil strata are normally consolidated and will compress along a "virgin" compression line (OCR = 1). Site-specific correlations for the compressibility index, C_c , as it relates to moisture content and liquid limit were generated based on all of the consolidation tests performed. We then plotted moisture content and liquid limit profiles for each Soils Reach and developed compressibility profiles for each soils reach.

In an effort to evaluate the time rate of settlement, we estimated the coefficient of consolidation (c_v) values from the consolidation tests and adjusted these values to match the historical data for BA-39 as discussed in the Settlement Analyses section of this report. Some of our soil borings and CPTs, especially those in Soils Reach 2, encountered layers of silty sand and poorly graded sand below a depth of about 20-ft. These sand layers will not compress as much as clay layers. As such, we neglected the presence of these sand layers in our analyses to provide a conservative estimate of settlement. In addition, these sand layers would behave as a drainage layer beneath the upper cohesive soils. The presence of a sand layer beneath the cohesive material would decrease the drainage path within the cohesive layer above and increase the rate of consolidation within the cohesive material.

As part of our consolidation testing program, some of the tested soil specimens were selected from Borings B-3 and B-5, which were performed within the formerly constructed BA-39 area. As previously mentioned, fill material was placed within the BA-39 area between November 2009 and April 2010. To develop our compressibility design profile within Soils Reach 1, the consolidation data from Borings B-3 and B-5 were considered in addition to the other borings within Soils Reach 1; however, we neglected any effects of consolidation from the application of the fill material.

In addition, we understand that the containment dikes within Soils Reach 1 will be constructed by excavating in-situ material from the interior of the footprint of the pipeline access corridor. The borrow excavation will be backfilled with the same sand fill material used to construct the pipeline access corridor. We anticipate the borrow excavation may extend to a depth of approximately 8-ft assuming a cut-to-fill ratio for the containment dikes of approximately 2.5:1.0. We understand the borrow excavation may extend to within 25-ft of the containment dike toes in the footprint of the pipeline access corridor. Therefore, most of the highly organic materials encountered in the upper 10-ft of our soil borings and CPTs will be removed and replaced with less compressible poorly graded sand. We evaluated the settlement of the pipeline access corridor fill material and foundation soils assuming the sand fill extended to EI. -9-ft. We also evaluated the settlement of





the pipeline access corridor fill material and foundation soils outside of the borrow excavation and the containment dikes assuming the in-situ compressible organic material was present.

We encountered a thick layer of organic clay and peat within the upper 20-ft of Borings B-42 and B-43 in the Marsh Creation Area. The Marsh Creation Area lies to the west of Soils Reach 2. The thick layer of organic material within the upper 20-ft of the Marsh Creation Area will compress more than the soils encountered within Soils Reach 2. To evaluate the range in compression that will occur in the March Creation Area, we evaluated the compressibility using both the compressibility profile defined for Soils Reach 2 and the more conservative profile based on Borings B-42 and B-43.

Soils Reach 1: Compressibility Parameters

Bottom of	Generalized			
Layer	Soil		C_{v} ,	
Elevation, ft	Classification	C_c	C _v , ft²/day	e _o
-3.0	Peat	1.50	0.06	3.20
-38.0	Fat Clay	0.35	0.20	1.50
-58.0	Fat Clay	0.68	0.20	1.80

C_c = Coefficient of Compression

C_v = Coefficient of Consolidation

 e_0 = in situ initial void ratio

Note: The settlement analyses of the section of the pipeline access corridor in the vicinity of the borrow excavation assumed poorly graded sand was present from the mudline to El. -9-ft. We assumed the poorly graded sand was incompressible in our settlement analyses.

Soils Reach 2: Compressibility Parameters

Bottom of	Generalized					
Layer	Soil		C_{v} ,			
Elevation, ft	Classification	C_c	ft ² /day	e _o		
-7.0	Peat	2.00	0.06	5.50		
-30.0	Fat Clay	0.34	0.20	2.40		
-45.0	Fat Clay	0.47	0.20	1.72		
-60.0	Fat Clay	0.34	0.20	1.40		
1						

C_c = Coefficient of Compression

 C_v = Coefficient of Consolidation

e_o = in situ initial void ratio





Soils Reach 3: Compressibility Parameters

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Bottom of	Generalized				
Layer	Soil		C_{v} ,		
Elevation, ft	Classification	C_c	ft²/day	e _o	
-7.5	Peat	0.47	0.003	1.35	
-25.0	Fat Clay	0.29	0.03	1.00	
-32.5	Fat Clay	0.56	0.03	1.62	
-36.0	Fat Clay	0.34	0.03	1.50	
-60.0	Fat Clay	0.51	0.03	1.60	

 C_c = Coefficient of Compression

 C_v = Coefficient of Consolidation

 e_o = in situ initial void ratio

Marsh Creation Area: Compressibility Parameters (Based on B-42 and B-43)

Bottom of	Generalized			
Layer	Soil		C _v ,	
Elevation, ft	Classification	C_c	C _v , ft²/day	e _o
-15.0	Peat	2.00	0.003	5.5
-22.5	Organic Clay	1.40	0.003	4.5
-60.0	Fat Clay	0.62	0.030	2.0

 C_c = Coefficient of Compression

 C_v = Coefficient of Consolidation

e_o = in situ initial void ratio





6.0 PROJECT FEATURES

Preliminary cross-sections for the design of the sediment pipeline corridor have been provided by Moffatt and Nichol throughout the course of our study. The most recent versions of these drawings at the time of this report are included in Appendix E.

We understand temporary containment dikes will be constructed along the portion of the access corridor between BA-39 and Bayou DuPont to contain the fill material as it is placed (see Cross-section 2 in Appendix E). In addition, a containment dike is also planned along the eastern edge of the access corridor adjacent to the existing canal for the section of the alignment south of the fish camp (see Cross-section 5 in Appendix E). We assumed the crown of the containment dike would be constructed to an elevation 1-ft above the adjacent access corridor fill material at the time of construction. Current plans have the containment dikes constructed of in-situ material excavated from the near-surface materials.

Subsequent to forming the containment dikes, sediment from the Mississippi River will be pumped to create the marsh platform along the pipeline access corridor alignment. In addition, an area adjacent to the pipeline corridor has been targeted for additional marsh creation.

We understand that the containment dikes along the access access corridor between BA-39 and Bayou DuPont will be degraded to an inclination of 20 Horizontal to 1 Vertical after construction of the access corridor (see Cross-section 2 in Appendix E). In addition, the section of the access corridor between Bayou DuPont and the fish camp, the western edge of the corridor south of the fish camp, and the marsh creation fill material will be constructed with a slope of approximately 20 Horizontal to 1 Vertical (see Cross-sections 4, 5, and 6 in Appendix E).

A brief discussion of the scope of engineering for each area of the project is included below.

6.1 Containment Dikes

Containment dikes will be constructed to contain the pipeline corridor fill material as it is placed along segments of the pipeline corridor. The final design of the containment dikes should consider the desired final elevation, side slopes, and crest width, which is based on the properties of the proposed material used for the construction of the containment dikes. The design should account for expected consolidation during construction, and the time needed for settlement to occur. For our analyses, we generated the following for the containment dikes:

- Time-settlement curves during construction;
- Short-term slope stability of the proposed side-slope inclinations;
- Cut to fill ratio for construction; and





Construction sequence and recommendations

6.2 Pipeline Access Corridor and Adjacent Marsh Apron Fill Area

Hydraulically pumped borrow fill material from the Mississippi River will be placed within the containment dikes to create the pipeline access corridor and adjacent marsh apron. We have assumed that the material will be similar to the sand placed to create the BA-39 area. The following analyses were performed relative to the pipeline access corridor and marsh apron fill area:

- Time-settlement curves over the 20 year project life to meet certain elevation criteria including self-weight compression of the sand fill along with settlement of the underlying soils;
- Slope stability of the side slopes of the pipeline access corridor; and
- Cut to fill ratio for construction.

6.3 Additional Marsh Creation Fill Area

Hydraulically pumped borrow fill material from the Mississippi River will be placed in areas adjacent to the pipeline access corridor to create additional marsh restoration area. At the time of this report, the area to the west of Soils Reach 2 near Boring locations B-42 and B-43 were evaluated for additional marsh creation. The following analyses were performed relative to marsh creation area.

- Time-settlement curves over the 20 year project life to meet the elevation criteria set by Moffatt and Nichol including self-weight compression of the sand fill along with settlement of the underlying soils; and
- Cut to fill ratio for construction.

The analyses associated with the project features are discussed in the following sections. The results of our settlement analyses are discussed in Section 7.0, the results of our slope stability analyses are discussed in Section 8.0 and Construction Considerations are included in Section 9.0.





7.0 SETTLEMENT ANALYSES

Settlement analyses for the site were performed using the computer program Settle^{3D} developed by RocScience. Settle^{3D} uses Boussinesq's theory to compute stresses within the in-situ material under applied loads. The program then uses soil compressibility parameters to evaluate the change in thickness of individual layers and computes the overall movement at select locations. Settle^{3D} was used to compute the settlement of the in-situ material due to the application of the fill material for the containment dikes and the pipeline corridor fill material. We have presented a discussion of our settlement models and results in the following sections.

7.1 Settlement Models

For design purposes, we assigned the elevation of the water in the marsh to be at EI. +0.5-ft, which is the mean low water level provided by Moffatt and Nichol. By using the mean low water level in our analyses, loads applied to the native soils by the fill material are more conservative than those computed using the mean sea level and the mean high water level. The current plan is to construct the pipeline corridor and marsh creation areas with the same material used to construct BA-39. Therefore, we assumed the placed fill material for the pipeline corridor will consist of poorly graded sand with an approximate total unit weight of 105 pcf. We understand the perimeter containment dikes will be constructed by excavating material along the centerline of the alignment. Accordingly, the containment dikes will be constructed of the organic clays and peat found in the upper strata of our soil borings. We assumed the containment dike material will have a total unit weight after placement of about 85 pcf. The soil compressibility profiles for each Soils Reach are included in Section 5.5.

Based on our understanding that the access corridors will be constructed of poorly graded sand, the majority of the self-weight compression of the sand material will occur during the construction process. We have estimated the self-weight compression of the fill material to be on the order of 2 to 3% of the fill height at the end of construction.

Moffatt and Nichol provided typical preliminary cross-sections of the pipeline access corridor and containment dikes. We evaluated the various cross-sections using the compressibility profile for the soils reach in which the cross-section is planned to be constructed. Moffatt and Nichol provided a range of mudline elevations within each soils reach. We evaluated the settlement using an upper and lower bound mudline elevation within each soils reach. The assumed mudline elevations evaluated for each soils reach are presented in the following table.





	Assumed Upper-	Assumed Lower-
	bound Mudline	bound Mudline
Soils Reach	Elevation, ft	Elevation, ft
1	+1.0	-1.0
2	+1.0	-2.0
3	+1.0	-2.5

Based on the parameters above, we evaluated various fill thicknesses for the pipeline access corridor to determine the minimum elevation needed to meet the long-term elevation criteria. We made the following assumptions about the construction process in developing our models:

- containment dikes would be constructed to an elevation 1-ft above the top of the pipeline access corridor at the end of construction;
- containment dikes would be constructed approximately two weeks prior to placement of the pipeline access corridor fill material
- pipeline access corridor fill material would be placed in less than or equal to seven days at a specific location;
- process survey would be conducted within approximately 30 days following the completion of fill placement; and
- the period of time between the beginning of placement of the pipeline access corridor fill material and the process survey was considered to be the duration of construction.

7.2 Settlement Analyses of the Pipeline Corridor and Containment Dikes

Moffatt and Nichol provided settlement criteria for the pipeline access corridor fill material as presented in the table below.

Years after	Target Design Elevation of Access
Construction	Corridor and Marsh Fill Material
5	+1.3-ft
20	+0.5- to +0.9-ft

We evaluated the settlement of the pipeline access corridor and the containment dikes using the upper- and lower-bound mudline elevations presented in the table in Section 7.1. The containment dikes were designed so that the crown of the dike was approximately 1-ft above the top elevation of the pipeline access corridor fill material at the end of construction. The results of our settlement analyses for the access corridor fill material and the containment dikes are presented in the





following tables. Plots of top of fill elevation versus time for the pipeline corridor fill material and the containment dikes are presented on Plates 31 through 35.





Soils Reach 1: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Lower-bound mudline at El. -1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
3.0	+2.0	0.41	3.41	0.20	0.11	0.72	+1.69	1.09	1.37	+0.60	+0.32
3.5	+2.5	0.44	3.94	0.22	0.12	0.78	+2.14	1.21	1.53	+0.93	+0.61
4.0	+3.0	0.47	4.47	0.22	0.14	0.83	+2.64	1.31	1.69	+1.33	+0.95

Soils Reach 1: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
1.0	+2.0	0.14	1.14	0.06	0.04	0.24	+1.90	0.60	0.92	+1.30	+0.98
1.5	+2.5	0.18	1.68	0.08	0.05	0.31	+2.37	0.77	1.20	+1.60	+1.17
2.0	+3.0	0.21	2.21	0.10	0.07	0.38	+2.84	0.91	1.41	+1.93	+1.43

Soils Reach 1: Settlement of Access Corridor and Marsh Apron Fill Material (borrow excavation to El. -9.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
3.0	+2.0	0.02	3.02	0.03	0.33	0.38	+1.64	0.20	0.36	+1.44	+1.28
3.5	+2.5	0.02	3.52	0.03	0.35	0.40	+2.12	0.25	0.43	+1.87	+1.69
4.0	+3.0	0.02	4.02	0.04	0.36	0.42	+2.60	0.28	0.50	+2.32	+2.10





Soils Reach 2: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Lower-bound mudline at El. -2.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
4.0	+2.0	0.36	4.36	0.17	0.14	0.67	+1.70	1.28	1.82	+0.42	-0.12
5.0	+3.0	0.43	5.43	0.18	0.17	0.78	+2.64	1.48	2.13	+1.16	+0.51
5.5	+3.5	0.42	5.92	0.20	0.18	0.80	+3.12	1.52	2.18	+1.60	+0.94

Soils Reach 2: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

				Settlement of			•				
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
1.0	+2.0	0.12	1.12	0.05	0.04	0.21	+1.91	0.52	0.92	+1.39	+0.99
1.5	+2.5	0.16	1.66	0.07	0.05	0.28	+2.38	0.69	1.19	+1.69	+1.19
2.0	+3.0	0.17	2.17	0.07	0.07	0.31	+2.86	0.74	1.32	+2.12	+1.54

Soils Reach 3: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Lower-bound mudline at El. -2.5-ft)

				Settlement of	_	•					
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
4.5	+2.0	0.26	4.76	0.12	0.15	0.53	+1.74	1.00	1.72	+0.74	+0.02
5.0	+2.5	0.27	5.27	0.13	0.16	0.56	+2.22	1.06	1.83	+1.16	+0.39
5.5	+3.0	0.28	5.78	0.13	0.18	0.59	+2.70	1.14	2.02	+1.56	+0.68





Soils Reach 3: Settlement of Access Corridor and Marsh Apron Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
1.0	+2.0	0.08	1.08	0.04	0.03	0.15	+1.93	0.35	0.65	+1.58	+1.28
1.5	+2.5	0.11	1.61	0.04	0.05	0.20	+2.41	0.45	0.85	+1.96	+1.56
2.0	+3.0	0.12	2.12	0.05	0.07	0.24	+2.89	0.53	1.03	+2.36	+1.86

Soils Reach 1: Settlement of Containment Dike Fill Material (assumed Lower-bound mudline at El. -1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
4.5	+3.5	0.44	4.94	0.27	0.52	1.23	+2.71	1.11	1.32	+1.60	+1.39
5.0	+4.0	0.48	5.48	0.26	0.57	1.31	+3.17	1.16	1.40	+2.01	+1.77
5.5	+4.5	0.53	6.03	0.27	0.63	1.43	+3.61	1.29	1.58	+2.32	+2.03

Soils Reach 1: Settlement of Containment Dike Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
2.0	+3.0	0.21	3.21	0.09	0.23	0.53	+2.68	0.73	1.08	+1.95	+1.60
2.5	+3.5	0.23	2.73	0.11	0.28	0.62	+3.11	0.84	1.25	+2.27	+1.86
3.0	+4.0	0.25	3.25	0.12	0.34	0.71	+3.54	0.94	1.40	+2.60	+2.14





Soils Reach 2: Settlement of Containment Dike Fill Material (assumed Lower-bound mudline at El. -2.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
6.0	+4.0	0.43	6.43	0.24	0.67	1.34	+3.09	1.41	1.93	+1.68	+1.16
6.5	+4.5	0.45	6.95	0.25	0.72	1.42	+3.53	1.48	2.03	+2.05	+1.50
7.0	+5.0	0.46	7.46	0.24	0.77	1.47	+3.99	1.49	2.05	+2.50	+1.94

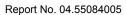
Soils Reach 2: Settlement of Containment Dike Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

							<u> </u>				
				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
2.0	+3.0	0.18	2.18	0.08	0.23	0.49	+2.69	0.66	1.09	+2.03	+1.60
2.5	+3.5	0.20	2.70	0.09	0.28	0.57	+3.13	0.81	1.28	+2.32	+1.85
3.0	+4.0	0.21	3.21	0.11	0.33	0.65	+3.56	0.88	1.44	+2.68	+2.12

Soils Reach 3: Settlement of Containment Dike Fill Material (assumed Lower-bound mudline at El. -2.5-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
6.0	+3.5	0.26	6.26	0.15	0.64	1.05	+2.71	0.94	1.48	+1.77	+1.23
6.5	+4.0	0.26	6.76	0.16	0.69	1.11	+3.15	0.97	1.56	+2.18	+1.59
7.0	+4.5	0.28	7.28	0.15	0.74	1.17	+3.61	0.99	1.57	+2.62	+2.04







Soils Reach 3: Settlement of Containment Dike Fill Material (assumed Upper-bound mudline at El. +1.0-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
2.0	+3.0	0.11	2.11	0.05	0.22	0.38	+2.73	0.40	0.73	+2.33	+2.00
2.5	+3.5	0.12	2.62	0.06	0.27	0.45	+3.17	0.47	0.86	+2.70	+2.31
3.0	+4.0	0.14	3.14	0.06	0.32	0.52	+3.61	0.53	0.96	+3.08	+2.65





7.3 Settlement of Marsh Creation Areas

In addition to the areas of the pipeline access corridor and containment dikes, Moffatt and Nichol also requested that we perform soil borings in an area of potential additional marsh creation, specifically in the area of borings B-42 and B-43. We performed settlement analyses for the marsh creation area using the compressibility profile developed from Soil Borings B-42 and B-43 and the Soils Reach 2 compressibility profile presented in Section 5.5. We believe the settlement computed using these two compressibility profiles will provide a range of anticipated settlement within the marsh creation area due to the varying soil conditions.

The settlement criteria for the marsh creation area are the same as that presented above in Section 7.2 for the pipeline access corridor fill material. The extent of the marsh creation area was unknown at the time of our analysis. We assumed an area 2,000-ft across to model the marsh creation area. The results of our settlement analysis for the marsh creation area are presented in the tables on the following page. Plots of top of fill elevation versus time for the marsh creation fill material are presented on Plate 36.





Marsh Creation Area: Settlement of Additional Marsh Creation Fill Material – Based on B-42 and B-43 (assumed mudline at El. -2.5-ft)

									,		
				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
6.0	+3.5	0.42	6.42	0.22	0.18	0.82	+3.08	1.76	3.04	+1.32	+0.04
6.5	+4.0	0.43	6.93	0.23	0.21	0.87	+3.55	1.85	3.17	+1.70	+0.38
7.0	+4.5	0.44	7.44	0.24	0.23	0.91	+4.02	1.93	3.32	+2.09	+0.70

Marsh Creation Area: Settlement of Additional Marsh Creation Fill Material – Using Soils Reach 2 Compressibility Profile (assumed mudline at El. -2.5-ft)

				Settlement of							
				Fdtn. Soils b/t		Total	Design Top		Foundation	Top of	Top of
Nominal	Top of Fill	Settlement		End of	Self-Weight	Settlement	of Fill El. At	Foundation	Settlement	Fill El.	Fill El.
Fill	El. at End of	During Fill	Actual Fill	Placement and	Compression	at End of	End of	Settlement	after 20	After 5	After 20
Thickness	Placement	Placement	Thickness	Process Survey	of Fill	Construction	Construction	after 5 years	years	years	years
feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet	feet
5.5	+3.0	0.40	5.90	0.22	0.18	0.80	+2.60	1.54	2.22	+1.06	+0.38
6.0	+3.5	0.42	6.42	0.22	0.20	0.84	+3.08	1.62	2.35	+1.46	+0.73
6.5	+4.0	0.43	6.93	0.23	0.21	0.87	+3.55	1.68	2.47	+1.87	+1.08





8.0 SLOPE STABILITY ANALYSES

Slope stability analyses were performed for the containment dikes and marsh fill areas to determine the factor of safety for the proposed design. Moffatt and Nichol provided typical cross-sections of the pipeline corridor and containment dikes along the pipeline alignment. The provided cross-sections that were used in our slope stability analyses are presented in Appendix E. We have described which cross-section was evaluated within each Soils Reach in the table below.

Cross-Section No. (see Appendix E)	Description of Section of Alignment Corresponding to Cross-Section	Design Parameters used in Analysis
2	Between BA-39 and Bayou DuPont	Soils Reach 1
4	From BA-48 to the Fish Camp (Sta. 470+28.82)	Soils Reach 2
5	From the Fish Camp to Barataria Waterway	Soils Reach 2 and 3
6	Additional Marsh Creation Area	Soils Reach 2

The factor of safety against stability failure is expected to increase with time as the underlying foundation material consolidates and gains strength, and after placing the dredged material. The analyses were performed using Slope/W Version 7.17 (GeoStudio, 2007). The factor of safety was determined using Spencer's (1967) method of slices where force and moment equilibrium is achieved for each slice in this method. We evaluated circular failure surfaces in our analyses.

8.1 Material Properties

We used the undrained shear strength and total unit weight profiles presented on Plates 28, 29, and 30 for our slope stability analyses. We assumed the containment dike material had a total unit weight of 85 pcf and an undrained shear strength of 80 psf. We assumed the pipeline corridor material and the marsh creation fill material consisted of poorly graded sand with a total unit weight of 105 pcf and an internal angle of friction of 30 degrees.

8.2 Stability Models

We understand temporary containment dikes will be constructed along the portion of the pipeline corridor between BA-39 and Bayou DuPont to contain the fill material as it is placed (see Crosssection 2 in Appendix E). In addition, a containment dike is also planned along the eastern edge of the pipeline corridor adjacent to the existing canal for the section of the alignment south of the fish camp (see Cross-section 5 in Appendix E). We evaluated the stability of the containment dikes assuming a 3 Horizontal to 1 Vertical side slope inclination and a crown width of 6-ft. In addition,





we assumed the crown of the containment dike would be constructed to an elevation 1-ft above the adjacent pipeline corridor fill material at the end of construction. Current plans have the containment dikes constructed of in-situ material excavated from the near-surface materials. We assumed a cut-to-fill ratio of approximately 2.5:1 for the containment dike material. Therefore, we assumed the bottom of the containment dike borrow excavation would be between approximately El. -9-ft to -11.5-ft depending on the existing mudline in the vicinity of the borrow area. We performed our stability analyses using the lower-bound mudline elevations evaluated in our settlement analyses for each soils reach. Using the lower-bound mudline elevations is a conservative approach for evaluating the stability of the containment dikes and pipeline corridor marsh apron as this would simulate fill placed at higher elevations than using the upper-bound mudline elevations. We assumed the containment dikes would be constructed to an elevation approximately 1-ft above the elevation of the pipeline access corridor fill material at the end of construction.

We understand that the containment dikes and fill along the pipeline corridor between BA-39 and Bayou DuPont will be degraded to an inclination of 20 Horizontal to 1 Vertical after construction of the pipeline corridor (see Cross-section 2 in Appendix E). In addition, the section of the access corridor and marsh apron between Bayou DuPont and the fish camp, the western edge of the corridor south of the fish camp, and the additional marsh creation fill material will also have side slopes of 20 Horizontal to 1 Vertical (see Cross-sections 4, 5, and 6 in Appendix E). We performed a stability analysis to evaluate the side slopes of the pipeline corridor using the appropriate design soil parameters for each cross-section.

8.3 Slope Stability Analysis Results

The results of our slope stability analyses for the various cross-sections and design soil parameters are summarized in the following table. The failure surfaces corresponding to the factors of safety presented in the following table are presented on Plates 37 through 43.





Soils Reach	Cross-Section (from Appendix E)	Description of Analysis	Side Slope Inclination	Elevation of Top	Factor of Safety
		Containment Dike			
1	2	adjacent to Borrow Area	3H:1V	+4.5	1.26
1	2	Pipeline Corridor	20H:1V	+3.0	2.99
		Containment Dike			
2	5	adjacent to Canal	3H:1V	+5.0	1.22
2	4	Pipeline Corridor	20H:1V	+3.5	1.72
		Containment Dike			
3	5	adjacent to Canal	3H:1V	+4.0	1.28
3	5	Pipeline Corridor	20H:1V	+3.0	4.39
2	6	Marsh Creation Area	20H:1V	+3.5	1.74

The reported factors of safety presented in the table above and on Plates 37 through 43, are above 1.2, which we believe is an acceptable factor of safety for the application of these structures. Factors of safety less than 1.2 were observed for shallow surficial slip surfaces. These shallow failure surfaces are more indicative of a localized bearing capacity failure and not a global slope stability failure.





9.0 CONSTRUCTION RECOMMENDATIONS

9.1 Containment Dike

The containment dike will be constructed from borrow material excavated and handled within the restoration area. The borrow material will likely be from the upper 10 feet and will comprise primarily of organic fat clays. Since the moisture content in the upper 10 feet ranged from 60 to over 200 percent, a moisture content of 125 percent was assumed to be a representative average value during dredging. Based on published values in similar material, we estimate the cut-to-fill ratio for dike construction for similar materials is in the range of 2.0 to 3.0:1.

In our stability model, a single-staged construction of the dike was assumed. However if the construction schedule permits, multiple-stage construction is preferred. This will significantly reduce possible displacements and shallow bearing capacity failures.

To reduce the potential of ponding of surface water on the containment dike, it is recommended that positive surface gradients be incorporated into the construction of the dike.

9.2 Access Corridor and Marsh Creation Fill Material

The borrow material for the fill area will be dredged from the Mississippi River. We have assumed that the material will be similar in consistency to that placed for BA-39.

We believe the volume of material required to fill the pipeline access corridor area will be approximately 1.2 to 1.5 times the initial calculated fill volume based on pre-construction survey data. The additional volume of material will need to be placed to accommodate potential shallow "mud waves" and settlement of the underlying native materials during construction prior to the process survey. As such, we recommend a cut to fill ratio between 1.2 to 1.5:1 be assumed for the borrow material.

9.3 Additional Construction Considerations

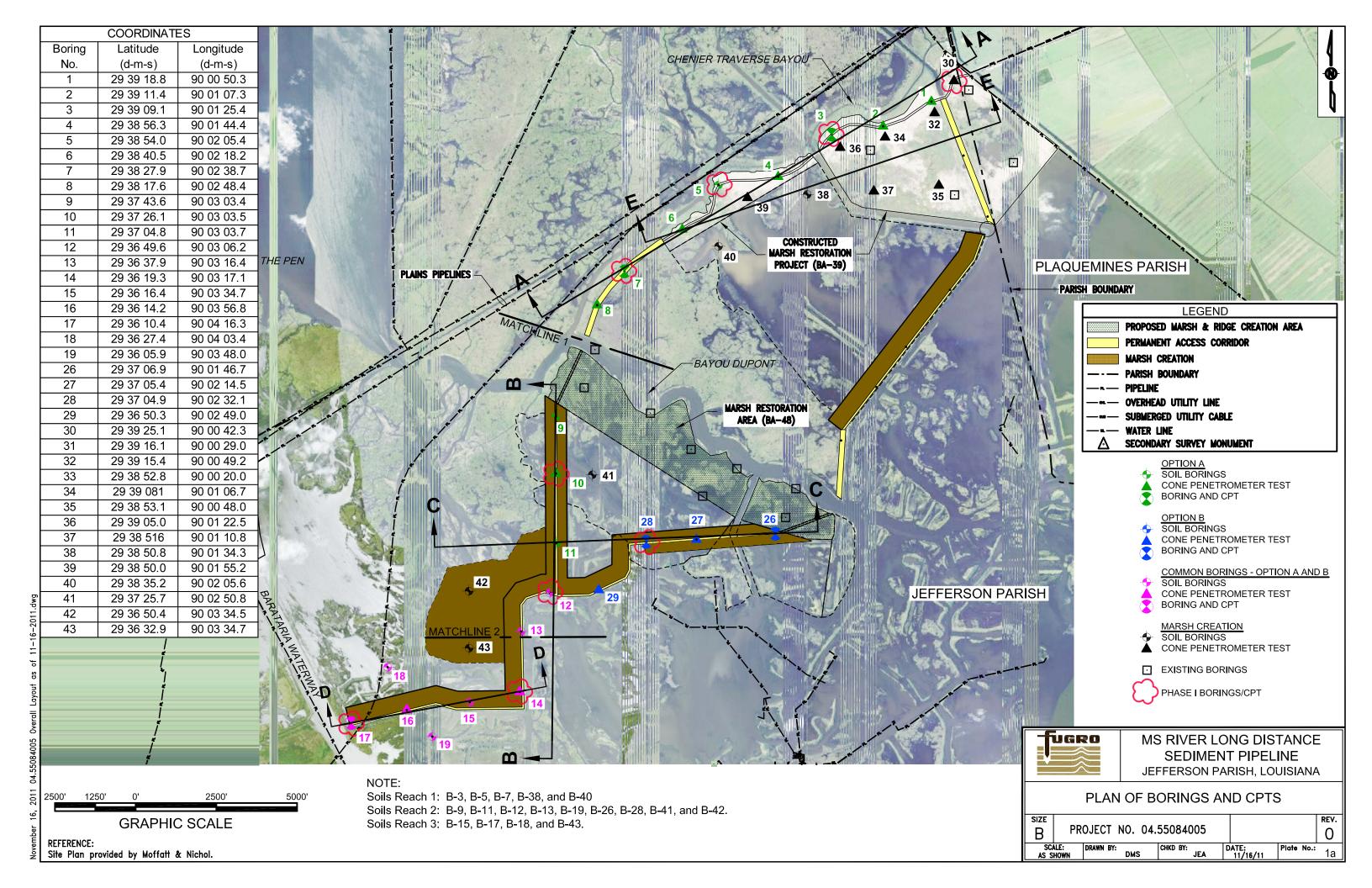
Due to the very soft sediment located in the top 10-ft, it is likely that placement of material for both the containment dikes and marsh creation fill material will generate mud waves, or shallow bearing capacity failures at the site. The design recommendations considered more significant, deeper seated failures. If shallow mud waves are problematic and will not create a stable base for containment dikes, geotextiles or other methods of confinement may be required.

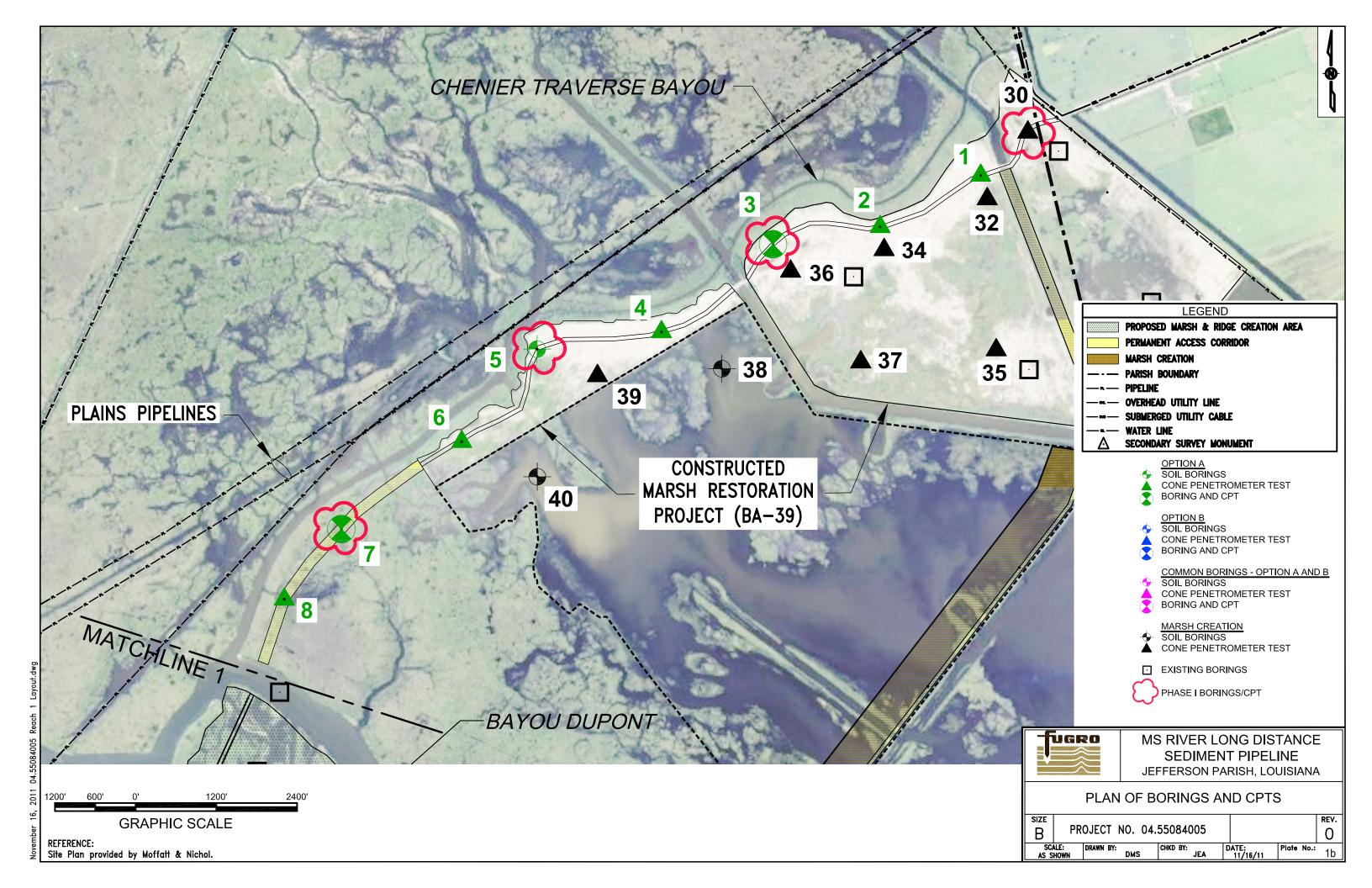


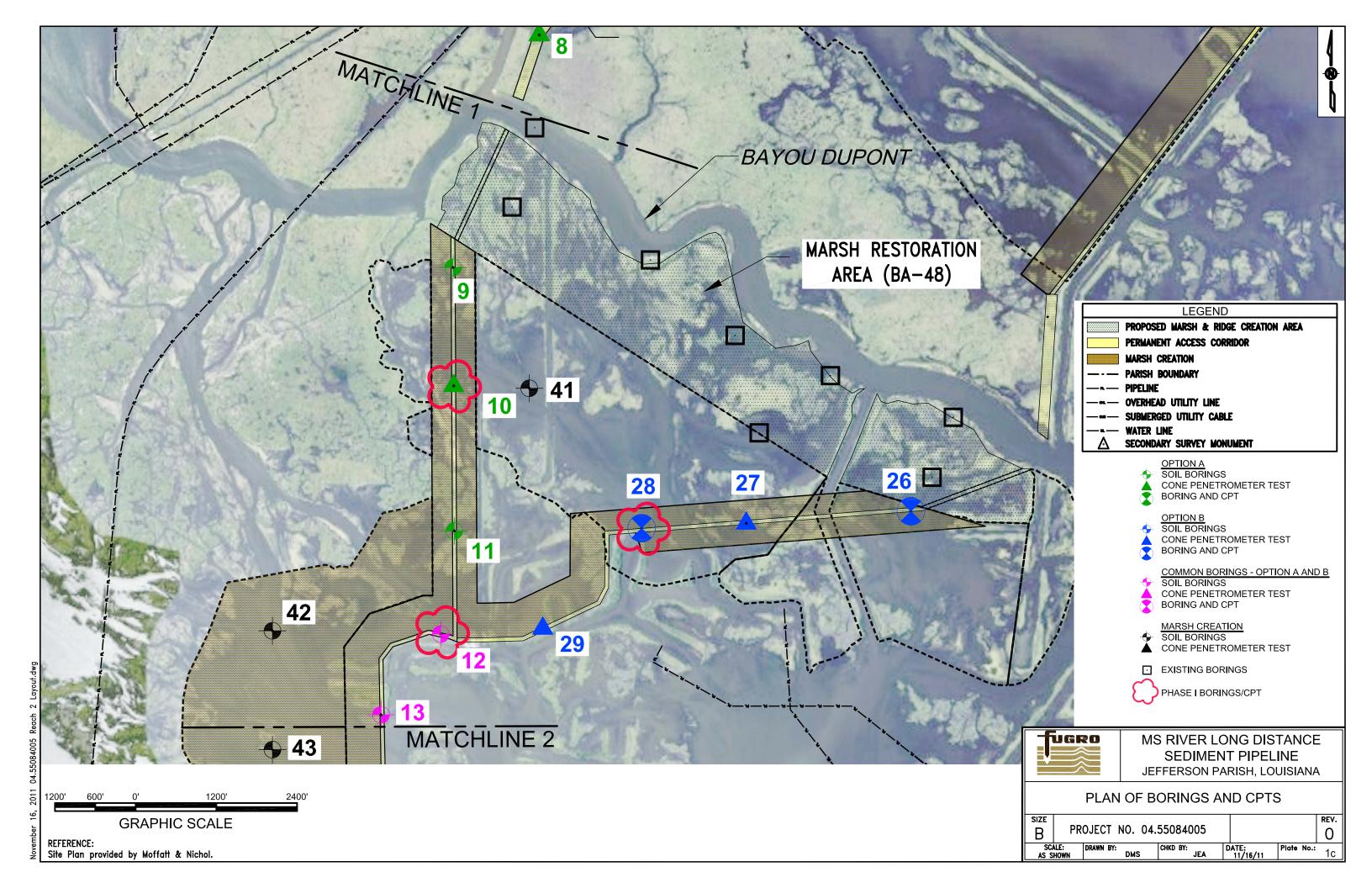


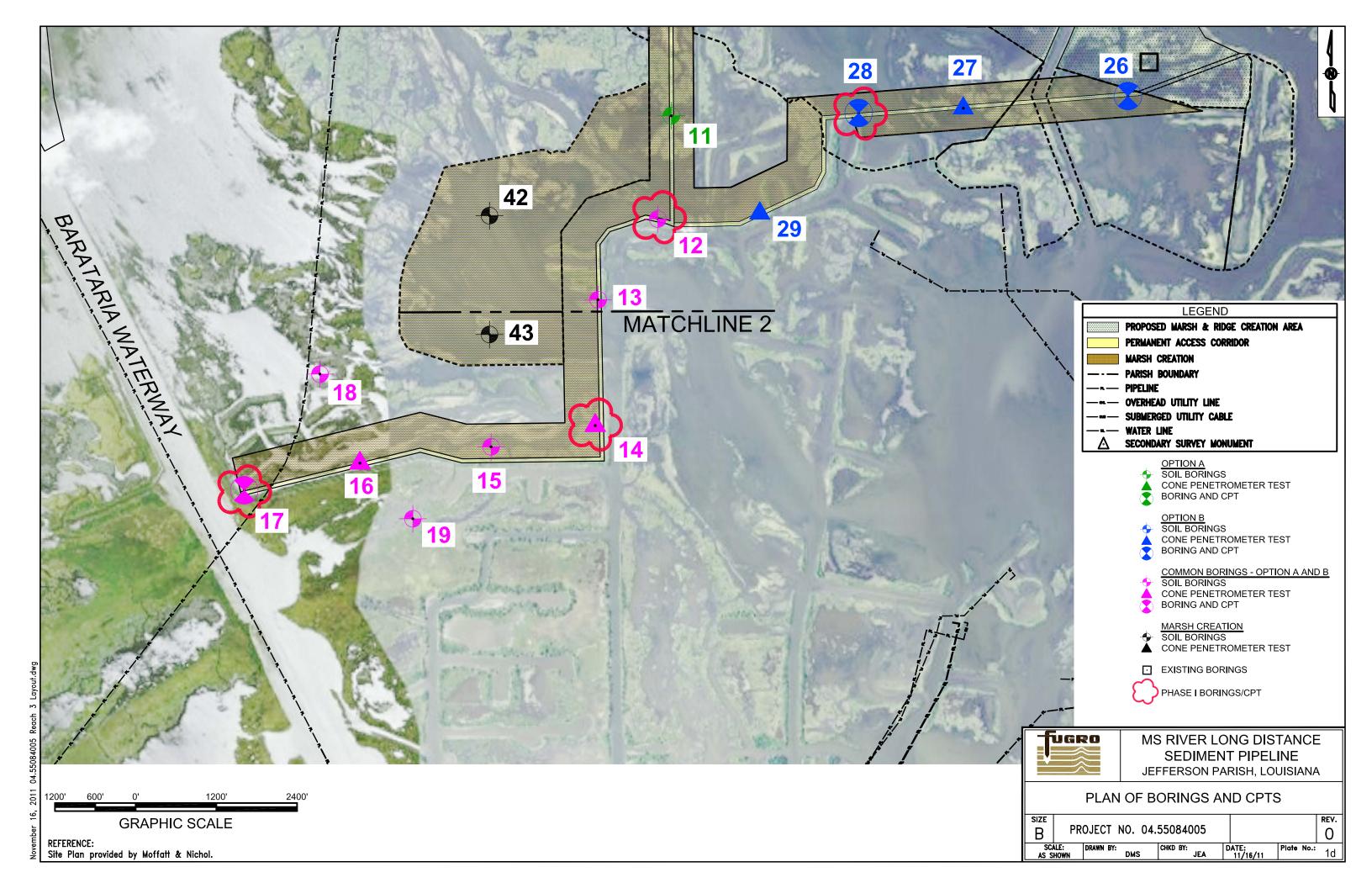
ILLUSTRATIONS











				LOCATION OF BUILD			CL/	ASSIF	ICAT	ION			SHE	AR S	TREN	GTH
ОЕРТН, FT	WATER LEVEL	SYMBOL	BLOWS PER FOOT	LOCATION: See Plate 1 COORDINATES: N 29° 39' 09.1" W 90° 01' 25.4" SURFACE EL.: 1.5' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	□Pe	enetrom ervane eld Van	eter e	Uı	nconfined ▼ Triaxial ● ure Vane ▲
			N=Pusl	POORLY GRADED SAND (SP) loose brown		-		21			-	0.	.2 0	.4 0.	.6 0.	8 1.0
-5 - -	 		N=7	FAT CLAY (CH), soft, gray, with silt traces	6.0	_	5	18 53	73	25	48					
				and organics - with ferrous nodules below 9'		_		52 53 65			-		A			
				- with sand pockets below 11' POORLY GRADED SAND (SP), gray, fine-grained	12.0		55 3	37 20	54	19	35	4				
 15				LEAN CLAY (CL), very soft, gray	14.0	78	88	37	43	23	20		•			
				FAT CLAY (CH), soft, dark gray, with organics and shell fragments	18.0 19.0	-		68			-		A			
-20 - - ·				LEAN CLAY (CL), very soft, gray		- - -	83									
				FAT CLAY (CH), soft to firm, gray, with silt layers	24.0	55 _ 55 -		78			_ _ _		40			
- -30 -						59 _	100	68	72	24	48_		•			
- - - - - - -						- - -		80			- - -		•			
						- - - _ 59		69			- - -			A •	•	
4	1. T	erms	COMPLETION DATE: August 24, 2011 TOTAL DEPTH: 60' CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 60' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro													
	ū	F	20	MS River Long Distance Sedimer	nt Pip	elin	е		L	OG	OF	во	RIN	IG N	1 O.	B-3
Fugr	о Со	onsulta	nts, Inc.	Jefferson Parish, Louisiana						ect No. 55 0	840	05		PL	.ATI	∃ 2a



	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION		:	SHEA	AR S	ΓREN	GTH	
DEPTH, FT WATER LEVEL SYMBOL SAMPLES BLOWS PER FOOT	COORDINATES: N 29° 39' 09.1" W 90° 01' 25.4" SURFACE EL.: 1.5'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	netrom rvane eld Van	е	Un Miniatu R SQ F		ial 🗨
\$ \ -	STRATUM DESCRIPTION)	2 1					0.			6 0.8		0
-45 -	FAT CLAY (CH), soft to firm, gray, with silt layers		- - - -		61			- - - -		•				
-50 -			- - - - - - 69		58 56			- - - -		•				
-55 - 		+ 60.0	- - - -		_60_			- - - 		_ _			. — —	
			- - - - -					- - - - -						
			- - - - -					- - - -						
			- - - -					- - - -						
	pols defined on Plates 20a and 20b. recovered with splitspoon due to low recovery with s	shelby to	ube.			TOTA CAVE DRY WET BACK	AL DE ED DI AUG ROT KFILL	TION EPTH: EPTH: ER: N ARY: : Cen T. Fe	60' Not lot Ap 0' to nent-l	Apploplica	icable	e	11	
TUGRO	MS River Long Distance Sedimer	nt Pip	elin	e		L	.OG	OF	во	RIN	IG N	10.	B-:	3
Fugro Consultants, Inc.	Jefferson Parish, Louisiana					Proje	ect No. 55 0	840	05		PL	.ATE	= 2	b

	_				LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHE	AR S	TREN	IGTH	
ОЕРТН, FT	WATER LEVE	SYMBOL SAMPLES		BLOWS PER FOOT	COORDINATES: N 29° 38' 54.0" W 90° 02' 05.4" SURFACE EL.: 1.3' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetrom orvane eld Van K	е		nconfine Triaxia ture Van	al 🗨
	+	:::)	/NI-	=WOH	POORLY GRADED SAND (SP), very loose.			4	21				0	.2 0	.4 0	.6 0.	8 1.0	_
 - 5 -		· · · · · · · · · · · · · · · · · · ·		=WOH N=27	gray and brown, fine-grained - medium-dense at 2.5'		- - - -	5	19			- - -	- - - -					
 -10					FAT CLAY (CH), very soft to soft, gray, with organics	7.0	59 - - -	97	68 54 15	81	24	57	-		•			
					- with silt and sand pockets at 13'		- - -		29	66	22	44						
15 					LEAN CLAY (CL) , very soft to soft, gray with shell fragments from 16' to 25'	15.0	-		39 37			-		A				
							84 -	97	37	32	25	7_	•					
				N=20			- - 55 - - - -		77	46	22	- - - - 24 -	-	••				
 -35 -			(1	N=20	LEAN CLAY WITH SAND (CL), gray	33.5	- - - -	84	31			- - -	-					
-35 -40					FAT CLAY (CH), soft, gray, with silt layers	38.0	59		71_			- -	 		•			_
1.	OTES: 1. Terms and symbols defined on Plates 20a and 20b. 2. WOH = Weight of Hammer CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-5																	
_	u	G		0	MS River Long Distance Sedime	ent Pip	elin	e		L	.OG	OF	во	RIN	IG N	NO.	B-5	
Fugro	Co	onsult	ant	s, Inc.	Jefferson Parish, Louisiana					Proje	ect No. 55 0	840	05		F	PLA ⁻	ΤΕ ;	3



			LOCATION: See Plate 1			CLA	SSIF	ICAT	ION		s	HEA	R S	TREN	IGTH	ı
DEPTH, FT	SYMBOL SAMPI ES	BLOWS PER FOOT	COORDINATES: N 29° 38' 27.9" W 90° 02' 38.7" SURFACE EL.: -0.8' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)		vane d Vane KIF	PS PE	Miniat R SQ F	ure Va	kial ● ine ▲
	+ (=)		ORGANIC CLAY (OH), very soft, black								0.2	2 0.4	4 0.	.6 0.	8 1.	.0
		N=WOH		5.0	39	89	135 184 125	133	35	98						
- 5 - - ·			LEAN CLAY (CL) , very soft to soft, gray and dark gray	5.0	- - -		33 42 35			-	A					
—10 –	1 ///				F		37 42	38	22	16						
			FAT CLAY (CH), very soft, dark gray	11.0	- -		70	00		-	•					
- 15 - -			- with shell fragments below 14' - with organics below 15'		- - -		73 155 93 53	99	32	67 _	•					
- -20 - -			LEAN CLAY (CL) , very soft, gray, with shell fragments, and sand seams	+ 18.0	- - - -		36			- - -						
- 25 - - 25 - 			FAT CLAY (CH), soft, gray, with silt seams and lenses	24.0	_ 64 - - -		62			- - - -	A					
- 30 - - 3					- 54 - - -	100	74	85	27	58_		•				
- -35 - - -					- 57 - - -		75			- - - -		•	•			
-40 -					<u>-</u>		68			-		•				
NOT	TES:							COM	PLET	ION E	DATE:	Aug	ust 2	23, 20	11	

FCBR_LOG (FINAL) 0 TO 1 04.55084005.GPJ FUGRO DATA TEMPLATE 042610.GDT 11/16/11

1. Terms and symbols defined on Plates 20a and 20b.

2. Depth to mudline below water surface = 1.3'.

3. WOH = Weight of Hammer

TOTAL DEPTH: 60'

CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 60'

BACKFILL: Cement-Bentonite Grout

LOGGER: T. Ferro



MS River Long Distance Sediment Pipeline

LOG OF BORING NO. B-7

Fugro Consultants, Inc.

Jefferson Parish, Louisiana

Project No. 04.55084005

PLATE 4a

				LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHE	AR S	TREN	IGTH	l
ᇤ	<u> </u>		BLOWS PER FOOT	LOCATION: See Plate 1 COORDINATES: N 29° 38' 27.9"	≅F								netrom			nconfin	
DEPTH, FT	WATER I EVE	SYMBOL	VS F	W 90° 02' 38.7"	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	₽⊢	일 는	PLASTICITY INDEX (PI)	♦To	rvane			Triax	kial
)EP	\TE	SAN	LOV	SURFACE EL.: -0.8'	STR	IT DR	SSIN	WATI	LIQUID	PLASTIC LIMIT	ASTI	ΔFIE	eld Van		Miniat		ine 📥
-	>		В	STRATUM DESCRIPTION		S	PA 20	8			= ⊒	١ ,			R SQ F .6 0.		0
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=	4			and lenses		_		69			-						
 45 -	1			FAT CLAY (CH), soft to firm, gray, with silt	45.0			09			_		_				
Ē]			seams and lenses							_						
-	+					-					-						
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NO.			. on d	hala defined on Dieter 200 and 200							ION E PTH:		: Au	gust 2	23, 20	11	
DAT				bols defined on Plates 20a and 20b. ne below water surface = 1.3'.					CAVI	ED DI	EPTH:	Not			е		
UGR				of Hammer							ER: N ARY:			ble			
H L H											ART: .: Cen			nite	Grout		
1005.0									LOG	GER:	T. Fe	erro					
.55084																	
0 1 04																	
FCBR_LOG (FINAL) 0 TO 1 04.55084005.GPJ FUGRO DATA TEMPLATE 042610.GDT 1/1/6/11 E	F	JG	RO	MS River Long Distance Sedime	nt Pip	elin	е	LOG OF BORING NO. B-7									
ANIMA ANIMA																	
501								Project No.									
Fug	ro C	onsult	ants, Inc.	Jefferson Parish, Louisiana					04.	550	840	05		PL	ATI	E 4	ŀb

				_	LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHEA	AR S	TREN	GTH	_
DEPTH, FT	WATER LEVEI	SYMBOL		BLOWS PER FOOT	COORDINATES: N 29° 37' 43.6" W 90° 03' 03.4" SURFACE EL.: -1.3'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetrom ervane eld Vand Kl	е		nconfine Triaxi ure Var	ial 🌑
	H	<u> </u>	 	14/01/1	PEAT (PT), very soft, black, with roots				04.4				0	.2 0.	.4 0	.6 0.	8 1.0)
 			N=	:WOH		4.0	- - 22	47	395 264	191	54	137	_					
5 					FAT CLAY (CH), very soft, gray, with organics	4.0	_ - - -		53 86			- -	A					
 - 10 -							- - -		49 40			-	A					
 - 15 —							- - -		68 44	55	24	31 _	•					
 							- - -		54			- - -	•					
 -20 							- - -		35			- - -	•					
 - 25					SILT (ML), very soft to soft, gray, with clay pockets, and sand lenses SILTY SAND (SM), gray, fine-grained	23.0	74		30 47	25	24	1		• 🛦				
 - 30 -)	=Push J=26	- medium-dense from 30' to 38.5'		- - - - -	44	28			- - - - -						
				N=7	- loose below 38.5'	40.0	- - - - -	44	35			- - - - -						- — .
04.55084005.GPJ FUGRO DA	1. T 2. D 3. V	erms epth /OH =	completion Date: August 26, 2011 Total Depth: 40' Caved Depth: Not Applicable DRY AUGER: Not Applicable Wet Rotary: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro MS River Long Distance Sediment Pipeline LOG OF BORING NO. B-9															
FCBR_LOG (FINAL) 0 TO 1	u	F		0	MS River Long Distance Sedim	ent Pip	elin	е		L	OG	OF	во	RIN	IG N	NO.	B-9	
Fugro	o Co	nsulta	ants	, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		Р	PLA ⁻	ΓΕ	5



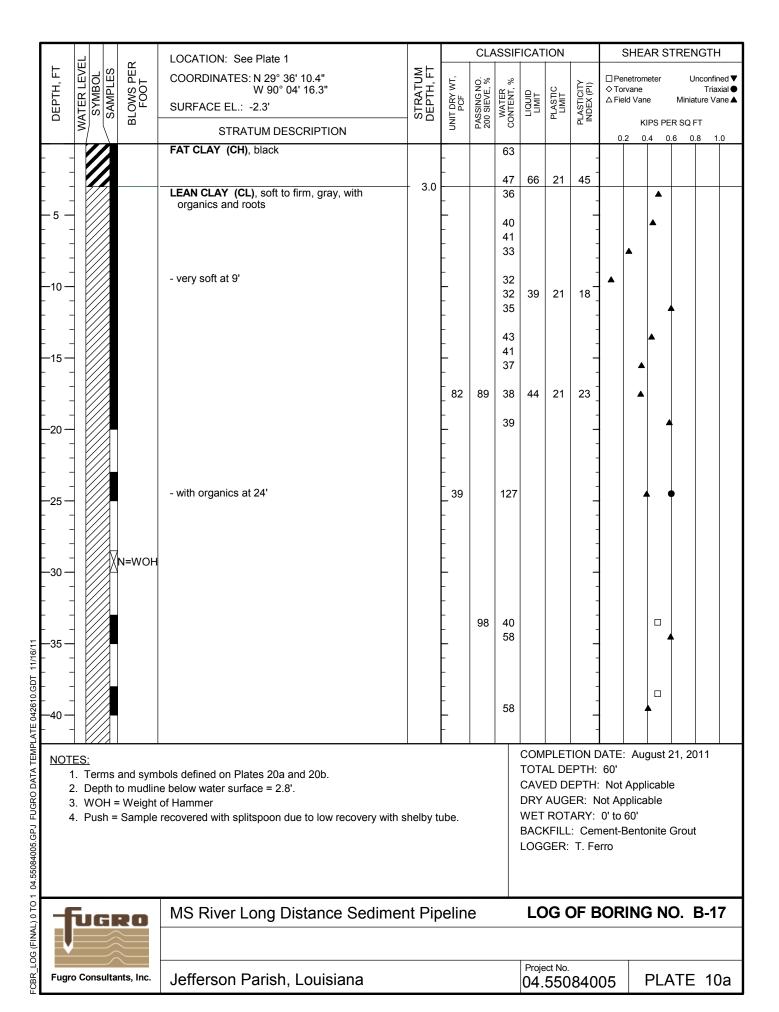
	یر		_~		LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR S	TREN	IGTH	ł
ОЕРТН, FT	WATER LEVE	SYMBOL SAMPLES	BLOWS PEF	FOOT	COORDINATES: N 29° 37' 04.8" W 90° 03' 03.7" SURFACE EL.: -1.8'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetron orvane eld Var K	ne	Ui Miniat ER SQ F	ure Va	xial
					STRATUM DESCRIPTION		⊃	шк	Ŭ				C).4 C			.0
 			7	VOH	PEAT (PT), very soft, black, with, wood pieces		- - - -		913 447	548	254	294 _ -	•					
 - 10 -					with clay pockets at 6'with clay layers below 10'		- - - - 13	80	266 465	312	152	160_	^					
 15					ORGANIC CLAY (OH), very soft, gray	14.0	- - -		275 320			- - -	A					
 				-	FAT CLAY (CH), very soft, gray - with sand lenses below 18' LEAN CLAY (CL), very soft, gray, with sand	16.0	-		128 130 83 36	125	35	90	A					
20 25					lenses FAT CLAY (CH), very soft, gray, with sand lenses	20.0	- - - - 58		68			-	•					
 30 - 							- - - - -		80 58			- - - -	•					
							70 -		49			- - -	_	•				
40	- - -					40.0	_ 		78 73			- -	-4					
2	1. T 2. C 3. V	erms Depth t VOH =	to m = We	udline eight o	pols defined on Plates 20a and 20b. e below water surface = 2.4'. of Hammer recovered with splitspoon due to low recovery with	shelby t	ube.	ı		TOTA CAVI DRY WET BACK	AL DE ED DE AUGI ROT KFILL	TION EPTH: EPTH: ER: N ARY: : Cen T. Fe	40' : Not lot A _l 0' to nent-	: Apploplica	licabl able	е		
1	Fu	[H	∷	D	MS River Long Distance Sedime	ent Pip	elin	е		LC)G (OF E	BOF	RINC	3 N	O. I	3-1	1
Fugr	ugro Consultants, Inc. Jefferson Parish, Louisiana Project No. 04.55084005 PLATE 6																	

	Ι.		Τ		LOCATION, Con Dista 4			CLA	ASSIF	ICAT	ION			SHEA	AR ST	ΓRENG	GTH.							
DEPTH, FT	WATER LEVEL	SYMBOL		BLOWS PER FOOT	LOCATION: See Plate 1 COORDINATES: N 29° 36' 49.6" W 90° 03' 06.2" SURFACE EL.: -2.8'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetrom orvane eld Van	е	Miniatu	confined ▼ Triaxial ● re Vane ▲							
	$ \mathbf{x} $				STRATUM DESCRIPTION		5	20 P	8				l ,		.4 0.	R SQ FT 6 0.8	1.0							
	 				PEAT (PT), very soft, black, with roots and grass		- - -		533 179 221	175	35	140	A											
5 	- - -				- with organic clay lenses below 6'		_ - - 18	28	230 283	287	57	230	•											
 -10 -]						- - - -		183 243			- - - -	•	•										
 15 	- - - -				FAT CLAY (CH), very soft, gray	14.0			77 92 52	77	23	54	4											
 -20					LEAN CLAY (CL), very soft, gray FAT CLAY (CH), soft, gray	19.0 20.0	_		33			_	_											
 - 25 	+ + + + + + + + +		N:	=Push			- - - - -					- - - - -												
	- - - - -						- 69 -		53			- - - -		•••										
- 35 –	- - - - -						- - - -		57			- - - -		•										
TE 042610	<u> </u>					- + 40.0	_ 68_ -		_55_			- - -	 			+	_							
04.55084005.GPJ FUGRO DA	1. T 2. C	erms Depth	to	mudline	symbols defined on Plates 20a and 20b. udline below water surface = 3.0'. nple recovered with splitspoon due to low recovery with shelby tube. MS River Long Distance Sediment Pipeline COMPLETION DATE: August 21, 2011 TOTAL DEPTH: 40' CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 40' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro												1							
FCBR_LOG (FINAL) 0 TO 1	J	G		0	MS River Long Distance Sedim	ent Pip	elin	е		LC)G (OF E	BOR	RING	S NO). B	3-12							
Fugre Fugre	o Co	onsulta	ants	s, Inc.	Jefferson Parish, Louisiana								05		fferson Parish, Louisiana Project No. 04.55084005 PLATE 7									



	ایا	~	LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHE	AR S	TREN	GTH	1
ОЕРТН, FT	WATER LEVE SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 37.9" W 90° 03' 16.4" SURFACE EL.: -3.5'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetrom orvane eld Van	ie	Ur Miniat ER SQ F	ure Va	xial
	>/		STRATUM DESCRIPTION		n	₽ 2					0			.6 0.		.0
 - 5 		N=WOR	ORGANIC CLAY (OH), very soft, black		- - - - -		205 92	187	47	140_ - -						
 -10			with wood pieces at 8'with wood pieces at 11'		- - -		157			- -						
 -15 -			FAT CLAY (CH), very soft, gray	15.0	- - -		168 176 138	125	38	87 _	A					
 20			- with roots from 16' to 20'		_ _ 45 _	87	91 82	76	26	50 _	A					
 - 25 		N=Push			- - - - -		51	58	22	- - 36 - - - -						
 -30 -35			- very soft to soft, with silt pockets, lenses, and layers below 28'		56 - - - - -		77 79 77			- - - -	A					
- - -40				- 40.0	_ _ 60		67_			- - 		4 •				
3 4	Terms Depth t WOR =	o mudline Weight	pools defined on Plates 20a and 20b. e below water surface = 4.0'. of Rod recovered with splitspoon due to low recovery with	shelby to	ube.			TOTA CAVE DRY WET BACK	AL DE ED DE AUGI ROT KFILL	TION EPTH: EPTH: ER: N ARY: : Cen T. Fe	40' : Not lot Ap 0' to nent-	Apploplica	icabl	е		
Fugro	VGI	20	MS River Long Distance Sedime	nt Pip	elin	e		LC)G (OF E	BOR	RINC	3 N	O. I	3-1	3
Fugro	o Consulta	nts, Inc.	Jefferson Parish, Louisiana						ct No. 550	840	05		F	PLA ⁻	ΓΕ	8

					LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR S	TREN	GTH	1
ОЕРТН, FT	WATER LEVE	SYMBOL	MPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 16.4" W 90° 03' 34.7"	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetron orvane eld Var		Ur		xial
DEI	WATE	5	δ N	BLO F	SURFACE EL.: -1.0'	ST	D TINC	PASSII 200 SI	CONT	95	PLA	PLAS		K	IPS PE	RSQF	Т	
			M	11100	STRATUM DESCRIPTION FAT CLAY (CH), very soft, black, with roots								0	.2 0	.4 0	.6 0.8	3 1.	.0
-	-		ĬΝ	=WOR		2.0	-		61			-						
- - 5 -					LEAN CLAY (CL), soft to firm, gray - with silt traces at 4'	3.0	-	0.4	36	45	10	-		•				
-	-				- with roots at 6'		_ 86 -	94	34	45	18	27 _		•				
- - -10 -							- -		42			-		•				
-	-				- with organics at 12'		-		36			-			•			
-	-					45.0	-		35			-		•				
—15 - - - -	_				SILTY CLAY (CL-ML), very soft to soft, gray	15.0	-	92	29 34 31	34	24	10	A	A				
- 20 -					FAT CLAY (CH), soft, gray, with organics	19.0	_		65			-		•				
-							-					-						
25 - -							_ -	96	93	142	37	105_		•				
- - -30 -	- - - -				- with silt layers below 28' - very soft to soft at 29'		- - - 64		60			- -] 		•			
- - - - - - - - -	- - - - -				- with silt lenses from 33' to 35'		- - - -		52 26	52	20	32	-	•				
E 042610.GDT 1	- - -				- soft to firm, with silt layers below 39'	- + 40.0	_ _ 62		64_			- - - -			•			
О БАТА	2.	Term Depth	n to		pols defined on Plates 20a and 20b. e below water surface = 2.0'. of Rod					TOTA CAVE DRY WET BACK	AL DE ED DI AUG ROT KFILL	FION EPTH: EPTH ER: N ARY: : Cer T. Fe	40' : Not Not Ap 0' to nent-	: Apploplica	icable	е		
INAL) 0 TO 1	F	JG	:	20	MS River Long Distance Sedime	ent Pip	elin	e		LC)G (OF E	BOR	RINC	3 N	O. E	3-1	5
FCBR_LOG (FINAL) 0 TO 1	jro C	onsul	tant	s, Inc.	Jefferson Parish, Louisiana						ect No. 55 0	840	05		F	'LAT	ΓΕ	9



	Τ			LOCATION: Oct District			CLA	SSIF	ICAT	ION		,	SHE	AR S	TREN	GTH		
DEPTH, FT	WATER LEVEL	SYMBOL	BLOWS PER FOOT	LOCATION: See Plate 1 COORDINATES: N 29° 36' 10.4" W 90° 04' 16.3" SURFACE EL.: -2.3' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	□Pe ◇To	netrom rvane eld Van	eter		nconfin Triax ure Va	ed ▼ kial ●	
	+	\rightarrow			-							0.	.2 0	.4 0	.6 0.8	3 1.	.0	
- - 45				LEAN CLAY (CL), soft to firm, gray, with organics and roots FAT CLAY (CH), soft to firm, gray	45.0	_ _ 		41			- - -							
- - - -50 -						- - - 64 -		60			- - -			□▲	•			
- - - 55 -						- - -	100	62	85	27	- - 58_				•			
- - - -60 -					60.0	- - - 69_		51_			- - 			_	•			
- - - 65 -						- - - -												
	- - -					_ - -												
—70 — - · · · · · · · · · · · · · · · · · · ·	- - - -					- - - -					-							
-75 -	<u>-</u> - -					_ - -					-							
.TE 042610.GDT	- - - -					- - - -												
JGRO DA	1. T 2. D 3. W	epth t /OH =	o mudlin Weight	bols defined on Plates 20a and 20b. e below water surface = 2.8'. of Hammer recovered with splitspoon due to low recovery with s	shelby t	ube.		COMPLETION DATE: August 21, 2011 TOTAL DEPTH: 60' CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable WET ROTARY: 0' to 60' BACKFILL: Cement-Bentonite Grout LOGGER: T. Ferro										
INAL) 0 TO	Tu	G	30	MS River Long Distance Sedime	nt Pip	elin	e LOG OF BORING NO. B-17											
FCBR_LOG (I	о Со	nsulta	nts, Inc.	Jefferson Parish, Louisiana					Proje	ect No. 550	840	05	ı	PLA	TE	10)b	

				LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHE	AR S	TREN	GTH
DEPTH, FT	WATER LEVE	SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 27.4" W 90° 04' 03.4" SURFACE EL.: -2.5'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetron orvane eld Var			nconfined ▼ Triaxial ● ure Vane ▲
ā	\ <u>\</u>	$^{\prime\prime} ^{\circ} $	BL	STRATUM DESCRIPTION	S I	TINO	PAS 200	S S		립_	38				RSQF	
	7	<u>/</u> }	N=WOR	PEAT (PT), very soft, black, with organic clay,				653			_	0	0.2 0	.4 0	.6 0.	8 1.0
]	7.\A	11-11011	shells, roots, and wood		-					-					
-	1 🖹	<u>//</u> :		ORGANIC CLAY (OH), very soft, gray, with	3.0			809 180			_	A				
-5-	1 🖺		N=Push	wood and roots		Ē		206			_]				
					7.0	_					-					
-				FAT CLAY (CH) , soft, gray, with silt pockets, organics, and wood	/.0	61	99	60	94	30	64		^			
- 10						L		54			-		•			
-						-		57			-		•			
						-		00			-					
- -15 -						-		82 58	83	27	56					
- 13 -						F		76			-		•			
				- very soft from 17' to 20'		-		93			-	•				
						-		31			-					
—20 —						<u> </u>					_					
-						-					-					
			N=WOR			-					-					
25						_					_					
ļ .						-					-					
				- with silt layers at 28'							-					
 30						58		73			_	ł				
						-					-					
-			N=Push			-					-					
			N=Pusn			Ē		66			_]				
-						Ŀ					-					
-				- very soft below 38'							_					
- -40 -					40.0	L	ļ	72		L		L		L	$\lfloor - floor$	
.		-				}					-					
NOT	ES:		L		•	•					ION [: Au	gust 2	28, 20	11
	1. Te			ools defined on Plates 20a and 20b. e below water surface = 3.0'.							PTH: EPTH:		Apn	licable	е	
	3. W	OR =	Weight	of Rod					DRY	AUG	ER: N	lot A	pplica			
·	4. Pu	ısh =	Sample	recovered with splitspoon due to low recovery with s	shelby t	ube.					ARY: .: Cen			onite (Grout	
											T. Fe				J. 50t	
	Fu	GE	20	MS River Long Distance Sedimer	nt Pip	elin	е		LC	G (OF E	BOF	RINC	3 N	O. I	3-18

Jefferson Parish, Louisiana

Project No. 04.55084005

PLATE 11

FCBR_LOG (FINAL) 0 TO 1 04.55084005.GPJ FUGRO DATA TEMPLATE 042610.GDT 11/16/11

Fugro Consultants, Inc.

	ایر		~	LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION	ı		SHE	AR S	TREN	GTH
ОЕРТН, FT	WATER LEVE	SYMBOL	BLOWS PER FOOT	COORDINATES: N 29° 36' 05.9" W 90° 03 48.0" SURFACE EL.: -1.0' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetrom rvane eld Van K	е		confined Triaxial Tri
	-											0	.2 0	.4 0	0.6 0.8	1.0
 			N=WOR N=Push	ORGANIC CLAY (OH), very soft, black, with roots, grass, and wood		- - -		230	189	43	- - 146					
 -5-				FAT CLAY (CH), very soft, gray, with organics and roots	5.0	- 		70			-	A				
 				- with silt seams and traces from 7' to 10'		- 73 -	100	49 58	70	23	47 _	•				
—10 — 						- - -		56			- - -	•				
- -					14.0	_		55			-	A				
—15 — 				LEAN CLAY (CL), very soft, gray, with silt layers	14.0	 - -		37 40	43	18	25	•				
 - 20 -						- - -		78			- - -	•				
 						- - -					- -					
 25 				SILTY SAND (SM), gray, fine-grained	24.0	- - -		26	NP	NP	NP_ -					
 30 						- - - -	13	24			- - -					
 -35 - 			N=5	POORLY GRADED SAND WITH CLAY (SP-SC), loose to medium, gray, fine-grained	33.5	- -					- -					
 			N=25		40.0	- - -	9	24			- - -					
						<u> </u>										
2 3	l. Te 2. De 3. W	epth to	o mudlin Weight	bols defined on Plates 20a and 20b. e below water surface = 1.1'. of Rod. recovered with splitspoon due to low recovery with	shelby t	ube.			TOTA CAVI DRY WET BACI	AL DE ED DI AUG ROT KFILL	EPTH: EPTH: ER: N ARY:	40' Not lot Ap 0' to nent-l	Apploplica	icabl ıble	29, 20 e Grout	11
Fugro	u	GF	50	MS River Long Distance Sedime	nt Pip	elin	е		LC)G (OF E	BOR	INC	3 N	O. E	B-19
Fugro	o Cor	nsultar	nts, Inc.	Jefferson Parish, Louisiana						ect No. 55 0	840	05		PL	_ATE	12

	Ι,		Τ		LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHEA	AR S	TREN	GTH	
DEPTH, FT	WATER LEVEI	SYMBOL	0,000	FOOT	COORDINATES: N 29° 37' 06.9" W 90° 01' 46.7" SURFACE EL.: -3.5' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To		e PS PE	Miniat R SQ F	Т	kial ● ine ▲
	$+\ell$		/NI-	WOLL	ORGANIC CLAY (OH), very soft to soft, black	+	_		20.4				0	.2 0	4 0.	.6 0.8	3 1.	0
- - - - 5 -			N=	WOH		7.0	- - - -		158 145 198 357	l .	39	146	_ _ _ _ _	•				
					FAT CLAY (CH), very soft, black and gray, - with silt pockets at 7' - dark gray, with sand pockets and layers from 9'	7.0	_ 42 -	99	110 29	115	34	81	•					
-10 - - - - - -15 -					to 13' - gray below 12' - with organics from 12' to 18'		- - - -	72	49 54 73	54	20	34	•					
- - -	- - -						 - -		77 78	82	25	57	⁴					
- -20 -					LEAN CLAY (CL), gray, with silty sand pockets	20.0	- - -		70			-	<u> </u>					
- - -25 -					- very stiff at 24' FAT CLAY (CH), soft, gray	25.0	97		26			-						1.8
- - -30 -			N	N=2	- with silt pockets below 28.5'		- - - -		58			- - -	-					
- - - - - - - -			N=	:Push			- - - -		46			- - -	-					
ATE 042610.GD - 042610.GD				N=8	SILTY CLAY (CL-ML), firm, gray, with sand pockets	38.0	 - - -	96	38			- -	-					
04.55084005.GPJ FUGRO DA	1. T 2. E 3. V	erms Depth VOH	to n = W	nudline /eight c	pols defined on Plates 20a and 20b. be below water surface = 3.4'. If Hammer. recovered with splitspoon due to low recovery with seconds.	shelby t	ube.			TOTA CAVI DRY WET BACK	AL DE ED DI AUG ROT KFILL	ION EPTH: EPTH ER: N ARY: : Cer T. Fe	60' : Not Not Ap 0' to nent-	Appl oplica 60'	icable ble	е		
FCBR_LOG (FINAL) 0 TO 1	Fu		:	0	MS River Long Distance Sedime	nt Pip	elin	е		LC)G (OF E	BOR	RINC	S NO). E	3-2	6
Fugi	о Сс	onsulta	ants	, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PLA	ΛTE	13	a

- 3. WOH = Weight of Hammer.
- 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube.



	LOCATION: See Plate 1			CLA	SSIF	ICAT	ION		,	SHE	AR S	ΓRENG	STH .
DEPTH, FT WATER LEVEL SYMBOL SAMPLES BLOWS PER	COORDINATES: N 29° 37′ 06.9" W 90° 01′ 46.7" SURFACE EL.: -3.5′	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	netrom rvane eld Van	е	Miniatur	onfined ▼ Triaxial ● re Vane ▲
	STRATUM DESCRIPTION		S	P/ 20	Ö			ш-	0.		.4 0.	R SQ FT .6 0.8	1.0
	SILTY CLAY WITH SAND (CL-ML), firm, gray	42.0	_					_					
45 — N=	FAT CLAY (CH), firm, gray, with silt layers	45.0	- - -	72	32			-					
-50 —			- _ 73 _		49			- - -			□ ▲ •	,	
-55 -			- - -		41 58			-			□▲		
-60 -		60.0	- - 66		_56_			- - 				•	
			- - -					- - -					
 70 -			- - -					-					
			- - -					-					
-75 - 119V1			- - -					-					
E 042810.GDT			- - -					- - -					
2. Depth to m 3. WOH = We 4. Push = Sar	symbols defined on Plates 20a and 20b. Idline below water surface = 3.4'. Ight of Hammer. Inple recovered with splitspoon due to low recovery with s	shelby to	ube.			TOTA CAVI DRY WET BACK	AL DE ED DI AUG ROT KFILL	ION EPTH: EPTH: ER: N ARY: : Cen T. Fe	60' Not lot Ap 0' to nent-l	Apploplica	icable ble		1
Fugro Consultants, I	MS River Long Distance Sedimer	nt Pip	eline	e		LC)G (OF E	BOR	INC	S NO	Э. В	-26
Fugro Consultants, I	Jefferson Parish, Louisiana						ect No. 550	840	05	ı	⊃LA	TE	13b

	Τ.			LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHE	AR S	TREN	GTH
ОЕРТН, FT	WATER LEVEI	SYMBOL	BLOWS PER FOOT	COORDINATES: N 29° 37' 04.9" W 90° 02' 32.1" SURFACE EL.: -2.9'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	netrom rvane eld Van K	е		confined ▼ Triaxial ● ire Vane ▲
-	-		N=WO	STRATUM DESCRIPTION ORGANIC CLAY (OH), very soft, dark gray, with roots, peat, and shells		- - -		182 185 208	158	36	122	0	.2 0	.4 0	.6 0.8	1.0
- 5 - - -	_		\	LEAN CLAY (CL), very soft, dark gray, with organics	- 6.0	60	96	72	44	20	24	_				
- - 10 -	_ _ _ _			FAT CLAY (CH), very soft to soft, gray, with organics and roots - dark gray below 10'	- 8.0	- - -		81 169	78	24	54		•			
- - -	_ _ _			ORGANIC CLAY (OH), soft, dark gray, with roots FAT CLAY (CH), very soft, gray, with organics	- 12.0 - 13.0	53	27 98	83 119 80	86	28	58	A				
15 - - -			\	and roots LEAN CLAY (CL), gray	- 15.0	- - -		35			-	-				
- 20 - - -	_		N=4	- with sand seams at 18.5'		- - -	87	31			- - -	-				
- - 25 - -			N=2			- - - -		41			- - -					
- - -30 - -			N=Pus	SILTY SAND (SM), very loose to medium-dense, gray	- 28.0	- - -	27	27			- - -					
- - - - - - - - - - - - - - - - - - -	_ :		N=15			- - - -	12	22			- - -					
ATE 042610.GDT	_ ;		N=WO	LEAN CLAY (CL), very soft, gray	- 38.0	- - -					- -					
04.55084005.GPJ FUGRO DA	1. T 2. [3. V	Terms Depth WOH	to mudl = Weigh	mbols defined on Plates 20a and 20b. ine below water surface = 3.6'. it of Hammer. e recovered with splitspoon due to low recovery with s	helby t	ube.			TOTA CAVE DRY WET BACK	AL DE ED DE AUGI ROT KFILL	I FION E EPTH: ER: N ARY: :: Cen T. Fe	60' : Not lot Ap 0' to nent-l	Apploplica	icable	е	11
FCBR_LOG (FINAL) 0 TO 1	Fu	[F]	RO	MS River Long Distance Sedimer	nt Pip	elin	е		LC	G (OF E	BOR	INC	3 NO). E	3-28
FCBR_LOG	ro Co	onsulta	ants, Inc.	Jefferson Parish, Louisiana						ct No. 550	840	05		PLA	ΛΤΕ	14a

		_			LOCATION: See Plate 1			CLA	SSIF	ICAT	ION		,	SHE	AR ST	ΓREN	GTH	
DEPTH, FT		WATER LEVE SYMBOL	SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 37' 04.9" W 90° 02' 32.1" SURFACE EL.: -2.9' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	netrom rvane eld Van K	е	Un Miniatu R SQ F		ial 🗨
-	-	+	\forall		LEAN CLAY (CL), very soft, gray								0.	.2 0	.4 0.	3.0	3 1.	0
- - 45 -	_				FAT CLAY (CH), firm, gray, with organics and	45.0			31 26	37	19	18						
-	_				roots		- - -					- -						
- 50 -	_						- _ 64 -		62			- - -			A	•		
- - - -55 - -	-						- - - 70 - -	100	50	69	23	46_ -			_			
- - 60 -	- -					60.0	- - - 71 		49_			- - -				- - -		
							- - -					- -						
65 - - -	_						- -					- -						
- - -70 -	_						- - -					- -						
							- - -					- - -						
—75 - - ∑ -	_						- -					- -						
.6DT 11/16/ - 08 -	_						- - -					- - -						
LATE 04261(_						- - -					- - -						
FCBR_LOG (FINAL) 0 TO 1 04.55084005 GPJ FUGRO DATA TEMPLATE 042610.GDT 11/16/11 6	1. 2. 3.	. Ter . Dep . WC	oth to	o mudlin Weight	bols defined on Plates 20a and 20b. e below water surface = 3.6'. of Hammer. recovered with splitspoon due to low recovery with s	shelby t	ube.			TOTA CAVI DRY WET BACK	AL DE ED DE AUGI ROT KFILL	TION E EPTH: ER: N ARY: :: Cen T. Fe	60' Not lot Ap 0' to nent-l	Apploplica	icable ble	e	11	
FINAL) 0 TO	f	u		50	MS River Long Distance Sedimer	nt Pip	elin	е		LC)G (OF E	BOR	INC	S NO). E	3-28	3
FCBR_LOG (gro	Cons	ultar	nts, Inc.	Jefferson Parish, Louisiana						ect No. 550	840	05		PLA	ΛΤΕ	14	b

		T		LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHE	AR S	TREN	GTH
ОЕРТН, FT	SYMBOL	SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 38' 50.8" W 90° 01' 34.3" SURFACE EL.: -1.8'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	enetrom orvane eld Van K	е		nconfined ▼ Triaxial € ure Vane ▲
		\downarrow		STRATUM DESCRIPTION								0	.2 0	.4 0.	.6 0.	3 1.0
 		XN	I=WOH	ORGANIC CLAY (OH), very soft, black, with roots - with peat at 2'		- - - 39	98	322 130	152	41	- - 111					
 - 5 - 				LEAN CLAY (CL), very soft, gray, with silt seams	4.0	- - -		62 69			- -	•				
 - 10 				FAT CLAY (CH), soft, gray, with peat and organics	8.0	- - -		68 97 103	89	30	59 _	•	•			
 -15 				- very soft, with shell fragments at 13'		- - -		77 105 49			- - - -	•	•			
 -20 						68 - -	100	53	54	21	33_	•				
 -25 		<u> </u>	I=Push	SILTV SAND (SM) grov	28.0	- - - -		50	52	21	31 - - -					
30 — 30 — 35 — 				SILTY SAND (SM), gray	29.0	- - - - -	16	21			- - - - - -					
- TAIE 042810:				FAT CLAY (CH), very soft to soft, gray with silt pockets at 39'	38.0	_ 59 _ _		73 32			- -	A	•			
04.55084005.GPJ FUGRO DA	Term Depth WOH	n to	mudline Weight	pols defined on Plates 20a and 20b. e below water surface = 1.9'. of Hammer. recovered with splitspoon due to low recovery with	shelby t	ube.			TOTA CAVI DRY WET BACK	AL DE ED DI AUG ROT KFILL	FION E EPTH: EPTH: ER: N ARY: :: Cen T. Fe	60' : Not lot Ap 0' to nent-l	Apploplica	icable ble	е	
FCBR_LOG (FINAL) 0 TO 1	UG	:	10	MS River Long Distance Sedime	nt Pip	elin	е		LC	G (OF E	BOR	RINC	S NO). E	3-38
Fugro	o Consul	tan	ts, Inc.	Jefferson Parish, Louisiana						ct No. 55 0	840	05		PLA	TE	15a

- 3. WOH = Weight of Hammer.
- 4. Push = Sample recovered with splitspoon due to low recovery with shelby tube.



	T					LOCATION: Con Dieto 1			CLA	ASSIF	ICAT	ION		,	SHE	AR S	TREN	GTH	
ե	į		الا الا		BLOWS PER FOOT	LOCATION: See Plate 1 COORDINATES: N 29° 38' 50.8"	ΣF	ļ							netror			nconfin	
DEPTH, FT		WATER LEVEI	SYMBOL		NS F OOT	W 90° 01' 34.3"	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	윽늘	STIC	PLASTICITY INDEX (PI)	♦To	rvane eld Va			Triax ure Va	cial
DEP		ATE	SAN		ا آب	SURFACE EL.: -1.8'	STF	I DE	ASSIN 00 SIE	WAT	LIQUID	PLASTIC LIMIT	LAST INDE)						
		≥			_	STRATUM DESCRIPTION		5	7. 20.	Ō			ш	0.			ER SQ F 0.6 0.		0
-	-					FAT CLAY (CH), soft, gray - with organic traces at 43'	42.0	-		44			-						
- 45	$\frac{1}{2}$					- with diganic traces at 43		F		64			-						
- 45 ⋅	7							F					_						
-	+							-					-						
F]							- ^-					-						
 50 -	1							65		59			-			^ '			
F]							Ē					-						
-	\exists							-		52			-						
_ _55 -	4							<u> </u>		58			_						
Ł	1							-					-						
F	7							-					-						
- 60 -	_			L		- soft to firm below 59'	60.0	63_		64			-	L	L_	▲•			
-	$\frac{1}{2}$						00.0	-					-						
ļ								<u>-</u>					-						
-	+							-					-						
 65 · -	7							-					-						
-	+							-					-						
F]							-					-						
 70 -	\dashv							F					-						
F	7							-					-						
L	1							Ŀ					-						
-75 -	4							<u> </u>					_						
<u>-</u> -	1												-						
1/16/1	+							-					-						
-80 -	╛							_					-						
2610.0	+							ŀ					-						
TE 04	_							<u> </u>					-						
EMPLA				_							COM	PI FT	ION E) ATF	· Δι	lanst	25 20	11	
Ā NO			erms	an	ıd syml	bols defined on Plates 20a and 20b.					TOTA	AL DE	PTH:	60'					
0 DA	2.	D	epth	to	mudlin	e below water surface = 1.9'.							EPTH: ER: N				е		
FUGF						of Hammer. recovered with splitspoon due to low recovery with:	shelby t	ube.					ER. IN ARY:			able			
GPJ					•		, .						: Cen		Bent	onite	Grout		
38400											LUG	∍EK:	T. Fe	erro					
04.55(
L) 0 TO 1	F	Ü	G	;	0	MS River Long Distance Sedime	nt Pip	elin	e		LC	G (OF B	OR	IN	G N	O. I	3-38	8
G (FINA	J			~~															
FCBR_LOG (FINAL) 0 TO 1 04.55084005.GPJ FUGRO DATA TEMPLATE 042610.GDT 11/16/11	ro	Cor	nsulta	ants	s, Inc.	Jefferson Parish, Louisiana						ct No. 550	840	05		PL	ATE	15	b

						Ι	CL A	ASSIF	ICAT	ION			SHEA	AR S	ΓREN	GTH	
ᅜ	VEL	L S	Ä	LOCATION: See Plate 1 COORDINATES: N 29° 38' 35.2"	≅E								enetrom			confined	_
DEPTH,	WATER LEVE	SYMBOL SAMPLES	BLOWS PER FOOT	W 90° 02' 05.6"	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	₽⊨	5 E E	PLASTICITY INDEX (PI)	♦To	netrom rvane eld Van			Triaxial ure Vane	•
DEP	ATE	SA	3LOV F	SURFACE EL.: -1.5'	STF	AG FIN	ASSIN 00 SIE	WAT	LIQUID	PLASTIC LIMIT	LAST INDE)				R SQ F		
	3			STRATUM DESCRIPTION		5	2.2	0				0			6 0.8		
-	+		N=WOF	ORGANIC CLAY (OH), very soft, black, with roots and grass		-		191			-						
ļ		<u>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</u>		PEAT (PT), gray, with organics, grass, and roots	2.0			338	232	64	168 -						
-	+	<u> </u>		10013	5.0	ŀ					-	-					
- 5 -	7			FAT CLAY (CH), very soft, gray, with peat	5.0	_		55			-	^					
Ŀ						-		50			-	•					
ŀ	-					ŀ		77			-	_					
—10 -	7					-					-						
-	-			- with silt traces and shells from 12' to 19'		-		80			-	↑					
F]			- dark gray from 14' to 16'		48	99	88	82	26	56	▲					
—15 -	┪					F		96			-	•					
-	-			- gray below 16'		-		102			-	▲					
ļ	1			- with organics at 18'		-		94	105	28	77						
-2 0	-					ŀ		67			-	^					
-	-					-					-						
			N=Push					53			-						
— 25	-					F					_						
F	-					-					-						
Ŀ				- soft, with silt layers below 28'		Ŀ					-						
— 30	_					53		82			_	ł	-				
ļ						ļ					-						
-	-					-		78			-						
- -35	-					Ĺ		61			_		•				
-35 -											-						
J.GDT	-					-					-						
-40 -40	₫				40.0	60_	ļ	67				<u> </u>	▲ ●			_	
04.55084005.GPJ FUGRO DATA TEMPLATE 042610.GDT						<u> </u>					-						_
NO JEME	TES										ION [PTH:		: Au	gust 2	25, 20	11	
DATA				abols defined on Plates 20a and 20b. The below water surface = 2.1'.							EPTH:		Appl	icable	9		
UGRO	3. \	WOR =	Weight	of Rod.	,				DRY	AUG	ER: N	lot Ap	plica				
PJ FI	4. I	-ush =	Sample	recovered with splitspoon due to low recovery with	shelby t	ube.					ARY: .: Cer			nite (Grout		
4005.C									LOG	GER:	T. Fe	erro					
4.5508																	
				T													
FCBR_LOG (FINAL) 0 TO 1	Æ	G	20	MS River Long Distance Sedime	ent Pip	elin	е		LC	G (OF E	BOR	INC	N	D. E	3-40	
(FINA																	
PO LOG				1.6						ect No.					. —	.	
Fug	jro C	onsulta	nts, Inc.	Jefferson Parish, Louisiana					04.	550	840	05		۲L	АГ	E 16	

- 3. WOR = Weight of Rod.



			LOCATION: See Plate 1			CLA	SSIF	ICAT	ION		S	SHEAF	R ST	REN	GTH	_
DEPTH, FT	WATER LEVEI SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 37' 25.7" W 90° 02' 50.8" SURFACE EL.: -2.5' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦ Ton Δ Fiel	d Vane KIP	S PER	Miniatu R SQ F1		al ● e ▲
		N=WOH	PEAT (PT), very soft, black				378				0.2	2 0.4	0.6	3 0.8	3 1.0	\dashv
		N=Push			- -		221			-						
-5-		N=Push	FAT CLAY (CH), dark gray	4.0	_		115	68	20	48 –						
	<u> </u>	\	PEAT (PT), very soft, dark gray	6.0						-					+	
- - -10 - -					- - - -		240 175	295	77	- - - 218	A					
			FAT CLAY (PT), very soft, gray, with organics	13.0			65	293	11	210	A				+	
—15 — -					_		97			-	•					
- - - -20 -					- - -		89 82			-	A					
- - - -25 -			LEAN CLAY (CL) , very soft to soft, gray, with silt layers	- 23.0	62	99	62	37	17	20		•				
- -30 - - -		N=WOR		24.0	- - - -		65			- - - -						
-35 - - - -			FAT CLAY (CH), soft to firm, gray	+ 34.0	_ 56 - - -		75 36			- - - -		40				
-40 -					_		32			<u>-</u>		•				
	1. Terms		pols defined on Plates 20a and 20b. e below water surface = 3.0'.					TOT	AL DE	ION E PTH: EPTH:	60'	_			11	

- 2. Depth to mudline below water surface = 3.0'.
- 3. WOH = Weight of Hammer.
- 4. WOR = Weight of Rod.
- 5. Push = Sample recovered with splitspoon due to low recovery with shelby tube.

DRY AUGER: Not Applicable WET ROTARY: 0' to 60'

BACKFILL: Cement-Bentonite Grout

LOGGER: T. Ferro



FCBR_LOG (FINAL) 0 TO 1 04.55084005.GPJ FUGRO DATA TEMPLATE 042610.GDT 11/16/11

MS River Long Distance Sediment Pipeline

LOG OF BORING NO. B-41

Jefferson Parish, Louisiana Fugro Consultants, Inc.

Project No. 04.55084005

PLATE 17a

					LOCATION: See Plate 1			CLA	SSIF	ICAT	ION			SHE	AR S	TREN	GTH	
L.		WATER LEVEI	OL ES	BLOWS PER FOOT	COORDINATES: N 29° 37' 25.7"	₽F.	Ť,	0.%	%			~ (□Pe	netron	neter	Un	confine	d▼
DEPTH, FT	-	FR	SYMBOL SAMPLES		W 90° 02' 50.8"	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)		rvane eld Var	ne	Miniatu	Triaxia ure Van	
DEF	j	/ATE	SA	BLO	SURFACE EL.: -2.5'	STI	NT D	ASSII 00 SII	WA	SE	PLA	PLAS' INDE		ĸ	IPS PE	R SQ F	г	
		>	$\overline{}$		STRATUM DESCRIPTION		ס	8 8					0.			.6 0.8		
ŀ	-				FAT CLAY (CH), soft to firm, gray		-					-						
- 45	- 						85		34			_		•	•			
F ^`	<i>-</i>						-					-						
t	-						-					-						
ŀ	_						-		60 51			-						
 50) —						_					_			_			
-	_						-					-						
L	_											-						
- 55	5 —						73		49			_			•			
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-	_						-		55			-						
- 60	- า —					60.0		l	67		L	- -	L	L_	L_:			
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910.GF - - - - - - - - - - - -	— ر -						F					_						
E 042	-						E					-						
/PLAT										00:	D					20.00	11	
A TEN		<u>ES:</u>	orma	and ave	shale defined on Plates 20s and 20h							ION E PTH:		: Au	gust 2	26, 20	17	
D DAT					ubols defined on Plates 20a and 20b. ne below water surface = 3.0'.					CAVE	ED DE	EPTH:	Not			е		
-UGR(3	8. W	/OH =	- Weight	of Hammer.							ER: N ARY:			able			
3PJ F					of Rod. recovered with splitspoon due to low recovery with s	shelby t	ube.					: Cen			onite	Grout		
4005.0				-	·	-				LOG	GER:	T. Fe	erro					
1.5508																		
0 1 04					T													
FCBR_LOG (FINAL) 0 TO 1 04.55084005.GPJ FUGRO DATA TEMPLATE 042610.GDT 11/16/11	f	u	GI	20	MS River Long Distance Sedimer	nt Pip	elin	е		LC	G (OF E	BOR	INC	3 NO	O. E	3-41	
(FINA	V																	
5 Log											ect No.							
HOE FI	ugro	CO	nsulta	nts, Inc.	Jefferson Parish, Louisiana					04.	550	840	05		۲LA	TE	17)

						LOCATION: See Plate 1			CLA	ASSIF	ICAT	ION			SHEA	AR ST	ΓREN	GTH
ОЕРТН, FT	WATER LEVE	SYMBOL	SAIVITLES	BLOWS PER FOOT		COORDINATES: N 29° 36' 50.4" W 90° 03' 34.5" SURFACE EL.: -2.8'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦ To		e PS PE	Miniatu R SQ F	
	Н	11/	M	I=WO	R	PEAT (PT), very soft, black, with roots				748				0	.2 0.	4 0.	6 0.8	1.0
 		<u> </u>		1-VV		- with wood pieces below 4'		- - -		215		68	174_	A				
 		<u> </u>				- soft at 7' - dark gray below 8'		- - -		319 204			- - -	•	•			
		<u> </u>						24	83	223	159	40	119	▲				
 —15 —						- with sand pockets below 12' LEAN CLAY (CL), very soft, dark gray, with sand pockets	13.0	_		33 35			-	A				
 —20 —						FAT CLAY (CH), very soft to soft, gray	10.0	- - -		98 77 72	66	23	43	A				
 - 25 - 				√l=Pus	h			- - - - -		84			- - - - -	-				
-30 								_ 54 - - -		73 91			- - - -					
 -40				- — —			40.0	- - - _ <u>57</u>		75			- - - -		A •			
2 3	. T 2. C 3. V	erm epth	to =	mud Weigl	ine nt o	ols defined on Plates 20a and 20b. below water surface = 3.3'. Not Rod. ecovered with splitspoon due to low recovery wi	th shelby t	I ube.			TOTA CAVI DRY WET BACI	AL DE ED DI AUG ROT KFILL	ION [EPTH: EPTH ER: N ARY: :: Cer	40' : Not Not A _l 0' to ment-	Applica oplica	cable ble)	111
J	u	G	:	20		MS River Long Distance Sedim	nent Pip	elin	e		LC)G (OF E	BOR	RING	S NO). E	3-42
Fugro	o Co	nsul	tan	ts, Inc		Jefferson Parish, Louisiana						ect No. 55 0	840	05		PL	ATE	E 18



		LOCATION: See Plate 1						SHEAR STRENGTH								
DEPTH, FT	WATER LEVEL SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 32.9" W 90° 03' 34.7" SURFACE EL.: -2.6' STRATUM DESCRIPTION	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	□Pe ♦To	netrome rvane Ild Vane KII	eter S PE	Uı	nconfir Triax ture Va	ned ▼ xial ● ane ▲
		N=Push	PEAT (PT), very soft, dark gray and black,		-		379			_	0.	2 0.2	+ 0.	.6 0.	.6 1	.0
-			with organics and roots	1.0	- - 25	63	518 236	203	55	- 148	A					
-5 - - -			LEAN CLAY (CL), soft to firm, gray, with organics and wood	4.0	_ - -		61				4		•			
- - -10 - - -			FAT CLAY (CH), soft to firm, gray, with organics and wood	+ 8.0	- - - - -		106 64 78	88	36	52 _		•		• 🗆		
- 15 -			- with shell fragments at 14'	15.0	_		94			-						
- - - -			ORGANIC CLAY (OH), very soft, gray, with wood		- - - 31	73	153 171	200	52	148	4	`				
20 - - - -		N=Push	FAT CLAY (CH), very soft to soft, gray	20.0	-	70	67	62	22	- - - 40 -	_					
25 - - - - -		N=Push			- - -		78			- - -						
30 - - -					- - - - 55		77			- - - -						
-35 - - - - - 40 -					- - - -		76 72			- - - -	-	•				
NO	NOTES: 1. Terms and symbols defined on Plates 20a and 20b. 2. Depth to mudline below water surface = 3.0'. 3. Push = Sample recovered with splitspoon due to low recovery with shelby tube. COMPLETION DATE: August 28, 2011 TOTAL DEPTH: 60' CAVED DEPTH: Not Applicable DRY AUGER: Not Applicable															

WET ROTARY: 0' to 60'

BACKFILL: Cement-Bentonite Grout

LOGGER: T. Ferro



FCBR_LOG (FINAL) 0 TO 1 04.55084005.GPJ FUGRO DATA TEMPLATE 042610.GDT 11/16/11

MS River Long Distance Sediment Pipeline

LOG OF BORING NO. B-43

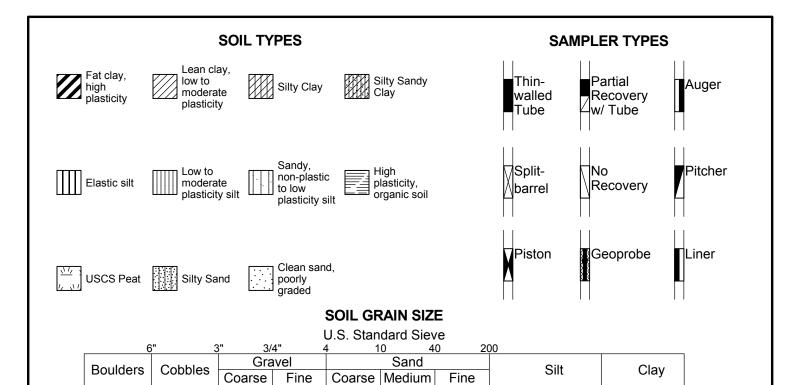
Fugro Consultants, Inc.

Jefferson Parish, Louisiana

Project No. 04.55084005

PLATE 19a

	~	LOCATION: See Plate 1		CLASSIFICATION SHEAR STRENGTH							GTH			
DEPTH, FT WATER LEVE SYMBOL SAMPLES	BLOWS PER FOOT	COORDINATES: N 29° 36' 32.9" W 90° 03' 34.7" SURFACE EL.: -2.6'	STRATUM DEPTH, FT	UNIT DRY WT, PCF	PASSING NO. 200 SIEVE, %	WATER CONTENT, %	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX (PI)	♦To	netron rvane eld Var	ie	Miniat	nconfined ▼ Triaxial ● ure Vane ▲
	B	STRATUM DESCRIPTION	_	S	20 PA	8	8			۱ ،	.2 0		R SQ F	T 8 1.0
		FAT CLAY (CH), very soft to soft, gray		_					_	Ť				
-45 -45 				55 55 		74 61 61			- - - - -		•	•		
55		- with silt layers below 53'		58 - - -		73 72			- - - - -		•	•		
-60			60.0			63 69			- 			 		
				- - - - - - - - - - - -										
-80 —				-					_					
E 042(E					-					
2. Depth t	o mudlin	bols defined on Plates 20a and 20b. e below water surface = 3.0'. recovered with splitspoon due to low recovery with	shelby t	ube.			TOTA CAVI DRY WET BACK	AL DE ED DI AUG ROT KFILL	FION EPTH: EPTH: ER: N ARY: :: Cen T. Fe	60' Not lot Ap 0' to nent-l	Apploplica	icable	е	
INAL) 0 TO	50	MS River Long Distance Sedime	nt Pip	elin	е		LC)G (OF E	BOR	INC	3 N	O. E	3-43
Fugro Consulta	Fugro Consultants, Inc. Jefferson Parish, Louisiana Project No. 04.55084005 PLATE 19b							19b						



2.00

0.075

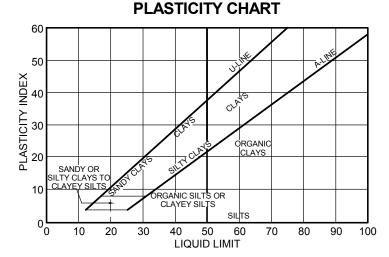
0.005

(mm)

75.0

19.0

4.75



SOIL STRUCTURE

Slickensided ·····	Having planes of weakness that appear slick and glossy.
Fissured·····	······ Containing shrinkage or relief cracks, often filled with fine sand or silt; usually more or less vertical.
Pocket·····	······ Inclusion of material of different texture that is smaller than the diameter of the sample.
Parting·····	······ Inclusion less than 1/8 inch thick extending through the sample.
Seam·····	······ Inclusion 1/8 inch to 3 inches thick extending through the sample.
Layer·····	····· Inclusion greater than 3 inches thick extending through the sample.
Laminated · · · · · · · · · · · · · · · · · · ·	······ Soil sample composed of alternating partings or seams of different soil type.
Interlayered ······	······ Soil sample composed of alternating layers of different soil type.
Intermixed · · · · · · · · · · · · · · · · · · ·	······ Soil sample composed of pockets of different soil type and layered or laminated structure is not evident.
Calcareous · · · · · · · · · · · · · · · · · · ·	······ Having appreciable quantities of carbonate.
Carbonate ·····	······ Having more than 50% carbonate content.

-fug Ro	TERMS AND SYMBOLS USED ON BORING LOGS
	SOIL CLASSIFICATION (1 of 2)
Fugro Consultants, Inc.	Project No. 04.55084005 PLATE 20a

STANDARD PENETRATION TEST (SPT)

A 2-in.-OD, 1-3/8-ID split spoon sampler is driven 1.5 ft into undisturbed soil with a 140-pound hammer free falling 30 in. After the sampler is seated 6 in. into undisturbed soil, the number of blows required to drive the sampler the last 12 in. is the Standard Penetration Resistance or "N" value, which is recorded as blows per foot as described below.

SPLIT-BARREL SAMPLER DRIVING RECORD

Blows Per Foot	Description
25 · · · · · · · · · · · · · · · · · · ·	25 blows drove sampler 12 inches, after initial 6 inches of seating.
50/7" · · · · · · · · · · · · · · · · · · ·	50 blows drove sampler 7 inches, after initial 6 inches of seating.
Ref/3" · · · · · · · · · · · · · · · · · · ·	50 blows drove sampler 3 inches during initial 6-inch seating interval.

NOTE: To avoid damage to sampling tools, driving is limited to 50 blows during or after seating interval.

DENSITY OF GRANULAR SOILS

STRENGTH OF COHESIVE SOILS

Descriptive Term	*Relative Density, %	**Blows Per Foot (SPT)	Term	Undrained Shear Strength, ksf	Blows Per Foot (SPT) (approximate)
Very Loose······	15	0 to 4	Very Soft ·····	·····< 0.25 ······	·····0 to 2
Loose······	·····15 to 35 ·····	5 to 10	Soft ·····	·····0.25 to 0.50 ······	·····2 to 4
Medium Dense	·····-35 to 65 ·····	·····-11 to 30	Firm·····	····· 0.50 to 1.00 ······	4 to 8
Dense	·····65 to 85 ·····	·····31 to 50	Stiff ·····	······1.00 to 2.00 ······	·····8 to 16
Very Dense······	> 85	·····> 50	Very Stiff ·····	·····-2.00 to 4.00 ······	·····16 to 32
*Estimated from	m sampler driving re	ecord	Hard ······	·····> 4.00 ·····	> 32

^{**}Requires correction for depth, groundwater level, and grain size.

SHEAR STRENGTH TEST METHOD

U = Unconfined Q = Unconsolidated - Undrained Triaxial

P = Pocket Penetrometer T = Torvane V = Miniature Vane F = Field Vane

HAND PENETROMETER CORRECTION

Our experience has shown that the hand penetrometer generally overestimates the in-situ undrained shear strength of over consolidated Pleistocene Gulf Coast clays. These strengths are partially controlled by the presence of macroscopic soil defects such as slickensides, which generally do not influence smaller scale tests like the hand penetrometer. Based on our experience, we have adjusted these field estimates of the undrained shear strength of natural, overconsolidated Pleistocene Gulf Coast soils by multiplying the measured penetrometer reading by a factor of 0.6. These adjusted strength estimates are recorded in the "Shear Strength" column on the boring logs. Except as described in the text, we have not adjusted estimates of the undrained shear strength for projects located outside of the Pleistocene Gulf Coast formations.

Information on each boring log is a compilation of subsurface conditions and soil or rock classifications obtained from the field as well as from laboratory testing of samples. Strata have been interpreted by commonly accepted procedures. The stratum lines on the logs may be transitional and approximate in nature. Water level measurements refer only to those observed at the time and places indicated, and can vary with time, geologic condition, or construction activity.

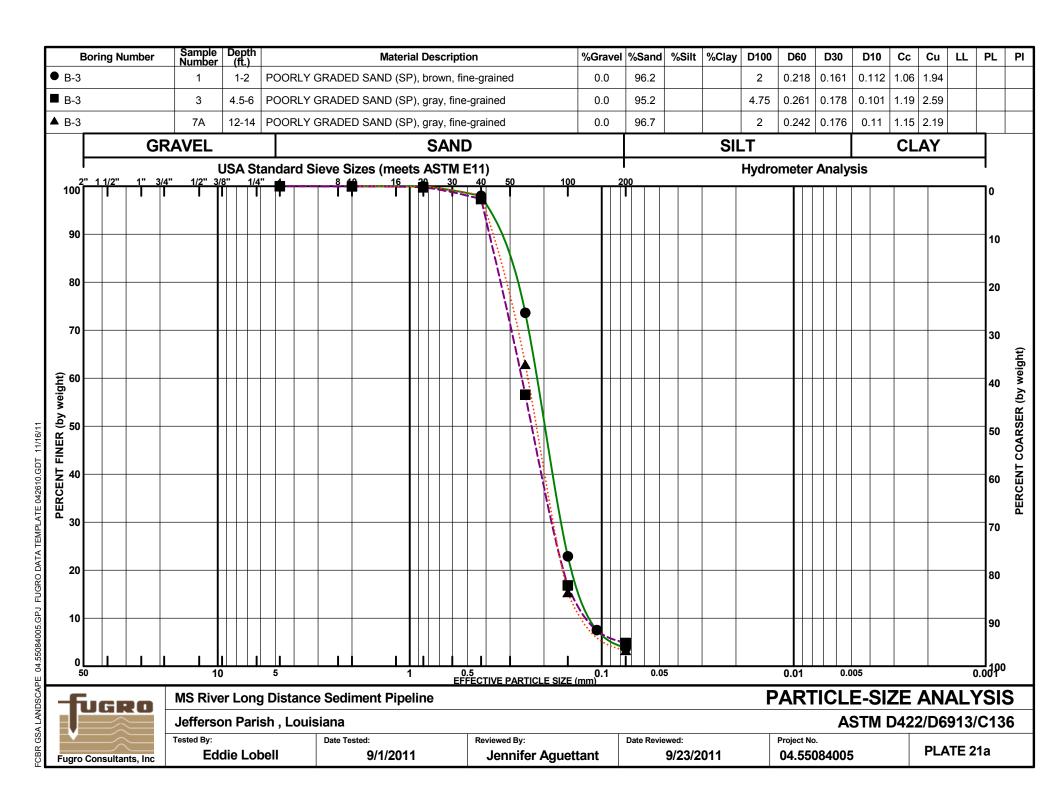


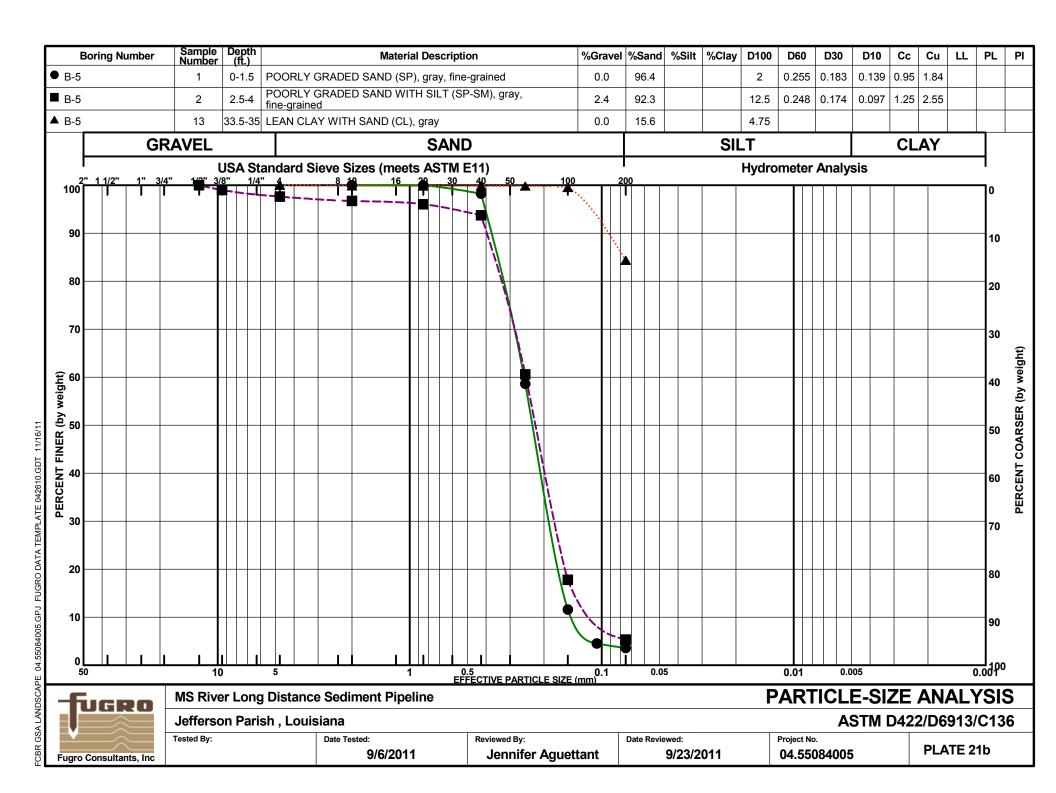
TERMS AND SYMBOLS USED ON BORING LOGS

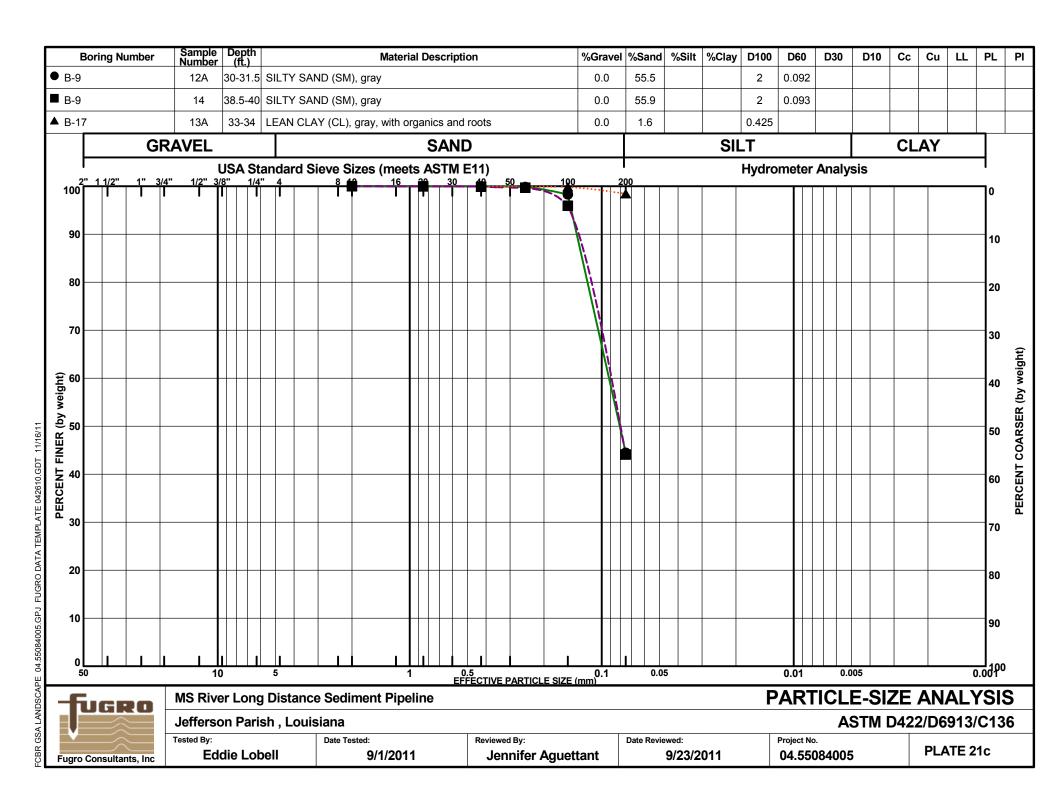
SOIL CLASSIFICATION (2 of 2)

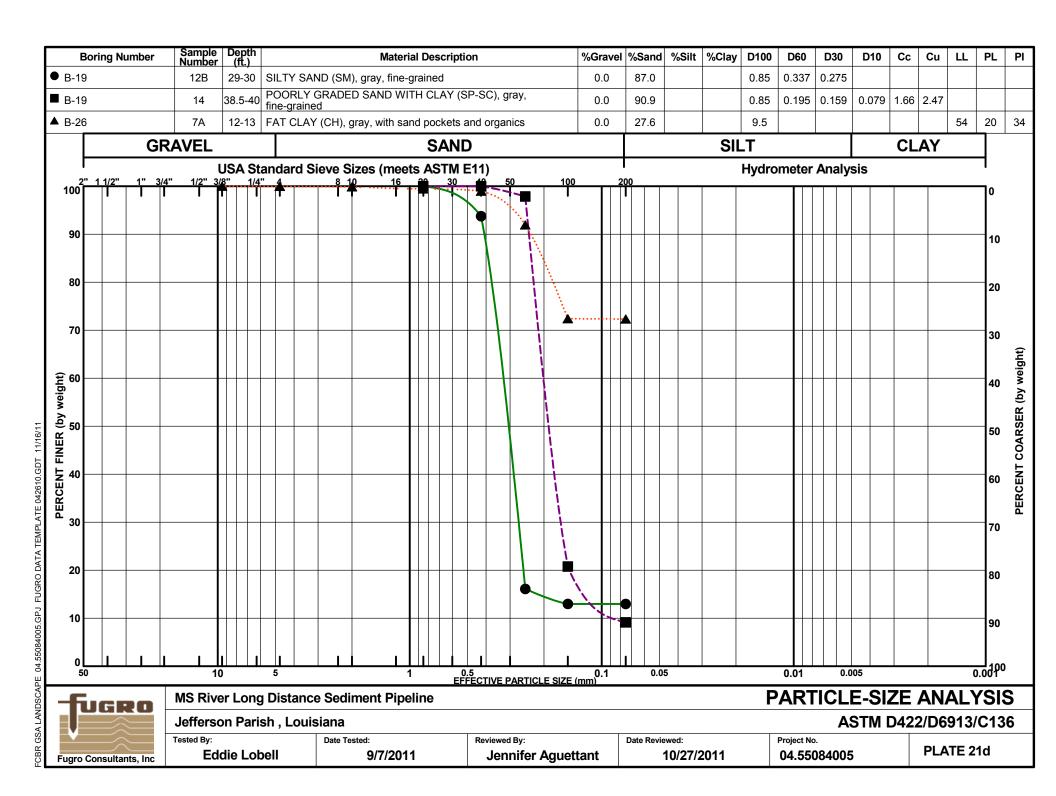
Project No. **04.55084005**

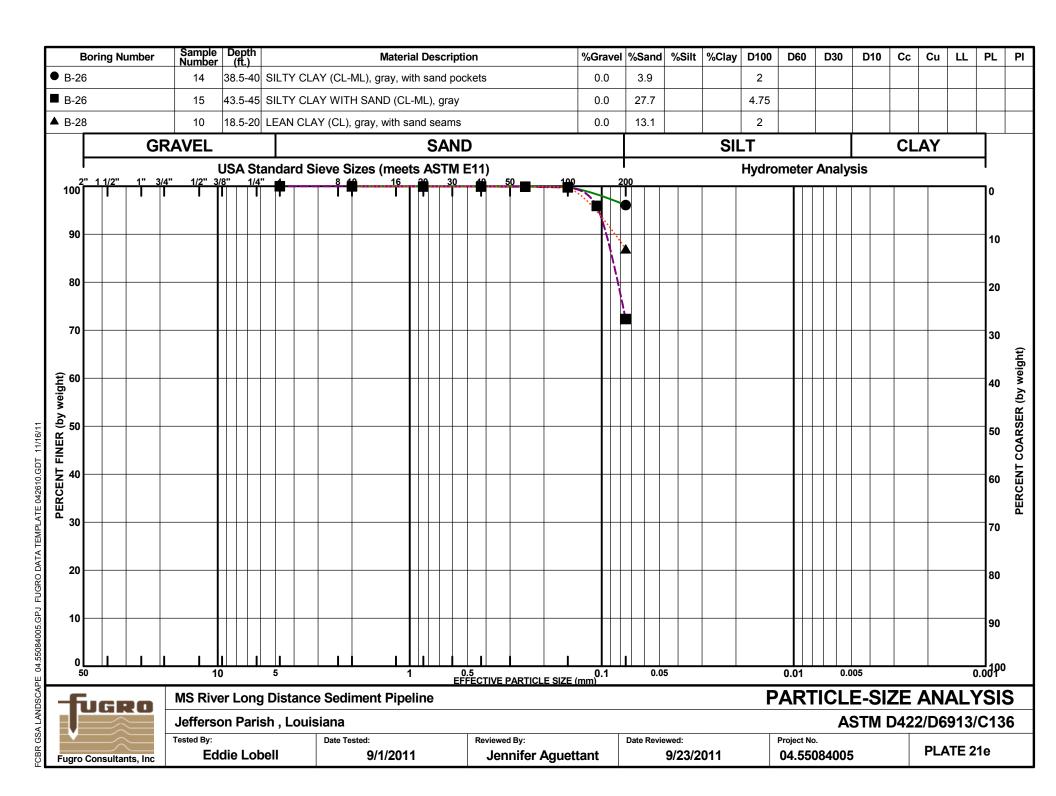
PLATE 20b

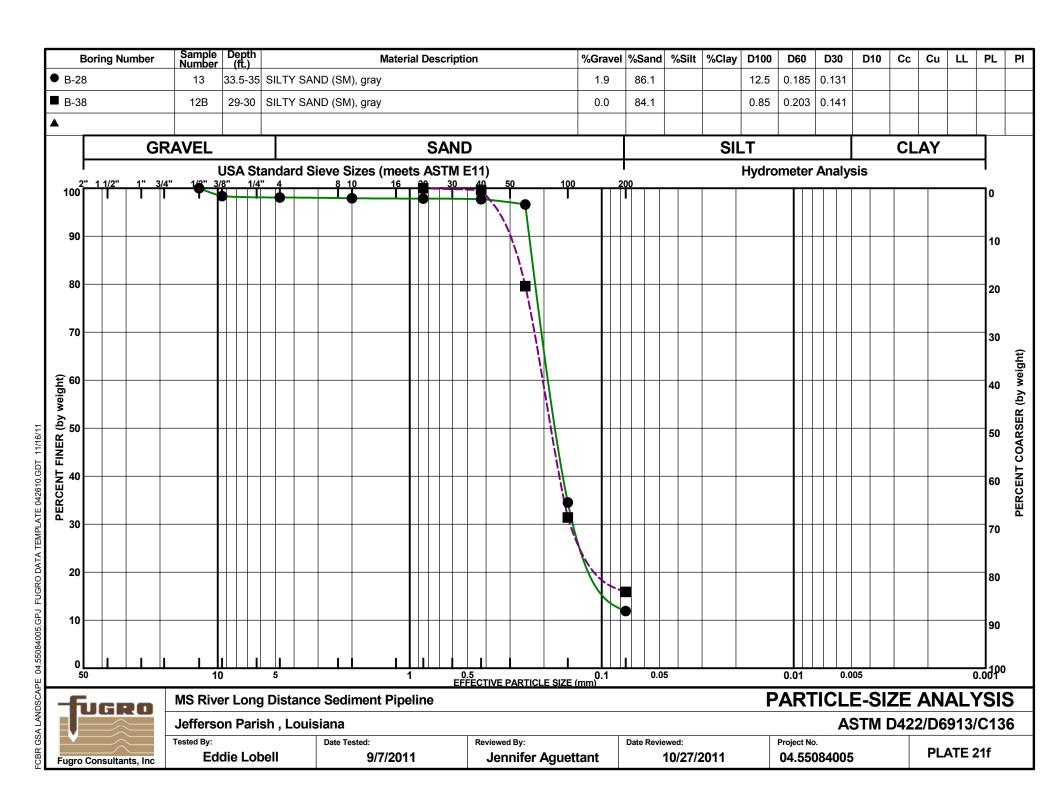


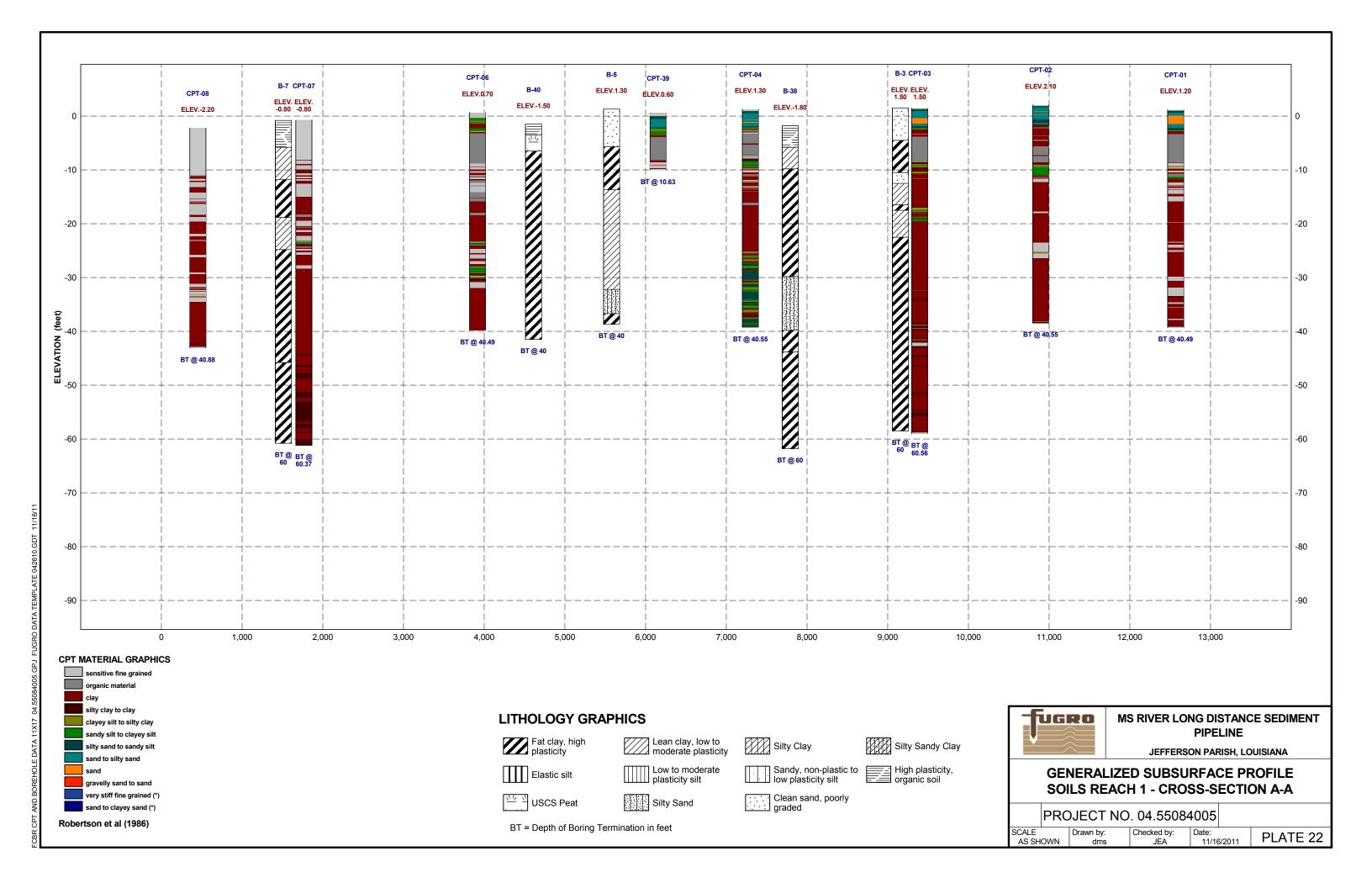


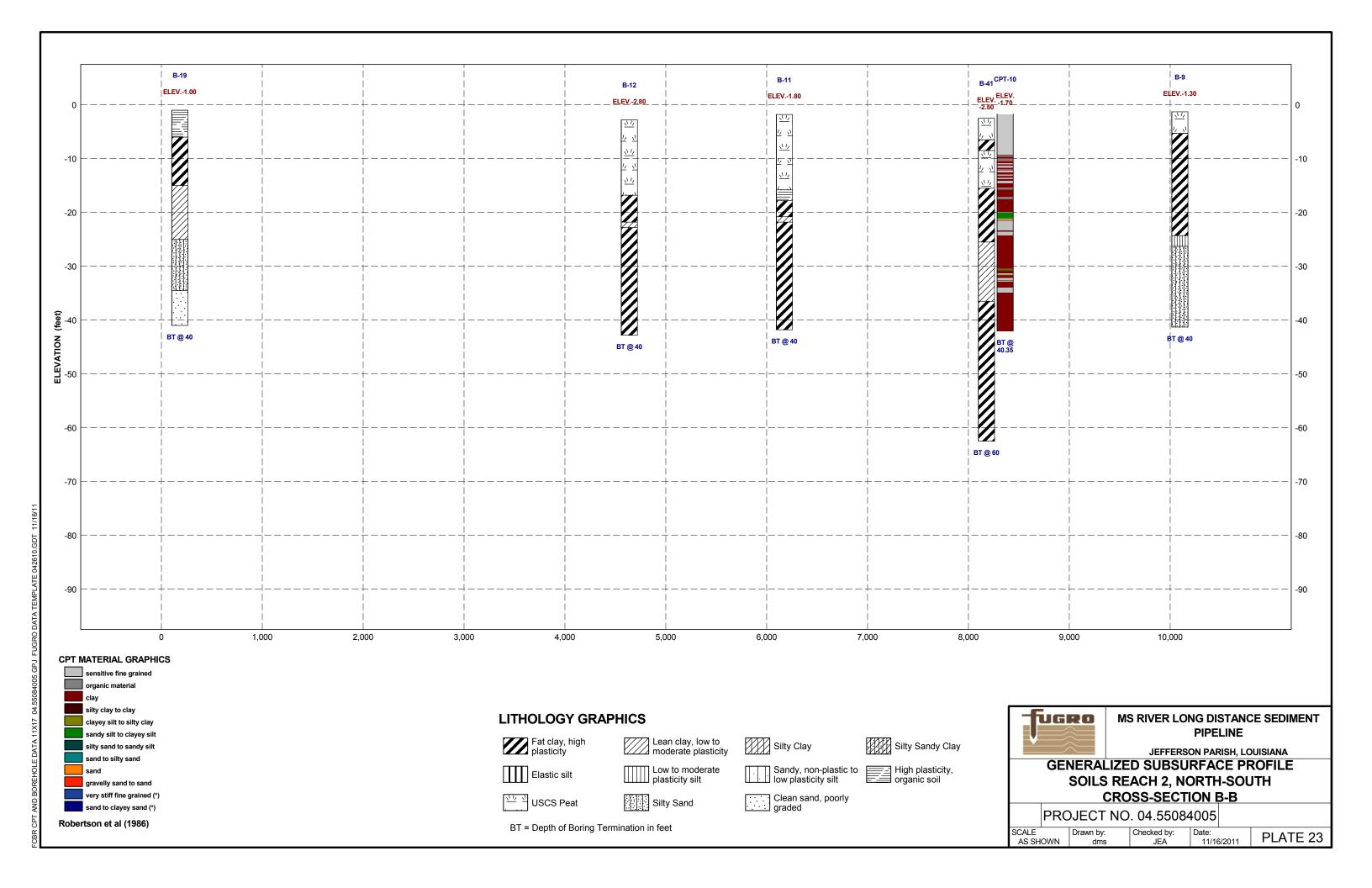


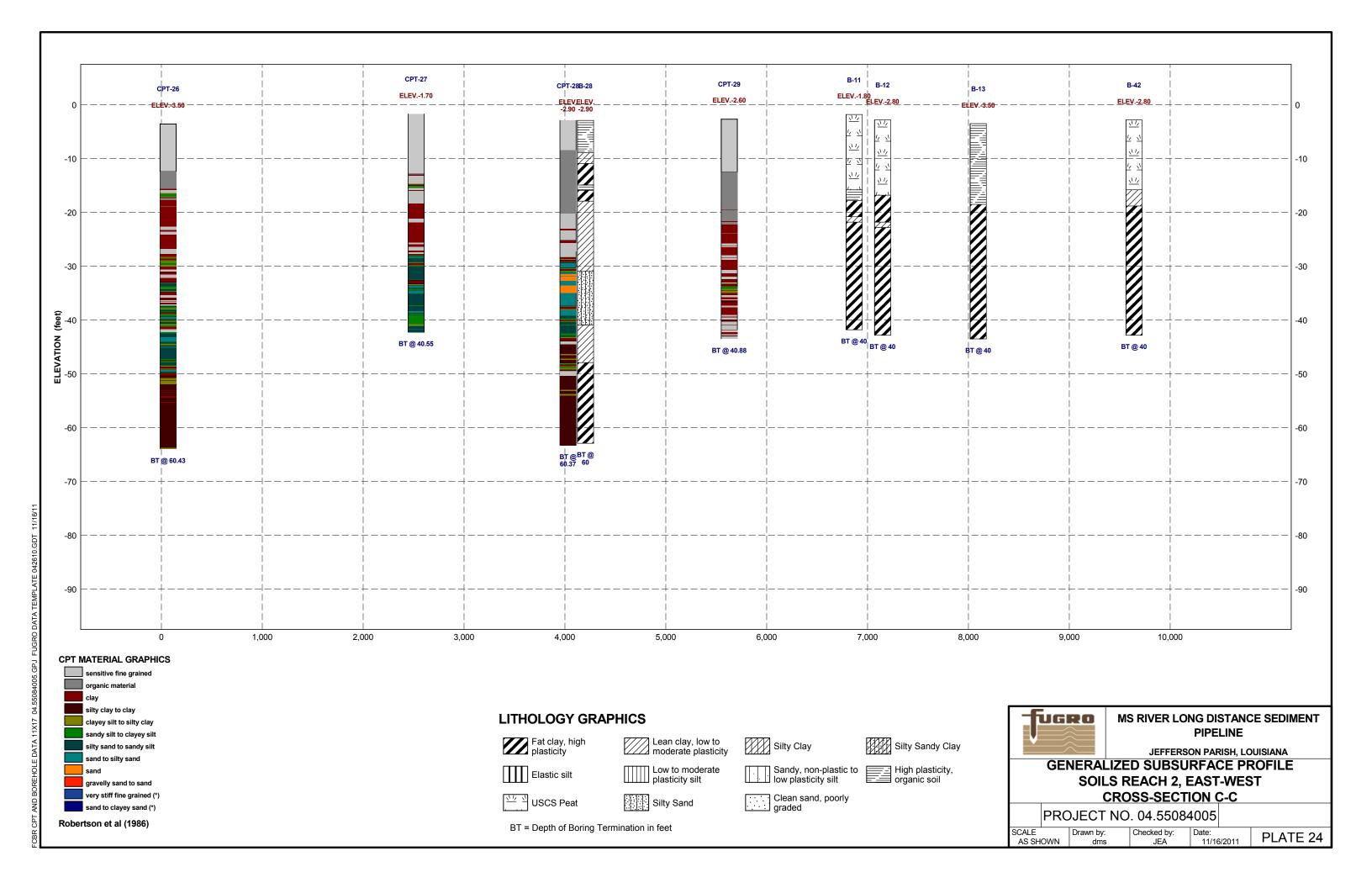


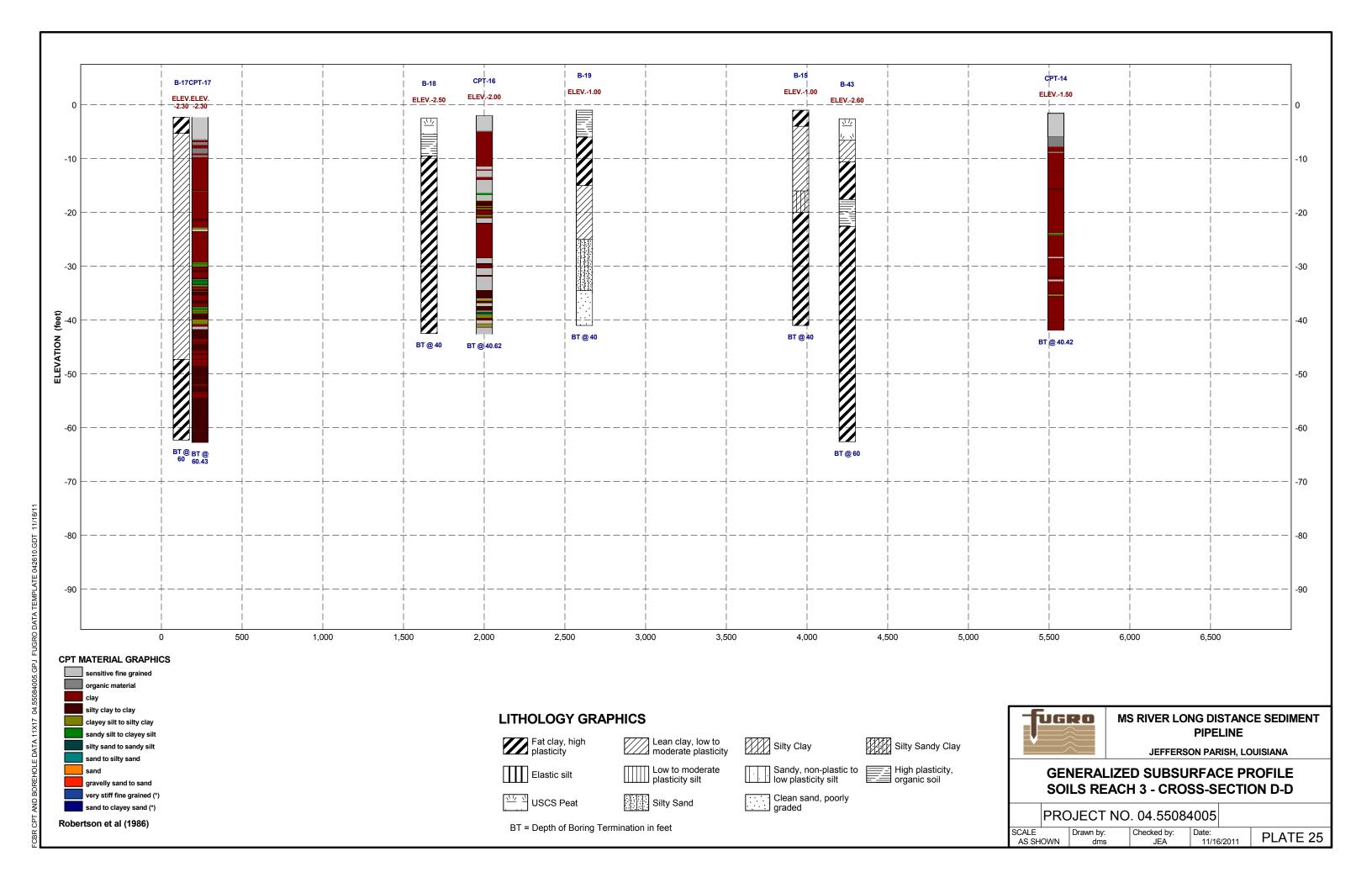


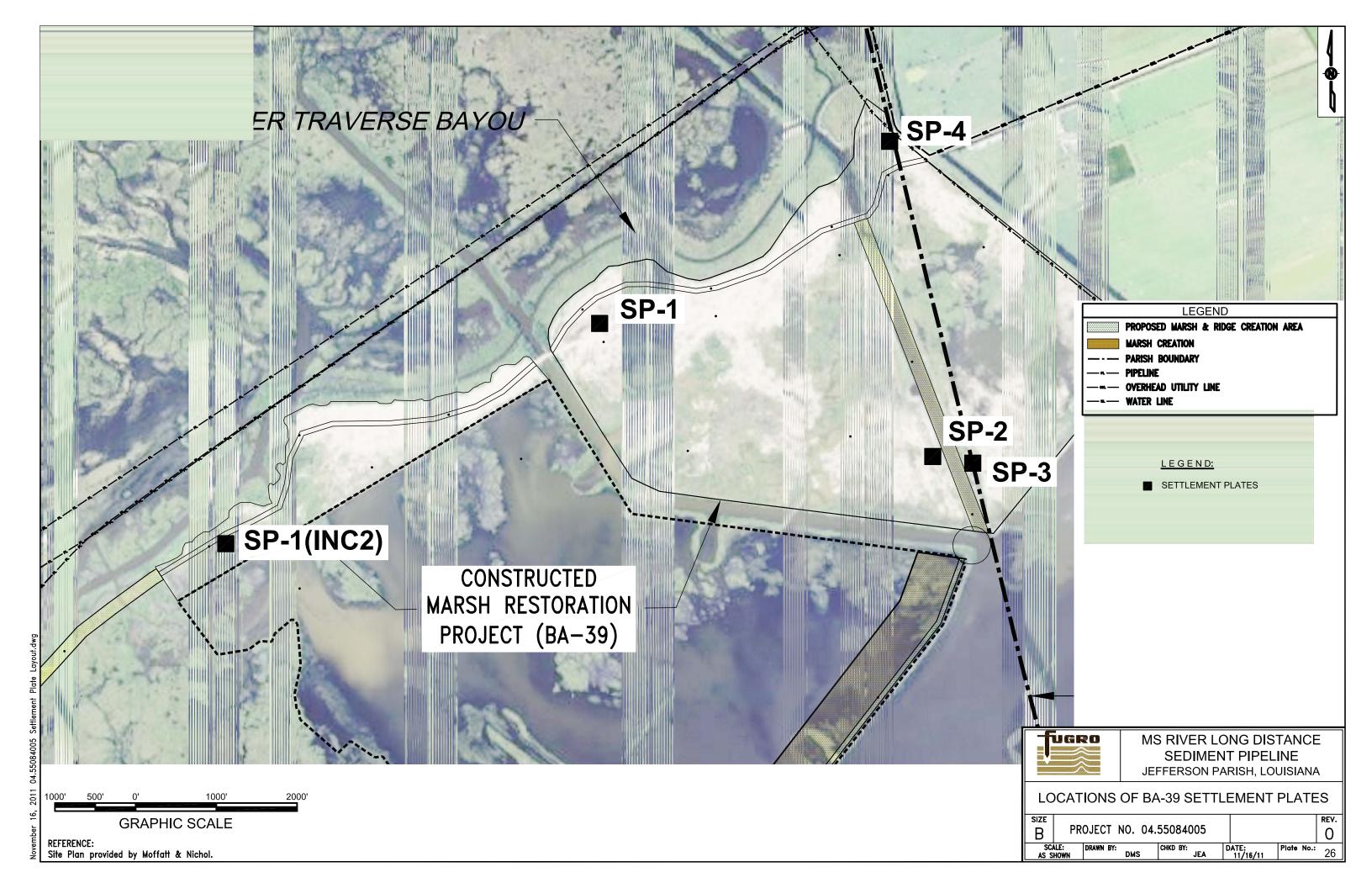


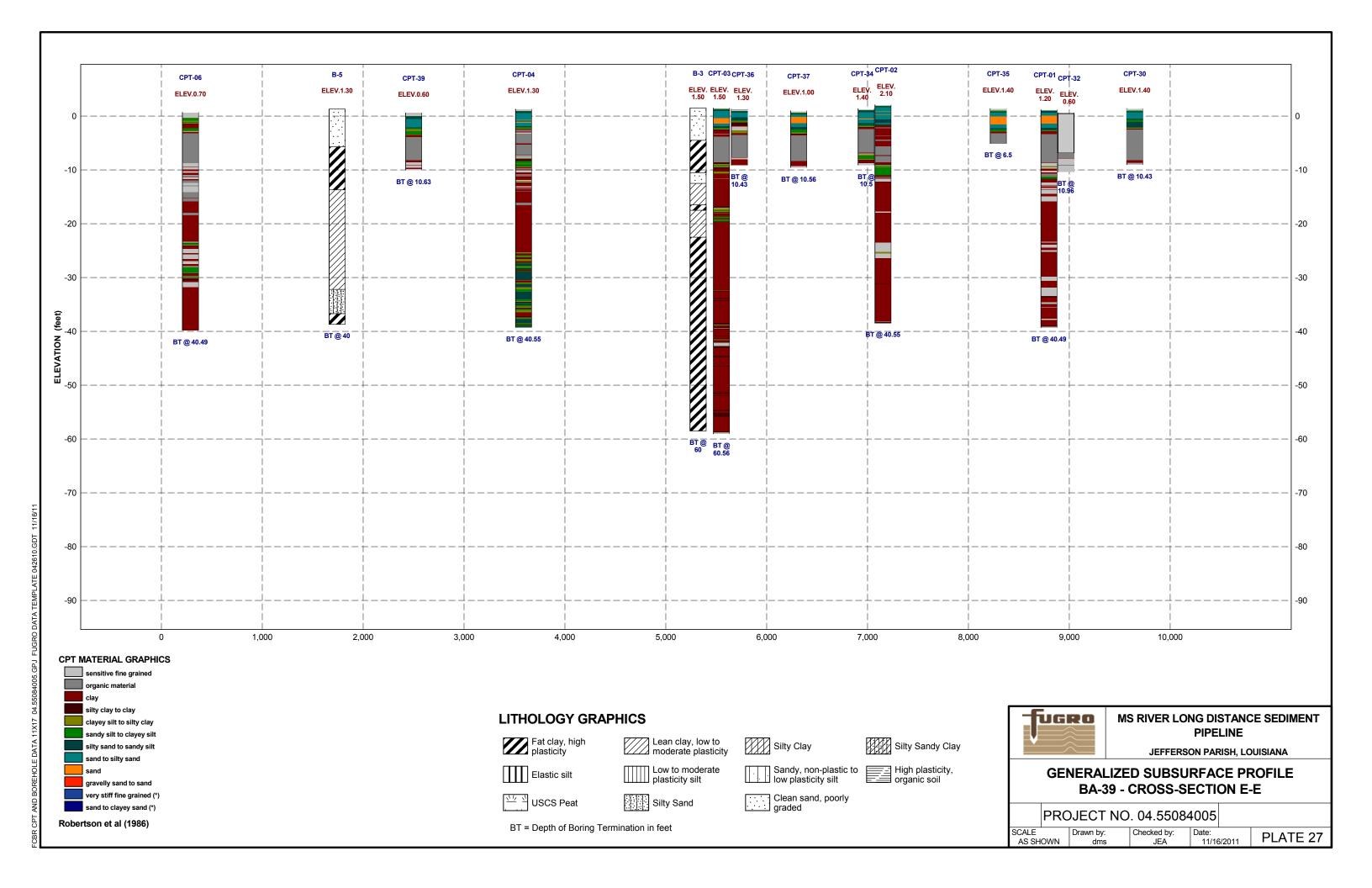


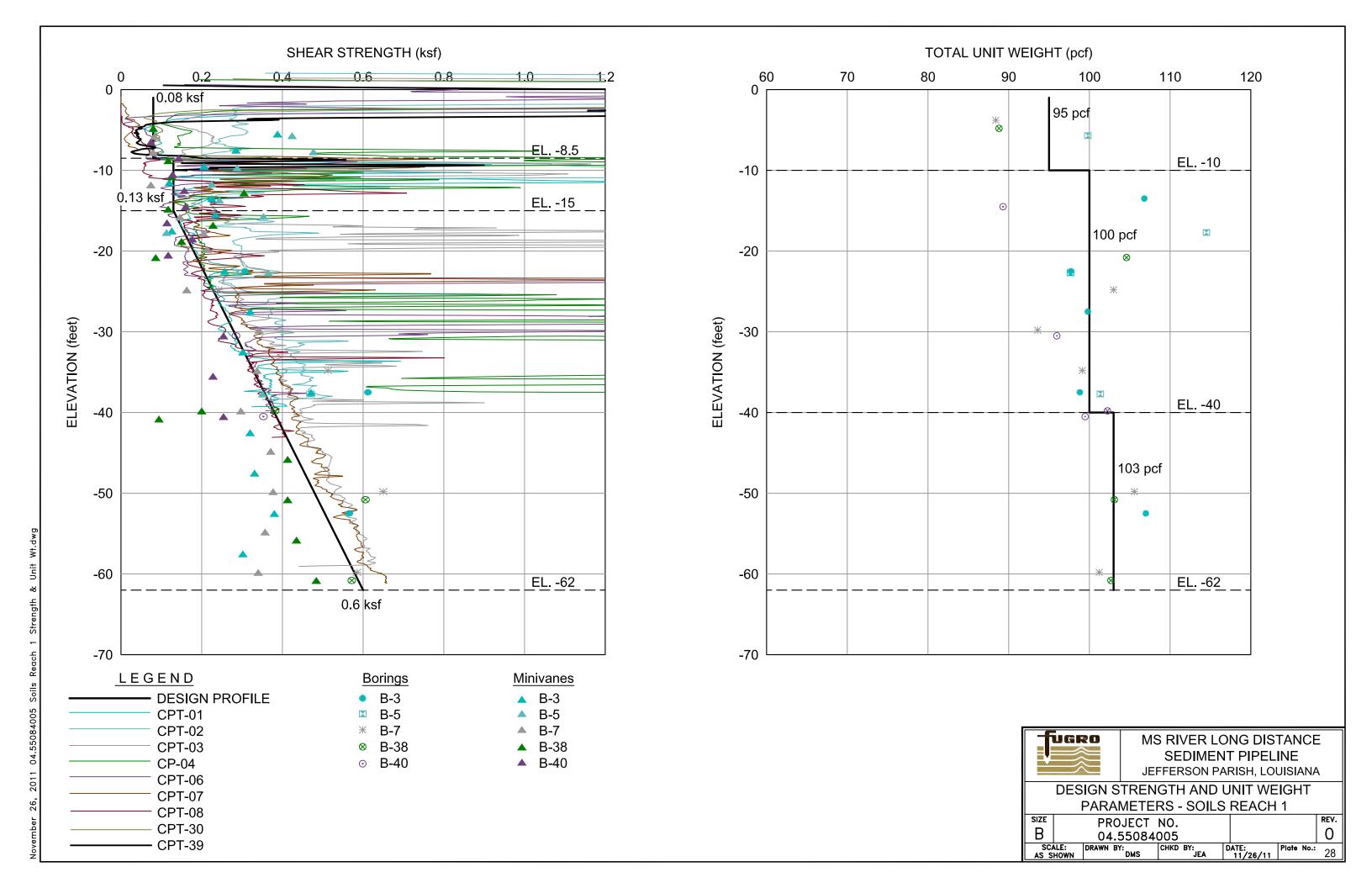


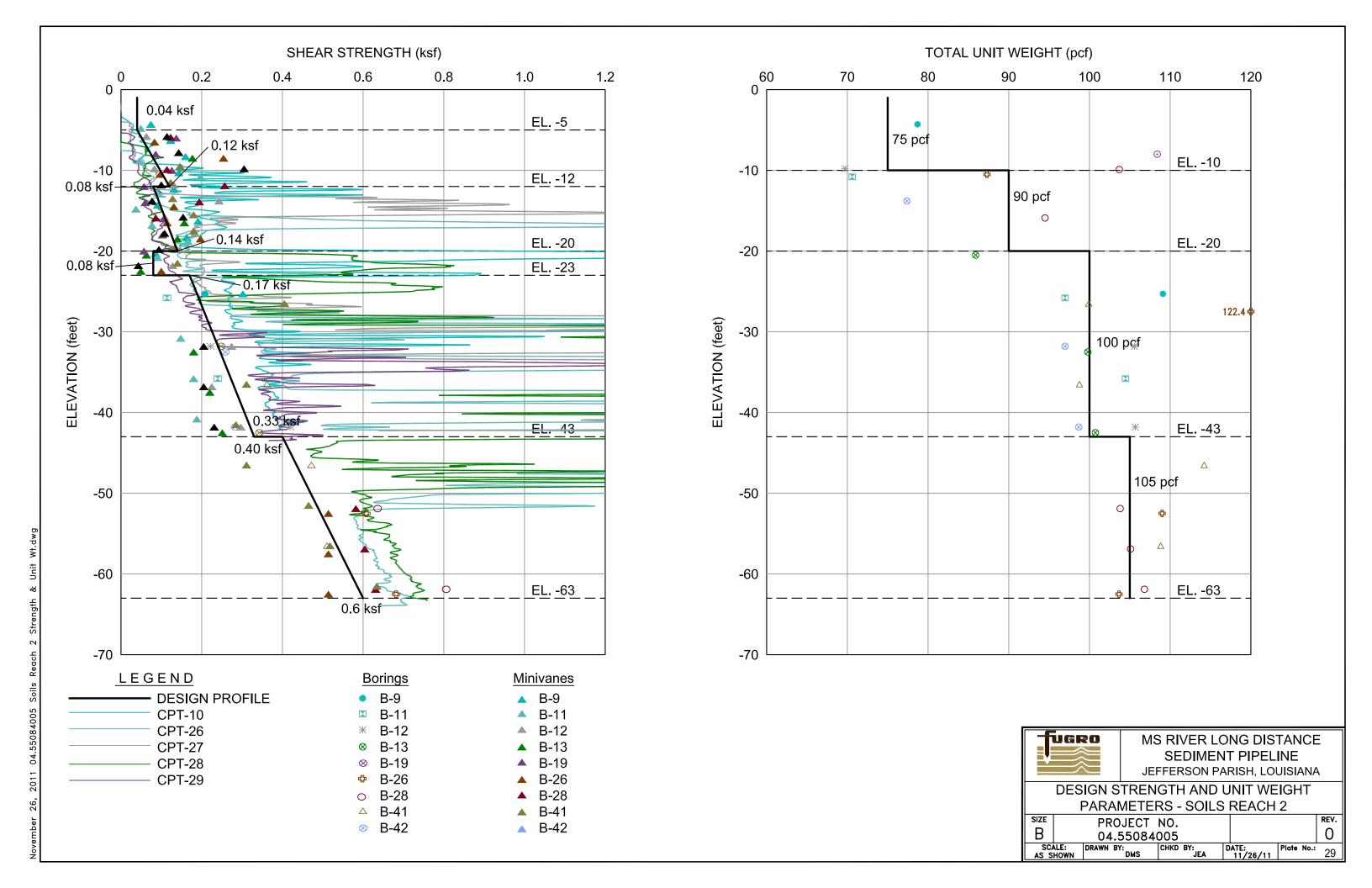


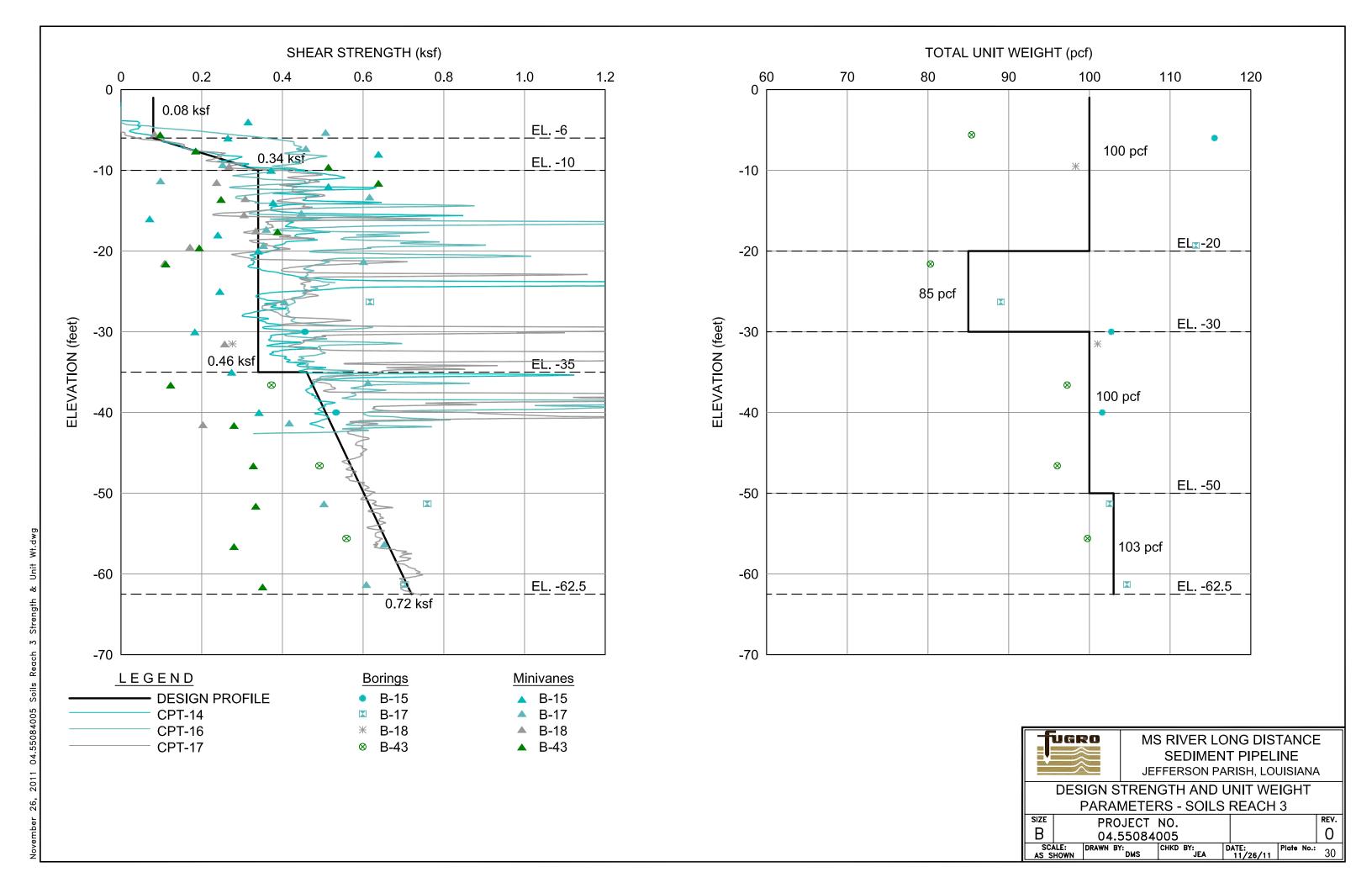












SOILS REACH 1 - MUDLINE EL. -1.0'

Time (months)	Description of Activity	Top of Fill Elevation (feet) EL. +3.0 EL. +2.5 EL. +2.0		
0.25	End of Fill Placement	3.00	2.50	2.00
1.25	Process Survey	2.64	2.14	1.69
60	5 yr Post Const.	1.33	0.93	0.60
240	20 yr Post Const.	0.95	0.61	0.32

SOILS REACH 2 - MUDLINE AT EL. -2.0'

	Time (months)	Description of Activity	Top of F	Fill Elevation	on (feet)
			EL. +3.5 EL. +3.0 EL. +2.		
	0.25	End of Fill Placement	3.50	3.00	2.00
	1.25	Process Survey	3.12	2.64	1.70
	60	5 yr Post Const.	1.60	1.16	0.42
	240	20 yr Post Const.	0.94	0.51	-0.12

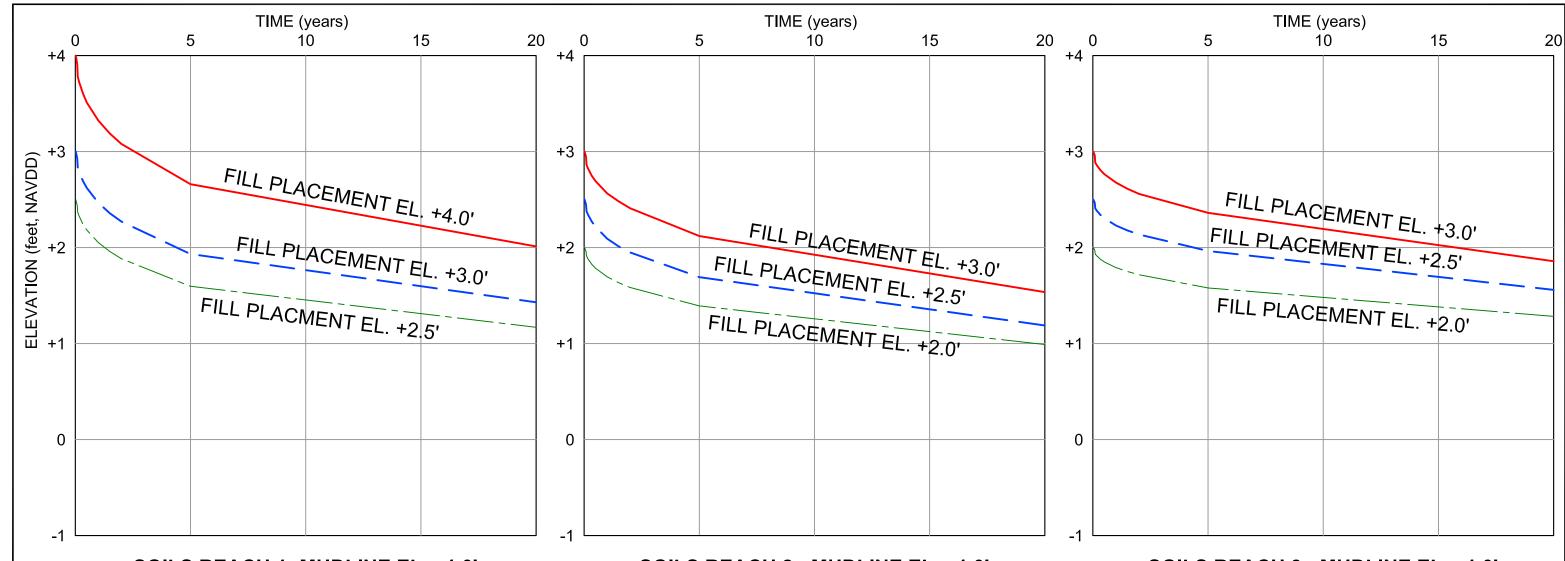
SOILS REACH 3 - MUDLINE AT EL. -2.5'

Time (months)	Description of Activity	Top of Fill Elevation (feet)		
		EL. +3.0 EL. +2.5 EL. +2.0		
0.25	End of Fill Placement	3.00	2.50	2.00
1.25	Process Survey	2.70	2.22	1.74
60	5 yr Post Const.	1.56	1.16	0.74
240	20 yr Post Const.	0.68	0.39	0.02



MS RIVER LONG DISTANCE SEDIMENT PIPELINE JEFFERSON PARISH, LOUISIANA

TIME RATE OF SETTLEMENT - PIPELINE CORRIDOR - LOWER BOUND INTERFACE



SOILS REACH 1- MUDLINE EL. +1.0'

Time (months)	Description of Activity	Top of Fill Elevation (feet)		
		EL. +4.0 EL. +3.0 EL. +2.5		EL. +2.5
0.25	End of Fill Placement	4.00	3.00	2.50
1.25	Process Survey	3.78	2.84	2.37
60	5 yr Post Const.	2.66	1.93	1.60
240	20 yr Post Const.	2.01	1.43	1.17

SOILS REACH 2 - MUDLINE EL. +1.0'

Time (months)	Description of Activity	Top of Fill Elevation (feet)		
		EL. +3.0 EL. +2.5 EL. +2.0		EL. +2.0
0.25	End of Fill Placement	3.00	2.50	2.00
1.25	Process Survey	2.86	2.38	1.91
60	5 yr Post Const.	2.12	1.69	1.39
240	20 yr Post Const.	1.54	1.19	0.99

SOILS REACH 3 - MUDLINE EL. +1.0'

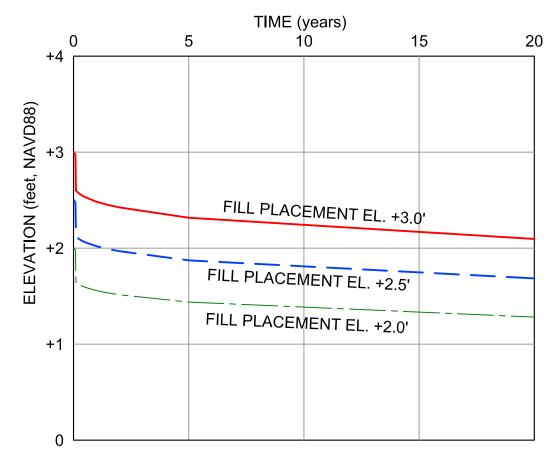
Time (months)	Description of Activity	Top of Fill Elevation (feet) EL. +3.0' EL. +2.5 EL. +2.0		
0.25	End of Fill Placement	3.00	2.50	2.00
1.25	Process Survey	2.89	2.41	1.93
60	5 yr Post Const.	2.36	1.96	1.58
240	20 yr Post Const.	1.86	1.56	1.28



MS RIVER LONG DISTANCE SEDIMENT PIPELINE JEFFERSON PARISH, LOUISIANA

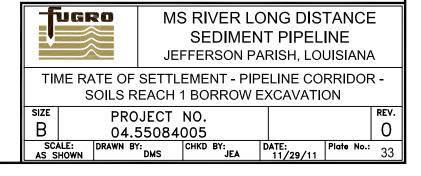
TIME RATE OF SETTLEMENT - PIPELINE CORRIDOR - UPPER BOUND INTERFACE





SOILS REACH 1- MUDLINE EL. -9.0'

Time (months)	Description of Activity	Top of Fill Elevation (feet) EL. +3.0 EL. +2.5 EL. +2.0		
0.25	End of Fill Placement	3.00	2.50	2.00
1.25	Process Survey	2.60	2.12	1.64
60	5 yr Post Const.	2.32	1.87	1.44
240	20 yr Post Const.	2.10	1.69	1.28



SOILS REACH 1- MUDLINE EL. -1.0'

Time (months)	Description of Activity	Top of Fill Elevation (fee		on (feet)
		EL. +4.5 EL. +4.0 EL. +3.5		
0.25	End of Fill Placement	4.50	4.00	3.50
1.25	Process Survey	3.61	3.17	2.71
60	5 yr Post Const.	2.32	2.01	1.60
240	20 yr Post Const.	2.03	1.77	1.39

SOILS REACH 2- MUDLINE EL. -2.0'

Time (months)	Description of Activity	Top of Fill Elevation (feet)		
		EL. +5.0 EL. +4.5 EL. +4.		EL. +4.0
0.25	End of Fill Placement	5.00	4.50	4.00
1.25	Process Survey	3.99	3.53	3.09
60	5 yr Post Const.	2.50	2.05	1.68
240	20 yr Post Const.	1.94	1.50	1.16

SOILS REACH 3- MUDLINE EL. -2.5'

Time (months)	Description of Activity	Top of Fill Elevation (feet) EL. +4.5 EL. +4.0 EL. +3.5		
0.25	End of Fill Placement	4.50	4.00	3.50
1.25	Process Survey	2.61	3.15	2.71
60	5 yr Post Const.	2.62	2.18	1.77
240	20 yr Post Const.	2.04	1.59	1.23



MS RIVER LONG DISTANCE SEDIMENT PIPELINE JEFFERSON PARISH, LOUISIANA

TIME RATE OF SETTLEMENT - CONTAINMENT DIKE - LOWER BOUND INTERFACE

SOILS REACH 1 - MUDLINE AT EL. +1.0'

Time (months)	Description of Activity	Top of Fill Elevation (feet) EL. +4.0 EL. +3.5 EL. +3.0		
0.25	End of Fill Placement	4.00	3.50	3.00
1.25	Process Survey	3.54	3.11	2.68
60	5 yr Post Const.	2.60	2.27	1.95
240	20 yr Post Const.	2.14	1.86	1.60

SOILS REACH 2 - MUDLINE AT EL. +1.0'

Time (months)	Description of Activity	Top of Fill Elevation (feet)		
(monuto)		EL. +4.0 EL. +3.5 EL. +3	EL. +3.0	
0.25	End of Fill Placement	4.00	3.50	3.00
1.25	Process Survey	3.56	3.13	2.69
60	5 yr Post Const.	2.68	2.32	2.03
240	20 yr Post Const.	2.12	1.85	1.60

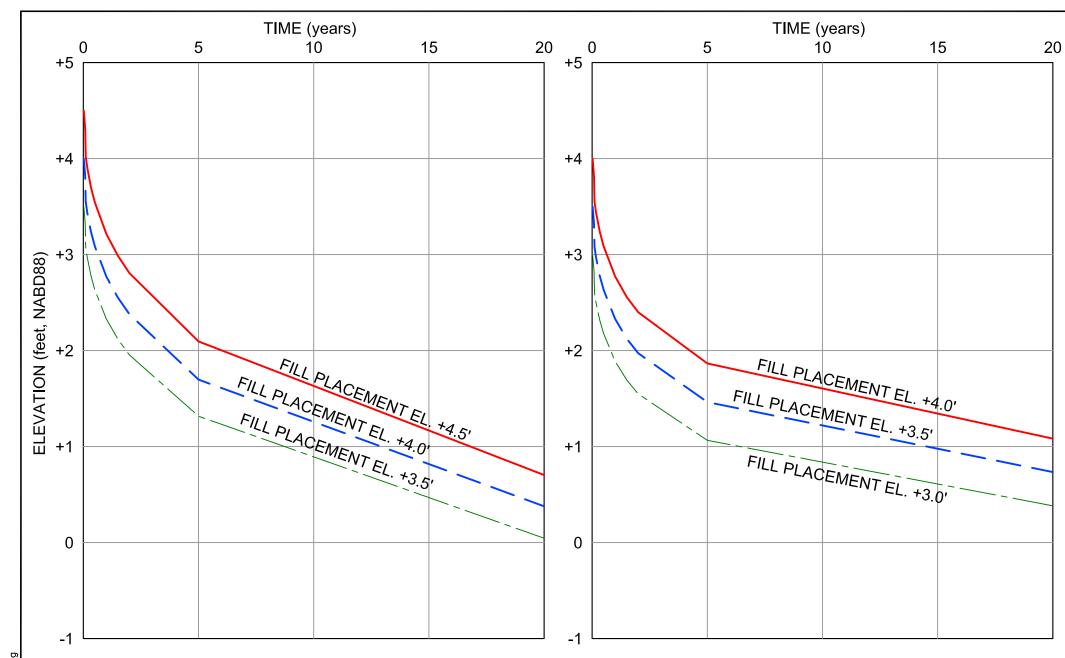
SOILS REACH 3 - MUDLINE AT EL. +1.0'

Time (months)	Description of Activity	Top of F	Fill Elevation	on (feet)
(1110111110)		EL. +4.0	EL. +3.5	EL. +3.0
0.25	End of Fill Placement	4.00	3.50	3.00
1.25	Process Survey	3.61	3.17	2.73
60	5 yr Post Const.	3.08	2.70	2.33
240	20 yr Post Const.	2.65	2.13	2.00

TUGRO

MS RIVER LONG DISTANCE SEDIMENT PIPELINE JEFFERSON PARISH, LOUISIANA

TIME RATE OF SETTLEMENT - CONTAINMENT DIKE - UPPER BOUND INTERFACE

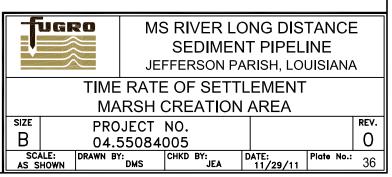


B-42 AND B-43 PROFILE

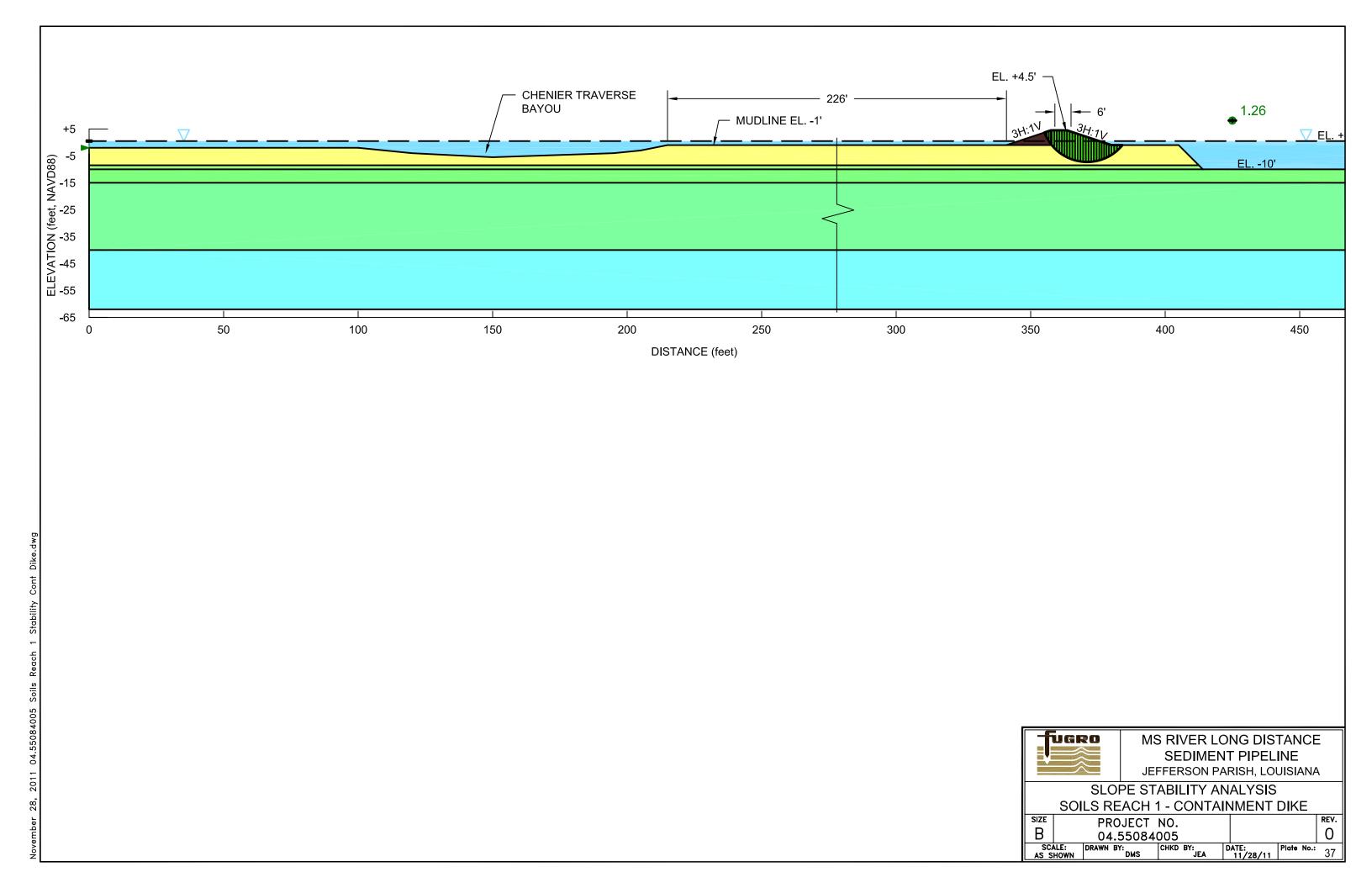
Time (months)	Description of Activity	Top of F	Fill Elevation	on (feet)
(5.1416)		EL. +4.5'	EL. +4.0'	EL. +3.5'
0.25	End of Fill Placement	4.50	4.00	3.50
1.25	Process Survey	4.02	3.55	3.08
60	5 yr Post Const.	2.09	1.70	1.32
240	20 yr Post Const.	0.70	0.38	0.04

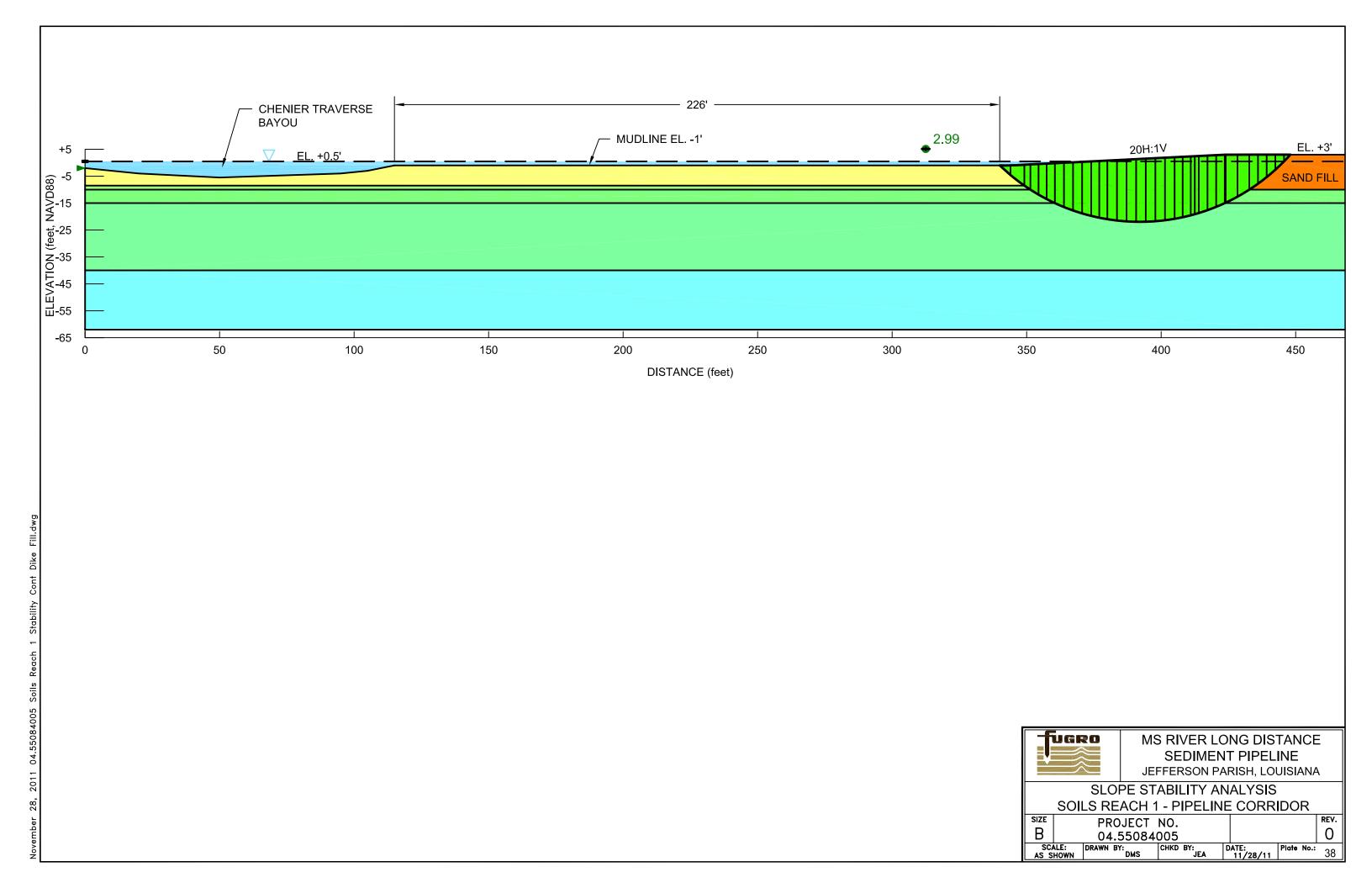
SOILS REACH 2 PROFILE

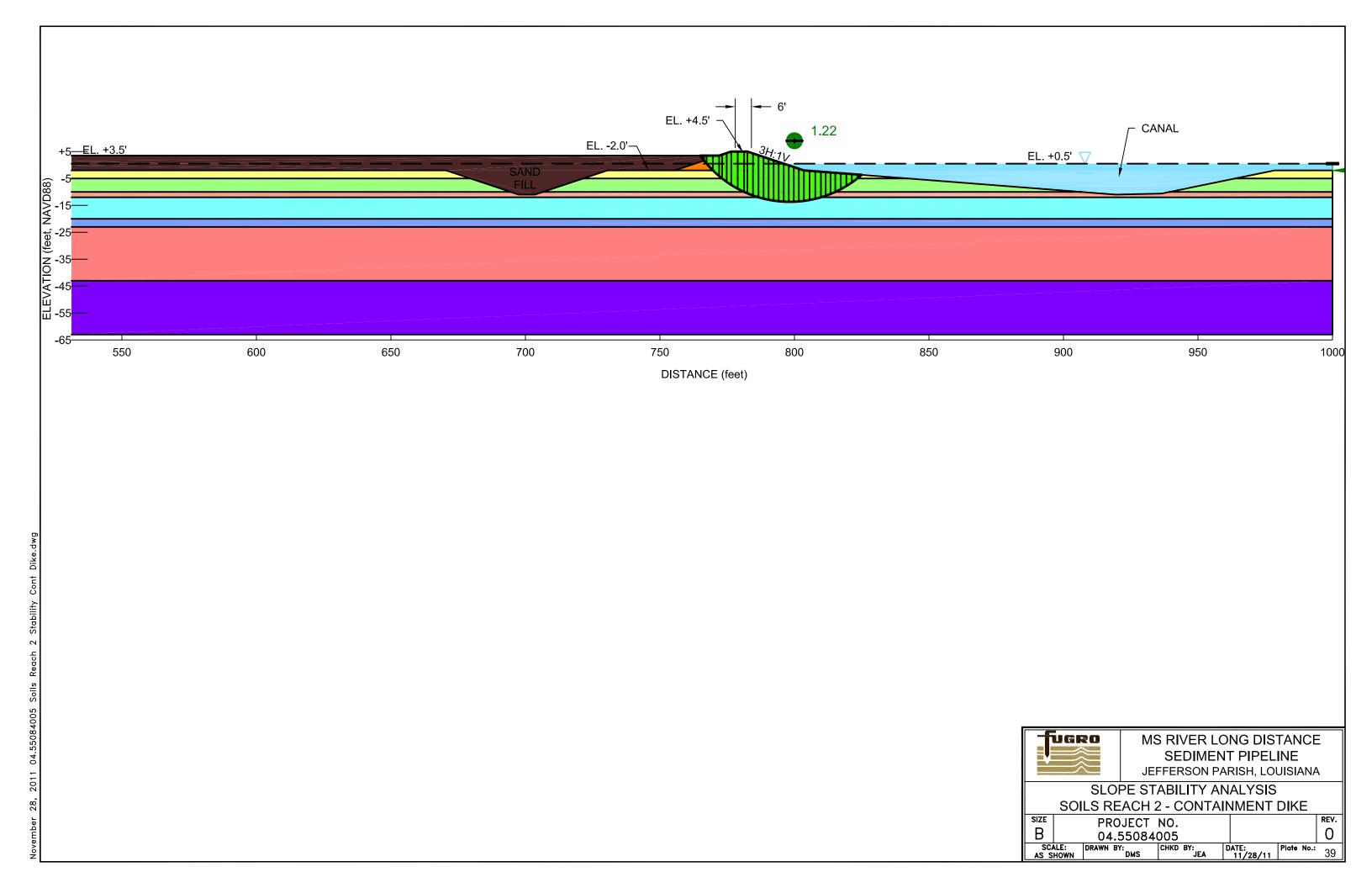
Time (months)	Description of Activity	Top of F	Fill Elevation	on (feet)
(monalo)		EL. +4.0'	EL. +3.5'	EL. +3.0'
0.25	End of Fill Placement	4.00	3.50	3.00
1.25	Process Survey	3.55	3.08	2.60
60	5 yr Post Const.	1.87	1.46	1.06
240	20 yr Post Const.	1.08	0.73	0.38

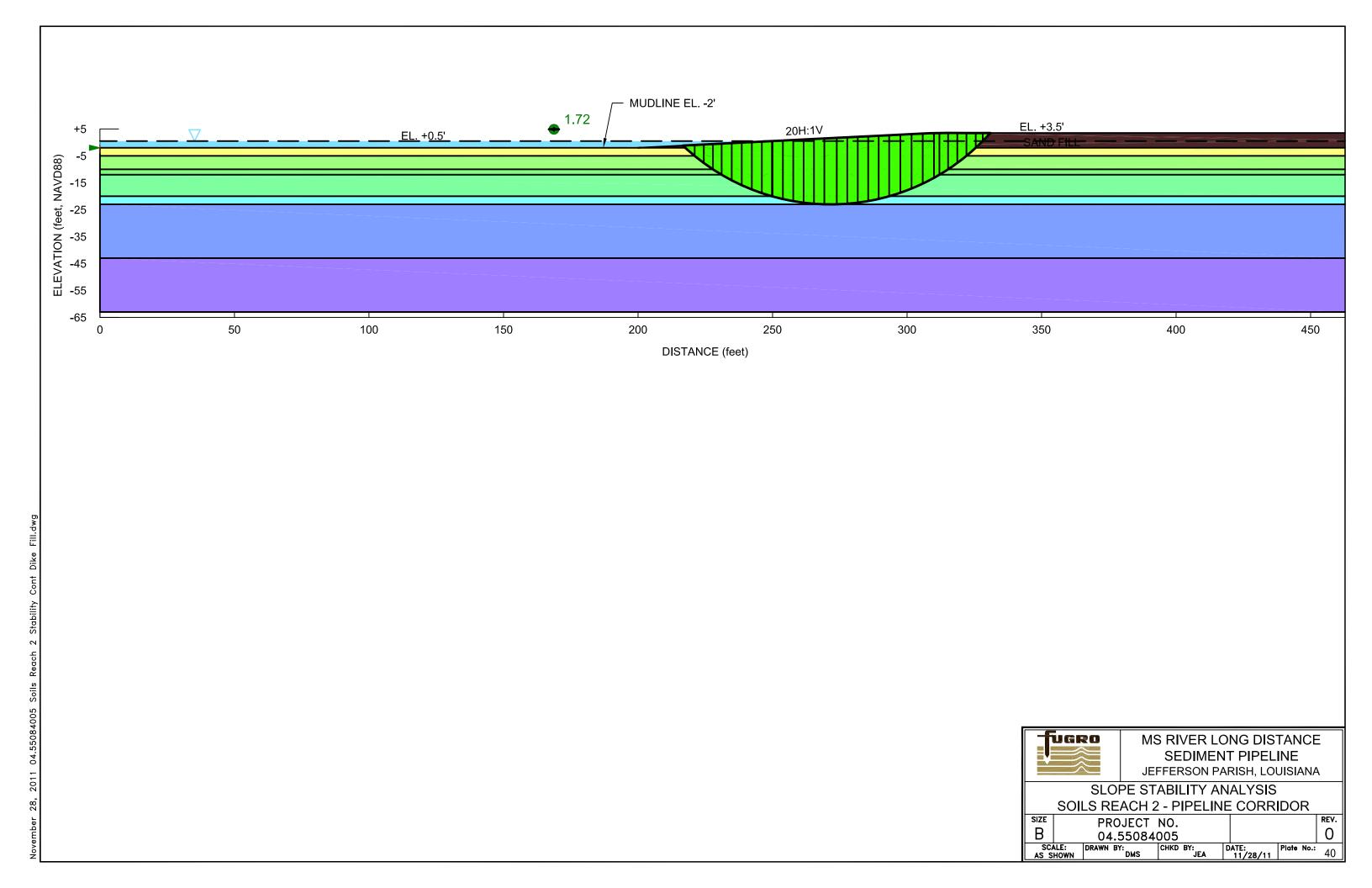


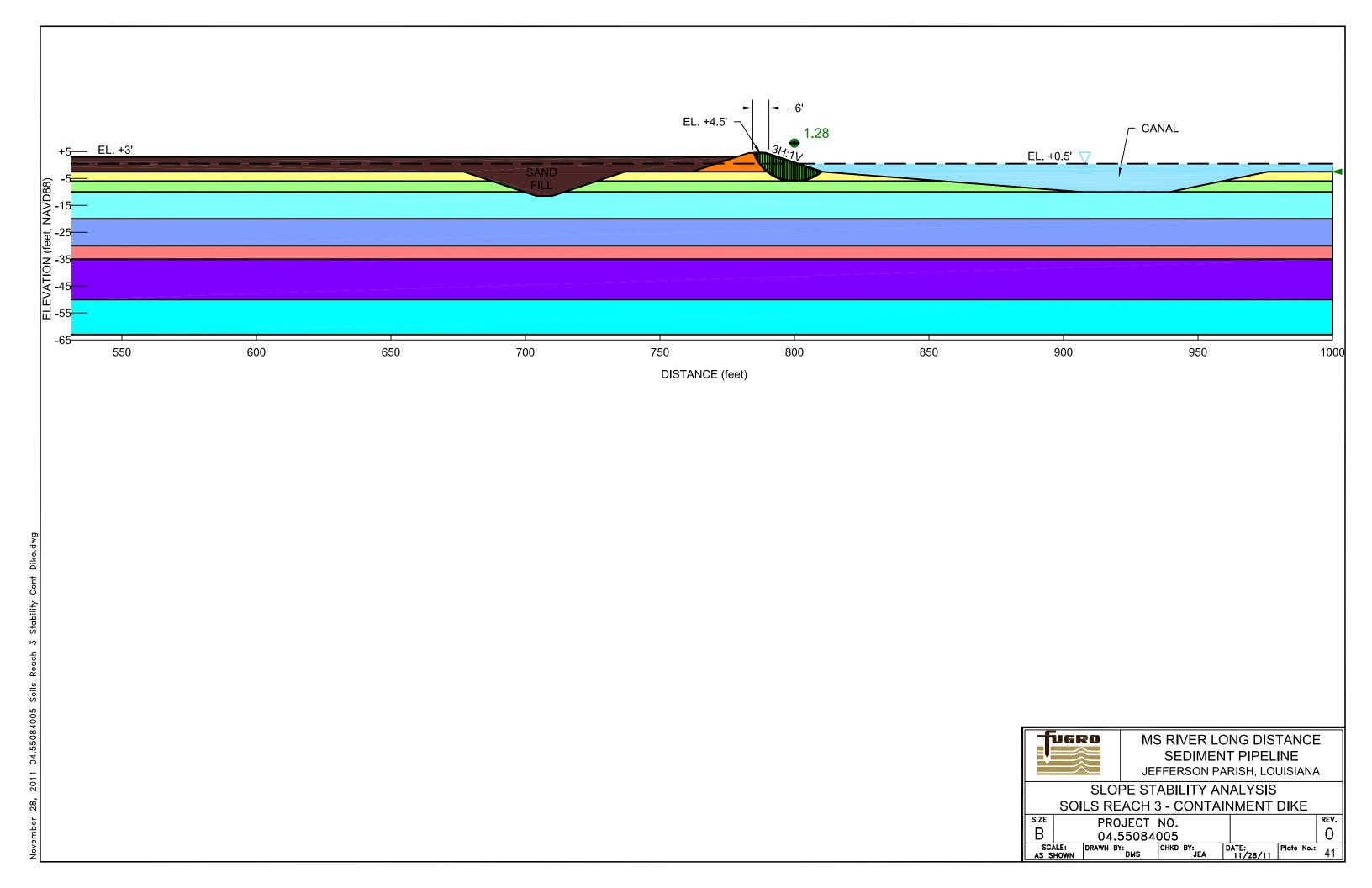
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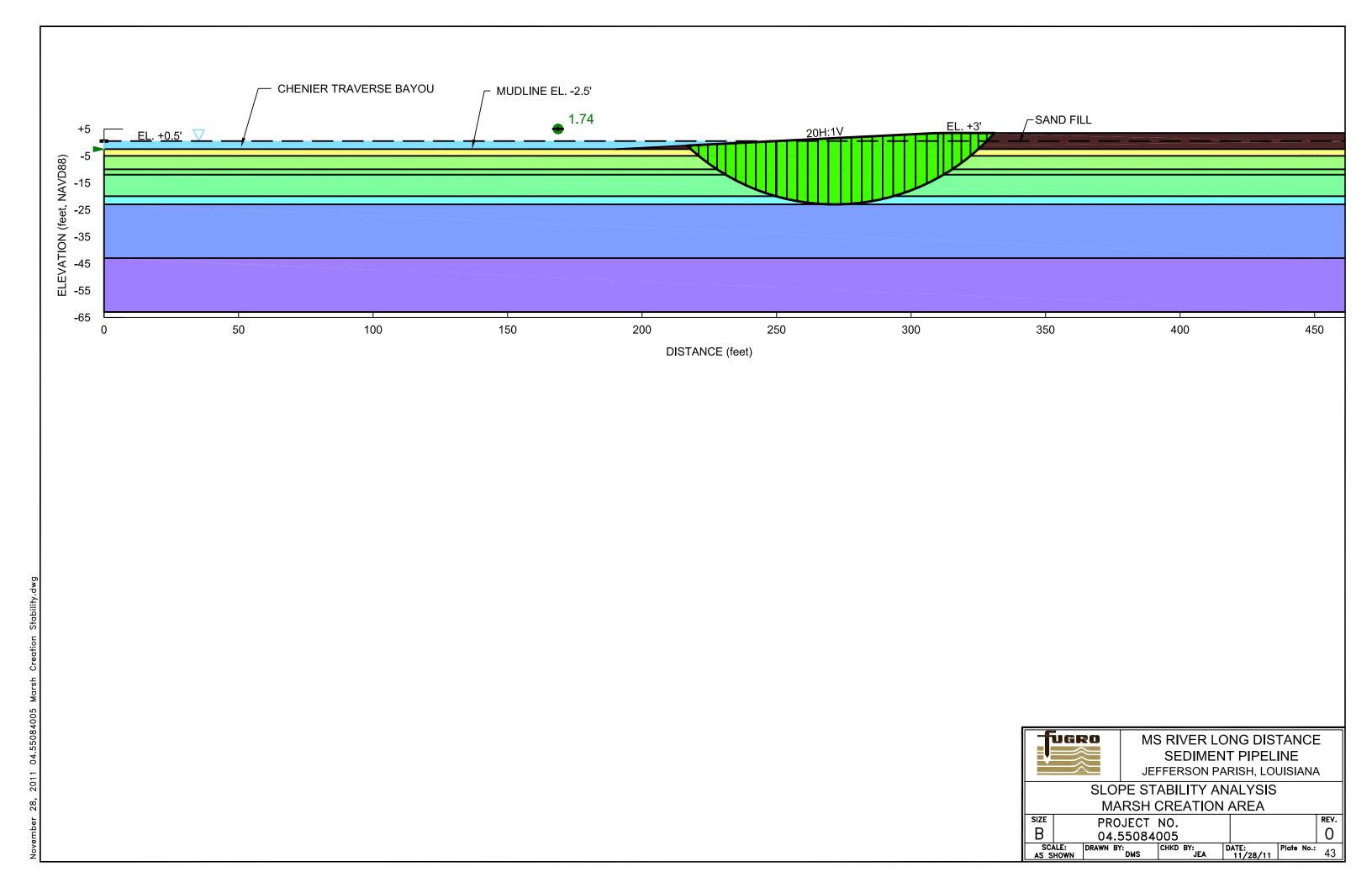


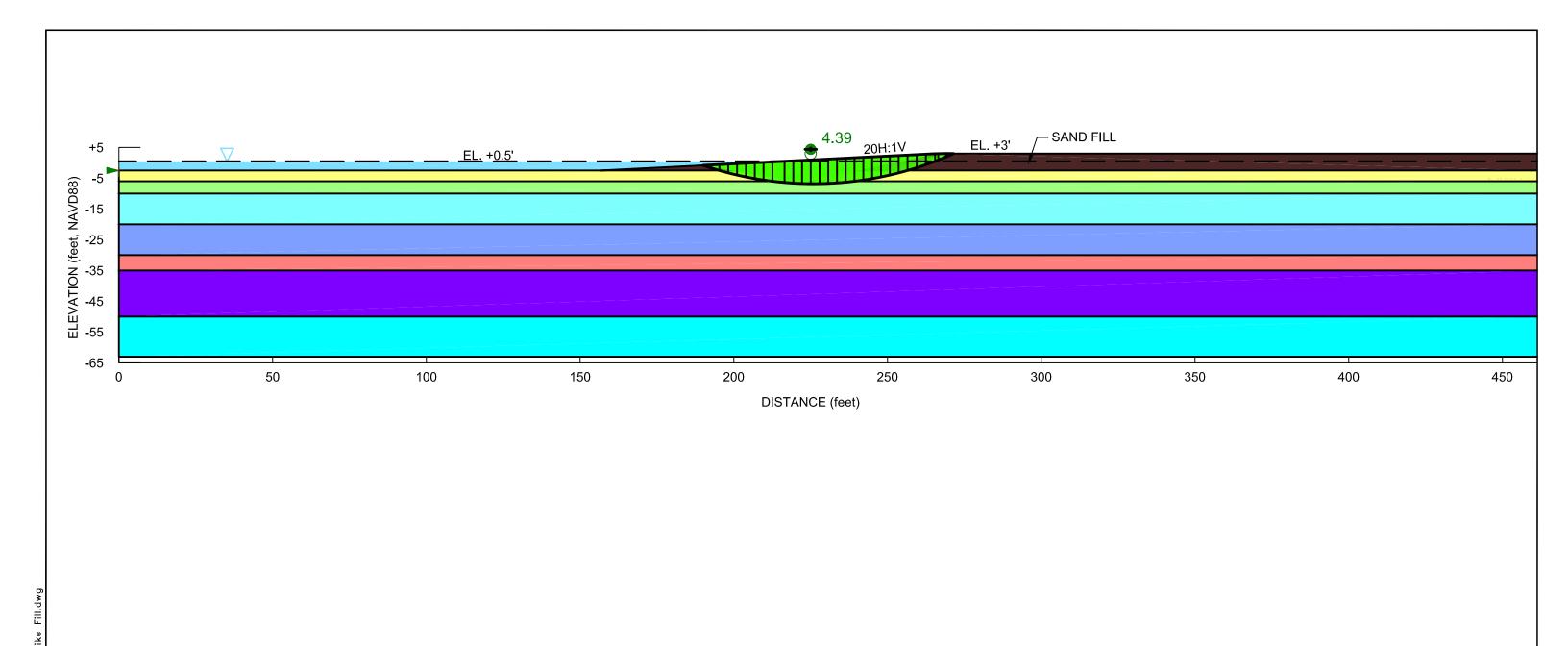








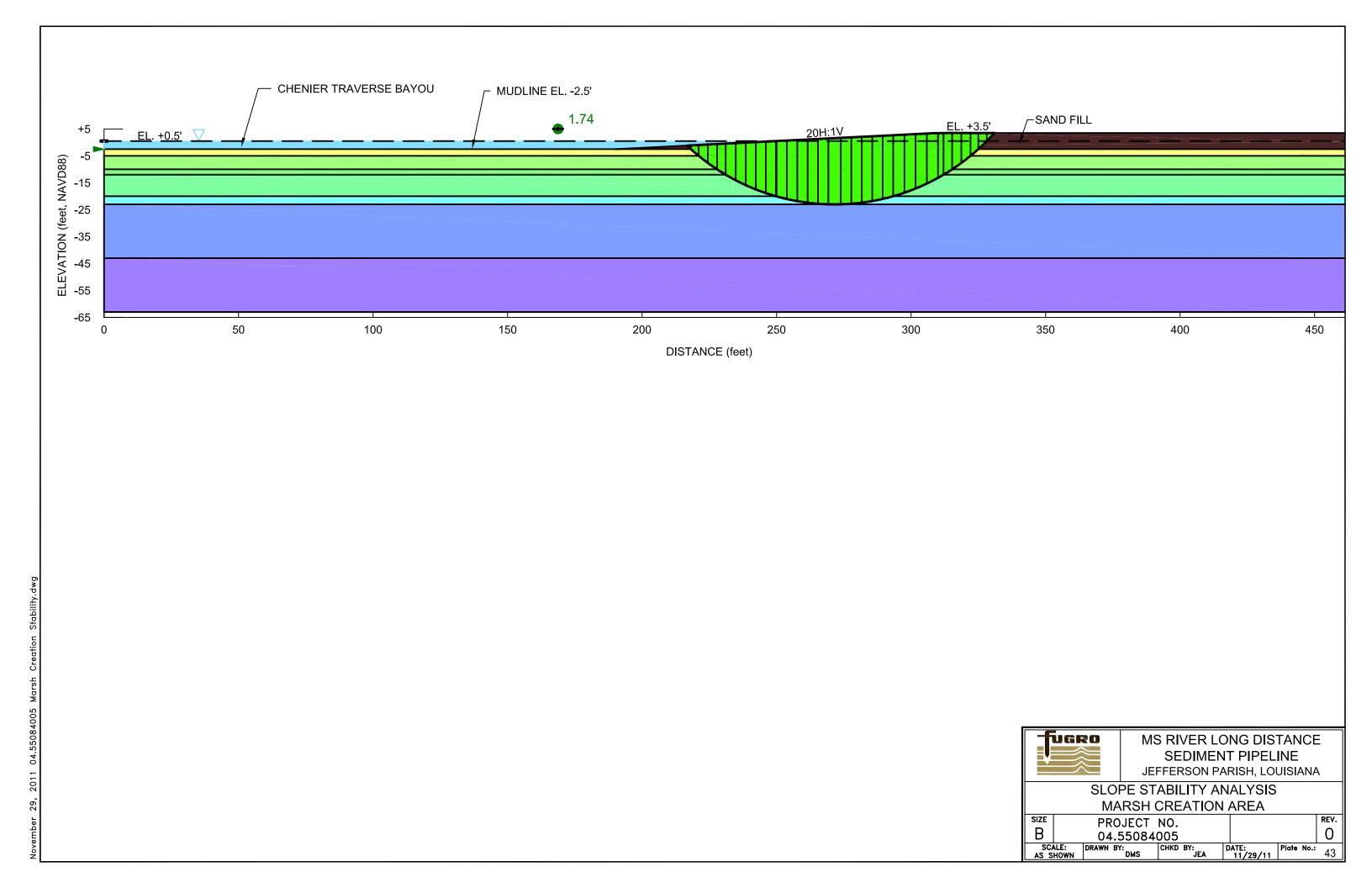






MS RIVER LONG DISTANCE SEDIMENT PIPELINE JEFFERSON PARISH, LOUISIANA

SLOPE STABILITY ANALYSIS SOILS REACH 3 - PIPELINE CORRIDOR





APPENDIX A SUMMARY OF TEST RESULTS



			lde	entifica	tion Tes	sts		Field She Strength Est	ar imate	Miniatu Te	re Vane sts			(Compres	sion Tests	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing		Torvane (ksf)		Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	1-2				14		4													
2	2-4				21															
3	4.5-6				18		5													
4A	6-7	0.59	73	25	53															
4B	7-8				52					0.39										
5A	8-9				53															
5B	9-10				65					0.29	0.36									
6A	10-11																			
6B	11-12	0.51	54	19	37		55			0.21										
7A	12-14				20		3													
7B	13-14				22					0.12										
8B	15-16	0.69	43	23	37	78	88			0.23										
9B	17-18				68					0.23										
10A	18-19							0.50												
10B	19-20				38					0.13										
11A	23-24				83															
11B	24-25				78	55				0.26		UU	78	17	0.31		0.8	55	6.9	Α
12A	28-29																			
12B	29-30	0.92	72	24	68	59	100			0.32										
13A	33-34																			
13B	34-35				80					0.30										
14B	39-40				69	59				0.47		UU	69	22	0.61		0.8	59	2.7	В
15B	44-45				61					0.32										
16A	48-49																			

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-3

LELAP Lab ID #10001

Jefferson Parish, Louisiana



			ld	entifica	tion Tes	sts		Field She Strength Est	ear imate	Miniatu Te	re Vane sts			(Compres	sion Tests	3			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)		Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
16B	49-50				58					0.33										
17B	54-55				56	69				0.38		UU	56	38	0.57		0.8	69	4.7	В
18A	58-59																			
18B	59-60				60					0.30										

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture



SUMMARY OF TEST RESULTS - BORING B-3

LELAP Lab ID #10001

Jefferson Parish, Louisiana



					tion Tes			Field She Strength Est	ar imate	Miniatu Te	re Vane sts			(Compres	sion Tests	3			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)	Torvane (ksf)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				21		4													
2	2.5-4				19		5													
4B	7-8	0.78	81	24	68	59	97			0.42										
5	8-9																			
5B	9-10				54					0.48	0.24									
6B	11-12				15					0.29										
7B	13-14	0.15	66	22	29					0.23										
8B	15-16				39					0.24										
9B	17-18				37					0.35	0.24									
10B	19-20	1.69	32	25	37	84	97			0.11										
11B	24-25				77	55				0.37		UU	77	17	0.29		0.9	55	8.4	Α
12	28-30	0.70	46	22	39															
12	29-30																			
13	33.5-35				31		84													
14B	39-40				71	59				0.35		UU	71	27	0.47		0.7	59	4.0	В

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-5

LELAP Lab ID #10001

Jefferson Parish, Louisiana



					tion Tes			Field She Strength Est	ear imate	Miniatu Te	re Vane sts			(Compres	sion Tests	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)	Torvane (ksf)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0.5-2				135															
2A	2-3				184															
2B	3-4	0.92	133	35	125	39	89			0.02										
3A	4-5																			
3B	5-6				33			0.50		0.08										
4A	6-7				42															
4B	7-8				35					0.08	0.10									
5A	8-9																			
5B	9-10				37															
6A	10-11	1.28	38	22	42															
6B	11-12				70					0.07										
7B	13-14				73															
8A	14-15																			
8B	15-16				155					0.15										
9A	16-17	0.91	99	32	93															
9B	17-18				53					0.21										
10A	18-19																			
10B	19-20				36					0.21										
11B	24-25				62	64				0.16		UU	62	17	0.24		1.8	64	11.9	Α
12B	29-30	0.81	85	27	74	54	100			0.34										
13B	34-35				75	57				0.34		UU	75	24	0.51		0.9	57	4.3	В
14A	38-39																			
14B	39-40				68					0.30										
15A	43-44																			

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-7

LELAP Lab ID #10001

Fugro Consultants, Inc

Jefferson Parish, Louisiana

			lde	entifica	tion Tes	sts		Field She Strength Est	ear imate	Miniatu Te	re Vane sts			(Compres	sion Tests	3			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)			Remolded	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
15B	44-45				69			0.50		0.37									_	
16B	49-50				54	69				0.38		UU	54	34	0.65		0.6	69	1.9	В
17A	53-54																			
17B	54-55				49			0.50		0.36										
18B	59-60				61	63				0.34		UU	61	41	0.59		0.6	63	5.1	В
																				

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture



SUMMARY OF TEST RESULTS - BORING B-7

LELAP Lab ID #10001

Fugro Consultants, Inc

UGRO

Jefferson Parish, Louisiana

					tion Tes			Field She Strength Est	ear imate	Miniatu Te	re Vane sts				Compres	sion Tests	3			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)	Torvane (ksf)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				214															
2A	2-3				395															
2B	3-4	1.54	191	54	264	22	47			0.07										
3B	5-6				53					0.12	0.12									
4B	7-8				86					0.16										
5B	9-10				49					0.14										
6B	11-12				40					0.13										
7A	12-13	1.42	55	24	68															
7B	13-14				44					0.09										
8B	15-16				77					0.19										
9B	17-18				54					0.16										
10B	19-20				35					0.09										
11A	23-24	7.10	25	24	30															
11B	24-25				47	74				0.30		UU	47	18	0.21		2.5	74	13.9	Α
12A	30-31.5				28		44													
14	38.5-40				35		44													

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-9

LELAP Lab ID #10001

Jefferson Parish, Louisiana



			lde	entifica	tion Tes	sts		Field She Strength Est	ar imate	Miniatu Te	re Vane sts			(Compres	sion Tests	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				852															
2a	2-3																			
2B	3-4	2.24	548	254	913					0.05										
3	4-6				447															
4b	7-8				266					0.05										
5a	8-9																			
5b	9-10	1.95	312	152	465	13	80			0.20										
6b	11-12				275					0.09										
7b	13-14				320					0.04										
8b	15-16				128					0.08										
9b	16-17	1.06	125	35	130															
9b	17-18				83					0.17										
10b	19-20				36					0.09	0.15									
11b	24-25				68	58						UU	68	18	0.11		1.0	58	14.6	Α
12a	28-29				80															
12b	29-30				58					0.15										
13b	34-35				49	70				0.18		UU	49	26	0.24		1.2	70	9.3	А
14a	38-39				78															
14b	39-40				73					0.19										

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-11

LELAP Lab ID #10001

Jefferson Parish, Louisiana



			lde	entifica	tion Tes	sts		Field She Strength Est	ar imate	Miniatu Te	re Vane sts			(Compres	sion Tests	3			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-2				533															
2	2-3	1.03	175	35	179															
2B	3-4				221					0.06										
3	4-6																			
4A	6-7				230															
4B	7-8	0.98	287	57	283	18	28			0.08										
5A	8-9																			
5B	9-10				183					0.13										
6B	11-12				243					0.24	0.20									
7A	12-13																			
7B	13-14				271					0.11										
8A	14-15																			
8B	15-16				77					0.18										
9A	16-17	1.28	77	23	92															
9B	17-18				52					0.15										
10A	18-19																			
10B	19-20				33					0.13										
11	23-25																			
12B	29-30				53	69				0.27		UU	53	20	0.22		1.1	69	10.4	Α
13A	33-34																			
13B	34-35				57					0.23										
14B	39-40				55	68				0.30		UU	55	27	0.42		0.8	68	4.3	A,B

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-12

LELAP Lab ID #10001

Jefferson Parish, Louisiana



					tion Tes			Field She Strength Est	ear imate	Miniatu Te	re Vane sts				Compres	sion Tests	3			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)	Torvane (ksf)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				412															
3A	4-5	1.13	187	47	205															
3B	5-6				92					0.18										
4B	7-8				101															
5B	9-10				157						0.24									
6B	11-12				151															
7A	12-13	1.49	125	38	168															
7B	13-14				176					0.16										
8B	15-16				138					0.14										
9B	17-18	1.30	76	26	91	45	87			0.06										
10B	19-20				82					0.05										
11	23-25	0.79	58	22	51															
12B	29-30				77	56				0.18		UU	77	20	0.26		0.8	56	11.1	Α
13A	33-34				79															
13B	34-35				77					0.22										
14B	39-40				67	60				0.25		UU	67	27	0.34		0.7	60	6.6	Α

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-13

LELAP Lab ID #10001

Jefferson Parish, Louisiana



					tion Tes			Field She Strength Est	ar imate	Miniatu Te	re Vane sts			(Compres	sion Tests	3			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)	Torvane (ksf)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				61															
2B	3-4				36					0.32	0.25									
3B	5-6	0.60	45	18	34	86	94			0.27										
4B	7-8				39					0.64										
5B	9-10				42					0.37										
6B	11-12				36					0.51										
7B	13-14				35					0.38										
8B	15-16				29					0.07										
9A	16-17	1.10	34	24	34		92													
9B	17-18				31					0.24										
10B	19-20				65					0.34										
11B	24-25	0.53	142	37	93		96			0.25										
12B	29-30				60	64				0.18		UU	60	20	0.46		0.8	64	3.8	С
13A	33-34	0.99	52	20	52															
13B	34-35				26					0.27										
14B	39-40				64	62				0.34		UU	64	27	0.53		0.8	62	5.6	В
																		L		

UGRO

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-15

LELAP Lab ID #10001

Fugro Consultants, Inc

Jefferson Parish, Louisiana

					tion Tes			Field She Strength Est	ear imate	Miniatu Te	re Vane sts			(Compres	sion Test	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)		Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1				63															
2A	2-3	0.58	66	21	47															
2B	3-4				36					0.51										
3A	4-5																			
3B	5-6				40					0.46										
4A	6-7				41															
4B	7-8				33					0.25	0.53									
5B	9-10				32					0.10										
6A	10-11	0.63	39	21	32															
6B	11-12				35					0.62										
7A	12-13																			
7B	13-14				43					0.45										
8A	14-15				41															
8B	15-16				37					0.36										
9B	17-18	0.73	44	21	38	82	89			0.35										
10B	19-20				39					0.60										
11B	24-25				127	39				0.41		UU	127	17	0.62		0.9	39	2.7	Α
12	28.5-30																			
13A	33-34				40		98	0.50												
13B	34-35				58					0.61										
14A	38-39							0.50												
14B	39-40				58					0.42										
15A	43-44																			
15B	44-45				41															

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-17

LELAP Lab ID #10001

Jefferson Parish, Louisiana



					tion Tes			Field She Strength Est	ar imate	Miniatu Te	re Vane sts				Compres	sion Tests	3			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)	Torvane (ksf)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				653															
2A	2-3				809															
2B	3-4				180					0.08										
3	4-6				206															
4B	7-8	0.47	94	30	60	61	99			0.27										
5B	9-10				54					0.24										
6B	11-12				57					0.31										
7B	13-14				82					0.31										
8A	14-15	0.55	83	27	58															
8B	15-16				76					0.33										
9B	17-18				93					0.17	0.15									
10B	19-20				31					0.11										
11	23-25				47															
12B	29-30				73	58				0.26		UU	73	20	0.28		1.1	58	8.1	A,B
13	33-35				66															
14B	39-40				72					0.20										

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-18

LELAP Lab ID #10001

Fugro Consultants, Inc

Jefferson Parish, Louisiana

				tion Tes			Field She Strength Est	imate	Te	re Vane sts			(Compres	sion Tests	3			
Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)			Remolded	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
0-1.5				230															
2-4	1.46	189	43	256															
5-6				70					0.14										
7-8	0.56	70	23	49	73	100			0.09										
9-10				58					0.13										
11-12				56					0.06										
13-14				55					0.06	0.06									
15-16				37					0.11										
16-17	0.86	43	18	40															
17-18				78					0.10										
19-20				41					0.06										
24-25	-1230.53	NP	NP	26															
29-30				24		13													
33-35				38															
38.5-40				24		9													
	0-1.5 2-4 5-6 7-8 9-10 11-12 13-14 15-16 16-17 17-18 19-20 24-25 29-30 33-35	0-1.5 2-4 1.46 5-6 7-8 0.56 9-10 11-12 13-14 15-16 16-17 0.86 17-18 19-20 24-25 -1230.53 29-30 33-35	0-1.5 2-4 1.46 189 5-6 7-8 0.56 70 9-10 11-12 13-14 15-16 16-17 0.86 43 17-18 19-20 24-25 -1230.53 NP 29-30 33-35	0-1.5 2-4 1.46 189 43 5-6 7-8 0.56 70 23 9-10 11-12 13-14 15-16 16-17 0.86 43 18 17-18 19-20 24-25 -1230.53 NP NP 29-30 33-35	0-1.5 230 2-4 1.46 189 43 256 5-6 70 23 49 9-10 58 11-12 56 13-14 55 15-16 37 16-17 0.86 43 18 40 17-18 78 19-20 41 24-25 -1230.53 NP NP 26 29-30 24 33-35 38	0-1.5 230 2-4 1.46 189 43 256 5-6 70 23 49 73 9-10 58 11-12 56 13-14 55 15-16 37 16-17 0.86 43 18 40 17-18 78 19-20 41 24-25 -1230.53 NP NP 26 29-30 24 33-35 38	0-1.5 230 2-4 1.46 189 43 256 5-6 70 23 49 73 100 9-10 58 11-12 56 13-14 55 13-14 55 37 15-16 37 16-17 0.86 43 18 40 17-18 78 19-20 41 41 41 42-25 -1230.53 NP NP 26 24 13 33-35 38 38 38 38	(ft) (76) (DCI) (78) 0-1.5	0-1.5 230 2-4 1.46 189 43 256 5-6 70 23 49 73 100 9-10 58 100 11-12 56 13-14 55 15-16 37 15-16 16-17 0.86 43 18 40 17-18 78 19-20 41 19-20 41 13 29-30 24 13 33-35 38 13	0-1.5 230 2-4 1.46 189 43 256 5-6 70 23 49 73 100 0.09 9-10 58 0.13 11-12 56 0.06 13-14 55 0.06 15-16 37 0.11 16-17 0.86 43 18 40 17-18 78 0.10 19-20 41 0.06 24-25 -1230.53 NP NP 26 29-30 24 13 33-35 38 8	0-1.5 230 0.14 0.14 0.14 0.14 0.14 0.14 0.09 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.01 0.01 0.01 0.01 0.06	0-1.5 230 230 0.14 0.14 0.14 0.14 0.14 0.09 0.00	0-1.5 230 0.16 0.16 0.14 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.06	0-1.5 230 </td <td>0-1.5 S 230 S<!--</td--><td>0-1.5 230 <!--</td--><td>0-1.5 Image: color of the colo</td><td>0-1.5 Image: color of the colo</td><td>0-1.5 Image: contract of the contract</td></td></td>	0-1.5 S 230 S </td <td>0-1.5 230 <!--</td--><td>0-1.5 Image: color of the colo</td><td>0-1.5 Image: color of the colo</td><td>0-1.5 Image: contract of the contract</td></td>	0-1.5 230 </td <td>0-1.5 Image: color of the colo</td> <td>0-1.5 Image: color of the colo</td> <td>0-1.5 Image: contract of the contract</td>	0-1.5 Image: color of the colo	0-1.5 Image: color of the colo	0-1.5 Image: contract of the contract

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-19

LELAP Lab ID #10001

Jefferson Parish, Louisiana



			lde	entifica	tion Tes	sts		Field She Strength Est	ar imate	Miniatu Te	re Vane sts			(Compres	sion Tests	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing		Torvane (ksf)		Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				264															
2A	2-3	0.81	185	39	158															
2B	3-4				145					0.08										
3	4-5				198															
3B	5-6				357					0.25	0.11									
4B	7-8	0.94	115	34	110	42	99			0.10										
5B	9-10				29															
6B	11-12				49					0.13										
7A	12-13	1.01	54	20	54		72													
7B	13-14				73					0.11										
8B	15-16				42					0.20										
9B	17-18				77															
10A	18-19	0.94	82	25	78															
10B	19-20				70					0.10										
11B	24-25				26	97						UU	26	17	1.82		6.5	97	15.0	Α
12	28.5-30				58															
13	33-35				46															
14	38.5-40				38		96													
15	43.5-45				32		72													
16A	48-49							0.50												
16B	49-50				49	73				0.51		UU	49	34	0.61		0.6	73	7.1	В
17A	53-54				41			0.50												
17B	54-55				58					0.51										
	54.1-				52															

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-26

LELAP Lab ID #10001

Jefferson Parish, Louisiana



		lde	entificat	tion Tes	sts		Field She Strength Est	ar imate	Miniatu Te	re Vane sts			(Compres	sion Tests	8			
Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)			Remolded	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
59-60				56	66				0.51		UU	56	41	0.68		0.7	66	3.8	С
			Depth (ft) Liquidity Index Limit (%)	Depth (ft) Liquid Liquid Limit (%)	Depth (ft) Liquid Liquid Limit (%) Plastic Limit (%) Content (%)		Depth (ft) Liquidity Index Liquid Limit (%) Plastic Limit (%) Plastic Content (%) Plastic Content (%) Weight (pcf) No. 200 Sieve (%)	Depth (ft) Liquidity Index Liquid (%) Liquid (%) Plastic Limit (%) Plastic Content (%) Moisture Content (%) Moisture Content (%) Penetrometer* (ksf)	Depth (ft) Depth (ft) Dept	Depth (ft) Content (%) Co	Depth (ft) Liquidity Index (limit (%) Plastic (%) Pla	Depth (ft) Depth (ft) Dept	Depth (ft) Depth (ft) Dept	Depth (ft) Depth (ft) Dept	Depth (ft) Depth (ft) Dept	Depth (ft) Depth	Depth (ft) Content (%) Co	Depth (ft) Content (%) Co	Depth (ft) Depth (ft) (ft) Depth (ft) (ft) Depth (ft) (ft) Depth (ft) (ft) (ft) Depth (ft) (ft) (ft) (ft) Depth (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft)

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-26

LELAP Lab ID #10001

Jefferson Parish, Louisiana



			lde	entifica	tion Tes	sts		Field She Strength Est	ar imate	Miniatu Te	re Vane sts			(Compres	sion Tests	6			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing		Torvane (ksf)		Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0.5-2				182															
2	2-3	1.22	158	36	185															
2B	3-4				208					0.12										
4A	6-7																			
4B	7-8	2.16	44	20	72	60	96			0.11										
5A	8-9	1.05	78	24	81															
5B	9-10				169					0.26										
6A	10-11																			
6B	11-12				83					0.19										
7A	12-13				119		27													
7B	13-14	0.89	86	28	80	53	98			0.09										
8B	15-16				35						0.20									
10	18.5-20				31		87													
11	23.5-25				41															
12	28-30				27		27													
13	33.5-35				22		12													
14	38.5-40																			
15A	43-44	0.63	37	19	31															
15B	44-45				26															
16A	48-49							0.75												
16B	49-50				62	64				0.58		UU	62	34	0.64		0.6	64	3.3	A,C
17A	53-54							0.50												
17B	54-55	0.58	69	23	50	70	100			0.60										
18B	59-60				49	71				0.63		UU	49	41	0.81		0.8	71	4.2	В

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture



MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-28

LELAP Lab ID #10001

Fugro Consultants, Inc

Jefferson Parish, Louisiana

			lde	entifica	tion Tes	sts		Field She Strength Est	Miniatu Te	re Vane sts			(Compres	sion Tests	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing			Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				170														
2A	2-3				322														
2B	3-4	0.80	152	41	130	39	98		0.08										
3	4-5				62														
4B	7-8				69				0.12										
5B	9-10				68				0.13										
6A	10-11	1.15	89	30	97														
6B	11-12				103				0.31										
7B	13-14				77				0.12	0.20									
8B	15-16				105				0.23										
9B	17-18				49				0.15										
10B	19-20	0.98	54	21	53	68	100		0.09										
11	23-25	0.95	52	21	50														
12B	29-30				21		16												
14A	38-39				73	59			0.20		UU	73	27	0.38		1.3	59	11.8	Α
14B	39-40				32				0.09										
15A	43-44				44														
15B	44-45				64				0.41										
16B	49-50				59	65			0.41		UU	59	34	0.61		0.8	65	6.8	В
17A	53-54				52														
17B	54-55				58				0.44										
18B	59-60				64	63			0.48		UU	64	41	0.57		1.2	63	7.0	С

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-38

LELAP Lab ID #10001

Fugro Consultants, Inc

UGRO

Jefferson Parish, Louisiana

			lde	entifica	tion Tes	sts		Field She Strength Est	ar imate	Miniatu Te	re Vane sts			(Compres	sion Tests	3			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)		Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				191															
2	2-4	1.63	232	64	338															
2B	3-4				249															
3B	5-6				55					0.07										
4B	7-8				50					0.14	0.09									
5B	9-10				77					0.13										
6B	11-12				80					0.16										
7B	13-14	1.11	82	26	88	48	99			0.16										
8B	15-16				96					0.11										
9B	17-18				102					0.18										
10A	18-19	0.86	105	28	94															
10B	19-20				67					0.12										
11	23-25				53															
12B	29-30				82	53				0.25		UU	82	20	0.29		1.0	53	9.1	Α
13A	33-34				78															
13B	34-35				61					0.23										
14B	39-40				67	60				0.25		UU	67	27	0.35		0.7	60	7.6	Α

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-40

04.55084005

Project No.

LELAP Lab ID #10001

Jefferson Parish, Louisiana



			lde	entifica	tion Tes	sts		Field She Strength Est	ar imate	Miniatu Te	re Vane sts			(Compres	sion Tests	S			
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing		Torvane (ksf)		Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				378															
2	2-4				221															
3	4-6	1.99	68	20	115															
4B	7-8				277					0.15										
5B	9-10				240					0.12	0.31									
6B	11-12				175					0.13										
7A	12-13	0.79	295	77	250															
7B	13-14				65					0.18										
8B	15-16				97					0.18										
9B	17-18				89					0.13										
10B	19-20				82					0.14										
11B	24-25	2.18	37	17	62	62	99			0.41										
12	28.5-30				65															
13B	34-35				75	56				0.31		UU	75	24	0.36		0.7	56	3.0	Α
14A	38-39				36															
14B	39-40				32					0.29										
15B	44-45				34	85				0.31		UU	34	31	0.47		1.1	85	8.1	Α
16A	48-49				60															
16B	49-50				51					0.47										
17B	54-55				49	73				0.52		UU	49	38	0.51		0.8	73	4.7	В
18A	58-59				55															
18B	59-60				67					0.63										

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-41

LELAP Lab ID #10001

Jefferson Parish, Louisiana



			lde	entifica	tion Tes	sts		Field She Strength Est	Miniature Vane Tests		Compression Tests									
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)		Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure
1	0-1.5				748															
2B	3-4				215					0.11										
3A	4-5	1.19	242	68	276															
3B	5-6				177					0.14										
4B	7-8				319					0.31	0.15									
5B	9-10				204					0.10										
6B	11-12	1.54	159	40	223	24	83			0.08										
7B	13-14				33					0.15										
8B	15-16				35					0.11										
9B	17-18				98					0.09										
10A	18-19	1.25	66	23	77															
10B	19-20				72					0.04										
11	23-25				84															
12B	29-30				80	54				0.21		UU	80	20	0.25		0.8	54	4.3	В
13A	33-34				73															
13B	34-35				91					0.21										
14B	39-40				75	57				0.23		UU	75	27	0.28		0.9	57	10.3	Α

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-42

LELAP Lab ID #10001

Jefferson Parish, Louisiana



			ld	entifica	tion Tes	sts		Field Shear Strength Estimate		Miniature Vane Tests		Compression Tests									
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)	Torvane (ksf)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure	
1	0-1.5				379																
2A	2-3				518																
2B	3-4	1.23	203	55	236	25	63			0.10											
3B	5-6				61					0.19	0.30										
4B	7-8				40					0.51											
5B	9-10				106			0.75		0.64											
6A	10-11	0.54	88	36	64																
6B	11-12				78					0.25											
7B	13-14				94																
8B	15-16				153					0.39											
9B	17-18				171					0.19											
10B	19-20	0.70	200	52	156	31	73			0.11											
11	23-25	1.11	62	22	67																
12	28-30				78																
13B	34-35				77	55				0.12		UU	77	24	0.37		0.6	55	3.2	Α	
14A	38-39				76																
14B	39-40				72					0.28											
15B	44-45				74	55				0.33		UU	74	31	0.49		0.9	55	4.1	В	
16A	48-49				61																
16B	49-50				61					0.33											
17A	53-54				73	58						UU	73	38	0.56		0.7	58	2.5	В	
17B	54-55				72					0.28											
18A	58-59				63																
18B	59-60				69					0.35											

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture



SUMMARY OF TEST RESULTS - BORING B-43

LELAP Lab ID #10001

Fugro Consultants, Inc

Jefferson Parish, Louisiana

			ld	entifica	tion Tes	sts		Field She Strength Est	Miniatu Te	re Vane sts	Compression Tests										
Sample No.	Depth (ft)	Liquidity Index	Liquid Limit (%)	Plastic Limit (%)	Moisture Content (%)	Dry Unit Weight (pcf)	Passing No. 200 Sieve (%)	Penetrometer* (ksf)			Remolded	Type Test	Moisture Content (%)	Confining Pressure (psi)	Shear Strength (ksf)	Remolded Shear Strength (ksf)	E50 Strain (%)	Dry Unit Weight (pcf)	Failure Strain (%)	Type of Failure	
16A	48-49							0.50													
16B	49-50				60	64				0.50		UU	60	34	0.76		0.8	64	2.5	С	
17A	53-54							0.50													
17B	54-55	0.60	85	27	62		100			0.65											
18A	58-59							0.50													
18B	59-60				51	69				0.61		UU	51	41	0.70		1.0	69	5.3	В	
		-								1			-	-						-	

NP = Non-Plastic Material *Corrected as described on Terms and Symbols Used on Boring Logs.

TYPE OF TEST

U - Unconfined Compression

UU - Unconsolidated - Undrained Triaxial

CU - Consolidated - Undrained Triaxial

TYPE OF FAILURE

A - Bulge

B - Single Shear Plane C - Multiple Shear Plane

D - Vertical Fracture

MS River Long Distance Sediment Pipeline

SUMMARY OF TEST RESULTS - BORING B-17

LELAP Lab ID #10001

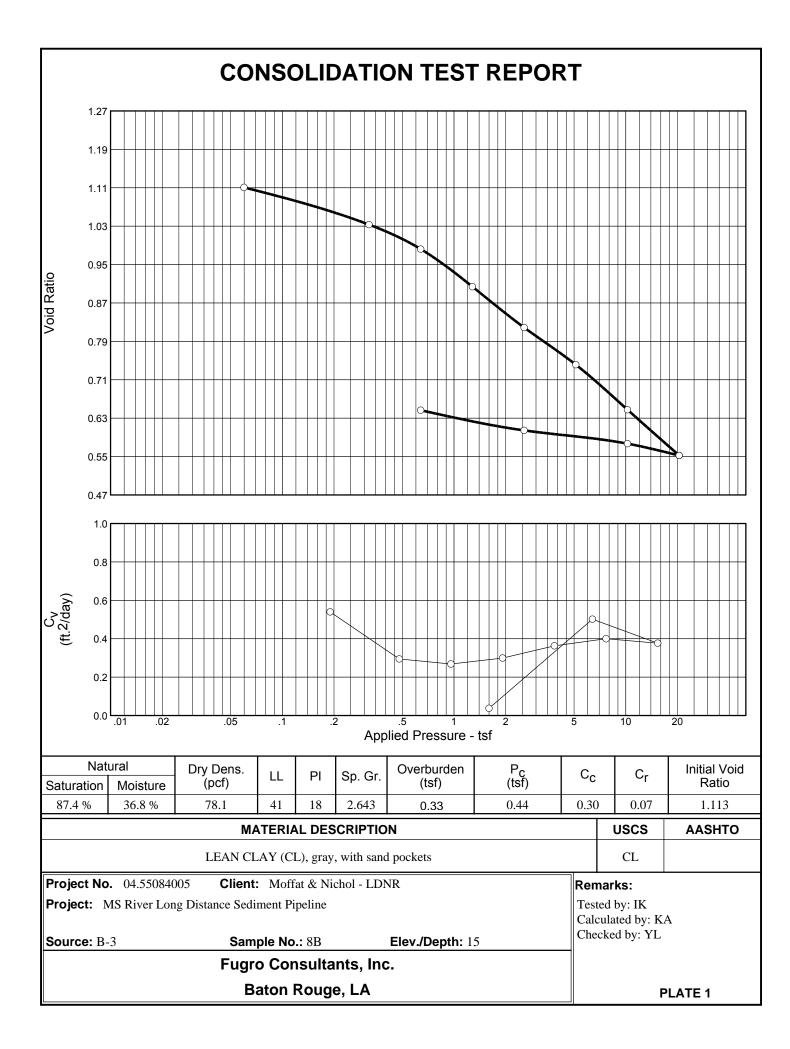
Jefferson Parish, Louisiana Fugro Consultants, Inc

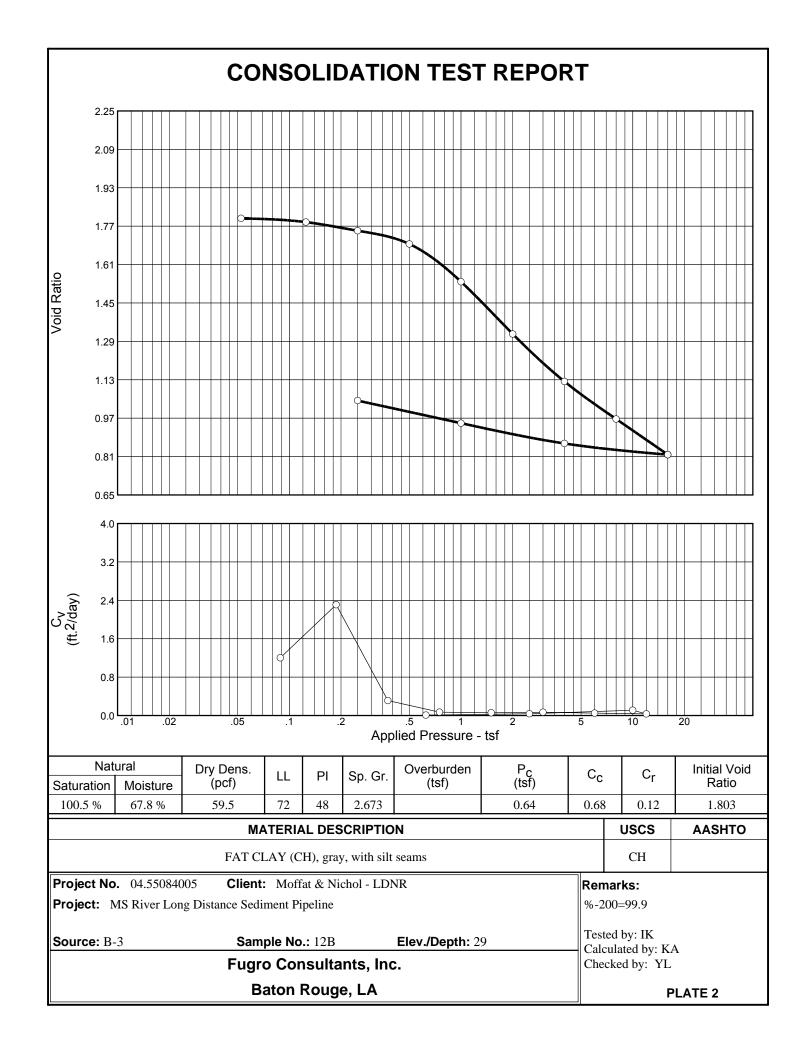


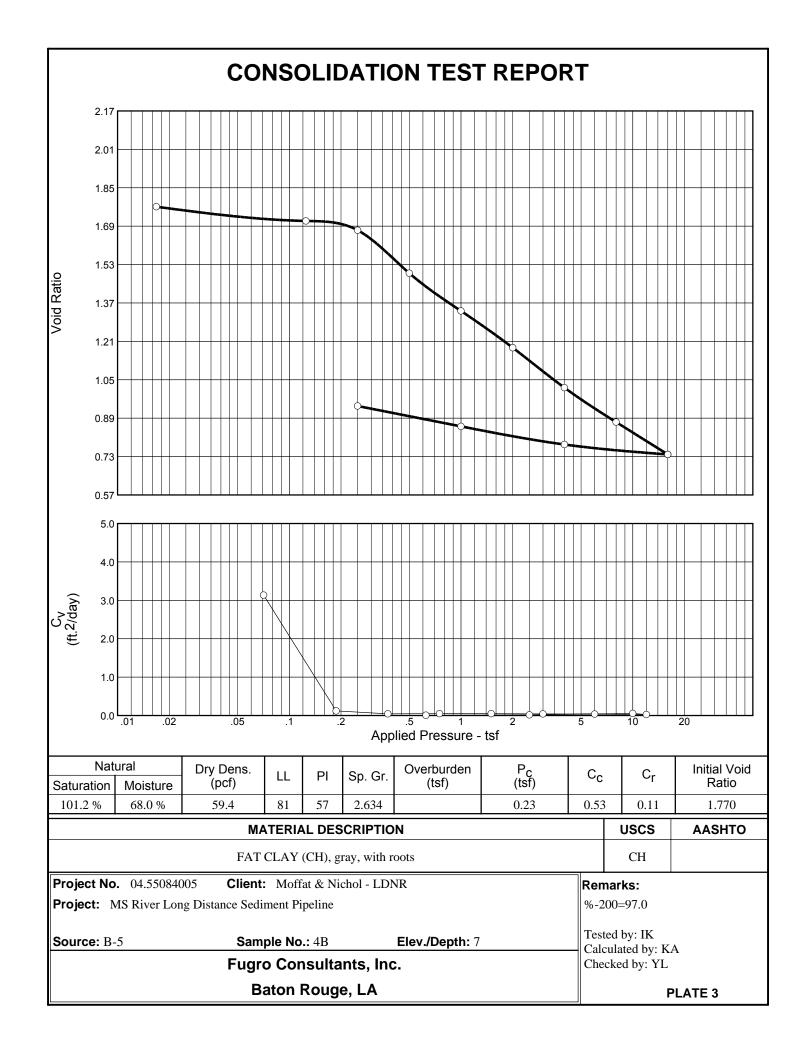


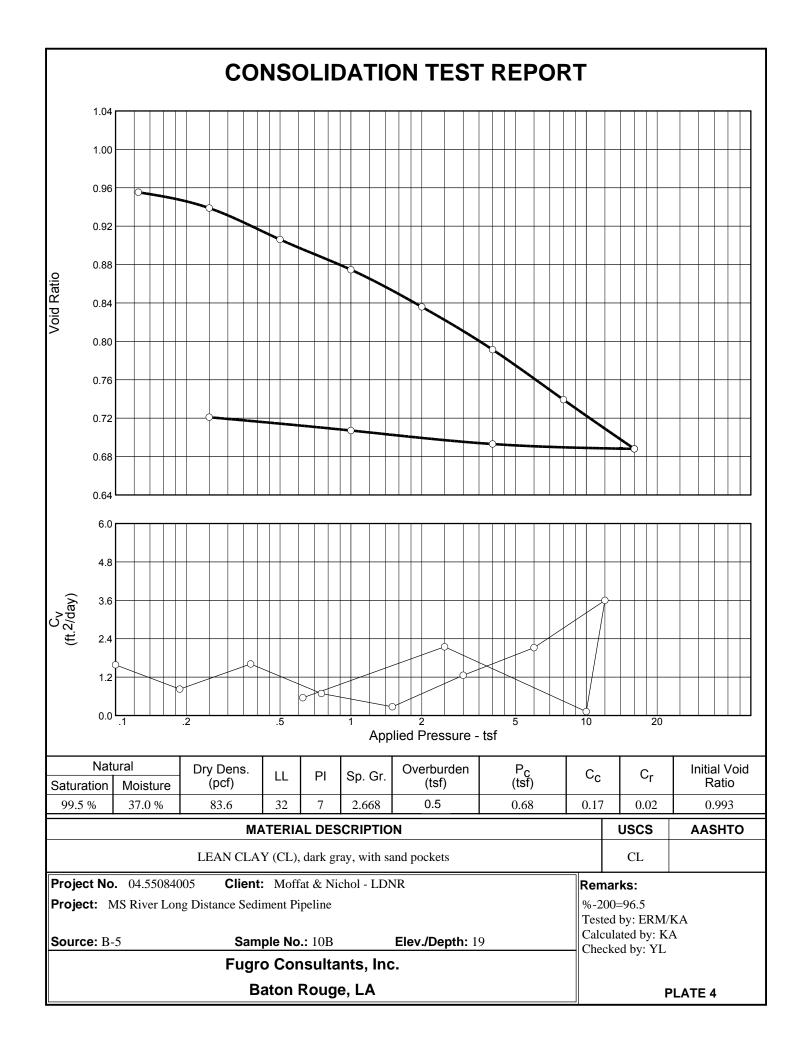
APPENDIX B ONE DIMENSIONAL CONSOLIDATION TEST RESULTS

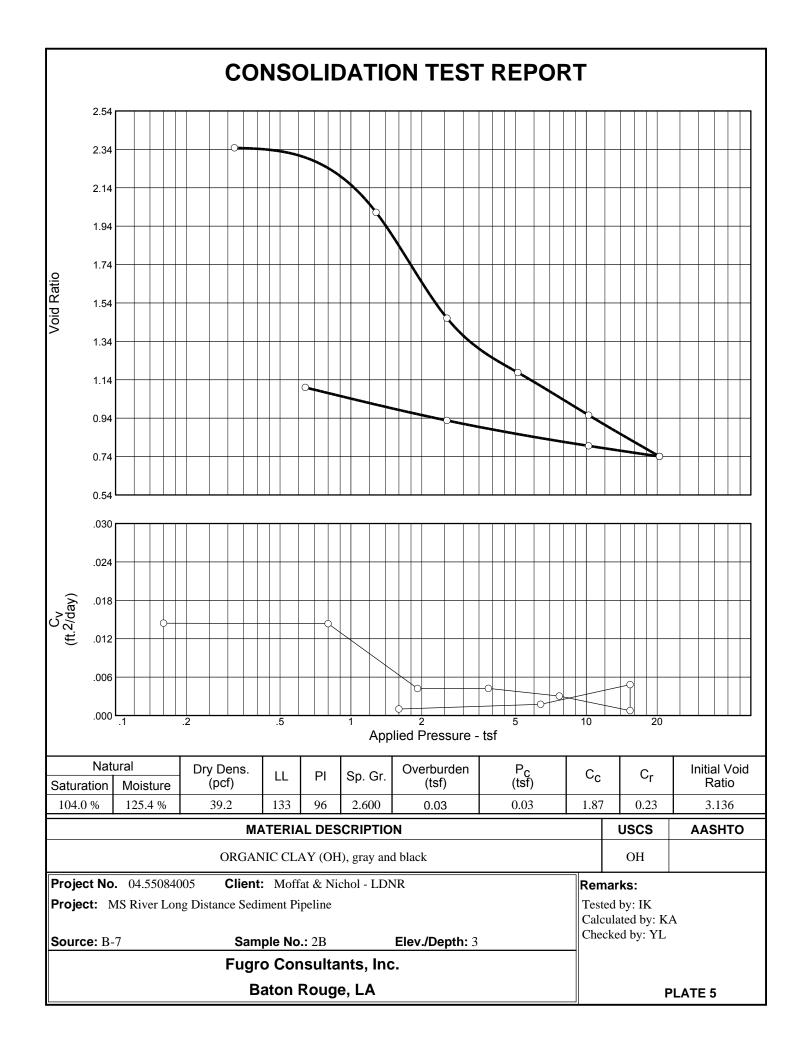


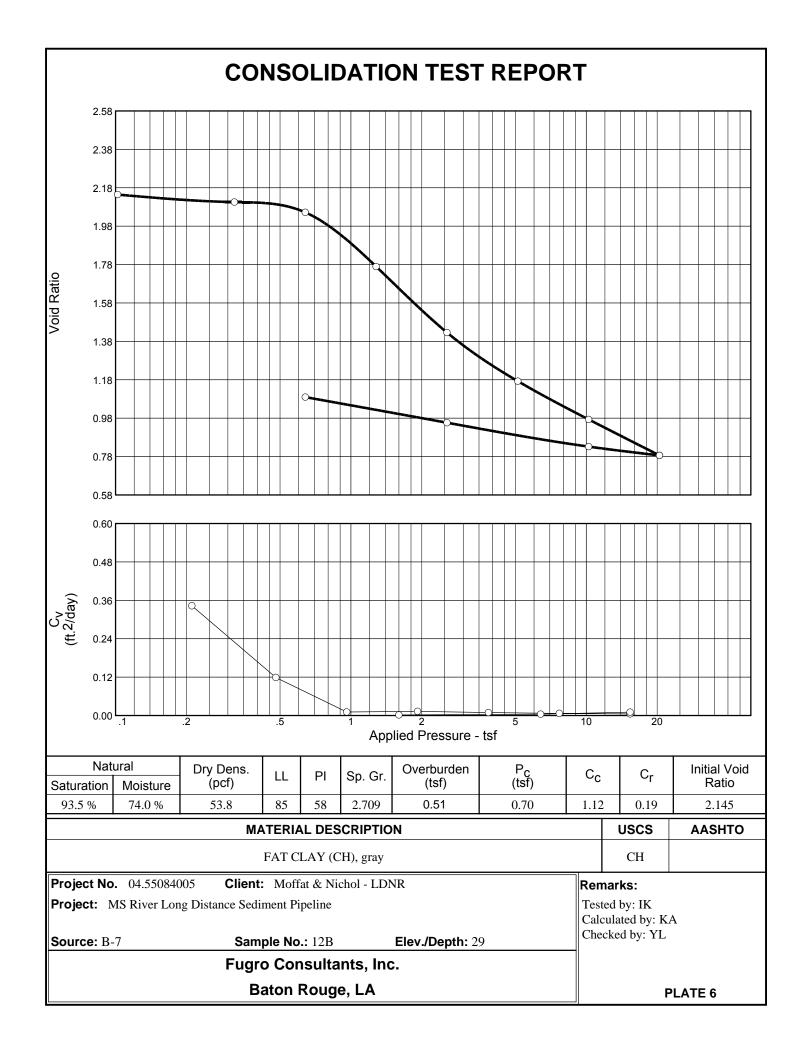


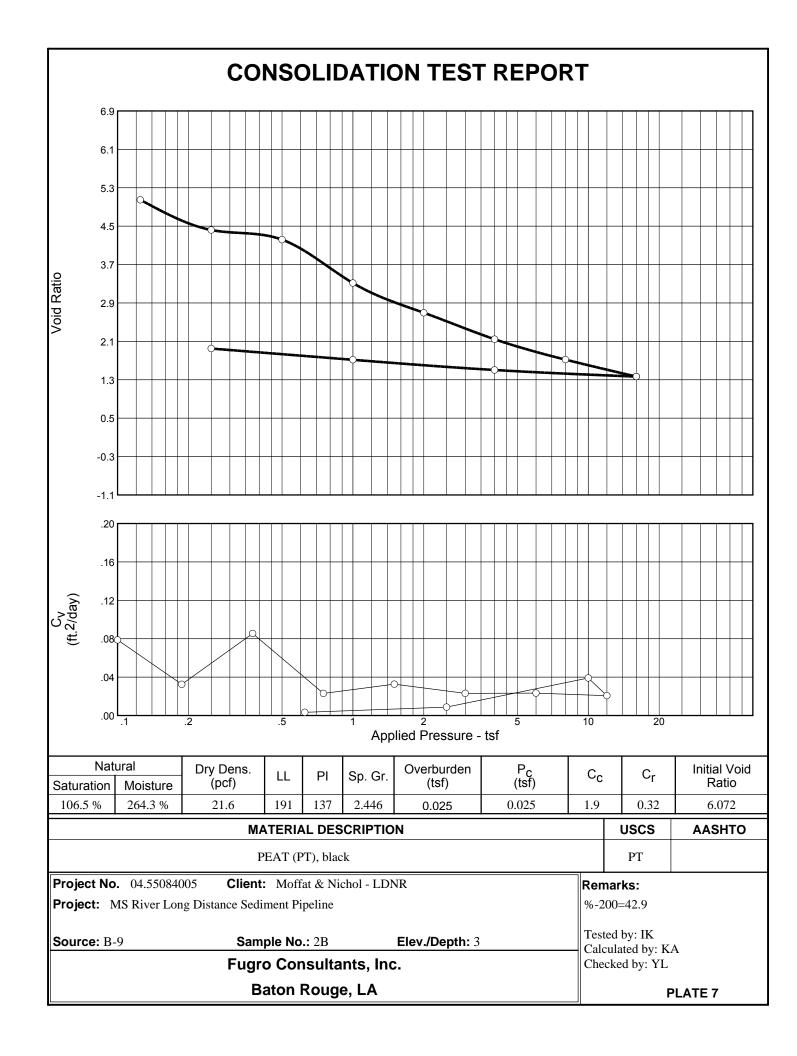


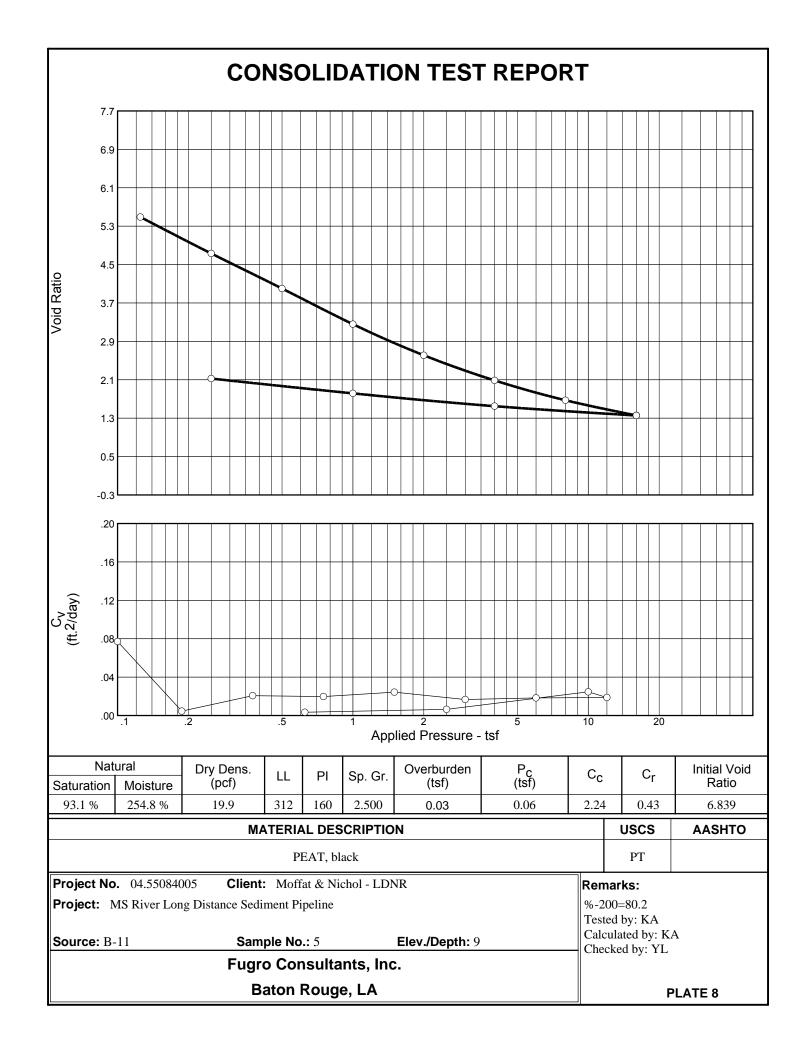


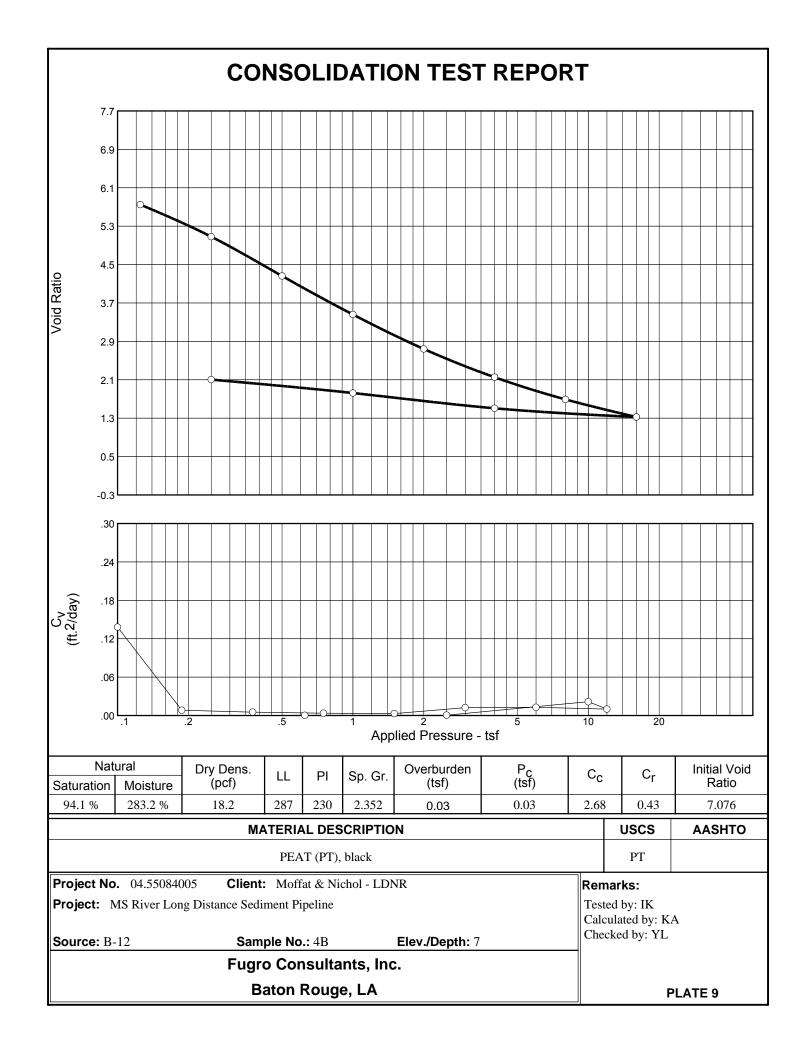


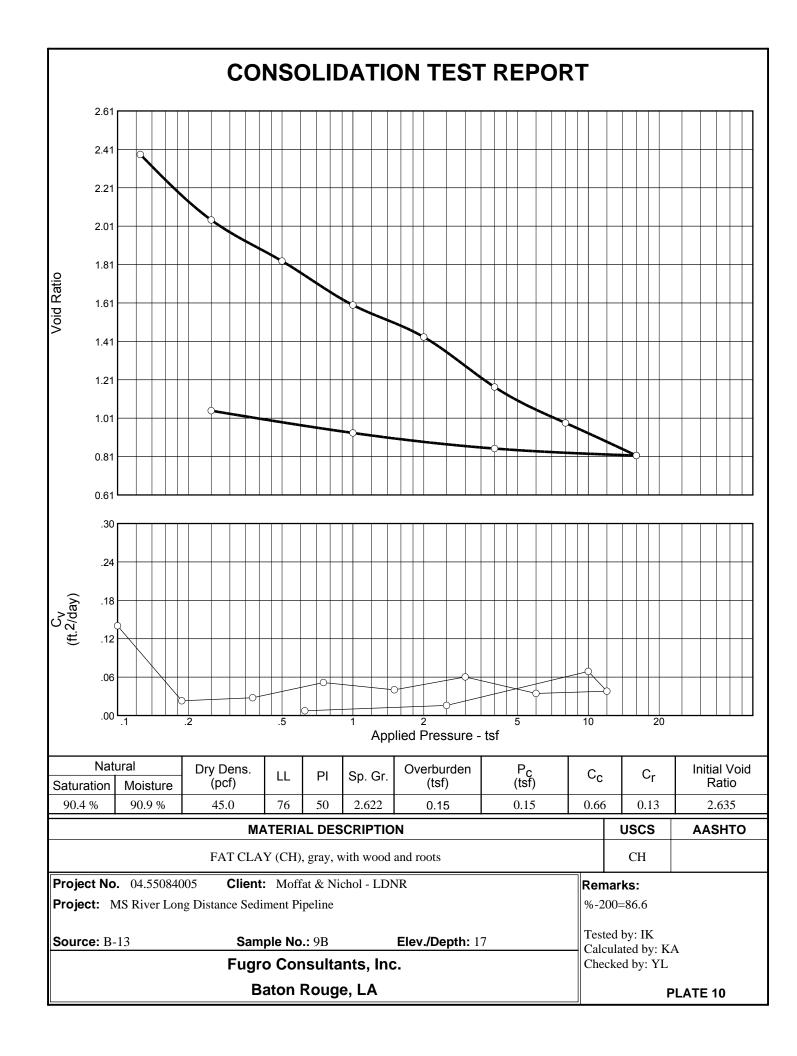


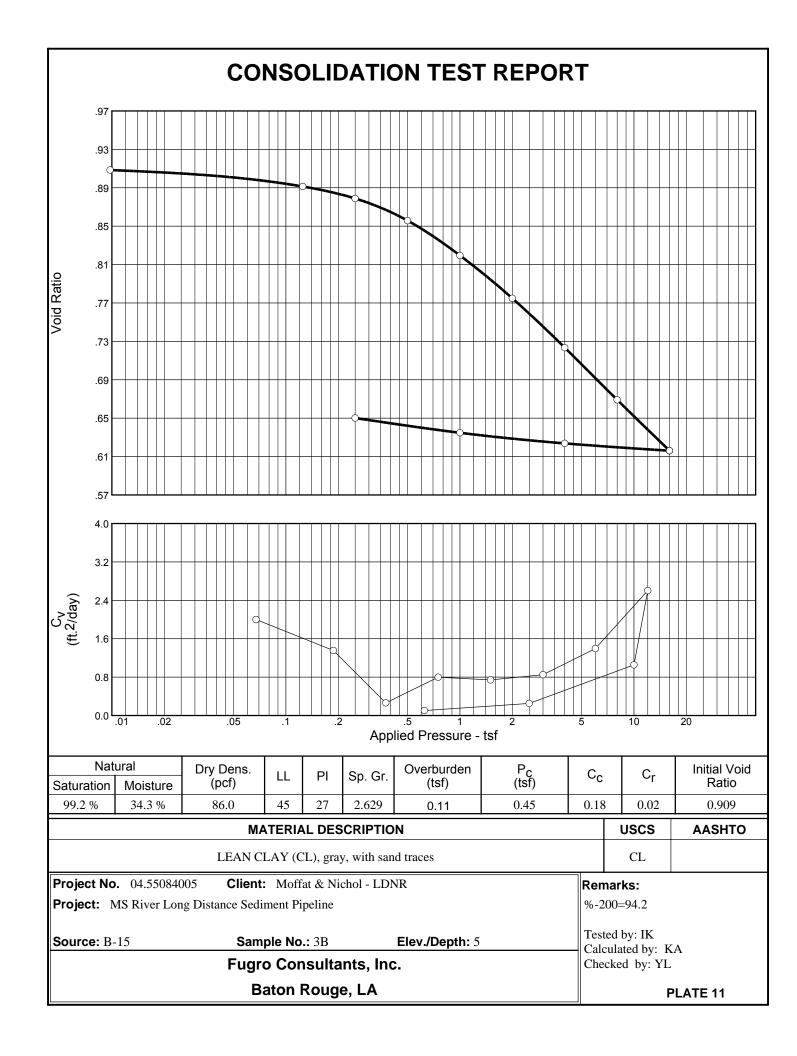


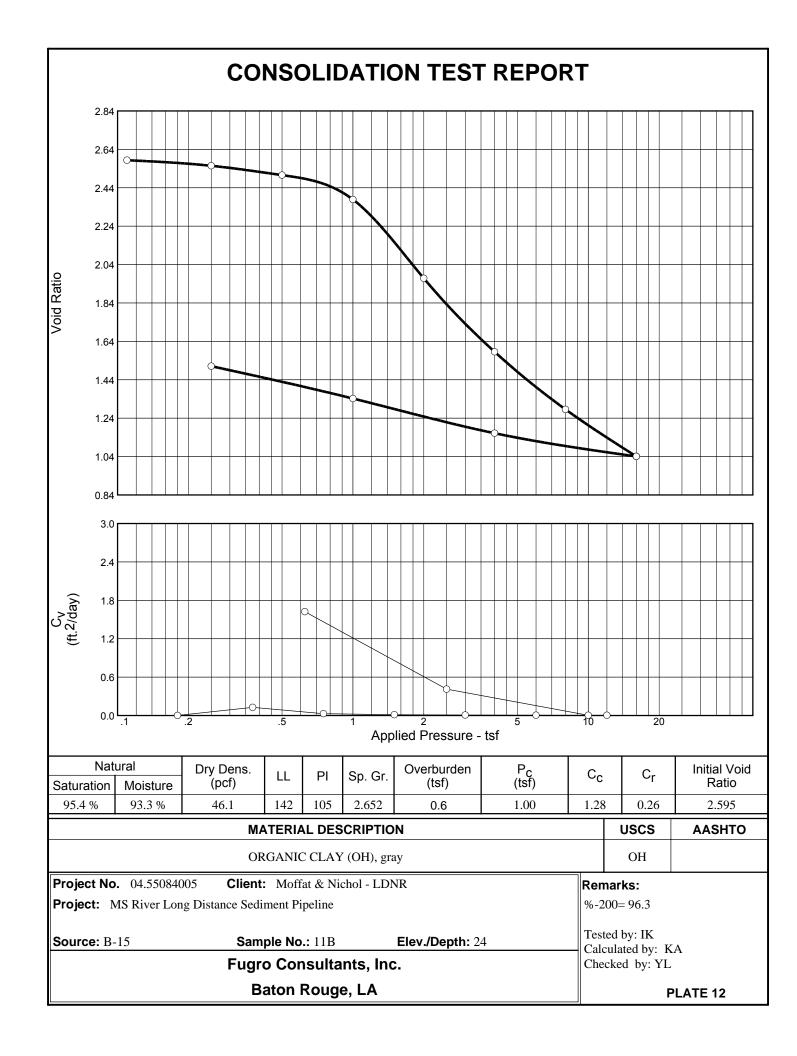


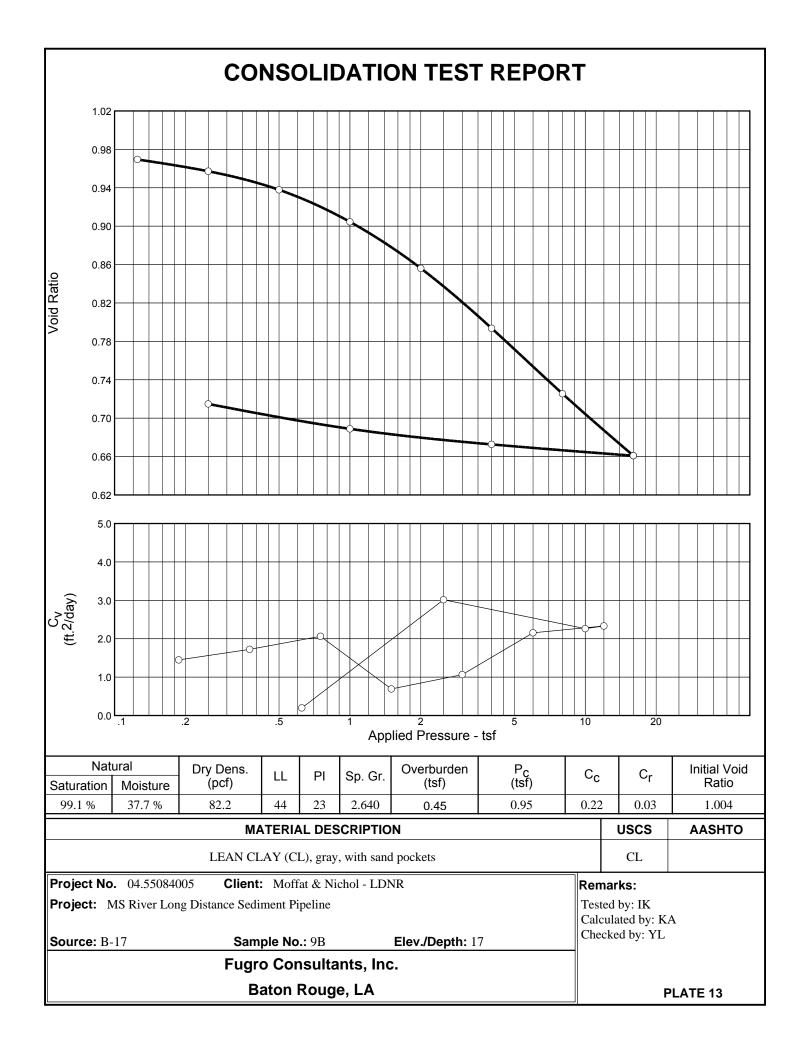


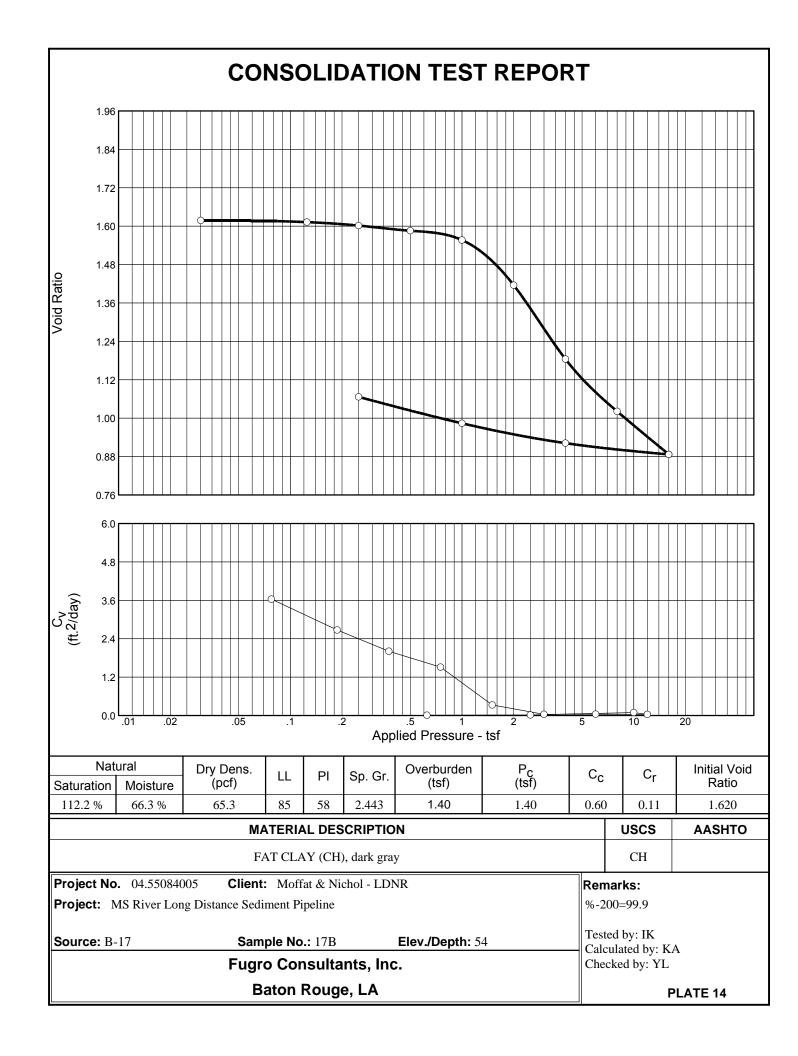


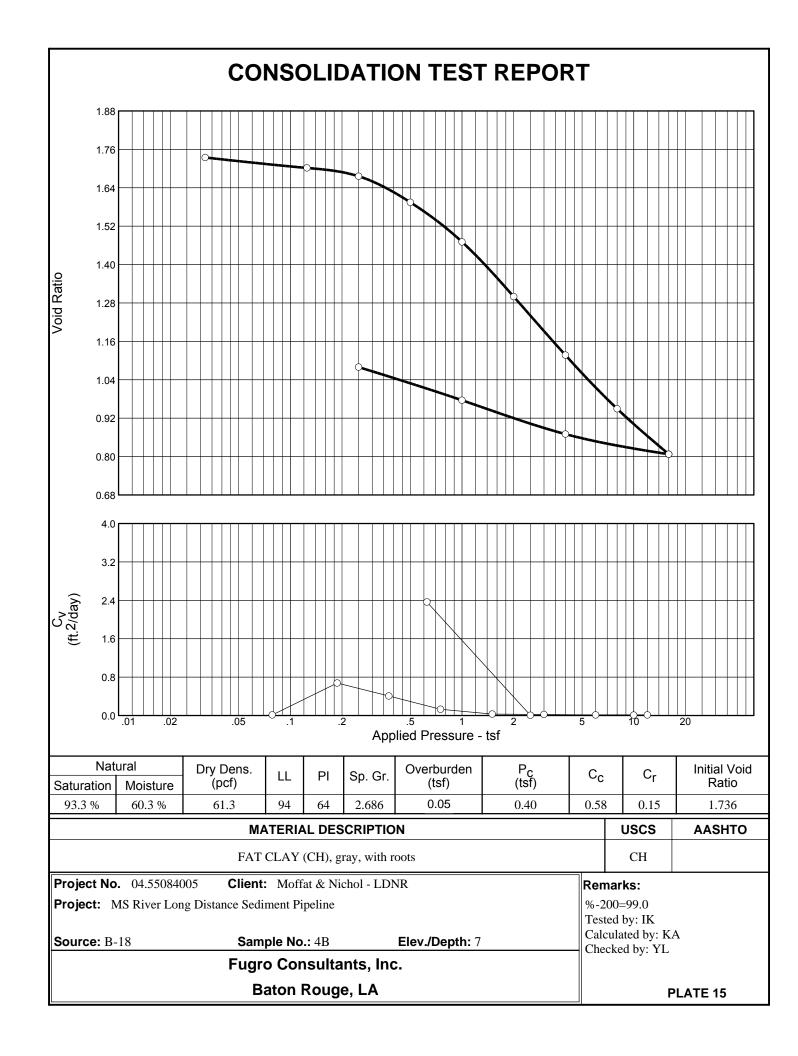


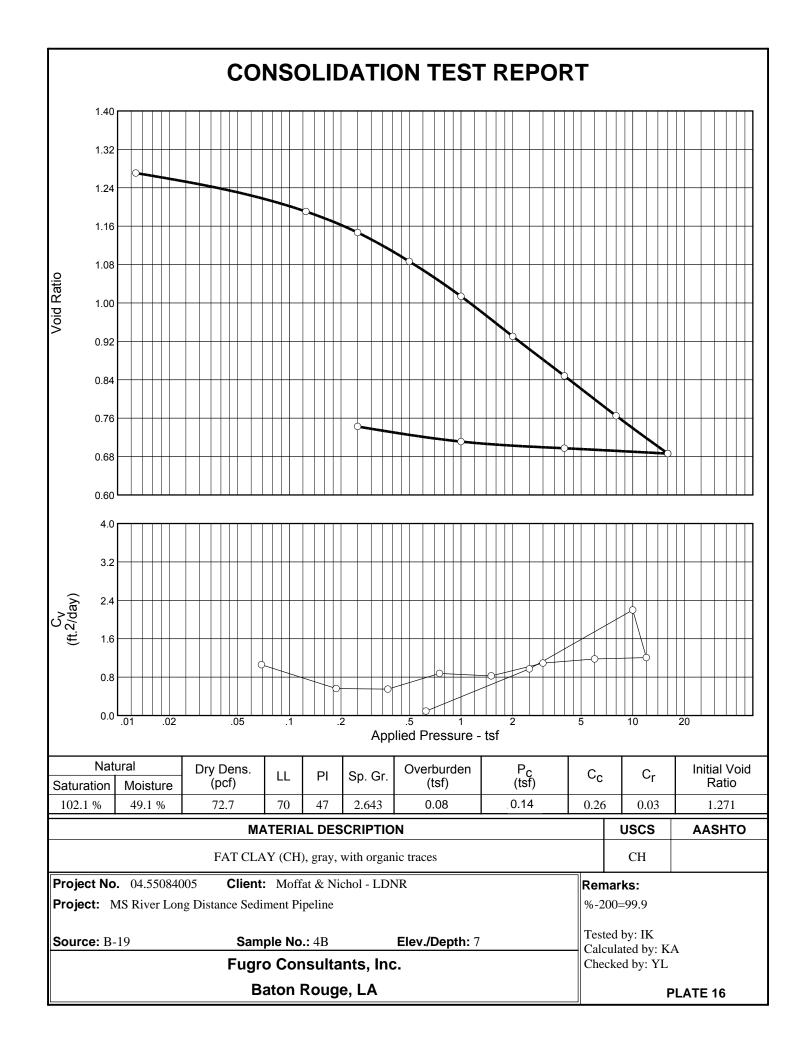


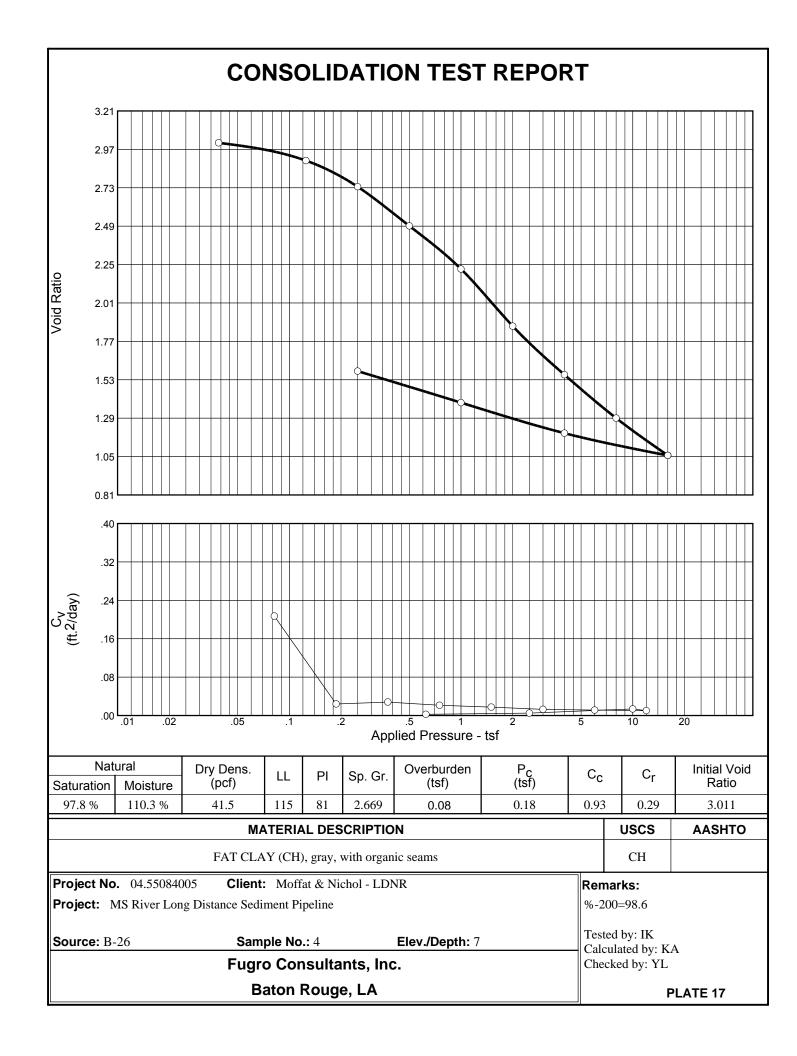


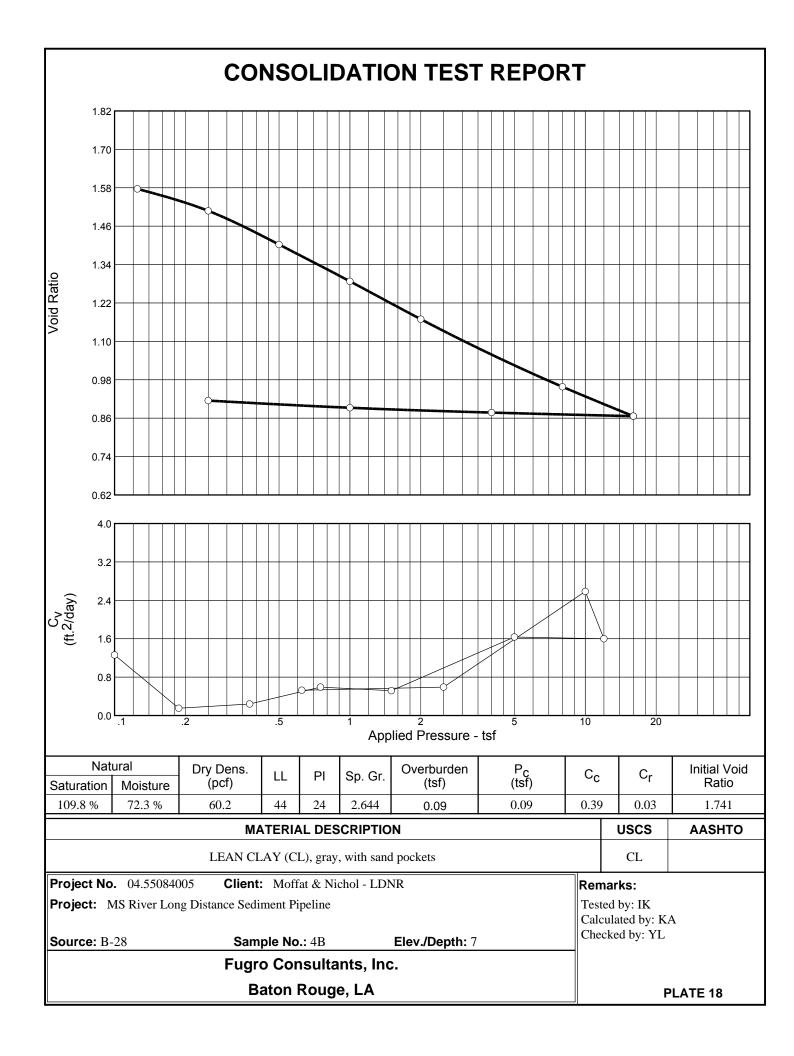


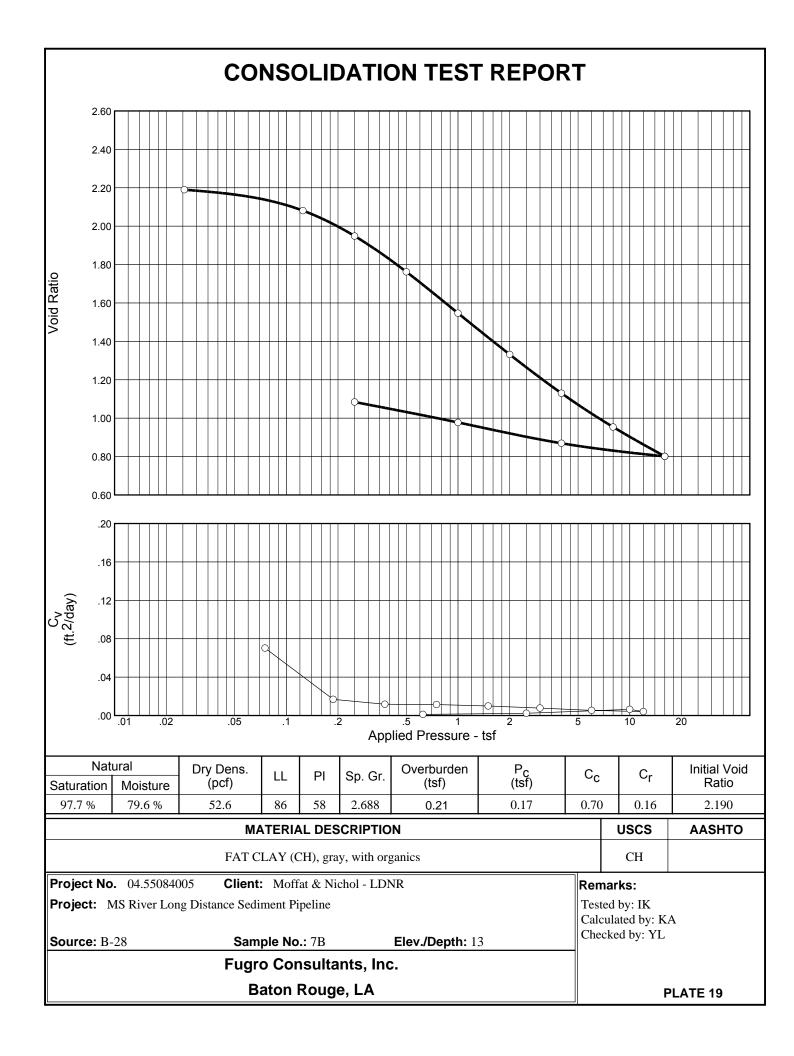


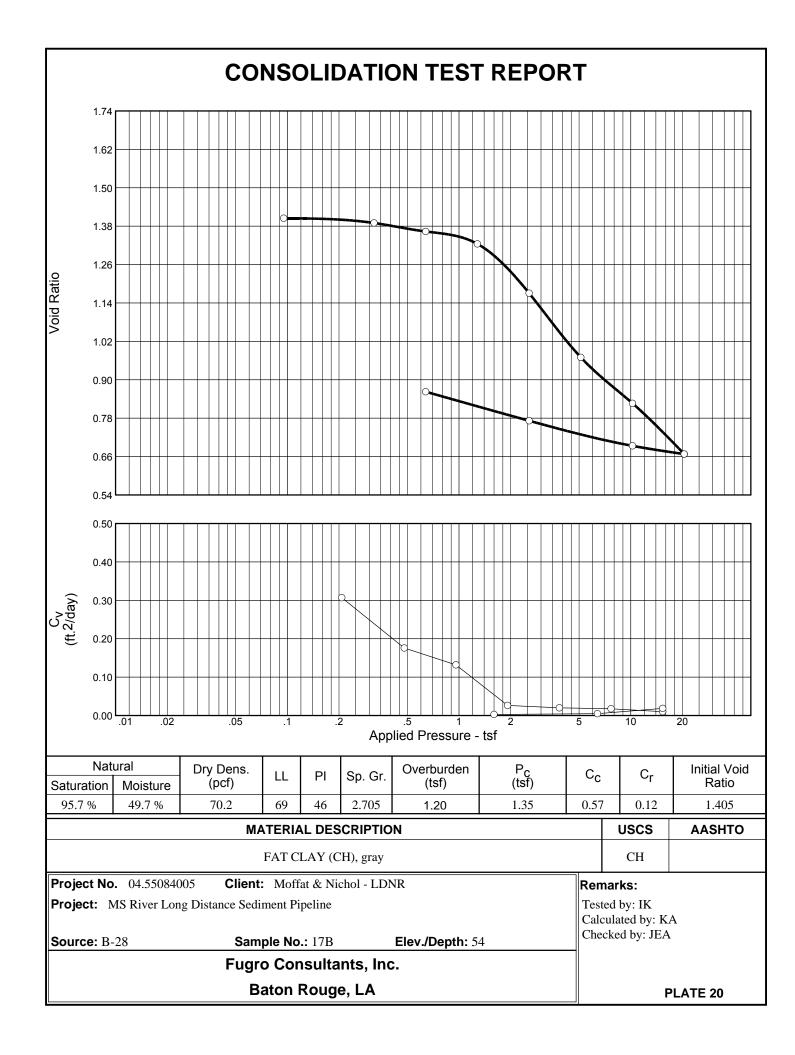


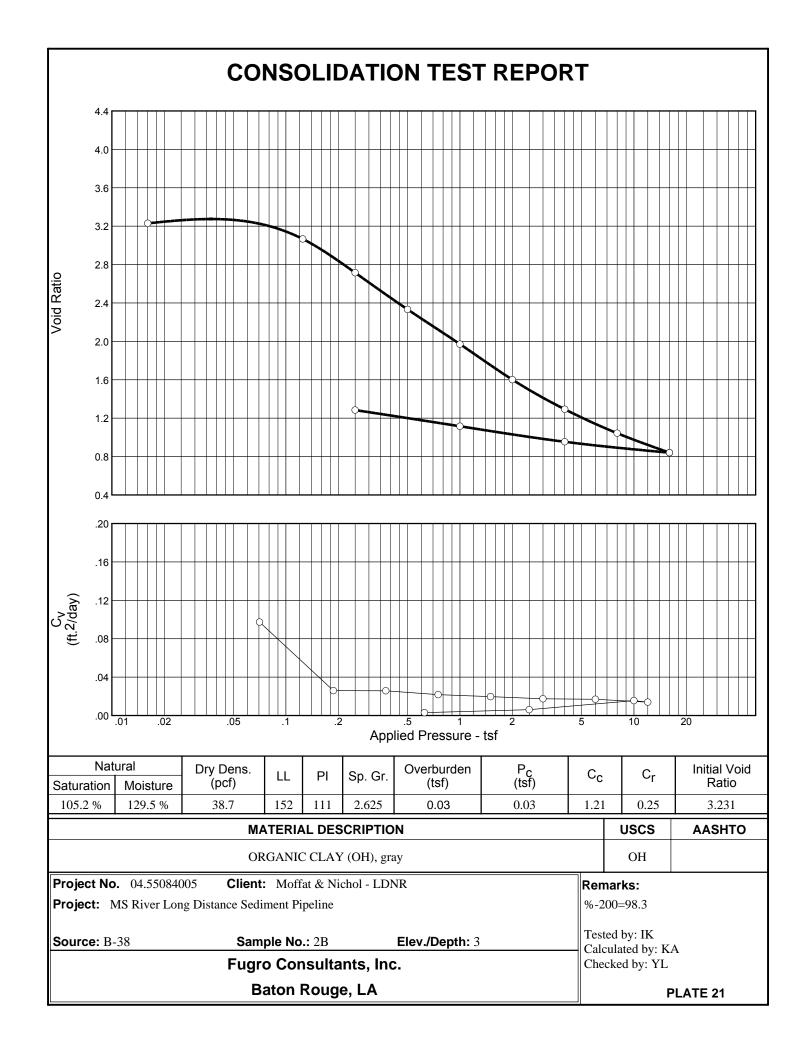


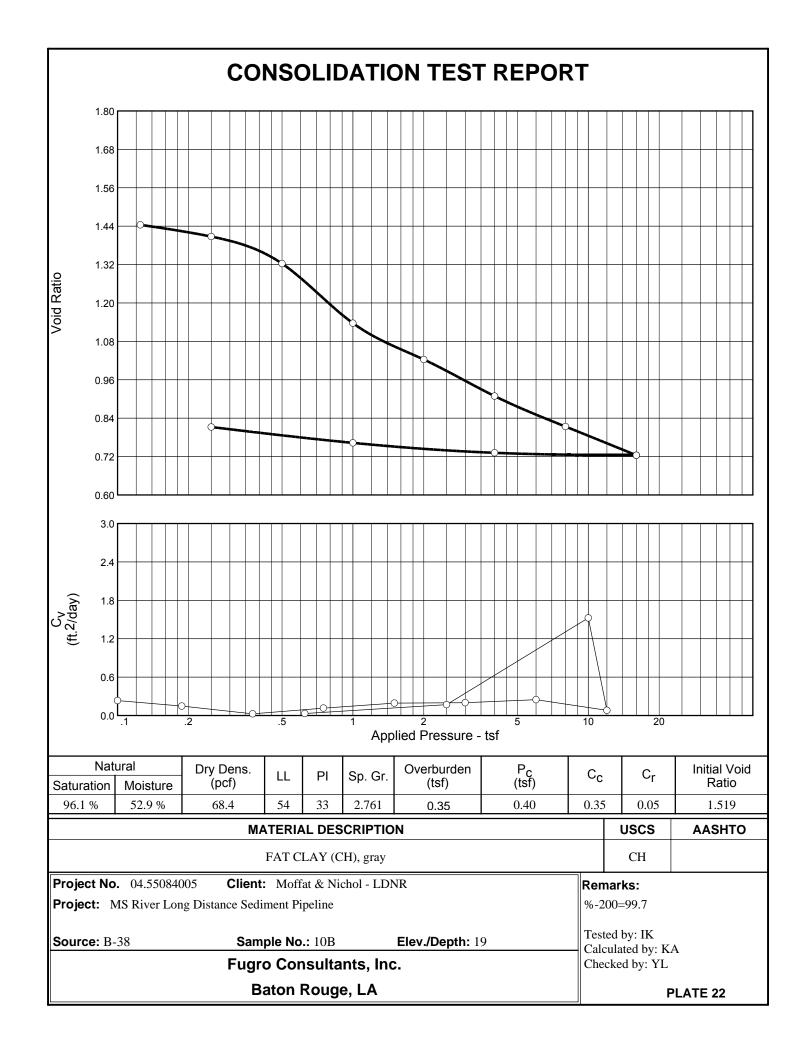


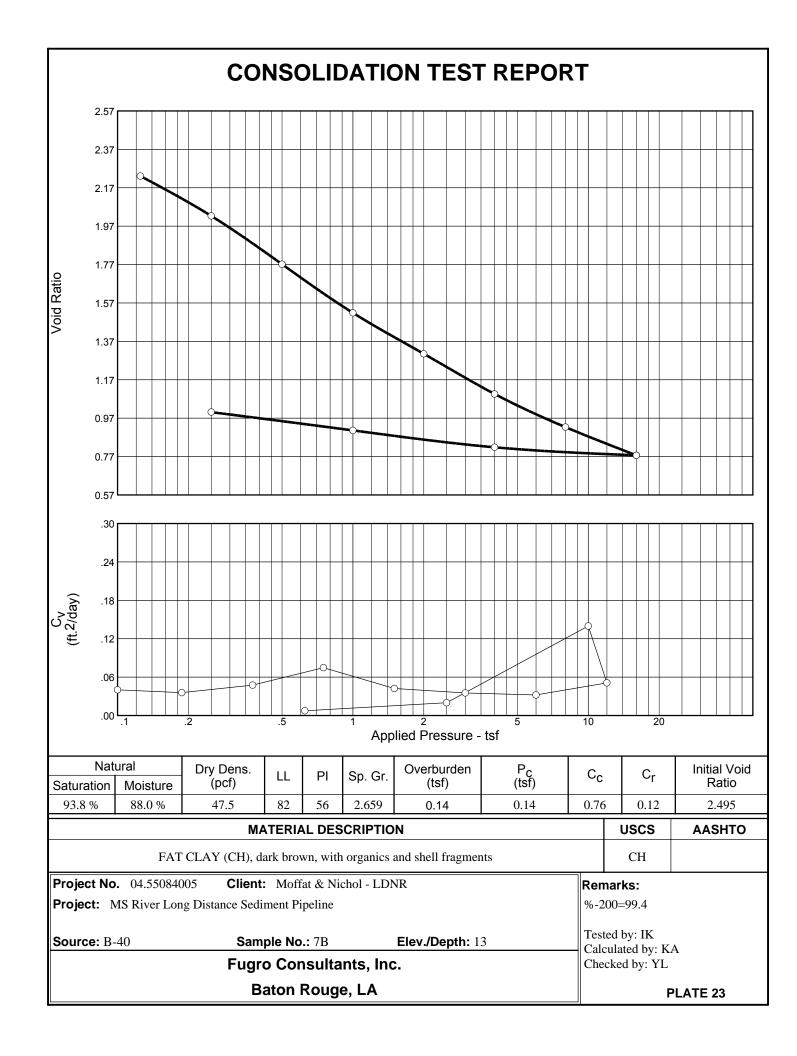


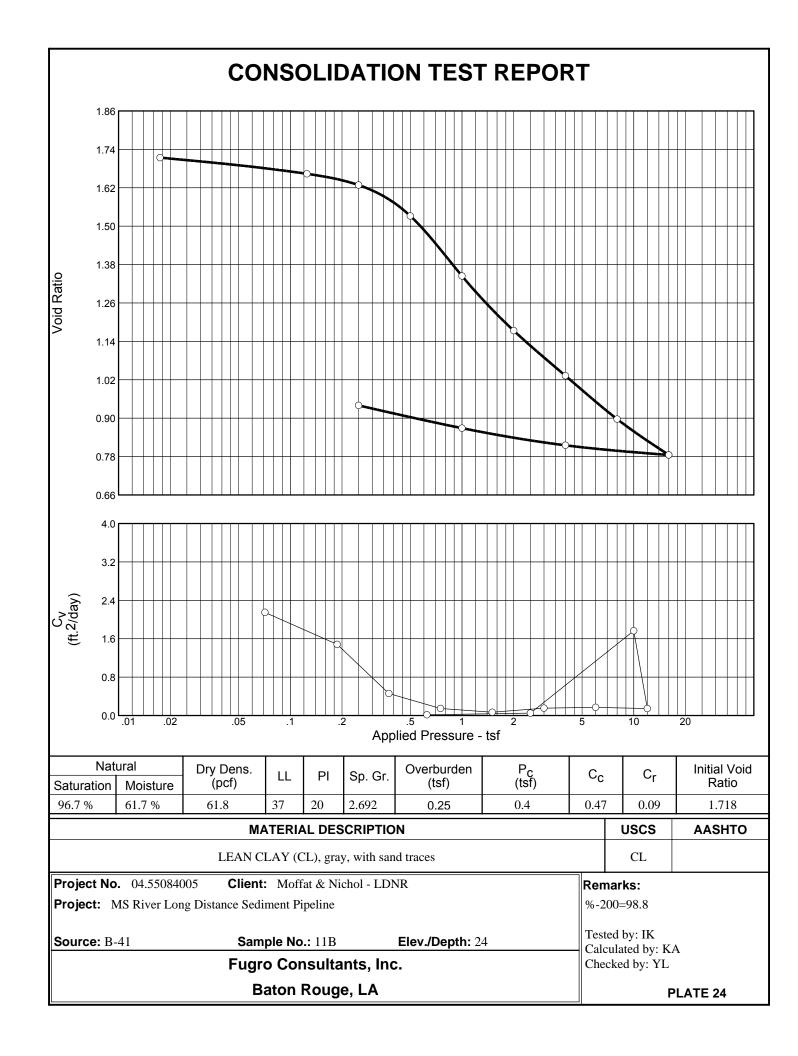


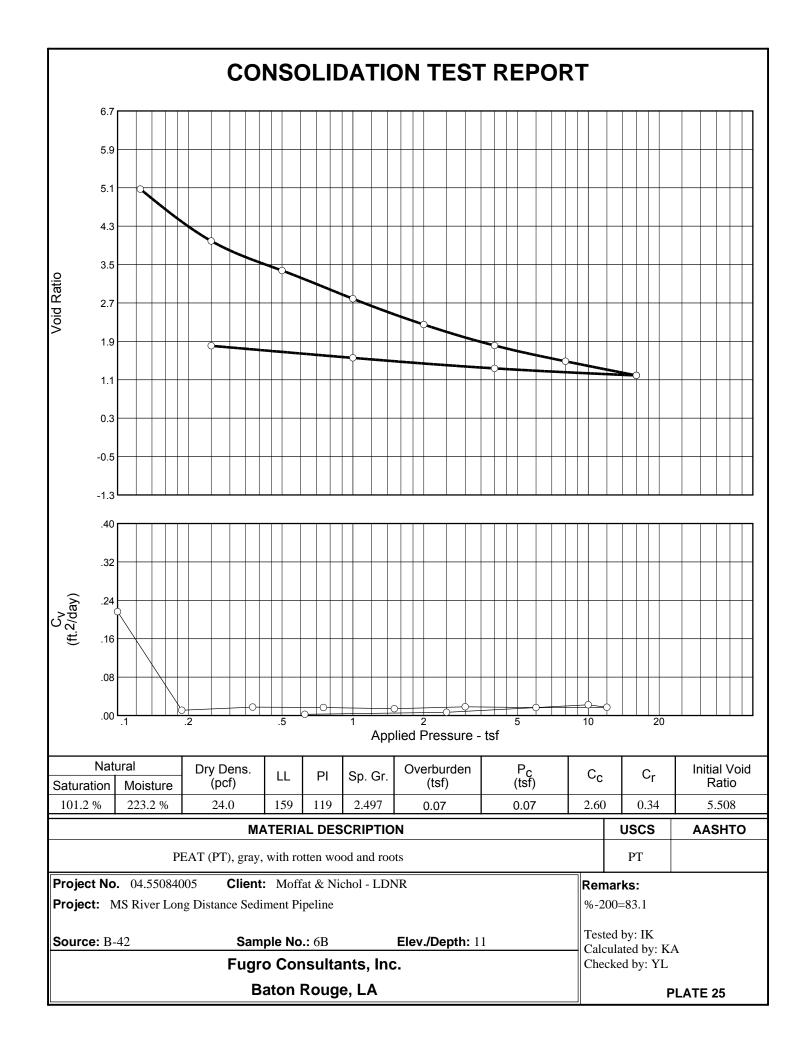


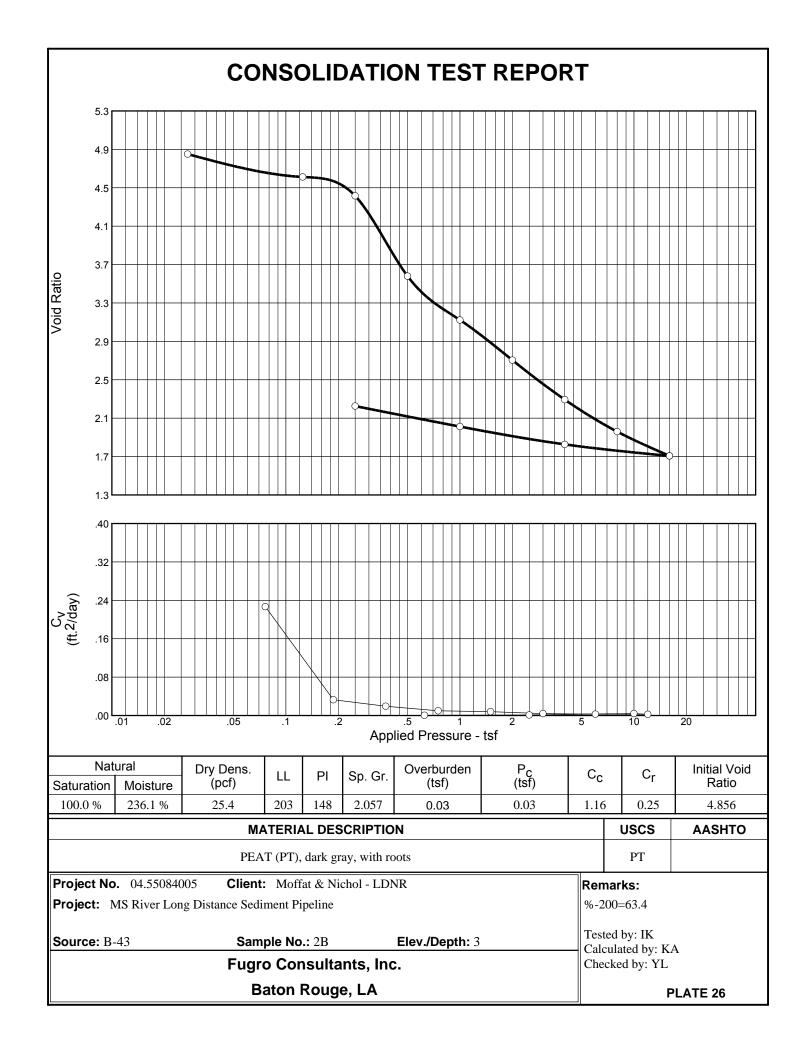


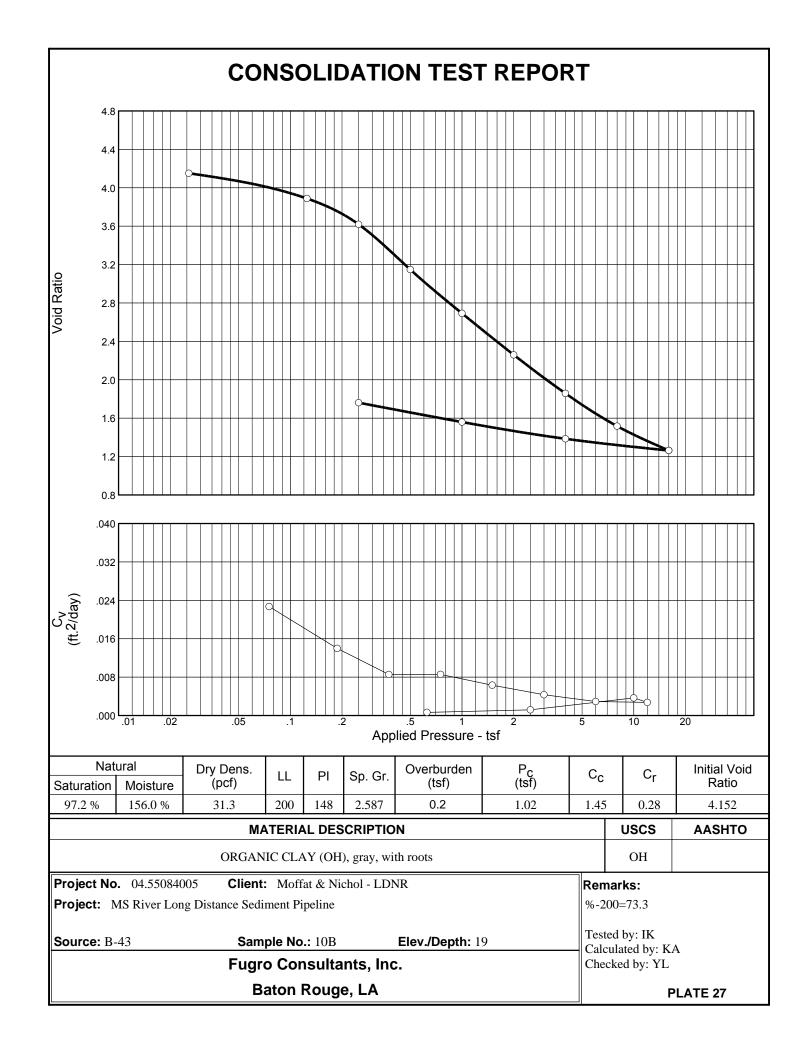












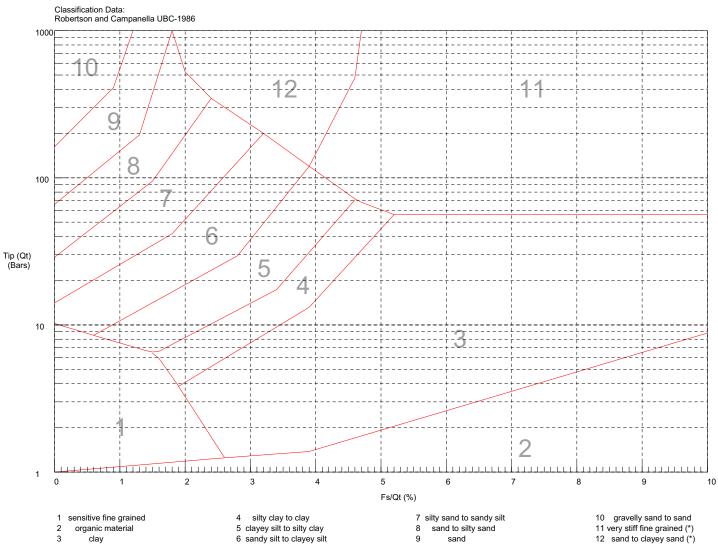


APPENDIX C CONE PENETRATION TEST LOGS





12 Zone Soil Behavior Chart



^{*} Overconsolidated or cemented





Job Number 04.5508-4005

CPT Number CPT-01

Location Baton Rouge-LA

Operator

David Cline

Date and Tin 24-Aug-2011 14:16:29

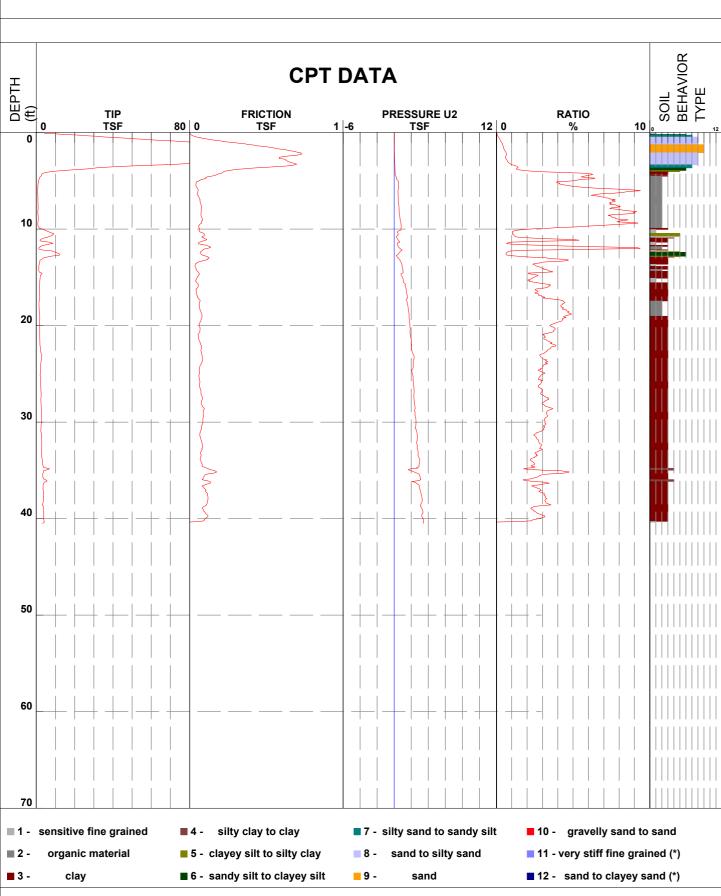
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc.

Elevation _____1.2'

Coordinate:N 29 39 18.8 W 90 00 50.3





Job Number 04.5508-4005

CPT Number CPT-02

Elevation

Location Baton Rouge-LA

Operator

David Cline

Date and Tin 25-Aug-2011 07:52:39

Cone Number A15F2.5CKE2H2403

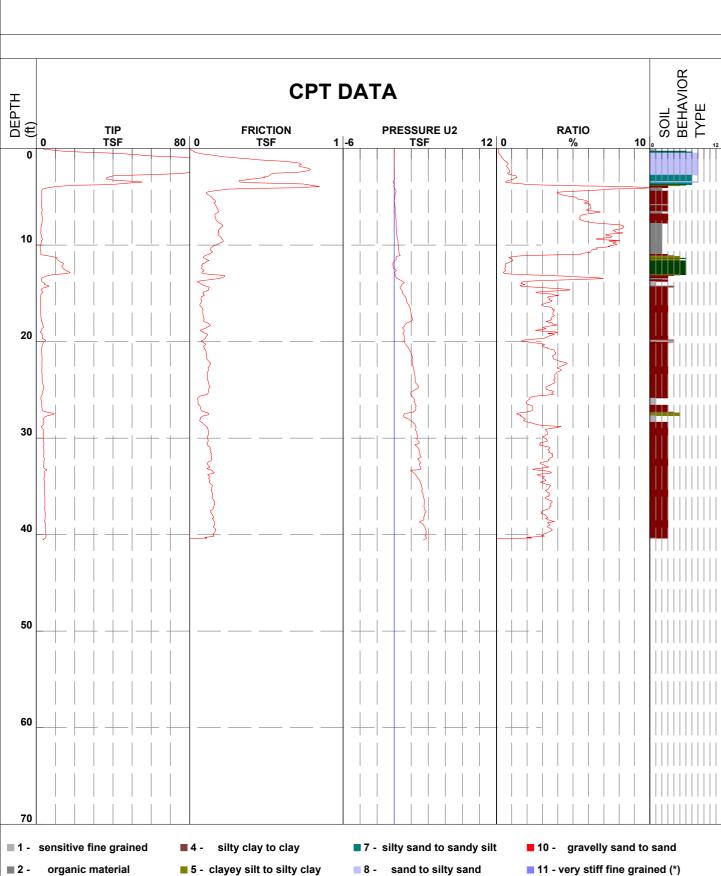
Client

Fugro Consultants, Inc.

2.1'

Coordinate:N 29 39 11.4 W 90 01 07.3

■ 12 - sand to clayey sand (*)



sand

■ 6 - sandy silt to clayey silt

■ 3 -

clay



Job Number 04.5508-4005

CPT Number CPT-03

Location Baton Rouge-LA

Cone Number A15F2.5CKE2H2403

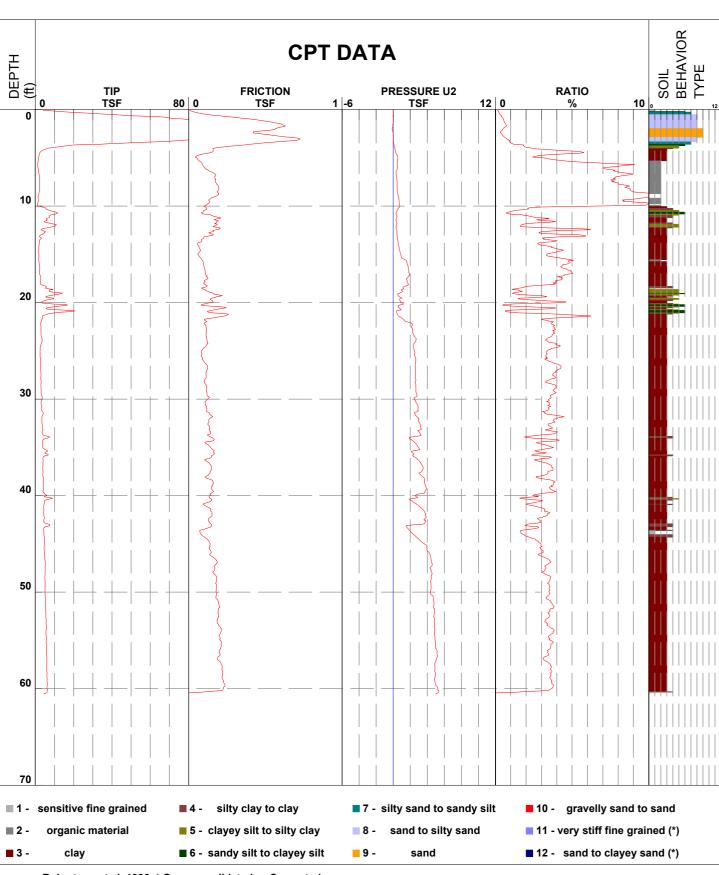
Operator

David Cline

Date and Tir 18-Aug-2011 09:28:47

Client Fugro Consultants, Inc. Elevation 1.5'

Coordinate:N 29 39 09.1 W 90 01 25.4





Job Number 04.5508-4005

CPT Number CPT-04

Elevation

Location Baton Rouge-LA

Operator

Herbert Jackson

Date and Tin 13-Sep-2011 15:22:16

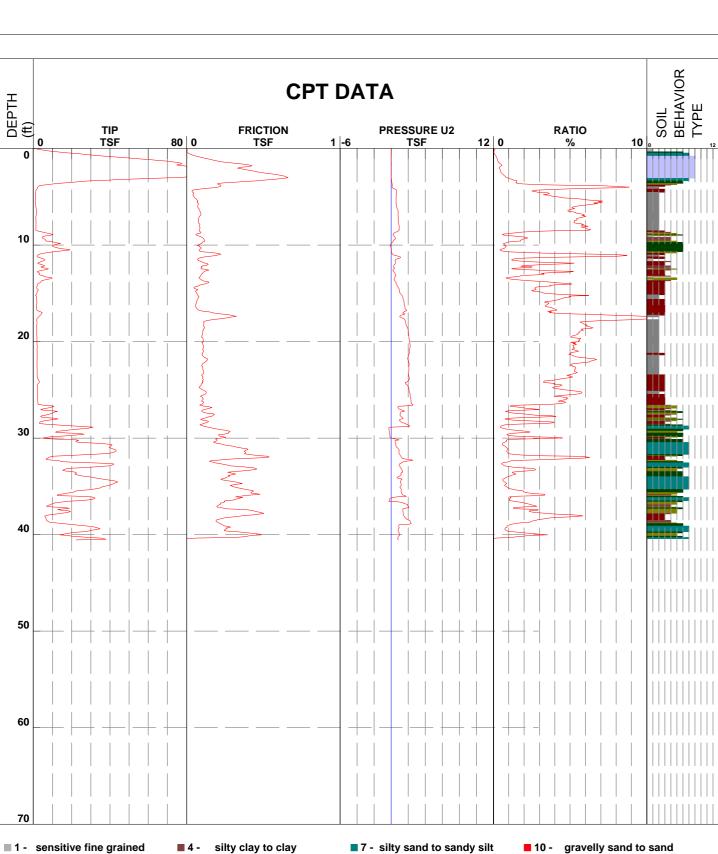
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc.

1.3'

Coordinate:N 29 38 56.3 W 90 01 44.4



sand to silty sand

sand

11 - very stiff fine grained (*)

■ 12 - sand to clayey sand (*)

■ 2 -

3 -

organic material

clay

■ 5 - clayey silt to silty clay

■ 6 - sandy silt to clayey silt



Job Number 04.5508-4005

CPT Number CPT-06

Baton Rouge-LA

Operator

Herbert Jackson

Date and Tin 13-Sep-2011 12:47:17

Location

Cone Number A15F2.5CKE2H2403

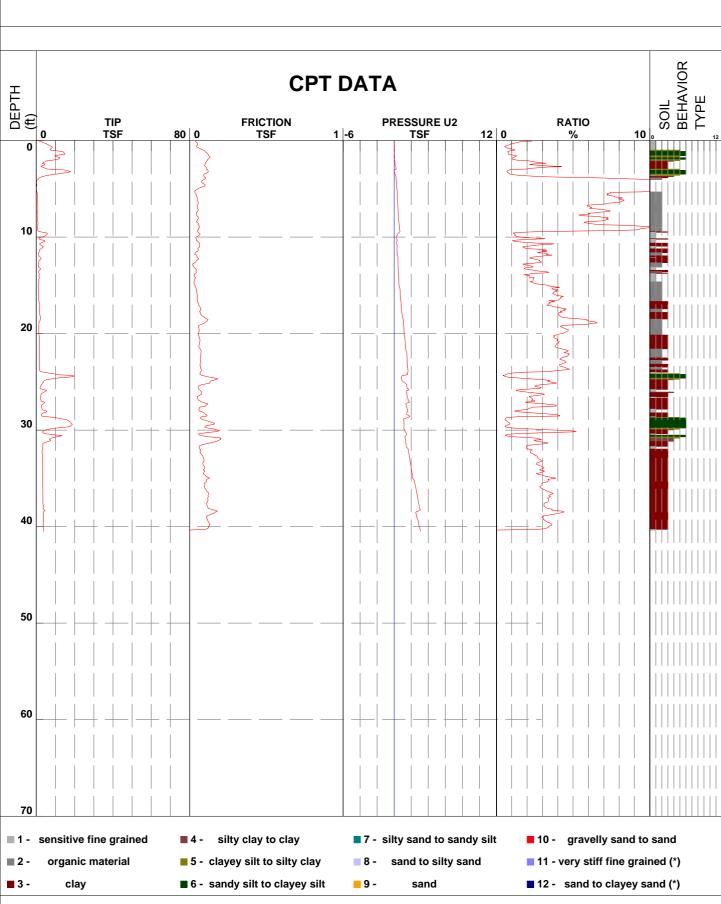
Client

Fugro Consultants, Inc.

Elevation

0.7'

Coordinate:N 29 38 40.5 W 90 02 18.2





Job Number 04.5508-4005

CPT Number CPT-7

Location Baton Rouge-LA

Operator

David Cline

Date and Tin 17-Aug-2011 14:16:21

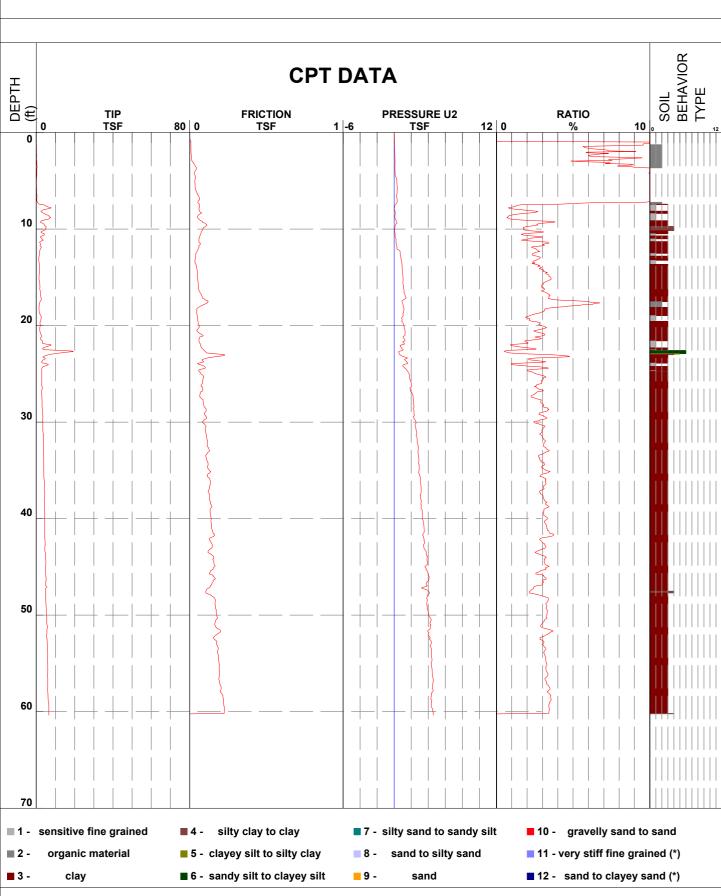
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc.

Elevation -0.80'

Coordinate(N 29 38 27.9 W 90 02 38.7





Job Number 04.5508-4005

CPT Number CPT-08

Location Baton Rouge-LA

Operator

Herbert Jackson

Date and Tin 13-Sep-2011 10:55:19

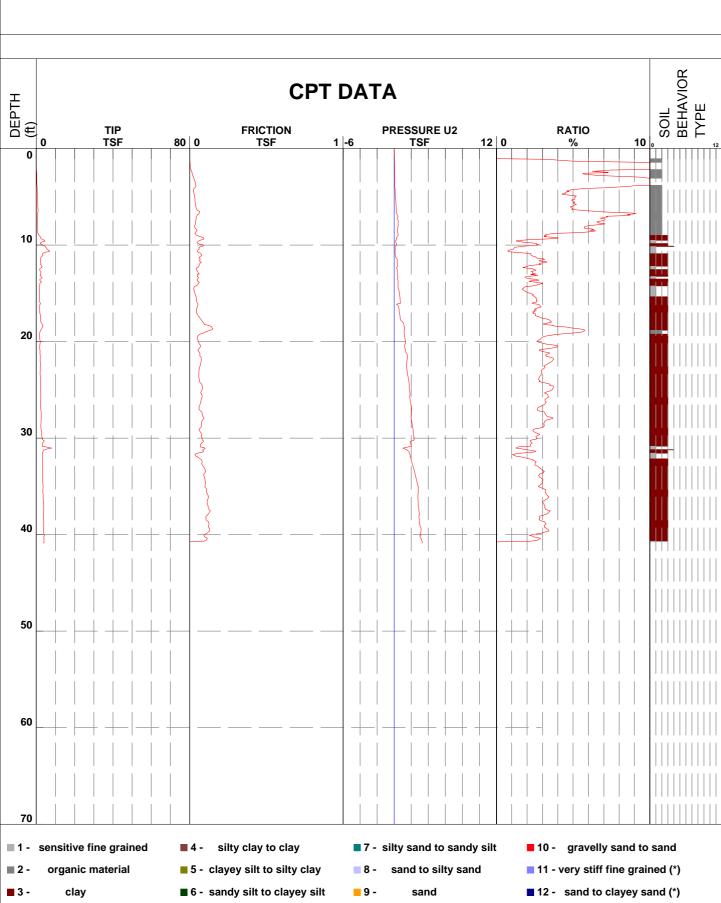
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc.

Elevation -2.2'

Coordinate:N 29 38 17.6 W 90 02 48.4





Job Number 04.5508-4005

CPT Number CPT-10 Location **Baton Rouge-LA**

Operator

David Cline

Date and Tin 17-Aug-2011 11:54:25

Cone Number A15F2.5CKE2H2403

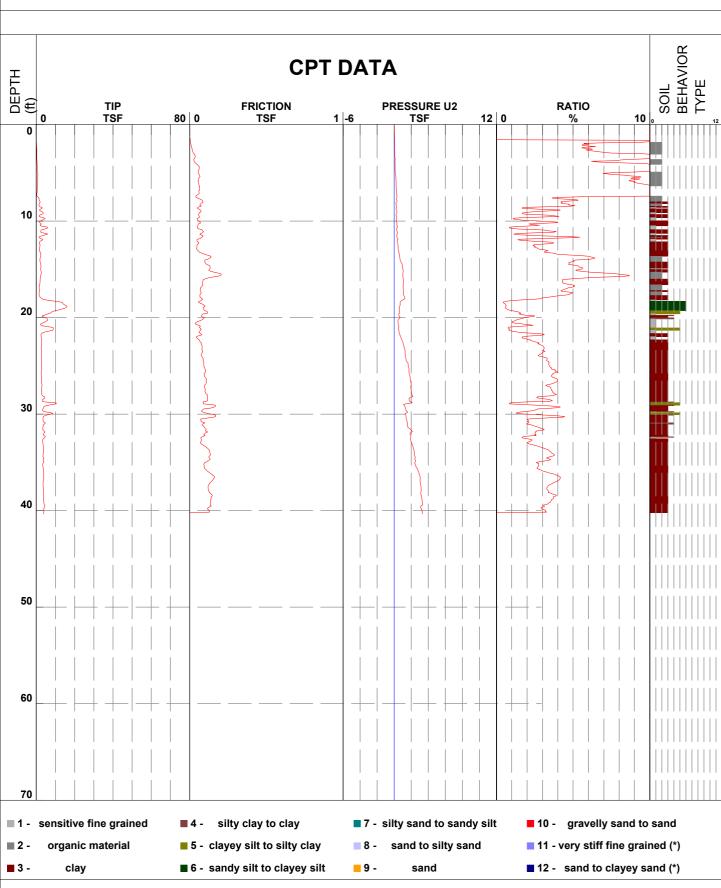
Client

Fugro Consultants, Inc.

Elevation

-1.7'

Coordinate:N 29 37 26.1 W 90 03 03.5





Job Number 04.5508-4005

CPT Number CPT-14

_

Location

Baton Rouge-LA

Operator

David Cline

Date and Tin 17-Aug-2011 08:02:21

-

Cone Number <u>A15F2.5CKE2H2403</u> CoordinatesN 29 36 19.3 W 90 03 17.1

Client Fugro Consultants, Inc. Elevation -1.5' **CPT DATA** DEPTH (ft) **FRICTION** PRESSURE U2 TIP **RATIO** 10 **TSF** 80 0 **TSF** 1 -6 **TSF** 12 0 0 10 20 30 40 50 60 70

■ 7 - silty sand to sandy silt

sand

sand to silty sand

■ 10 - gravelly sand to sand

11 - very stiff fine grained (*)12 - sand to clayey sand (*)

silty clay to clay

■ 5 - clayey silt to silty clay

■ 6 - sandy silt to clayey silt

sensitive fine grained

organic material

clay

■ 1 -■ 2 -

■ 3 -



Job Number 04.5508-4005

CPT Number CPT-16 Location **Baton Rouge-LA**

Operator

Herbert Jackson

Date and Tin 12-Sep-2011 09:56:21

Cone Number A15F2.5CKE2H2053

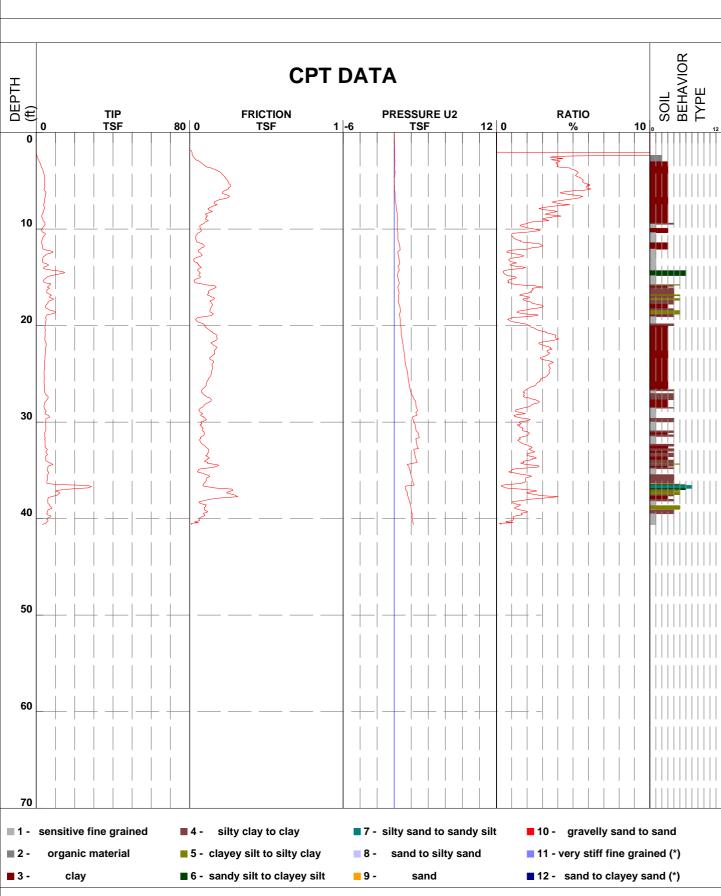
Client

Fugro Consultants, Inc.

Elevation

-2.0'

Coordinate N 29 36 14.2 W 90 03 56.8





Job Number 04.5508-4005

CPT Number CPT-17

Location Baton Rouge-LA

Operator

David Cline

Date and Tin 19-Aug-2011 08:42:08

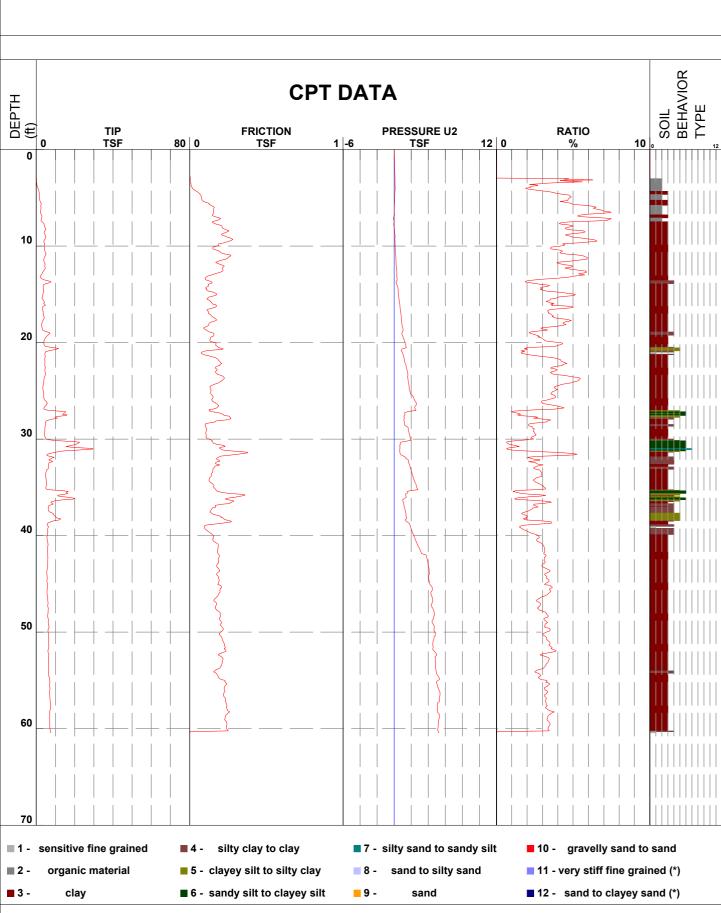
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc.

Elevation -2.30'

Coordinate:N 29 36 10.4 W 90 04 16.3





Job Number 04.5508-4005

CPT Number_ CPT-26 Location **Baton Rouge-LA**

Operator

Herbert Jackson

Date and Tin 13-Sep-2011 08:02:27

Client

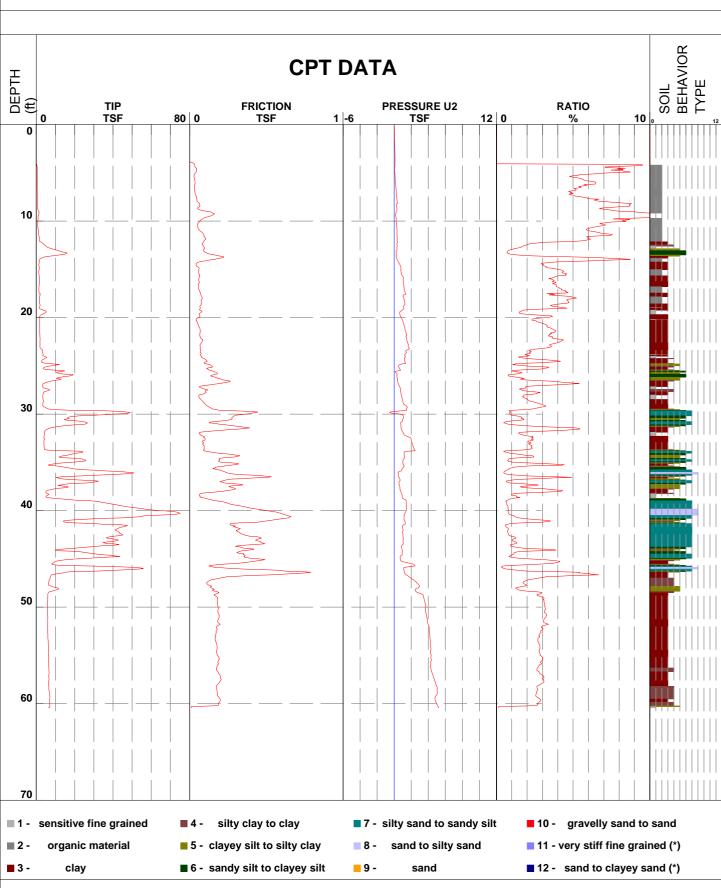
Fugro Consultants, Inc.

Cone Number A15F2.5CKE2H2403

Elevation

-3.5'

Coordinate:N 29 37 06.9 W 90 01 46.7





Job Number 04.5508-4005

CPT Number CPT-27

Location Baton Rouge-LA

Operator

Herbert Jackson

Date and Tin 12-Sep-2011 15:03:18

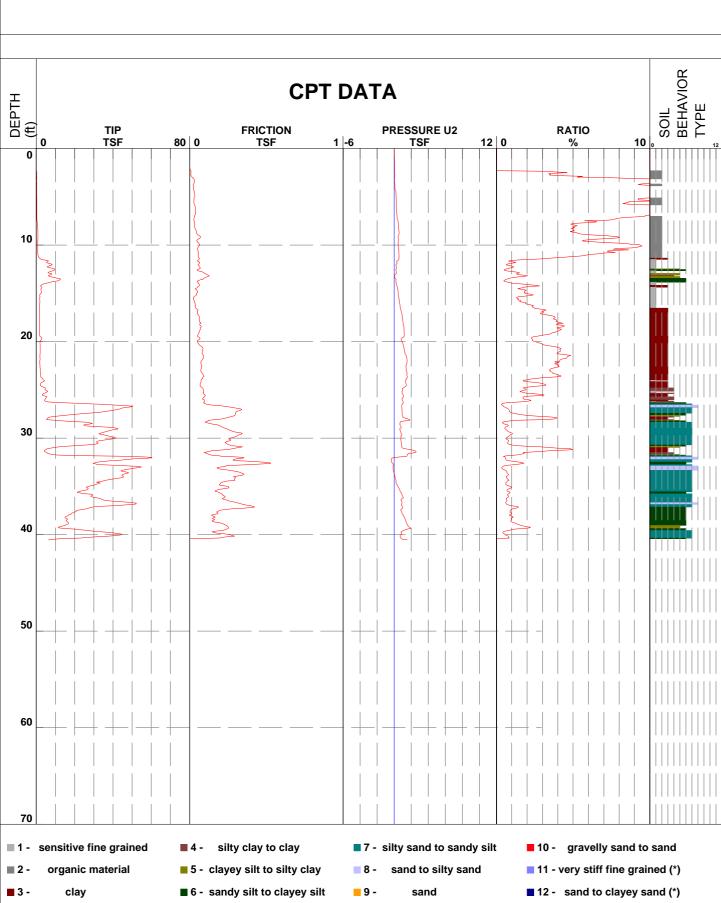
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc.

Elevation -1.7'

Coordinate:N 29 37 05.4 W 90 02 14.5





Job Number 04.5508-4005

CPT Number CPT-28

Operator

David Cline

Date and Tin 17-Aug-2011 10:27:31

Client

Fugro Consultants, Inc.

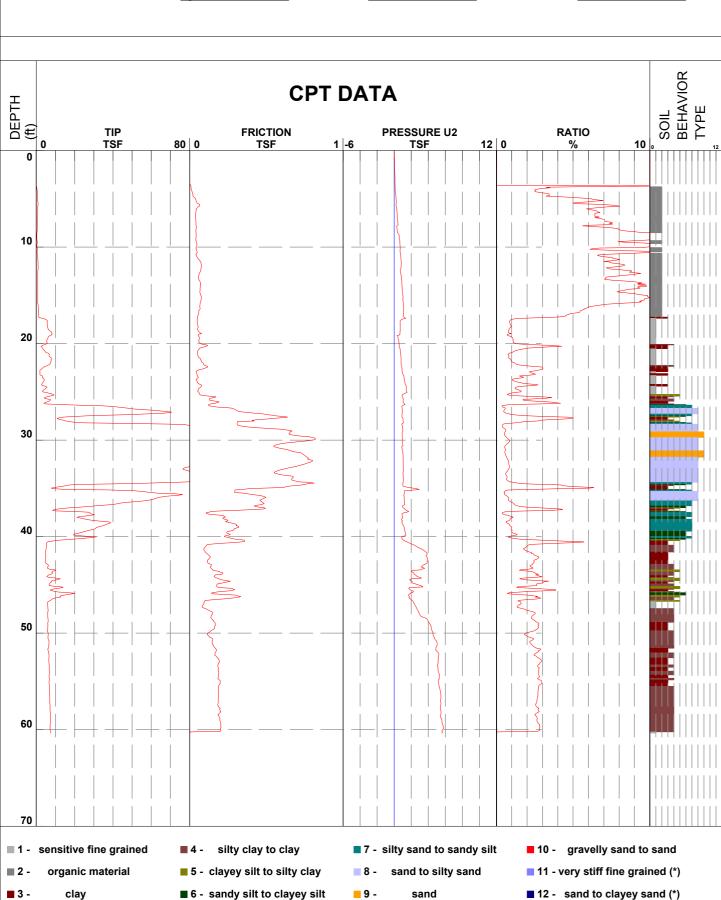
Elevation

2.9'

Location Baton Rouge-LA

Cara Nambar A4550 50K5010402

Cone Number <u>A15F2.5CKE2H2403</u> CoordinatesN 29 37 04.9 W 90 02 32.1





Job Number 04.5508-4005

CPT Number CPT-29

Location Baton Rouge-LA

Operator

Herbert Jackson

Date and Tin 12-Sep-2011 13:02:30

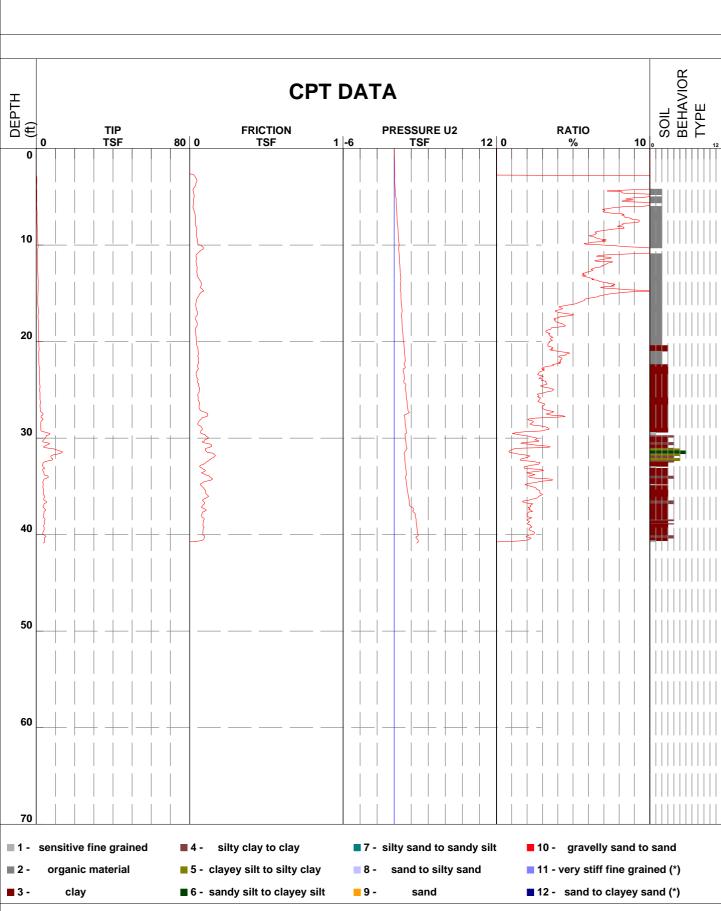
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc.

Elevation -1.8'

Coordinate N 29 36 50.3 W 90 02 49.0





Job Number 04.5508-4005

CPT Number CPT-30

Location Baton Rouge-LA

Operator

David Cline

Date and Tin 18-Aug-2011 11:47:12

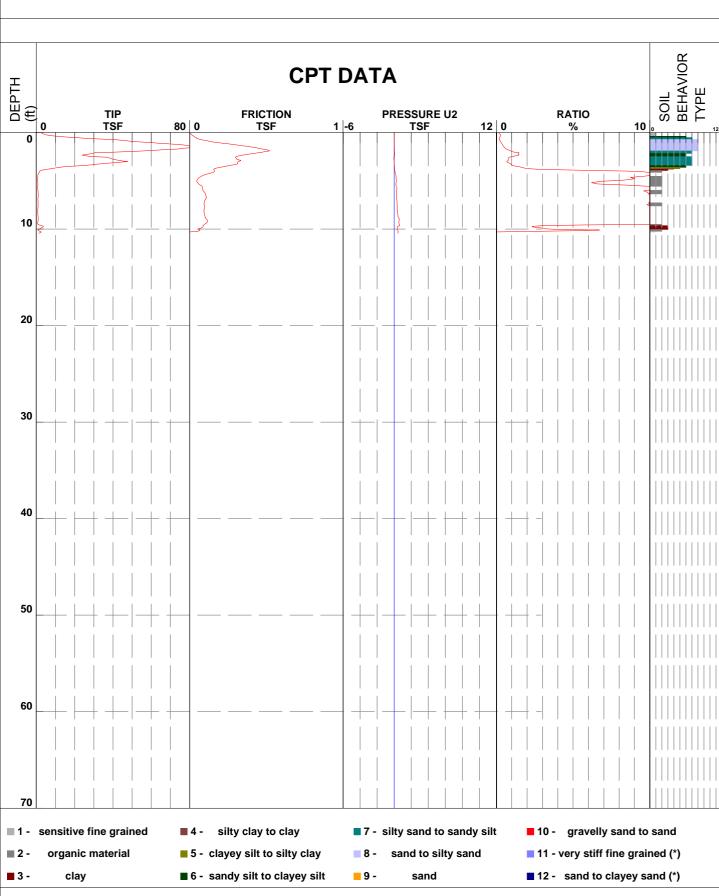
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc. Elevation

1.40'

Coordinate:N 29 39 25.1 W 90 00 42.3





Job Number 04.5508-4005

CPT Number CPT-32

Location Baton Rouge-LA

Operator

Herbert Jackson

Date and Tin 14-Sep-2011 10:00:13

Cone Number A15F2.5CKE2H2403

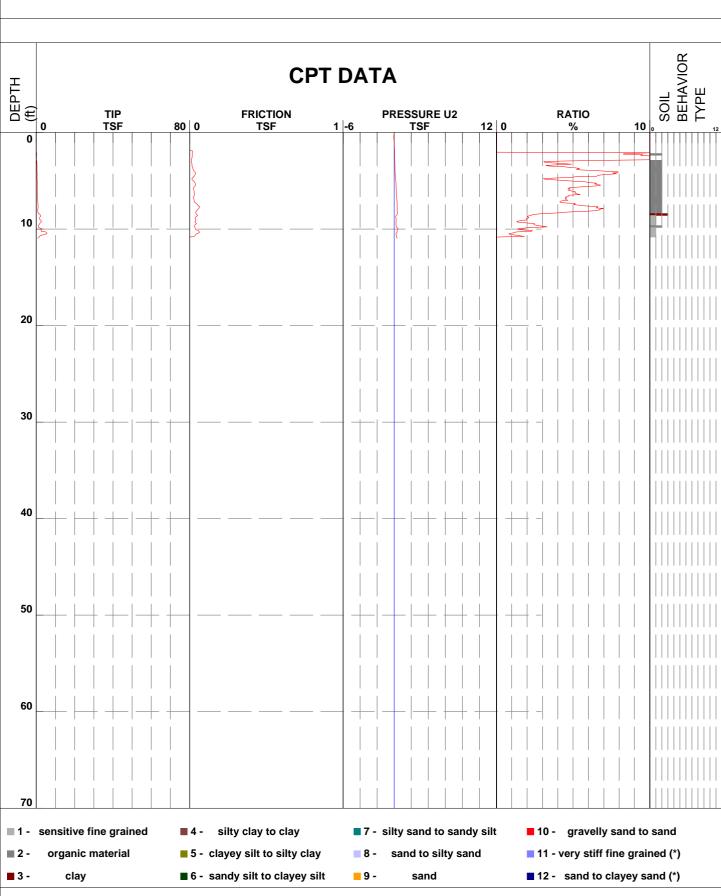
Client

Fugro Consultants, Inc.

Elevation

0.6'

CoordinatesN29 39 15.4 W 90 00 49.2





Job Number 04.5508-4005

CPT Number CPT-34

Location Baton Rouge-LA

Operator

David Cline

Date and Tin 25-Aug-2011 10:14:22

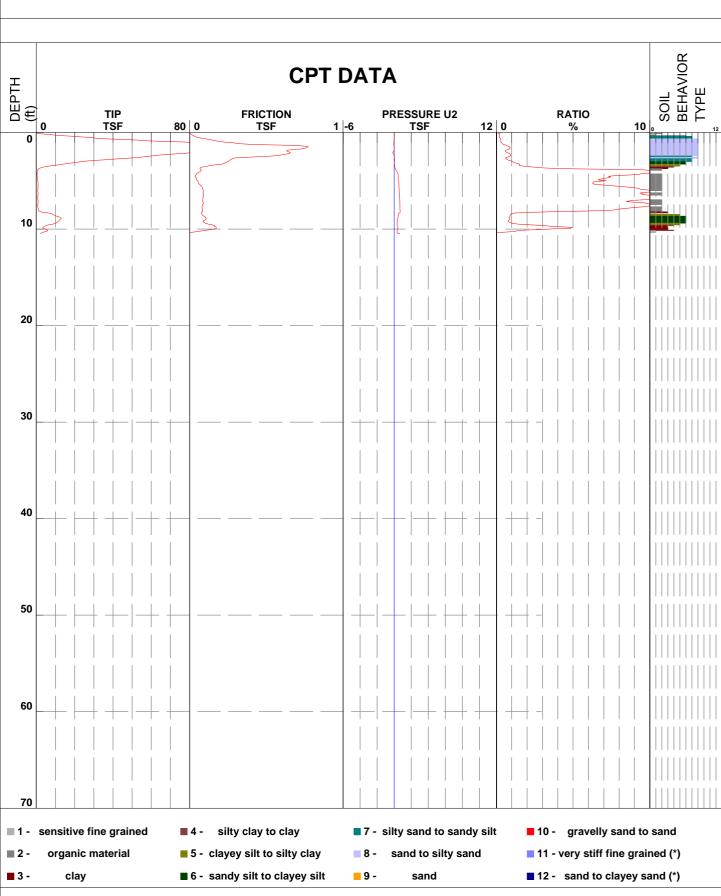
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc.

Elevation 1.4'

CoordinatesN 29 39 081 W 90 01 06.7





Job Number 04.5508-4005

CPT Number_ CPT-35A Location **Baton Rouge-LA**

Operator

David Cline

Date and Tin 25-Aug-2011 11:31:38

Cone Number A15F2.5CKE2H2403

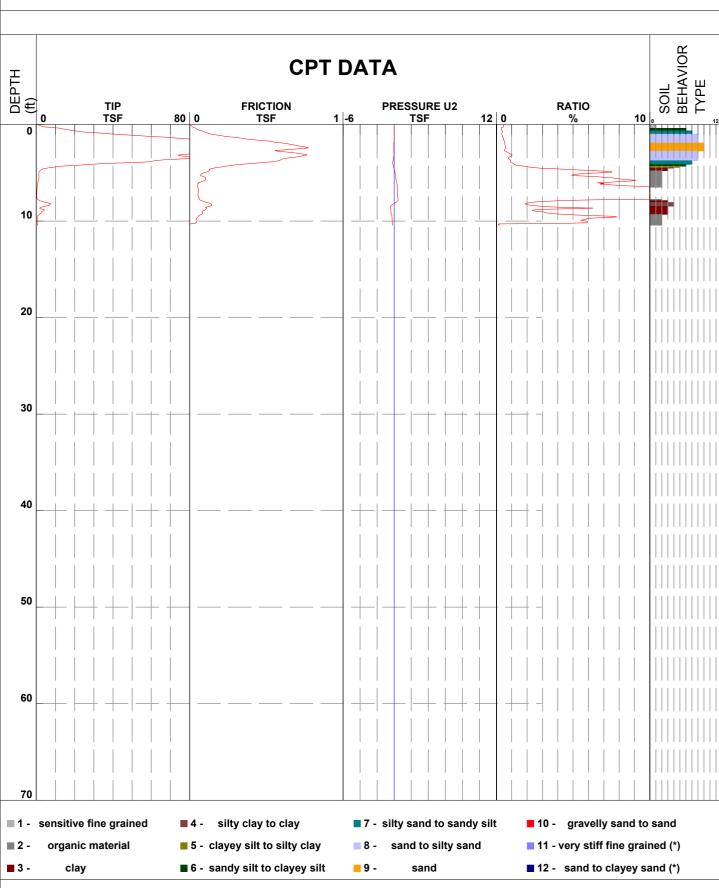
Client

Fugro Consultants, Inc.

Elevation

1.4'

Coordinate:N 29 38 53.1 W 90 00 48.0





Job Number 04.5508-4005

CPT Number CPT-36 Location **Baton Rouge-LA**

Operator

David Cline

Date and Tin 25-Aug-2011 08:51:51

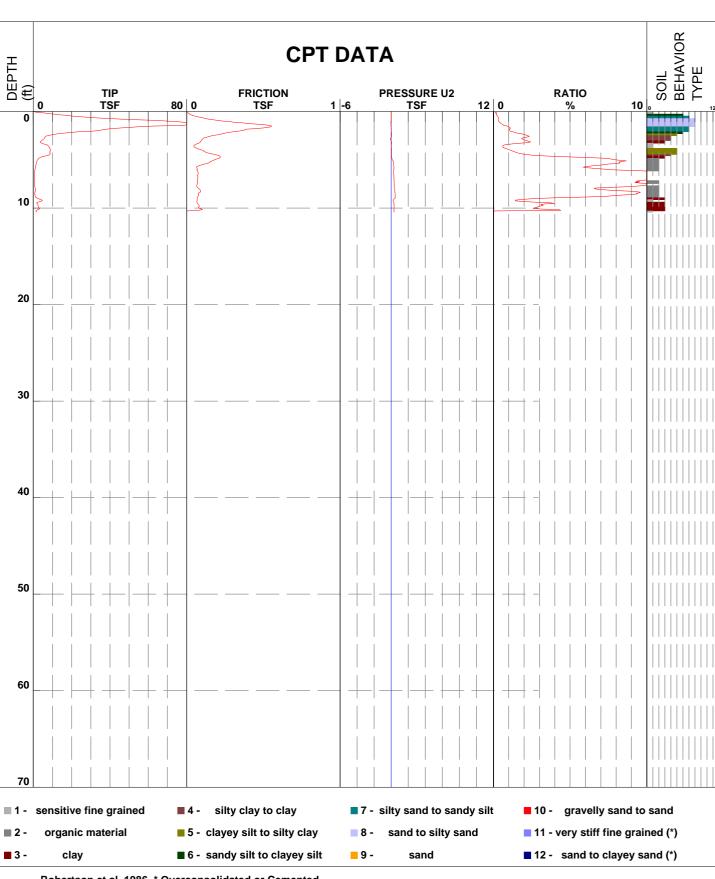
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc.

Coordinate:N 29 39 05.0 W 90 01 22.5







Job Number 04.5508-4005

CPT Number CPT-37

Operator David Cline

Date and Tin 25-Aug-2011 12:24:30

Client

Fugro Consultants, Inc.

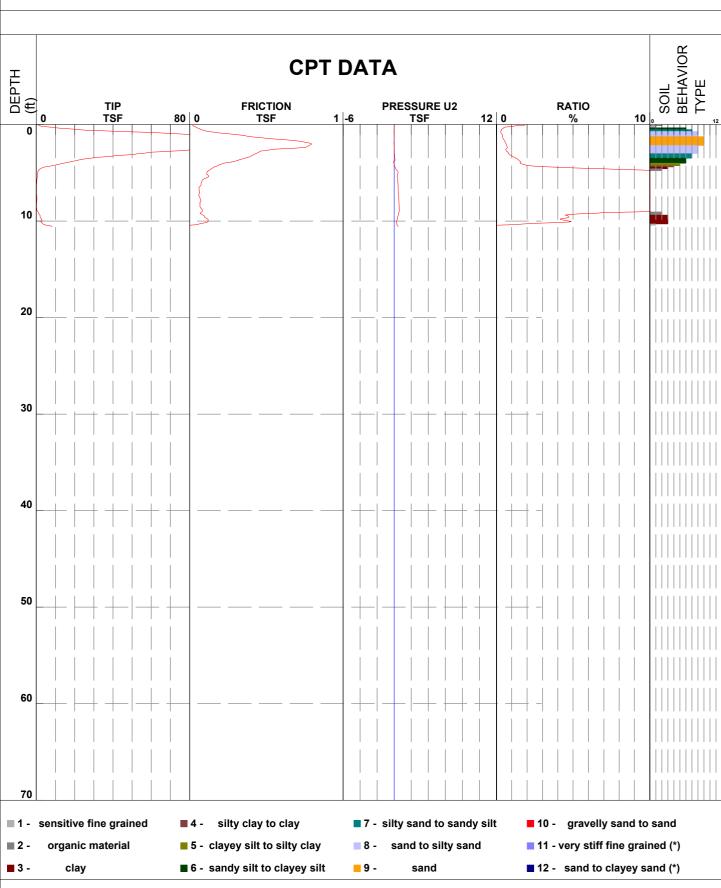
Elevation

1.0'

Location Baton Rouge-LA

Cone Number A15F2.5CKE2H2403

CoordinatesN 29 38 516 W 90 01 10.8





Job Number 04.5508-4005

CPT Number CPT-39

Location Baton Rouge-LA

Operator

Herbert Jackson

Date and Tin 13-Sep-2011 14:28:20

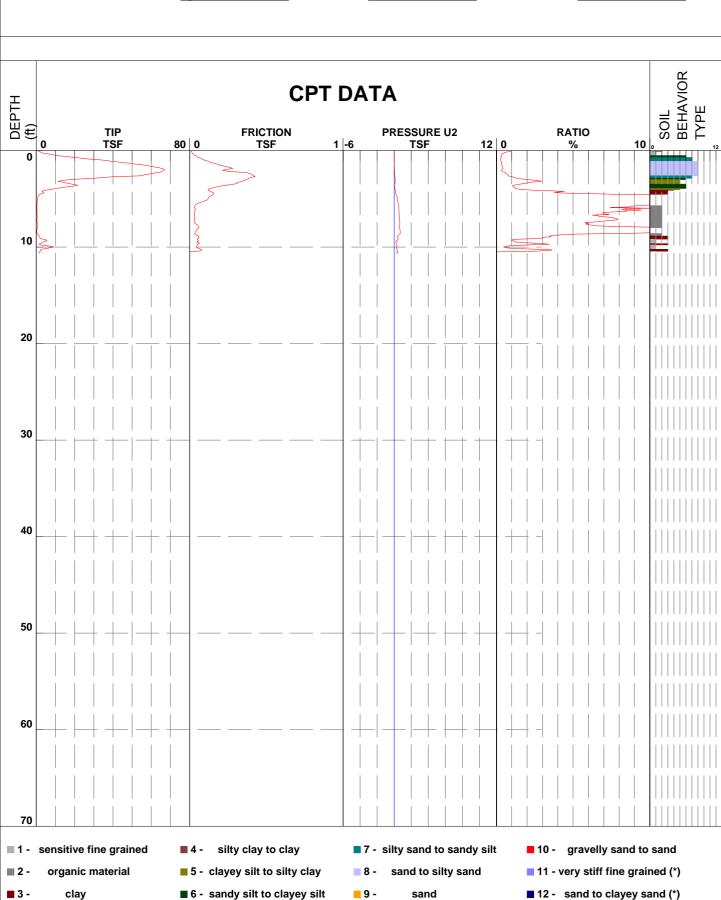
Cone Number A15F2.5CKE2H2403

Client

Fugro Consultants, Inc.

Elevation 0.6'

Coordinate:N 29 38 50.0 W 90 01 55.2

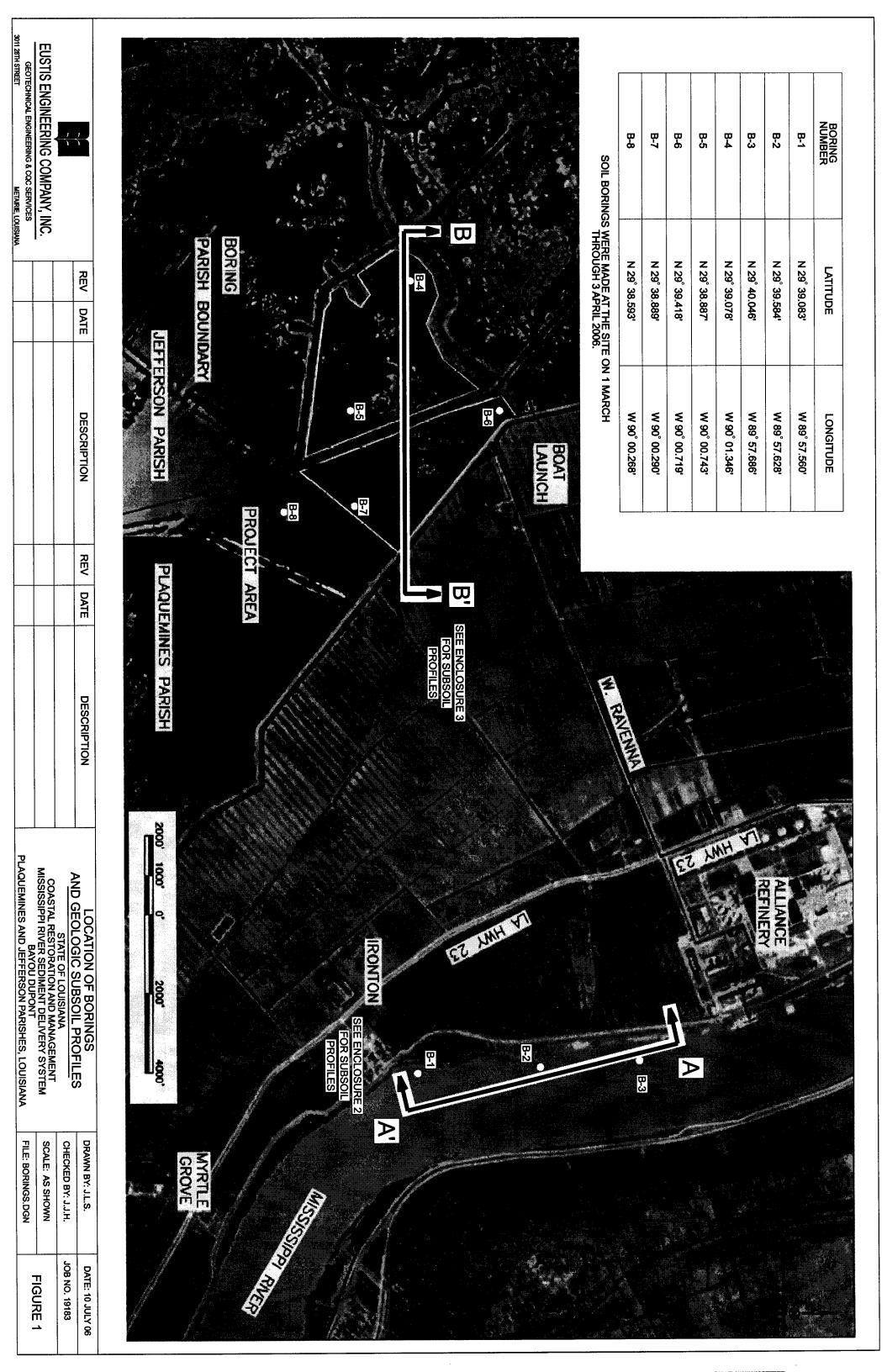




APPENDIX D SUBSURFACE INFORMATION OBTAINED BY OTHERS



APPENDIX I LOGS OF SOIL BORINGS AND LABORATORY TEST RESULTS





PP	Pocket penetrometer: Resistance in tons per square foot														
SPT	Standard Penetration Test: Number of blows of a 140-lb hammer dropped 30 inches required to drive 2-in. O.D., 1.4-in. I.D. sampler a distance of 1 foot into the soil after first seating it 6 inches														
SPLR	Туре	of Sampling	Shelby	SPT	Auger	No sample									
SYMBOL	Clay	Silt IIII IIIII Iinant type shown hea	Sand Output Sand Output Sand Sa	Peat/Hum	nus Shells	Stone/Gravel									
USC	Unified	Soil Classification													
DENSITY	Unit we	eight in pounds per cul	bic foot												
SHEAR TES															
Ø	Angle of internal friction in degrees														
С	Cohe	esion in pounds per sq	uare foot												
ATTERBER LL PL PI	Liqui Plast	S d Limit tic Limit ticity Index													
OTHER TE	STS														
CON		solidation													
PD	Particle size distribution (sieve and/or hydrometer)														
k		ficient of permeability	•												
SP	Swel	ling pressure in pound	is per square foot												

GENERAL NOTES

Other laboratory test results reported on separate figures

- (1) If a ground water depth is shown on the boring log, these observations were made at the time of drilling and were measured below the existing ground surface. These observations are shown on the boring logs. However, ground water levels may vary due to seasonal fluctuations and other factors. If important to construction, the depth to ground water should be determined by those persons responsible for construction immediately prior to beginning work.
- (2) While the individual logs of borings are considered to be representative of subsurface conditions at their respective locations on the dates shown, it is not warranted that they are representative of subsurface conditions at other locations and times.

EUSTIS ENGINEERING COMPANY, INC.

LOG OF BORING AND TEST RESULTS
STATE OF LOUISIANA
COASTAL RESTORATION AND MANAGEMENT
MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM
BAYOU DUPONT, LOUISIANA

Job No.: 19183

(Sheet 1 of 1)

Refer to "Legends & Notes"	Other	Tests					9			C					PD											
Refer to "L																										
	imits	Ы					42				48				43				42							
-	Atterberg Limits	చ					23				54				27				77							
Boring:	Atte	Ⅎ					65				72				20				25					-		
å	sts	၁					114				75				139				503							
	Shear Tests	8				ŀ	1				0				ı				t							
90	ফ	Туре				98	2				80				2				2							
Date Drilled: 3/01/06	Density	Wet				122	104				109				111				102							
e Drille	Der	Dry				86	29				42				77				99							
	Water	Percent		33		25	56				47				43				55							
19183	Depth	In Feet	0-1.5	2-3.5	မှာ	7-9 7-8	11-12	13-14	15-16	:	19-20		23-24	25-26	27-28	29-30	31-32	32-34	35-36	37-38	39-40					
Job No.:	Sample	Number	1	7	ю •	4 rc	9	7	ထတ)	25		12	13	4	15	16	17	18	19	20					
	2	22	ML		M		ਲ	SM		팡		Æ		동		용	·	Ä	공	-						
NAVD 88 Gr. Water Depth: N/A	Vieual Classification	Visual Classification	Loose gray clayey silt		Loose gray sandy silt		Very soft gray clay	Loose to medium dense gray silty sand	w/clay layers	Very soft gray clay w/silty sand lenses & layers		Loose brown & gray sandy silt w/clay		Very soft to soft brown & gray clay w/silt	lenses & pockets			Medium compact gray sandy silt	Soft brown & gray clay w/silt lenses & pockets							
Datum:	Cympol			<u>;;;</u>																						
Dati	ωL	그모	Ż	X			-111	Λ÷	•••••					111												=
-18.3	CDT	- 5	_	တ		····•																				
Ground Elev.:	8				, ,		***************************************				0.25			0.25	0.25	0.25	0.25		0.50	0.25	0.25					
Groun	Scale	Feet	0	<u>'</u>	1 ('	P '	•	1		- R		r	'	,	 တို		'	' '	,			•	1	1	20

Comments: Estimated water surface at el 2.7. N 29° 39.083'; W 89° 57.560'

LOG OF BORING AND TEST RESULTS
STATE OF LOUISIANA
COASTAL RESTORATION AND MANAGEMENT
MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM
BAYOU DUPONT, LOUISIANA

(Sheet 1 of 1)

k Notes"	Other	Tests									DQ				, , , , , , , , , , , , , , , , , , , 		6												
Refer to "Legends & Notes"																					*****							-	
Refer	ts	۵	34	23			36)																					┪
	Atterberg Limits	PL	16	17			22	}																					
: 5	Atterb	ιΓ	20	40			28)																					
Boring:	sts	၁		75			9							200						1107									1
	Shear Tests	Type ø		uc			S C							nc I						OB 0									
و					.,																		-						_
3/01/0	Density	y Wet		5 116			70 106							76 109						101 122									
illed:		ıt Dry		82			_	•						_	·														\dashv
Date Drilled: 3/01/06	Water	Percent	30	37			53	3	26	20				43	!					22									
19183 D	Depth	In Feet	0-2	34	5-6	7-8	6-10	2	11-12	13-14	15-16	17-18	19-20	21-22	22-24	25-26	26-28	28-30	30-32	32-34	34-36	36-38	38-40						
Job No.:	Sample	Number	1	2	က	4	ĸ)	9	7	œ	6	9		12	ζ.	4	15	16	17	18	19	50						
	S.	3	ರ		万			Ä	ರ	SM	S S			F.	SM			•				7	5 7			· · · · · ·			
Datum: NAVD 88 Gr. Water Depth: N/A	Visual Classification		Very soft gray silty clay		Very soft gray clay w/silt lenses & pockets			Loose gray clavey silt	Very soft gray silty clay	Loose gray sandy silt	Loose gray silty fine sand w/clay layers			Very soft gray clay w/silt pockets & lenses	Loose gray silty sand w/clay layers							Very soft aray silty clay w/sand layers	Medium stiff gray silty clay w/silt lenses						
ı: NA	S G							MM																					
Datun							27	100		1.						•••													
	, Fan	<u>5</u>																											_
ev.:	0	Ė			0.25	0.25	0.05	3.0															0.50						
Ground Elev.: -33.3	Scale	Feet	0			ſ		6 □	1		-	ı	8	₹	T	T	1	1	၂ ၉		I		1	5	1		1	1	20

Comments: Estimated water surface at el 2.7. N 29° 39.584'; W 89° 57.628'

LOG OF BORING AND TEST RESULTS
STATE OF LOUISIANA
COASTAL RESTORATION AND MANAGEMENT
MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM
BAYOU DUPONT, LOUISIANA

Date Drilled: 3/05/06

Job No.: 19183

Gr. Water Depth: N/A

Ground Elev.: -27.3 Datum: NAVD 88

Boring: 3

(Sheet 1 of 1)

Refer to "Legends & Notes"

Other	Tests							OA.								G.							 *****		
			<u></u>																						
Atterberg Limits	רו או או																				_				
Shear Tests	Type ø C		UC - 28			OB 0 204																			
Density	Dry Wet		74 109			90 117													·						
Water			48 7			9 00 																			
Depth		0-5	2-4	4-6	8-9	8-10	10-12	12-14	14-16	16-18	18-19	19-20.5	22-23		25-26	28-29	31-32		34-35	37-38	39-40				
Sample		1	2	က	4	c.	<u>ه</u>	7	∞	<u>ი</u>	_		12			4	15	!	9	14	<u>~</u>				
-) 	겅			×	<u> </u>	₩S		-		_	S				·		·							
Mercal Classification		Extremely soft to very soft gray silty clay			Very loose to loose gray sandy sift		Loose gray silty sand w/clay					Medium dense gray silty sand					•							-	
Chumbo	oyiiibo																								
S d												×1 ••	2	13	J	25 X	24 ×	<u> </u>	₽ 8 	18	20 				
0	<u> </u>	0.25	0.25	0.25																					
Scale	Feet	0		· ·		,	<u> </u>			'		28	T	Т	1	ľ	e e	ı		Ţ 1	9	ř	 i i	T	50

Comments: Estimated water surface at el 2.7. N 29° 40.046; W 89° 57.686'

LOG OF BORING AND TEST RESULTS STATE OF LOUISIANA

COASTAL RESTORATION AND MANAGEMENT MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM

BAYOU DUPONT, LOUISIANA

Job No.: 19183 Date Drilled: 4/03/06

(Sheet 1 of 1)

Refer to "Legends & Notes"

4

Other Tests 00 00 179 8 / ₫ Atterberg Limits ٦ 25 23 88 109 267 님 32 - 173 125 148 2 28 O Shear Tests 1 Ø ł 0 0 Type 9 8 2 9 9 Wet 102 92 93 74 86 Density ٥ 23 20 20 55 8 Water Content Percent 29 262 92 63 87 Depth In Feet 11-12 13-14 15-16 17-18 24-25 34-35 39-40 19-20 29-30 7.0-8 9-10 1-2 5-6 Sample Number 7 13 4 Ξ 6 9 ω nsc F ╛ 끙 Gr. Water Depth: N/A w/sand pockets & shell fragments Very soft gray clay w/sandy silt lenses & Visual Classification Very soft gray organic clay Loose gray sandy silt Very soft gray clay pockets Datum: NAVD 88 S P Symbol R SPT Ground Elev.: -1.3 0.00 0.50 0.25 0.00 0.25 0.50 0.75 0.50 0.50 0.00 0.00 0.00 0.50 0.00 4 80 各 | 20 6 Scale In Feet

Estimated water surface at el 0.2. N 29° 39.078'; 90° 01.346' Comments:

LOG OF BORING AND TEST RESULTS STATE OF LOUISIANA

COASTAL RESTORATION AND MANAGEMENT MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM BAYOU DUPONT, LOUISIANA

Job No.: 19183 Date Drilled: 3/30/06

Gr. Water Depth: N/A

Datum: NAVD 88

Ground Elev.: -1.8

Ŋ

Boring:

(Sheet 1 of 2)

Refer to "Legends & Notes"

Other Tests 0 0 0 103 427 ₫ 27 o Atterberg Limits 245 귑 26 47 7 672 30 Ⅎ 48 35 53.2 160 392 0 1658 180 355 65 ပ Shear Tests 0 ł ŀ 0 Ø 0 1 Type 2 2 OB 9 80 OB 8 101 122 Wet 117 8 66 99 96 Density Dry 25 ဗွ 8 6 29 88 Water Content Percent 8 63 664 8 24 82 7 Depth In Feet 11-12 15-16 17-18 24-25 29-30 34-35 39-40 44-45 49-50 13-14 19-20 9-10 2-6 7-8 34 Sample Number 5 9 5 5 4 9 Ξ nsc 동 끙 H 물 ద Ξ Loose to medium compact gray clayey silt w/ clay layers Very soft gray clay w/silt lenses & pockets Medium compact gray sandy silt w/clay layers Visual Classification w/sandy silt lenses & layers Soft gray clay w/sand lenses Very soft black humus Very soft gray clay S P Symbol R SPT 0.75 0.50 0.00 0.25 0.00 0.25 0.25 0.75 0.00 0.25 0.25 0.25 0.25 0.00 ద 8 | | 各 | ا 8 두 Scale In Feet

Estimated water surface at el 0.2. N 29° 38.887°; W 90° 00.743' Comments:

LOG OF BORING AND TEST RESULTS
STATE OF LOUISIANA

COASTAL RESTORATION AND MANAGEMENT MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM BAYOU DUPONT, LOUISIANA

Refer to "Legends & Notes" Boring: 5 Date Drilled: 3/30/06 Job No.: 19183 Gr. Water Depth: N/A

Other Tests Atterberg Limits ā 겁 Ⅎ 395 ပ Shear Tests 0 Туре 2 Wet 102 Density 5 83 Water Content Percent 8 Depth In Feet 59-60 54-55 Sample Number 8 7 OSC 동 동 Visual Classification Medium stiff gray clay Soft gray clay Datum: NAVD 88 S P Symbol R SPT Ground Elev.: -1.8 0.50 0.75 윱 8 8 5 8 Scale In Feet 100 20

Comments: Estimated water surface at el 0.2. N 29° 38.887; W 90° 00.743'

(Sheet 2 of 2)

LOG OF BORING AND TEST RESULTS
STATE OF LOUISIANA
COASTAL RESTORATION AND MANAGEMENT
MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM
BAYOU DUPONT, LOUISIANA
Job No.: 19183 Date Drilled: 4/03/06

Gr. Water Depth: N/A

Datum: NAVD 88

Ground Elev.: -0.3

Boring: 6

(Sheet 1 of 1)

Refer to "Legends & Notes"

i	Other Tests		CON																			
nits	<u>a</u>		61		58				40													
Atterberg Limits	P.		27		23				28													
Atte	Н		88		8				89													
	C		- 145		- 215		0 552		0 150						- 233							
Shear Tests	Type		2		2		OB		OB						S							
<u>_</u>	 t		100		100		115	•	102						100							
Density	λo	_	61		62		83		65						61							
Water	Content		63		63		38		257						64							
1	Depth In Feet	1-2	3.4	9-9	2-8	9-10	11-12	13-14	15-16	17-18	19-20		24-25		29-30	34-35		39-40				
-10	Sample Number	-	7	က	4	2	9	7	80	6	10		=		12	13		41				
	OSO	£	공				¥		<u>გ</u>													
	Visual Classification	Very soft dark brown humus	Very soft gray clay w/silt pockets				Medium compact gray clayey silt w/clay lenses		Very soft gray clay w/silt lenses & layers				w/sandy silt pockets									
	L Symbol R																					
	SPT L																					
	<u>G</u>	0.00	0.75	1.00	0.75	0.50	1.25	1.25	0.50	0.50	0.75		0:20		1.00	0.75		0.75				
Scale	Feet	0	ı	Ī	Ī	9	?	ī	T	Ť	7 8	· 1	<u> </u>	T T	90		1 1	04	1	1	i	- 20

Comments: Estimated water surface at el 0.2. N 29° 39.418; W 90° 00.719'

LOG OF BORING AND TEST RESULTS STATE OF LOUISIANA

COASTAL RESTORATION AND MANAGEMENT MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM

BAYOU DUPONT, LOUISIANA

Gr. Water Depth: N/A

Datum: NAVD 88

Ground Elev.: -2.7

Job No.: 19183 Date Drilled: 4/03/06

Boring:

(Sheet 1 of 1)

Refer to "Legends & Notes"

Other Tests 8 55 22 ₫ 2 Atterberg Limits చ 25 22 સ Ⅎ 8 7 36 616 9 86 ပ 4 95 Shear Tests ł Ø 0 0 0 Type 8 2 2 8 9 Wet 120 96 66 8 97 Density 5 32 83 8 57 ω Water Content Percent 29 700 74 69 8 34-35 39-40 Depth In Feet 11-12 13-14 15-16 17-18 19-20 24-25 29-30 9-10 5-6 7-8 34 Sample Number 4 3 4 Ξ O nsc 끙 끙 물 ₽ Very soft gray clay w/sand lenses & pockets w/sand lenses & pockets Medium compact gray clayey silt Visual Classification w/sand pockets Very soft black humus Medium stiff gray clay S P Symbol R SPT 0.75 1.0 0.25 0.50 0.00 0.00 0.50 0.00 0.50 0.00 0.00 1.50 0.75 0.50 占 8 지 있 40 Scale In Feet

Estimated water surface at el 0.2. N 29° 38.889°; W 90° 00.290' Comments:

LOG OF BORING AND TEST RESULTS STATE OF LOUISIANA

COASTAL RESTORATION AND MANAGEMENT MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM BAYOU DUPONT, LOUISIANA Gr. Water Depth: N/A

Datum: NAVD 88

Ground Elev.: -1.8

Job No.: 19183 Date Drilled: 3/31/06

Boring:

(Sheet 1 of 1)

Refer to "Legends & Notes"

Other Tests 800 157 ₫ Atterberg Limits 29 చ 224 ᆸ 155 130 221 ပ 5 22 Shear Tests 0 ١ ŀ Ø 0 Type В 9 2 2 2 115 Wet 9 93 65 92 Density 5 9 22 83 22 8 Water Content Percent 208 528 38 57 8 Depth In Feet 39-40 11-12 13-14 15-16 17-18 24-25 29-30 34-35 9-10 5-6 7-8 34 Sample Number 42 5 4 Ξ 9 OSC 핑 ₹ 챕 ద Very soft dark gray humus w/roots and clay layers w/sand lenses & pockets Visual Classification Very loose gray clayey silt Very soft black humus Very soft gray clay S P Symbol R SPT 0.25 0.50 0.50 0.00 0.00 0.00 0.00 0.50 0.00 0.00 0.00 0.00 0.00 0.00 В 8 40 30 5 Scale In Feet

Comments: Estimated water surface at el 0.2. N 29° 38.593°; W 90° 00.268°

LOG OF BORING AND TEST RESULTS
STATE OF LOUISIANA
COASTAL RESTORATION AND MANAGEMENT
MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM
BAYOU DUPONT, LOUISIANA

(Sheet 1 of 1)

Refer to "Legends & Notes"	Other	Tests							G				G.			PD										
Refer to "I																										
	imits	颪					42				48				43				42							
-	Atterberg Limits	귑					23				24				27				22							
Boring:	Atte	ㅂ					65				72				2				64							
ğ	ests	၁					114				75				139				503							
	Shear Tests	Ø				ŀ	1				0				ı				t							İ
90/	S	Туре				08	2				80				ဌ				2							
Date Drilled: 3/01/06	Density	Wet				122	104				109				111				102							
e Drille		Dry				86	29				42				4				99							
	Water	Percent		33		25	99				47				43				55				·			
19183	Depth	In Feet	0-1.5	2-3.5	မှ	6-7 7-8	11-12	13-14	15-16 16-17	:	19-20		23-24	25-26	27-28	29-30	31-32	32-34	35-36	37-38	39-40					
Job No.:	Sample	Number	-	7	က	4 ro	ဖ	2	စတ	•	25		12	13	4	15	16	17	9	19	20	•				
	J	22	ML		¥		공	SM		ᆼ		¥		ᆼ		귱		ML	ਲ							
NAVD 88 Gr. Water Depth: N/A	Vieual Classification		Loose gray clayey silt		Loose gray sandy silt		Very soft gray clay	Loose to medium dense gray silty sand	Wiciay layers	Very soft gray clay w/silty sand lenses & layers		Loose brown & gray sandy silt w/clay		Very soft to soft brown & gray clay w/silt	lenses & pockets			Medium compact gray sandy silt	Soft brown & gray clay w/silt lenses & pockets							
Datum:	Cumbol	ymoo																								
1	S	, R	Ż	X				V.	••••					al)			"								-	
-18.3	Tas	5	-	2			······																			
Ground Elev.:	9	_			,			ī	,		0.25			0.25	0.25	0.25	0.25		0.50	0.25	0.25		-	Ţ		
Groun	Scale	Feet	0	· 			10 1	,	1		- S - C	•	r	'	,	30		'		,	<u> </u>		•	'	•	50

Comments: Estimated water surface at el 2.7. N 29° 39.083'; W 89° 57.560'

LOG OF BORING AND TEST RESULTS
STATE OF LOUISIANA
COASTAL RESTORATION AND MANAGEMENT
MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM
BAYOU DUPONT, LOUISIANA

(Sheet 1 of 1)

k Notes"	Other	Tests									DQ				, , , , , , , , , , , , , , , , , , , 		6												
Refer to "Legends & Notes"																					*****							-	
Refer	ts	۵	34	23			36)																					┪
	Atterberg Limits	PL	16	17			22	}																					
: 5	Atterb	ιΓ	20	40			28)																					
Boring:	sts	၁		75			9							200						1107									1
	Shear Tests	Type ø		uc			S C							nc I						OB 0									
و					.,																		-						_
3/01/0	Density	y Wet		5 116			70 106							76 109						101 122									
illed:		ıt Dry		82			_	•						_	·														\dashv
Date Drilled: 3/01/06	Water	Percent	30	37			53	3	26	20				43	!					22									
19183 D	Depth	In Feet	0-2	34	5-6	7-8	6-10	2	11-12	13-14	15-16	17-18	19-20	21-22	22-24	25-26	26-28	28-30	30-32	32-34	34-36	36-38	38-40						
Job No.:	Sample	Number	1	2	က	4	ĸ)	9	7	œ	6	9		12	ζ.	4	15	16	17	18	19	50						
	S.	3	ರ		万			Ä	ರ	SM	S S			F.	SM			•				7	5 7			· · · · · ·			
Datum: NAVD 88 Gr. Water Depth: N/A	Visual Classification		Very soft gray silty clay		Very soft gray clay w/silt lenses & pockets			Loose gray clavey silt	Very soft gray silty clay	Loose gray sandy silt	Loose gray silty fine sand w/clay layers			Very soft gray clay w/silt pockets & lenses	Loose gray silty sand w/clay layers							Very soft aray silty clay w/sand layers	Medium stiff gray silty clay w/silt lenses						
ı: NA	S G							MM																					
Datun							27	100		1.						•••													
	, Fan	<u>5</u>																											_
ev.:	0	Ė			0.25	0.25	0.05	3.0															0.50						
Ground Elev.: -33.3	Scale	Feet	0			ſ		6 □	1		-	ı	8	₹	T	T	1	1	၂ ၉		I		1	5	1		1	1	20

Comments: Estimated water surface at el 2.7. N 29° 39.584'; W 89° 57.628'

LOG OF BORING AND TEST RESULTS
STATE OF LOUISIANA
COASTAL RESTORATION AND MANAGEMENT
MISSISSIPPI RIVER SEDIMENT DELIVERY SYSTEM
BAYOU DUPONT, LOUISIANA

Date Drilled: 3/05/06

Job No.: 19183

Gr. Water Depth: N/A

Ground Elev.: -27.3 Datum: NAVD 88

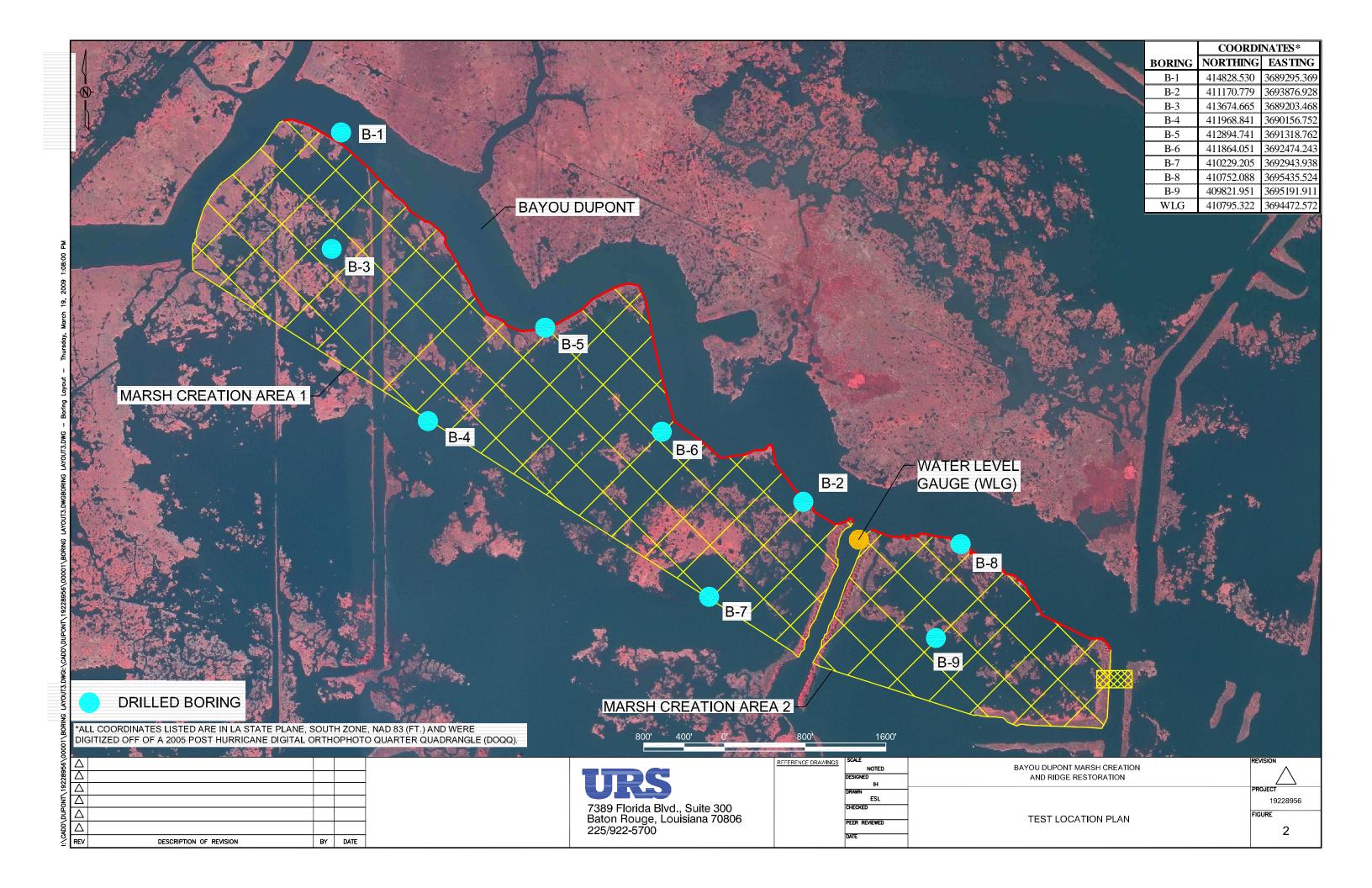
Boring: 3

(Sheet 1 of 1)

Refer to "Legends & Notes"

Other	Tests							OA.								G.							*****		
			<u></u>																						
Atterberg Limits	רו או או																				_				
Shear Tests	Type ø C		UC - 28			OB 0 204																			
Density	Dry Wet		74 109			90 117													·						
Water			48 7			9 00 																			
Depth		0-5	2-4	4-6	8-9	8-10	10-12	12-14	14-16	16-18	18-19	19-20.5	22-23		25-26	28-29	31-32		34-35	37-38	39-40				
Sample		1	2	က	4	c.	<u>ه</u>	7	∞	<u>ი</u>	_		12			4	15	!	9	14	<u>~</u>				
-) 	겅			×	<u> </u>	₩S		-		_	S				·		·							
Mercal Classification		Extremely soft to very soft gray silty clay			Very loose to loose gray sandy sift		Loose gray silty sand w/clay		-			Medium dense gray silty sand					•							-	
Chumbo	oyiiibo																								
S d												×1 ••	2	13	J	25 X	24 ×	<u> </u>	₽ 8 	18	20 				
0	<u> </u>	0.25	0.25	0.25																					
Scale	Feet	0		· ·		,	<u> </u>			'		28	T	Т	1	ľ	e e	ı		Ţ 1	9	ř	 i i	T	50

Comments: Estimated water surface at el 2.7. N 29° 40.046; W 89° 57.686'



Project Number: 19228956.00001

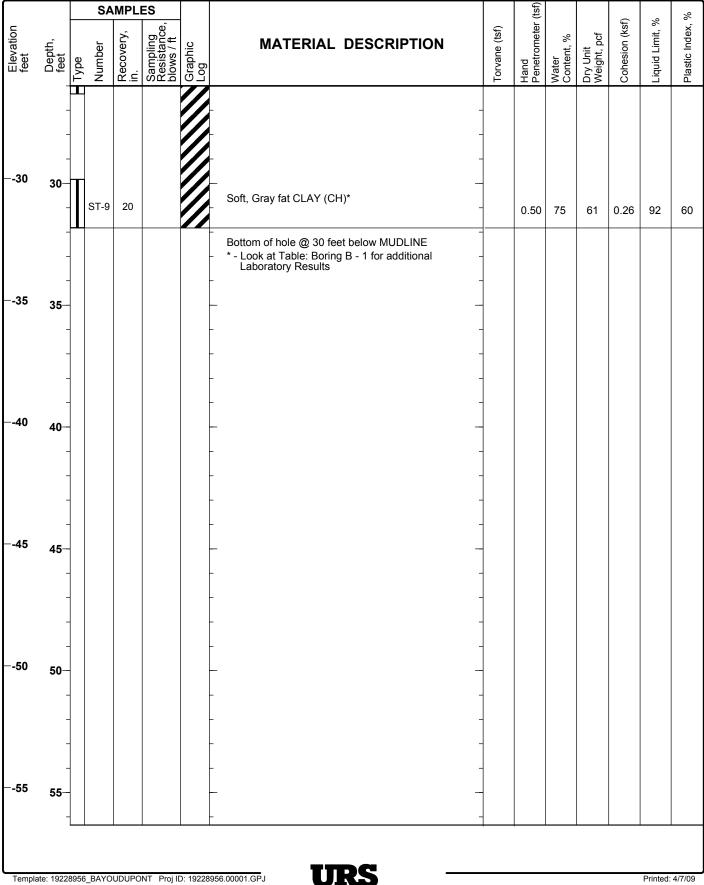
Log of Boring B-1

Date(s) Drilled 2/20/09 - 2/20/09	Logged By	A. Bukkapatnam	Checked By I. Harrouch
Drilling Method Rotary Wash	Drill Bit Size/Type	Bottom Discharge 4(5/8)"	Total Depth Drilled (feet) 31.8
Drill Rig Type Marsh Buggy	Drilling Contractor	SESI	Sampler Piston Sampler/ Shelby Tube
Groundwater Level and Date Measured -0.2' 2/20/2009	Hammer Data	140 LBS Safety	Approximate Surface Elevation -0.2'
Location N414828.534 E3689295.369			Borehole Backfill Cement Grout

			SA	MPL	ES				(tsf)					%
Elevation feet	Depth, feet	Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
							_ WATER MUDLINE EI2.03'							
	-	S	T-1	20			ORGANICS with Clay (OH)			607				
- -5	5-	s	T-2	15			Very Soft, Brown to Black HUMUS with Clay (OH)*		0.10	305	21	0.08	618	395
	-	S	T-3	15			Very Soft, CLAY with Organics (CH - OH)			230	24	0.06	202	150
40	-	s	T-4	22			Very Soft, Gray Lean CLAY (CL)*		0.75	64	72	0.15	46	20
⊢-10	10-	s	T-5	22			Very Soft, Gray SILT with Clay, Organics and trace Fine Sand (CL-ML)*		0.25	54	74	0.17	43	18
−-1 5	- 15	s	T-6	22			Very Soft, Gray CLAY with Silt (CH)		0.25	88	55	0.12		
- -20	20 -	s	Т-7	15			- Very Soft, Gray fat CLAY (CH)* -		0.25	87	47	0.20	85	54
−-25	25-	s	T-8	15			Very Soft, Gray CLAY with trace Organic Pockets (CH)*		0.25	79	56	0.08		

Project Number: 19228956.00001

Log of Boring B-1



Project Number: 19228956.00001

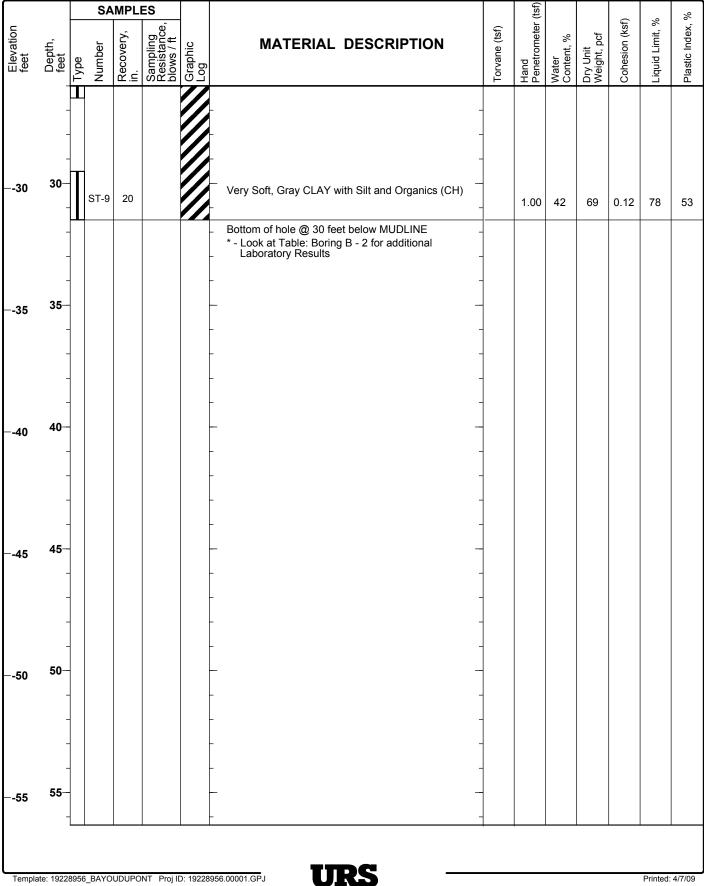
Log of Boring B-2

Date(s) Drilled 2/19/09 - 2/19/09	Logged By	A. Bukkapatnam	Checked By I. Harrouch
Drilling Method Rotary Wash	Drill Bit Size/Type	Bottom Discharge 4(5/8)"	Total Depth Drilled (feet) 31.5
Drill Rig Type Marsh Buggy	Drilling Contractor	SESI	Sampler Piston Sampler/ Shelby Tube
Groundwater Level and Date Measured 0.2' 2/19/2009	Hammer Data	140 LBS Safety	Approximate Surface Elevation 0.2'
Location N411170.779 E3693876.982			Borehole Backfill Cement Grout

			SA	MPLI	ES				(tsf)				_	%
Elevation		Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, 9
-0	0-						WATER							
	-					//	MUDLINE El1.3'							
] s	ST-1	20			ORGANICS with Clay (OH)			915				
		\mathbb{H}					Very Soft, Brown ORGANICS with Clay and Peat							
_	5-	S	ST-2	20			(OH)*		0.25	475	12	0.12	400	254
├5		H					Very Coff Crow and Disals CLAV with Ownering							
			ST-3	20			Very Soft, Gray and Black CLAY with Organics and Silt traces (CH)*		0.25	204	27	0.13		
	-	Ħ					Very Soft, Gray CLAY with Organic pockets (CH)	-						
			ST-4	22			- -		0.25	95	50	0.06	123	90
−-1 0	10-	\prod_{z}		40										
		\coprod	ST-5	18			-	-	0.25	88	52	0.07	97	70
								_						
							-							
−-1 5	15-	T												
			ST-6	18			-	-	0.25	141	36	0.07	144	104
	-						_	-						
							-							
							-							
20	20-		ST-7	20			Very Soft, Gray CLAY with Silt (CH)	-						
		Щ	,,,,	20			_	-	0.50	50	75	0.14	58	36
							-	-						
							-							
	0.E						-							
−-2 5	25-	S	ST-8	16			Very Soft, Gray CLAY with Silt pockets and Organics (CH)*		0.25	98	51	0.11		
Ļ		0050	241/01	IDLIDO	NT D : 11	10000	956.00001.GPJ TIRS						Printed:	

Project Number: 19228956.00001

Log of Boring B-2



Project Number: 19228956.00001

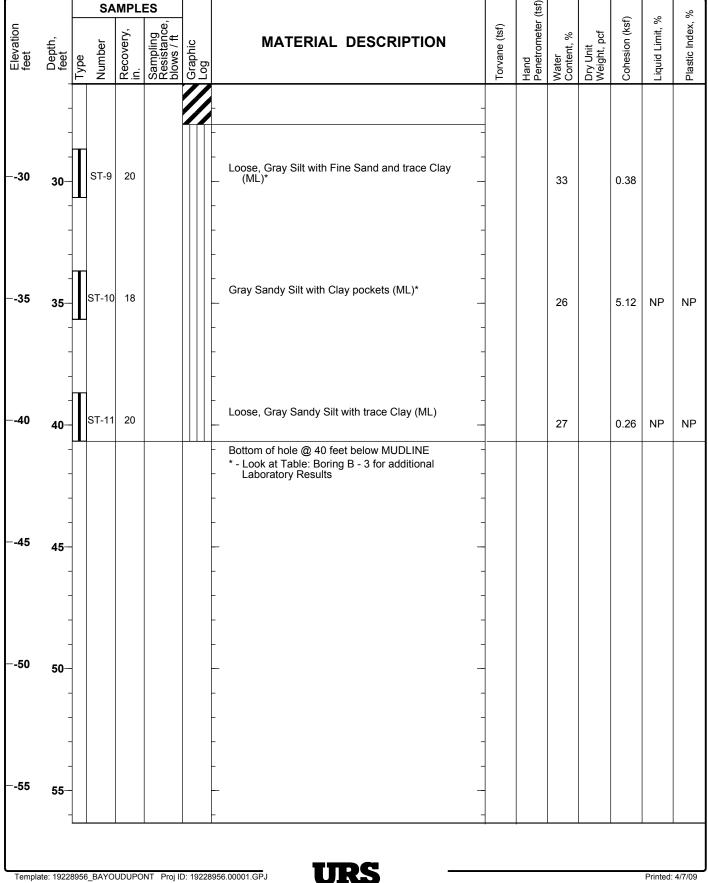
Log of Boring B-3

Date(s) Drilled 2/20/09 - 2/20/09	Logged By	A. Bukkapatnam	Checked By I. Harrouch
Drilling Method Rotary Wash	Drill Bit Size/Type	Bottom Discharge 4(5/8)"	Total Depth Drilled (feet) 40.7
Drill Rig Type Marsh Buggy	Drilling Contractor	SESI	Sampler Type(s) Piston Sampler/ Shelby Tube
Groundwater Level and Date Measured -0.2' 2/20/20	Hammer Data	140 LBS Safety	Approximate Surface Elevation -0.2'
Location N413674.665 E368920	3.468		Borehole Backfill Cement Grout

			SA	MPLI	ES				(tsf)				_	%
Elevation feet	Depth, feet	Туре	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
	0-	\blacksquare				~~~	WATER MUDLINE EI0.87'							
	-	s	ST-1	14		^^^	PEAT (PT)*			1171			996	644
	-	S	ST-2	12			Very Soft, Black PEAT with Clay (PT)*	_	0.25	383		0.12		
−-5	5-	S	ST-3	18			Very Soft, Gray CLAY with Organic pockets (CL)*			171		0.06	141	102
	-	S	ST-4	18			Very Soft, Gray Lean CLAY with trace Organics (CL)*		0.25	43		0.14		
−-10	10-		ST-5	16			Very Soft, Gray Lean Clay (CL - ML)*		0.50	46		0.07	45	15
−-1 5	- - 15-		ST-6	12			Very Soft, Gray CLAY with Silt, Shells and Organics (CH)*		0.50	90		0.08	126	104
- -20	- 20- -		ST-7	18			- Very Soft, Gray Clay becoming Organic Peat and — Clay (CH) – -		0.50	230		0.11		
25	25—		8-T3	18			Very Soft, Gray CLAY with Organics (CH)*	-		100		0.13	108	81

Project Number: 19228956.00001

Log of Boring B-3



Project Number: 19228956.00001

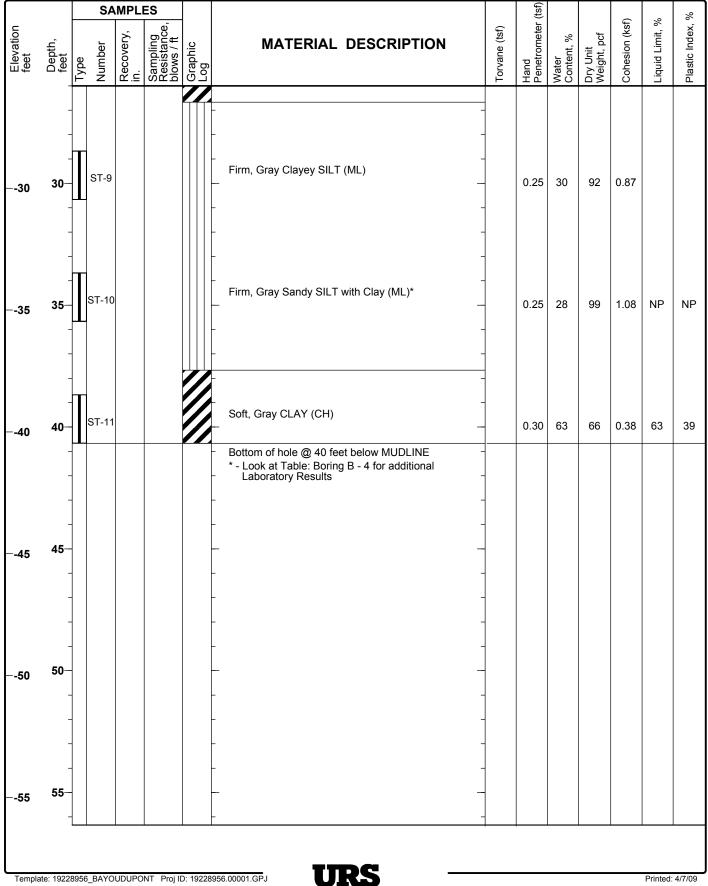
Log of Boring B-4

Date(s) Drilled 2/17/09 - 2/17/09	Logged By	A. Bukkapatnam	Checked By I. Harrouch
Drilling Method Rotary Wash	Drill Bit Size/Type	Bottom Discharge 4(5/8)"	Total Depth Drilled (feet) 40.7
Drill Rig Type Marsh Buggy	Drilling Contractor	SESI	Sampler Piston Sampler/ Shelby Tube
Groundwater Level and Date Measured 0.2' 2/17/2009	Hammer Data	140 LBS Safety	Approximate Surface Elevation 0.2'
Location N411968.841 E3690156.752			Borehole Backfill Cement Grout

	SAMPLES		ES				(tsf)					,	
Elevation feet		Type Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-0	0-					WATER							
	-	ST-1			****	MUDLINE EI0.47' PEAT with Clay *			860			958	427
	-	ST-2				 Very Soft, Dark Gray CLAY with Organic pockets - (OH)* - 			333	17	0.11	482	386
- -5	5-	ST-3				Very Soft, Gray CLAY with Organic pockets (CH)			80	56	0.07	122	83
	-	ST-4				 Very Soft, Gray CLAY with Organic pockets and trace Shells (CH)* 			72	49	0.06	64	41
10	10-	ST-5				Very Soft CLAY with Silt, Organic pockets and Shells (CH)*			90	50	0.07		
15	15— -	ST-6				- Very Soft, Gray CLAY with Organic and Silty Clay — (CH)* –			114	45	0.10	91	58
20	20- -	ST-7				Very Soft, Gray CLAY with Silt and Organic pockets (CH)* -			91	50	0.09		
- -25	25—	ST-8				- Very Soft, Gray CLAY with Organic pockets, Sandy Silt and Silty Sand layers (CH)*	-	0.25	97	57	0.10	101	62

Project Number: 19228956.00001

Log of Boring B-4



Project Number: 19228956.00001

Log of Boring B-5

Date(s) Drilled 2/16/09 - 2/17/09	Logged By	A. Bukkapatnam	Checked By I. Harrouch
Drilling Method Rotary Wash	Drill Bit Size/Type	Bottom Discharge 4(5/8)"	Total Depth Drilled (feet) 60.4
Drill Rig Type Marsh Buggy	Drilling Contractor	SESI	Sampler Piston Sampler/ Shelby Tube
Groundwater Level and Date Measured 0.2' 2/17/2009	Hammer Data	140 LBS Safety	Approximate Surface Elevation 0.2'
Location N412894.741 E3691318.762			Borehole Backfill Cement Grout

			SA	MPL	ES				(tsf)					%
. Elevation feet	Depth, feet	Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, ⁹
-0	-		ST-1	17			WATER MUDLINE EI0.22' Very Soft PEAT (PT)	-		428	11	0.05		
	-		ST-2	24			PEAT with Clay and Organics (PT-OH)*	-		223			223	165
−-5	5- -		ST-3	13			Very Soft, PEAT with Clay and Organics (PT-OH)*	-		334	17	0.07		
	-		ST-4	23			Very Soft Gray CLAY with Organic pockets (CH)	-		84	55	0.05	68	42
−-10	10-	1	ST-5	22			Very Soft Gray CLAY with Organic pockets and trace Silt pockets (CH)			62	64			
15	- 15— -		ST-6	20			Very Soft, Gray Lean CLAY with Organics and Fine Sand (CH)* -			117	39	0.08	78	42
20	- 20		ST-7	22			Very Soft Gray CLAY with Organic pockets (CH)*			138	40	0.07		
25	- 25—		ST-8	23			Very Soft, Gray SILTY CLAY (CL)* ———————————————————————————————————			168	40	0.09	47	23

Project Number: 19228956.00001

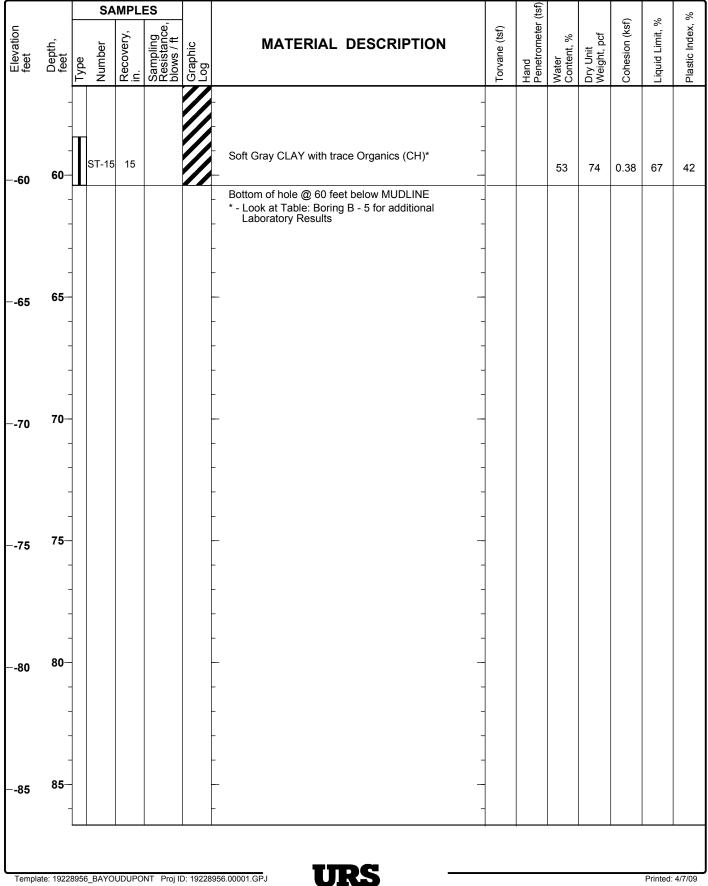
Log of Boring B-5

			SAI	MPLI	ES				(tsf)			_		%
Elevation feet	Depth, feet	Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
30	30-	SI	Г-9	23			- Very Soft, Gray CLAYEY Silt with Clay and Sand (CL-ML)			33	81	0.09	34	6
35	- 35-	ST	-10	17			- Alternating layers of Very Soft, Gray SILTY CLAY with Sand (CL)			47	72			
40	40-	ST	·-11	24			Loose Gray SILT with CLAY layers (ML)*			38	89	0.46	NP	NP
45	- 45	ST	·-12	19			Medium, Gray CLAYEY Silt with Clay (CL-ML)*			32	95	0.60		
50	50—	ST	·-13	18			Very Soft to Soft Gray CLAY (CH)*			68	62	0.24	79	44
55	- 55—	ST	-14	22			Very Soft to Soft, Gray CLAY with Silt pockets and trace Organics (CH)*			56	69	0.22		
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Project Number: 19228956.00001

Log of Boring B-5

Sheet 3 of 3



Project Number: 19228956.00001

Log of Boring B-6

Date(s) Drilled 2/17/09 - 2/17/09	Logged By	A. Bukkapatnam	Checked By I. Harrouch
Drilling Method Rotary Wash	Drill Bit Size/Type	Bottom Discharge 4(5/8)"	Total Depth Drilled (feet) 62.2
Drill Rig Type Marsh Buggy	Drilling Contractor	SESI	Sampler Piston Sampler/ Shelby Type(s) Tube
Groundwater Level and Date Measured 0.2' 2/17/2009	Hammer Data	140 LBS Safety	Approximate Surface Elevation 0.2'
Location N411864.051 E3692474.243			Borehole Backfill Cement Grout

			SA	MPL	ES				(tsf)					%
Elevation feet	Depth, feet	Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, 9
-0							WATER							
	_						MUDLINE EI1.97'							
	-		ST-1	22			- Very Soft, PEAT with Clay (PT)* -			194	23		289	145
- -5	5-		ST-2	23			 Very Soft, Brown Organic CLAY with Peat (PT/OH/CH)* 			374	18	0.08		
	-		ST-3	18			 Very Soft, Gray CLAY with Organic pockets (CH)* 	-		123	43	0.07	120	76
−-10	10-		ST-4	19			 Very Soft, Gray CLAY with Organic pockets (CH) 	-						
	- - -		ST-5	22			 Very Soft, Gray CLAY with Organic pockets (CH)* - 	-		99	52	0.10	67	33
15	- 15 - -		ST-6	22			Very Soft, Gray CLAY with Organic pockets (CH)	-		124	44			
- -20	20— 		ST-7	12			Very Soft, Gray CLAY becoming Gray SANDY - SILT with Clay (CH becoming ML)*	-		104	47	0.10		
— -25	25 —	1	BAYO	UDUPO	NT Proi II	D: 19228	956.00001.GPJ	-					Printed: 8	5/27/09

Project Number: 19228956.00001

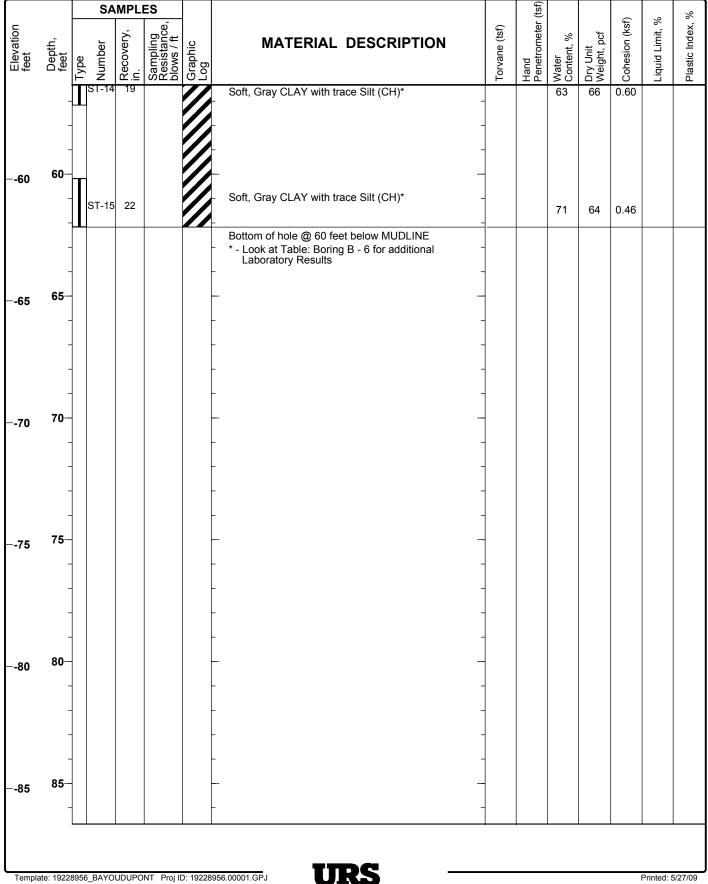
Log of Boring B-6

ST-10 21 ST-10 21 Soft Gray CLAY with Silt (CH)* ST-12 23 Soft Gray CLAY with Silt pockets (CH) ST-13 22 Medium, Gray CLAY with Silt pockets (CH) ST-13 22 Medium, Gray CLAY with Silt pockets (CH) ST-13 22 Medium, Gray CLAY with Silt pockets (CH) ST-13 22 Medium, Gray CLAY with Silt pockets (CH) ST-13 22 Medium, Gray CLAY with Silt pockets (CH) ST-13 22 Medium, Gray CLAY with Silt pockets (CH) ST-13 22 Medium, Gray CLAY with Silt pockets (CH) ST-13 22 Medium, Gray CLAY with Silt pockets (CH) ST-13 ST-13 ST-13 ST-13 ST-13 ST-13 ST-13 ST-14 ST-15 ST-1			SA	MPL	ES				(tsf)					%
-35 35	Elevation feet	Depth, feet	⊢ Z		Sampling Resistance, blows / ft	Graphic Log		Torvane (tsf)	Hand Penetrometer (Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, 9
ST-3 22		-	ST-8	22			Very Soft, Gray CLAY becoming Gray SILT with Clay (CH) -				63	0.16	130	90
ST-10 21 Soft, Gray CLAY becoming Gray SiLT with Clay 46 84 0.36 83 52 ST-11 10 ST-11 10 ST-12 23 Soft, Gray CLAY with trace Silt and Organics 62 68 62 62 68 62 62 62 62 62 62 62 62 62 62 62 62 62	30	30	ST-9	22			Very Soft, Gray CLAY with Silt (CH)* -			71	61	0.18		
ST-11 10 Soft, Gray CLAY with trace Silt and Organics 62 68 ST-12 23 ST-12 ST-	35	35- - -	ST-10	21			Soft, Gray CLAY becoming Gray SILT with Clay - (CH)*			46	84	0.36	83	52
ST-12 23 Loose, Gray SILT with trace Organics, trace silt and silt lenses, with Clay (MH)* 50 76 0.33 55 22 ST-13 22 Medium, Gray CLAY with Silt pockets (CH) 50 81 0.34	- -40	40	ST-11	10			Soft, Gray CLAY with trace Silt and Organics - (CH)*			62	68			
ST-13 22 Medium, Gray CLAY with Silt pockets (CH) 50 81 0.3455 55	4 5	- 45 - - -	ST-12	23			Loose, Gray SILT with trace Organics, trace silt and silt lenses, with Clay (MH)*			50	76	0.33	55	22
	−-50	50- - - -	ST-13	22			Medium, Gray CLAY with Silt pockets (CH)			50	81	0.34		
	−-5 5	55- -					- - -							
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Project Number: 19228956.00001

Log of Boring B-6

Sheet 3 of 3



Project Number: 19228956.00001

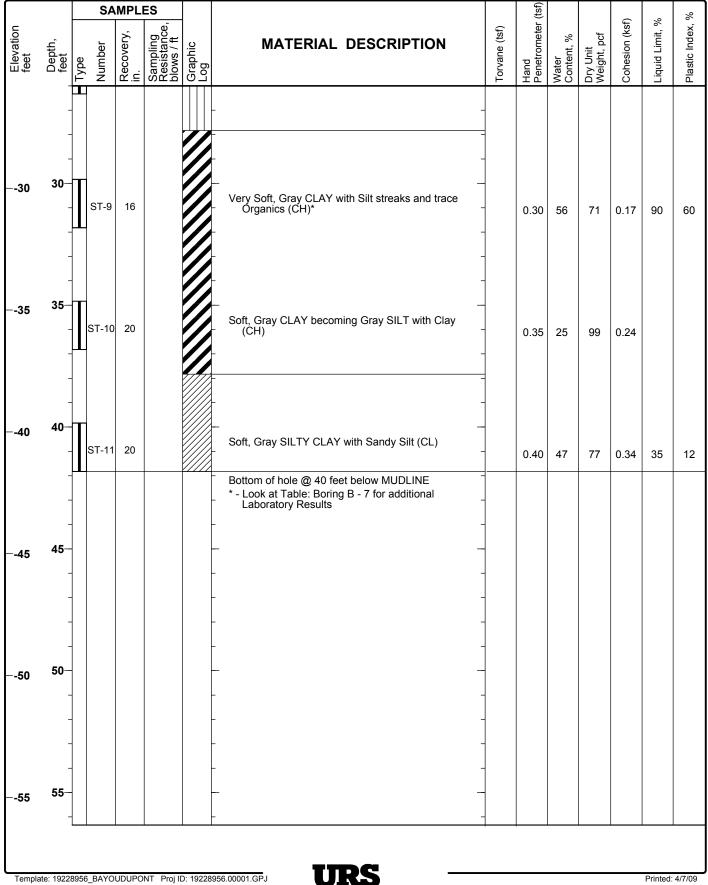
Log of Boring B-7

Date(s) Drilled 2/17/09 - 2/17/09	Logged By	A. Bukkapatnam	Checked By I. Harrouch
Drilling Method Rotary Wash	Drill Bit Size/Type	Bottom Discharge 4(5/8)"	Total Depth Drilled (feet) 41.8
Drill Rig Type Marsh Buggy	Drilling Contractor	SESI	Sampler Piston Sampler/ Shelby Tube
Groundwater Level and Date Measured 0.2' 2/17/2009	Hammer Data	140 LBS Safety	Approximate Surface Elevation 0.2'
Location N410229.205 E3692943.938			Borehole Backfill Cement Grout

			SA	MPLI	ES				(tsf)					%
Elevation feet	Depth, feet	Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, º
- 0	0-						_ WATER							
	4						MUDLINE EI -1.63'							
	-		ST-1	20			Very Soft, PEAT with Clay pockets (PT)		<0.25	955	6	0.04	925	595
- -5	5-		ST-2	15		~	Very Soft, PEAT becoming Clay with Organics (PT)*		<0.25	309	18		384	284
			ST-3	22			Very Soft, Gray CLAY with Organics (CH)		<0.25	112	45	0.05		
	40		ST-4	18			Very Soft, Gray SILTY CLAY with trace Organics (CL)*		<0.25	90	52	0.06		
−-10	10-		ST-5	15			Very Soft, Gray CLAY with Humus, Organic layers and pockets (OH)*		<0.25	334	18	0.10	240	178
−-15	15		ST-6	16			Very Soft, Intermixed Gray CLAY, SILT and SANDY SILT (CL to ML)		<0.25	55	70	0.08		
- -20	20		ST-7	18			Soft, Gray SILTY CLAY with trace Organics (CL)*		0.25	48	83	0.29	43	22
−-25	25-		ST-8	18			Firm, CLAYEY SILT with trace Sand (ML)*		0.25	29	99	1.06		

Project Number: 19228956.00001

Log of Boring B-7



Project Number: 19228956.00001

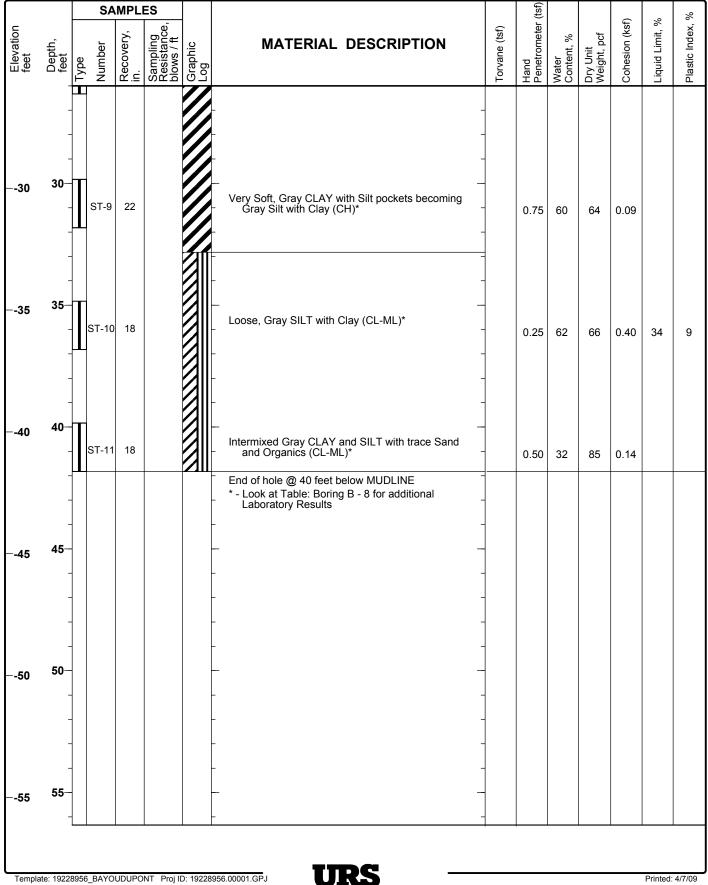
Log of Boring B-8

Date(s) Drilled 2/19/09 - 2/19/09	Logged By	A. Bukkapatnam	Checked By I. Harrouch
Drilling Method Rotary Wash	Drill Bit Size/Type	Bottom Discharge 4(5/8)"	Total Depth Drilled (feet) 41.8
Drill Rig Type Marsh Buggy	Drilling Contractor	SESI	Sampler Piston Sampler/ Shelby Type(s) Tube
Groundwater Level and Date Measured 0.2' 2/19/2009	Hammer Data	140 LBS Safety	Approximate Surface Elevation 0.2'
Location N410752.088 E3695435.524			Borehole Backfill Cement Grout

			SA	MPL	ES				(tsf)					%
Elevation feet	Depth, feet	Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, 9
-0	0-						WATER							
							MUDLINE EI1.63'							
	_		ST-1	20		**** *****	Very Soft, PEAT (PT)*	-		766	8	0.07		
5	5-		ST-2	20		****	Very Soft, PEAT with Clay pockets (PT)*	-	0.25	383	15	0.13		
	-		ST-3	22			Very Soft, Gray CLAY with Organic pockets (CH-OH)*		0.25	140	36	0.09	185	137
	-		ST-4	18			Very Soft, Gray CLAY with Organic pockets (CH)		0.25	117	44	0.06	96	63
−-10	10-		ST-5	18			Very Loose, Gray SILTY CLAY with Clay and Organic pockets (MH)*		0.25	130	40	0.05	87	36
1 5	15—		ST-6	16			Loose, Gray SILT with trace Sand and Silty Clay pockets (ML)*		0.25	50	75	0.82	NP	NP
20	20		ST-7	22			Loose, Gray SILT with trace Fine Sand and Clay and Organic pockets (ML)*		0.75	29	96	0.98	NP	NP
25	25-		ST-8	18			Very Soft, Gray CLAY with Silt and Organics (CH)		0.50	107	46	0.13	107	71

Project Number: 19228956.00001

Log of Boring B-8



Project Number: 19228956.00001

Log of Boring B-9

Date(s) Drilled 2/19/09 - 2/19/09	Logged By	A. Bukkapatnam	Checked By I. Harrouch					
Drilling Method Rotary Wash	Drill Bit Size/Type	Bottom Discharge 4(5/8)"	Total Depth Drilled (feet) 62.8					
Drill Rig Type Marsh Buggy	Drilling Contractor	SESI	Sampler Piston Sampler/ Shelby Tube					
Groundwater Level and Date Measured 0.2' 2/19/2009	Hammer Data	140 LBS Safety	Approximate Surface Elevation 0.2'					
Location N409821.951 E3695191.911								

		S	AMPL	.ES				(tsf)					%
Elevation feet	Depth, feet	Type Number	Recovery,	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, 9
-0	0-7												
	- - -	ST	1 20"		*****	WATER MUDLINE EI2.63' PEAT (PT)			894	6			
−-5	5- -	ST-	2 12"		<pre> </pre>	Very Soft, PEAT with Clay and Organics (PT)*			255	20	0.06	257	173
	-	ST-	3 18"			Very Soft, Gray CLAY with Organics (CH)*		0.25	135	36	0.11		
−-10	10-	ST-	4 20"		~	PEAT with Clay pockets and Silt pockets (PT)*	-	0.25	334	17	0.17	573	427
	-	ST-	5 18"			Very Soft, SILTY CLAY with Organics (CL)*		0.25	205	22	0.05		
	- 15	ST-	6 18"			Very Soft, Gray CLAY with trace Silt and Organic pockets (CH)*		0.50	60	62	0.08	65	39
⊢-15]	ST	7 20"			Very Soft, Gray CLAY with trace Organic pockets (CH)	-	0.25	59	72	0.15		
	-	ST-	8 18"			Very Soft, Gray CLAY with Silt and trace Organic (CH)	-	0.25	49	81	0.13	54	26
- -20	20-	ST-	9 20"			Loose, Gray SILT with clay pockets and trace Fine Sand (ML) -	-	0.75	34	87	0.53		
	-	ST-	10 22"			Firm, Gray SILT with trace Fine Sand and Clay (ML)*	-	0.25	25	95	2.94	NP	NP
−-25	25-	ST-	11 18"			Very Soft, Gray CLAY with Silt lenses (CH)	-	0.25	98	51	0.10		
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Project Number: 19228956.00001

Log of Boring B-9

		SA	MPL	ES				(tsf)					%
Elevation feet	Depth, feet	Type Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, 9
	1	S1-12				Soft, Gray CLAY with Silt pockets (CH)*		0.25	51	67		66	39
	-	ST-13	18"			Very Soft, Gray CLAY with Silt (CH)*		0.25	80	58	0.11		
30	30-	ST-14	22"			Soft, Gray CLAY with Silt pockets (CH)		0.25	64	62			
]	ST-15	16"			Very Soft, Gray CLAY with trace Silt and trace Organics (CH)*		0.50	71	60	0.14	72	45
	25	ST-16	20"		-	Loose, Gray SANDY SILT with Clay pockets (ML)	-	0.50	30	94			
⊢-35	35—	ST-17	16"			Soft, Intermixed CLAY and SANDY SILT (CL-ML)		0.75	39	82	0.48	38	7
	-	ST-18	20"			Soft, Gray SILT with CLAY pockets (ML)*		0.25	43	78			
40	40-	ST-19	16"			Soft, Gray SILT with CLAY pockets (ML)	-	0.25	55	66	0.31	86	52
	-	ST-20	16"		-	Soft, Gray SILT with CLAY pockets and layers (ML)	-	0.50	53	68			
		ST-21	16"			Very Soft, Gray CLAY with trace Silt (CH)		0.50	63	64	0.15		
−-45	45 <u> </u>	ST-22	18"			Very Soft, Gray CLAY with Silt pockets (CH)	-	0.25	54			60	34
	-	ST-23	18"			Soft, Gray CLAY with Sandy Silt pockets (CH)*	-	0.25	58	65			
50	50-	ST-24	22"			Very Soft, Gray CLAY with Silt pockets (CH)	<u>-</u>	0.25	57	67	0.19	52	31
	-	ST-25	12"			Sandy Clayey SILT (ML)*	-	0.25	34				
	-	ST-26	22"			Medium, Gray CLAY with Silt pockets (CH)	-	0.50	43	76	0.46	56	30
−-55	55 <u> </u>	ST-27	22"			Very Soft, Gray CLAY with trace Silt and Organics (CH)	-	0.75					
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Project Number: 19228956.00001

Log of Boring B-9

Sheet 3 of 3

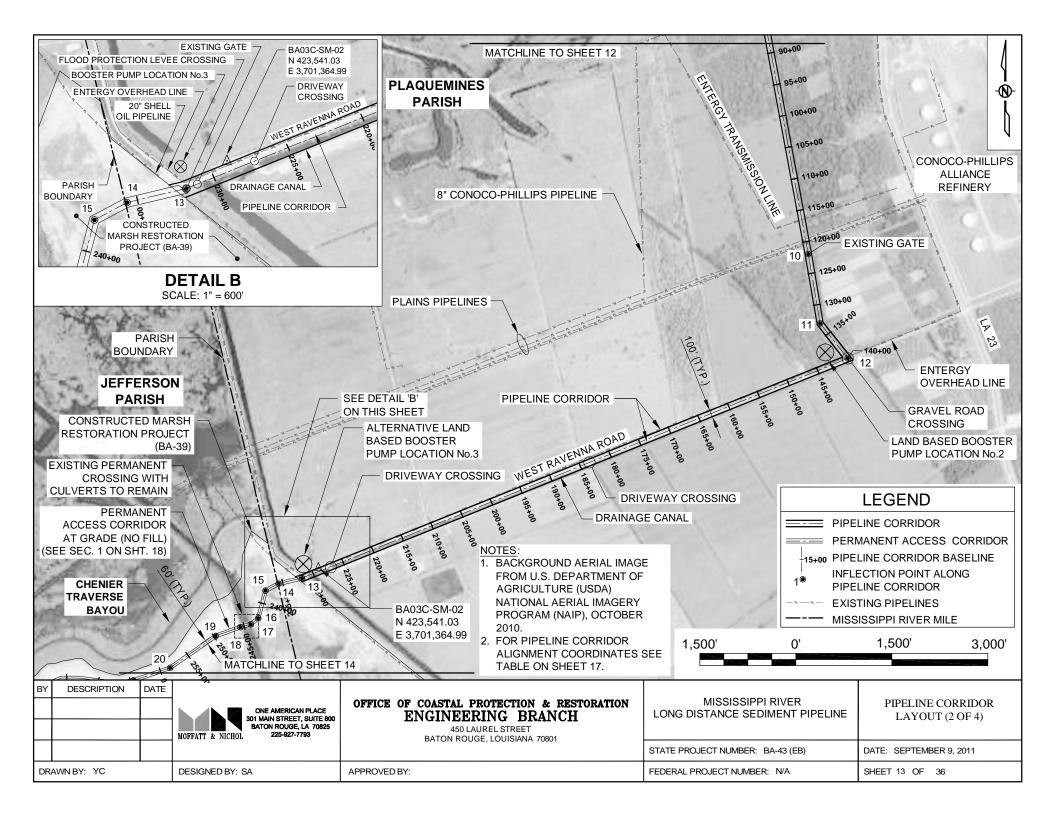
		S	AMPL	ES				(tsf)					%
Elevation feet	Depth, feet	Type Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, 9
	_	ST-2	8 22"			Soft, Gray CLAY with Silt (CH)*		0.50	59	67	0.36	76	49
60	60-	ST-2 ^t	9 20"			Soft to Medium, Gray CLAY (CH)		0.50	58				
	-	ST-3	0 18"			Very Soft, CLAY with trace Silt (CH)*		0.50	57	66	0.15	69	43
	65-				 - 	* - Look at Table: Boring B - 9 for additional Laboratory Results							
−-65	-				_	-							
	_				_	-							
70	70-					- -							
	_				_	- -							
	- 75–				-	_ _							
−-75	-				-	- -							
	-				-	- -							
80	80-				_	- -							
	-				-	-							
−-85	- 85—				-	- -							
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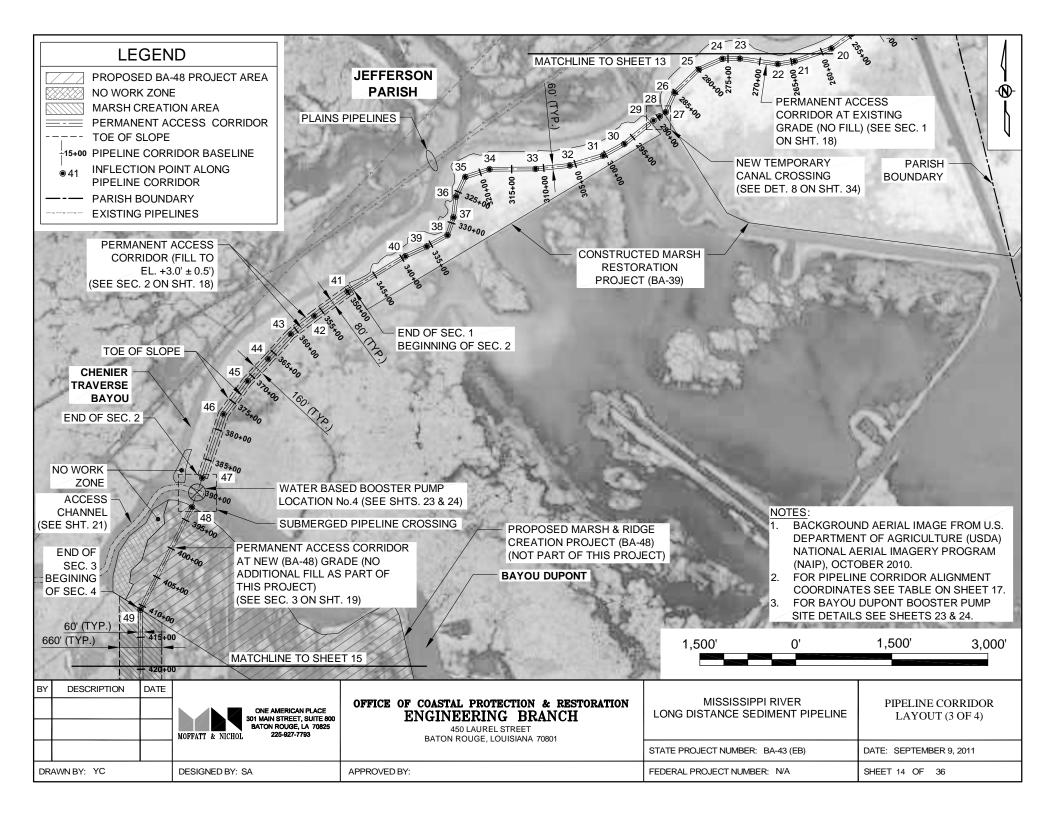


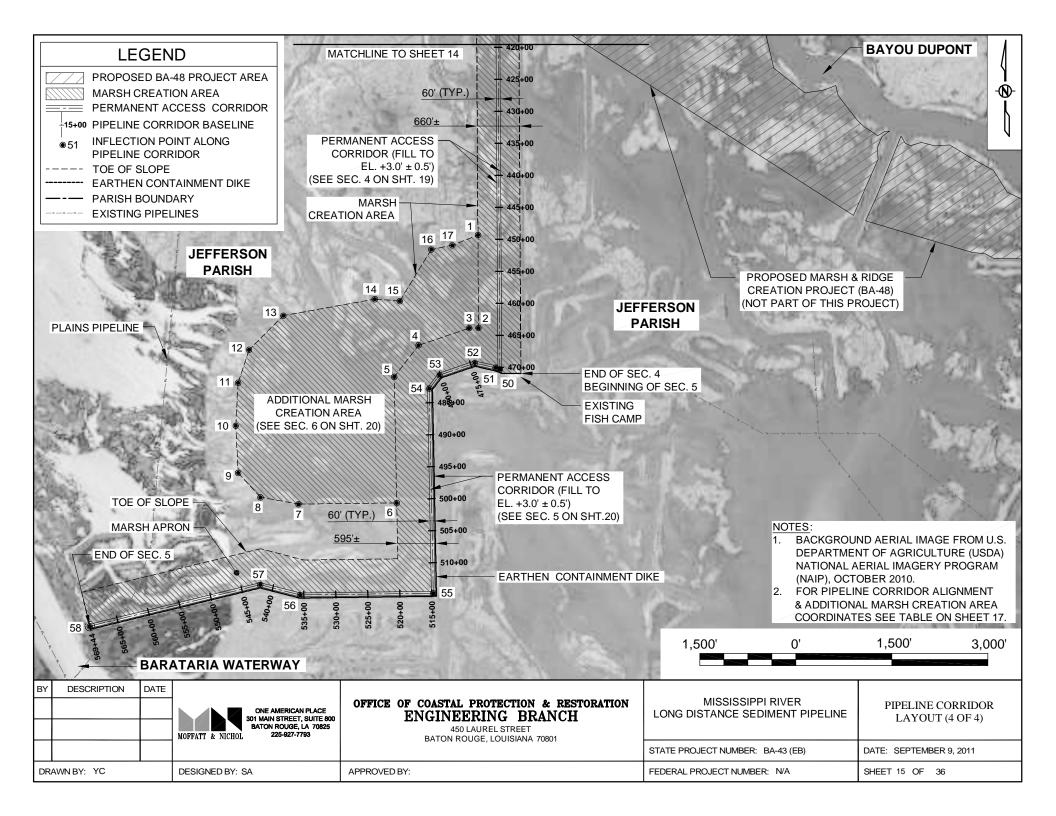
APPENDIX E

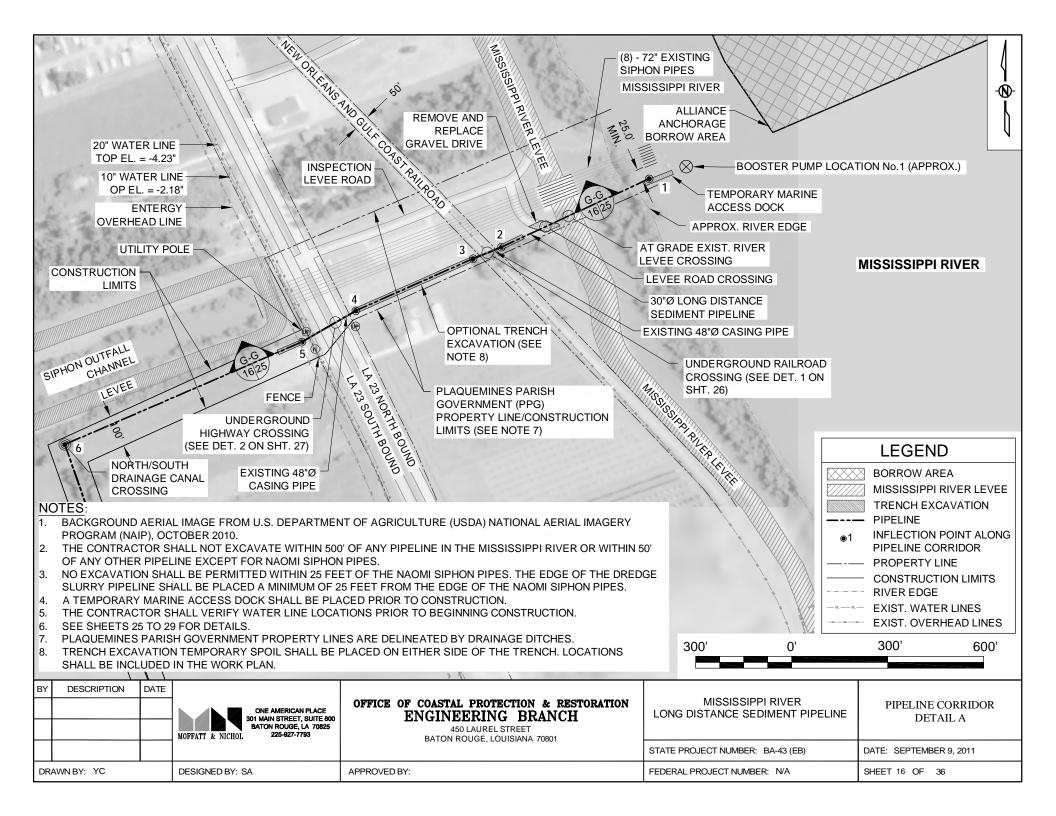
TYPICAL CROSS-SECTIONS PROVIDED BY MOFFATT AND NICHOL











PIPELINE CORRIDOR ALIGNMENT

PT.	EASTING	NOTRHING
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2	3708833.00	439073.60
3	3708745.00	439037.80
4	3708378.00	438874.90
5	3708210.00	438777.60
6	3707468.37	438457.08
7	3708010.71	436924.44
8	3708151.13	433271.33
9	3708274.87	432470.08
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18	3700308.33	422615.52
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20	3699047.76	421979.44
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29	3696265.66	420853.30
30	3695810.63	420487.43
31	3695480.80	
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	3694958.57	420150.54
33	3694425.06 3693702.83	420098.06 420090.22
1		
35	3693324.98	419970.64
36	3693181.49	419664.54
37	3693138.44	419339.30
38	3693047.57	419061.89
39	3692722.33	418884.92
40	3692387.88	418732.22
41	3691538.38	418212.51
42	3690965.90	417799.60
43	3690596.95	417515.21
44	3690245.94	417128.33
45	3689923.11	416782.44

PT.	EASTING	NOTRHING				
46	3689546.48	416264.89				
47	3689213.40	415268.22				
48	3689054.74	414815.39				
49	3688249.91	413214.21				
50	3688282.83	407251.28				
51	3688214.75	407277.40				
52	3687891.71	407348.42				
53	3687340.48	407159.87				
54	3687180.94	406952.63				
55	3687243.43	403753.80				
56	3685161.39	403726.37				
57	3684537.11	403885.76				
58	3681873.45	403237.73				

ADDITIONAL MARSH AREA

PT. EASTING NOTRHIN 1 3687941.24 409350.34 2 3687949.27 407895.63 3 3687802.63 407895.63 4 3687011.95 407626.56 5 3686632.31 407133.33	1 1 1
2 3687949.27 407895.6 ⁻ 3 3687802.63 407895.6 ⁻ 4 3687011.95 407626.56	1
3 3687802.63 407895.6 ² 4 3687011.95 407626.56	1
4 3687011.95 407626.56	
5 3686632.31 407133.37	3
	7
6 3686670.77 405164.44	1
7 3685135.17 405145.15	5
8 3684540.07 405252.97	7
9 3684192.66 405633.55	5
10 3684154.49 406370.0	4
11 3684191.67 407042.4	4
12 3684363.02 407557.4	6
13 3684898.65 408089.5	4
14 3686328.06 408348.4	6
15 3686719.48 408317.6	8
16 3687210.41 409124.0	0
17 3687540.48 409189.2	6

PROBABLE BOOSTER PUMP LOCATIONS

No.	EASTING	NOTRHING
1	3709411.03	439325.16
2	3709430.00	426505.97
3	3701075.84	423518.50
4	3689132.52	415040.26

ACCESS CHANNEL ALIGNMENT

PT.		NOTRHING			
1	3674046.30	417690.06			
2	3674443.87	417928.38			
3	3674549.10	417843.37			
4	3674605.34	417650.30			
5	3674768.33	417626.30			
6	3674891.14	417524.89			
7	3675173.97	417404.50			
8	3675374.37	417400.08			
9	3675899.41	417192.18			
10	3676242.80	417171.66			
11	3676428.65	417358.88			
12	3676548.44	417686.20			
13	3676739.59	417811.17			
14	3677375.53	417869.55			
15	3677870.90	417830.11			
16	3678337.82	417708.89			
17	3678811.83	417514.80			
18	3679772.32	416805.21			
19	3679930.74	416596.04			
20	3680221.29	416069.93			
21	3680593.81	415970.76			
22	3680718.25	415816.36			
23	3680950.88	415619.43			
24	3681378.51	415564.60			
25	3681635.27	415496.11			
26	3681977.36	415432.46			
27	3682205.59	415229.13			
28	3682250.83	415129.57			
29	3682397.09	414968.27			
30	3683138.30	414802.76			
31	3683474.36	414513.64			
32	3683792.94	414308.27			
33	3684035.91	414239.78			
34	3684285.57	414253.96			
35	3684542.75	414352.05			
36	3684764.87	414409.57			
37	3685015.36	414387.73			
38	3685168.42	414252.81			
39	3685281.66	414088.33			
40	3685359.42	414002.16			
41	3685450.50	413949.56			
42	3685898.07	413778.66			
43	3686447.21	413686.62			
44	3686740.16	413671.24			
45	3687188.62	413691.73			

PT.	EASTING	NOTRHING			
46	3687438.03	413721.65			
47	3687616.06	413782.04			
48	3687710.79	413852.06			
49	3687766.22	414034.24			
50	3687811.91	414175.11			
51	3687930.02	414339.53			
52	3688053.13	414460.19			
53	3688138.44	414524.38			
54	3688306.59	414717.17			
55	3688397.69	414842.33			
56	3688450.73	414937.10			
57	3688547.73	415047.00			
58	3688627.47	415092.91			
59	3688728.60	415115.08			
60	3688878.22	415127.36			
61	3689243.43	415004.47			

E	Y DESCRIPTION	DATE	ONE AMERICAN PLACE 301 MAIN STREET, SUITE 800 BATON ROUGE, LA 70825 225-927-7793	OFFICE OF COASTAL PROTECTION & RESTORATION ENGINEERING BRANCH 450 LAUREL STREET BATON ROUGE. LOUISIANA 70801	MISSISSIPPI RIVER LONG DISTANCE SEDIMENT PIPELINE	PROJECT ALIGNMENT TABLES	
					STATE PROJECT NUMBER: BA-43 (EB)	DATE: SEPTEMBER 9, 2011	
DRAWN BY: YC			DESIGNED BY: SA	APPROVED BY:	FEDERAL PROJECT NUMBER: N/A	SHEET 17 OF 36	

