URS

July 23, 2009

LDNR/CED
617 North 3rd Street,
Suite 1036D,
Baton Rouge, LA 70802

Attn: Ms. Whitney Thompson, P.E.

Re: Geotechnical Investigation Report
Bayou DuPont Marsh Creation and Ridge Restoration
Jefferson Parish, Louisiana.
URS Project Number 19228956

Dear Ms. Thompson:

URS Corporation has completed the geotechnical investigation and analyses for the above referenced project. This investigation was performed in support of the proposed Bayou DuPont Marsh Creation and Ridge Restoration Project as per LDNR Contract No: 2503-09-17. The report presented, contains the details pertaining to the Geotechnical Investigation Data Report (GIDR) and the Geotechnical Engineering Report (GER).

The scope of our geotechnical evaluation was to provide geotechnical field investigation, laboratory testing, engineering analyses and recommendations for the design and construction of an earthen dike along the boundaries of the proposed site. Our analysis involved the estimation of time-dependent settlement issues for the dike and the evaluation of settlements due to the placement of dredged fill within the dike boundaries. The results of the field investigation, laboratory testing and engineering analyses are presented herein.

Site Location

The site is located in Jefferson Parish, Louisiana, along the southern bank of Bayou DuPont, southeast of the Pen, approximately 4.5 miles southeast of Lafitte. The approximate coordinates of the center of the project areas are as follows: X = 3,692,332, Y = 411,524 (NAD 83 Louisiana State Plane, South Zone, U.S. survey feet). The site location can be seen highlighted on the Site Location Plan (Figure 1) in Appendix A.

Field Investigation

The subsurface investigation, as requested by LDNR, consisted of drilling and sampling nine (9) geotechnical exploratory soil borings using a marsh-buggy mounted rotary drill rig. The soil test borings were conducted to varying depths of 30, 40 and 60 feet. The approximate boring locations and their coordinates are shown on the attached Test Location Plan (Figure 2) in Appendix A. The boring logs are included in Appendix B.

Table 1 below shows the GPS coordinates of the drilled borings. Wet rotary drilling procedures were used with the samples being collected using a Piston Sampler/Shelby tube. The boreholes were tremie grouted full depth with a cement grout per Louisiana DOTD requirements after the

drilling process was completed and the samples retrieved.

Two 30 feet borings (B-1 and B-2), four 40 feet borings (B-3, B-4, B-7 and B-8), and three 60 feet borings (B-5, B-6 and B-9) were drilled. One 60 foot boring (B-9) was sampled continuously at 2 foot intervals to 60 feet, and the remaining borings sampled continuously for the top 10 feet and then on 5 foot centers thereafter until termination.

Table 1: Boring Coordinates

Boring No.	Date Drilled		Boring Coordinates			
	Started	Ended	Latitude (N)	Longitude (W)	Northing	Easting
B1	2/20/2009	2/20/2009	29.63439	90.04759	414828.534	3689295.369
B2	2/19/2009	2/19/2009	29.62419	90.03330	411170.779	3693876.982
B3	2/20/2009	2/20/2009	29.63122	90.04792	413674.665	3689203.468
B4	2/17/2009	2/17/2009	29.62650	90.04498	411968.841	3690156.752
B5	2/16/2009	2/17/2009	29.62901	90.04129	412894.741	3691318.762
B6	2/17/2009	2/17/2009	29.62614	90.03769	411864.051	3692474.243
B7	2/17/2009	2/17/2009	29.62163	90.03627	410229.205	3692943.938
B8	2/19/2009	2/19/2009	29.62299	90.02841	410752.088	3695435.524
B9	2/19/2009	2/19/2009	29.62044	90.02921	409821.951	3695191.911

From the soil test borings, undisturbed samples of cohesive soils were recovered using a 3-inch diameter thin walled Shelby tube using a Piston Sampler (ASTM D-1587). The tubes were capped at both ends and sealed to preserve the sample's natural characteristics and brought to the laboratory. In the laboratory, the samples were extruded and visually classified by an engineer.

Geological Information

The New Orleans area and the upper delta of the Mississippi River are underlain by Pleistocene and Holocene coastal-plain deposits of the Mississippi River deltaic plain (Kolb, 1962; Kolb and others, 1975; Dunbar et al., 1994; Saucier, 1994). In the Bayou DuPont area (west bank of the Mississippi River west of Myrtle Grove), the Holocene deposits generally range from 100 to 150 feet thick (Kolb and others, 1975, Plate 4; Saucier, 1994, Plate 27) and are underlain by undifferentiated alluvial deposits of the Pleistocene-age Prairie Formation (Prairie Complex). Along the alignment of Bayou DuPont, the Holocene sediments consist of fine-grained sediments deposited in near-shore shelf environments, delta front, deltaic (inter-distributary) bays, and marshes. The Holocene sediments also include silt and fine sand that were deposited in inter-distributary bay and natural-levee sedimentary environments. The Pleistocene Prairie Complex consists of undifferentiated alluvial deposits.

The geologic interpretation of the subsurface soils of the south side of Bayou DuPont has been based on the soil boring logs for project borings B-1 through B-9. The soil boring logs extend from the sediment-water interface (depths of approximately 0.4 to 2.8 feet below water level) to elevations ranging from -31 to approximately -63 feet NGVD. Selected soil boring logs that were utilized for engineering geologic mapping of the Mississippi River deltaic plain (Dunbar and others, 1994) also were reviewed for the Bayou DuPont area. The geological investigation also utilized information from previous investigations including Kolb (1962), Kolb and others (1975), Kolb and Saucier (1982), Dunbar and others (1994), and Saucier (1994).

Summary of Stratigraphy along the South Side of Bayou DuPont

This section summarizes the stratigraphy in the project area with reference to the geologic cross section (profile) that has been constructed as part of this project. The lithologic and stratigraphic units in the project area have been identified based on the recognized stratigraphic units in the adjacent area (Dunbar and others, 1994, Barataria Quadrangle and Pointe A La Hache Quadrangle). The subsurface stratigraphy along the alignment of Bayou DuPont generally consists of the following lithologic or stratigraphic units from the sediment-water interface downward:

Lithologic or Stratigraphic Unit	Approximate Elevation Range (feet NGVD)	Range of Thickness (feet)	Predominant Lithology
Holocene Marsh Deposits	0 to -11	4 to 8	Dark gray, brown, and black soft organic clay and peat.
Holocene Natural Levee Deposits and Distributary Deposits	-5 to -26	Natural levee deposits 7 to 9 feet thick; the combined thickness of levee and distributary deposits can be up to 19 feet thick.	Gray silty clay, clayey silt, silt, and sandy silt. Natural levee deposits can be interbedded with gray clay. Natural levee deposits can underlie and overlie marsh deposits or can be absent in some areas.
Holocene Inter-distributary Deposits	-5 to -60	34 to 55	Inter-distributary deposits consist of gray and dark gray clay interbedded with silt and silty sand laminae and lenses.
Holocene Prodelta Deposits	-60	Exceeds 40 feet	Soft to medium dark gray clay. Silt lenses and strata can occur in the upper portion.

One geologic cross section (profile) has been prepared to illustrate the subsurface conditions and the distribution of the lithologic and stratigraphic units along the south side of Bayou DuPont. The geologic section extends along the entire length of the marsh creation project areas. The geologic profiles have been developed using the soil boring logs and extend from the sediment-water interface to elevations of approximately -60 feet NGVD. The identification and geologic interpretation of the stratigraphic units in the geologic profiles has been based on the lithologies shown on the soil boring logs, the vertical sequence of lithologies, and the stratigraphic identifications of Dunbar and others (1994) for the Pointe A La Hache Quadrangle (Section B-B'). The subdivision of the stratigraphic units in the geologic profiles generally follows the subdivisions and geologic criteria used by Dunbar and others (1994).

Soft clay, organic clay, and peat have been deposited in marsh environments throughout the area. The marsh deposits were identified by the presence of peat and organic clay layers and occur between elevations of 0 and -11 feet NGVD. The marsh deposits generally occur above the natural levee deposits, but also can be interbedded with natural levee deposits. The marsh deposits are 4 to 8 feet in thickness.

The natural levee deposits and distributary channel deposits consist of gray silty clay, clayey silt, silt, and sandy silt. The natural levee deposits make up the upper part of these deposits and generally occur in the elevation range of -5 to -15 feet NGVD. The thickness of the natural levee deposits ranges from 7 to 9 feet. The natural levee deposits are interpreted to be deposited in the natural levees of Bayou DuPont or in the distal natural levees of the Mississippi River or of Bayou Barataria. Organic-rich clay layers deposited in marsh or swamp environments can be interbedded with the natural levee deposits. The natural levee deposits are variable in thickness and are absent at boring B-4 on the south side of Marsh Creation Area 1 and at borings B-5, B-6, and B-2 on the south side of Bayou DuPont. The distributary deposits occur to elevations of -21 to -26 feet NGVD in borings B-7, B-8, and B-9 in the eastern portion of the project area. Where the natural levee deposits and distributary deposits are absent, the marsh deposits directly overly the inter-distributary deposits.

The inter-distributary deposits in the project area consist of soft gray clay with interbeds and laminae of silt and sand. The top of the inter-distributary deposits generally occurs between -5 and -15 feet NGVD and can occur at elevations of -21 to -26 feet NGVD where the distributary deposits are present. A silt interval consisting of interbedded clayey silt, silt, and sandy silt occurs within the inter-distributary deposits in borings B-3, B-4, B-5, B-6, B-7, B-8, and B-9. The top of the silt zone occurs at an elevation range from approximately -25 to -42 feet NGVD and the base of the silt zone occurs at elevations of approximately -38 to -47 feet NGVD. The thickness of the silt zone ranges from 5 to 21 feet in the project area. The silt zone is interpreted to represent a crevasse-splay deposit from a deltaic distributary channel. The silt zone generally is interbedded with thin beds and lenses of clay. The Bayou des Familles channel located to the west of the project area could have been the source of sediment discharge for the crevasse splay deposit. Crevasse splay deposits typically consist of lobes of silt and sand that extend away from the source channel.

The inter-distributary deposits are underlain by prodelta clay. The top of the prodelta deposits generally occurs at elevations of -60 feet NGVD in this area (Dunbar and others, 1994). The prodelta deposits have a lower percentage of silt and sand strata than the overlying inter-distributary deposits. The prodelta deposits can include silt strata or lenses. The base of the prodelta clay was not encountered during drilling of the project borings. The prodelta clay overlies the Pleistocene Prairie complex in the project area (Dunbar and others, 1994).

The Pleistocene Prairie complex was not encountered during drilling of the soil boring logs. The top of the Pleistocene occurs at an elevation of -100 to -150 feet NGVD in the project area. The stratigraphy of the Pleistocene units and the elevation contours of the top of the Pleistocene are shown in Dunbar and others (1994) for the Barataria Quadrangle and the Pointe A La Hache Quadrangle.

Geologic History

The Pleistocene Prairie Complex was deposited in a coastal-plain setting approximately 135,000 to 150,000 years before present (Saucier, 1994). During the late-Pleistocene (Wisconsin Stage) glaciation between 120,000 and approximately 10,000 years before present (B.P.), the Prairie Complex was exposed to weathering and erosion due to the low stand of sea level that accompanied

glaciation. During the low-stand period, the Prairie Complex sediments were oxidized and desiccated resulting in over-consolidation of the soil and the development of soil-weathering features such as iron oxidation and precipitation of calcium carbonate nodules. The erosion surface of the Pleistocene sediments is a distinct contact that generally can be recognized by the contrast between the Holocene and Pleistocene sediments in color, soil consistency and strength, and water content. The overlying Holocene sediments typically are dark gray or blue gray in color. The upper portion of the Pleistocene generally is tan, reddish brown, or brown in color as a result of the soil oxidation accompanying weathering during the sea-level low stand. Where the Pleistocene contact is deeper than 50 feet below sea level, the color of the Pleistocene sediment can be mottled tan, orange, and greenish gray and have a smaller contrast with the Holocene sediments. The soil cohesive strengths in the upper portion of the Pleistocene clay range from 0.5 to more than 2.0 tons per square foot (tsf). The immediately overlying Holocene near-shore clays have much lower cohesive strengths. The high soil strengths of the majority of the Pleistocene soils are due to cementation by hydrous iron oxides, calcium carbonate, siderite, and manganese carbonate (Kolb and others, 1975) resulting from the exposure and weathering that took place during the glacial low stand of sea level. The water content of the overlying Holocene sediments is generally much higher than the Pleistocene sediments, which have water contents less than 50 percent.

The Holocene transgression (rise) of sea level started approximately 18,000 years B.P. and was at an elevation of approximately -100 feet msl by 9,000 years ago. The shoreline was located in the Bayou DuPont area by approximately 10,000 to 9,000 years B.P. (Saucier, 1994). Approximately 6,000 years ago, the elevation of sea level was approximately 10 to 15 feet below its present level. As sea level continued to rise, clay and sand was deposited across the area in near shore Gulf environments. The St. Bernard delta complex of the Mississippi River delta began to form approximately 4,700 years B.P. and fine-grained sediments were deposited in the delta-front environment (prodelta) and in inter-distributary bays. The Bayou des Familles distributary of the St. Bernard delta complex, located 2 to 4 miles southwest and west of the project area, was active from as early as 4,600 years b.p. until approximately 2,000 years b.p. The Bayou Sauvage distributary of the St. Bernard delta complex was located to the north of the project area and was active until approximately 1,000 years b.p. or more recently. The prodelta deposits consist of soft dark-gray clay that accumulated in the delta-front environment to a thickness of over 40 feet. The prodelta deposits grade upward into the inter-distributary deposits with interbedded silt and sand as the depositional environment shallowed. The distributary channels of the delta complex prograded into the near shore Gulf environment resulting in shallower water depths in bays that formed between the distributary channels. The proximity of the distributary channels resulted in periodic deposition of silt and sand layers during periods of flooding. Deposition of silt and sand in lobate crevasse splay deposits occurred in areas adjacent to flood discharges from the distributary channels. As the areas of inter-distributary deposition across the area became shallower, coastal marsh deposits formed. The Mississippi River established its present course approximately 600 years ago and has deposited clay, silty clay, and silt in natural-levee deposits adjacent to the river during periods of river flooding. The natural-levee deposits are up to approximately 5 to 10 feet in thickness and generally become thinner or absent away from the river. The upper 5 to 20 feet of the Holocene sediments can consist of soft to very soft clays deposited in fresh-water marshes and swamps and in coastal marshes. The natural-levee sediments can be underlain and overlain by marsh and swamp deposits. Figure 3 in Appendix B shows the geological profile for the project site as described above.

Subsurface Conditions

Based upon the field investigation and the laboratory test results, the soils encountered at the site may be categorized into five (5) general strata for discussion purposes and for the purposes of our

engineering analysis. The soils at the test site may be generally described as a surficial layer of approximately 4.5 feet of Organic Peat (PT), underlain by a Organic Clay (CH-OH) layer extending to an average depth of 12 feet, intermittent Silt and Silty Clay (CL) layers extending to a depth of 42 feet, underlain by Silty Clay and fat Clay layers (CL, CH) extending to the maximum explored depth of 60 feet. Soil boring logs are included in Appendix B which show a detailed description of the materials encountered at each of the boring locations as well as the results from the associated laboratory tests.

Surface Water Elevation

Water level depths at the site were monitored throughout the field investigation to determine the mud-line elevations at the boring locations and to establish a generalized elevation for the test site. An existing water gauge (Station I.D. BA03C-61) located at the following GPS coordinate (N410795.322, E3694472.572) was used to determine the daily water elevation of the test site.

Table 2 shows the water level elevations and the mud-line elevations for each boring along with the water gauge reading on the day the boring was drilled. For our engineering analysis the water level was assumed to be at El. 0 feet (NAVD) and the mud-line to be at El. -1.4 feet (NAVD).

Table 2: Water Level Measurements

Boring No.	Date Drilled		Water Gauge Elevation (NAVD)	Depth from Water Surface to Mud-Line (feet)	Mud-Line Elevation (feet)
	Started	Ended			
B1	2/20/2009	2/20/2009	-0.2	1.83	-2.03
B2	2/19/2009	2/19/2009	0.2	1.50	-1.30
B3	2/20/2009	2/20/2009	-0.2	0.67	-0.87
B4	2/17/2009	2/17/2009	0.2	0.67	-0.47
B5	2/16/2009	2/17/2009	0.2	0.42	-0.22
B6	2/17/2009	2/17/2009	0.2	2.17	-1.97
B7	2/17/2009	2/17/2009	0.2	1.83	-1.63
B8	2/19/2009	2/19/2009	0.2	1.83	-1.63
B9	2/19/2009	2/19/2009	0.2	2.83	-2.63
				Average Mud-Line Elevation	**-1.40**

Laboratory Testing

Laboratory tests were assigned based on visual classification for materials representative of the five general soil strata encountered at the site. At least two (2) classification and strength tests were assigned for each of the representative soil strata. Consolidation tests were performed to evaluate soil past consolidation history. Unconsolidated Undrained (UU) triaxial shear tests were performed on selected samples to evaluate soil parameters for use in calculating undrained shear strength. Atterberg Limits, Grain-size distribution tests, Water Content and Organic Content determinations were performed to classify the subsurface soils more accurately than using the field classification.

The results of the laboratory analysis are presented in the soil boring logs in Appendix B and in the tables (Summary of all Lab Tests) presented in Appendix C. The stress-strain curves and the consolidation curves for all the samples tested are presented sequentially (according to the borings) in a separate folder titled "Bayou DuPont Lab Results". The sub-surface undrained shear strength

profile and shear strength contour plots are presented in Figure 4 and Figure 5 as shown in Appendix C. Spreadsheet summaries of all laboratory test results are included in Appendix C.

Engineering Analyses

Based on the scope of services for the proposed project, the overall stability of the nourished marsh, earthen dike construction, and ridge restoration as well as settlement analyses were part of the engineering analyses. Soils suitable for the construction of the earthen dike were evaluated based on the time-rate settlement calculations using 1-D Terzaghi consolidation theory. Slope-Stability analysis using the Slope-W software was performed to evaluate if the dike was stable against failure, by considering a minimum factor of safety of 1.3. Long term settlement evaluations for the dredged fill material were calculated using the U.S. Army Corps of Engineers Program: Primary consolidation, Secondary compression and Desiccation of Dredged Fill (PSDDF), and compared with hand calculations using the Finite-Strain consolidation theory.

PSDDF Analysis for placement of Dredged Fill

The PSDDF program was used to calculate the long-term settlements of the soil sub-layers as well as the self-weight consolidation settlement of the dredge fill material. As requested, this phase of the project was subcontracted to Dr. Gouping Zhang, P.E., Assistant Professor at Louisiana State University Department of Civil and Environmental Engineering. The PSDDF analysis results and report provided by Dr. Zhang is included in Appendix E.

As part of the PSDDF analysis results, the time-rate settlement curves were provided for five different dredge fill heights along with the settlement curves of the soil sub-layers for a maximum time period of 20 Years. A fill material having a specific gravity of 2.7 and initial void ratio of 0.98 was used for the analysis.

After a comprehensive review of the analysis results from the software, it was determined that PSDDF assumes the dredge fill material to be saturated. Accordingly, PSDDF uses the effective stress condition for all settlement calculations. This was subsequently verified by the developer of the software program.

For the purposes of our analysis for this project, we assumed the water level was assumed to be at El. 0 feet (NAVD) and the mud-line to be at El. -1.4 feet (NAVD). Hence, total stress conditions must be considered for settlement calculations due to the dredge fill materials extending above the water level. Consequently, we consider the original PSDDF settlement analysis results provided for the dredge fill material and soil sub-layers to likely be underestimated for this project.

To compensate for what we consider to likely be underestimated PSDDF settlement results, the effective stress dredge fill height was increased sufficiently to obtain an equivalent total stress condition dredge fill height. The greater PSDDF settlement values obtained using the equivalent dredge fill height were verified using hand calculations performed based on the Finite-Strain consolidation theory, with the results being in close agreement with each other.

Table 3 shows the summary of ultimate settlement of the dredge fill and the soil sub layers using actual the fill height (effective stress condition) and also due to the equivalent fill height (total stress condition).

Table 3: PSDDF Settlement of Dredge Fill and Soil Sub-layers					
Actual Fill Height (feet)	Settlement of sub-layers from Actual Fill Height after 20 Years (feet)	Equivalent Fill Height (feet)	Settlement of sub-layers from Equivalent fill height after 20 Years (feet)	Estimated Fill Settlement (feet)	Total Settlement from Equivalent Fill Height after 20 Years (feet)
2.0	0.74	2.7	1.10	0.06	1.16
2.5	1.02	3.8	1.58	0.07	1.65
3.0	1.24	4.9	2.01	0.09	2.10
4.0	1.66	7.0	2.50	0.13	2.63
5.0	2.07	9.2	2.67	0.17	2.84
6.0	2.44	11.4	2.75	0.21	2.96

The settlement curves obtained using the actual dredge fill heights and the curves obtained using the equivalent dredge fill heights can be seen in Figures 7 and 10 respectively, and are presented in Appendix D of this report. The output from PSDDF for various dredge fill heights and the output for the corresponding equivalent dredge fill heights are presented in Appendix D. The surface elevation curves and the degree of consolidation curves can be seen in Figure 6 and Figure 8 for the actual fill heights, Figure 9 and Figure 11 for the equivalent fill heights, and are presented in Appendix D.

Design of Earthen Containment Dike

Construction of an earthen containment dike along the boundary of the project site is necessary before the placement of dredged fill material. Current plans call for the dike materials to be obtained through excavation of the existing soils from within the containment area at a minimum distance of 25 feet from the inner toe of the dike.

The uppermost soil layer at the site is mostly Organic Peat material having a specific gravity of 1.98 and initial void ratio of 6.5. Considering the low strength characteristics of the organic laden soil materials as well as likely construction difficulties, the stability of the containment dike system was analyzed having top crown widths of 6 feet and 10 feet, and with side slopes of 4H:1V and 5H:1V.

Dike crown heights of 3, 3.5, 4, 5, 6 and 7 feet were analyzed for settlement of each case with the 1-D Terzaghi Consolidation Theory and using stresses computed from Boussinesq's Theory for embankment settlement calculations. PSDDF was also used for analyzing the dike settlement but the program does not consider a Boussinesq stress reduction due to the dike geometry and thus tends to overestimate settlements. However, the PSDDF settlement results were used for comparison purposes to those determined using the Terzaghi and Boussinesq based hand calculations, and were found to be greater as expected.

Table 4 and Table 5 below show a summary of the calculated settlements for 5H:1V side slope and 4H:1V side slopes respectively. Surface Elevation and Settlement curves for six (6) different dike heights can be seen in Figures 12, 13, 16 and 17 for a crown width of 6 feet, and Figures 14, 15, 18, 19 for a crown width of 10 feet, presented in Appendix F of this report.

Table 4: Settlement of and Soil sub-layers (Mud-line @El. -1.4 feet NAVD) (Using Boussinesq Stress Theory and 1-D Terzaghi Consolidation Theory)					
Crown Width – 10 feet (Side Slope - 5H:1V)					
Height of Dike (feet)	Settlement of sub-layers after 20 Years (feet)	Ultimate Settlement of Soil Layers* (feet)	Estimated Dike Settlement** (feet)	Total Settlement of after 20 Years (feet)	Surface Elevation of Dike after 20Years (feet)
3.0	0.80	1.05	0.08	0.89	0.71
3.5	1.05	1.34	0.12	1.17	0.93
4.0	1.30	1.64	0.17	1.47	1.13
5.0	1.80	2.24	0.29	2.09	1.51
6.0	2.32	2.84	0.43	2.75	1.85
7.0	2.84	3.31	0.60	3.44	2.16
Crown Width – 6 feet (Side Slope - 5H:1V)					
3.0	0.76	0.81	0.08	0.84	0.76
3.5	1.00	1.07	0.12	1.12	0.98
4.0	1.24	1.33	0.17	1.41	1.19
5.0	1.74	1.87	0.29	2.03	1.58
6.0	2.25	2.42	0.43	2.68	1.92
7.0	2.76	2.98	0.60	3.37	2.23

* - Ultimate Settlement corresponds to the settlement of the sub-surface soils due to the placement of the dike beyond 20 years.

** - Internal Settlement of the Dike in 20 years.

Table 5: Settlement of and Soil sub-layers (Mud-line @El. -1.4 feet NAVD) (Using Boussinesq Stress Theory and 1-D Terzaghi Consolidation Theory)					
Crown Width – 10 feet (Side Slope - 4H:1V)					
Height of Dike (feet)	Settlement of sub-layers after 20 Years (feet)	Ultimate Settlement of Soil Layers* (feet)	Estimated Dike Settlement** (feet)	Total Settlement of after 20 Years (feet)	Surface Elevation of Dike after 20Years (feet)
3	0.78	0.84	0.08	0.87	0.73
3.5	1.02	1.09	0.12	1.14	0.96
4	1.27	1.36	0.17	1.44	1.17
5	1.76	1.89	0.29	2.05	1.55
6	2.27	2.44	0.43	2.70	1.90
7	2.78	3.00	0.60	3.38	2.22
Crown Width – 6 feet (Side Slope - 4H:1V)					
3	0.73	0.78	0.08	0.82	0.79
3.5	0.96	1.03	0.12	1.08	1.02
4	1.20	1.28	0.17	1.37	1.23
5	1.69	1.81	0.29	1.97	1.63
6	2.19	2.35	0.43	2.62	1.98
7	2.69	2.90	0.60	3.29	2.31

* - Ultimate Settlement corresponds to the settlement of the sub-surface soils due to the placement of the dike beyond 20 years.

** - Internal Settlement of the Dike in 20 years.

Slope Stability Analysis of Containment Dike

Slope stability analysis was performed using Slope-W software to determine the factor of safety against failure for varying conditions and dike crown heights. The stability analysis was conducted for a containment dike crown width of 6 feet and 10 feet.

A dike configuration having a 10 feet crown width, a height of 5.0 feet, and 5H:1V side slopes will result in an overall dike base width of 60 feet. For dike configurations having an overall base width up to 60 feet, the dike was designed with the outside slope toe to be at the project boundary. For dike configurations having an overall base width greater than 60 feet, the dike was designed for the outside slope toe to be at a distance of 70 feet inside of the project boundary. The offset of the outer toe is required to provide access to construction equipment on both sides of the dike.

Based upon information provided by LDNR, we understand that approximately 300 linear feet of a typical containment dike can be constructed using one (1) soil excavator equipment in a single day. From the provided aerial photo of the site as shown on Test Location Plan, we estimate the perimeter of the project boundary to be approximately 27,000 linear feet. Therefore, we estimate it would approximately take 90 days to complete the first stage of dike construction around the site.

URS used the provided survey report performed by PBS&J, Inc. to locate the most critical transect profile from a total of 49 transects (T-1 to T-49) across the project site. The transect layout vicinity map can be seen in Figure 20 presented in Appendix G of this report. A stability check was performed using a minimum factor of safety of 1.3 for all analysis conditions. For the analysis, it was assumed that the fill soils used to construct the dike would be excavated from the existing site soils at least 25 feet away from the inside toe of the dike. The stability analysis was performed for dike side slopes of 4H:1V and 5H:1V, and considering a borrow excavation bottom extending to an elevation of -10 feet and -20 feet. In addition, considerations were also given in the stability analysis to the case of the channel being full or empty of water for the various dike configurations and fill heights. The complete results for the slope stability analyses are shown in Figures 21-74 in Appendix G with the distance in feet and Elevations in feet (NAVD). A summary of these results (global stability) are presented in Table 6 below.

An analysis for sliding failure was performed for the various dike configurations and fill heights and it was determined that an adequate factor of safety exists. A long term internal friction angle of the dike material was estimated to be 12 degrees. The hand-calculations for the sliding failure are presented in Appendix G of this report.

Containment Ridge along Channel Side Boundary

As requested by LDNR, we understand that a 6 feet height containment ridge is to be constructed instead of a dike along the channel side boundary. The proposed ridge location is shown on the Test Location Plan (Figure 2, Appendix A) and denoted as a red line. We understand the ridge will incorporate a crown width of 30 feet and side slopes of 4H to 1V. Slope stability analysis results indicate the ridge has an adequate Factor of Safety against failure except when the borrow excavation bottom is at an elevation of -20 feet. Figures 75-80 in Appendix G show the various conditions analyzed and types of slope failure for the 6 feet high ridge. Settlement curves of the ridge are presented on Figures 81-84 in Appendix H. The ridge settlements were analyzed based upon two different conditions, with the mud-line at Elevation 0' (NAVD) and at Elevation -1.4 feet (NAVD).

Table 6: Stability Analysis of Dike (Side Slope - 5H:1V)					
Dike Ht (ft)	Fill Ht (ft)	Crown width - 6 feet		Crown width - 10 feet	
		Factor of Safety (Spencer's Method)		Factor of Safety (Spencer's Method)	
		Circular	Wedge	Circular	Wedge
4.0	3.0	1.78*	1.93	1.89*	2.03
5.0	4.0	1.41*	1.49	1.49*	1.60
6.0	5.0	1.22*	1.31	1.25*	1.34
Borrow Excavation Bottom at El. -10 ft (Without Fill Material)					
Dike Ht (ft)	Fill Ht (ft)	Crown width - 6 feet		Crown width - 10 feet	
		Factor of Safety (Spencer's Method)		Factor of Safety (Spencer's Method)	
		Circular	Wedge	Circular	Wedge
4.0	0.0	1.75*	1.85	2.04*	2.16
5.0	0.0	1.48*	1.57	1.69*	1.78
6.0	0.0	1.30*	1.37	1.41*	1.51
Borrow Excavation Bottom at El. -20 ft (Without Fill Material)					
Dike Ht (ft)	Fill Ht (ft)	Crown width - 6 feet		Crown width - 10 feet	
		Factor of Safety (Spencer's Method)		Factor of Safety (Spencer's Method)	
		Circular	Wedge	Circular	Wedge
4.0	0.0	1.54	1.49*	1.51	1.44*
5.0	0.0	1.40	1.35*	1.37	1.29*
6.0	0.0	1.28	1.25*	1.25	1.17*
Stability Analysis of Dike (Side Slope - 4H:1V)					
Dike Ht (ft)	Fill Ht (ft)	Crown width - 10 feet			
		Factor of Safety (Spencer's Method)			
		Circular		Wedge	
4.0	3.0	1.79*		1.89	
5.0	4.0	1.43*		1.52	
6.0	5.0	1.18*		1.26	
Borrow Excavation Bottom at El. -10 ft (Without Fill Material)					
Dike Ht (ft)	Fill Ht (ft)	Crown width - 10 feet			
		Factor of Safety (Spencer's Method)			
		Circular		Wedge	
4.0	0.0	1.85*		2.04	
5.0	0.0	1.56*		1.69	
6.0	0.0	1.35*		1.42	
Borrow Excavation Bottom at El. -20 ft (Without Fill Material)					
Dike Ht (ft)	Fill Ht (ft)	Crown width - 10 feet			
		Factor of Safety (Spencer's Method)			
		Circular		Wedge	
4.0	0.0	1.47		1.42*	
5.0	0.0	1.36		1.29*	
6.0	0.0	1.25		1.17*	
*** Controls the design**					

Bearing Capacity Evaluation

The nature of this project requires analysis of rather soft soils having low strength characteristics that are subject to shear failure when subjected to fill loadings. Based on the soil strength profile developed for the site, the uppermost layer of Organic Peat had the lowest shear strength and controlled the bearing capacity analysis. A moist unit weight of 116 pcf was used for dredged fill material and a unit weight of 71 pcf used for containment dike and ridge. The ultimate bearing capacity (Q_u) was calculated using the Terzaghi bearing capacity formula as shown in Equation 1.

$$Q_u = c' N_c + \sigma_{zd}' N_q + 0.5\gamma' B N_\gamma \quad (1)$$

The friction angle of the existing soil sub-layers was assumed to be zero (ϕ' = 0; N_c= 5.7, N_q= 1, N_γ= 0), and was also assumed that no surcharge acts on the fill or the dike (σ_{zd}' = 0). As requested by LDNR, the factor of safety for bearing failure is assumed to be 1.5. Thus, the net allowable soil bearing capacity (Q_{all}) can be calculated using Equation 2.

$$Q_{all} = 5.7c'/1.5 \quad (2)$$

An allowable soil bearing capacity of 285 psf for the existing soils was calculated using the lowest shear strength value (S_u = c' = 75psf) from the uppermost soil layer. Based on the allowable bearing capacity, the dike could be designed to a maximum height of 5.2 feet and the dredge fill could be placed to a maximum height of 3.2 feet in order to maintain an adequate Factor of Safety against bearing capacity failure. The calculation for the bearing capacity and the safe design heights are presented in Table 7 and the hand calculations are attached to Appendix I.

Table 7: Bearing Capacity Calculations

Bearing Capacity Check of Dredge Fill (Factor of Safety = 1.5)					Bearing Capacity Check of Dike (Factor of Safety = 1.5)				
Height of Fill (feet)	**Q_{ult} Psf**	**Q_{all} Psf**	**Max. Allow. Height* (feet)**	**Design Height**	**Height of Dike (feet)**	**Q_{ult} psf**	**Q_{all} psf**	**Max. Allow. Height* (feet)**	**Design Height**
2	427.5	285.0	3.2	SAFE	3	427.5	285.0	5.2	SAFE
2.5	427.5	285.0	3.2	SAFE	3.5	427.5	285.0	5.2	SAFE
3	427.5	285.0	3.2	SAFE	4	427.5	285.0	5.2	SAFE
4	427.5	285.0	3.2	Not Safe	5	427.5	285.0	5.2	SAFE
5	427.5	285.0	3.2	Not Safe	6	427.5	285.0	5.2	Not Safe
6	427.5	285.0	3.2	Not Safe	7	427.5	285.0	5.2	Not Safe

* - Maximum allowable height in feet

URS also performed the strength gain evaluation of the sub-layers using SHANSEP theory calculated using equation 3.

$$\Delta\sigma_{gain} = 0.23 * \sigma_v' * U \quad (3)$$

Where, $\Delta\sigma_{gain}$ is the strength gain in psf, σ_v' is the total vertical stress due to the fill (surcharge load) and U is the degree of consolidation of the soil sub-layers in percentage. The formula is derived

from the information provided by Ladd and Foott (1974) and from Ladd and DeGroot (2003). The coefficient 0.23 is taken as the average of the values provided and considered to be nominal for highly organic soils.

The strength gain of the soil sub-layers due to the placement of the dredged fill were estimated for both the actual and equivalent fill height and can be seen in Figure 85 and Figure 86 respectively in Appendix G. However, the calculated soil strength gain due to fill placement at this site was minimal.

Conclusions and Recommendations

Long-term settlement analyses were to be performed for the construction of an earthen dike around the site. Finite-Strain consolidation theory, 1-D Terzaghi consolidation theory and 1-D Terzaghi bearing capacity analysis were used to determine the maximum safe height of the earthen dike and dredge fill. The final 20 year dike crown elevations for various dike configurations (constructed height, side slope) were calculated and can be seen in Figures 12, 14, 16 and 18 presented in Appendix F. The bearing capacity calculations and the strength gain of the soil sub-layer due to the placement of the dredged fill were estimated for both the actual and equivalent fill height as can be seen in Figure 85 and Figure 86 respectively.

Results from the slope stability analysis, bearing capacity analysis, and settlement calculations show that a maximum construction elevation of +3.6 feet (NAVD) for the containment dike and +2.6 feet (NAVD) for the dredge fill material (assuming the existing mud-line elevation to be -1.4 feet NAVD) to provide an alternative for a dike/dredge fill elevation difference of at least 1 foot after 20 years. The final construction elevation for this alternative is shown in Figure 87 and is attached to Appendix I of this report. However, the bearing capacity Factor of Safety of 1.5 for the dredge fill is not obtained with this proposed dredge fill height.

Based on the survey report by PBS&J, Inc., transect T-17 had the deepest elevation of -1.91 feet at the boundary of the site, but our analysis was performed with the average mud-line at El. -1.4 feet (NAVD) from the top of the water surface assumed at El. 0' (NAVD). Additional fill materials would be required at this location in order to obtain final surface elevation.

We recommend that a geotechnical instrumentation program be incorporated with the final design and construction of this project. The instrumentation program should consist, as a minimum, of the installation of settlement plates, slope inclinometers, and piezometers at the project site. The instrumentation would be used to monitor settlements and stability of the existing soils and fill materials. In addition, we recommend a Cone Penetration Test (CPT) program consisting of soundings conducted throughout the construction area both before and after fill placement in order to allow for an evaluation of in-situ soil strength characteristics. The results of the instrumentation and CPT program would be used to more accurately develop modeling and analysis techniques and procedures for future projects.

Limitations

Professional judgments and recommendations are presented in this geotechnical investigation. They are based partly on the information provided, partly on evaluations of technical information gathered, and partly on our general experience with subsurface conditions in the area. The recommendations presented in this report are applicable only to this specific site and should not be used for other project sites. If any changes to the above mentioned recommendations are made

during construction phase URS should be consulted before the beginning of the construction.

Attached at the end of this report is a document entitled "Important Information about your Geotechnical Engineering Report," which is published by ASFE, The Association of Engineering Firms Practicing in the Geosciences, Appendix J. This document should be considered as part of the report and should be furnished to all persons who receive part or all of this report.

Very truly yours,

Ignacio Harrouch
Project Manager

Scott H. Slaughter, P.E
Principal Engineer

Ananth T. Bukkapatnam
Staff Geotechnical Engineer

Keun Y. Rhee
Staff Geotechnical Engineer

Mahendra Shewalla
Staff Geotechnical Engineer

STATE OF LOUISIANA
SCOTT H. SLAUGHTER
REG. No. 28165
REGISTERED
PROFESSIONAL ENGINEER
IN
ENGINEERING

IH/ABT/KYR/MS/SHS: hdm
Appendix A – Test Location Plan and Site Location Plan
Appendix B – Soil Boring Logs and Geological Profile
Appendix C – Laboratory Results
Appendix D – PSDDF Analysis by URS
Appendix E – PSDDF Analysis by Dr. Zhang
Appendix F – Dike Settlement Analysis and Hand Calculations.
Appendix G – Slope Stability Analysis and Hand Calculations
Appendix H – Ridge Design
Appendix I – Bearing Capacity calculations, Strength-gain plots, and Final Construction Elevation Drawing
Appendix J – ASFE Document

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APPENDIX A

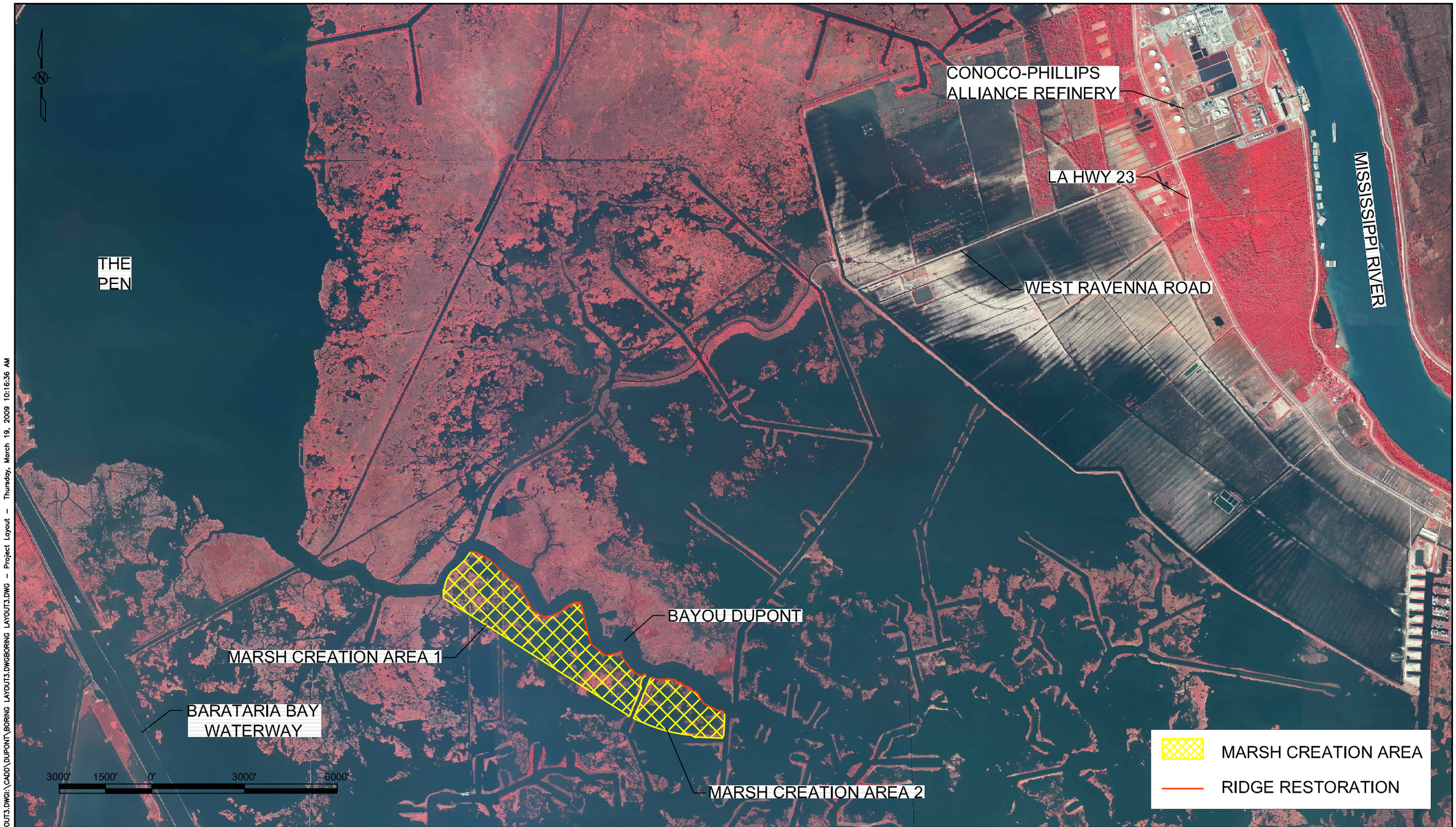

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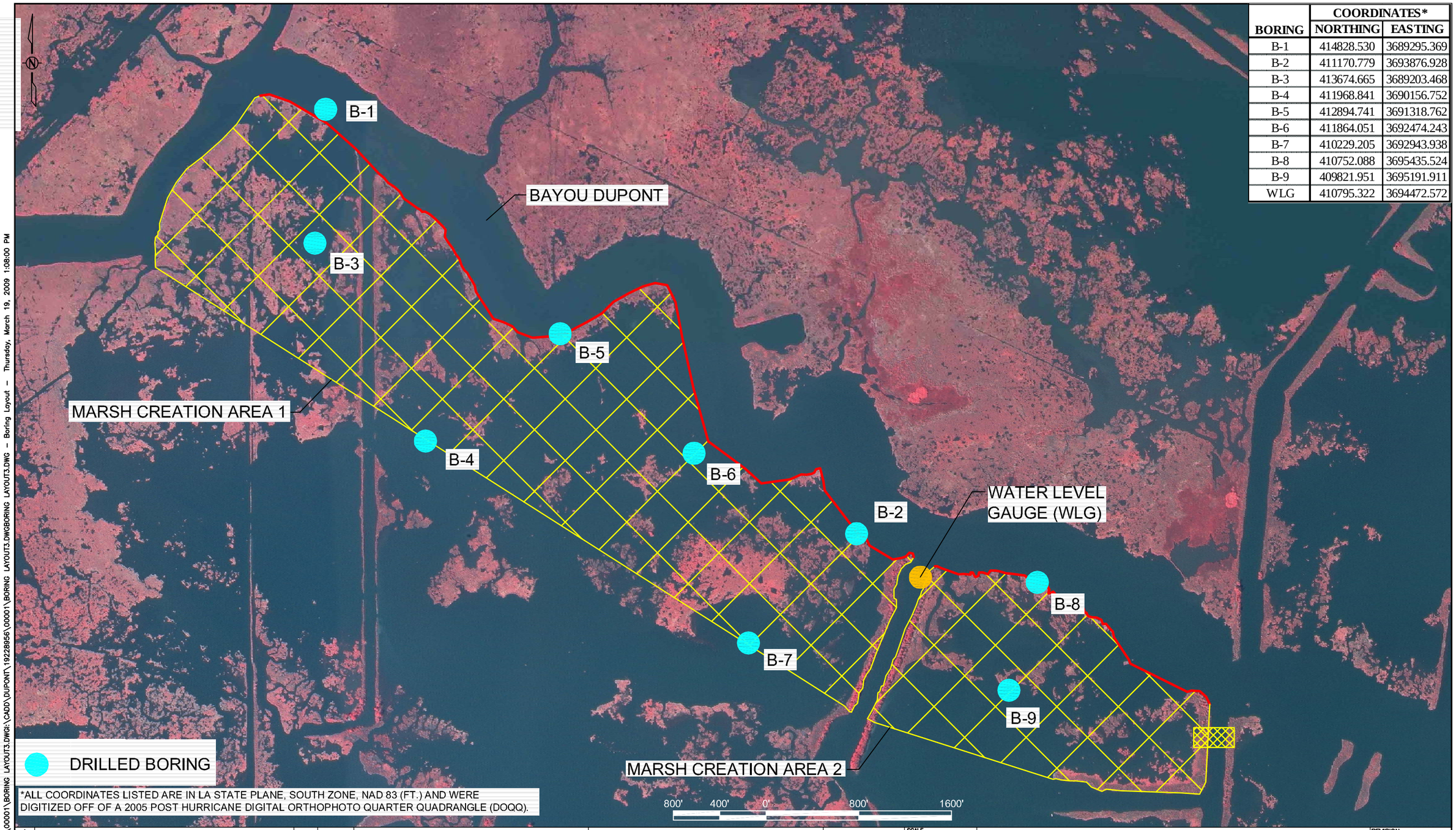
FIGURE	1



BORING	COORDINATES*	
	NORTHING	EASTING
B-1	414828.530	3689295.369
B-2	411170.779	3693876.928
B-3	413674.665	3689203.468
B-4	411968.841	3690156.752
B-5	412894.741	3691318.762
B-6	411864.051	3692474.243
B-7	410229.205	3692943.938
B-8	410752.088	3695435.524
B-9	409821.951	3695191.911
WLG	410795.322	3694472.572

DRILLED BORING

*ALL COORDINATES LISTED ARE IN LA STATE PLANE, SOUTH ZONE, NAD 83 (FT.) AND WERE DIGITIZED OFF OF A 2005 POST HURRICANE DIGITAL ORTHOPHOTO QUARTER QUADRANGLE (DOQQ).

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FIGURE	2

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DISTANCE ALONG PROFILE, feet

0 1,000 2,000 3,000 4,000 5,000 6,000 7,000 8,000

B-1 B-3 B-4 B-5 B-6 B-7 B-2 B-8 B-9

WATER SURFACE WATER SURFACE

MUD LINE

MARSH MARSH MARSH

NATURAL LEVEE

NATURAL LEVEE/ DISTRIBUTARY

NATURAL LEVEE/ DISTRIBUTARY

INTERDISTRIBUTARY INTERDISTRIBUTARY INTERDISTRIBUTARY

SILT ZONE (CREVASSE SPLAY)

SILT ZONE (CREVASSE SPLAY)

SILT/SILTY CLAY

INTERDISTRIBUTARY

CLAY

PRODELTA

ELEVATION, feet

5 0 -5 -10 -15 -20 -25 -30 -35 -40 -45 -50 -55 -60 -65

0 1,000 2,000 3,000 4,000 5,000 6,000 7,000 8,000

DISTANCE ALONG PROFILE, feet

WATER GAUGE ELEVATIONS

B-1 & B-3: -0.2 FT.
B-2, B-4, B-5, B-6, B-7, B-8 & B-9: +0.2 FT.

LEGEND

- ORGANICS W/CLAY
- CLAY
- SILTY CLAY
- SILT
- MARSH
- HIGH PLASTIC SILT

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GEOLOGICAL PROFILE

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PROJECT 19228956
FIGURE 3

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APPENDIX B

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-1

Sheet 1 of 2

Date(s) Drilled	**2/20/09 - 2/20/09**	Logged By	**A. Bukkapatnam**	Checked By	**I. Harrouch**
Drilling Method	**Rotary Wash**	Drill Bit Size/Type	**Bottom Discharge 4(5/8)"**	Total Depth Drilled (feet)	**31.8**
Drill Rig Type	**Marsh Buggy**	Drilling Contractor	**SESI**	Sampler Type(s)	**Piston Sampler/ Shelby Tube**
Groundwater Level and Date Measured	**-0.2' 2/20/2009**	Hammer Data	**140 LBS Safety**	Approximate Surface Elevation	**-0.2'**
Location	**N414828.534 E3689295.369**			Borehole Backfill	**Cement Grout**

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
	0						WATER MUDLINE El. -2.03'							
			ST-1	20			ORGANICS with Clay (OH)			607				
-5	5		ST-2	15			Very Soft, Brown to Black HUMUS with Clay (OH)*		0.10	305	21	0.08	618	395
			ST-3	15			Very Soft, CLAY with Organics (CH - OH)			230	24	0.06	202	150
			ST-4	22			Very Soft, Gray Lean CLAY (CL)*		0.75	64	72	0.15	46	20
-10	10		ST-5	22			Very Soft, Gray SILT with Clay, Organics and trace Fine Sand (CL-ML)*		0.25	54	74	0.17	43	18
-15	15		ST-6	22			Very Soft, Gray CLAY with Silt (CH)		0.25	88	55	0.12		
-20	20		ST-7	15			Very Soft, Gray fat CLAY (CH)*		0.25	87	47	0.20	85	54
-25	25		ST-8	15			Very Soft, Gray CLAY with trace Organic Pockets (CH)*		0.25	79	56	0.08		

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-1

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-30	30	ST-9	20				Soft, Gray fat CLAY (CH)*		0.50	75	61	0.26	92	60
							Bottom of hole @ 30 feet below MUDLINE * - Look at Table: Boring B - 1 for additional Laboratory Results							
-35	35													
-40	40													
-45	45													
-50	50													
-55	55													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-2

Sheet 1 of 2

Date(s) Drilled	**2/19/09 - 2/19/09**	Logged By	**A. Bukkapatnam**	Checked By	**I. Harrouch**
Drilling Method	**Rotary Wash**	Drill Bit Size/Type	**Bottom Discharge 4(5/8)"**	Total Depth Drilled (feet)	**31.5**
Drill Rig Type	**Marsh Buggy**	Drilling Contractor	**SESI**	Sampler Type(s)	**Piston Sampler/ Shelby Tube**
Groundwater Level and Date Measured	**0.2' 2/19/2009**	Hammer Data	**140 LBS Safety**	Approximate Surface Elevation	**0.2'**
Location	**N411170.779 E3693876.982**			Borehole Backfill	**Cement Grout**

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
0	0						WATER MUDLINE El. -1.3'							
			ST-1	20			ORGANICS with Clay (OH)			915				
-5	5		ST-2	20			Very Soft, Brown ORGANICS with Clay and Peat (OH)*		0.25	475	12	0.12	400	254
			ST-3	20			Very Soft, Gray and Black CLAY with Organics and Silt traces (CH)*		0.25	204	27	0.13		
			ST-4	22			Very Soft, Gray CLAY with Organic pockets (CH)		0.25	95	50	0.06	123	90
-10	10		ST-5	18			Very Soft, Gray CLAY with Organics (CH)*		0.25	88	52	0.07	97	70
-15	15		ST-6	18			Very Soft, Gray CLAY with Organic pockets (CH)		0.25	141	36	0.07	144	104
-20	20		ST-7	20			Very Soft, Gray CLAY with Silt (CH)		0.50	50	75	0.14	58	36
-25	25		ST-8	16			Very Soft, Gray CLAY with Silt pockets and Organics (CH)*		0.25	98	51	0.11		

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-2

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-30	30	ST-9	20				Very Soft, Gray CLAY with Silt and Organics (CH)		1.00	42	69	0.12	78	53
							Bottom of hole @ 30 feet below MUDLINE * - Look at Table: Boring B - 2 for additional Laboratory Results							
-35	35													
-40	40													
-45	45													
-50	50													
-55	55													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-3

Date(s) Drilled	**2/20/09 - 2/20/09**	Logged By	**A. Bukkapatnam**	Checked By	**I. Harrouch**
Drilling Method	**Rotary Wash**	Drill Bit Size/Type	**Bottom Discharge 4(5/8)"**	Total Depth Drilled (feet)	**40.7**
Drill Rig Type	**Marsh Buggy**	Drilling Contractor	**SESI**	Sampler Type(s)	**Piston Sampler/ Shelby Tube**
Groundwater Level and Date Measured	**-0.2' 2/20/2009**	Hammer Data	**140 LBS Safety**	Approximate Surface Elevation	**-0.2'**
Location	**N413674.665 E3689203.468**			Borehole Backfill	**Cement Grout**

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
	0						WATER MUDLINE El. -0.87'							
			ST-1	14			PEAT (PT)*			1171			996	644
			ST-2	12			Very Soft, Black PEAT with Clay (PT)*		0.25	383		0.12		
-5	5		ST-3	18			Very Soft, Gray CLAY with Organic pockets (CL)*			171		0.06	141	102
			ST-4	18			Very Soft, Gray Lean CLAY with trace Organics (CL)*		0.25	43		0.14		
-10	10		ST-5	16			Very Soft, Gray Lean Clay (CL - ML)*		0.50	46		0.07	45	15
-15	15		ST-6	12			Very Soft, Gray CLAY with Silt, Shells and Organics (CH)*		0.50	90		0.08	126	104
-20	20		ST-7	18			Very Soft, Gray Clay becoming Organic Peat and Clay (CH)		0.50	230		0.11		
-25	25		ST-8	18			Very Soft, Gray CLAY with Organics (CH)*			100		0.13	108	81

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-3

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-30	30		ST-9	20			Loose, Gray Silt with Fine Sand and trace Clay (ML)*			33		0.38		
-35	35		ST-10	18			Gray Sandy Silt with Clay pockets (ML)*			26		5.12	NP	NP
-40	40		ST-11	20			Loose, Gray Sandy Silt with trace Clay (ML)			27		0.26	NP	NP
							Bottom of hole @ 40 feet below MUDLINE * - Look at Table: Boring B - 3 for additional Laboratory Results							
-45	45													
-50	50													
-55	55													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-4

Sheet 1 of 2

Date(s) Drilled	**2/17/09 - 2/17/09**	Logged By	**A. Bukkapatnam**	Checked By	**I. Harrouch**
Drilling Method	**Rotary Wash**	Drill Bit Size/Type	**Bottom Discharge 4(5/8)"**	Total Depth Drilled (feet)	**40.7**
Drill Rig Type	**Marsh Buggy**	Drilling Contractor	**SESI**	Sampler Type(s)	**Piston Sampler/ Shelby Tube**
Groundwater Level and Date Measured	**0.2' 2/17/2009**	Hammer Data	**140 LBS Safety**	Approximate Surface Elevation	**0.2'**
Location	**N411968.841 E3690156.752**			Borehole Backfill	**Cement Grout**

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
0	0						WATER MUDLINE El. -0.47'							
			ST-1				PEAT with Clay *			860			958	427
			ST-2				Very Soft, Dark Gray CLAY with Organic pockets (OH)*			333	17	0.11	482	386
-5	5		ST-3				Very Soft, Gray CLAY with Organic pockets (CH)			80	56	0.07	122	83
			ST-4				Very Soft, Gray CLAY with Organic pockets and trace Shells (CH)*			72	49	0.06	64	41
-10	10		ST-5				Very Soft CLAY with Silt, Organic pockets and Shells (CH)*			90	50	0.07		
-15	15		ST-6				Very Soft, Gray CLAY with Organic and Silty Clay (CH)*			114	45	0.10	91	58
-20	20		ST-7				Very Soft, Gray CLAY with Silt and Organic pockets (CH)*			91	50	0.09		
-25	25		ST-8				Very Soft, Gray CLAY with Organic pockets, Sandy Silt and Silty Sand layers (CH)*		0.25	97	57	0.10	101	62

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-4

Elevation feet	Depth, feet	SAMPLES Type	SAMPLES Number	SAMPLES Recovery, in.	SAMPLES Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
							Firm, Gray Clayey SILT (ML)							
-30	30		ST-9						0.25	30	92	0.87		
							Firm, Gray Sandy SILT with Clay (ML)*							
-35	35		ST-10						0.25	28	99	1.08	NP	NP
							Soft, Gray CLAY (CH)							
-40	40		ST-11						0.30	63	66	0.38	63	39
							Bottom of hole @ 40 feet below MUDLINE							
							* - Look at Table: Boring B - 4 for additional Laboratory Results							
-45	45													
-50	50													
-55	55													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-5

Date(s) Drilled	**2/16/09 - 2/17/09**	Logged By	**A. Bukkapatnam**	Checked By	**I. Harrouch**
Drilling Method	**Rotary Wash**	Drill Bit Size/Type	**Bottom Discharge 4(5/8)"**	Total Depth Drilled (feet)	**60.4**
Drill Rig Type	**Marsh Buggy**	Drilling Contractor	**SESI**	Sampler Type(s)	**Piston Sampler/ Shelby Tube**
Groundwater Level and Date Measured	**0.2' 2/17/2009**	Hammer Data	**140 LBS Safety**	Approximate Surface Elevation	**0.2'**
Location	**N412894.741 E3691318.762**			Borehole Backfill	**Cement Grout**

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
0	0						WATER MUDLINE El. -0.22'							
			ST-1	17			Very Soft PEAT (PT)			428	11	0.05		
			ST-2	24			PEAT with Clay and Organics (PT-OH)*			223			223	165
-5	5		ST-3	13			Very Soft, PEAT with Clay and Organics (PT-OH)*			334	17	0.07		
			ST-4	23			Very Soft Gray CLAY with Organic pockets (CH)			84	55	0.05	68	42
			ST-5	22			Very Soft Gray CLAY with Organic pockets and trace Silt pockets (CH)			62	64			
-10	10													
			ST-6	20			Very Soft, Gray Lean CLAY with Organics and Fine Sand (CH)*			117	39	0.08	78	42
-15	15													
			ST-7	22			Very Soft Gray CLAY with Organic pockets (CH)*			138	40	0.07		
-20	20													
			ST-8	23			Very Soft, Gray SILTY CLAY (CL)*			168	40	0.09	47	23
-25	25													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-5

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-30	30		ST-9	23			Very Soft, Gray CLAYEY Silt with Clay and Sand (CL-ML)			33	81	0.09	34	6
-35	35		ST-10	17			Alternating layers of Very Soft, Gray SILTY CLAY with Sand (CL)			47	72			
-40	40		ST-11	24			Loose Gray SILT with CLAY layers (ML)*			38	89	0.46	NP	NP
-45	45		ST-12	19			Medium, Gray CLAYEY Silt with Clay (CL-ML)*			32	95	0.60		
-50	50		ST-13	18			Very Soft to Soft Gray CLAY (CH)*			68	62	0.24	79	44
-55	55		ST-14	22			Very Soft to Soft, Gray CLAY with Silt pockets and trace Organics (CH)*			56	69	0.22		

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-5

Elevation feet	Depth, feet	SAMPLES Type	SAMPLES Number	SAMPLES Recovery, in.	SAMPLES Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-60	60		ST-15	15			Soft Gray CLAY with trace Organics (CH)*			53	74	0.38	67	42
							Bottom of hole @ 60 feet below MUDLINE * - Look at Table: Boring B - 5 for additional Laboratory Results							
-65	65													
-70	70													
-75	75													
-80	80													
-85	85													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-6

Sheet 1 of 3

Date(s) Drilled	**2/17/09 - 2/17/09**	Logged By	**A. Bukkapatnam**	Checked By	**I. Harrouch**
Drilling Method	**Rotary Wash**	Drill Bit Size/Type	**Bottom Discharge 4(5/8)"**	Total Depth Drilled (feet)	**62.2**
Drill Rig Type	**Marsh Buggy**	Drilling Contractor	**SESI**	Sampler Type(s)	**Piston Sampler/ Shelby Tube**
Groundwater Level and Date Measured	**0.2' 2/17/2009**	Hammer Data	**140 LBS Safety**	Approximate Surface Elevation	**0.2'**
Location	**N411864.051 E3692474.243**			Borehole Backfill	**Cement Grout**

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
0	0						WATER							
							MUDLINE El. -1.97'							
			ST-1	22			Very Soft, PEAT with Clay (PT)*			194	23		289	145
-5	5		ST-2	23			Very Soft, Brown Organic CLAY with Peat (PT/OH/CH)*			374	18	0.08		
			ST-3	18			Very Soft, Gray CLAY with Organic pockets (CH)*			123	43	0.07	120	76
			ST-4	19			Very Soft, Gray CLAY with Organic pockets (CH)							
-10	10		ST-5	22			Very Soft, Gray CLAY with Organic pockets (CH)*			99	52	0.10	67	33
-15	15		ST-6	22			Very Soft, Gray CLAY with Organic pockets (CH)			124	44			
-20	20		ST-7	12			Very Soft, Gray CLAY becoming Gray SANDY SILT with Clay (CH becoming ML)*			104	47	0.10		
-25	25													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-6

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
		ST	8	22			Very Soft, Gray CLAY becoming Gray SILT with Clay (CH)			83	63	0.16	130	90
-30	30	ST	9	22			Very Soft, Gray CLAY with Silt (CH)*			71	61	0.18		
-35	35	ST	10	21			Soft, Gray CLAY becoming Gray SILT with Clay (CH)*			46	84	0.36	83	52
-40	40	ST	11	10			Soft, Gray CLAY with trace Silt and Organics (CH)*			62	68			
-45	45	ST	12	23			Loose, Gray SILT with trace Organics, trace silt and silt lenses, with Clay (MH)*			50	76	0.33	55	22
-50	50	ST	13	22			Medium, Gray CLAY with Silt pockets (CH)			50	81	0.34		
-55	55													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-6

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
		ST	ST-14	19			Soft, Gray CLAY with trace Silt (CH)*			63	66	0.60		
-60	60	ST	ST-15	22			Soft, Gray CLAY with trace Silt (CH)*			71	64	0.46		
							Bottom of hole @ 60 feet below MUDLINE * - Look at Table: Boring B - 6 for additional Laboratory Results							
-65	65													
-70	70													
-75	75													
-80	80													
-85	85													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-7

Sheet 1 of 2

Date(s) Drilled	**2/17/09 - 2/17/09**	Logged By	**A. Bukkapatnam**	Checked By	**I. Harrouch**
Drilling Method	**Rotary Wash**	Drill Bit Size/Type	**Bottom Discharge 4(5/8)"**	Total Depth Drilled (feet)	**41.8**
Drill Rig Type	**Marsh Buggy**	Drilling Contractor	**SESI**	Sampler Type(s)	**Piston Sampler/ Shelby Tube**
Groundwater Level and Date Measured	**0.2' 2/17/2009**	Hammer Data	**140 LBS Safety**	Approximate Surface Elevation	**0.2'**
Location	**N410229.205 E3692943.938**			Borehole Backfill	**Cement Grout**

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
0	0						WATER MUDLINE El -1.63'							
			ST-1	20			Very Soft, PEAT with Clay pockets (PT)		<0.25	955	6	0.04	925	595
-5	5		ST-2	15			Very Soft, PEAT becoming Clay with Organics (PT)*		<0.25	309	18		384	284
			ST-3	22			Very Soft, Gray CLAY with Organics (CH)		<0.25	112	45	0.05		
			ST-4	18			Very Soft, Gray SILTY CLAY with trace Organics (CL)*		<0.25	90	52	0.06		
-10	10		ST-5	15			Very Soft, Gray CLAY with Humus, Organic layers and pockets (OH)*		<0.25	334	18	0.10	240	178
-15	15		ST-6	16			Very Soft, Intermixed Gray CLAY, SILT and SANDY SILT (CL to ML)		<0.25	55	70	0.08		
-20	20		ST-7	18			Soft, Gray SILTY CLAY with trace Organics (CL)*		0.25	48	83	0.29	43	22
-25	25		ST-8	18			Firm, CLAYEY SILT with trace Sand (ML)*		0.25	29	99	1.06		

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-7

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-30	30	ST	9	16			Very Soft, Gray CLAY with Silt streaks and trace Organics (CH)*		0.30	56	71	0.17	90	60
-35	35	ST	10	20			Soft, Gray CLAY becoming Gray SILT with Clay (CH)		0.35	25	99	0.24		
-40	40	ST	11	20			Soft, Gray SILTY CLAY with Sandy Silt (CL)		0.40	47	77	0.34	35	12
							Bottom of hole @ 40 feet below MUDLINE * - Look at Table: Boring B - 7 for additional Laboratory Results							
-45	45													
-50	50													
-55	55													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-8

Sheet 1 of 2

Date(s) Drilled	**2/19/09 - 2/19/09**	Logged By	**A. Bukkapatnam**	Checked By	**I. Harrouch**
Drilling Method	**Rotary Wash**	Drill Bit Size/Type	**Bottom Discharge 4(5/8)"**	Total Depth Drilled (feet)	**41.8**
Drill Rig Type	**Marsh Buggy**	Drilling Contractor	**SESI**	Sampler Type(s)	**Piston Sampler/ Shelby Tube**
Groundwater Level and Date Measured	**0.2' 2/19/2009**	Hammer Data	**140 LBS Safety**	Approximate Surface Elevation	**0.2'**
Location	**N410752.088 E3695435.524**			Borehole Backfill	**Cement Grout**

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
0	0						WATER MUDLINE El. -1.63'							
			ST-1	20			Very Soft, PEAT (PT)*			766	8	0.07		
-5	5		ST-2	20			Very Soft, PEAT with Clay pockets (PT)*		0.25	383	15	0.13		
			ST-3	22			Very Soft, Gray CLAY with Organic pockets (CH-OH)*		0.25	140	36	0.09	185	137
			ST-4	18			Very Soft, Gray CLAY with Organic pockets (CH)		0.25	117	44	0.06	96	63
-10	10		ST-5	18			Very Loose, Gray SILTY CLAY with Clay and Organic pockets (MH)*		0.25	130	40	0.05	87	36
-15	15		ST-6	16			Loose, Gray SILT with trace Sand and Silty Clay pockets (ML)*		0.25	50	75	0.82	NP	NP
-20	20		ST-7	22			Loose, Gray SILT with trace Fine Sand and Clay and Organic pockets (ML)*		0.75	29	96	0.98	NP	NP
-25	25		ST-8	18			Very Soft, Gray CLAY with Silt and Organics (CH)		0.50	107	46	0.13	107	71

Project: Bayou DuPont Marsh Restoration
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Log of Boring B-8

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
-30	30	ST	9	22			Very Soft, Gray CLAY with Silt pockets becoming Gray Silt with Clay (CH)*		0.75	60	64	0.09		
-35	35	ST	10	18			Loose, Gray SILT with Clay (CL-ML)*		0.25	62	66	0.40	34	9
-40	40	ST	11	18			Intermixed Gray CLAY and SILT with trace Sand and Organics (CL-ML)*		0.50	32	85	0.14		
-45	45						End of hole @ 40 feet below MUDLINE * - Look at Table: Boring B - 8 for additional Laboratory Results							
-50	50													
-55	55													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-9

Date(s) Drilled	**2/19/09 - 2/19/09**	Logged By	**A. Bukkapatnam**	Checked By	**I. Harrouch**
Drilling Method	**Rotary Wash**	Drill Bit Size/Type	**Bottom Discharge 4(5/8)"**	Total Depth Drilled (feet)	**62.8**
Drill Rig Type	**Marsh Buggy**	Drilling Contractor	**SESI**	Sampler Type(s)	**Piston Sampler/ Shelby Tube**
Groundwater Level and Date Measured	**0.2' 2/19/2009**	Hammer Data	**140 LBS Safety**	Approximate Surface Elevation	**0.2'**
Location	**N409821.951 E3695191.911**			Borehole Backfill	**Cement Grout**

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
0	0						WATER MUDLINE El. -2.63'							
			ST-1	20"			PEAT (PT)			894	6			
-5	5		ST-2	12"			Very Soft, PEAT with Clay and Organics (PT)*			255	20	0.06	257	173
			ST-3	18"			Very Soft, Gray CLAY with Organics (CH)*		0.25	135	36	0.11		
-10	10		ST-4	20"			PEAT with Clay pockets and Silt pockets (PT)*		0.25	334	17	0.17	573	427
			ST-5	18"			Very Soft, SILTY CLAY with Organics (CL)*		0.25	205	22	0.05		
			ST-6	18"			Very Soft, Gray CLAY with trace Silt and Organic pockets (CH)*		0.50	60	62	0.08	65	39
-15	15		ST-7	20"			Very Soft, Gray CLAY with trace Organic pockets (CH)		0.25	59	72	0.15		
			ST-8	18"			Very Soft, Gray CLAY with Silt and trace Organic (CH)		0.25	49	81	0.13	54	26
-20	20		ST-9	20"			Loose, Gray SILT with clay pockets and trace Fine Sand (ML)		0.75	34	87	0.53		
			ST-10	22"			Firm, Gray SILT with trace Fine Sand and Clay (ML)*		0.25	25	95	2.94	NP	NP
			ST-11	18"			Very Soft, Gray CLAY with Silt lenses (CH)		0.25	98	51	0.10		
-25	25													

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-9

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
		ST	ST-12	18"			Soft, Gray CLAY with Silt pockets (CH)*		0.25	51	67		66	39
		ST	ST-13	18"			Very Soft, Gray CLAY with Silt (CH)*		0.25	80	58	0.11		
-30	30	ST	ST-14	22"			Soft, Gray CLAY with Silt pockets (CH)		0.25	64	62			
		ST	ST-15	16"			Very Soft, Gray CLAY with trace Silt and trace Organics (CH)*		0.50	71	60	0.14	72	45
		ST	ST-16	20"			Loose, Gray SANDY SILT with Clay pockets (ML)		0.50	30	94			
-35	35	ST	ST-17	16"			Soft, Intermixed CLAY and SANDY SILT (CL-ML)		0.75	39	82	0.48	38	7
		ST	ST-18	20"			Soft, Gray SILT with CLAY pockets (ML)*		0.25	43	78			
-40	40	ST	ST-19	16"			Soft, Gray SILT with CLAY pockets (ML)		0.25	55	66	0.31	86	52
		ST	ST-20	16"			Soft, Gray SILT with CLAY pockets and layers (ML)		0.50	53	68			
		ST	ST-21	16"			Very Soft, Gray CLAY with trace Silt (CH)		0.50	63	64	0.15		
-45	45	ST	ST-22	18"			Very Soft, Gray CLAY with Silt pockets (CH)		0.25	54			60	34
		ST	ST-23	18"			Soft, Gray CLAY with Sandy Silt pockets (CH)*		0.25	58	65			
-50	50	ST	ST-24	22"			Very Soft, Gray CLAY with Silt pockets (CH)		0.25	57	67	0.19	52	31
		ST	ST-25	12"			Sandy Clayey SILT (ML)*		0.25	34				
		ST	ST-26	22"			Medium, Gray CLAY with Silt pockets (CH)		0.50	43	76	0.46	56	30
-55	55	ST	ST-27	22"			Very Soft, Gray CLAY with trace Silt and Organics (CH)		0.75					

Project: Bayou DuPont Marsh Restoration
Project Location: Jefferson Parish, Louisiana
Project Number: 19228956.00001

Log of Boring B-9

Elevation feet	Depth, feet	SAMPLES Type	Number	Recovery, in.	Sampling Resistance, blows / ft	Graphic Log	MATERIAL DESCRIPTION	Torvane (tsf)	Hand Penetrometer (tsf)	Water Content, %	Dry Unit Weight, pcf	Cohesion (ksf)	Liquid Limit, %	Plastic Index, %
			ST-28	22"			Soft, Gray CLAY with Silt (CH)*		0.50	59	67	0.36	76	49
-60	60		ST-29	20"			Soft to Medium, Gray CLAY (CH)		0.50	58				
			ST-30	18"			Very Soft, CLAY with trace Silt (CH)*		0.50	57	66	0.15	69	43
							Bottom of the hole @ 60 feet below mudline							
							* - Look at Table: Boring B - 9 for additional Laboratory Results							
-65	65													
-70	70													
-75	75													
-80	80													
-85	85													

APPENDIX C

LABORATORY RESULTS SHEET

URS

TABLE : Boring B - 1

SAMPLE DESIGNATION		INDEX TESTS (ASTM Designation)								STRENGTH TESTS			GRAIN SIZE DISTRIBUTION			CONSOLIDATION TESTS						USCS
		D2216	D2166	D854	D2974	D4318			D427	D2166	D2850		D422, C136 or C117			D2435						
Boring	Depth from Mudline (feet)	Moisture Content, ω (%)	Dry Unit Weight, γ_d (pcf)	Specific Gravity G_s	Organic Content (%)	Atterberg Limits (%)				UC (ksf)	UU (ksf)	σ_3 (psi)	Sand (%)	Silt (%)	Clay (%)	e_0	σ_c' (psf)	C_c	C_r	C_v	C_α	
						LL	PL	PI	SL													
B-1	0-2	607.1																				OH
B-1	2-4	305.0	20.6	2.00	23.6	618	223	395		0.077												OH
B-1	4-6	230.0	23.8			202	52	150			0.061	2.0				4.599						CH-OH
B-1	6-8	63.8	72.0			46	26	20		0.146			0.8	57.6	41.6							CL
B-1	8-10	54.1	74.3	2.71	2.4	43	25	18	23.4		0.170	3.3	2.1	81.6	16.3							CL-ML
B-1	13-15	87.5	54.6							0.118												CH
B-1	18-20	87.1	47.0			85	31	54			0.204	6.6	0.2	39.1	60.7							CH
B-1	23-25	78.9	56.4		2.8					0.083												CH
B-1	28-30	75.0	61.4			92	32	60			0.256	9.9	0.4	27.7	71.9							CH

Remarks:

NP - Non-Plastic; LL - Liquid Limit; PL - Plastic Limit; PI - Plasticity Index; SL - Shrinkage Limit

e_0 - Initial Void Ratio ; C_c - Compression Index ; C_r - Recompression Index ; C_v - Consolidation Coefficient ; C_α - Secondary Compression Coefficient

σ_3 - Cell / Confining Pressure ; σ_c' - Pre-Consolidation Pressure

The results were obtained from the Laboratory Testing Results provided by Southern Earth Sciences, Inc.	**The results presented only relate to those samples tested**	**Date : 06-05- 2009**

LABORATORY RESULTS SHEET

URS

TABLE : Boring B - 2

SAMPLE DESIGNATION		INDEX TESTS (ASTM Designation)								STRENGTH TESTS			GRAIN SIZE DISTRIBUTION			CONSOLIDATION TESTS						USCS
		D2216	D2166	D854	D2974	D4318			D427	D2166	D2850		D422, C136 or C117			D2435						
Boring	Depth from Mudline (feet)	Moisture Content, ω (%)	Dry Unit Weight, γ_d (pcf)	Specific Gravity G_s	Organic Content (%)	Atterberg Limits (%)				UC (ksf)	UU (ksf)	σ_3 (psi)	Sand (%)	Silt (%)	Clay (%)	e_0	σ_c' (psf)	C_c	C_r	C_v	C_α	
						LL	PL	PI	SL													
B-2	0-2	915.0																				OH
B-2	2-4	475.0	12.2	1.980	32.0	400	146	254	13.6	0.117												OH
B-2	4-6	203.7	27.4								0.125	2.0	2.5	18.5	79.0							CH
B-2	6-8	94.9	50.0			123	33	90		0.056												CH
B-2	8-10	88.2	52.4	2.786	5.2	97	27	70	21.3		0.071	3.3	3.5	50.7	45.8							CH
B-2	13-15	141.4	36.4			144	40	104		0.068						2.367						CH
B-2	18-20	50.0	75.3			58	22	36			0.137	6.6	3.3	74.0	22.7							CH
B-2	23-25	98.0	50.5		5.0					0.111												CH
B-2	28-30	41.5	69.4			78	25	53			0.117	9.9	1.1	53.2	45.7							CH

Remarks:

NP - Non-Plastic; LL - Liquid Limit; PL - Plastic Limit; PI - Plasticity Index; SL - Shrinkage Limit

e_0 - Initial Void Ratio ; C_c - Compression Index ; C_r - Recompression Index ; C_v - Consolidation Coefficient ; C_α - Secondary Compression Coefficient

σ_3 - Cell / Confining Pressure ; σ_c' - Pre-Consolidation Pressure

The results were obtained from the Laboratory Testing Results provided by Southern Earth Sciences, Inc.	**The results presented only relate to those samples tested**	**Date : 06-05- 2009**

LABORATORY RESULTS SHEET

URS

TABLE : Boring B - 3

SAMPLE DESIGNATION		INDEX TESTS (ASTM Designation)								STRENGTH TESTS			GRAIN SIZE DISTRIBUTION			CONSOLIDATION TESTS						USCS
		D2216	D2166	D854	D2974	D4318			D427	D2166	D2850		D422, C136 or C117			D2435						
Boring	Depth from Mudline (feet)	Moisture Content, ω (%)	Dry Unit Weight, γ_d (pcf)	Specific Gravity G_s	Organic Content (%)	Atterberg Limits (%)				UC (ksf)	UU (ksf)	σ_3 (psi)	Sand (%)	Silt (%)	Clay (%)	e_0	σ_c' (psf)	C_c	C_r	C_v	C_α	
						LL	PL	PI	SL													
B-3	0-2	1171.0			63.2	996	352	644														PT
B-3	2-4	383.3	14.7						16.6		0.118	1.3										CL
B-3	4-6	171.4	34.1	2.792		141	39	102		0.064												CL
B-3	6-8	43.0	82.6		1.5						0.141	2.6										CL
B-3	8-10	46.3	72.5			45	30	15	23	0.074			1.2	73.7	25.1							CL-ML
B-3	13-15	89.7	51.8	2.778		126	22	104			0.076	5.0	2.5	55.3	42.2							CH
B-3	18-20	230.3	25.0							0.112												CH
B-3	23-25	100.0	46.0			108	27	81			0.133	8.2	0.3	18.5	81.2							CH
B-3	28-30	33.3	90.6							0.379												ML
B-3	33-35	26.2	103.3			NP	NP	NP			5.115	11.5	33.4	63.3	3.3	0.744						ML
B-3	38-40	26.5	95.1			NP	NP	NP		0.262												ML

Remarks:

NP - Non-Plastic; LL - Liquid Limit; PL - Plastic Limit; PI - Plasticity Index; SL - Shrinkage Limit

e_0 - Initial Void Ratio ; C_c - Compression Index ; C_r - Recompression Index ; C_v - Consolidation Coefficient ; C_α - Secondary Compression Coefficient

σ_3 - Cell / Confining Pressure ; σ_c' - Pre-Consolidation Pressure

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LABORATORY RESULTS SHEET

URS

TABLE : Boring B - 4

SAMPLE DESIGNATION		INDEX TESTS (ASTM Designation)								STRENGTH TESTS			GRAIN SIZE DISTRIBUTION			CONSOLIDATION TESTS						USCS
		D2216	D2166	D854	D2974	D4318			D427	D2166	D2850		D422, C136 or C117			D2435						
Boring	Depth from Mudline (feet)	Moisture Content, ω (%)	Dry Unit Weight, γ_d (pcf)	Specific Gravity G_s	Organic Content (%)	Atterberg Limits (%)				UC (ksf)	UU (ksf)	σ_3 (psi)	Sand (%)	Silt (%)	Clay (%)	e_0	σ_c' (psf)	C_c	C_r	C_v	C_α	
						LL	PL	PI	SL													
B-4	0-2	860.0			64.3	958	531	427														PT
B-4	2-4	333.3	17.0			482	96	386	11		0.106	1.3										OH
B-4	4-6	80.4	56.4			122	39	83		0.070												CH
B-4	6-8	71.9	47.9	2.78	6.4	64	23	41			0.057	2.6	2.3	50.7	47.0							CH
B-4	8-10	89.6	50.0						4.5	0.071												CH
B-4	13-15	113.8	44.6			91	33	58			0.098	5.0	1.2	44.4	54.4							CH
B-4	18-20	91.4	50.1		4.1					0.094												CH
B-4	23-25	97.3	55.0	2.78	3.7	101	39	62	16.4		0.098	8.2	2.7	87.2	10.1	2.785						CH
B-4	28-30	30.0	92.0							0.869												ML
B-4	33-35	28.0	99.0			NP	NP	NP			1.076	11.5	12.6	77.2	10.2							ML
B-4	38-40	62.7	65.7			63	24	39		0.379												CH

Remarks:

NP - Non-Plastic; LL - Liquid Limit; PL - Plastic Limit; PI - Plasticity Index; SL - Shrinkage Limit

e_0 - Initial Void Ratio ; C_c - Compression Index ; C_r - Recompression Index ; C_v - Consolidation Coefficient ; C_α - Secondary Compression Coefficient

σ_3 - Cell / Confining Pressure ; σ_c' - Pre-Consolidation Pressure

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LABORATORY RESULTS SHEET

URS

TABLE : Boring B - 5

SAMPLE DESIGNATION		INDEX TESTS (ASTM Designation)								STRENGTH TESTS			GRAIN SIZE DISTRIBUTION			CONSOLIDATION TESTS						USCS
		D2216	D2166	D854	D2974	D4318			D427	D2166	D2850		D422, C136 or C117			D2435						
Boring	Depth from Mudline (feet)	Moisture Content, ω (%)	Dry Unit Weight, γ_d (pcf)	Specific Gravity G_s	Organic Content (%)	Atterberg Limits (%)				UC (ksf)	UU (ksf)	σ_3 (psi)	Sand (%)	Silt (%)	Clay (%)	e_0	σ_c' (psf)	C_c	C_r	C_v	C_α	
						LL	PL	PI	SL													
B-5	0-2	427.9	10.9								0.045	0.7										PT
B-5	2-4	223.4		2.399	14.5	223	58	165														PT-OH
B-5	4-6	334.1	16.9			NP	NP	NP	22.0		0.070	2.0	3.5	23.0	73.5							PT-OH
B-5	6-8	84.4	55.3			68	26	42		0.048												CH
B-5	8-10	61.6	64.2	2.792																		CH
B-5	13-15	117.1	38.7		8.6	78	36	42	16.0	0.080			22.0	31.3	46.7	2.633						CH
B-5	18-20	138.2	39.5								0.065	6.6	8.3	32.2	59.5							CH
B-5	23-25	167.9	40.3	2.762	11.5	47	24	23	26.1	0.094												CH
B-5	28-30	33.3	81.1			34	28	6			0.092	9.9										CL-ML
B-5	33-35	46.7	71.6																			CH-CL
B-5	38-40	37.7	88.9			NP	NP	NP		0.456			13.3	81.0	5.7							ML
B-5	43-45	31.6	94.9	2.684	1				15.3		0.604	14.8										CL-ML
B-5	48-50	67.9	61.7			79	35	44		0.238				22.1	77.9							CH
B-5	53-55	55.9	68.7								0.224	18.1										CH
B-5	58-60	52.7	73.7			67	25	42	16.3	0.377				38.9	61.1							CH

Remarks:

NP - Non-Plastic; LL - Liquid Limit; PL - Plastic Limit; PI - Plasticity Index; SL - Shrinkage Limit

e_0 - Initial Void Ratio ; C_c - Compression Index ; C_r - Recompression Index ; C_v - Consolidation Coefficient ; C_α - Secondary Compression Coefficient

σ_3 - Cell / Confining Pressure ; σ_c' - Pre-Consolidation Pressure

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LABORATORY RESULTS SHEET

URS

TABLE : Boring B - 6

SAMPLE DESIGNATION		INDEX TESTS (ASTM Designation)								STRENGTH TESTS			GRAIN SIZE DISTRIBUTION			CONSOLIDATION TESTS						USCS
		D2216	D2166	D854	D2974	D4318			D427	D2166	D2850		D422, C136 or C117			D2435						
Boring	Depth from Mudline (feet)	Moisture Content, ω (%)	Dry Unit Weight, γ_d (pcf)	Specific Gravity G_s	Organic Content (%)	Atterberg Limits (%)				UC (ksf)	UU (ksf)	σ_3 (psi)	Sand (%)	Silt (%)	Clay (%)	e_0	σ_c' (psf)	C_c	C_r	C_v	C_α	
						LL	PL	PI	SL													
B-6	0-2	194.0	22.6		8.4	289	144	145	26.4													PT
B-6	2-4	374.2	17.5								0.083	1.3	xx	xx	xx							PT/OH
B-6	4-6	122.8	42.8	2.797	4.8	120	44	76			0.066	2.0										CH
B-6	6-8																					CH
B-6	8-10	98.9	52.3		4.2	67	34	33			0.099	3.3	1.9	45.6	52.5							CH
B-6	13-15	123.5	44.2	2.798																		CH
B-6	18-20	104.0	47.2						20.0		0.100	6.6	0.0	30.2	69.8							CH
B-6	23-25	83.1	63.2			130	40	90			0.163	8.2										CH
B-6	28-30	70.6	60.9	2.774					17.0		0.176	9.9										CH
B-6	33-35	45.9	83.6			83	31	52			0.361	11.5	0.0	39.1	60.9							CH
B-6	38-40	61.5	67.8		2.1																	CH
B-6	43-45	49.5	76.4			55	33	22			0.335	14.9	0	45.3	54.7							MH
B-6	48-50	50.4	80.5								0.338	16.5										CH
B-6	53-55	63	66			82	31	51	20.4		0.603	18.2	0.0	41.9	58.1	1.462						CH
B-6	58-60	70.8	63.8		4.5						0.457	19.7										CH

Remarks:

NP - Non-Plastic; LL - Liquid Limit; PL - Plastic Limit; PI - Plasticity Index; SL - Shrinkage Limit

e_0 - Initial Void Ratio ; C_c - Compression Index ; C_r - Recompression Index ; C_v - Consolidation Coefficient ; C_α - Secondary Compression Coefficient

σ_3 - Cell / Confining Pressure ; σ_c' - Pre-Consolidation Pressure

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LABORATORY RESULTS SHEET

URS

TABLE : Boring B - 7

SAMPLE DESIGNATION		INDEX TESTS (ASTM Designation)								STRENGTH TESTS			GRAIN SIZE DISTRIBUTION			CONSOLIDATION TESTS						USCS
		D2216	D2166	D854	D2974	D4318			D427	D2166	D2850		D422, C136 or C117			D2435						
Boring	Depth from Mudline (feet)	Moisture Content, ω (%)	Dry Unit Weight, γ_d (pcf)	Specific Gravity G_s	Organic Content (%)	Atterberg Limits (%)				UC (ksf)	UU (ksf)	σ_3 (psi)	Sand (%)	Silt (%)	Clay (%)	e_0	σ_c' (psf)	C_c	C_r	C_v	C_α	
						LL	PL	PI	SL													
B-7	0-2	955.0	5.6			925	330	595			0.042	0.7										PT
B-7	2-4	308.8	18.0	2.400	20.6	384	100	284	20.1				0.0	21.0	79.0							PT
B-7	4-6	112.3	45.3								0.050	2.0										CH
B-7	6-8	89.8	51.8						16.7		0.060	2.6										CL
B-7	8-10	334.0	18.3	2.811	24.4	240	62	178			0.096	3.3										OH
B-7	13-15	54.9	70.2								0.083	5.0										CL
B-7	18-20	48.1	82.8		1.4	43	21	22			0.288	6.6	3.5	74.2	22.3							CL
B-7	23-25	28.9	98.7						23.7		1.058	8.3										ML
B-7	28-30	56.3	70.7			90	30	60			0.174	9.9	0.5	56.4	43.1	2.332						CH
B-7	33-35	25.1	99.2								0.235	11.6										CH
B-7	38-40	47.2	77.4			35	23	12			0.337	13.2										CL

Remarks:

NP - Non-Plastic; LL - Liquid Limit; PL - Plastic Limit; PI - Plasticity Index; SL - Shrinkage Limit

e_0 - Initial Void Ratio ; C_c - Compression Index ; C_r - Recompression Index ; C_v - Consolidation Coefficient ; C_α - Secondary Compression Coefficient

σ_3 - Cell / Confining Pressure ; σ_c' - Pre-Consolidation Pressure

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LABORATORY RESULTS SHEET

URS

TABLE : Boring B - 8

SAMPLE DESIGNATION		INDEX TESTS (ASTM Designation)								STRENGTH TESTS			GRAIN SIZE DISTRIBUTION			CONSOLIDATION TESTS						USCS
		D2216	D2166	D854	D2974	D4318			D427	D2166	D2850		D422, C136 or C117			D2435						
Boring	Depth from Mudline (feet)	Moisture Content, ω (%)	Dry Unit Weight, γ_d (pcf)	Specific Gravity G_s	Organic Content (%)	Atterberg Limits (%)				UC (ksf)	UU (ksf)	σ_3 (psi)	Sand (%)	Silt (%)	Clay (%)	e_0	σ_c' (psf)	C_c	C_r	C_v	C_α	
						LL	PL	PI	SL													
B-8	0-2	766.1	7.6		40.7						0.070	0.7										PT
B-8	2-4	382.5	14.7						34.9		0.125	1.3										PT
B-8	4-6	140.3	36.4	2.80		185	48	137			0.090	2.0	1.3	17.9	80.8							CH-OH
B-8	6-8	117.1	43.9		2.9	96	33	63			0.060	2.6										CH
B-8	8-10	129.8	40.4			87	51	36			0.053	3.3	1.9	45.2	52.9							MH
B-8	13-15	50.0	74.9			NP	NP	NP			0.817	5.0	29.4	62.4	8.2							ML
B-8	18-20	28.8	95.5		0.8	NP	NP	NP	20.1		0.976	6.6										ML
B-8	23-25	106.7	46.1			107	36	71			0.126	8.3										CH
B-8	28-30	60.1	63.7		2.4						0.090	9.9				0.891						CH
B-8	33-35	62.1	66.2	2.75		34	25	9	21.9		0.402	11.6	4.4	69.1	26.5							CL-ML
B-8	38-40	31.9	85.2								0.145	13.2										CL-ML

Remarks:

NP - Non-Plastic; LL - Liquid Limit; PL - Plastic Limit; PI - Plasticity Index; SL - Shrinkage Limit

e_0 - Initial Void Ratio ; C_c - Compression Index ; C_r - Recompression Index ; C_v - Consolidation Coefficient ; C_α - Secondary Compression Coefficient

σ_3 - Cell / Confining Pressure ; σ_c' - Pre-Consolidation Pressure

The results were obtained from the Laboratory Testing Results provided by Southern Earth Sciences, Inc.	**The results presented only relate to those samples tested**	**Date : 06-05- 2009**

LABORATORY RESULTS SHEET

URS

TABLE : Boring B - 9

SAMPLE DESIGNATION		INDEX TESTS (ASTM Designation)								STRENGTH TESTS			GRAIN SIZE DISTRIBUTION			CONSOLIDATION TESTS						USCS
		D2216	D2166	D854	D2974	D4318			D427	D2166	D2850		D422, C136 or C117			D2435						
Boring	Depth from Mudline (feet)	Moisture Content, ω (%)	Dry Unit Weight, γ_d (pcf)	Specific Gravity G_s	Organic Content (%)	Atterberg Limits (%)				UC (ksf)	UU (ksf)	σ_3 (psi)	Sand (%)	Silt (%)	Clay (%)	e_0	σ_c' (psf)	C_c	C_r	C_v	C_α	
						LL	PL	PI	SL													
B-9	0-2	893.5	5.9																			PT
B-9	2-4	255.1	20.3		15.1	257	84	173	4.9		0.060	1.3				6.504						PT
B-9	4-6	134.8	36.3								0.108	2.0	1.6	24.9	73.5							CH
B-9	6-8	334.4	16.8	2.21		573	146	427	15.7		0.173	2.6										PT
B-9	8-10	204.6	22.0		10.5						0.048	3.3	4.8	45.5	49.7							CL-ML
B-9	10-12	60.2	62.2			65	26	39	13.9		0.075	3.9										CH
B-9	12-14	58.9	72.0	2.78							0.148	4.6										CH
B-9	14-16	49.3	80.7			54	28	26			0.135	5.3	1.3	70.1	28.6							CH
B-9	16-18	33.9	86.9								0.534	6.0										ML
B-9	18-20	25.4	94.9		0.6	NP	NP	NP			2.936	6.6	4.6	52.6	4.8	0.811						ML
B-9	20-22	98.4	51.0								0.105	7.3										CH
B-9	22-24	50.9	67.1	2.8		66	27	39														CH
B-9	24-26	79.8	58.1								0.112	8.5	1.6	40.0	58.4							CH
B-9	26-28	64.4	61.9																			CH
B-9	28-30	71.2	59.9			72	27	45			0.142	9.9	0.6	84.8	14.8	1.964						CH

Remarks:

NP - Non-Plastic; LL - Liquid Limit; PL - Plastic Limit; PI - Plasticity Index; SL - Shrinkage Limit

e_0 - Initial Void Ratio ; C_c - Compression Index ; C_r - Recompression Index ; C_v - Consolidation Coefficient ; C_α - Secondary Compression Coefficient

σ_3 - Cell / Confining Pressure ; σ_c' - Pre-Consolidation Pressure

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LABORATORY RESULTS SHEET

URS

TABLE : Boring B - 9

SAMPLE DESIGNATION		INDEX TESTS (ASTM Designation)								STRENGTH TESTS			GRAIN SIZE DISTRIBUTION			CONSOLIDATION TESTS						USCS
		D2216	D2166	D854	D2974	D4318			D427	D2166	D2850		D422, C136 or C117			D2435						
Boring	Depth from Mudline (feet)	Moisture Content, ω (%)	Dry Unit Weight, γ_d (pcf)	Specific Gravity G_s	Organic Content (%)	Atterberg Limits (%)				UC (ksf)	UU (ksf)	σ_3 (psi)	Sand (%)	Silt (%)	Clay (%)	e_0	σ_c' (psf)	C_c	C_r	C_v	C_α	
						LL	PL	PI	SL													
B-9	30-32	30.0	93.6																			ML
B-9	32-34	38.5	82.4	2.65		38	31	7	19.1		0.484	11.2										CL-ML
B-9	34-36	42.8	78.2										0.6	72.9	26.5							ML
B-9	36-38	55.2	66.3			86	34	52			0.310	12.5				1.620						ML
B-9	38-40	53.1	67.8		2.8								0.0	73.3	26.7							ML
B-9	40-42	63.4	63.6								0.146	13.9										CH
B-9	42-44	53.8				60	26	34														CH
B-9	44-46	57.7	64.8		3.0				11.4				0.0	35.3	64.7							CH
B-9	46-48	57.3	67.2	2.80		52	21	31			0.191	15.9										CH
B-9	48-50	34.3											1.4	76.3	22.3							ML
B-9	50-52	43.0	76.1			56	26	30			0.458	17.2										CH
B-9	52-54																					CH
B-9	54-56	59	66.5			76	27	49			0.360	18.4	0.0	27.7	72.3	1.508						CH
B-9	56-58	57.9																				CH
B-9	58-60	57.4	65.6		2.3	69	26	43			0.153	19.7	0.0	30.2	69.8							CH

Remarks:

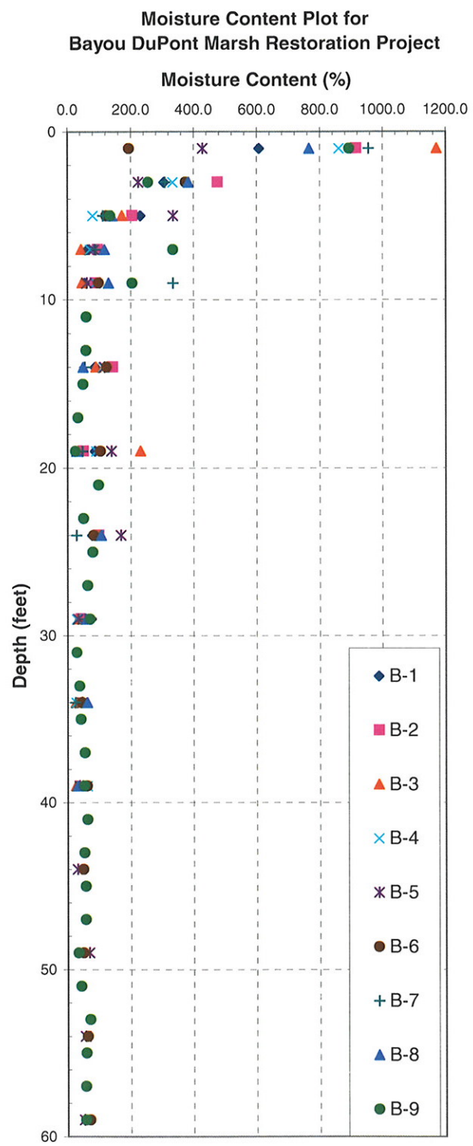
NP - Non-Plastic; LL - Liquid Limit; PL - Plastic Limit; PI - Plasticity Index; SL - Shrinkage Limit

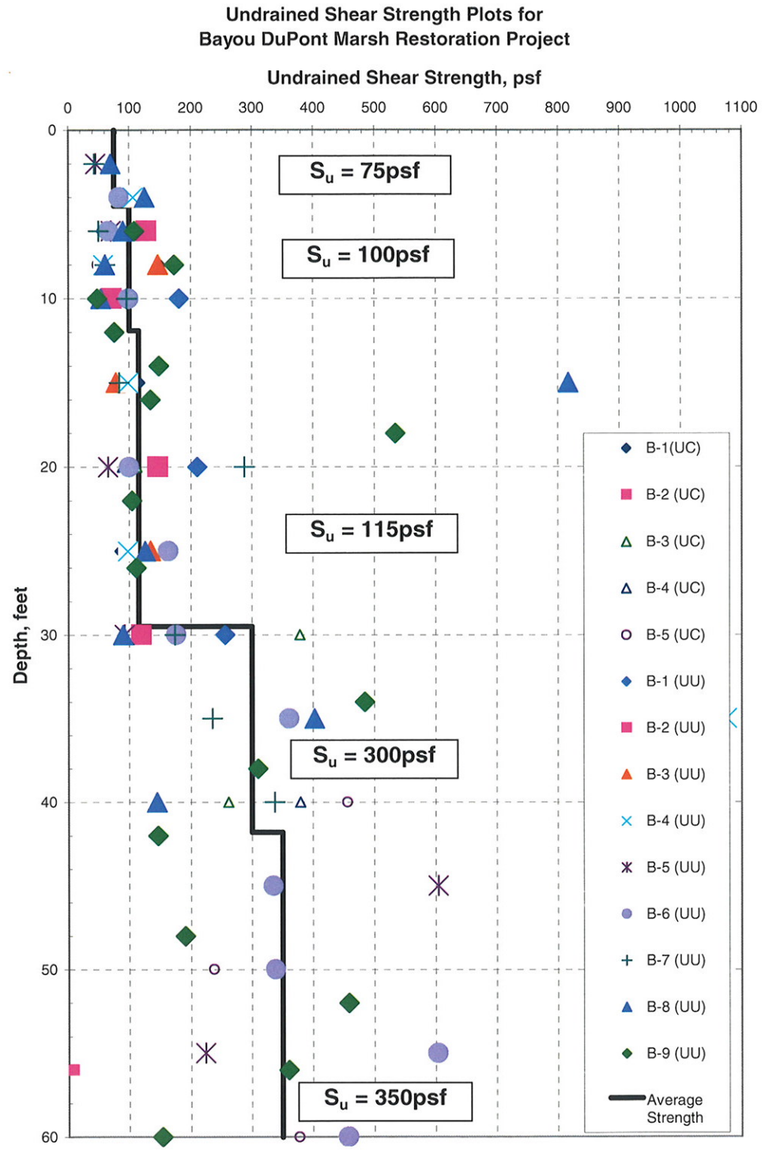
e_0 - Initial Void Ratio ; C_c - Compression Index ; C_r - Recompression Index ; C_v - Consolidation Coefficient ; C_α - Secondary Compression Coefficient

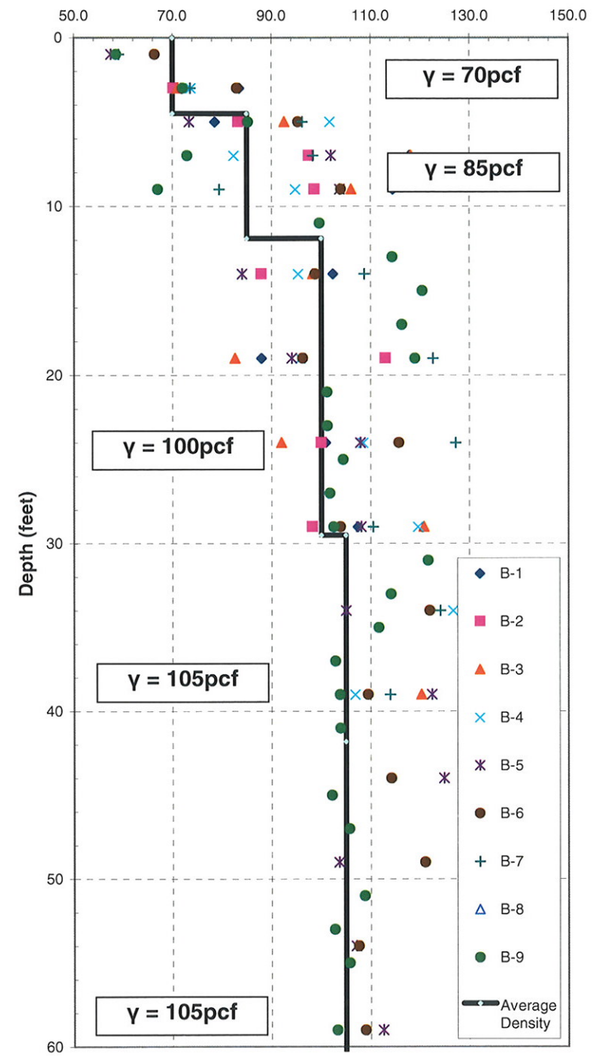
σ_3 - Cell / Confining Pressure ; σ_c' - Pre-Consolidation Pressure

The results were obtained from the Laboratory Testing Results provided by Southern Earth Sciences, Inc.	**The results presented only relate to those samples tested**	**Date : 06-05- 2009**

Borings used:
B-1
B-2
B-3
B-4
B-5
B-6
B-7
B-8
B-9







Bayou DuPont Marsh Restoration Project	URS Project No. 19228956.00001	Index Properties and Strength Plots from the Boring Logs	URS	Figure No. 4

Undrained Shear Strength Contour Plot - Bayou DuPont

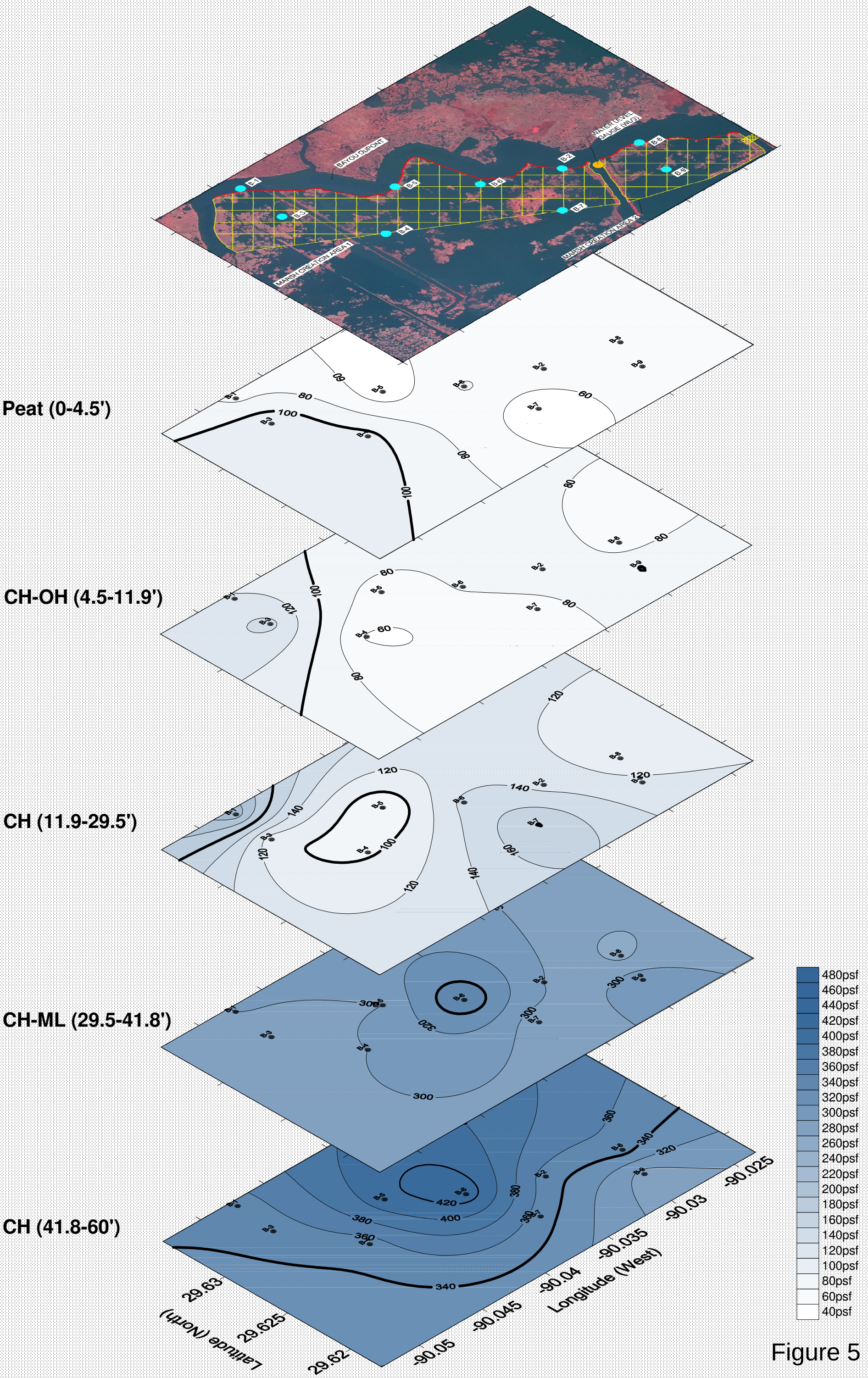


Figure 5

APPENDIX D

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou DuPont - 2.5ft fill with Equivalent fill height of 3.8

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	3.8	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.990E-01	.570	.30000E-03	z = .06

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	5.89	6
60.02	60.02	21.35	6.49	6.49	5.87	6
59.45	59.45	21.27	6.47	6.47	5.86	6
58.89	58.89	21.20	6.46	6.46	5.85	6

58.33	58.33	21.12	6.44	6.44	5.83	6
57.76	57.76	21.05	6.43	6.43	5.82	6
57.20	57.20	20.97	6.42	6.42	5.80	6
56.64	56.64	20.90	6.40	6.40	5.79	6
56.08	56.08	20.82	6.39	6.39	5.78	6
56.08	56.08	20.82	4.51	4.51	4.01	5
54.82	54.82	20.59	4.44	4.44	3.94	5
53.56	53.56	20.36	4.38	4.38	3.88	5
52.32	52.32	20.12	4.32	4.32	3.81	5
51.10	51.10	19.89	4.25	4.25	3.75	5
49.88	49.88	19.66	4.19	4.19	3.69	5
48.69	48.69	19.43	4.13	4.13	3.62	5
48.69	48.69	19.43	1.93	1.93	1.90	4
46.69	46.69	18.75	1.92	1.92	1.88	4
44.70	44.70	18.06	1.91	1.91	1.87	4
42.72	42.72	17.38	1.89	1.89	1.85	4
40.75	40.75	16.70	1.88	1.88	1.82	4
38.79	38.79	16.01	1.86	1.86	1.80	4
36.85	36.85	15.33	1.84	1.84	1.78	4
34.91	34.91	14.65	1.82	1.82	1.76	4
33.00	33.00	13.97	1.80	1.80	1.74	4
31.09	31.09	13.28	1.78	1.78	1.72	4
31.09	31.09	13.28	1.47	1.47	1.44	3
29.70	29.70	12.72	1.46	1.46	1.43	3
28.32	28.32	12.16	1.45	1.45	1.42	3
26.94	26.94	11.59	1.44	1.44	1.41	3
25.57	25.57	11.03	1.43	1.43	1.40	3
24.21	24.21	10.47	1.42	1.42	1.39	3
22.84	22.84	9.90	1.41	1.41	1.38	3
21.49	21.49	9.34	1.40	1.40	1.37	3
20.14	20.14	8.78	1.39	1.39	1.36	3
18.80	18.80	8.21	1.38	1.38	1.35	3
18.80	18.80	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.43	3.29	1.28	1.28	1.26	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.25	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	438.39	.00	438.39	235.87	202.52	6
60.02	478.34	4.62	473.72	271.20	202.52	6
59.45	518.22	9.24	508.98	306.46	202.52	6
58.89	558.03	13.86	544.17	341.66	202.52	6
58.33	597.78	18.48	579.30	376.79	202.52	6
57.76	637.47	23.10	614.37	411.85	202.52	6
57.20	677.09	27.72	649.36	446.85	202.52	6
56.64	716.64	32.34	684.30	481.78	202.52	6
56.08	756.12	36.96	719.16	516.65	202.52	6
56.08	756.12	36.96	719.16	516.65	202.52	5
54.82	861.10	62.71	798.39	595.87	202.52	5
53.56	965.15	88.46	876.69	674.17	202.52	5
52.32	1068.27	114.21	954.06	751.54	202.52	5
51.10	1170.48	139.96	1030.51	828.00	202.52	5
49.88	1271.75	165.71	1106.04	903.52	202.52	5

48.69	1372.11	191.46	1180.65	978.13	202.52	5
48.69	1372.11	191.46	1180.65	978.13	202.52	4
46.69	1572.55	267.32	1305.23	1102.71	202.52	4
44.70	1772.49	343.18	1429.31	1226.79	202.52	4
42.72	1971.88	419.04	1552.84	1350.33	202.52	4
40.75	2170.83	494.90	1675.93	1473.42	202.52	4
38.79	2369.03	570.76	1798.27	1595.75	202.52	4
36.85	2566.33	646.62	1919.71	1717.19	202.52	4
34.91	2762.72	722.48	2040.25	1837.73	202.52	4
33.00	2958.21	798.34	2159.88	1957.36	202.52	4
31.09	3152.80	874.19	2278.60	2076.09	202.52	4
31.09	3152.80	874.19	2278.60	2076.09	202.52	3
29.70	3301.37	936.05	2365.32	2162.80	202.52	3
28.32	3449.54	997.91	2451.63	2249.11	202.52	3
26.94	3597.35	1059.77	2537.58	2335.06	202.52	3
25.57	3744.81	1121.63	2623.18	2420.66	202.52	3
24.21	3891.92	1183.49	2708.43	2505.91	202.52	3
22.84	4038.68	1245.35	2793.33	2590.82	202.52	3
21.49	4185.09	1307.21	2877.89	2675.37	202.52	3
20.14	4331.16	1369.06	2962.10	2759.58	202.52	3
18.80	4476.88	1430.92	3045.96	2843.44	202.52	3
18.80	4476.88	1430.92	3045.96	2843.44	202.52	2
16.88	4682.55	1517.02	3165.53	2963.01	202.52	2
14.97	4887.69	1603.12	3284.57	3082.05	202.52	2
13.07	5092.30	1689.22	3403.08	3200.56	202.52	2
11.18	5296.38	1775.31	3521.06	3318.54	202.52	2
9.30	5499.93	1861.41	3638.52	3436.00	202.52	2
7.43	5702.95	1947.51	3755.44	3552.92	202.52	2
5.56	5905.45	2033.61	3871.85	3669.33	202.52	2
3.70	6107.57	2119.71	3987.87	3785.35	202.52	2
1.85	6309.34	2205.80	4103.53	3901.02	202.52	2
.00	6510.75	2291.90	4218.85	4016.33	202.52	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.78	1.91	.98	.98	.98	1
2.84	2.84	1.43	.98	.98	.92	1
1.89	1.89	.95	.98	.98	.91	1
.94	.94	.48	.98	.98	.90	1
.00	.00	.00	.98	.98	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

3.78	.00	.00	.00	.00	.00	1
2.84	109.60	.00	109.60	58.97	50.63	1
1.89	219.19	.00	219.19	117.94	101.26	1
.94	328.79	.00	328.79	176.90	151.89	1
.00	438.39	.00	438.39	235.87	202.52	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.51	21.42	6.50	6.07	5.89	6
60.02	59.97	21.35	6.49	6.20	5.87	6
59.45	59.42	21.27	6.47	6.30	5.86	6
58.89	58.87	21.20	6.46	6.36	5.85	6
58.33	58.31	21.12	6.44	6.40	5.83	6
57.76	57.75	21.05	6.43	6.41	5.82	6
57.20	57.19	20.97	6.42	6.41	5.80	6
56.64	56.63	20.90	6.40	6.40	5.79	6
56.08	56.07	20.82	6.39	6.39	5.78	6
56.08	56.07	20.82	4.51	4.51	4.01	5
54.82	54.80	20.59	4.44	4.44	3.94	5
53.56	53.55	20.36	4.38	4.38	3.88	5
52.32	52.31	20.12	4.32	4.31	3.81	5
51.10	51.08	19.89	4.25	4.25	3.75	5
49.88	49.87	19.66	4.19	4.19	3.69	5
48.69	48.68	19.43	4.13	4.12	3.62	5
48.69	48.68	19.43	1.93	1.93	1.90	4
46.69	46.68	18.75	1.92	1.92	1.88	4
44.70	44.69	18.06	1.91	1.91	1.87	4
42.72	42.71	17.38	1.89	1.89	1.85	4
40.75	40.74	16.70	1.88	1.88	1.82	4
38.79	38.78	16.01	1.86	1.86	1.80	4
36.85	36.84	15.33	1.84	1.84	1.78	4
34.91	34.91	14.65	1.82	1.82	1.76	4
33.00	32.99	13.97	1.80	1.80	1.74	4
31.09	31.09	13.28	1.78	1.78	1.72	4
31.09	31.09	13.28	1.47	1.47	1.44	3
29.70	29.70	12.72	1.46	1.46	1.43	3
28.32	28.31	12.16	1.45	1.45	1.42	3
26.94	26.94	11.59	1.44	1.44	1.41	3
25.57	25.56	11.03	1.43	1.43	1.40	3
24.21	24.20	10.47	1.42	1.42	1.39	3
22.84	22.84	9.90	1.41	1.41	1.38	3
21.49	21.48	9.34	1.40	1.40	1.37	3
20.14	20.13	8.78	1.39	1.39	1.36	3
18.80	18.79	8.21	1.38	1.38	1.35	3
18.80	18.79	8.21	1.34	1.34	1.31	2

16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.51	431.29	141.73	289.56	228.77	60.79	6
59.97	469.56	99.22	370.34	262.43	107.92	6
59.42	508.38	66.45	441.92	296.62	145.30	6
58.87	547.58	45.06	502.52	331.20	171.32	6
58.31	587.01	33.84	553.17	366.01	187.16	6
57.75	626.54	29.99	596.55	400.92	195.63	6
57.19	666.09	30.65	635.45	435.85	199.59	6
56.63	705.62	33.72	671.90	470.76	201.14	6
56.07	745.09	38.01	707.08	505.61	201.47	6
56.07	745.09	38.01	707.08	505.61	201.47	5
54.80	850.03	63.58	786.45	584.80	201.65	5
53.55	954.05	89.33	864.72	663.07	201.65	5
52.31	1057.14	115.11	942.03	740.41	201.62	5
51.08	1159.31	140.88	1018.43	816.83	201.60	5
49.87	1260.55	166.62	1093.93	892.32	201.61	5
48.68	1360.88	192.28	1168.60	966.90	201.70	5
48.68	1360.88	192.28	1168.60	966.90	201.70	4
46.68	1561.32	267.32	1293.99	1091.48	202.52	4
44.69	1761.24	343.18	1418.06	1215.54	202.52	4
42.71	1960.64	421.73	1538.91	1339.09	199.83	4
40.74	2159.48	507.73	1651.75	1462.06	189.68	4
38.78	2357.60	573.59	1784.01	1584.33	199.69	4
36.84	2554.89	646.64	1908.25	1705.76	202.49	4
34.91	2751.29	722.48	2028.81	1826.29	202.52	4
32.99	2946.78	798.34	2148.44	1945.92	202.52	4
31.09	3141.36	874.19	2267.17	2064.65	202.52	4
31.09	3141.36	874.19	2267.17	2064.65	202.52	3
29.70	3289.93	936.05	2353.88	2151.36	202.52	3
28.31	3438.10	997.91	2440.19	2237.67	202.52	3
26.94	3585.91	1060.98	2524.93	2323.62	201.31	3
25.56	3733.36	1123.19	2610.17	2409.21	200.96	3
24.20	3880.46	1185.07	2695.39	2494.45	200.94	3
22.84	4027.21	1246.81	2780.40	2579.35	201.05	3
21.48	4173.62	1308.56	2865.06	2663.90	201.16	3
20.13	4319.68	1370.23	2949.45	2748.10	201.35	3
18.79	4465.39	1431.78	3033.61	2831.95	201.66	3
18.79	4465.39	1431.78	3033.61	2831.95	201.66	2
16.87	4671.06	1517.28	3153.77	2951.52	202.25	2
14.97	4876.20	1603.12	3273.08	3070.56	202.52	2
13.07	5080.81	1689.22	3391.59	3189.07	202.52	2
11.18	5284.88	1775.31	3509.57	3307.05	202.52	2
9.29	5488.44	1861.41	3627.03	3424.51	202.52	2
7.42	5691.46	1947.51	3743.94	3541.43	202.52	2
5.55	5893.98	2033.61	3860.37	3657.85	202.52	2
3.69	6096.08	2122.89	3973.18	3773.85	199.33	2
1.84	6297.80	2236.62	4061.18	3889.48	171.70	2
.00	6498.81	2492.98	4005.83	4004.39	1.44	2

Time = 30. Degree of Consolidation = 5.%

Total Settlement = .078

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 30. = .078

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
3.78	3.67	1.91	.98	.98	.98	1
2.84	2.74	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.91	.90	1
.00	.00	.00	.98	.91	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.67	.00	.00	.00	.00	.00	1
2.74	108.58	40.39	68.19	57.95	10.24	1
1.82	216.34	83.22	133.13	115.08	18.04	1
.91	323.87	117.20	206.67	171.98	34.69	1
.00	431.29	141.73	289.56	228.77	60.79	1

Time = 30. Degree of Consolidation = 94.%

Total Settlement = .114

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 30. = .114

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 2.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.46	21.42	6.50	6.03	5.89	6
60.02	59.93	21.35	6.49	6.13	5.87	6
59.45	59.39	21.27	6.47	6.21	5.86	6
58.89	58.84	21.20	6.46	6.28	5.85	6
58.33	58.29	21.12	6.44	6.33	5.83	6

57.76	57.73	21.05	6.43	6.36	5.82	6
57.20	57.17	20.97	6.42	6.37	5.80	6
56.64	56.62	20.90	6.40	6.38	5.79	6
56.08	56.06	20.82	6.39	6.37	5.78	6
56.08	56.06	20.82	4.51	4.50	4.01	5
54.82	54.79	20.59	4.44	4.44	3.94	5
53.56	53.54	20.36	4.38	4.37	3.88	5
52.32	52.30	20.12	4.32	4.31	3.81	5
51.10	51.08	19.89	4.25	4.25	3.75	5
49.88	49.87	19.66	4.19	4.18	3.69	5
48.69	48.67	19.43	4.13	4.12	3.62	5
48.69	48.67	19.43	1.93	1.93	1.90	4
46.69	46.68	18.75	1.92	1.92	1.88	4
44.70	44.69	18.06	1.91	1.91	1.87	4
42.72	42.71	17.38	1.89	1.89	1.85	4
40.75	40.74	16.70	1.88	1.88	1.82	4
38.79	38.78	16.01	1.86	1.86	1.80	4
36.85	36.83	15.33	1.84	1.84	1.78	4
34.91	34.90	14.65	1.82	1.82	1.76	4
33.00	32.99	13.97	1.80	1.80	1.74	4
31.09	31.08	13.28	1.78	1.78	1.72	4
31.09	31.08	13.28	1.47	1.47	1.44	3
29.70	29.69	12.72	1.46	1.46	1.43	3
28.32	28.31	12.16	1.45	1.45	1.42	3
26.94	26.93	11.59	1.44	1.44	1.41	3
25.57	25.56	11.03	1.43	1.43	1.40	3
24.21	24.19	10.47	1.42	1.42	1.39	3
22.84	22.83	9.90	1.41	1.41	1.38	3
21.49	21.48	9.34	1.40	1.40	1.37	3
20.14	20.13	8.78	1.39	1.39	1.36	3
18.80	18.79	8.21	1.38	1.38	1.35	3
18.80	18.79	8.21	1.34	1.34	1.31	2
16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.46	431.20	156.59	274.62	228.69	45.93	6
59.93	469.19	123.86	345.33	262.05	83.28	6
59.39	507.61	95.65	411.97	295.86	116.11	6
58.84	546.40	73.28	473.11	330.02	143.09	6
58.29	585.46	57.24	528.22	364.46	163.76	6
57.73	624.70	47.14	577.56	399.08	178.48	6
57.17	664.05	42.05	622.01	433.81	188.19	6
56.62	703.45	40.74	662.70	468.59	194.12	6
56.06	742.84	42.05	700.79	503.36	197.43	6
56.06	742.84	42.05	700.79	503.36	197.43	5
54.79	847.67	65.86	781.81	582.44	199.37	5
53.54	951.62	90.76	860.86	660.65	200.21	5
52.30	1054.67	116.19	938.49	737.95	200.54	5
51.08	1156.81	141.80	1015.00	814.33	200.68	5
49.87	1258.02	167.45	1090.57	889.79	200.78	5
48.67	1358.32	193.02	1165.29	964.34	200.95	5

48.67	1358.32	193.03	1165.29	964.34	200.95	4
46.68	1558.75	267.32	1291.43	1088.92	202.52	4
44.69	1758.68	343.57	1415.11	1212.98	202.13	4
42.71	1958.07	426.41	1531.66	1336.51	195.15	4
40.74	2156.85	512.81	1644.04	1459.43	184.60	4
38.78	2354.92	577.04	1777.88	1581.64	196.23	4
36.83	2552.18	647.56	1904.62	1703.05	201.57	4
34.90	2748.57	722.48	2026.10	1823.58	202.52	4
32.99	2944.07	798.34	2145.73	1943.21	202.52	4
31.08	3138.65	874.20	2264.45	2061.94	202.52	4
31.08	3138.65	874.20	2264.45	2061.94	202.52	3
29.69	3287.22	936.05	2351.17	2148.65	202.52	3
28.31	3435.39	997.91	2437.48	2234.96	202.52	3
26.93	3583.19	1061.83	2521.36	2320.91	200.46	3
25.56	3730.64	1124.49	2606.15	2406.49	199.66	3
24.19	3877.73	1186.42	2691.31	2491.73	199.58	3
22.83	4024.48	1248.16	2776.32	2576.62	199.70	3
21.48	4170.88	1309.86	2861.02	2661.16	199.86	3
20.13	4316.93	1371.35	2945.58	2745.35	200.23	3
18.79	4462.64	1432.63	3030.01	2829.20	200.81	3
18.79	4462.64	1432.63	3030.01	2829.20	200.81	2
16.87	4668.30	1517.59	3150.72	2948.76	201.95	2
14.96	4873.44	1603.23	3270.20	3067.80	202.40	2
13.06	5078.05	1689.22	3388.83	3186.31	202.52	2
11.17	5282.13	1775.31	3506.81	3304.29	202.52	2
9.29	5485.68	1861.41	3624.27	3421.75	202.52	2
7.42	5688.70	1947.51	3741.19	3538.67	202.52	2
5.55	5891.21	2033.61	3857.60	3655.08	202.52	2
3.69	6093.31	2129.20	3964.11	3771.09	193.02	2
1.84	6294.97	2259.54	4035.43	3886.65	148.78	2
.00	6495.91	2493.17	4002.73	4001.49	1.25	2

Time = 60. Degree of Consolidation = 7.%

Total Settlement = .123

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 60. = .123

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.78	3.66	1.91
2.84	2.74	1.43
1.89	1.82	.95
.94	.91	.48
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.66	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

2.74	108.58	40.93	67.64	57.95	9.70	1
1.82	216.32	87.06	129.26	115.06	14.20	1
.91	323.82	128.72	195.09	171.93	23.16	1
.00	431.20	156.59	274.62	228.69	45.93	1

Time = 60. Degree of Consolidation = 95.%

Total Settlement = .115

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 60. = .115

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 2.14

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.39	21.42	6.50	5.98	5.89	6
60.02	59.86	21.35	6.49	6.06	5.87	6
59.45	59.32	21.27	6.47	6.12	5.86	6
58.89	58.78	21.20	6.46	6.18	5.85	6
58.33	58.24	21.12	6.44	6.23	5.83	6
57.76	57.69	21.05	6.43	6.27	5.82	6
57.20	57.14	20.97	6.42	6.30	5.80	6
56.64	56.59	20.90	6.40	6.32	5.79	6
56.08	56.03	20.82	6.39	6.34	5.78	6
56.08	56.03	20.82	4.51	4.47	4.01	5
54.82	54.77	20.59	4.44	4.41	3.94	5
53.56	53.52	20.36	4.38	4.36	3.88	5
52.32	52.29	20.12	4.32	4.30	3.81	5
51.10	51.06	19.89	4.25	4.24	3.75	5
49.88	49.86	19.66	4.19	4.18	3.69	5
48.69	48.66	19.43	4.13	4.12	3.62	5
48.69	48.66	19.43	1.93	1.93	1.90	4
46.69	46.67	18.75	1.92	1.92	1.88	4
44.70	44.68	18.06	1.91	1.90	1.87	4
42.72	42.70	17.38	1.89	1.89	1.85	4
40.75	40.73	16.70	1.88	1.87	1.82	4
38.79	38.77	16.01	1.86	1.86	1.80	4
36.85	36.83	15.33	1.84	1.84	1.78	4
34.91	34.90	14.65	1.82	1.82	1.76	4
33.00	32.98	13.97	1.80	1.80	1.74	4
31.09	31.08	13.28	1.78	1.78	1.72	4
31.09	31.08	13.28	1.47	1.47	1.44	3
29.70	29.69	12.72	1.46	1.46	1.43	3
28.32	28.30	12.16	1.45	1.45	1.42	3
26.94	26.93	11.59	1.44	1.44	1.41	3
25.57	25.56	11.03	1.43	1.43	1.40	3
24.21	24.19	10.47	1.42	1.42	1.39	3
22.84	22.83	9.90	1.41	1.41	1.38	3
21.49	21.48	9.34	1.40	1.40	1.37	3
20.14	20.13	8.78	1.39	1.39	1.36	3
18.80	18.78	8.21	1.38	1.38	1.35	3

18.80	18.78	8.21	1.34	1.34	1.31	2
16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.39	431.12	170.53	260.59	228.61	31.98	6
59.86	468.85	146.54	322.31	261.71	60.59	6
59.32	506.90	124.49	382.41	295.15	87.26	6
58.78	545.25	105.06	440.19	328.87	111.31	6
58.24	583.86	88.72	495.14	362.86	132.28	6
57.69	622.67	75.66	547.01	397.05	149.96	6
57.14	661.65	65.82	595.82	431.41	164.42	6
56.59	700.74	58.90	641.85	465.88	175.96	6
56.03	739.92	54.39	685.52	500.44	185.08	6
56.03	739.92	54.39	685.52	500.44	185.08	5
54.77	844.37	74.74	769.63	579.14	190.48	5
53.52	948.06	96.97	851.09	657.08	194.01	5
52.29	1050.92	120.53	930.39	734.19	196.20	5
51.06	1152.92	144.98	1007.94	810.44	197.50	5
49.86	1254.03	170.02	1084.01	885.80	198.21	5
48.66	1354.24	195.46	1158.78	960.26	198.52	5
48.66	1354.24	195.46	1158.78	960.26	198.52	4
46.67	1554.67	268.54	1286.12	1084.83	201.29	4
44.68	1754.58	347.08	1407.49	1208.88	198.61	4
42.70	1953.93	433.96	1519.97	1332.37	187.60	4
40.73	2152.65	518.96	1633.69	1455.23	178.46	4
38.77	2350.64	582.38	1768.26	1577.37	190.89	4
36.83	2547.85	650.38	1897.48	1698.72	198.76	4
34.90	2744.23	722.58	2021.65	1819.24	202.41	4
32.98	2939.72	798.34	2141.39	1938.87	202.52	4
31.08	3134.31	874.20	2260.11	2057.60	202.52	4
31.08	3134.31	874.20	2260.11	2057.60	202.52	3
29.69	3282.88	936.05	2346.82	2144.31	202.52	3
28.30	3431.05	997.91	2433.14	2230.62	202.52	3
26.93	3578.85	1063.07	2515.78	2316.56	199.22	3
25.56	3726.28	1126.62	2599.66	2402.14	197.53	3
24.19	3873.36	1189.00	2684.36	2487.36	197.00	3
22.83	4020.10	1250.81	2769.29	2572.23	197.05	3
21.48	4166.48	1312.26	2854.22	2656.76	197.46	3
20.13	4312.52	1373.48	2939.04	2740.94	198.10	3
18.78	4458.22	1434.27	3023.94	2824.78	199.16	3
18.78	4458.22	1434.27	3023.94	2824.78	199.16	2
16.87	4663.87	1518.27	3145.60	2944.34	201.27	2
14.96	4869.01	1603.58	3265.42	3063.37	202.05	2
13.06	5073.61	1689.22	3384.40	3181.88	202.52	2
11.17	5277.69	1775.31	3502.38	3299.86	202.52	2
9.29	5481.25	1861.41	3619.84	3417.32	202.52	2
7.41	5684.26	1947.51	3736.75	3534.24	202.52	2
5.55	5886.78	2033.63	3853.15	3650.66	202.50	2
3.69	6088.86	2144.13	3944.72	3766.63	178.09	2
1.84	6290.42	2289.84	4000.58	3882.09	118.48	2
.00	6491.27	2493.42	3997.84	3996.85	1.00	2

Time = 120. Degree of Consolidation = 11.%

Total Settlement = .196

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 120. = .196

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.91	.90	1
.00	.00	.00	.98	.90	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.57	41.41	67.16	57.94	9.22	1
1.82	216.31	90.45	125.85	115.05	10.81	1
.91	323.78	139.18	184.59	171.89	12.70	1
.00	431.12	170.53	260.59	228.61	31.98	1

Time = 120. Degree of Consolidation = 96.%

Total Settlement = .116

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 120. = .116

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.07

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.28	21.42	6.50	5.97	5.89	6
60.02	59.75	21.35	6.49	6.02	5.87	6

59.45	59.22	21.27	6.47	6.06	5.86	6
58.89	58.68	21.20	6.46	6.11	5.85	6
58.33	58.14	21.12	6.44	6.15	5.83	6
57.76	57.60	21.05	6.43	6.18	5.82	6
57.20	57.06	20.97	6.42	6.22	5.80	6
56.64	56.51	20.90	6.40	6.24	5.79	6
56.08	55.96	20.82	6.39	6.27	5.78	6
56.08	55.96	20.82	4.51	4.41	4.01	5
54.82	54.71	20.59	4.44	4.37	3.94	5
53.56	53.48	20.36	4.38	4.32	3.88	5
52.32	52.25	20.12	4.32	4.26	3.81	5
51.10	51.03	19.89	4.25	4.21	3.75	5
49.88	49.83	19.66	4.19	4.15	3.69	5
48.69	48.65	19.43	4.13	4.09	3.62	5
48.69	48.65	19.43	1.93	1.93	1.90	4
46.69	46.65	18.75	1.92	1.92	1.88	4
44.70	44.67	18.06	1.91	1.90	1.87	4
42.72	42.69	17.38	1.89	1.89	1.85	4
40.75	40.72	16.70	1.88	1.87	1.82	4
38.79	38.76	16.01	1.86	1.85	1.80	4
36.85	36.82	15.33	1.84	1.84	1.78	4
34.91	34.89	14.65	1.82	1.82	1.76	4
33.00	32.97	13.97	1.80	1.80	1.74	4
31.09	31.07	13.28	1.78	1.78	1.72	4
31.09	31.07	13.28	1.47	1.47	1.44	3
29.70	29.68	12.72	1.46	1.46	1.43	3
28.32	28.30	12.16	1.45	1.45	1.42	3
26.94	26.92	11.59	1.44	1.44	1.41	3
25.57	25.55	11.03	1.43	1.43	1.40	3
24.21	24.18	10.47	1.42	1.42	1.39	3
22.84	22.82	9.90	1.41	1.41	1.38	3
21.49	21.47	9.34	1.40	1.40	1.37	3
20.14	20.12	8.78	1.39	1.39	1.36	3
18.80	18.78	8.21	1.38	1.38	1.35	3
18.80	18.78	8.21	1.34	1.34	1.31	2
16.88	16.86	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.28	4.11	1.29	1.29	1.26	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.28	430.82	174.76	256.06	228.30	27.76	6
59.75	468.42	159.57	308.85	261.28	47.56	6
59.22	506.23	144.78	361.45	294.48	66.97	6
58.68	544.26	130.64	413.62	327.88	85.74	6
58.14	582.47	117.38	465.09	361.47	103.62	6
57.60	620.87	105.20	515.67	395.25	120.42	6
57.06	659.43	94.26	565.17	429.19	135.98	6
56.51	698.14	84.65	613.49	463.28	150.21	6
55.96	736.97	76.38	660.59	497.49	163.10	6
55.96	736.97	76.38	660.59	497.49	163.10	5
54.71	840.68	94.38	746.29	575.45	170.85	5
53.48	943.70	114.08	829.63	652.72	176.90	5
52.25	1045.99	135.34	910.65	729.27	181.39	5

51.03	1147.50	158.05	989.44	805.02	184.43	5
49.83	1248.16	182.09	1066.07	879.93	186.14	5
48.65	1347.94	207.36	1140.58	953.96	186.62	5
48.65	1347.94	207.36	1140.58	953.96	186.62	4
46.65	1548.29	278.96	1269.33	1078.45	190.87	4
44.67	1748.13	357.84	1390.30	1202.43	187.86	4
42.69	1947.40	446.52	1500.88	1325.85	175.04	4
40.72	2146.03	526.88	1619.15	1448.61	170.53	4
38.76	2343.94	589.47	1754.47	1570.66	183.80	4
36.82	2541.08	655.39	1885.68	1691.94	193.74	4
34.89	2737.41	724.97	2012.44	1812.42	200.02	4
32.97	2932.89	798.34	2134.55	1932.03	202.52	4
31.07	3127.47	874.20	2253.28	2050.76	202.52	4
31.07	3127.47	874.20	2253.28	2050.76	202.52	3
29.68	3276.04	936.05	2339.99	2137.47	202.52	3
28.30	3424.22	997.91	2426.31	2223.79	202.52	3
26.92	3572.01	1064.77	2507.24	2309.72	197.51	3
25.55	3719.43	1129.63	2589.80	2395.29	194.52	3
24.18	3866.49	1192.93	2673.57	2480.49	193.08	3
22.82	4013.20	1255.05	2758.15	2565.34	192.81	3
21.47	4159.56	1316.44	2843.12	2649.84	193.28	3
20.12	4305.58	1377.27	2928.31	2734.00	194.31	3
18.78	4451.26	1437.53	3013.73	2817.82	195.91	3
18.78	4451.26	1437.53	3013.73	2817.82	195.91	2
16.86	4656.90	1520.51	3136.38	2937.36	199.02	2
14.96	4862.02	1604.78	3257.24	3056.39	200.85	2
13.06	5066.62	1689.77	3376.85	3174.89	201.97	2
11.17	5270.70	1775.31	3495.39	3292.87	202.52	2
9.28	5474.26	1861.41	3612.85	3410.33	202.52	2
7.41	5677.27	1947.51	3729.76	3527.24	202.52	2
5.54	5879.78	2040.42	3839.36	3643.66	195.70	2
3.69	6081.79	2169.17	3912.62	3759.57	153.05	2
1.84	6283.23	2320.64	3962.58	3874.91	87.68	2
.00	6484.00	2493.68	3990.32	3989.58	.74	2

Time = 240. Degree of Consolidation = 18.%

Total Settlement = .307

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 240. = .307

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.82	202.52	228.30	228.30	.00	1

Time = 240. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 240. = .121

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.95

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.17	21.42	6.50	5.94	5.89	6
60.02	59.65	21.35	6.49	5.98	5.87	6
59.45	59.12	21.27	6.47	6.02	5.86	6
58.89	58.59	21.20	6.46	6.06	5.85	6
58.33	58.05	21.12	6.44	6.09	5.83	6
57.76	57.51	21.05	6.43	6.13	5.82	6
57.20	56.98	20.97	6.42	6.16	5.80	6
56.64	56.43	20.90	6.40	6.19	5.79	6
56.08	55.89	20.82	6.39	6.21	5.78	6
56.08	55.89	20.82	4.51	4.37	4.01	5
54.82	54.65	20.59	4.44	4.32	3.94	5
53.56	53.42	20.36	4.38	4.27	3.88	5
52.32	52.21	20.12	4.32	4.22	3.81	5
51.10	51.00	19.89	4.25	4.17	3.75	5
49.88	49.81	19.66	4.19	4.11	3.69	5
48.69	48.63	19.43	4.13	4.05	3.62	5
48.69	48.63	19.43	1.93	1.92	1.90	4
46.69	46.64	18.75	1.92	1.91	1.88	4
44.70	44.65	18.06	1.91	1.90	1.87	4
42.72	42.68	17.38	1.89	1.89	1.85	4
40.75	40.71	16.70	1.88	1.87	1.82	4
38.79	38.76	16.01	1.86	1.85	1.80	4
36.85	36.81	15.33	1.84	1.84	1.78	4
34.91	34.88	14.65	1.82	1.82	1.76	4
33.00	32.97	13.97	1.80	1.80	1.74	4
31.09	31.07	13.28	1.78	1.78	1.72	4
31.09	31.07	13.28	1.47	1.47	1.44	3
29.70	29.68	12.72	1.46	1.46	1.43	3
28.32	28.29	12.16	1.45	1.45	1.42	3
26.94	26.92	11.59	1.44	1.44	1.41	3
25.57	25.54	11.03	1.43	1.43	1.40	3

24.21	24.18	10.47	1.42	1.42	1.39	3
22.84	22.82	9.90	1.41	1.41	1.38	3
21.49	21.47	9.34	1.40	1.40	1.37	3
20.14	20.12	8.78	1.39	1.39	1.36	3
18.80	18.77	8.21	1.38	1.38	1.35	3
18.80	18.77	8.21	1.34	1.34	1.31	2
16.88	16.86	7.39	1.33	1.33	1.30	2
14.97	14.95	6.57	1.32	1.32	1.29	2
13.07	13.05	5.75	1.31	1.31	1.28	2
11.18	11.16	4.93	1.30	1.30	1.27	2
9.30	9.28	4.11	1.29	1.29	1.26	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.68	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.17	430.82	186.00	244.82	228.30	16.52	6
59.65	468.25	172.39	295.85	261.11	34.74	6
59.12	505.87	159.10	346.77	294.11	52.66	6
58.59	543.68	146.28	397.39	327.30	70.10	6
58.05	581.66	134.11	447.55	360.66	86.88	6
57.51	619.81	122.74	497.07	394.19	102.87	6
56.98	658.12	112.29	545.83	427.88	117.95	6
56.43	696.57	102.86	593.71	461.71	132.00	6
55.89	735.15	94.51	640.64	495.67	144.97	6
55.89	735.15	94.51	640.64	495.67	144.97	5
54.65	838.20	112.37	725.83	572.97	152.86	5
53.42	940.59	131.74	808.85	649.61	159.24	5
52.21	1042.25	152.59	889.66	725.53	164.14	5
51.00	1143.15	174.91	968.23	800.67	167.57	5
49.81	1243.21	198.65	1044.56	874.98	169.58	5
48.63	1342.40	223.75	1118.65	948.42	170.23	5
48.63	1342.40	223.75	1118.65	948.42	170.23	4
46.64	1542.64	293.81	1248.84	1072.81	176.03	4
44.65	1742.39	371.62	1370.77	1196.69	174.08	4
42.68	1941.57	459.69	1481.88	1320.01	161.87	4
40.71	2140.11	533.90	1606.20	1442.69	163.51	4
38.76	2337.93	595.38	1742.56	1564.66	177.90	4
36.81	2535.01	659.81	1875.20	1685.88	189.32	4
34.88	2731.30	727.49	2003.81	1806.31	197.50	4
32.97	2926.76	798.72	2128.05	1925.91	202.13	4
31.07	3121.35	874.38	2246.97	2044.64	202.33	4
31.07	3121.35	874.38	2246.97	2044.64	202.33	3
29.68	3269.92	936.05	2333.87	2131.35	202.52	3
28.29	3418.10	997.91	2420.19	2217.67	202.52	3
26.92	3565.89	1065.91	2499.98	2303.60	196.38	3
25.54	3713.30	1131.86	2581.43	2389.15	192.28	3
24.18	3860.34	1195.97	2664.37	2474.34	190.03	3
22.82	4007.03	1258.63	2748.41	2559.17	189.24	3
21.47	4153.37	1320.17	2833.20	2643.65	189.55	3
20.12	4299.37	1380.77	2918.60	2727.79	190.81	3
18.77	4445.03	1440.59	3004.44	2811.59	192.85	3
18.77	4445.03	1440.59	3004.44	2811.59	192.85	2
16.86	4650.65	1522.68	3127.97	2931.11	196.86	2
14.95	4855.76	1606.04	3249.73	3050.13	199.60	2
13.05	5060.36	1690.52	3369.84	3168.63	201.21	2
11.16	5264.44	1775.54	3488.89	3286.60	202.29	2
9.28	5467.99	1861.41	3606.57	3404.06	202.52	2

7.41	5671.01	1947.51	3723.50	3520.98	202.52	2
5.54	5873.50	2049.83	3823.67	3637.37	186.29	2
3.68	6075.45	2186.70	3888.75	3753.23	135.53	2
1.84	6276.82	2335.99	3940.83	3868.49	72.34	2
.00	6477.55	2493.81	3983.74	3983.13	.61	2

Time = 365. Degree of Consolidation = 24.%

Total Settlement = .411

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 365. = .411

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.82	202.52	228.30	228.30	.00	1

Time = 365. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 365. = .121

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.85

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.05	21.42	6.50	5.93	5.89	6
60.02	59.53	21.35	6.49	5.96	5.87	6
59.45	59.00	21.27	6.47	5.99	5.86	6
58.89	58.47	21.20	6.46	6.02	5.85	6
58.33	57.94	21.12	6.44	6.05	5.83	6
57.76	57.40	21.05	6.43	6.08	5.82	6
57.20	56.87	20.97	6.42	6.11	5.80	6
56.64	56.33	20.90	6.40	6.13	5.79	6
56.08	55.79	20.82	6.39	6.15	5.78	6
56.08	55.79	20.82	4.51	4.31	4.01	5
54.82	54.56	20.59	4.44	4.27	3.94	5
53.56	53.35	20.36	4.38	4.22	3.88	5
52.32	52.15	20.12	4.32	4.16	3.81	5
51.10	50.95	19.89	4.25	4.11	3.75	5
49.88	49.78	19.66	4.19	4.05	3.69	5
48.69	48.61	19.43	4.13	3.99	3.62	5
48.69	48.61	19.43	1.93	1.92	1.90	4
46.69	46.62	18.75	1.92	1.91	1.88	4
44.70	44.64	18.06	1.91	1.90	1.87	4
42.72	42.67	17.38	1.89	1.88	1.85	4
40.75	40.70	16.70	1.88	1.87	1.82	4
38.79	38.75	16.01	1.86	1.85	1.80	4
36.85	36.81	15.33	1.84	1.83	1.78	4
34.91	34.88	14.65	1.82	1.82	1.76	4
33.00	32.96	13.97	1.80	1.80	1.74	4
31.09	31.06	13.28	1.78	1.77	1.72	4
31.09	31.06	13.28	1.47	1.47	1.44	3
29.70	29.67	12.72	1.46	1.46	1.43	3
28.32	28.29	12.16	1.45	1.45	1.42	3
26.94	26.91	11.59	1.44	1.44	1.41	3
25.57	25.54	11.03	1.43	1.43	1.40	3
24.21	24.17	10.47	1.42	1.42	1.39	3
22.84	22.82	9.90	1.41	1.41	1.38	3
21.49	21.46	9.34	1.40	1.40	1.37	3
20.14	20.11	8.78	1.39	1.39	1.36	3
18.80	18.77	8.21	1.38	1.38	1.35	3
18.80	18.77	8.21	1.34	1.34	1.31	2
16.88	16.86	7.39	1.33	1.33	1.30	2
14.97	14.95	6.57	1.32	1.32	1.29	2
13.07	13.05	5.75	1.31	1.31	1.28	2
11.18	11.16	4.93	1.30	1.30	1.27	2
9.30	9.28	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.05	430.82	188.63	242.19	228.30	13.89	6
59.53	468.19	178.06	290.13	261.05	29.08	6
59.00	505.71	167.69	338.02	293.95	44.07	6
58.47	543.37	157.62	385.75	326.99	58.76	6
57.94	581.18	147.98	433.20	360.18	73.02	6
57.40	619.12	138.88	480.23	393.50	86.73	6
56.87	657.18	130.43	526.75	426.94	99.81	6
56.33	695.36	122.74	572.62	460.50	112.12	6

55.79	733.64	115.89	617.75	494.16	123.59	6
55.79	733.64	115.89	617.75	494.16	123.59	5
54.56	835.91	134.57	701.34	570.68	130.66	5
53.35	937.49	154.48	783.02	646.51	136.50	5
52.15	1038.34	175.63	862.70	721.61	141.10	5
50.95	1138.40	198.07	940.33	795.92	144.41	5
49.78	1237.63	221.77	1015.86	869.40	146.46	5
48.61	1335.99	246.72	1089.28	942.01	147.26	5
48.61	1335.99	246.72	1089.28	942.01	147.26	4
46.62	1536.09	315.38	1220.71	1066.25	154.46	4
44.64	1735.69	391.87	1343.81	1189.99	153.82	4
42.67	1934.73	479.02	1455.72	1313.18	142.54	4
40.70	2133.14	543.91	1589.24	1435.73	153.51	4
38.75	2330.86	603.51	1727.35	1557.59	169.77	4
36.81	2527.86	666.05	1861.81	1678.72	183.08	4
34.88	2724.08	731.83	1992.25	1799.09	193.16	4
32.96	2919.50	801.44	2118.06	1918.65	199.41	4
31.06	3114.07	875.71	2238.36	2037.35	201.00	4
31.06	3114.07	875.71	2238.36	2037.35	201.00	3
29.67	3262.63	936.05	2326.58	2124.06	202.52	3
28.29	3410.81	997.91	2412.90	2210.38	202.52	3
26.91	3558.60	1067.24	2491.36	2296.31	195.05	3
25.54	3706.00	1134.35	2571.65	2381.85	189.80	3
24.17	3853.03	1199.21	2653.81	2467.02	186.79	3
22.82	3999.70	1262.41	2737.29	2551.83	185.45	3
21.46	4146.01	1324.12	2821.89	2636.29	185.60	3
20.11	4291.99	1384.70	2907.29	2720.41	186.88	3
18.77	4437.63	1444.12	2993.51	2804.19	189.32	3
18.77	4437.63	1444.12	2993.51	2804.19	189.32	2
16.86	4643.23	1525.40	3117.83	2923.69	194.14	2
14.95	4848.33	1607.92	3240.41	3042.69	197.71	2
13.05	5052.91	1692.00	3360.91	3161.18	199.73	2
11.16	5256.98	1776.73	3480.25	3279.15	201.10	2
9.28	5460.52	1862.30	3598.22	3396.59	201.63	2
7.40	5663.54	1949.88	3713.66	3513.51	200.15	2
5.54	5866.00	2060.69	3805.31	3629.87	175.43	2
3.68	6067.90	2201.56	3866.34	3745.67	120.66	2
1.84	6269.21	2347.00	3922.21	3860.89	61.32	2
.00	6469.92	2493.90	3976.02	3975.50	.52	2

Time = 540. Degree of Consolidation = 31.%

Total Settlement = .533

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 540. = .533

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1

.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.82	202.52	228.30	228.30	.00	1

Time = 540. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 540. = .121

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.73

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.93	21.42	6.50	5.92	5.89	6
60.02	59.41	21.35	6.49	5.95	5.87	6
59.45	58.88	21.27	6.47	5.97	5.86	6
58.89	58.36	21.20	6.46	6.00	5.85	6
58.33	57.83	21.12	6.44	6.02	5.83	6
57.76	57.30	21.05	6.43	6.04	5.82	6
57.20	56.76	20.97	6.42	6.06	5.80	6
56.64	56.23	20.90	6.40	6.08	5.79	6
56.08	55.69	20.82	6.39	6.09	5.78	6
56.08	55.69	20.82	4.51	4.26	4.01	5
54.82	54.48	20.59	4.44	4.21	3.94	5
53.56	53.28	20.36	4.38	4.16	3.88	5
52.32	52.09	20.12	4.32	4.11	3.81	5
51.10	50.91	19.89	4.25	4.05	3.75	5
49.88	49.74	19.66	4.19	3.99	3.69	5
48.69	48.59	19.43	4.13	3.93	3.62	5
48.69	48.59	19.43	1.93	1.92	1.90	4
46.69	46.60	18.75	1.92	1.91	1.88	4
44.70	44.62	18.06	1.91	1.89	1.87	4
42.72	42.65	17.38	1.89	1.88	1.85	4
40.75	40.69	16.70	1.88	1.86	1.82	4
38.79	38.74	16.01	1.86	1.85	1.80	4
36.85	36.80	15.33	1.84	1.83	1.78	4
34.91	34.87	14.65	1.82	1.81	1.76	4
33.00	32.96	13.97	1.80	1.79	1.74	4
31.09	31.05	13.28	1.78	1.77	1.72	4

31.09	31.05	13.28	1.47	1.47	1.44	3
29.70	29.67	12.72	1.46	1.46	1.43	3
28.32	28.28	12.16	1.45	1.45	1.42	3
26.94	26.91	11.59	1.44	1.44	1.41	3
25.57	25.53	11.03	1.43	1.43	1.40	3
24.21	24.17	10.47	1.42	1.42	1.39	3
22.84	22.81	9.90	1.41	1.41	1.38	3
21.49	21.46	9.34	1.40	1.40	1.37	3
20.14	20.11	8.78	1.39	1.39	1.36	3
18.80	18.77	8.21	1.38	1.38	1.35	3
18.80	18.77	8.21	1.34	1.34	1.31	2
16.88	16.85	7.39	1.33	1.33	1.30	2
14.97	14.95	6.57	1.32	1.32	1.29	2
13.07	13.05	5.75	1.31	1.31	1.28	2
11.18	11.16	4.93	1.30	1.30	1.27	2
9.30	9.28	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	430.82	190.72	240.10	228.30	11.80	6
59.41	468.14	182.57	285.57	261.00	24.57	6
58.88	505.58	174.58	330.99	293.82	37.17	6
58.36	543.13	166.86	376.27	326.75	49.52	6
57.83	580.78	159.50	421.28	359.79	61.50	6
57.30	618.54	152.60	465.94	392.93	73.02	6
56.76	656.40	146.24	510.16	426.16	84.00	6
56.23	694.34	140.52	553.81	459.48	94.34	6
55.69	732.35	135.53	596.82	492.87	103.95	6
55.69	732.35	135.53	596.82	492.87	103.95	5
54.48	833.90	155.28	678.62	568.67	109.95	5
53.28	934.72	176.01	758.71	643.74	114.97	5
52.09	1034.78	197.77	837.01	718.05	118.96	5
50.91	1134.04	220.57	913.47	791.56	121.91	5
49.74	1232.46	244.43	988.04	864.24	123.80	5
48.59	1330.01	269.32	1060.69	936.03	124.66	5
48.59	1330.01	269.32	1060.69	936.03	124.66	4
46.60	1529.95	337.49	1192.47	1060.12	132.35	4
44.62	1729.41	413.26	1316.15	1183.71	132.44	4
42.65	1928.31	499.71	1428.60	1306.75	121.85	4
40.69	2126.58	554.80	1571.79	1429.17	142.62	4
38.74	2324.18	612.58	1711.61	1550.91	160.70	4
36.80	2521.08	673.38	1847.70	1671.95	175.76	4
34.87	2717.23	737.46	1979.76	1792.24	187.53	4
32.96	2912.59	805.27	2107.33	1911.74	195.59	4
31.05	3107.12	877.79	2229.33	2030.41	198.92	4
31.05	3107.12	877.79	2229.33	2030.41	198.92	3
29.67	3255.68	936.52	2319.15	2117.11	202.04	3
28.28	3403.85	998.34	2405.52	2203.43	202.09	3
26.91	3551.63	1068.52	2483.12	2289.35	193.77	3
25.53	3699.03	1136.33	2562.69	2374.88	187.81	3
24.17	3846.04	1201.90	2644.15	2460.04	184.11	3
22.81	3992.70	1265.41	2727.29	2544.83	182.46	3
21.46	4139.00	1327.24	2811.76	2629.28	182.48	3
20.11	4284.96	1387.76	2897.19	2713.38	183.82	3
18.77	4430.58	1447.04	2983.54	2797.14	186.40	3
18.77	4430.58	1447.04	2983.54	2797.14	186.40	2

16.85	4636.16	1527.99	3108.17	2916.62	191.55	2
14.95	4841.25	1610.17	3231.07	3035.61	195.46	2
13.05	5045.82	1693.91	3351.91	3154.09	197.83	2
11.16	5249.87	1778.64	3471.23	3272.04	199.19	2
9.28	5453.40	1864.74	3588.66	3389.47	199.19	2
7.40	5656.40	1953.69	3702.70	3506.37	196.33	2
5.54	5858.83	2069.51	3789.32	3622.71	166.61	2
3.68	6060.69	2211.22	3849.47	3738.47	111.00	2
1.84	6261.96	2353.46	3908.51	3853.64	54.86	2
.00	6462.66	2493.95	3968.71	3968.24	.47	2

Time = 730. Degree of Consolidation = 38.%

Total Settlement = .649

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 730. = .649

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.82	202.52	228.30	228.30	.00	1

Time = 730. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 730. = .121

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.61

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.75	21.42	6.50	5.91	5.89	6
60.02	59.23	21.35	6.49	5.93	5.87	6
59.45	58.70	21.27	6.47	5.94	5.86	6
58.89	58.18	21.20	6.46	5.95	5.85	6
58.33	57.65	21.12	6.44	5.97	5.83	6
57.76	57.13	21.05	6.43	5.98	5.82	6
57.20	56.60	20.97	6.42	5.99	5.80	6
56.64	56.07	20.90	6.40	5.99	5.79	6
56.08	55.54	20.82	6.39	6.00	5.78	6
56.08	55.54	20.82	4.51	4.19	4.01	5
54.82	54.34	20.59	4.44	4.14	3.94	5
53.56	53.16	20.36	4.38	4.08	3.88	5
52.32	51.99	20.12	4.32	4.03	3.81	5
51.10	50.83	19.89	4.25	3.97	3.75	5
49.88	49.69	19.66	4.19	3.91	3.69	5
48.69	48.56	19.43	4.13	3.84	3.62	5
48.69	48.56	19.43	1.93	1.91	1.90	4
46.69	46.57	18.75	1.92	1.90	1.88	4
44.70	44.59	18.06	1.91	1.89	1.87	4
42.72	42.63	17.38	1.89	1.87	1.85	4
40.75	40.67	16.70	1.88	1.86	1.82	4
38.79	38.72	16.01	1.86	1.84	1.80	4
36.85	36.78	15.33	1.84	1.83	1.78	4
34.91	34.86	14.65	1.82	1.81	1.76	4
33.00	32.95	13.97	1.80	1.79	1.74	4
31.09	31.05	13.28	1.78	1.77	1.72	4
31.09	31.05	13.28	1.47	1.47	1.44	3
29.70	29.66	12.72	1.46	1.46	1.43	3
28.32	28.27	12.16	1.45	1.45	1.42	3
26.94	26.90	11.59	1.44	1.44	1.41	3
25.57	25.53	11.03	1.43	1.43	1.40	3
24.21	24.16	10.47	1.42	1.42	1.39	3
22.84	22.80	9.90	1.41	1.41	1.38	3
21.49	21.45	9.34	1.40	1.40	1.37	3
20.14	20.10	8.78	1.39	1.39	1.36	3
18.80	18.76	8.21	1.38	1.38	1.35	3
18.80	18.76	8.21	1.34	1.34	1.31	2
16.88	16.85	7.39	1.33	1.33	1.30	2
14.97	14.94	6.57	1.32	1.32	1.29	2
13.07	13.04	5.75	1.31	1.31	1.28	2
11.18	11.15	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.75	430.81	193.87	236.95	228.30	8.65	6
59.23	468.07	189.28	278.79	260.93	17.86	6
58.70	505.38	184.83	320.55	293.63	26.92	6

58.18	542.76	180.61	362.16	326.39	35.77	6
57.65	580.20	176.67	403.53	359.20	44.33	6
57.13	617.69	173.10	444.59	392.07	52.52	6
56.60	655.23	169.95	485.28	424.99	60.28	6
56.07	692.81	167.31	525.50	457.95	67.55	6
55.54	730.42	165.23	565.19	490.94	74.24	6
55.54	730.42	165.23	565.19	490.94	74.24	5
54.34	830.87	186.72	644.15	565.64	78.51	5
53.16	930.54	208.87	721.67	639.56	82.11	5
51.99	1029.40	231.72	797.68	712.67	85.01	5
50.83	1127.43	255.27	872.16	784.95	87.21	5
49.69	1224.60	279.53	945.07	856.37	88.70	5
48.56	1320.88	304.49	1016.39	926.91	89.48	5
48.56	1320.88	304.49	1016.39	926.91	89.48	4
46.57	1520.58	373.30	1147.28	1050.75	96.54	4
44.59	1719.79	449.80	1269.99	1174.09	95.90	4
42.63	1918.44	520.36	1398.08	1296.89	101.20	4
40.67	2116.48	573.46	1543.02	1419.07	123.95	4
38.72	2313.87	629.10	1684.78	1540.60	144.18	4
36.78	2510.59	687.48	1823.10	1661.45	161.65	4
34.86	2706.58	749.14	1957.44	1781.59	175.85	4
32.95	2901.82	814.86	2086.96	1900.97	185.99	4
31.05	3096.24	885.85	2210.39	2019.53	190.86	4
31.05	3096.24	885.85	2210.39	2019.53	190.86	3
29.66	3244.75	943.17	2301.58	2106.18	195.40	3
28.27	3392.89	1004.34	2388.55	2192.46	196.09	3
26.90	3540.64	1073.91	2466.73	2278.35	188.38	3
25.53	3688.00	1141.41	2546.59	2363.86	182.74	3
24.16	3834.99	1207.04	2627.95	2448.99	178.97	3
22.80	3981.61	1270.68	2710.94	2533.75	177.19	3
21.45	4127.89	1332.51	2795.37	2618.16	177.21	3
20.10	4273.81	1393.03	2880.78	2702.23	178.55	3
18.76	4419.41	1452.10	2967.30	2785.97	181.33	3
18.76	4419.41	1452.10	2967.30	2785.97	181.33	2
16.85	4624.96	1532.59	3092.38	2905.42	186.95	2
14.94	4830.02	1614.30	3215.72	3024.38	191.34	2
13.04	5034.57	1697.56	3337.01	3142.84	194.18	2
11.15	5238.60	1782.74	3455.85	3260.77	195.09	2
9.27	5442.10	1870.33	3571.77	3378.17	193.60	2
7.40	5645.06	1960.89	3684.17	3495.03	189.14	2
5.54	5847.44	2081.08	3766.36	3611.32	155.04	2
3.68	6049.25	2221.54	3827.71	3727.03	100.68	2
1.84	6250.50	2359.39	3891.11	3842.17	48.94	2
.00	6451.18	2494.00	3957.17	3956.76	.42	2

Time = 1080. Degree of Consolidation = 49.%

Total Settlement = .833

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 1080. = .833

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.81	202.52	228.30	228.30	.00	1

Time = 1080. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 1080. = .121

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.43

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.59	21.42	6.50	5.91	5.89	6
60.02	59.07	21.35	6.49	5.91	5.87	6
59.45	58.55	21.27	6.47	5.92	5.86	6
58.89	58.02	21.20	6.46	5.92	5.85	6
58.33	57.50	21.12	6.44	5.92	5.83	6
57.76	56.98	21.05	6.43	5.93	5.82	6
57.20	56.45	20.97	6.42	5.93	5.80	6
56.64	55.93	20.90	6.40	5.93	5.79	6
56.08	55.41	20.82	6.39	5.93	5.78	6
56.08	55.41	20.82	4.51	4.13	4.01	5
54.82	54.23	20.59	4.44	4.07	3.94	5
53.56	53.06	20.36	4.38	4.02	3.88	5
52.32	51.90	20.12	4.32	3.96	3.81	5
51.10	50.76	19.89	4.25	3.90	3.75	5
49.88	49.63	19.66	4.19	3.83	3.69	5
48.69	48.52	19.43	4.13	3.77	3.62	5
48.69	48.52	19.43	1.93	1.91	1.90	4
46.69	46.53	18.75	1.92	1.90	1.88	4
44.70	44.56	18.06	1.91	1.88	1.87	4
42.72	42.60	17.38	1.89	1.87	1.85	4
40.75	40.64	16.70	1.88	1.85	1.82	4

38.79	38.70	16.01	1.86	1.84	1.80	4
36.85	36.76	15.33	1.84	1.82	1.78	4
34.91	34.84	14.65	1.82	1.81	1.76	4
33.00	32.93	13.97	1.80	1.79	1.74	4
31.09	31.03	13.28	1.78	1.77	1.72	4
31.09	31.03	13.28	1.47	1.47	1.44	3
29.70	29.65	12.72	1.46	1.46	1.43	3
28.32	28.26	12.16	1.45	1.45	1.42	3
26.94	26.89	11.59	1.44	1.44	1.41	3
25.57	25.52	11.03	1.43	1.43	1.40	3
24.21	24.16	10.47	1.42	1.42	1.39	3
22.84	22.80	9.90	1.41	1.41	1.38	3
21.49	21.45	9.34	1.40	1.40	1.37	3
20.14	20.10	8.78	1.39	1.39	1.36	3
18.80	18.76	8.21	1.38	1.38	1.35	3
18.80	18.76	8.21	1.34	1.34	1.31	2
16.88	16.84	7.39	1.33	1.33	1.30	2
14.97	14.94	6.57	1.32	1.32	1.29	2
13.07	13.04	5.75	1.31	1.31	1.28	2
11.18	11.15	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.28	1.26	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.59	430.81	196.57	234.24	228.30	5.95	6
59.07	468.01	194.87	273.14	260.87	12.26	6
58.55	505.22	193.29	311.94	293.47	18.47	6
58.02	542.46	191.89	350.58	326.09	24.49	6
57.50	579.72	190.71	389.01	358.72	30.29	6
56.98	616.99	189.83	427.16	391.37	35.79	6
56.45	654.27	189.29	464.98	424.04	40.95	6
55.93	691.56	189.15	502.41	456.70	45.71	6
55.41	728.85	189.46	539.38	489.37	50.02	6
55.41	728.85	189.46	539.38	489.37	50.02	5
54.23	828.40	212.42	615.98	563.17	52.81	5
53.06	927.12	235.79	691.33	636.14	55.18	5
51.90	1025.00	259.60	765.40	708.27	57.13	5
50.76	1122.01	283.86	838.16	779.53	58.62	5
49.63	1218.15	308.56	909.59	849.92	59.67	5
48.52	1313.39	333.70	979.69	919.41	60.28	5
48.52	1313.39	333.70	979.69	919.41	60.28	4
46.53	1512.88	404.15	1108.73	1043.05	65.69	4
44.56	1711.87	482.56	1229.32	1166.18	63.14	4
42.60	1910.30	539.35	1370.95	1288.74	82.21	4
40.64	2108.12	591.27	1516.85	1410.70	106.15	4
38.70	2305.31	645.51	1659.80	1532.03	127.77	4
36.76	2501.83	702.52	1799.31	1652.70	146.61	4
34.84	2697.66	762.81	1934.84	1772.66	162.18	4
32.93	2892.74	827.17	2065.57	1891.89	173.68	4
31.03	3087.02	897.08	2189.94	2010.31	179.63	4
31.03	3087.02	897.09	2189.94	2010.31	179.63	3
29.65	3235.46	953.37	2282.10	2096.89	185.20	3
28.26	3383.54	1014.47	2369.07	2183.11	185.96	3
26.89	3531.24	1082.45	2448.79	2268.95	179.84	3
25.52	3678.55	1148.78	2529.78	2354.41	175.37	3
24.16	3825.50	1213.47	2612.03	2439.50	172.53	3

22.80	3972.09	1276.53	2695.57	2524.23	171.34	3
21.45	4118.33	1338.13	2780.20	2608.61	171.59	3
20.10	4264.23	1398.45	2865.78	2692.65	173.13	3
18.76	4409.79	1457.56	2952.23	2776.35	175.88	3
18.76	4409.79	1457.56	2952.23	2776.35	175.88	2
16.84	4615.31	1538.21	3077.10	2895.78	181.33	2
14.94	4820.34	1620.11	3200.23	3014.70	185.53	2
13.04	5024.85	1703.58	3321.27	3133.12	188.15	2
11.15	5228.84	1789.02	3439.82	3251.01	188.81	2
9.27	5432.31	1876.89	3555.41	3368.38	187.04	2
7.40	5635.22	1967.80	3667.42	3485.19	182.23	2
5.53	5837.56	2090.77	3746.79	3601.44	145.35	2
3.68	6039.34	2228.55	3810.80	3717.12	93.68	2
1.84	6240.56	2363.58	3876.97	3832.24	44.74	2
.00	6441.23	2494.04	3947.19	3946.81	.38	2

Time = 1440. Degree of Consolidation = 58.%

Total Settlement = .993

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 1440. = .993

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.81	202.52	228.30	228.30	.00	1

Time = 1440. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 1440. = .121

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.27

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.45	21.42	6.50	5.90	5.89	6
60.02	58.93	21.35	6.49	5.90	5.87	6
59.45	58.41	21.27	6.47	5.89	5.86	6
58.89	57.88	21.20	6.46	5.89	5.85	6
58.33	57.36	21.12	6.44	5.89	5.83	6
57.76	56.84	21.05	6.43	5.88	5.82	6
57.20	56.32	20.97	6.42	5.88	5.80	6
56.64	55.80	20.90	6.40	5.87	5.79	6
56.08	55.29	20.82	6.39	5.87	5.78	6
56.08	55.29	20.82	4.51	4.08	4.01	5
54.82	54.12	20.59	4.44	4.02	3.94	5
53.56	52.96	20.36	4.38	3.96	3.88	5
52.32	51.82	20.12	4.32	3.90	3.81	5
51.10	50.69	19.89	4.25	3.83	3.75	5
49.88	49.57	19.66	4.19	3.77	3.69	5
48.69	48.48	19.43	4.13	3.71	3.62	5
48.69	48.48	19.43	1.93	1.90	1.90	4
46.69	46.50	18.75	1.92	1.89	1.88	4
44.70	44.53	18.06	1.91	1.88	1.87	4
42.72	42.57	17.38	1.89	1.86	1.85	4
40.75	40.62	16.70	1.88	1.85	1.82	4
38.79	38.67	16.01	1.86	1.83	1.80	4
36.85	36.74	15.33	1.84	1.82	1.78	4
34.91	34.82	14.65	1.82	1.80	1.76	4
33.00	32.92	13.97	1.80	1.78	1.74	4
31.09	31.02	13.28	1.78	1.77	1.72	4
31.09	31.02	13.28	1.47	1.47	1.44	3
29.70	29.63	12.72	1.46	1.46	1.43	3
28.32	28.25	12.16	1.45	1.45	1.42	3
26.94	26.88	11.59	1.44	1.44	1.41	3
25.57	25.51	11.03	1.43	1.42	1.40	3
24.21	24.15	10.47	1.42	1.41	1.39	3
22.84	22.79	9.90	1.41	1.40	1.38	3
21.49	21.44	9.34	1.40	1.39	1.37	3
20.14	20.09	8.78	1.39	1.39	1.36	3
18.80	18.75	8.21	1.38	1.38	1.35	3
18.80	18.75	8.21	1.34	1.33	1.31	2
16.88	16.84	7.39	1.33	1.32	1.30	2
14.97	14.93	6.57	1.32	1.31	1.29	2
13.07	13.04	5.75	1.31	1.30	1.28	2
11.18	11.15	4.93	1.30	1.29	1.27	2
9.30	9.27	4.11	1.29	1.28	1.26	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.45	430.81	198.90	231.91	228.30	3.62	6
58.93	467.96	199.68	268.28	260.82	7.46	6
58.41	505.09	200.55	304.53	293.33	11.20	6
57.88	542.21	201.56	340.64	325.83	14.82	6
57.36	579.31	202.75	376.55	358.31	18.24	6
56.84	616.39	204.17	412.22	390.77	21.45	6
56.32	653.45	205.86	447.60	423.21	24.38	6
55.80	690.49	207.85	482.64	455.63	27.01	6
55.29	727.49	210.20	517.30	488.01	29.28	6
55.29	727.49	210.20	517.30	488.01	29.28	5
54.12	826.28	234.46	591.82	561.05	30.77	5
52.96	924.19	258.92	665.27	633.21	32.06	5
51.82	1021.22	283.61	737.61	704.49	33.12	5
50.69	1117.36	308.54	808.82	774.88	33.94	5
49.57	1212.60	333.70	878.90	844.37	34.52	5
48.48	1306.94	359.11	947.83	912.96	34.87	5
48.48	1306.94	359.11	947.83	912.96	34.87	4
46.50	1506.25	431.86	1074.39	1036.41	37.98	4
44.53	1705.04	507.21	1197.83	1159.35	38.49	4
42.57	1903.26	556.92	1346.34	1281.70	64.64	4
40.62	2100.87	608.37	1492.51	1403.46	89.05	4
38.67	2297.86	661.86	1636.00	1524.59	111.41	4
36.74	2494.19	717.96	1776.24	1645.06	131.18	4
34.82	2689.84	777.38	1912.46	1764.85	147.61	4
32.92	2884.75	840.94	2043.82	1883.90	159.91	4
31.02	3078.88	910.24	2168.63	2002.16	166.47	4
31.02	3078.88	910.24	2168.63	2002.16	166.47	3
29.63	3227.24	965.92	2261.32	2088.67	172.65	3
28.25	3375.24	1027.40	2347.84	2174.81	173.03	3
26.88	3522.87	1093.66	2429.20	2260.58	168.62	3
25.51	3670.12	1158.70	2511.42	2345.98	165.44	3
24.15	3817.02	1222.35	2594.68	2431.02	163.66	3
22.79	3963.56	1284.77	2678.79	2515.70	163.09	3
21.44	4109.76	1345.98	2763.77	2600.04	163.74	3
20.09	4255.61	1405.94	2849.67	2684.03	165.64	3
18.75	4401.13	1464.80	2936.33	2767.69	168.64	3
18.75	4401.13	1464.80	2936.33	2767.69	168.64	2
16.84	4606.61	1545.06	3061.55	2887.07	174.48	2
14.93	4811.59	1626.57	3185.02	3005.96	179.06	2
13.04	5016.07	1709.67	3306.39	3124.33	182.06	2
11.15	5220.02	1794.74	3425.28	3242.19	183.09	2
9.27	5423.45	1882.25	3541.20	3359.52	181.68	2
7.40	5626.33	1972.80	3653.53	3476.30	177.23	2
5.53	5828.65	2097.52	3731.13	3592.52	138.61	2
3.68	6030.40	2234.34	3796.06	3708.18	87.88	2
1.84	6231.60	2366.43	3865.17	3823.28	41.89	2
.00	6432.27	2494.06	3938.21	3937.85	.36	2

Time = 1825. Degree of Consolidation = 67.%

Total Settlement = 1.136

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 1825. = 1.136

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.81	202.52	228.30	228.30	.00	1

Time = 1825. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 1825. = .121

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.12

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.23	21.42	6.50	5.89	5.89	6
60.02	58.71	21.35	6.49	5.87	5.87	6
59.45	58.20	21.27	6.47	5.86	5.86	6
58.89	57.68	21.20	6.46	5.85	5.85	6
58.33	57.16	21.12	6.44	5.83	5.83	6
57.76	56.64	21.05	6.43	5.82	5.82	6
57.20	56.13	20.97	6.42	5.80	5.80	6
56.64	55.62	20.90	6.40	5.79	5.79	6
56.08	55.10	20.82	6.39	5.78	5.78	6
56.08	55.10	20.82	4.51	4.01	4.01	5
54.82	53.95	20.59	4.44	3.94	3.94	5
53.56	52.81	20.36	4.38	3.88	3.88	5
52.32	51.69	20.12	4.32	3.81	3.81	5
51.10	50.58	19.89	4.25	3.75	3.75	5
49.88	49.49	19.66	4.19	3.69	3.69	5
48.69	48.41	19.43	4.13	3.62	3.62	5

48.69	48.41	19.43	1.93	1.90	1.90	4
46.69	46.43	18.75	1.92	1.88	1.88	4
44.70	44.47	18.06	1.91	1.87	1.87	4
42.72	42.51	17.38	1.89	1.86	1.85	4
40.75	40.57	16.70	1.88	1.84	1.82	4
38.79	38.63	16.01	1.86	1.83	1.80	4
36.85	36.70	15.33	1.84	1.81	1.78	4
34.91	34.79	14.65	1.82	1.80	1.76	4
33.00	32.89	13.97	1.80	1.78	1.74	4
31.09	31.00	13.28	1.78	1.76	1.72	4
31.09	31.00	13.28	1.47	1.46	1.44	3
29.70	29.61	12.72	1.46	1.45	1.43	3
28.32	28.23	12.16	1.45	1.44	1.42	3
26.94	26.86	11.59	1.44	1.43	1.41	3
25.57	25.49	11.03	1.43	1.42	1.40	3
24.21	24.13	10.47	1.42	1.41	1.39	3
22.84	22.78	9.90	1.41	1.40	1.38	3
21.49	21.43	9.34	1.40	1.39	1.37	3
20.14	20.08	8.78	1.39	1.38	1.36	3
18.80	18.74	8.21	1.38	1.37	1.35	3
18.80	18.74	8.21	1.34	1.33	1.31	2
16.88	16.83	7.39	1.33	1.32	1.30	2
14.97	14.93	6.57	1.32	1.31	1.29	2
13.07	13.03	5.75	1.31	1.30	1.28	2
11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.27	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.23	430.81	202.52	228.30	228.30	.00	6
58.71	467.87	207.14	260.74	260.74	.00	6
58.20	504.87	211.76	293.11	293.11	.00	6
57.68	541.79	216.38	325.42	325.42	.00	6
57.16	578.65	221.00	357.66	357.66	.00	6
56.64	615.45	225.62	389.83	389.83	.00	6
56.13	652.18	230.24	421.94	421.94	.00	6
55.62	688.84	234.86	453.98	453.98	.00	6
55.10	725.44	239.48	485.96	485.96	.00	6
55.10	725.44	239.48	485.96	485.96	.00	5
53.95	823.14	265.23	557.91	557.91	.00	5
52.81	919.92	290.98	628.94	628.94	.00	5
51.69	1015.77	316.73	699.04	699.04	.00	5
50.58	1110.70	342.48	768.22	768.22	.00	5
49.49	1204.70	368.23	836.47	836.47	.00	5
48.41	1297.78	393.98	903.80	903.80	.00	5
48.41	1297.78	393.98	903.80	903.80	.00	4
46.43	1496.85	469.84	1027.01	1027.01	.00	4
44.47	1695.36	532.23	1163.13	1149.66	13.46	4
42.51	1893.27	582.89	1310.38	1271.72	38.67	4
40.57	2090.57	634.48	1456.10	1393.16	62.94	4
38.63	2287.25	687.69	1599.56	1513.98	85.59	4
36.70	2483.28	743.21	1740.07	1634.15	105.92	4
34.79	2678.63	801.97	1876.66	1753.64	123.02	4
32.89	2873.25	865.07	2008.18	1872.40	135.78	4
31.00	3067.09	934.08	2133.00	1990.38	142.63	4
31.00	3067.09	934.09	2133.00	1990.38	142.63	3

29.61	3215.30	989.41	2225.89	2076.73	149.16	3
28.23	3363.15	1052.74	2310.41	2162.73	147.69	3
26.86	3510.65	1116.71	2393.94	2248.36	145.58	3
25.49	3657.78	1179.59	2478.19	2333.63	144.56	3
24.13	3804.56	1241.54	2563.02	2418.56	144.46	3
22.78	3951.00	1302.37	2648.63	2503.14	145.49	3
21.43	4097.10	1362.24	2734.86	2587.38	147.48	3
20.08	4242.87	1421.30	2821.57	2671.29	150.28	3
18.74	4388.30	1479.54	2908.77	2754.86	153.90	3
18.74	4388.30	1479.54	2908.77	2754.86	153.90	2
16.83	4593.69	1558.74	3034.95	2874.16	160.79	2
14.93	4798.59	1639.22	3159.38	2992.96	166.42	2
13.03	5002.99	1721.27	3281.72	3111.26	170.46	2
11.14	5206.88	1805.29	3401.60	3229.05	172.54	2
9.27	5410.25	1891.74	3518.52	3346.32	172.19	2
7.39	5613.08	1981.20	3631.88	3463.05	168.83	2
5.53	5815.34	2108.11	3707.23	3579.22	128.01	2
3.68	6017.06	2241.38	3775.68	3694.84	80.84	2
1.84	6218.24	2369.89	3848.35	3809.92	38.44	2
.00	6418.90	2494.09	3924.81	3924.48	.33	2

Time = 2520. Degree of Consolidation = 79.%

Total Settlement = 1.351

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 2520. = 1.349

Settlement caused by Secondary Compression at time 2520. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.78	3.66	1.91
2.84	2.73	1.43
1.89	1.82	.95
.94	.91	.48
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.66	.00	.00
2.73	108.47	50.63
1.82	216.11	101.26
.91	323.53	151.89
.00	430.81	202.52

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
57.84	57.84	.00	1
114.85	114.85	.00	1
171.65	171.65	.00	1
228.30	228.30	.00	1

Time = 2520. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 2520. = .121

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .91

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.21	21.42	6.50	5.89	5.89	6
60.02	58.69	21.35	6.49	5.87	5.87	6
59.45	58.17	21.27	6.47	5.86	5.86	6
58.89	57.65	21.20	6.46	5.84	5.85	6
58.33	57.13	21.12	6.44	5.83	5.83	6
57.76	56.62	21.05	6.43	5.82	5.82	6
57.20	56.10	20.97	6.42	5.80	5.80	6
56.64	55.59	20.90	6.40	5.79	5.79	6
56.08	55.08	20.82	6.39	5.77	5.78	6
56.08	55.08	20.82	4.51	4.01	4.01	5
54.82	53.92	20.59	4.44	3.94	3.94	5
53.56	52.79	20.36	4.38	3.88	3.88	5
52.32	51.66	20.12	4.32	3.81	3.81	5
51.10	50.55	19.89	4.25	3.75	3.75	5
49.88	49.46	19.66	4.19	3.69	3.69	5
48.69	48.38	19.43	4.13	3.62	3.62	5
48.69	48.38	19.43	1.93	1.90	1.90	4
46.69	46.41	18.75	1.92	1.88	1.88	4
44.70	44.44	18.06	1.91	1.87	1.87	4
42.72	42.49	17.38	1.89	1.86	1.85	4
40.75	40.54	16.70	1.88	1.84	1.82	4
38.79	38.61	16.01	1.86	1.82	1.80	4
36.85	36.68	15.33	1.84	1.81	1.78	4
34.91	34.77	14.65	1.82	1.79	1.76	4
33.00	32.87	13.97	1.80	1.77	1.74	4
31.09	30.98	13.28	1.78	1.76	1.72	4
31.09	30.98	13.28	1.47	1.46	1.44	3
29.70	29.60	12.72	1.46	1.45	1.43	3
28.32	28.22	12.16	1.45	1.44	1.42	3
26.94	26.85	11.59	1.44	1.43	1.41	3
25.57	25.49	11.03	1.43	1.42	1.40	3
24.21	24.13	10.47	1.42	1.41	1.39	3
22.84	22.77	9.90	1.41	1.40	1.38	3
21.49	21.42	9.34	1.40	1.39	1.37	3
20.14	20.08	8.78	1.39	1.38	1.36	3
18.80	18.74	8.21	1.38	1.37	1.35	3
18.80	18.74	8.21	1.34	1.33	1.31	2
16.88	16.83	7.39	1.33	1.32	1.30	2
14.97	14.93	6.57	1.32	1.31	1.29	2
13.07	13.03	5.75	1.31	1.30	1.28	2
11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2

1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.21	430.81	202.52	228.30	228.30	.00	6
58.69	467.87	207.14	260.73	260.73	.00	6
58.17	504.85	211.76	293.10	293.10	.00	6
57.65	541.77	216.38	325.39	325.39	.00	6
57.13	578.62	221.00	357.63	357.63	.00	6
56.62	615.41	225.62	389.79	389.79	.00	6
56.10	652.13	230.24	421.89	421.89	.00	6
55.59	688.79	234.86	453.93	453.93	.00	6
55.08	725.37	239.48	485.90	485.90	.00	6
55.08	725.37	239.48	485.90	485.90	.00	5
53.92	823.07	265.23	557.84	557.84	.00	5
52.79	919.83	290.98	628.85	628.85	.00	5
51.66	1015.67	316.73	698.94	698.94	.00	5
50.55	1110.59	342.48	768.11	768.11	.00	5
49.46	1204.58	368.23	836.35	836.35	.00	5
48.38	1297.65	393.98	903.67	903.67	.00	5
48.38	1297.65	393.98	903.67	903.67	.00	4
46.41	1496.72	469.84	1026.88	1026.88	.00	4
44.44	1695.21	534.97	1160.24	1149.52	10.73	4
42.49	1893.08	588.31	1304.76	1271.52	33.24	4
40.54	2090.30	642.12	1448.18	1392.88	55.30	4
38.61	2286.88	697.00	1589.87	1513.60	76.27	4
36.68	2482.79	753.79	1729.00	1633.65	95.34	4
34.77	2678.00	813.24	1864.76	1753.01	111.75	4
32.87	2872.49	876.69	1995.80	1871.64	124.16	4
30.98	3066.18	946.17	2120.01	1989.47	130.54	4
30.98	3066.18	946.17	2120.01	1989.47	130.54	3
29.60	3214.32	1001.88	2212.44	2075.75	136.69	3
28.22	3362.10	1066.15	2295.95	2161.67	134.28	3
26.85	3509.51	1129.20	2380.32	2247.23	133.09	3
25.49	3656.58	1191.21	2465.37	2332.44	132.93	3
24.13	3803.30	1252.35	2550.95	2417.30	133.65	3
22.77	3949.68	1312.45	2637.24	2501.82	135.42	3
21.42	4095.73	1371.62	2724.11	2586.01	138.10	3
20.08	4241.44	1430.02	2811.42	2669.86	141.56	3
18.74	4386.83	1487.81	2899.02	2753.39	145.63	3
18.74	4386.83	1487.81	2899.02	2753.39	145.63	2
16.83	4592.17	1565.98	3026.20	2872.64	153.56	2
14.93	4797.03	1645.88	3151.15	2991.40	159.76	2
13.03	5001.39	1727.36	3274.03	3109.66	164.37	2
11.14	5205.25	1810.81	3394.44	3227.42	167.02	2
9.26	5408.58	1896.67	3511.91	3344.65	167.26	2
7.39	5611.38	1985.54	3625.84	3461.35	164.49	2
5.53	5813.62	2113.54	3700.08	3577.49	122.59	2
3.68	6015.32	2244.92	3770.40	3693.09	77.31	2
1.84	6216.48	2371.62	3844.86	3808.16	36.70	2
.00	6417.14	2494.11	3923.04	3922.72	.31	2

Time = 2880. Degree of Consolidation = 81.%

Total Settlement = 1.379

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 2880. = 1.375

Settlement caused by Secondary Compression at time 2880. = .004

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.81	202.52	228.30	228.30	.00	1

Time = 2880. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 2880. = .121

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .88

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.18	21.42	6.50	5.89	5.89	6
60.02	58.66	21.35	6.49	5.87	5.87	6
59.45	58.14	21.27	6.47	5.86	5.86	6
58.89	57.62	21.20	6.46	5.84	5.85	6
58.33	57.11	21.12	6.44	5.83	5.83	6
57.76	56.59	21.05	6.43	5.81	5.82	6
57.20	56.08	20.97	6.42	5.80	5.80	6
56.64	55.57	20.90	6.40	5.79	5.79	6
56.08	55.05	20.82	6.39	5.77	5.78	6
56.08	55.05	20.82	4.51	4.01	4.01	5
54.82	53.90	20.59	4.44	3.94	3.94	5

53.56	52.76	20.36	4.38	3.88	3.88	5
52.32	51.64	20.12	4.32	3.81	3.81	5
51.10	50.53	19.89	4.25	3.75	3.75	5
49.88	49.44	19.66	4.19	3.68	3.69	5
48.69	48.36	19.43	4.13	3.62	3.62	5
48.69	48.36	19.43	1.93	1.90	1.90	4
46.69	46.38	18.75	1.92	1.88	1.88	4
44.70	44.42	18.06	1.91	1.87	1.87	4
42.72	42.46	17.38	1.89	1.85	1.85	4
40.75	40.52	16.70	1.88	1.84	1.82	4
38.79	38.59	16.01	1.86	1.82	1.80	4
36.85	36.66	15.33	1.84	1.81	1.78	4
34.91	34.75	14.65	1.82	1.79	1.76	4
33.00	32.85	13.97	1.80	1.77	1.74	4
31.09	30.97	13.28	1.78	1.75	1.72	4
31.09	30.97	13.28	1.47	1.46	1.44	3
29.70	29.59	12.72	1.46	1.45	1.43	3
28.32	28.21	12.16	1.45	1.44	1.42	3
26.94	26.84	11.59	1.44	1.43	1.41	3
25.57	25.48	11.03	1.43	1.42	1.40	3
24.21	24.12	10.47	1.42	1.41	1.39	3
22.84	22.76	9.90	1.41	1.40	1.38	3
21.49	21.42	9.34	1.40	1.39	1.37	3
20.14	20.07	8.78	1.39	1.38	1.36	3
18.80	18.73	8.21	1.38	1.37	1.35	3
18.80	18.73	8.21	1.34	1.33	1.31	2
16.88	16.82	7.39	1.33	1.32	1.30	2
14.97	14.92	6.57	1.32	1.31	1.29	2
13.07	13.03	5.75	1.31	1.30	1.28	2
11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.18	430.81	202.52	228.30	228.30	.00	6
58.66	467.86	207.14	260.73	260.73	.00	6
58.14	504.84	211.76	293.08	293.08	.00	6
57.62	541.75	216.38	325.37	325.37	.00	6
57.11	578.59	221.00	357.60	357.60	.00	6
56.59	615.37	225.62	389.75	389.75	.00	6
56.08	652.08	230.24	421.85	421.85	.00	6
55.57	688.73	234.86	453.87	453.87	.00	6
55.05	725.31	239.48	485.83	485.83	.00	6
55.05	725.31	239.48	485.83	485.83	.00	5
53.90	823.00	265.23	557.77	557.77	.00	5
52.76	919.76	290.98	628.78	628.78	.00	5
51.64	1015.59	316.73	698.86	698.86	.00	5
50.53	1110.50	342.48	768.02	768.02	.00	5
49.44	1204.48	368.23	836.25	836.25	.00	5
48.36	1297.53	393.98	903.55	903.55	.00	5
48.36	1297.53	393.98	903.55	903.55	.00	4
46.38	1496.61	469.84	1026.77	1026.77	.00	4
44.42	1695.09	536.57	1158.53	1149.40	9.13	4
42.46	1892.93	591.53	1301.39	1271.37	30.03	4
40.52	2090.10	646.98	1443.12	1392.69	50.44	4
38.59	2286.61	703.46	1583.15	1513.33	69.81	4

36.66	2482.43	761.66	1720.77	1633.30	87.47	4
34.75	2677.55	822.48	1855.07	1752.56	102.52	4
32.85	2871.92	887.29	1984.63	1871.06	113.57	4
30.97	3065.48	958.28	2107.20	1988.77	118.43	4
30.97	3065.48	958.28	2107.20	1988.77	118.43	3
29.59	3213.53	1015.45	2198.09	2074.96	123.12	3
28.21	3361.24	1078.92	2282.32	2160.81	121.51	3
26.84	3508.59	1141.22	2367.36	2246.30	121.06	3
25.48	3655.59	1202.54	2453.05	2331.44	121.61	3
24.12	3802.25	1263.03	2539.22	2416.24	122.97	3
22.76	3948.57	1322.48	2626.09	2500.71	125.38	3
21.42	4094.56	1381.05	2713.51	2584.84	128.67	3
20.07	4240.22	1438.88	2801.34	2668.64	132.70	3
18.73	4385.56	1496.13	2889.43	2752.12	137.31	3
18.73	4385.56	1496.13	2889.43	2752.12	137.31	2
16.82	4590.86	1573.21	3017.65	2871.32	146.33	2
14.92	4795.67	1652.53	3143.14	2990.04	153.10	2
13.03	4999.99	1733.44	3266.56	3108.26	158.30	2
11.14	5203.81	1816.29	3387.52	3225.98	161.54	2
9.26	5407.12	1901.56	3505.55	3343.19	162.37	2
7.39	5609.88	1989.82	3620.07	3459.86	160.21	2
5.53	5812.10	2118.85	3693.25	3575.98	117.28	2
3.68	6013.78	2248.38	3765.40	3691.56	73.84	2
1.84	6214.94	2373.32	3841.62	3806.62	35.00	2
.00	6415.59	2494.12	3921.47	3921.17	.30	2

Time = 3240. Degree of Consolidation = 82.%

Total Settlement = 1.404

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 3240. = 1.398

Settlement caused by Secondary Compression at time 3240. = .005

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.81	202.52	228.30	228.30	.00	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 3240. = .121

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .86

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.16	21.42	6.50	5.89	5.89	6
60.02	58.64	21.35	6.49	5.87	5.87	6
59.45	58.12	21.27	6.47	5.85	5.86	6
58.89	57.60	21.20	6.46	5.84	5.85	6
58.33	57.08	21.12	6.44	5.83	5.83	6
57.76	56.57	21.05	6.43	5.81	5.82	6
57.20	56.06	20.97	6.42	5.80	5.80	6
56.64	55.54	20.90	6.40	5.78	5.79	6
56.08	55.03	20.82	6.39	5.77	5.78	6
56.08	55.03	20.82	4.51	4.01	4.01	5
54.82	53.88	20.59	4.44	3.94	3.94	5
53.56	52.74	20.36	4.38	3.88	3.88	5
52.32	51.62	20.12	4.32	3.81	3.81	5
51.10	50.51	19.89	4.25	3.75	3.75	5
49.88	49.41	19.66	4.19	3.68	3.69	5
48.69	48.34	19.43	4.13	3.62	3.62	5
48.69	48.34	19.43	1.93	1.90	1.90	4
46.69	46.36	18.75	1.92	1.88	1.88	4
44.70	44.40	18.06	1.91	1.87	1.87	4
42.72	42.44	17.38	1.89	1.85	1.85	4
40.75	40.50	16.70	1.88	1.84	1.82	4
38.79	38.57	16.01	1.86	1.82	1.80	4
36.85	36.64	15.33	1.84	1.80	1.78	4
34.91	34.73	14.65	1.82	1.79	1.76	4
33.00	32.84	13.97	1.80	1.77	1.74	4
31.09	30.95	13.28	1.78	1.75	1.72	4
31.09	30.95	13.28	1.47	1.46	1.44	3
29.70	29.57	12.72	1.46	1.45	1.43	3
28.32	28.20	12.16	1.45	1.44	1.42	3
26.94	26.83	11.59	1.44	1.43	1.41	3
25.57	25.47	11.03	1.43	1.42	1.40	3
24.21	24.11	10.47	1.42	1.41	1.39	3
22.84	22.76	9.90	1.41	1.40	1.38	3
21.49	21.41	9.34	1.40	1.39	1.37	3
20.14	20.07	8.78	1.39	1.38	1.36	3
18.80	18.73	8.21	1.38	1.37	1.35	3
18.80	18.73	8.21	1.34	1.33	1.31	2
16.88	16.82	7.39	1.33	1.32	1.30	2
14.97	14.92	6.57	1.32	1.31	1.29	2
13.07	13.03	5.75	1.31	1.30	1.28	2

11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.16	430.81	202.52	228.30	228.30	.00	6
58.64	467.86	207.14	260.72	260.72	.00	6
58.12	504.82	211.76	293.07	293.07	.00	6
57.60	541.72	216.38	325.35	325.35	.00	6
57.08	578.56	221.00	357.56	357.56	.00	6
56.57	615.33	225.62	389.71	389.71	.00	6
56.06	652.03	230.24	421.79	421.79	.00	6
55.54	688.67	234.86	453.81	453.81	.00	6
55.03	725.24	239.48	485.76	485.76	.00	6
55.03	725.24	239.48	485.76	485.76	.00	5
53.88	822.93	265.23	557.70	557.70	.00	5
52.74	919.69	290.98	628.71	628.71	.00	5
51.62	1015.52	316.73	698.79	698.79	.00	5
50.51	1110.42	342.48	767.94	767.95	.00	5
49.41	1204.40	368.23	836.17	836.18	.00	5
48.34	1297.46	393.98	903.48	903.48	.00	5
48.34	1297.46	393.98	903.48	903.48	.00	4
46.36	1496.54	469.84	1026.70	1026.70	.00	4
44.40	1695.02	537.98	1157.04	1149.32	7.72	4
42.44	1892.82	594.37	1298.45	1271.27	27.18	4
40.50	2089.96	651.24	1438.72	1392.54	46.18	4
38.57	2286.40	709.17	1577.24	1513.13	64.11	4
36.64	2482.15	768.92	1713.23	1633.02	80.22	4
34.73	2677.17	831.37	1845.80	1752.18	93.63	4
32.84	2871.42	897.86	1973.56	1870.57	102.99	4
30.95	3064.84	970.75	2094.09	1988.13	105.96	4
30.95	3064.84	970.75	2094.09	1988.13	105.96	3
29.57	3212.82	1029.67	2183.16	2074.25	108.90	3
28.20	3360.45	1092.52	2267.92	2160.02	107.91	3
26.83	3507.72	1154.27	2353.46	2245.43	108.02	3
25.47	3654.65	1215.06	2439.59	2330.51	109.08	3
24.11	3801.24	1274.84	2526.40	2415.24	111.17	3
22.76	3947.50	1333.61	2613.89	2499.64	114.25	3
21.41	4093.43	1391.55	2701.88	2583.71	118.17	3
20.07	4239.03	1448.79	2790.25	2667.45	122.79	3
18.73	4384.32	1505.48	2878.84	2750.88	127.96	3
18.73	4384.32	1505.48	2878.84	2750.88	127.96	2
16.82	4589.56	1581.46	3008.11	2870.03	138.08	2
14.92	4794.33	1659.98	3134.35	2988.69	145.66	2
13.03	4998.61	1740.08	3258.53	3106.87	151.66	2
11.14	5202.39	1822.11	3380.27	3224.56	155.72	2
9.26	5405.66	1906.55	3499.11	3341.73	157.38	2
7.39	5608.40	1993.94	3614.46	3458.37	156.09	2
5.53	5810.59	2123.52	3687.08	3574.47	112.61	2
3.68	6012.26	2251.42	3760.83	3690.03	70.80	2
1.84	6213.40	2374.81	3838.59	3805.08	33.51	2
.00	6414.05	2494.13	3919.92	3919.63	.29	2

Time = 3650. Degree of Consolidation = 84.%

Total Settlement = 1.428

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 3650. = 1.422

Settlement caused by Secondary Compression at time 3650. = .007

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.78	3.66	1.91
2.84	2.73	1.43
1.89	1.82	.95
.94	.91	.48
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.66	.00	.00
2.73	108.47	50.63
1.82	216.11	101.26
.91	323.53	151.89
.00	430.81	202.52

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
57.84	57.84	.00	1
114.85	114.85	.00	1
171.65	171.65	.00	1
228.30	228.30	.00	1

Time = 3650. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 3650. = .121

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .83

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
60.58	59.12	21.42
60.02	58.60	21.35
59.45	58.08	21.27
58.89	57.56	21.20
58.33	57.05	21.12
57.76	56.53	21.05

***** Void Ratios *****

Einitial	E	Eeop	Material
6.50	5.89	5.89	6
6.49	5.86	5.87	6
6.47	5.85	5.86	6
6.46	5.84	5.85	6
6.44	5.82	5.83	6
6.43	5.81	5.82	6

57.20	56.02	20.97	6.42	5.79	5.80	6
56.64	55.51	20.90	6.40	5.78	5.79	6
56.08	55.00	20.82	6.39	5.77	5.78	6
56.08	55.00	20.82	4.51	4.01	4.01	5
54.82	53.84	20.59	4.44	3.94	3.94	5
53.56	52.70	20.36	4.38	3.88	3.88	5
52.32	51.58	20.12	4.32	3.81	3.81	5
51.10	50.47	19.89	4.25	3.75	3.75	5
49.88	49.38	19.66	4.19	3.68	3.69	5
48.69	48.30	19.43	4.13	3.62	3.62	5
48.69	48.30	19.43	1.93	1.90	1.90	4
46.69	46.33	18.75	1.92	1.88	1.88	4
44.70	44.36	18.06	1.91	1.87	1.87	4
42.72	42.41	17.38	1.89	1.85	1.85	4
40.75	40.47	16.70	1.88	1.84	1.82	4
38.79	38.53	16.01	1.86	1.82	1.80	4
36.85	36.61	15.33	1.84	1.80	1.78	4
34.91	34.71	14.65	1.82	1.78	1.76	4
33.00	32.81	13.97	1.80	1.76	1.74	4
31.09	30.93	13.28	1.78	1.74	1.72	4
31.09	30.93	13.28	1.47	1.45	1.44	3
29.70	29.55	12.72	1.46	1.44	1.43	3
28.32	28.18	12.16	1.45	1.43	1.42	3
26.94	26.81	11.59	1.44	1.42	1.41	3
25.57	25.45	11.03	1.43	1.41	1.40	3
24.21	24.09	10.47	1.42	1.40	1.39	3
22.84	22.74	9.90	1.41	1.39	1.38	3
21.49	21.40	9.34	1.40	1.38	1.37	3
20.14	20.06	8.78	1.39	1.38	1.36	3
18.80	18.72	8.21	1.38	1.37	1.35	3
18.80	18.72	8.21	1.34	1.33	1.31	2
16.88	16.81	7.39	1.33	1.32	1.30	2
14.97	14.91	6.57	1.32	1.31	1.29	2
13.07	13.02	5.75	1.31	1.30	1.28	2
11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.12	430.81	202.52	228.30	228.30	.00	6
58.60	467.85	207.14	260.71	260.71	.00	6
58.08	504.80	211.76	293.04	293.04	.00	6
57.56	541.68	216.38	325.31	325.31	.00	6
57.05	578.50	221.00	357.51	357.51	.00	6
56.53	615.26	225.62	389.64	389.64	.00	6
56.02	651.95	230.24	421.71	421.71	.00	6
55.51	688.57	234.86	453.71	453.71	.00	6
55.00	725.12	239.48	485.64	485.64	.00	6
55.00	725.12	239.48	485.64	485.64	.00	5
53.84	822.81	265.23	557.58	557.59	.00	5
52.70	919.57	290.98	628.59	628.59	.00	5
51.58	1015.40	316.73	698.67	698.67	.00	5
50.47	1110.31	342.48	767.83	767.83	.00	5
49.38	1204.29	368.23	836.06	836.06	.00	5
48.30	1297.34	393.98	903.36	903.36	.00	5
48.30	1297.34	393.98	903.36	903.36	.00	4

46.33	1496.42	469.84	1026.59	1026.59	.00	4
44.36	1694.89	539.67	1155.22	1149.19	6.02	4
42.41	1892.67	597.93	1294.74	1271.11	23.63	4
40.47	2089.75	656.81	1432.94	1392.33	40.61	4
38.53	2286.12	716.72	1569.40	1512.84	56.56	4
36.61	2481.76	778.45	1703.31	1632.63	70.68	4
34.71	2676.65	843.13	1833.52	1751.66	81.86	4
32.81	2870.75	912.21	1958.54	1869.90	88.64	4
30.93	3063.98	988.22	2075.76	1987.27	88.49	4
30.93	3063.98	988.22	2075.77	1987.27	88.49	3
29.55	3211.85	1050.08	2161.77	2073.28	88.49	3
28.18	3359.36	1112.76	2246.60	2158.93	87.67	3
26.81	3506.52	1174.02	2332.50	2244.23	88.27	3
25.45	3653.34	1234.02	2419.32	2329.20	90.12	3
24.09	3799.83	1292.93	2506.89	2413.82	93.07	3
22.74	3945.99	1350.91	2595.08	2498.12	96.96	3
21.40	4091.82	1408.10	2683.72	2582.10	101.62	3
20.06	4237.33	1464.65	2772.69	2665.75	106.93	3
18.72	4382.53	1520.68	2861.85	2749.09	112.76	3
18.72	4382.53	1520.68	2861.85	2749.09	112.76	2
16.81	4587.68	1595.43	2992.25	2868.15	124.10	2
14.91	4792.37	1672.60	3119.77	2986.73	133.04	2
13.02	4996.57	1751.32	3245.25	3104.84	140.41	2
11.14	5200.29	1831.97	3368.32	3222.46	145.86	2
9.26	5403.50	1914.97	3488.53	3339.57	148.96	2
7.39	5606.20	2001.28	3604.91	3456.17	148.74	2
5.53	5808.35	2131.32	3677.03	3572.23	104.81	2
3.68	6009.99	2256.51	3753.48	3687.77	65.72	2
1.84	6211.12	2377.31	3833.81	3802.80	31.01	2
.00	6411.77	2494.15	3917.62	3917.35	.27	2

Time = 4320. Degree of Consolidation = 86.%

Total Settlement = 1.465

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 4320. = 1.456

Settlement caused by Secondary Compression at time 4320. = .008

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.78	3.66	1.91
2.84	2.73	1.43
1.89	1.82	.95
.94	.91	.48
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.66	.00	.00
2.73	108.47	50.63

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
57.84	57.84	.00	1

1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.81	202.52	228.30	228.30	.00	1

Time = 4320. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 4320. = .121

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .79

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.08	21.42	6.50	5.89	5.89	6
60.02	58.57	21.35	6.49	5.86	5.87	6
59.45	58.05	21.27	6.47	5.85	5.86	6
58.89	57.53	21.20	6.46	5.83	5.85	6
58.33	57.02	21.12	6.44	5.82	5.83	6
57.76	56.50	21.05	6.43	5.81	5.82	6
57.20	55.99	20.97	6.42	5.79	5.80	6
56.64	55.47	20.90	6.40	5.78	5.79	6
56.08	54.96	20.82	6.39	5.76	5.78	6
56.08	54.96	20.82	4.51	4.01	4.01	5
54.82	53.81	20.59	4.44	3.94	3.94	5
53.56	52.67	20.36	4.38	3.88	3.88	5
52.32	51.55	20.12	4.32	3.81	3.81	5
51.10	50.44	19.89	4.25	3.75	3.75	5
49.88	49.35	19.66	4.19	3.68	3.69	5
48.69	48.27	19.43	4.13	3.62	3.62	5
48.69	48.27	19.43	1.93	1.90	1.90	4
46.69	46.29	18.75	1.92	1.88	1.88	4
44.70	44.33	18.06	1.91	1.87	1.87	4
42.72	42.38	17.38	1.89	1.85	1.85	4
40.75	40.43	16.70	1.88	1.83	1.82	4
38.79	38.50	16.01	1.86	1.82	1.80	4
36.85	36.59	15.33	1.84	1.80	1.78	4
34.91	34.68	14.65	1.82	1.78	1.76	4
33.00	32.79	13.97	1.80	1.76	1.74	4
31.09	30.91	13.28	1.78	1.74	1.72	4
31.09	30.91	13.28	1.47	1.45	1.44	3
29.70	29.53	12.72	1.46	1.44	1.43	3
28.32	28.16	12.16	1.45	1.43	1.42	3
26.94	26.80	11.59	1.44	1.42	1.41	3
25.57	25.44	11.03	1.43	1.41	1.40	3
24.21	24.08	10.47	1.42	1.40	1.39	3
22.84	22.73	9.90	1.41	1.39	1.38	3
21.49	21.39	9.34	1.40	1.38	1.37	3
20.14	20.05	8.78	1.39	1.37	1.36	3

18.80	18.71	8.21	1.38	1.36	1.35	3
18.80	18.71	8.21	1.34	1.33	1.31	2
16.88	16.81	7.39	1.33	1.32	1.30	2
14.97	14.91	6.57	1.32	1.31	1.29	2
13.07	13.02	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.08	430.81	202.52	228.30	228.30	.00	6
58.57	467.84	207.14	260.70	260.70	.00	6
58.05	504.77	211.76	293.01	293.01	.00	6
57.53	541.64	216.38	325.26	325.26	.00	6
57.02	578.44	221.00	357.45	357.45	.00	6
56.50	615.18	225.62	389.56	389.56	.00	6
55.99	651.85	230.24	421.61	421.61	.00	6
55.47	688.46	234.86	453.60	453.60	.00	6
54.96	725.00	239.48	485.52	485.52	.00	6
54.96	725.00	239.48	485.52	485.52	.00	5
53.81	822.69	265.23	557.46	557.46	.00	5
52.67	919.45	290.98	628.47	628.47	.00	5
51.55	1015.28	316.73	698.55	698.55	.00	5
50.44	1110.18	342.48	767.70	767.70	.00	5
49.35	1204.16	368.23	835.93	835.93	.00	5
48.27	1297.22	393.98	903.24	903.24	.00	5
48.27	1297.22	393.98	903.24	903.24	.00	4
46.29	1496.30	469.84	1026.46	1026.46	.00	4
44.33	1694.76	541.16	1153.60	1149.06	4.53	4
42.38	1892.51	601.05	1291.46	1270.95	20.50	4
40.43	2089.54	661.53	1428.01	1392.12	35.89	4
38.50	2285.84	723.21	1562.63	1512.57	50.06	4
36.59	2481.40	786.80	1694.60	1632.27	62.33	4
34.68	2676.18	853.39	1822.80	1751.19	71.61	4
32.79	2870.14	924.76	1945.38	1869.29	76.09	4
30.91	3063.21	1003.23	2059.99	1986.50	73.49	4
30.91	3063.21	1003.23	2059.99	1986.50	73.49	3
29.53	3210.98	1067.67	2143.31	2072.41	70.90	3
28.16	3358.39	1130.18	2228.21	2157.96	70.24	3
26.80	3505.46	1191.22	2314.24	2243.17	71.07	3
25.44	3652.18	1251.03	2401.15	2328.03	73.12	3
24.08	3798.57	1309.77	2488.80	2412.57	76.23	3
22.73	3944.64	1367.62	2577.02	2496.77	80.25	3
21.39	4090.38	1424.70	2665.67	2580.65	85.02	3
20.05	4235.80	1481.00	2754.80	2664.22	90.58	3
18.71	4380.90	1536.45	2844.46	2747.47	96.99	3
18.71	4380.90	1536.45	2844.46	2747.47	96.99	2
16.81	4585.96	1610.03	2975.94	2866.43	109.51	2
14.91	4790.56	1685.80	3104.76	2984.93	119.83	2
13.02	4994.69	1763.13	3231.56	3102.96	128.61	2
11.13	5198.34	1842.35	3355.98	3220.51	135.48	2
9.26	5401.49	1923.91	3477.58	3337.56	140.02	2
7.39	5604.13	2012.13	3592.00	3454.11	137.90	2
5.53	5806.26	2139.26	3667.00	3570.13	96.87	2
3.68	6007.86	2261.68	3746.18	3685.64	60.54	2
1.84	6208.98	2379.85	3829.13	3800.66	28.47	2

.00	6409.62	2494.17	3915.45	3915.20	.25	2

Time = 5040. Degree of Consolidation = 88.%

Total Settlement = 1.499

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 5040. = 1.489

Settlement caused by Secondary Compression at time 5040. = .010

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.81	202.52	228.30	228.30	.00	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 5040. = .121

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .76

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.07	21.42	6.50	5.89	5.89	6

60.02	58.55	21.35	6.49	5.86	5.87	6
59.45	58.03	21.27	6.47	5.85	5.86	6
58.89	57.51	21.20	6.46	5.83	5.85	6
58.33	57.00	21.12	6.44	5.82	5.83	6
57.76	56.48	21.05	6.43	5.80	5.82	6
57.20	55.97	20.97	6.42	5.79	5.80	6
56.64	55.46	20.90	6.40	5.78	5.79	6
56.08	54.94	20.82	6.39	5.76	5.78	6
56.08	54.94	20.82	4.51	4.01	4.01	5
54.82	53.79	20.59	4.44	3.94	3.94	5
53.56	52.65	20.36	4.38	3.88	3.88	5
52.32	51.53	20.12	4.32	3.81	3.81	5
51.10	50.42	19.89	4.25	3.75	3.75	5
49.88	49.33	19.66	4.19	3.68	3.69	5
48.69	48.25	19.43	4.13	3.62	3.62	5
48.69	48.25	19.43	1.93	1.90	1.90	4
46.69	46.28	18.75	1.92	1.88	1.88	4
44.70	44.31	18.06	1.91	1.87	1.87	4
42.72	42.36	17.38	1.89	1.85	1.85	4
40.75	40.42	16.70	1.88	1.83	1.82	4
38.79	38.49	16.01	1.86	1.82	1.80	4
36.85	36.57	15.33	1.84	1.80	1.78	4
34.91	34.66	14.65	1.82	1.78	1.76	4
33.00	32.77	13.97	1.80	1.76	1.74	4
31.09	30.90	13.28	1.78	1.74	1.72	4
31.09	30.90	13.28	1.47	1.45	1.44	3
29.70	29.52	12.72	1.46	1.44	1.43	3
28.32	28.15	12.16	1.45	1.43	1.42	3
26.94	26.79	11.59	1.44	1.42	1.41	3
25.57	25.43	11.03	1.43	1.41	1.40	3
24.21	24.07	10.47	1.42	1.40	1.39	3
22.84	22.72	9.90	1.41	1.39	1.38	3
21.49	21.38	9.34	1.40	1.38	1.37	3
20.14	20.04	8.78	1.39	1.37	1.36	3
18.80	18.71	8.21	1.38	1.36	1.35	3
18.80	18.71	8.21	1.34	1.32	1.31	2
16.88	16.80	7.39	1.33	1.32	1.30	2
14.97	14.90	6.57	1.32	1.31	1.29	2
13.07	13.01	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.07	430.81	202.52	228.30	228.30	.00	6
58.55	467.83	207.14	260.69	260.69	.00	6
58.03	504.75	211.76	293.00	293.00	.00	6
57.51	541.61	216.38	325.24	325.24	.00	6
57.00	578.41	221.00	357.41	357.41	.00	6
56.48	615.13	225.62	389.52	389.52	.00	6
55.97	651.80	230.24	421.56	421.56	.00	6
55.46	688.39	234.86	453.53	453.53	.00	6
54.94	724.92	239.48	485.44	485.44	.00	6
54.94	724.92	239.48	485.44	485.44	.00	5
53.79	822.61	265.23	557.38	557.38	.00	5
52.65	919.37	290.98	628.39	628.39	.00	5

51.53	1015.20	316.73	698.47	698.47	.00	5
50.42	1110.11	342.48	767.63	767.63	.00	5
49.33	1204.09	368.23	835.86	835.86	.00	5
48.25	1297.14	393.98	903.16	903.16	.00	5
48.25	1297.14	393.98	903.16	903.16	.00	4
46.28	1496.23	469.84	1026.39	1026.39	.00	4
44.31	1694.68	541.89	1152.79	1148.98	3.80	4
42.36	1892.42	602.59	1289.83	1270.86	18.97	4
40.42	2089.42	663.91	1425.52	1392.01	33.51	4
38.49	2285.69	726.54	1559.15	1512.42	46.73	4
36.57	2481.21	791.13	1690.07	1632.07	58.00	4
34.66	2675.93	858.89	1817.04	1750.94	66.10	4
32.77	2869.82	931.41	1938.40	1868.96	69.44	4
30.90	3062.80	1010.72	2052.08	1986.09	65.99	4
30.90	3062.80	1010.72	2052.08	1986.09	65.99	3
29.52	3210.52	1075.98	2134.54	2071.95	62.59	3
28.15	3357.89	1139.29	2218.59	2157.46	61.13	3
26.79	3504.90	1200.85	2304.04	2242.61	61.43	3
25.43	3651.57	1260.83	2390.73	2327.42	63.31	3
24.07	3797.90	1319.58	2478.32	2411.90	66.42	3
22.72	3943.91	1377.42	2566.49	2496.05	70.44	3
21.38	4089.60	1434.46	2655.14	2579.87	75.26	3
20.04	4234.96	1490.52	2744.44	2663.38	81.06	3
18.71	4380.02	1545.76	2834.26	2746.58	87.68	3
18.71	4380.02	1545.76	2834.26	2746.58	87.68	2
16.80	4585.02	1618.75	2966.28	2865.48	100.79	2
14.90	4789.57	1693.70	3095.87	2983.93	111.94	2
13.01	4993.65	1770.19	3223.46	3101.92	121.54	2
11.13	5197.26	1848.58	3348.68	3219.43	129.25	2
9.26	5400.38	1929.27	3471.10	3336.45	134.66	2
7.39	5602.99	2018.67	3584.32	3452.96	131.36	2
5.53	5805.09	2144.04	3661.04	3568.96	92.08	2
3.68	6006.68	2264.80	3741.88	3684.46	57.42	2
1.84	6207.79	2381.38	3826.40	3799.46	26.94	2
.00	6408.42	2494.19	3914.24	3914.00	.23	2

Time = 5475. Degree of Consolidation = 89.%

Total Settlement = 1.518

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 5475. = 1.507

Settlement caused by Secondary Compression at time 5475. = .012

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

XI	Total Stresses	Effective Stresses	Total Pore Pressures	Static Pore Pressures	Excess Pore Pressures	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.81	202.52	228.30	228.30	.00	1

Time = 5475. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 5475. = .121

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .74

**********Current Conditions in Compressible Foundation**********

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.03	21.42	6.50	5.89	5.89	6
60.02	58.51	21.35	6.49	5.86	5.87	6
59.45	57.99	21.27	6.47	5.84	5.86	6
58.89	57.48	21.20	6.46	5.83	5.85	6
58.33	56.96	21.12	6.44	5.81	5.83	6
57.76	56.45	21.05	6.43	5.80	5.82	6
57.20	55.93	20.97	6.42	5.79	5.80	6
56.64	55.42	20.90	6.40	5.77	5.79	6
56.08	54.91	20.82	6.39	5.76	5.78	6
56.08	54.91	20.82	4.51	4.01	4.01	5
54.82	53.76	20.59	4.44	3.94	3.94	5
53.56	52.62	20.36	4.38	3.88	3.88	5
52.32	51.50	20.12	4.32	3.81	3.81	5
51.10	50.39	19.89	4.25	3.75	3.75	5
49.88	49.30	19.66	4.19	3.68	3.69	5
48.69	48.22	19.43	4.13	3.62	3.62	5
48.69	48.22	19.43	1.93	1.90	1.90	4
46.69	46.24	18.75	1.92	1.88	1.88	4
44.70	44.28	18.06	1.91	1.87	1.87	4
42.72	42.32	17.38	1.89	1.85	1.85	4
40.75	40.38	16.70	1.88	1.83	1.82	4
38.79	38.46	16.01	1.86	1.81	1.80	4
36.85	36.54	15.33	1.84	1.80	1.78	4
34.91	34.64	14.65	1.82	1.78	1.76	4
33.00	32.75	13.97	1.80	1.76	1.74	4
31.09	30.87	13.28	1.78	1.73	1.72	4
31.09	30.87	13.28	1.47	1.45	1.44	3
29.70	29.50	12.72	1.46	1.44	1.43	3
28.32	28.13	12.16	1.45	1.43	1.42	3
26.94	26.77	11.59	1.44	1.42	1.41	3

25.57	25.41	11.03	1.43	1.41	1.40	3
24.21	24.06	10.47	1.42	1.40	1.39	3
22.84	22.71	9.90	1.41	1.39	1.38	3
21.49	21.37	9.34	1.40	1.38	1.37	3
20.14	20.03	8.78	1.39	1.37	1.36	3
18.80	18.70	8.21	1.38	1.36	1.35	3
18.80	18.70	8.21	1.34	1.32	1.31	2
16.88	16.79	7.39	1.33	1.31	1.30	2
14.97	14.90	6.57	1.32	1.30	1.29	2
13.07	13.01	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.03	430.81	202.52	228.30	228.30	.00	6
58.51	467.82	207.14	260.68	260.68	.00	6
57.99	504.73	211.76	292.97	292.97	.00	6
57.48	541.57	216.38	325.20	325.20	.00	6
56.96	578.35	221.00	357.35	357.35	.00	6
56.45	615.06	225.62	389.45	389.45	.00	6
55.93	651.71	230.24	421.47	421.47	.00	6
55.42	688.29	234.86	453.43	453.43	.00	6
54.91	724.80	239.48	485.32	485.32	.00	6
54.91	724.80	239.48	485.32	485.32	.00	5
53.76	822.49	265.23	557.26	557.26	.00	5
52.62	919.25	290.98	628.27	628.27	.00	5
51.50	1015.08	316.73	698.35	698.35	.00	5
50.39	1109.99	342.48	767.51	767.51	.00	5
49.30	1203.97	368.23	835.74	835.74	.00	5
48.22	1297.02	393.98	903.04	903.04	.00	5
48.22	1297.02	393.98	903.04	903.04	.00	4
46.24	1496.11	469.84	1026.27	1026.27	.00	4
44.28	1694.55	543.22	1151.33	1148.86	2.47	4
42.32	1892.26	605.39	1286.88	1270.71	16.17	4
40.38	2089.23	668.33	1420.90	1391.81	29.09	4
38.46	2285.44	732.53	1552.91	1512.16	40.75	4
36.54	2480.87	798.94	1681.93	1631.73	50.20	4
34.64	2675.48	868.62	1806.86	1750.49	56.37	4
32.75	2869.24	943.56	1925.68	1868.39	57.29	4
30.87	3062.07	1024.37	2037.69	1985.36	52.34	4
30.87	3062.07	1024.37	2037.69	1985.36	52.34	3
29.50	3209.71	1091.07	2118.64	2071.14	47.50	3
28.13	3356.98	1155.44	2201.54	2156.56	44.99	3
26.77	3503.90	1217.70	2286.20	2241.62	44.59	3
25.41	3650.48	1278.33	2372.15	2326.33	45.82	3
24.06	3796.71	1337.55	2459.16	2410.71	48.45	3
22.71	3942.62	1395.53	2547.09	2494.76	52.34	3
21.37	4088.20	1452.41	2635.79	2578.48	57.31	3
20.03	4233.47	1508.35	2725.12	2661.89	63.23	3
18.70	4378.43	1563.33	2815.09	2744.99	70.11	3
18.70	4378.43	1563.33	2815.09	2744.99	70.11	2
16.79	4583.32	1635.71	2947.62	2863.78	83.83	2
14.90	4787.77	1709.34	3078.43	2982.13	96.29	2
13.01	4991.76	1784.53	3207.23	3100.03	107.20	2
11.13	5195.28	1861.60	3333.68	3217.45	116.23	2

9.25	5398.32	1940.98	3457.35	3334.39	122.95	2
7.39	5600.87	2033.78	3567.09	3450.84	116.25	2
5.53	5802.91	2155.10	3647.82	3566.79	81.03	2
3.68	6004.47	2272.01	3732.46	3682.24	50.22	2
1.84	6205.55	2384.92	3820.63	3797.23	23.40	2
.00	6406.18	2494.22	3911.97	3911.76	.20	2

Time = 6480. Degree of Consolidation = 91.%

Total Settlement = 1.554

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 6480. = 1.541

Settlement caused by Secondary Compression at time 6480. = .014

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1
1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.81	202.52	228.30	228.30	.00	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 6480. = .121

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .70

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.01	21.42	6.50	5.89	5.89	6
60.02	58.49	21.35	6.49	5.86	5.87	6
59.45	57.97	21.27	6.47	5.84	5.86	6
58.89	57.45	21.20	6.46	5.83	5.85	6
58.33	56.94	21.12	6.44	5.81	5.83	6
57.76	56.42	21.05	6.43	5.80	5.82	6
57.20	55.91	20.97	6.42	5.79	5.80	6
56.64	55.40	20.90	6.40	5.77	5.79	6
56.08	54.89	20.82	6.39	5.76	5.78	6
56.08	54.89	20.82	4.51	4.01	4.01	5
54.82	53.74	20.59	4.44	3.94	3.94	5
53.56	52.60	20.36	4.38	3.88	3.88	5
52.32	51.47	20.12	4.32	3.81	3.81	5
51.10	50.37	19.89	4.25	3.75	3.75	5
49.88	49.27	19.66	4.19	3.68	3.69	5
48.69	48.19	19.43	4.13	3.62	3.62	5
48.69	48.19	19.43	1.93	1.90	1.90	4
46.69	46.22	18.75	1.92	1.88	1.88	4
44.70	44.25	18.06	1.91	1.87	1.87	4
42.72	42.30	17.38	1.89	1.85	1.85	4
40.75	40.36	16.70	1.88	1.83	1.82	4
38.79	38.43	16.01	1.86	1.81	1.80	4
36.85	36.52	15.33	1.84	1.79	1.78	4
34.91	34.62	14.65	1.82	1.78	1.76	4
33.00	32.73	13.97	1.80	1.75	1.74	4
31.09	30.86	13.28	1.78	1.73	1.72	4
31.09	30.86	13.28	1.47	1.44	1.44	3
29.70	29.48	12.72	1.46	1.43	1.43	3
28.32	28.11	12.16	1.45	1.42	1.42	3
26.94	26.75	11.59	1.44	1.41	1.41	3
25.57	25.39	11.03	1.43	1.40	1.40	3
24.21	24.04	10.47	1.42	1.39	1.39	3
22.84	22.70	9.90	1.41	1.38	1.38	3
21.49	21.36	9.34	1.40	1.38	1.37	3
20.14	20.02	8.78	1.39	1.37	1.36	3
18.80	18.69	8.21	1.38	1.36	1.35	3
18.80	18.69	8.21	1.34	1.32	1.31	2
16.88	16.79	7.39	1.33	1.31	1.30	2
14.97	14.89	6.57	1.32	1.30	1.29	2
13.07	13.00	5.75	1.31	1.29	1.28	2
11.18	11.12	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.01	430.81	202.52	228.30	228.30	.00	6
58.49	467.82	207.14	260.68	260.68	.00	6
57.97	504.73	211.76	292.97	292.97	.00	6
57.45	541.57	216.38	325.20	325.20	.00	6
56.94	578.35	221.00	357.35	357.35	.00	6
56.42	615.06	225.62	389.45	389.45	.00	6
55.91	651.71	230.24	421.47	421.47	.00	6

55.40	688.29	234.86	453.43	453.43	.00	6
54.89	724.80	239.48	485.32	485.32	.00	6
54.89	724.80	239.48	485.32	485.32	.00	5
53.74	822.49	265.23	557.26	557.26	.00	5
52.60	919.25	290.98	628.27	628.27	.00	5
51.47	1015.08	316.73	698.35	698.35	.00	5
50.37	1109.98	342.48	767.51	767.51	.00	5
49.27	1203.97	368.23	835.74	835.74	.00	5
48.19	1297.02	393.98	903.04	903.04	.00	5
48.19	1297.02	393.98	903.04	903.04	.00	4
46.22	1496.11	469.84	1026.27	1026.27	.00	4
44.25	1694.55	544.01	1150.54	1148.85	1.69	4
42.30	1892.25	607.05	1285.20	1270.69	14.51	4
40.36	2089.19	670.95	1418.24	1391.77	26.47	4
38.43	2285.36	736.23	1549.12	1512.08	37.04	4
36.52	2480.73	803.72	1677.01	1631.60	45.41	4
34.62	2675.29	874.73	1800.56	1750.30	50.27	4
32.73	2868.96	951.11	1917.86	1868.11	49.74	4
30.86	3061.69	1032.91	2028.79	1984.98	43.81	4
30.86	3061.69	1032.91	2028.79	1984.98	43.81	3
29.48	3209.28	1100.56	2108.72	2070.71	38.01	3
28.11	3356.50	1165.89	2190.61	2156.07	34.54	3
26.75	3503.36	1229.09	2274.27	2241.07	33.19	3
25.39	3649.87	1290.36	2359.50	2325.72	33.78	3
24.04	3796.03	1349.88	2446.16	2410.03	36.13	3
22.70	3941.87	1407.85	2534.02	2494.01	40.01	3
21.36	4087.39	1464.74	2622.65	2577.66	44.98	3
20.02	4232.58	1520.68	2711.90	2661.00	50.90	3
18.69	4377.47	1575.49	2801.98	2744.03	57.95	3
18.69	4377.47	1575.49	2801.98	2744.03	57.95	2
16.79	4582.29	1647.17	2935.13	2862.76	72.37	2
14.89	4786.67	1720.13	3066.55	2981.04	85.51	2
13.00	4990.60	1794.64	3195.96	3098.86	97.09	2
11.12	5194.06	1871.06	3323.01	3216.23	106.78	2
9.25	5397.05	1949.77	3447.27	3333.12	114.16	2
7.39	5599.54	2045.38	3554.16	3449.51	104.65	2
5.53	5801.54	2163.58	3637.96	3565.42	72.54	2
3.68	6003.07	2277.54	3725.53	3680.85	44.68	2
1.84	6204.14	2387.64	3816.50	3795.82	20.68	2
.00	6404.76	2494.24	3910.52	3910.34	.18	2

Time = 7300. Degree of Consolidation = 92.%

Total Settlement = 1.577

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 7300. = 1.564

Settlement caused by Secondary Compression at time 7300. = .014

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
3.78	3.66	1.91	.98	.98	.98	1
2.84	2.73	1.43	.98	.92	.92	1

1.89	1.82	.95	.98	.91	.91	1
.94	.91	.48	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.66	.00	.00	.00	.00	.00	1
2.73	108.47	50.63	57.84	57.84	.00	1
1.82	216.11	101.26	114.85	114.85	.00	1
.91	323.53	151.89	171.65	171.65	.00	1
.00	430.81	202.52	228.30	228.30	.00	1

Time = 7300. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 7300. = .121

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .68

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.97	21.42	6.50	5.89	5.89	6
60.02	58.45	21.35	6.49	5.86	5.87	6
59.45	57.93	21.27	6.47	5.84	5.86	6
58.89	57.42	21.20	6.46	5.83	5.85	6
58.33	56.90	21.12	6.44	5.81	5.83	6
57.76	56.39	21.05	6.43	5.80	5.82	6
57.20	55.87	20.97	6.42	5.79	5.80	6
56.64	55.36	20.90	6.40	5.77	5.79	6
56.08	54.85	20.82	6.39	5.76	5.78	6
56.08	54.85	20.82	4.51	4.01	4.01	5
54.82	53.70	20.59	4.44	3.94	3.94	5
53.56	52.56	20.36	4.38	3.88	3.88	5
52.32	51.44	20.12	4.32	3.81	3.81	5
51.10	50.33	19.89	4.25	3.75	3.75	5
49.88	49.23	19.66	4.19	3.68	3.69	5
48.69	48.16	19.43	4.13	3.62	3.62	5
48.69	48.16	19.43	1.93	1.90	1.90	4
46.69	46.18	18.75	1.92	1.88	1.88	4
44.70	44.22	18.06	1.91	1.87	1.87	4
42.72	42.26	17.38	1.89	1.85	1.85	4
40.75	40.32	16.70	1.88	1.83	1.82	4
38.79	38.40	16.01	1.86	1.81	1.80	4
36.85	36.48	15.33	1.84	1.79	1.78	4
34.91	34.58	14.65	1.82	1.77	1.76	4
33.00	32.70	13.97	1.80	1.75	1.74	4

31.09	30.83	13.28	1.78	1.73	1.72	4
31.09	30.83	13.28	1.47	1.44	1.44	3
29.70	29.45	12.72	1.46	1.43	1.43	3
28.32	28.09	12.16	1.45	1.42	1.42	3
26.94	26.73	11.59	1.44	1.41	1.41	3
25.57	25.37	11.03	1.43	1.40	1.40	3
24.21	24.02	10.47	1.42	1.39	1.39	3
22.84	22.68	9.90	1.41	1.38	1.38	3
21.49	21.34	9.34	1.40	1.37	1.37	3
20.14	20.01	8.78	1.39	1.36	1.36	3
18.80	18.68	8.21	1.38	1.35	1.35	3
18.80	18.68	8.21	1.34	1.32	1.31	2
16.88	16.78	7.39	1.33	1.31	1.30	2
14.97	14.88	6.57	1.32	1.30	1.29	2
13.07	13.00	5.75	1.31	1.29	1.28	2
11.18	11.12	4.93	1.30	1.28	1.27	2
9.30	9.25	4.11	1.29	1.27	1.26	2
7.43	7.38	3.29	1.28	1.26	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.97	430.81	202.52	228.30	228.30	.00	6
58.45	467.82	207.14	260.68	260.68	.00	6
57.93	504.73	211.76	292.97	292.97	.00	6
57.42	541.57	216.38	325.20	325.20	.00	6
56.90	578.35	221.00	357.35	357.35	.00	6
56.39	615.06	225.62	389.45	389.45	.00	6
55.87	651.71	230.24	421.47	421.47	.00	6
55.36	688.29	234.86	453.43	453.43	.00	6
54.85	724.80	239.48	485.32	485.32	.00	6
54.85	724.80	239.48	485.32	485.32	.00	5
53.70	822.49	265.23	557.26	557.26	.00	5
52.56	919.25	290.98	628.27	628.27	.00	5
51.44	1015.08	316.73	698.35	698.35	.00	5
50.33	1109.99	342.48	767.51	767.51	.00	5
49.23	1203.97	368.23	835.74	835.74	.00	5
48.16	1297.02	393.98	903.04	903.04	.00	5
48.16	1297.02	393.98	903.04	903.04	.00	4
46.18	1496.11	469.84	1026.27	1026.27	.00	4
44.22	1694.54	545.21	1149.33	1148.85	.49	4
42.26	1892.22	609.58	1282.64	1270.66	11.97	4
40.32	2089.12	674.96	1414.16	1391.70	22.45	4
38.40	2285.23	741.92	1543.31	1511.96	31.35	4
36.48	2480.53	811.28	1669.25	1631.40	37.85	4
34.58	2674.98	884.26	1790.72	1749.99	40.73	4
32.70	2868.53	963.21	1905.32	1867.68	37.64	4
30.83	3061.10	1046.71	2014.39	1984.39	30.00	4
30.83	3061.10	1046.71	2014.39	1984.39	30.00	3
29.45	3208.61	1115.67	2092.94	2070.04	22.90	3
28.09	3355.74	1181.93	2173.81	2155.31	18.49	3
26.73	3502.50	1246.04	2256.46	2240.22	16.24	3
25.37	3648.91	1308.23	2340.68	2324.77	15.91	3
24.02	3794.98	1368.67	2426.30	2408.97	17.33	3
22.68	3940.71	1427.54	2513.16	2492.84	20.32	3
21.34	4086.11	1485.00	2601.11	2576.39	24.72	3
20.01	4231.19	1541.19	2690.01	2659.61	30.39	3
18.68	4375.96	1596.26	2779.71	2742.52	37.18	3

18.68	4375.96	1596.26	2779.71	2742.52	37.18	2
16.78	4580.66	1667.39	2913.27	2861.12	52.15	2
14.88	4784.92	1739.84	3045.07	2979.28	65.79	2
13.00	4988.72	1813.90	3174.83	3096.99	77.84	2
11.12	5192.07	1889.85	3302.22	3214.24	87.98	2
9.25	5394.94	1967.05	3427.89	3331.01	96.88	2
7.38	5597.34	2066.21	3531.13	3447.31	83.81	2
5.53	5799.27	2178.83	3620.43	3563.14	57.29	2
3.68	6000.74	2287.48	3713.26	3678.52	34.74	2
1.84	6201.78	2392.52	3809.26	3793.46	15.80	2
.00	6402.40	2494.28	3908.12	3907.98	.14	2

Time = 9125. Degree of Consolidation = 95.%

Total Settlement = 1.615

Settlement at End of Primary Consolidation = 1.707

Settlement caused by Primary Consolidation at time 9125. = 1.601

Settlement caused by Secondary Compression at time 9125. = .014

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.78	3.66	1.91
2.84	2.73	1.43
1.89	1.82	.95
.94	.91	.48
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.66	.00	.00
2.73	108.47	50.63
1.82	216.11	101.26
.91	323.53	151.89
.00	430.81	202.52

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
57.84	57.84	.00	1
114.85	114.85	.00	1
171.65	171.65	.00	1
228.30	228.30	.00	1

Time = 9125. Degree of Consolidation = 100.%

Total Settlement = .121

Settlement at End of Primary Consolidation = .121

Settlement caused by Primary Consolidation at time 9125. = .121

Settlement caused by Secondary Compression at time 9125. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .64

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Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou DuPont - 2ft fill with Equivalent fill height of 2.7 f

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	2.7	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.505E-01	.570	.30000E-03	z = .06

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	6.06	6
60.02	60.02	21.35	6.49	6.49	6.05	6
59.45	59.45	21.27	6.47	6.47	6.04	6
58.89	58.89	21.20	6.46	6.46	6.02	6

58.33	58.33	21.12	6.44	6.44	6.01	6
57.76	57.76	21.05	6.43	6.43	5.99	6
57.20	57.20	20.97	6.42	6.42	5.98	6
56.64	56.64	20.90	6.40	6.40	5.97	6
56.08	56.08	20.82	6.39	6.39	5.95	6
56.08	56.08	20.82	4.51	4.51	4.15	5
54.82	54.82	20.59	4.44	4.44	4.09	5
53.56	53.56	20.36	4.38	4.38	4.02	5
52.32	52.32	20.12	4.32	4.32	3.96	5
51.10	51.10	19.89	4.25	4.25	3.89	5
49.88	49.88	19.66	4.19	4.19	3.83	5
48.69	48.69	19.43	4.13	4.13	3.77	5
48.69	48.69	19.43	1.93	1.93	1.91	4
46.69	46.69	18.75	1.92	1.92	1.89	4
44.70	44.70	18.06	1.91	1.91	1.88	4
42.72	42.72	17.38	1.89	1.89	1.86	4
40.75	40.75	16.70	1.88	1.88	1.84	4
38.79	38.79	16.01	1.86	1.86	1.82	4
36.85	36.85	15.33	1.84	1.84	1.80	4
34.91	34.91	14.65	1.82	1.82	1.78	4
33.00	33.00	13.97	1.80	1.80	1.76	4
31.09	31.09	13.28	1.78	1.78	1.73	4
31.09	31.09	13.28	1.47	1.47	1.45	3
29.70	29.70	12.72	1.46	1.46	1.44	3
28.32	28.32	12.16	1.45	1.45	1.43	3
26.94	26.94	11.59	1.44	1.44	1.42	3
25.57	25.57	11.03	1.43	1.43	1.41	3
24.21	24.21	10.47	1.42	1.42	1.40	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.49	9.34	1.40	1.40	1.38	3
20.14	20.14	8.78	1.39	1.39	1.37	3
18.80	18.80	8.21	1.38	1.38	1.36	3
18.80	18.80	8.21	1.34	1.34	1.32	2
16.88	16.88	7.39	1.33	1.33	1.31	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.30	4.11	1.29	1.29	1.27	2
7.43	7.43	3.29	1.28	1.28	1.26	2
5.56	5.56	2.46	1.27	1.27	1.26	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.85	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.25	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	313.13	.00	313.13	168.48	144.65	6
60.02	353.08	4.62	348.46	203.81	144.66	6
59.45	392.96	9.24	383.72	239.07	144.65	6
58.89	432.78	13.86	418.92	274.26	144.66	6
58.33	472.53	18.48	454.05	309.39	144.66	6
57.76	512.21	23.10	489.11	344.46	144.65	6
57.20	551.83	27.72	524.11	379.46	144.66	6
56.64	591.38	32.34	559.04	414.39	144.65	6
56.08	630.87	36.96	593.91	449.25	144.65	6
56.08	630.87	36.96	593.91	449.25	144.65	5
54.82	735.84	62.71	673.13	528.48	144.65	5
53.56	839.89	88.46	751.43	606.78	144.65	5
52.32	943.02	114.21	828.81	684.15	144.65	5
51.10	1045.22	139.96	905.26	760.60	144.65	5
49.88	1146.50	165.71	980.79	836.13	144.65	5

48.69	1246.85	191.46	1055.39	910.74	144.65	5
48.69	1246.85	191.46	1055.39	910.74	144.65	4
46.69	1447.30	267.32	1179.98	1035.32	144.65	4
44.70	1647.24	343.18	1304.06	1159.40	144.66	4
42.72	1846.63	419.04	1427.59	1282.94	144.65	4
40.75	2045.58	494.90	1550.68	1406.02	144.66	4
38.79	2243.77	570.76	1673.02	1528.36	144.65	4
36.85	2441.07	646.62	1794.46	1649.80	144.65	4
34.91	2637.47	722.48	1914.99	1770.34	144.66	4
33.00	2832.96	798.34	2034.62	1889.97	144.65	4
31.09	3027.54	874.19	2153.35	2008.70	144.65	4
31.09	3027.54	874.19	2153.35	2008.70	144.65	3
29.70	3176.12	936.05	2240.06	2095.41	144.65	3
28.32	3324.29	997.91	2326.37	2181.72	144.65	3
26.94	3472.09	1059.77	2412.32	2267.67	144.66	3
25.57	3619.55	1121.63	2497.92	2353.27	144.65	3
24.21	3766.66	1183.49	2583.18	2438.52	144.66	3
22.84	3913.43	1245.35	2668.08	2523.42	144.66	3
21.49	4059.84	1307.21	2752.64	2607.98	144.65	3
20.14	4205.91	1369.06	2836.84	2692.19	144.66	3
18.80	4351.63	1430.92	2920.71	2776.05	144.66	3
18.80	4351.63	1430.92	2920.70	2776.05	144.65	2
16.88	4557.30	1517.02	3040.27	2895.62	144.65	2
14.97	4762.43	1603.12	3159.31	3014.66	144.65	2
13.07	4967.04	1689.22	3277.83	3133.17	144.65	2
11.18	5171.12	1775.31	3395.81	3251.15	144.66	2
9.30	5374.68	1861.41	3513.26	3368.61	144.66	2
7.43	5577.69	1947.51	3630.18	3485.53	144.66	2
5.56	5780.20	2033.61	3746.59	3601.94	144.66	2
3.70	5982.32	2119.71	3862.61	3717.96	144.66	2
1.85	6184.08	2205.80	3978.28	3833.62	144.66	2
.00	6385.50	2291.90	4093.60	3948.94	144.66	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.70	1.36	.98	.98	.98	1
2.03	2.03	1.02	.98	.98	.93	1
1.35	1.35	.68	.98	.98	.92	1
.68	.68	.34	.98	.98	.91	1
.00	.00	.00	.98	.98	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

2.70	.00	.00	.00	.00	.00	1
2.03	78.28	.00	78.28	42.12	36.16	1
1.35	156.57	.00	156.57	84.24	72.33	1
.68	234.85	.00	234.85	126.36	108.49	1
.00	313.13	.00	313.13	168.48	144.65	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.52	21.42	6.50	6.16	6.06	6
60.02	59.98	21.35	6.49	6.25	6.05	6
59.45	59.42	21.27	6.47	6.33	6.04	6
58.89	58.87	21.20	6.46	6.38	6.02	6
58.33	58.31	21.12	6.44	6.40	6.01	6
57.76	57.75	21.05	6.43	6.41	5.99	6
57.20	57.19	20.97	6.42	6.41	5.98	6
56.64	56.63	20.90	6.40	6.40	5.97	6
56.08	56.07	20.82	6.39	6.39	5.95	6
56.08	56.07	20.82	4.51	4.51	4.15	5
54.82	54.80	20.59	4.44	4.44	4.09	5
53.56	53.55	20.36	4.38	4.38	4.02	5
52.32	52.31	20.12	4.32	4.31	3.96	5
51.10	51.08	19.89	4.25	4.25	3.89	5
49.88	49.87	19.66	4.19	4.19	3.83	5
48.69	48.68	19.43	4.13	4.12	3.77	5
48.69	48.68	19.43	1.93	1.93	1.91	4
46.69	46.68	18.75	1.92	1.92	1.89	4
44.70	44.70	18.06	1.91	1.91	1.88	4
42.72	42.72	17.38	1.89	1.89	1.86	4
40.75	40.74	16.70	1.88	1.88	1.84	4
38.79	38.79	16.01	1.86	1.86	1.82	4
36.85	36.84	15.33	1.84	1.84	1.80	4
34.91	34.91	14.65	1.82	1.82	1.78	4
33.00	32.99	13.97	1.80	1.80	1.76	4
31.09	31.09	13.28	1.78	1.78	1.73	4
31.09	31.09	13.28	1.47	1.47	1.45	3
29.70	29.70	12.72	1.46	1.46	1.44	3
28.32	28.31	12.16	1.45	1.45	1.43	3
26.94	26.94	11.59	1.44	1.44	1.42	3
25.57	25.57	11.03	1.43	1.43	1.41	3
24.21	24.20	10.47	1.42	1.42	1.40	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3
18.80	18.79	8.21	1.34	1.34	1.32	2

16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.56	2.46	1.27	1.27	1.26	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.52	308.43	112.07	196.36	163.78	32.58	6
59.98	347.04	81.36	265.68	197.77	67.92	6
59.42	386.05	56.66	329.39	232.15	97.24	6
58.87	425.35	40.19	385.16	266.83	118.32	6
58.31	464.83	31.65	433.18	301.69	131.49	6
57.75	504.38	29.10	475.28	336.62	138.66	6
57.19	543.94	30.32	513.62	371.56	142.06	6
56.63	583.47	33.61	549.86	406.47	143.39	6
56.07	622.94	37.97	584.97	441.32	143.65	6
56.07	622.94	37.97	584.97	441.32	143.65	5
54.80	727.88	63.57	664.31	520.51	143.80	5
53.55	831.90	89.34	742.56	598.78	143.78	5
52.31	934.99	115.13	819.87	676.12	143.74	5
51.08	1037.16	140.88	896.28	752.54	143.73	5
49.87	1138.41	166.61	971.79	828.04	143.75	5
48.68	1238.73	192.27	1046.45	902.61	143.84	5
48.68	1238.73	192.27	1046.45	902.61	143.84	4
46.68	1439.17	267.32	1171.85	1027.19	144.65	4
44.70	1639.09	343.18	1295.91	1151.26	144.66	4
42.72	1838.50	421.73	1416.77	1274.80	141.96	4
40.74	2037.33	507.72	1529.61	1397.78	131.84	4
38.79	2235.45	573.57	1661.89	1520.04	141.85	4
36.84	2432.74	646.64	1786.10	1641.47	144.63	4
34.91	2629.14	722.48	1906.66	1762.01	144.65	4
32.99	2824.63	798.34	2026.29	1881.64	144.65	4
31.09	3019.21	874.19	2145.02	2000.36	144.65	4
31.09	3019.21	874.19	2145.02	2000.36	144.65	3
29.70	3167.78	936.05	2231.73	2087.08	144.65	3
28.31	3315.96	997.91	2318.04	2173.39	144.65	3
26.94	3463.76	1060.92	2402.84	2259.33	143.51	3
25.57	3611.21	1123.07	2488.14	2344.93	143.21	3
24.20	3758.31	1184.88	2573.44	2430.17	143.26	3
22.84	3905.07	1246.68	2658.39	2515.07	143.33	3
21.48	4051.48	1308.54	2742.94	2599.62	143.32	3
20.13	4197.54	1370.30	2827.24	2683.82	143.42	3
18.79	4343.25	1431.78	2911.47	2767.67	143.80	3
18.79	4343.25	1431.78	2911.47	2767.67	143.80	2
16.87	4548.91	1517.10	3031.82	2887.24	144.58	2
14.97	4754.05	1603.12	3150.93	3006.28	144.65	2
13.07	4958.66	1689.22	3269.45	3124.79	144.66	2
11.18	5162.74	1775.31	3387.43	3242.77	144.65	2
9.29	5366.30	1861.41	3504.88	3360.23	144.66	2
7.42	5569.31	1947.51	3621.80	3477.15	144.66	2
5.56	5771.83	2033.61	3738.22	3593.57	144.66	2
3.70	5973.93	2122.17	3851.77	3709.57	142.19	2
1.84	6175.67	2227.99	3947.68	3825.21	122.47	2
.00	6376.79	2435.54	3941.25	3940.23	1.01	2

Time = 30. Degree of Consolidation = 5.%

Total Settlement = .064

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 30. = .064

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.64	29.44	48.20	41.47	6.73	1
1.30	154.72	57.83	96.89	82.40	14.50	1
.65	231.63	87.70	143.93	123.14	20.79	1
.00	308.43	112.07	196.36	163.78	32.58	1

Time = 30. Degree of Consolidation = 95.%

Total Settlement = .075

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 30. = .075

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 1.16

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.49	21.42	6.50	6.15	6.06	6
60.02	59.94	21.35	6.49	6.21	6.05	6
59.45	59.40	21.27	6.47	6.27	6.04	6
58.89	58.85	21.20	6.46	6.32	6.02	6
58.33	58.29	21.12	6.44	6.35	6.01	6

57.76	57.74	21.05	6.43	6.37	5.99	6
57.20	57.18	20.97	6.42	6.38	5.98	6
56.64	56.62	20.90	6.40	6.38	5.97	6
56.08	56.06	20.82	6.39	6.37	5.95	6
56.08	56.06	20.82	4.51	4.50	4.15	5
54.82	54.80	20.59	4.44	4.44	4.09	5
53.56	53.54	20.36	4.38	4.38	4.02	5
52.32	52.30	20.12	4.32	4.31	3.96	5
51.10	51.08	19.89	4.25	4.25	3.89	5
49.88	49.87	19.66	4.19	4.18	3.83	5
48.69	48.67	19.43	4.13	4.12	3.77	5
48.69	48.67	19.43	1.93	1.93	1.91	4
46.69	46.68	18.75	1.92	1.92	1.89	4
44.70	44.69	18.06	1.91	1.91	1.88	4
42.72	42.71	17.38	1.89	1.89	1.86	4
40.75	40.74	16.70	1.88	1.88	1.84	4
38.79	38.78	16.01	1.86	1.86	1.82	4
36.85	36.84	15.33	1.84	1.84	1.80	4
34.91	34.91	14.65	1.82	1.82	1.78	4
33.00	32.99	13.97	1.80	1.80	1.76	4
31.09	31.09	13.28	1.78	1.78	1.73	4
31.09	31.09	13.28	1.47	1.47	1.45	3
29.70	29.70	12.72	1.46	1.46	1.44	3
28.32	28.31	12.16	1.45	1.45	1.43	3
26.94	26.94	11.59	1.44	1.44	1.42	3
25.57	25.56	11.03	1.43	1.43	1.41	3
24.21	24.20	10.47	1.42	1.42	1.40	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3
18.80	18.79	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.49	308.41	116.73	191.68	163.76	27.92	6
59.94	346.89	95.19	251.69	197.61	54.08	6
59.40	385.65	76.05	309.60	231.76	77.85	6
58.85	424.66	60.59	364.08	266.15	97.93	6
58.29	463.87	49.46	414.41	300.73	113.68	6
57.74	503.20	42.63	460.56	335.44	125.12	6
57.18	542.60	39.57	503.03	370.22	132.81	6
56.62	582.02	39.45	542.56	405.02	137.54	6
56.06	621.42	41.42	580.00	439.81	140.20	6
56.06	621.42	41.42	580.00	439.81	140.20	5
54.80	726.27	65.61	660.66	518.90	141.76	5
53.54	830.23	90.68	739.55	597.11	142.44	5
52.30	933.28	116.17	817.11	674.41	142.70	5
51.08	1035.41	141.80	893.61	750.80	142.82	5
49.87	1136.63	167.45	969.18	826.26	142.92	5
48.67	1236.92	193.03	1043.89	900.80	143.09	5

48.67	1236.92	193.03	1043.89	900.80	143.09	4
46.68	1437.36	267.32	1170.04	1025.38	144.65	4
44.69	1637.28	343.57	1293.71	1149.45	144.26	4
42.71	1836.67	426.39	1410.29	1272.98	137.31	4
40.74	2035.46	512.79	1522.67	1395.90	126.77	4
38.78	2233.52	577.01	1656.51	1518.11	138.40	4
36.84	2430.79	647.56	1783.23	1639.52	143.71	4
34.91	2627.18	722.48	1904.70	1760.05	144.65	4
32.99	2822.67	798.34	2024.34	1879.68	144.65	4
31.09	3017.26	874.19	2143.06	1998.41	144.65	4
31.09	3017.26	874.19	2143.06	1998.41	144.65	3
29.70	3165.83	936.05	2229.77	2085.12	144.65	3
28.31	3314.00	997.91	2316.09	2171.43	144.65	3
26.94	3461.80	1061.80	2400.00	2257.37	142.62	3
25.56	3609.24	1124.40	2484.85	2342.96	141.89	3
24.20	3756.34	1186.21	2570.13	2428.20	141.94	3
22.84	3903.09	1248.00	2655.08	2513.09	142.00	3
21.48	4049.49	1309.86	2739.62	2597.63	142.00	3
20.13	4195.54	1371.40	2824.14	2681.82	142.32	3
18.79	4341.25	1432.66	2908.59	2765.67	142.92	3
18.79	4341.25	1432.66	2908.59	2765.67	142.92	2
16.87	4546.91	1517.55	3029.36	2885.23	144.13	2
14.97	4752.05	1603.12	3148.93	3004.27	144.65	2
13.07	4956.66	1689.22	3267.44	3122.78	144.66	2
11.18	5160.73	1775.31	3385.42	3240.77	144.65	2
9.29	5364.29	1861.41	3502.88	3358.22	144.66	2
7.42	5567.31	1947.51	3619.79	3475.14	144.66	2
5.55	5769.82	2033.61	3736.21	3591.55	144.66	2
3.69	5971.92	2126.90	3845.02	3707.56	137.46	2
1.84	6173.61	2244.53	3929.08	3823.15	105.93	2
.00	6374.68	2435.68	3939.00	3938.12	.88	2

Time = 60. Degree of Consolidation = 8.%

Total Settlement = .098

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 60. = .098

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.70	2.62	1.36
2.03	1.96	1.02
1.35	1.30	.68
.68	.65	.34
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
2.62	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

1.96	77.64	29.55	48.08	41.47	6.61	1
1.30	154.72	58.97	95.75	82.39	13.36	1
.65	231.62	89.52	142.10	123.13	18.97	1
.00	308.41	116.73	191.68	163.76	27.92	1

Time = 60. Degree of Consolidation = 95.%

Total Settlement = .076

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 60. = .076

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 1.13

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.43	21.42	6.50	6.14	6.06	6
60.02	59.89	21.35	6.49	6.18	6.05	6
59.45	59.35	21.27	6.47	6.22	6.04	6
58.89	58.80	21.20	6.46	6.26	6.02	6
58.33	58.25	21.12	6.44	6.29	6.01	6
57.76	57.70	21.05	6.43	6.31	5.99	6
57.20	57.15	20.97	6.42	6.33	5.98	6
56.64	56.59	20.90	6.40	6.34	5.97	6
56.08	56.04	20.82	6.39	6.35	5.95	6
56.08	56.04	20.82	4.51	4.47	4.15	5
54.82	54.78	20.59	4.44	4.42	4.09	5
53.56	53.53	20.36	4.38	4.36	4.02	5
52.32	52.29	20.12	4.32	4.30	3.96	5
51.10	51.07	19.89	4.25	4.24	3.89	5
49.88	49.86	19.66	4.19	4.18	3.83	5
48.69	48.67	19.43	4.13	4.12	3.77	5
48.69	48.67	19.43	1.93	1.93	1.91	4
46.69	46.67	18.75	1.92	1.92	1.89	4
44.70	44.68	18.06	1.91	1.90	1.88	4
42.72	42.70	17.38	1.89	1.89	1.86	4
40.75	40.73	16.70	1.88	1.87	1.84	4
38.79	38.78	16.01	1.86	1.86	1.82	4
36.85	36.83	15.33	1.84	1.84	1.80	4
34.91	34.90	14.65	1.82	1.82	1.78	4
33.00	32.98	13.97	1.80	1.80	1.76	4
31.09	31.08	13.28	1.78	1.78	1.73	4
31.09	31.08	13.28	1.47	1.47	1.45	3
29.70	29.69	12.72	1.46	1.46	1.44	3
28.32	28.31	12.16	1.45	1.45	1.43	3
26.94	26.93	11.59	1.44	1.44	1.42	3
25.57	25.56	11.03	1.43	1.43	1.41	3
24.21	24.19	10.47	1.42	1.42	1.40	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3

18.80	18.79	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.43	308.40	120.52	187.88	163.74	24.14	6
59.89	346.77	106.16	240.60	197.49	43.11	6
59.35	385.33	92.71	292.62	231.44	61.18	6
58.80	424.08	80.73	343.35	265.56	77.79	6
58.25	462.98	70.63	392.35	299.85	92.51	6
57.70	502.02	62.65	439.37	334.26	105.11	6
57.15	541.15	56.82	484.33	368.77	115.55	6
56.59	580.35	53.01	527.34	403.35	123.98	6
56.04	619.59	50.93	568.67	437.98	130.69	6
56.04	619.59	50.93	568.67	437.98	130.69	5
54.78	724.14	72.71	651.43	516.77	134.66	5
53.53	827.88	95.83	732.05	594.77	137.29	5
52.29	930.78	119.92	810.86	671.91	138.95	5
51.07	1032.79	144.66	888.13	748.18	139.96	5
49.86	1133.91	169.83	964.09	823.55	140.54	5
48.67	1234.13	195.28	1038.84	898.01	140.83	5
48.67	1234.13	195.28	1038.84	898.01	140.83	4
46.67	1434.55	268.49	1166.06	1022.58	143.48	4
44.68	1634.47	347.13	1287.34	1146.63	140.71	4
42.70	1833.82	433.99	1399.83	1270.12	129.71	4
40.73	2032.53	518.94	1513.59	1392.98	120.61	4
38.78	2230.53	582.36	1648.17	1515.12	133.05	4
36.83	2427.74	650.34	1777.41	1636.47	140.94	4
34.90	2624.12	722.58	1901.54	1756.99	144.55	4
32.98	2819.61	798.34	2021.28	1876.62	144.65	4
31.08	3014.20	874.19	2140.00	1995.35	144.65	4
31.08	3014.20	874.19	2140.00	1995.35	144.65	3
29.69	3162.77	936.05	2226.71	2082.06	144.65	3
28.31	3310.94	997.91	2313.03	2168.37	144.65	3
26.93	3458.74	1062.82	2395.91	2254.31	141.60	3
25.56	3606.18	1126.30	2479.88	2339.89	139.99	3
24.19	3753.26	1188.85	2564.41	2425.11	139.29	3
22.83	3899.99	1250.66	2649.33	2509.99	139.34	3
21.48	4046.38	1312.27	2734.11	2594.52	139.59	3
20.13	4192.42	1373.45	2818.96	2678.70	140.27	3
18.79	4338.11	1434.37	2903.74	2762.54	141.21	3
18.79	4338.11	1434.37	2903.74	2762.54	141.21	2
16.87	4543.77	1518.54	3025.22	2882.09	143.13	2
14.96	4748.90	1603.41	3145.49	3001.13	144.37	2
13.06	4953.51	1689.22	3264.29	3119.64	144.66	2
11.17	5157.59	1775.31	3382.27	3237.62	144.66	2
9.29	5361.14	1861.41	3499.73	3355.08	144.66	2
7.42	5564.16	1947.51	3616.65	3471.99	144.66	2
5.55	5766.67	2033.61	3733.06	3588.41	144.66	2
3.69	5968.76	2137.52	3831.24	3704.40	126.84	2
1.84	6170.38	2266.42	3903.96	3819.92	84.04	2
.00	6371.39	2435.86	3935.52	3934.83	.69	2

Time = 120. Degree of Consolidation = 12.%

Total Settlement = .150

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 120. = .150

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.64	29.65	47.99	41.47	6.52	1
1.30	154.72	59.87	94.84	82.39	12.46	1
.65	231.61	90.98	140.63	123.12	17.51	1
.00	308.40	120.52	187.88	163.74	24.14	1

Time = 120. Degree of Consolidation = 96.%

Total Settlement = .076

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 120. = .076

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.07

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.35	21.42	6.50	6.13	6.06	6
60.02	59.81	21.35	6.49	6.16	6.05	6

59.45	59.27	21.27	6.47	6.18	6.04	6
58.89	58.73	21.20	6.46	6.21	6.02	6
58.33	58.18	21.12	6.44	6.23	6.01	6
57.76	57.63	21.05	6.43	6.25	5.99	6
57.20	57.09	20.97	6.42	6.27	5.98	6
56.64	56.54	20.90	6.40	6.29	5.97	6
56.08	55.98	20.82	6.39	6.30	5.95	6
56.08	55.98	20.82	4.51	4.43	4.15	5
54.82	54.73	20.59	4.44	4.38	4.09	5
53.56	53.49	20.36	4.38	4.33	4.02	5
52.32	52.26	20.12	4.32	4.27	3.96	5
51.10	51.04	19.89	4.25	4.22	3.89	5
49.88	49.84	19.66	4.19	4.15	3.83	5
48.69	48.65	19.43	4.13	4.09	3.77	5
48.69	48.65	19.43	1.93	1.93	1.91	4
46.69	46.66	18.75	1.92	1.92	1.89	4
44.70	44.67	18.06	1.91	1.90	1.88	4
42.72	42.69	17.38	1.89	1.89	1.86	4
40.75	40.73	16.70	1.88	1.87	1.84	4
38.79	38.77	16.01	1.86	1.85	1.82	4
36.85	36.83	15.33	1.84	1.84	1.80	4
34.91	34.90	14.65	1.82	1.82	1.78	4
33.00	32.98	13.97	1.80	1.80	1.76	4
31.09	31.08	13.28	1.78	1.78	1.73	4
31.09	31.08	13.28	1.47	1.47	1.45	3
29.70	29.69	12.72	1.46	1.46	1.44	3
28.32	28.30	12.16	1.45	1.45	1.43	3
26.94	26.93	11.59	1.44	1.44	1.42	3
25.57	25.55	11.03	1.43	1.43	1.41	3
24.21	24.19	10.47	1.42	1.42	1.40	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.35	308.39	123.30	185.09	163.73	21.36	6
59.81	346.68	114.05	232.63	197.40	35.22	6
59.27	385.10	105.11	279.99	231.20	48.78	6
58.73	423.64	96.67	326.97	265.13	61.85	6
58.18	462.30	88.89	373.42	299.17	74.25	6
57.63	501.07	81.91	419.16	333.31	85.85	6
57.09	539.93	75.83	464.10	367.55	96.55	6
56.54	578.87	70.70	508.16	401.87	106.29	6
55.98	617.87	66.55	551.32	436.25	115.06	6
55.98	617.87	66.55	551.32	436.25	115.06	5
54.73	721.88	87.06	634.82	514.51	120.31	5
53.49	825.13	108.68	716.45	592.02	124.43	5
52.26	927.59	131.38	796.21	668.72	127.49	5

51.04	1029.22	155.04	874.18	744.60	129.58	5
49.84	1129.98	179.59	950.39	819.61	130.78	5
48.65	1229.84	205.00	1024.84	893.73	131.12	5
48.65	1229.84	205.00	1024.84	893.73	131.12	4
46.66	1430.21	277.76	1152.45	1018.23	134.22	4
44.67	1630.05	357.18	1272.87	1142.22	130.65	4
42.69	1829.33	446.18	1383.15	1265.63	117.52	4
40.73	2027.96	526.76	1501.20	1388.40	112.79	4
38.77	2225.86	589.33	1636.53	1510.45	126.08	4
36.83	2423.00	655.32	1767.68	1631.73	135.95	4
34.90	2619.34	724.91	1894.43	1752.21	142.22	4
32.98	2814.82	798.34	2016.48	1871.83	144.65	4
31.08	3009.40	874.19	2135.21	1990.55	144.65	4
31.08	3009.40	874.20	2135.21	1990.55	144.65	3
29.69	3157.97	936.05	2221.92	2077.26	144.65	3
28.30	3306.15	997.91	2308.24	2163.58	144.65	3
26.93	3453.94	1064.61	2389.33	2249.52	139.82	3
25.55	3601.36	1129.44	2471.92	2335.08	136.84	3
24.19	3748.43	1192.61	2555.81	2420.28	135.53	3
22.83	3895.14	1254.64	2640.50	2505.14	135.36	3
21.48	4041.50	1316.09	2725.41	2589.64	135.77	3
20.13	4187.52	1377.11	2810.41	2673.80	136.61	3
18.78	4333.20	1437.58	2895.62	2757.62	138.00	3
18.78	4333.20	1437.58	2895.62	2757.62	138.00	2
16.87	4538.83	1520.77	3018.06	2877.16	140.91	2
14.96	4743.96	1604.60	3139.35	2996.18	143.17	2
13.06	4948.56	1689.35	3259.22	3114.69	144.53	2
11.17	5152.64	1775.31	3377.33	3232.67	144.65	2
9.29	5356.20	1861.41	3494.79	3350.13	144.66	2
7.41	5559.21	1947.51	3611.70	3467.04	144.66	2
5.55	5761.73	2036.24	3725.49	3583.46	142.02	2
3.69	5963.77	2155.11	3808.66	3699.41	109.25	2
1.84	6165.30	2288.48	3876.82	3814.84	61.98	2
.00	6366.25	2436.05	3930.21	3929.70	.51	2

Time = 240. Degree of Consolidation = 19.%

Total Settlement = .232

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 240. = .232

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.72	47.92	41.47	6.45	1
1.30	154.71	60.53	94.19	82.39	11.80	1
.65	231.60	92.05	139.55	123.11	16.44	1
.00	308.39	123.30	185.09	163.73	21.36	1

Time = 240. Degree of Consolidation = 96.%

Total Settlement = .076

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 240. = .076

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .99

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.28	21.42	6.50	6.12	6.06	6
60.02	59.74	21.35	6.49	6.15	6.05	6
59.45	59.20	21.27	6.47	6.17	6.04	6
58.89	58.66	21.20	6.46	6.19	6.02	6
58.33	58.12	21.12	6.44	6.20	6.01	6
57.76	57.57	21.05	6.43	6.22	5.99	6
57.20	57.02	20.97	6.42	6.24	5.98	6
56.64	56.48	20.90	6.40	6.25	5.97	6
56.08	55.93	20.82	6.39	6.26	5.95	6
56.08	55.93	20.82	4.51	4.40	4.15	5
54.82	54.68	20.59	4.44	4.35	4.09	5
53.56	53.45	20.36	4.38	4.30	4.02	5
52.32	52.23	20.12	4.32	4.24	3.96	5
51.10	51.02	19.89	4.25	4.18	3.89	5
49.88	49.82	19.66	4.19	4.12	3.83	5
48.69	48.64	19.43	4.13	4.06	3.77	5
48.69	48.64	19.43	1.93	1.93	1.91	4
46.69	46.65	18.75	1.92	1.91	1.89	4
44.70	44.66	18.06	1.91	1.90	1.88	4
42.72	42.68	17.38	1.89	1.89	1.86	4
40.75	40.72	16.70	1.88	1.87	1.84	4
38.79	38.76	16.01	1.86	1.85	1.82	4
36.85	36.82	15.33	1.84	1.84	1.80	4
34.91	34.89	14.65	1.82	1.82	1.78	4
33.00	32.97	13.97	1.80	1.80	1.76	4
31.09	31.07	13.28	1.78	1.78	1.73	4
31.09	31.07	13.28	1.47	1.47	1.45	3
29.70	29.68	12.72	1.46	1.46	1.44	3
28.32	28.30	12.16	1.45	1.45	1.43	3
26.94	26.92	11.59	1.44	1.44	1.42	3
25.57	25.55	11.03	1.43	1.43	1.41	3

24.21	24.19	10.47	1.42	1.40		3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.28	308.38	124.53	183.85	163.73	20.12	6
59.74	346.64	117.51	229.13	197.37	31.77	6
59.20	385.00	110.66	274.34	231.10	43.24	6
58.66	423.45	104.10	319.35	264.93	54.42	6
58.12	461.99	97.94	364.05	298.85	65.20	6
57.57	500.62	92.26	408.35	332.86	75.49	6
57.02	539.32	87.18	452.14	366.94	85.19	6
56.48	578.09	82.76	495.33	401.10	94.24	6
55.93	616.92	79.08	537.84	435.30	102.54	6
55.93	616.92	79.08	537.84	435.30	102.54	5
54.68	720.48	99.82	620.65	513.11	107.55	5
53.45	823.27	121.49	701.78	590.15	111.62	5
52.23	925.27	144.08	781.19	666.40	114.79	5
51.02	1026.44	167.60	858.84	741.83	117.01	5
49.82	1126.76	192.05	934.71	816.39	118.32	5
48.64	1226.18	217.39	1008.79	890.06	118.73	5
48.64	1226.18	217.39	1008.79	890.06	118.73	4
46.65	1426.46	289.53	1136.92	1014.48	122.44	4
44.66	1626.22	368.72	1257.50	1138.39	119.11	4
42.68	1825.42	457.79	1367.63	1261.73	105.90	4
40.72	2023.97	533.20	1490.77	1384.42	106.35	4
38.76	2221.81	594.87	1626.93	1506.39	120.54	4
36.82	2418.89	659.59	1759.30	1627.62	131.69	4
34.89	2615.18	727.32	1887.86	1748.05	139.81	4
32.97	2810.64	798.65	2012.00	1867.65	144.34	4
31.07	3005.23	874.33	2130.90	1986.38	144.52	4
31.07	3005.23	874.33	2130.90	1986.38	144.52	3
29.68	3153.80	936.05	2217.75	2073.09	144.65	3
28.30	3301.98	997.91	2304.06	2159.41	144.65	3
26.92	3449.76	1065.90	2383.87	2245.34	138.53	3
25.55	3597.18	1131.66	2465.52	2330.89	134.62	3
24.19	3744.22	1195.74	2548.48	2416.08	132.40	3
22.83	3890.92	1258.33	2632.59	2500.91	131.67	3
21.47	4037.26	1319.77	2717.48	2585.40	132.09	3
20.12	4183.26	1380.80	2802.46	2669.54	132.92	3
18.78	4328.92	1440.85	2888.06	2753.34	134.72	3
18.78	4328.92	1440.85	2888.06	2753.34	134.72	2
16.87	4534.53	1523.19	3011.34	2872.86	138.48	2
14.96	4739.64	1606.25	3133.39	2991.87	141.52	2
13.06	4944.24	1690.19	3254.05	3110.37	143.68	2
11.17	5148.32	1775.31	3373.00	3228.35	144.66	2
9.29	5351.87	1861.41	3490.46	3345.81	144.66	2

7.41	5554.89	1947.51	3607.38	3462.72	144.66	2
5.55	5757.40	2042.49	3714.91	3579.13	135.77	2
3.69	5959.40	2167.42	3791.98	3695.04	96.94	2
1.84	6160.88	2299.13	3861.75	3810.42	51.33	2
.00	6361.81	2436.13	3925.67	3925.25	.42	2

Time = 365. Degree of Consolidation = 25.%

Total Settlement = .304

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 365. = .304

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.75	47.89	41.47	6.42	1
1.30	154.71	60.82	93.90	82.39	11.51	1
.65	231.60	92.52	139.08	123.11	15.97	1
.00	308.38	124.53	183.85	163.73	20.12	1

Time = 365. Degree of Consolidation = 96.%

Total Settlement = .076

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 365. = .076

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .92

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.19	21.42	6.50	6.12	6.06	6
60.02	59.65	21.35	6.49	6.14	6.05	6
59.45	59.12	21.27	6.47	6.15	6.04	6
58.89	58.57	21.20	6.46	6.16	6.02	6
58.33	58.03	21.12	6.44	6.18	6.01	6
57.76	57.49	21.05	6.43	6.19	5.99	6
57.20	56.95	20.97	6.42	6.20	5.98	6
56.64	56.40	20.90	6.40	6.21	5.97	6
56.08	55.86	20.82	6.39	6.22	5.95	6
56.08	55.86	20.82	4.51	4.37	4.15	5
54.82	54.62	20.59	4.44	4.31	4.09	5
53.56	53.39	20.36	4.38	4.26	4.02	5
52.32	52.18	20.12	4.32	4.20	3.96	5
51.10	50.98	19.89	4.25	4.14	3.89	5
49.88	49.80	19.66	4.19	4.08	3.83	5
48.69	48.62	19.43	4.13	4.02	3.77	5
48.69	48.62	19.43	1.93	1.92	1.91	4
46.69	46.63	18.75	1.92	1.91	1.89	4
44.70	44.65	18.06	1.91	1.90	1.88	4
42.72	42.67	17.38	1.89	1.88	1.86	4
40.75	40.71	16.70	1.88	1.87	1.84	4
38.79	38.76	16.01	1.86	1.85	1.82	4
36.85	36.81	15.33	1.84	1.83	1.80	4
34.91	34.89	14.65	1.82	1.82	1.78	4
33.00	32.97	13.97	1.80	1.80	1.76	4
31.09	31.07	13.28	1.78	1.77	1.73	4
31.09	31.07	13.28	1.47	1.47	1.45	3
29.70	29.68	12.72	1.46	1.46	1.44	3
28.32	28.29	12.16	1.45	1.45	1.43	3
26.94	26.92	11.59	1.44	1.44	1.42	3
25.57	25.55	11.03	1.43	1.43	1.41	3
24.21	24.18	10.47	1.42	1.42	1.40	3
22.84	22.82	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.19	308.38	125.65	182.73	163.72	19.01	6
59.65	346.61	120.62	225.99	197.33	28.66	6
59.12	384.90	115.72	269.18	231.01	38.17	6
58.57	423.27	111.05	312.22	264.75	47.47	6
58.03	461.70	106.68	355.02	298.56	56.46	6
57.49	500.19	102.69	397.50	332.43	65.07	6
56.95	538.73	99.17	439.56	366.36	73.21	6
56.40	577.32	96.18	481.14	400.33	80.81	6

55.86	615.95	93.80	522.15	434.34	87.81	6
55.86	615.95	93.80	522.15	434.34	87.81	5
54.62	718.97	115.30	603.67	511.60	92.07	5
53.39	821.19	137.52	683.67	588.08	95.59	5
52.18	922.61	160.50	762.11	663.74	98.37	5
50.98	1023.19	184.26	838.93	738.57	100.36	5
49.80	1122.90	208.78	914.12	812.54	101.59	5
48.62	1221.72	234.07	987.65	885.61	102.05	5
48.62	1221.72	234.07	987.65	885.61	102.05	4
46.63	1421.89	305.77	1116.12	1009.92	106.21	4
44.65	1621.55	384.67	1236.88	1133.71	103.16	4
42.67	1820.64	473.70	1346.94	1256.94	89.99	4
40.71	2019.08	541.90	1477.17	1379.53	97.65	4
38.76	2216.82	602.26	1614.56	1501.41	113.15	4
36.81	2413.82	665.46	1748.36	1622.55	125.81	4
34.89	2610.05	731.66	1878.40	1742.92	135.47	4
32.97	2805.47	801.42	2004.05	1862.48	141.57	4
31.07	3000.04	875.71	2124.32	1981.19	143.14	4
31.07	3000.04	875.71	2124.32	1981.19	143.14	3
29.68	3148.60	936.05	2212.55	2067.89	144.65	3
28.29	3296.78	997.91	2298.87	2154.21	144.65	3
26.92	3444.57	1067.21	2377.36	2240.14	137.22	3
25.55	3591.97	1134.25	2457.72	2325.68	132.04	3
24.18	3739.00	1198.98	2540.02	2410.85	129.16	3
22.82	3885.67	1262.20	2623.47	2495.67	127.80	3
21.47	4031.99	1324.10	2707.89	2580.13	127.76	3
20.12	4177.96	1384.85	2793.12	2664.24	128.87	3
18.78	4323.60	1444.56	2879.04	2748.02	131.02	3
18.78	4323.60	1444.56	2879.04	2748.02	131.02	2
16.86	4529.20	1526.19	3003.01	2867.52	135.48	2
14.96	4734.29	1608.41	3125.89	2986.52	139.37	2
13.06	4938.88	1691.46	3247.41	3105.01	142.41	2
11.17	5142.95	1775.68	3367.27	3222.98	144.29	2
9.28	5346.50	1861.41	3485.09	3340.43	144.66	2
7.41	5549.52	1947.51	3602.01	3457.35	144.66	2
5.55	5752.02	2047.77	3704.25	3573.75	130.49	2
3.69	5953.99	2176.30	3777.69	3689.63	88.06	2
1.84	6155.44	2306.25	3849.19	3804.98	44.21	2
.00	6356.35	2436.19	3920.15	3919.79	.36	2

Time = 540. Degree of Consolidation = 32.%

Total Settlement = .391

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 540. = .391

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1

.68	.65	.34	.98	.91	1
.00	.00	.00	.98	.91	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.77	47.86	41.47	6.39	1
1.30	154.71	61.08	93.63	82.38	11.25	1
.65	231.60	92.95	138.65	123.11	15.54	1
.00	308.38	125.65	182.73	163.72	19.01	1

Time = 540. Degree of Consolidation = 96.%

Total Settlement = .076

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 540. = .076

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .83

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.11	21.42	6.50	6.12	6.06	6
60.02	59.57	21.35	6.49	6.13	6.05	6
59.45	59.03	21.27	6.47	6.14	6.04	6
58.89	58.49	21.20	6.46	6.15	6.02	6
58.33	57.95	21.12	6.44	6.15	6.01	6
57.76	57.41	21.05	6.43	6.16	5.99	6
57.20	56.87	20.97	6.42	6.17	5.98	6
56.64	56.33	20.90	6.40	6.17	5.97	6
56.08	55.79	20.82	6.39	6.18	5.95	6
56.08	55.79	20.82	4.51	4.33	4.15	5
54.82	54.56	20.59	4.44	4.28	4.09	5
53.56	53.34	20.36	4.38	4.22	4.02	5
52.32	52.14	20.12	4.32	4.16	3.96	5
51.10	50.95	19.89	4.25	4.10	3.89	5
49.88	49.77	19.66	4.19	4.04	3.83	5
48.69	48.61	19.43	4.13	3.98	3.77	5
48.69	48.61	19.43	1.93	1.92	1.91	4
46.69	46.62	18.75	1.92	1.91	1.89	4
44.70	44.64	18.06	1.91	1.90	1.88	4
42.72	42.66	17.38	1.89	1.88	1.86	4
40.75	40.70	16.70	1.88	1.87	1.84	4
38.79	38.75	16.01	1.86	1.85	1.82	4
36.85	36.81	15.33	1.84	1.83	1.80	4
34.91	34.88	14.65	1.82	1.81	1.78	4
33.00	32.97	13.97	1.80	1.79	1.76	4
31.09	31.06	13.28	1.78	1.77	1.73	4

31.09	31.06	13.28	1.47	1.47	1.45	3
29.70	29.67	12.72	1.46	1.46	1.44	3
28.32	28.29	12.16	1.45	1.45	1.43	3
26.94	26.91	11.59	1.44	1.44	1.42	3
25.57	25.54	11.03	1.43	1.43	1.41	3
24.21	24.18	10.47	1.42	1.42	1.40	3
22.84	22.82	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.95	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.11	308.37	126.63	181.74	163.72	18.02	6
59.57	346.58	123.35	223.22	197.30	25.92	6
59.03	384.82	120.19	264.63	230.93	33.71	6
58.49	423.11	117.22	305.89	264.60	41.30	6
57.95	461.44	114.50	346.94	298.31	48.63	6
57.41	499.81	112.12	387.69	332.05	55.64	6
56.87	538.21	110.12	428.09	365.83	62.26	6
56.33	576.63	108.58	468.05	399.64	68.41	6
55.79	615.07	107.57	507.50	433.46	74.05	6
55.79	615.07	107.57	507.50	433.46	74.05	5
54.56	717.58	129.86	587.71	510.21	77.50	5
53.34	819.27	152.75	666.52	586.16	80.36	5
52.14	920.13	176.23	743.90	661.27	82.63	5
50.95	1020.14	200.33	819.82	735.53	84.29	5
49.77	1119.28	225.03	894.25	808.91	85.34	5
48.61	1217.51	250.36	967.16	881.39	85.76	5
48.61	1217.51	250.36	967.16	881.39	85.76	4
46.62	1417.57	322.43	1095.14	1005.59	89.54	4
44.64	1617.11	401.49	1215.62	1129.28	86.35	4
42.66	1816.08	490.53	1325.56	1252.39	73.17	4
40.70	2014.41	551.05	1463.36	1374.86	88.51	4
38.75	2212.05	610.21	1601.84	1496.64	105.20	4
36.81	2408.97	671.87	1737.09	1617.69	119.40	4
34.88	2605.13	736.46	1868.67	1738.00	130.67	4
32.97	2800.50	804.63	1995.88	1857.51	138.36	4
31.06	2995.04	877.37	2117.67	1976.19	141.48	4
31.06	2995.04	877.37	2117.67	1976.19	141.48	3
29.67	3143.60	936.25	2207.35	2062.89	144.46	3
28.29	3291.78	998.08	2293.69	2149.21	144.48	3
26.91	3439.56	1068.32	2371.23	2235.13	136.10	3
25.54	3586.95	1136.26	2450.69	2320.67	130.02	3
24.18	3733.97	1201.76	2532.21	2405.82	126.39	3
22.82	3880.62	1265.01	2615.62	2490.62	124.99	3
21.47	4026.93	1326.91	2700.02	2575.07	124.95	3
20.12	4172.89	1387.65	2785.24	2659.17	126.07	3
18.78	4318.51	1447.11	2871.40	2742.93	128.47	3
18.78	4318.51	1447.11	2871.40	2742.93	128.47	2

16.86	4524.09	1528.26	2995.83	2862.42	133.41	2
14.95	4729.17	1609.99	3119.18	2981.40	137.78	2
13.06	4933.75	1692.54	3241.21	3099.88	141.33	2
11.17	5137.82	1776.23	3361.59	3217.85	143.74	2
9.28	5341.37	1861.41	3479.95	3335.30	144.66	2
7.41	5544.39	1947.51	3596.88	3452.22	144.66	2
5.54	5746.87	2052.33	3694.54	3568.61	125.93	2
3.69	5948.83	2181.91	3766.91	3684.46	82.45	2
1.84	6150.25	2310.68	3839.57	3799.79	39.78	2
.00	6351.15	2436.23	3914.92	3914.59	.33	2

Time = 730. Degree of Consolidation = 39.%

Total Settlement = .474

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 730. = .474

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.80	47.84	41.47	6.37	1
1.30	154.71	61.31	93.40	82.38	11.02	1
.65	231.60	93.32	138.27	123.10	15.17	1
.00	308.37	126.63	181.74	163.72	18.02	1

Time = 730. Degree of Consolidation = 96.%

Total Settlement = .076

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 730. = .076

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .75

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.98	21.42	6.50	6.11	6.06	6
60.02	59.44	21.35	6.49	6.11	6.05	6
59.45	58.90	21.27	6.47	6.12	6.04	6
58.89	58.36	21.20	6.46	6.12	6.02	6
58.33	57.83	21.12	6.44	6.12	6.01	6
57.76	57.29	21.05	6.43	6.12	5.99	6
57.20	56.75	20.97	6.42	6.12	5.98	6
56.64	56.21	20.90	6.40	6.11	5.97	6
56.08	55.68	20.82	6.39	6.11	5.95	6
56.08	55.68	20.82	4.51	4.28	4.15	5
54.82	54.46	20.59	4.44	4.22	4.09	5
53.56	53.25	20.36	4.38	4.16	4.02	5
52.32	52.06	20.12	4.32	4.10	3.96	5
51.10	50.89	19.89	4.25	4.04	3.89	5
49.88	49.73	19.66	4.19	3.98	3.83	5
48.69	48.58	19.43	4.13	3.92	3.77	5
48.69	48.58	19.43	1.93	1.92	1.91	4
46.69	46.59	18.75	1.92	1.90	1.89	4
44.70	44.61	18.06	1.91	1.89	1.88	4
42.72	42.64	17.38	1.89	1.88	1.86	4
40.75	40.68	16.70	1.88	1.86	1.84	4
38.79	38.73	16.01	1.86	1.85	1.82	4
36.85	36.80	15.33	1.84	1.83	1.80	4
34.91	34.87	14.65	1.82	1.81	1.78	4
33.00	32.96	13.97	1.80	1.79	1.76	4
31.09	31.06	13.28	1.78	1.77	1.73	4
31.09	31.06	13.28	1.47	1.47	1.45	3
29.70	29.67	12.72	1.46	1.46	1.44	3
28.32	28.29	12.16	1.45	1.45	1.43	3
26.94	26.91	11.59	1.44	1.44	1.42	3
25.57	25.54	11.03	1.43	1.43	1.41	3
24.21	24.17	10.47	1.42	1.42	1.40	3
22.84	22.82	9.90	1.41	1.41	1.39	3
21.49	21.46	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.77	8.21	1.38	1.38	1.36	3
18.80	18.77	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.95	6.57	1.32	1.32	1.30	2
13.07	13.05	5.75	1.31	1.31	1.29	2
11.18	11.16	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.98	308.37	128.15	180.22	163.71	16.51	6
59.44	346.53	127.51	219.01	197.25	21.76	6
58.90	384.70	126.97	257.73	230.80	26.92	6

58.36	422.87	126.58	296.30	264.36	31.94	6
57.83	461.05	126.38	334.67	297.92	36.76	6
57.29	499.23	126.43	372.80	331.48	41.32	6
56.75	537.41	126.80	410.61	365.03	45.58	6
56.21	575.58	127.52	448.06	398.58	49.48	6
55.68	613.74	128.65	485.09	432.12	52.97	6
55.68	613.74	128.65	485.09	432.12	52.97	5
54.46	715.46	152.23	563.23	508.09	55.13	5
53.25	816.33	176.18	640.15	583.22	56.94	5
52.06	916.34	200.48	715.86	657.47	58.38	5
50.89	1015.47	225.17	790.30	730.85	59.45	5
49.73	1113.70	250.22	863.48	803.33	60.15	5
48.58	1211.03	275.65	935.38	874.91	60.47	5
48.58	1211.03	275.65	935.38	874.91	60.47	4
46.59	1410.91	348.58	1062.33	998.94	63.39	4
44.61	1610.27	428.51	1181.77	1122.44	59.33	4
42.64	1809.06	510.36	1298.70	1245.37	53.34	4
40.68	2007.20	566.04	1441.16	1367.65	73.51	4
38.73	2204.67	623.63	1581.04	1489.26	91.78	4
36.80	2401.44	683.68	1717.76	1610.17	107.59	4
34.87	2597.47	746.48	1850.99	1730.34	120.65	4
32.96	2792.74	812.99	1979.75	1849.74	130.00	4
31.06	2987.18	884.45	2102.73	1968.33	134.40	4
31.06	2987.18	884.45	2102.73	1968.33	134.40	3
29.67	3135.70	942.18	2193.52	2054.99	138.53	3
28.29	3283.84	1003.58	2280.26	2141.27	138.98	3
26.91	3431.59	1073.49	2358.10	2227.17	130.94	3
25.54	3578.95	1141.42	2437.54	2312.67	124.87	3
24.17	3725.94	1206.91	2519.03	2397.80	121.23	3
22.82	3872.57	1270.17	2602.40	2482.57	119.83	3
21.46	4018.84	1332.07	2686.77	2566.98	119.79	3
20.12	4164.77	1392.82	2771.96	2651.06	120.90	3
18.77	4310.37	1452.09	2858.27	2734.79	123.49	3
18.77	4310.37	1452.09	2858.27	2734.79	123.49	2
16.86	4515.92	1532.67	2983.26	2854.25	129.01	2
14.95	4720.98	1613.80	3107.18	2973.21	133.97	2
13.05	4925.54	1695.76	3229.78	3091.66	138.12	2
11.16	5129.58	1778.82	3350.76	3209.61	141.15	2
9.28	5333.12	1863.37	3469.75	3327.05	142.70	2
7.41	5536.13	1949.82	3586.31	3443.96	142.35	2
5.54	5738.60	2056.36	3682.24	3560.33	121.90	2
3.69	5940.53	2186.39	3754.14	3676.17	77.97	2
1.84	6141.94	2312.88	3829.06	3791.48	37.58	2
.00	6342.84	2436.25	3906.59	3906.28	.31	2

Time = 1080. Degree of Consolidation = 50.%

Total Settlement = .607

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 1080. = .607

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.83	47.80	41.47	6.33	1
1.30	154.71	61.66	93.05	82.38	10.67	1
.65	231.59	93.90	137.69	123.10	14.59	1
.00	308.37	128.15	180.22	163.71	16.51	1

Time = 1080. Degree of Consolidation = 96.%

Total Settlement = .076

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 1080. = .076

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .62

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.86	21.42	6.50	6.11	6.06	6
60.02	59.33	21.35	6.49	6.10	6.05	6
59.45	58.79	21.27	6.47	6.10	6.04	6
58.89	58.25	21.20	6.46	6.09	6.02	6
58.33	57.72	21.12	6.44	6.09	6.01	6
57.76	57.18	21.05	6.43	6.08	5.99	6
57.20	56.65	20.97	6.42	6.08	5.98	6
56.64	56.11	20.90	6.40	6.07	5.97	6
56.08	55.58	20.82	6.39	6.06	5.95	6
56.08	55.58	20.82	4.51	4.24	4.15	5
54.82	54.37	20.59	4.44	4.18	4.09	5
53.56	53.18	20.36	4.38	4.12	4.02	5
52.32	52.00	20.12	4.32	4.05	3.96	5
51.10	50.84	19.89	4.25	3.99	3.89	5
49.88	49.69	19.66	4.19	3.93	3.83	5
48.69	48.55	19.43	4.13	3.86	3.77	5
48.69	48.55	19.43	1.93	1.91	1.91	4
46.69	46.57	18.75	1.92	1.90	1.89	4
44.70	44.59	18.06	1.91	1.89	1.88	4
42.72	42.62	17.38	1.89	1.87	1.86	4
40.75	40.66	16.70	1.88	1.86	1.84	4

38.79	38.72	16.01	1.86	1.84	1.82	4
36.85	36.78	15.33	1.84	1.83	1.80	4
34.91	34.86	14.65	1.82	1.81	1.78	4
33.00	32.95	13.97	1.80	1.79	1.76	4
31.09	31.05	13.28	1.78	1.77	1.73	4
31.09	31.05	13.28	1.47	1.47	1.45	3
29.70	29.66	12.72	1.46	1.46	1.44	3
28.32	28.28	12.16	1.45	1.45	1.43	3
26.94	26.90	11.59	1.44	1.44	1.42	3
25.57	25.53	11.03	1.43	1.43	1.41	3
24.21	24.17	10.47	1.42	1.42	1.40	3
22.84	22.81	9.90	1.41	1.41	1.39	3
21.49	21.46	9.34	1.40	1.40	1.38	3
20.14	20.11	8.78	1.39	1.39	1.37	3
18.80	18.77	8.21	1.38	1.38	1.36	3
18.80	18.77	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.95	6.57	1.32	1.32	1.30	2
13.07	13.05	5.75	1.31	1.31	1.29	2
11.18	11.16	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.86	308.36	129.39	178.97	163.71	15.26	6
59.33	346.49	130.92	215.57	197.22	18.36	6
58.79	384.60	132.50	252.09	230.70	21.39	6
58.25	422.68	134.21	288.47	264.16	24.31	6
57.72	460.73	136.07	324.66	297.60	27.06	6
57.18	498.76	138.13	360.63	331.01	29.62	6
56.65	536.76	140.44	396.32	364.38	31.94	6
56.11	574.72	143.02	431.71	397.73	33.98	6
55.58	612.65	145.92	466.73	431.03	35.70	6
55.58	612.65	145.92	466.73	431.03	35.70	5
54.37	713.73	170.58	543.15	506.36	36.79	5
53.18	813.93	195.42	618.50	580.81	37.69	5
52.00	913.23	220.44	692.79	654.36	38.42	5
50.84	1011.63	245.67	765.96	727.01	38.95	5
49.69	1109.12	271.08	838.04	798.75	39.29	5
48.55	1205.70	296.67	909.03	869.58	39.45	5
48.55	1205.70	296.67	909.03	869.58	39.45	4
46.57	1405.43	371.08	1034.36	993.46	40.90	4
44.59	1604.64	452.70	1151.94	1116.80	35.13	4
42.62	1803.25	524.57	1278.69	1239.56	39.13	4
40.66	2001.23	579.42	1421.81	1361.68	60.13	4
38.72	2198.55	636.22	1562.33	1483.13	79.19	4
36.78	2395.17	695.40	1699.76	1603.89	95.87	4
34.86	2591.07	757.32	1833.74	1723.93	109.81	4
32.95	2786.21	822.97	1963.24	1843.22	120.02	4
31.05	2980.53	893.85	2086.68	1961.68	125.00	4
31.05	2980.53	893.85	2086.68	1961.68	125.00	3
29.66	3128.99	951.02	2177.97	2048.29	129.68	3
28.28	3277.08	1012.50	2264.58	2134.52	130.06	3
26.90	3424.79	1080.87	2343.91	2220.36	123.55	3
25.53	3572.11	1147.38	2424.74	2305.83	118.91	3
24.17	3719.07	1212.22	2506.86	2390.93	115.93	3

22.81	3865.67	1275.48	2590.19	2475.67	114.52	3
21.46	4011.91	1337.38	2674.54	2560.05	114.48	3
20.11	4157.81	1398.12	2759.69	2644.09	115.60	3
18.77	4303.38	1457.18	2846.19	2727.80	118.39	3
18.77	4303.38	1457.18	2846.19	2727.80	118.39	2
16.86	4508.90	1537.31	2971.59	2847.23	124.36	2
14.95	4713.93	1618.00	3095.93	2966.16	129.77	2
13.05	4918.46	1699.51	3218.96	3084.59	134.37	2
11.16	5122.49	1782.11	3340.38	3202.52	137.86	2
9.28	5326.01	1866.18	3459.82	3319.94	139.89	2
7.41	5529.00	1952.14	3576.85	3436.83	140.02	2
5.54	5731.46	2059.00	3672.46	3553.19	119.26	2
3.69	5933.38	2188.11	3745.27	3669.02	76.25	2
1.84	6134.79	2313.72	3821.06	3784.33	36.74	2
.00	6335.68	2436.25	3899.43	3899.12	.30	2

Time = 1440. Degree of Consolidation = 59.%

Total Settlement = .722

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 1440. = .722

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.86	47.77	41.47	6.30	1
1.30	154.71	61.94	92.77	82.38	10.38	1
.65	231.59	94.37	137.22	123.10	14.12	1
.00	308.36	129.39	178.97	163.71	15.26	1

Time = 1440. Degree of Consolidation = 96.%

Total Settlement = .076

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 1440. = .076

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .50

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.76	21.42	6.50	6.11	6.06	6
60.02	59.22	21.35	6.49	6.10	6.05	6
59.45	58.69	21.27	6.47	6.09	6.04	6
58.89	58.15	21.20	6.46	6.07	6.02	6
58.33	57.62	21.12	6.44	6.06	6.01	6
57.76	57.08	21.05	6.43	6.05	5.99	6
57.20	56.55	20.97	6.42	6.04	5.98	6
56.64	56.02	20.90	6.40	6.03	5.97	6
56.08	55.49	20.82	6.39	6.01	5.95	6
56.08	55.49	20.82	4.51	4.20	4.15	5
54.82	54.29	20.59	4.44	4.14	4.09	5
53.56	53.11	20.36	4.38	4.07	4.02	5
52.32	51.94	20.12	4.32	4.01	3.96	5
51.10	50.78	19.89	4.25	3.95	3.89	5
49.88	49.64	19.66	4.19	3.88	3.83	5
48.69	48.52	19.43	4.13	3.82	3.77	5
48.69	48.52	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.89	4
44.70	44.56	18.06	1.91	1.88	1.88	4
42.72	42.60	17.38	1.89	1.87	1.86	4
40.75	40.64	16.70	1.88	1.85	1.84	4
38.79	38.70	16.01	1.86	1.84	1.82	4
36.85	36.77	15.33	1.84	1.82	1.80	4
34.91	34.85	14.65	1.82	1.80	1.78	4
33.00	32.94	13.97	1.80	1.79	1.76	4
31.09	31.04	13.28	1.78	1.77	1.73	4
31.09	31.04	13.28	1.47	1.47	1.45	3
29.70	29.65	12.72	1.46	1.46	1.44	3
28.32	28.27	12.16	1.45	1.45	1.43	3
26.94	26.90	11.59	1.44	1.44	1.42	3
25.57	25.53	11.03	1.43	1.43	1.41	3
24.21	24.16	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.40	1.38	3
20.14	20.11	8.78	1.39	1.39	1.37	3
18.80	18.77	8.21	1.38	1.38	1.36	3
18.80	18.77	8.21	1.34	1.33	1.32	2
16.88	16.86	7.39	1.33	1.32	1.31	2
14.97	14.95	6.57	1.32	1.32	1.30	2
13.07	13.05	5.75	1.31	1.31	1.29	2
11.18	11.16	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.76	308.36	130.49	177.87	163.70	14.17	6
59.22	346.46	133.85	212.61	197.18	15.42	6
58.69	384.51	137.27	247.24	230.61	16.62	6
58.15	422.51	140.77	281.74	263.99	17.74	6
57.62	460.46	144.39	316.07	297.32	18.75	6
57.08	498.36	148.16	350.19	330.60	19.59	6
56.55	536.20	152.12	384.08	363.82	20.26	6
56.02	573.98	156.28	417.70	396.99	20.72	6
55.49	611.71	160.68	451.02	430.09	20.93	6
55.49	611.71	160.68	451.02	430.09	20.93	5
54.29	712.25	186.31	525.93	504.88	21.05	5
53.11	811.86	211.96	599.90	578.75	21.15	5
51.94	910.56	237.66	672.90	651.69	21.21	5
50.78	1008.33	263.38	744.95	723.71	21.24	5
49.64	1105.18	289.13	816.06	794.82	21.24	5
48.52	1201.11	314.89	886.22	864.99	21.23	5
48.52	1201.11	314.89	886.22	864.99	21.23	4
46.54	1400.71	391.00	1009.71	988.74	20.98	4
44.56	1599.77	474.90	1124.88	1111.94	12.94	4
42.60	1798.23	537.91	1260.32	1234.54	25.78	4
40.64	1996.05	592.56	1403.49	1356.50	46.99	4
38.70	2193.21	649.01	1544.21	1477.80	66.41	4
36.77	2389.69	707.54	1682.15	1598.41	83.73	4
34.85	2585.44	768.85	1816.59	1718.31	98.28	4
32.94	2780.45	833.95	1946.50	1837.46	109.04	4
31.04	2974.65	904.38	2070.26	1955.80	114.46	4
31.04	2974.65	904.38	2070.26	1955.80	114.46	3
29.65	3123.04	961.09	2161.96	2042.34	119.62	3
28.27	3271.07	1023.30	2247.77	2128.50	119.27	3
26.90	3418.72	1090.59	2328.13	2214.29	113.83	3
25.53	3565.99	1156.07	2409.92	2299.71	110.21	3
24.16	3712.90	1219.94	2492.97	2384.76	108.21	3
22.81	3859.46	1282.36	2577.09	2469.46	107.64	3
21.46	4005.67	1343.53	2662.13	2553.81	108.33	3
20.11	4151.53	1403.61	2747.92	2637.82	110.11	3
18.77	4297.07	1462.46	2834.61	2721.49	113.12	3
18.77	4297.07	1462.46	2834.61	2721.49	113.12	2
16.86	4502.56	1542.13	2960.44	2840.89	119.55	2
14.95	4707.56	1622.35	3085.21	2959.79	125.42	2
13.05	4912.07	1703.38	3208.69	3078.20	130.49	2
11.16	5116.08	1785.51	3330.56	3196.11	134.46	2
9.28	5319.57	1869.09	3450.48	3313.50	136.98	2
7.41	5522.55	1954.54	3568.00	3430.38	137.62	2
5.54	5724.99	2061.73	3663.27	3546.73	116.54	2
3.69	5926.91	2189.88	3737.03	3662.55	74.48	2
1.84	6128.31	2314.60	3813.71	3777.85	35.86	2
.00	6329.20	2436.26	3892.94	3892.64	.30	2

Time = 1825. Degree of Consolidation = 68.%

Total Settlement = .826

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 1825. = .826

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.89	47.75	41.47	6.28	1
1.30	154.71	62.20	92.51	82.38	10.13	1
.65	231.59	94.79	136.80	123.10	13.70	1
.00	308.36	130.49	177.87	163.70	14.17	1

Time = 1825. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 1825. = .077

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .40

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.63	21.42	6.50	6.10	6.06	6
60.02	59.09	21.35	6.49	6.09	6.05	6
59.45	58.56	21.27	6.47	6.07	6.04	6
58.89	58.03	21.20	6.46	6.06	6.02	6
58.33	57.49	21.12	6.44	6.04	6.01	6
57.76	56.96	21.05	6.43	6.03	5.99	6
57.20	56.43	20.97	6.42	6.01	5.98	6
56.64	55.90	20.90	6.40	6.00	5.97	6
56.08	55.37	20.82	6.39	5.98	5.95	6
56.08	55.37	20.82	4.51	4.17	4.15	5
54.82	54.19	20.59	4.44	4.09	4.09	5
53.56	53.01	20.36	4.38	4.02	4.02	5
52.32	51.86	20.12	4.32	3.96	3.96	5
51.10	50.71	19.89	4.25	3.89	3.89	5
49.88	49.59	19.66	4.19	3.83	3.83	5
48.69	48.47	19.43	4.13	3.77	3.77	5

48.69	48.47	19.43	1.93	1.91	1.91	4
46.69	46.49	18.75	1.92	1.89	1.89	4
44.70	44.52	18.06	1.91	1.88	1.88	4
42.72	42.56	17.38	1.89	1.87	1.86	4
40.75	40.61	16.70	1.88	1.85	1.84	4
38.79	38.67	16.01	1.86	1.83	1.82	4
36.85	36.74	15.33	1.84	1.82	1.80	4
34.91	34.82	14.65	1.82	1.80	1.78	4
33.00	32.91	13.97	1.80	1.78	1.76	4
31.09	31.02	13.28	1.78	1.76	1.73	4
31.09	31.02	13.28	1.47	1.46	1.45	3
29.70	29.63	12.72	1.46	1.45	1.44	3
28.32	28.25	12.16	1.45	1.44	1.43	3
26.94	26.88	11.59	1.44	1.43	1.42	3
25.57	25.51	11.03	1.43	1.42	1.41	3
24.21	24.15	10.47	1.42	1.41	1.40	3
22.84	22.80	9.90	1.41	1.40	1.39	3
21.49	21.45	9.34	1.40	1.39	1.38	3
20.14	20.10	8.78	1.39	1.38	1.37	3
18.80	18.76	8.21	1.38	1.37	1.36	3
18.80	18.76	8.21	1.34	1.33	1.32	2
16.88	16.85	7.39	1.33	1.32	1.31	2
14.97	14.95	6.57	1.32	1.31	1.30	2
13.07	13.05	5.75	1.31	1.30	1.29	2
11.18	11.16	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.63	308.36	131.51	176.85	163.70	13.15	6
59.09	346.43	136.52	209.91	197.15	12.76	6
58.56	384.43	141.52	242.91	230.53	12.37	6
58.03	422.36	146.52	275.84	263.84	12.00	6
57.49	460.22	151.51	308.71	297.08	11.63	6
56.96	498.00	156.49	341.51	330.25	11.26	6
56.43	535.72	161.47	374.25	363.34	10.91	6
55.90	573.37	166.44	406.93	396.37	10.56	6
55.37	610.94	171.39	439.55	429.32	10.22	6
55.37	610.94	171.39	439.55	429.32	10.22	5
54.19	710.85	207.37	503.48	503.48	.00	5
53.01	809.71	233.12	576.59	576.59	.00	5
51.86	907.64	258.87	648.78	648.78	.00	5
50.71	1004.65	284.62	720.04	720.04	.00	5
49.59	1100.74	310.37	790.38	790.38	.00	5
48.47	1195.91	336.12	859.79	859.79	.00	5
48.47	1195.91	336.12	859.79	859.79	.00	4
46.49	1395.37	409.21	986.16	983.40	2.77	4
44.52	1594.34	487.84	1106.51	1106.51	.00	4
42.56	1792.69	549.62	1243.06	1228.99	14.07	4
40.61	1990.35	606.88	1383.47	1350.80	32.67	4
38.67	2187.33	665.03	1522.29	1471.91	50.38	4
36.74	2383.60	724.56	1659.04	1592.33	66.71	4
34.82	2579.15	786.52	1792.63	1712.02	80.61	4
32.91	2773.95	851.98	1921.96	1830.96	91.01	4
31.02	2967.93	922.61	2045.31	1949.08	96.24	4
31.02	2967.93	922.61	2045.31	1949.08	96.24	3

29.63	3116.21	979.41	2136.80	2035.50	101.30	3
28.25	3264.12	1043.47	2220.65	2121.55	99.09	3
26.88	3411.66	1109.54	2302.12	2207.23	94.89	3
25.51	3558.83	1173.87	2384.96	2292.54	92.42	3
24.15	3705.64	1236.65	2468.99	2377.50	91.49	3
22.80	3852.11	1298.06	2554.04	2462.11	91.94	3
21.45	3998.23	1358.28	2639.95	2546.37	93.58	3
20.10	4144.02	1417.46	2726.56	2630.30	96.26	3
18.76	4289.47	1475.76	2813.72	2713.90	99.82	3
18.76	4289.47	1475.76	2813.72	2713.90	99.82	2
16.85	4494.89	1553.86	2941.03	2833.22	107.81	2
14.95	4699.82	1632.95	3066.87	2952.05	114.82	2
13.05	4904.27	1712.84	3191.43	3070.40	121.03	2
11.16	5108.22	1793.80	3314.42	3188.25	126.17	2
9.28	5311.67	1876.17	3435.50	3305.60	129.90	2
7.41	5514.61	1960.38	3554.22	3422.44	131.78	2
5.54	5717.02	2068.36	3648.66	3538.76	109.91	2
3.69	5918.91	2194.20	3724.71	3654.55	70.16	2
1.84	6120.30	2316.72	3803.58	3769.84	33.74	2
.00	6321.19	2436.28	3884.91	3884.63	.28	2

Time = 2520. Degree of Consolidation = 78.%

Total Settlement = .954

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 2520. = .956

Settlement caused by Secondary Compression at time 2520. = -.002

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.70	2.62	1.36
2.03	1.96	1.02
1.35	1.30	.68
.68	.65	.34
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
2.62	.00	.00
1.96	77.63	29.91
1.30	154.71	62.43
.65	231.58	95.17
.00	308.36	131.51

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
47.72	41.47	6.25	1
92.28	82.38	9.90	1
136.41	123.09	13.32	1
176.85	163.70	13.15	1

Time = 2520. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 2520. = .077

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .27

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.60	21.42	6.50	6.10	6.06	6
60.02	59.07	21.35	6.49	6.08	6.05	6
59.45	58.53	21.27	6.47	6.06	6.04	6
58.89	58.00	21.20	6.46	6.05	6.02	6
58.33	57.47	21.12	6.44	6.03	6.01	6
57.76	56.94	21.05	6.43	6.01	5.99	6
57.20	56.41	20.97	6.42	5.99	5.98	6
56.64	55.88	20.90	6.40	5.97	5.97	6
56.08	55.35	20.82	6.39	5.95	5.95	6
56.08	55.35	20.82	4.51	4.15	4.15	5
54.82	54.17	20.59	4.44	4.09	4.09	5
53.56	53.00	20.36	4.38	4.02	4.02	5
52.32	51.84	20.12	4.32	3.96	3.96	5
51.10	50.70	19.89	4.25	3.89	3.89	5
49.88	49.57	19.66	4.19	3.83	3.83	5
48.69	48.46	19.43	4.13	3.77	3.77	5
48.69	48.46	19.43	1.93	1.91	1.91	4
46.69	46.48	18.75	1.92	1.89	1.89	4
44.70	44.50	18.06	1.91	1.88	1.88	4
42.72	42.54	17.38	1.89	1.87	1.86	4
40.75	40.59	16.70	1.88	1.85	1.84	4
38.79	38.65	16.01	1.86	1.83	1.82	4
36.85	36.72	15.33	1.84	1.82	1.80	4
34.91	34.80	14.65	1.82	1.80	1.78	4
33.00	32.90	13.97	1.80	1.78	1.76	4
31.09	31.01	13.28	1.78	1.76	1.73	4
31.09	31.01	13.28	1.47	1.46	1.45	3
29.70	29.62	12.72	1.46	1.45	1.44	3
28.32	28.25	12.16	1.45	1.44	1.43	3
26.94	26.87	11.59	1.44	1.43	1.42	3
25.57	25.51	11.03	1.43	1.42	1.41	3
24.21	24.15	10.47	1.42	1.41	1.40	3
22.84	22.79	9.90	1.41	1.40	1.39	3
21.49	21.44	9.34	1.40	1.39	1.38	3
20.14	20.10	8.78	1.39	1.38	1.37	3
18.80	18.76	8.21	1.38	1.37	1.36	3
18.80	18.76	8.21	1.34	1.33	1.32	2
16.88	16.85	7.39	1.33	1.32	1.31	2
14.97	14.94	6.57	1.32	1.31	1.30	2
13.07	13.05	5.75	1.31	1.30	1.29	2
11.18	11.16	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2

1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.60	308.35	132.14	176.21	163.70	12.52	6
59.07	346.41	138.26	208.15	197.13	11.01	6
58.53	384.38	144.37	240.00	230.48	9.52	6
58.00	422.26	150.47	271.79	263.74	8.05	6
57.47	460.05	156.54	303.51	296.92	6.59	6
56.94	497.76	162.61	335.15	330.00	5.15	6
56.41	535.38	168.66	366.72	363.01	3.72	6
55.88	572.92	174.69	398.23	395.92	2.31	6
55.35	610.37	180.71	429.66	428.75	.91	6
55.35	610.37	180.71	429.66	428.75	.91	5
54.17	710.16	207.37	502.79	502.79	.00	5
53.00	809.02	233.12	575.90	575.90	.00	5
51.84	906.96	258.87	648.09	648.09	.00	5
50.70	1003.97	284.62	719.35	719.35	.00	5
49.57	1100.06	310.37	789.69	789.69	.00	5
48.46	1195.22	336.12	859.11	859.11	.00	5
48.46	1195.22	336.12	859.11	859.11	.00	4
46.48	1394.69	409.21	985.48	982.71	2.77	4
44.50	1593.66	487.84	1105.83	1105.83	.00	4
42.54	1792.00	550.97	1241.03	1228.30	12.73	4
40.59	1989.64	609.68	1379.95	1350.08	29.87	4
38.65	2186.57	669.01	1517.56	1471.16	46.41	4
36.72	2382.79	729.85	1652.94	1591.52	61.42	4
34.80	2578.27	792.86	1785.41	1711.14	74.27	4
32.90	2772.98	859.15	1913.84	1829.99	83.84	4
31.01	2966.87	930.76	2036.11	1948.03	88.09	4
31.01	2966.87	930.76	2036.11	1948.03	88.09	3
29.62	3115.10	988.53	2126.57	2034.39	92.17	3
28.25	3262.95	1053.83	2209.13	2120.39	88.74	3
26.87	3410.43	1119.31	2291.13	2206.01	85.12	3
25.51	3557.55	1183.09	2374.47	2291.27	83.20	3
24.15	3704.32	1245.35	2458.96	2376.17	82.79	3
22.79	3850.73	1306.29	2544.45	2460.73	83.71	3
21.44	3996.81	1366.05	2630.76	2544.95	85.81	3
20.10	4142.55	1424.80	2717.75	2628.84	88.92	3
18.76	4287.97	1482.70	2805.27	2712.39	92.88	3
18.76	4287.97	1482.70	2805.27	2712.39	92.88	2
16.85	4493.35	1560.41	2932.94	2831.67	101.27	2
14.94	4698.24	1638.86	3059.38	2950.47	108.91	2
13.05	4902.65	1718.10	3184.55	3068.78	115.77	2
11.16	5106.57	1798.41	3308.17	3186.60	121.56	2
9.28	5310.00	1880.11	3429.88	3303.93	125.95	2
7.41	5512.91	1963.63	3549.28	3420.74	128.54	2
5.54	5715.31	2072.04	3643.27	3537.04	106.23	2
3.69	5917.19	2196.60	3720.59	3652.83	67.76	2
1.84	6118.57	2317.89	3800.67	3768.10	32.57	2
.00	6319.45	2436.29	3883.16	3882.89	.27	2

Time = 2880. Degree of Consolidation = 81.%

Total Settlement = .982

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 2880. = .982

Settlement caused by Secondary Compression at time 2880. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.93	47.71	41.47	6.24	1
1.30	154.71	62.57	92.14	82.38	9.76	1
.65	231.58	95.41	136.17	123.09	13.08	1
.00	308.35	132.14	176.21	163.70	12.52	1

Time = 2880. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 2880. = .077

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .24

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.59	21.42	6.50	6.10	6.06	6
60.02	59.06	21.35	6.49	6.08	6.05	6
59.45	58.52	21.27	6.47	6.06	6.04	6
58.89	57.99	21.20	6.46	6.05	6.02	6
58.33	57.46	21.12	6.44	6.03	6.01	6
57.76	56.93	21.05	6.43	6.01	5.99	6
57.20	56.40	20.97	6.42	5.99	5.98	6
56.64	55.87	20.90	6.40	5.97	5.97	6
56.08	55.34	20.82	6.39	5.95	5.95	6
56.08	55.34	20.82	4.51	4.15	4.15	5
54.82	54.16	20.59	4.44	4.09	4.09	5

53.56	52.99	20.36	4.38	4.02	4.02	5
52.32	51.83	20.12	4.32	3.96	3.96	5
51.10	50.69	19.89	4.25	3.89	3.89	5
49.88	49.56	19.66	4.19	3.83	3.83	5
48.69	48.45	19.43	4.13	3.77	3.77	5
48.69	48.45	19.43	1.93	1.91	1.91	4
46.69	46.47	18.75	1.92	1.89	1.89	4
44.70	44.49	18.06	1.91	1.88	1.88	4
42.72	42.53	17.38	1.89	1.87	1.86	4
40.75	40.58	16.70	1.88	1.85	1.84	4
38.79	38.64	16.01	1.86	1.83	1.82	4
36.85	36.71	15.33	1.84	1.81	1.80	4
34.91	34.79	14.65	1.82	1.80	1.78	4
33.00	32.89	13.97	1.80	1.78	1.76	4
31.09	31.00	13.28	1.78	1.76	1.73	4
31.09	31.00	13.28	1.47	1.46	1.45	3
29.70	29.62	12.72	1.46	1.45	1.44	3
28.32	28.24	12.16	1.45	1.44	1.43	3
26.94	26.87	11.59	1.44	1.43	1.42	3
25.57	25.50	11.03	1.43	1.42	1.41	3
24.21	24.14	10.47	1.42	1.41	1.40	3
22.84	22.79	9.90	1.41	1.40	1.39	3
21.49	21.44	9.34	1.40	1.39	1.38	3
20.14	20.09	8.78	1.39	1.38	1.37	3
18.80	18.76	8.21	1.38	1.37	1.36	3
18.80	18.76	8.21	1.34	1.33	1.32	2
16.88	16.84	7.39	1.33	1.32	1.31	2
14.97	14.94	6.57	1.32	1.31	1.30	2
13.07	13.05	5.75	1.31	1.30	1.29	2
11.18	11.16	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.59	308.35	132.14	176.21	163.70	12.52	6
59.06	346.41	138.26	208.14	197.13	11.01	6
58.52	384.38	144.37	240.00	230.48	9.52	6
57.99	422.26	150.47	271.79	263.74	8.05	6
57.46	460.05	156.55	303.50	296.92	6.59	6
56.93	497.76	162.61	335.15	330.00	5.14	6
56.40	535.38	168.66	366.72	363.00	3.71	6
55.87	572.92	174.70	398.22	395.92	2.30	6
55.34	610.37	180.72	429.65	428.75	.90	6
55.34	610.37	180.72	429.65	428.75	.90	5
54.16	710.16	207.37	502.79	502.79	.00	5
52.99	809.02	233.12	575.90	575.90	.00	5
51.83	906.96	258.87	648.09	648.09	.00	5
50.69	1003.97	284.62	719.35	719.35	.00	5
49.56	1100.06	310.37	789.69	789.69	.00	5
48.45	1195.22	336.12	859.10	859.11	.00	5
48.45	1195.22	336.12	859.10	859.11	.00	4
46.47	1394.69	409.21	985.48	982.71	2.77	4
44.49	1593.66	487.84	1105.83	1105.83	.00	4
42.53	1791.99	551.86	1240.14	1228.30	11.84	4
40.58	1989.62	611.54	1378.08	1350.06	28.01	4
38.64	2186.52	671.92	1514.60	1471.11	43.49	4

36.71	2382.70	733.45	1649.25	1591.43	57.82	4
34.79	2578.14	797.15	1780.98	1711.01	69.98	4
32.89	2772.79	864.13	1908.66	1829.80	78.86	4
31.00	2966.62	935.97	2030.66	1947.77	82.88	4
31.00	2966.62	935.97	2030.66	1947.77	82.88	3
29.62	3114.81	994.09	2120.73	2034.11	86.62	3
28.24	3262.63	1060.15	2202.48	2120.06	82.41	3
26.87	3410.08	1125.42	2284.66	2205.65	79.01	3
25.50	3557.16	1189.01	2368.15	2290.88	77.28	3
24.14	3703.89	1251.10	2452.79	2375.75	77.04	3
22.79	3850.28	1311.87	2538.41	2460.28	78.13	3
21.44	3996.32	1371.49	2624.84	2544.46	80.37	3
20.09	4142.04	1430.11	2711.93	2628.32	83.61	3
18.76	4287.43	1487.85	2799.57	2711.85	87.72	3
18.76	4287.43	1487.85	2799.57	2711.85	87.73	2
16.84	4492.77	1565.30	2927.47	2831.09	96.38	2
14.94	4697.64	1643.28	3054.36	2949.86	104.50	2
13.05	4902.02	1722.04	3179.98	3068.15	111.83	2
11.16	5105.92	1801.85	3304.06	3185.95	118.12	2
9.28	5309.32	1883.06	3426.26	3303.25	123.01	2
7.41	5512.22	1966.06	3546.16	3420.05	126.11	2
5.54	5714.60	2074.79	3639.81	3536.34	103.48	2
3.69	5916.48	2198.39	3718.08	3652.11	65.97	2
1.84	6117.85	2318.77	3799.07	3767.39	31.69	2
.00	6318.73	2436.30	3882.44	3882.17	.26	2

Time = 3240. Degree of Consolidation = 82.%

Total Settlement = .993

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 3240. = .994

Settlement caused by Secondary Compression at time 3240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.70	2.62	1.36
2.03	1.96	1.02
1.35	1.30	.68
.68	.65	.34
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
2.62	.00	.00
1.96	77.63	29.93
1.30	154.71	62.57
.65	231.58	95.41
.00	308.35	132.14

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
47.71	41.47	6.24	1
92.14	82.38	9.76	1
136.17	123.09	13.08	1
176.21	163.70	12.52	1

Time = 3240. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 3240. = .077

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .23

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.58	21.42	6.50	6.10	6.06	6
60.02	59.04	21.35	6.49	6.08	6.05	6
59.45	58.51	21.27	6.47	6.06	6.04	6
58.89	57.98	21.20	6.46	6.05	6.02	6
58.33	57.44	21.12	6.44	6.03	6.01	6
57.76	56.91	21.05	6.43	6.01	5.99	6
57.20	56.39	20.97	6.42	5.99	5.98	6
56.64	55.86	20.90	6.40	5.97	5.97	6
56.08	55.33	20.82	6.39	5.95	5.95	6
56.08	55.33	20.82	4.51	4.15	4.15	5
54.82	54.15	20.59	4.44	4.09	4.09	5
53.56	52.97	20.36	4.38	4.02	4.02	5
52.32	51.82	20.12	4.32	3.96	3.96	5
51.10	50.67	19.89	4.25	3.89	3.89	5
49.88	49.55	19.66	4.19	3.83	3.83	5
48.69	48.44	19.43	4.13	3.77	3.77	5
48.69	48.44	19.43	1.93	1.91	1.91	4
46.69	46.45	18.75	1.92	1.89	1.89	4
44.70	44.48	18.06	1.91	1.88	1.88	4
42.72	42.52	17.38	1.89	1.87	1.86	4
40.75	40.57	16.70	1.88	1.85	1.84	4
38.79	38.63	16.01	1.86	1.83	1.82	4
36.85	36.70	15.33	1.84	1.81	1.80	4
34.91	34.78	14.65	1.82	1.80	1.78	4
33.00	32.88	13.97	1.80	1.78	1.76	4
31.09	30.99	13.28	1.78	1.76	1.73	4
31.09	30.99	13.28	1.47	1.46	1.45	3
29.70	29.61	12.72	1.46	1.45	1.44	3
28.32	28.23	12.16	1.45	1.44	1.43	3
26.94	26.86	11.59	1.44	1.43	1.42	3
25.57	25.50	11.03	1.43	1.42	1.41	3
24.21	24.14	10.47	1.42	1.41	1.40	3
22.84	22.78	9.90	1.41	1.40	1.39	3
21.49	21.43	9.34	1.40	1.39	1.38	3
20.14	20.09	8.78	1.39	1.38	1.37	3
18.80	18.75	8.21	1.38	1.37	1.36	3
18.80	18.75	8.21	1.34	1.33	1.32	2
16.88	16.84	7.39	1.33	1.32	1.31	2
14.97	14.94	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2

11.18	11.16	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.58	308.35	132.14	176.21	163.70	12.52	6
59.04	346.41	138.26	208.14	197.13	11.01	6
58.51	384.38	144.37	240.00	230.48	9.52	6
57.98	422.26	150.47	271.79	263.74	8.05	6
57.44	460.05	156.55	303.50	296.92	6.59	6
56.91	497.76	162.61	335.14	330.00	5.14	6
56.39	535.38	168.66	366.72	363.00	3.71	6
55.86	572.92	174.70	398.22	395.92	2.30	6
55.33	610.37	180.72	429.65	428.75	.90	6
55.33	610.37	180.72	429.65	428.75	.90	5
54.15	710.16	207.37	502.79	502.79	.00	5
52.97	809.02	233.12	575.90	575.90	.00	5
51.82	906.96	258.87	648.09	648.09	.00	5
50.67	1003.97	284.62	719.35	719.35	.00	5
49.55	1100.06	310.37	789.69	789.69	.00	5
48.44	1195.22	336.12	859.10	859.11	.00	5
48.44	1195.22	336.12	859.10	859.11	.00	4
46.45	1394.69	409.21	985.47	982.71	2.77	4
44.48	1593.66	487.84	1105.83	1105.83	.00	4
42.52	1791.99	552.52	1239.47	1228.29	11.17	4
40.57	1989.60	612.93	1376.67	1350.05	26.62	4
38.63	2186.49	674.11	1512.37	1471.07	41.30	4
36.70	2382.63	736.53	1646.11	1591.36	54.74	4
34.78	2578.03	800.82	1777.21	1710.90	66.31	4
32.88	2772.64	868.30	1904.34	1829.65	74.69	4
30.99	2966.41	940.80	2025.61	1947.56	78.04	4
30.99	2966.41	940.80	2025.61	1947.56	78.04	3
29.61	3114.57	999.49	2115.09	2033.86	81.22	3
28.23	3262.35	1066.44	2195.91	2119.79	76.12	3
26.86	3409.77	1131.63	2278.14	2205.34	72.80	3
25.50	3556.81	1195.15	2361.66	2290.53	71.13	3
24.14	3703.51	1257.20	2446.31	2375.37	70.94	3
22.78	3849.86	1317.94	2531.93	2459.86	72.06	3
21.43	3995.87	1377.53	2618.34	2544.01	74.32	3
20.09	4141.55	1436.15	2705.40	2627.84	77.56	3
18.75	4286.91	1493.66	2793.25	2711.33	81.91	3
18.75	4286.91	1493.66	2793.25	2711.33	81.91	2
16.84	4492.22	1570.59	2921.63	2830.54	91.08	2
14.94	4697.05	1648.06	3049.00	2949.28	99.71	2
13.04	4901.41	1726.30	3175.11	3067.54	107.57	2
11.16	5105.29	1805.58	3299.70	3185.32	114.39	2
9.28	5308.67	1886.24	3422.42	3302.60	119.82	2
7.41	5511.55	1968.68	3542.87	3419.38	123.49	2
5.54	5713.92	2077.76	3636.16	3535.65	100.51	2
3.69	5915.78	2200.33	3715.45	3651.42	64.03	2
1.84	6117.14	2319.72	3797.42	3766.68	30.74	2
.00	6318.03	2436.30	3881.72	3881.47	.25	2

Time = 3650. Degree of Consolidation = 83.%

Total Settlement = 1.005

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 3650. = 1.005

Settlement caused by Secondary Compression at time 3650. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.93	47.71	41.47	6.24	1
1.30	154.71	62.57	92.14	82.38	9.76	1
.65	231.58	95.41	136.17	123.09	13.08	1
.00	308.35	132.14	176.21	163.70	12.52	1

Time = 3650. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 3650. = .077

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .22

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.56	21.42	6.50	6.10	6.06	6
60.02	59.03	21.35	6.49	6.08	6.05	6
59.45	58.49	21.27	6.47	6.06	6.04	6
58.89	57.96	21.20	6.46	6.05	6.02	6
58.33	57.43	21.12	6.44	6.03	6.01	6
57.76	56.90	21.05	6.43	6.01	5.99	6

57.20	56.37	20.97	6.42	5.99	5.98	6
56.64	55.84	20.90	6.40	5.97	5.97	6
56.08	55.31	20.82	6.39	5.95	5.95	6
56.08	55.31	20.82	4.51	4.15	4.15	5
54.82	54.13	20.59	4.44	4.09	4.09	5
53.56	52.96	20.36	4.38	4.02	4.02	5
52.32	51.80	20.12	4.32	3.96	3.96	5
51.10	50.66	19.89	4.25	3.89	3.89	5
49.88	49.53	19.66	4.19	3.83	3.83	5
48.69	48.42	19.43	4.13	3.77	3.77	5
48.69	48.42	19.43	1.93	1.91	1.91	4
46.69	46.44	18.75	1.92	1.89	1.89	4
44.70	44.46	18.06	1.91	1.88	1.88	4
42.72	42.50	17.38	1.89	1.87	1.86	4
40.75	40.55	16.70	1.88	1.85	1.84	4
38.79	38.61	16.01	1.86	1.83	1.82	4
36.85	36.68	15.33	1.84	1.81	1.80	4
34.91	34.77	14.65	1.82	1.79	1.78	4
33.00	32.87	13.97	1.80	1.77	1.76	4
31.09	30.98	13.28	1.78	1.75	1.73	4
31.09	30.98	13.28	1.47	1.46	1.45	3
29.70	29.60	12.72	1.46	1.45	1.44	3
28.32	28.22	12.16	1.45	1.44	1.43	3
26.94	26.85	11.59	1.44	1.43	1.42	3
25.57	25.49	11.03	1.43	1.42	1.41	3
24.21	24.13	10.47	1.42	1.41	1.40	3
22.84	22.77	9.90	1.41	1.40	1.39	3
21.49	21.43	9.34	1.40	1.39	1.38	3
20.14	20.08	8.78	1.39	1.38	1.37	3
18.80	18.75	8.21	1.38	1.37	1.36	3
18.80	18.75	8.21	1.34	1.33	1.32	2
16.88	16.84	7.39	1.33	1.32	1.31	2
14.97	14.94	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.56	308.35	132.14	176.21	163.70	12.52	6
59.03	346.41	138.26	208.14	197.13	11.01	6
58.49	384.38	144.37	240.00	230.48	9.52	6
57.96	422.26	150.47	271.79	263.74	8.05	6
57.43	460.05	156.55	303.50	296.92	6.59	6
56.90	497.76	162.61	335.14	330.00	5.14	6
56.37	535.38	168.66	366.72	363.00	3.71	6
55.84	572.92	174.70	398.22	395.92	2.30	6
55.31	610.37	180.72	429.65	428.75	.90	6
55.31	610.37	180.72	429.65	428.75	.90	5
54.13	710.16	207.37	502.79	502.79	.00	5
52.96	809.02	233.12	575.90	575.90	.00	5
51.80	906.96	258.87	648.09	648.09	.00	5
50.66	1003.97	284.62	719.35	719.35	.00	5
49.53	1100.06	310.37	789.69	789.69	.00	5
48.42	1195.22	336.12	859.10	859.11	.00	5
48.42	1195.22	336.12	859.10	859.11	.00	4

46.44	1394.69	409.21	985.47	982.71	2.77	4
44.46	1593.66	487.84	1105.83	1105.83	.00	4
42.50	1791.98	553.41	1238.58	1228.29	10.29	4
40.55	1989.58	614.79	1374.79	1350.03	24.77	4
38.61	2186.44	677.03	1509.41	1471.02	38.38	4
36.68	2382.54	740.65	1641.90	1591.27	50.62	4
34.77	2577.88	806.33	1771.55	1710.75	60.80	4
32.87	2772.42	875.09	1897.32	1829.43	67.90	4
30.98	2966.10	949.28	2016.82	1947.25	69.57	4
30.98	2966.10	949.28	2016.82	1947.25	69.57	3
29.60	3114.21	1009.32	2104.89	2033.50	71.39	3
28.22	3261.93	1076.36	2185.58	2119.37	66.21	3
26.85	3409.29	1141.54	2267.75	2204.86	62.89	3
25.49	3556.28	1205.06	2351.22	2290.00	61.23	3
24.13	3702.92	1267.10	2435.83	2374.78	61.05	3
22.77	3849.22	1327.83	2521.38	2459.22	62.17	3
21.43	3995.17	1387.43	2607.74	2543.31	64.43	3
20.08	4140.80	1446.05	2694.75	2627.08	67.67	3
18.75	4286.10	1503.29	2782.80	2710.52	72.28	3
18.75	4286.10	1503.29	2782.80	2710.52	72.28	2
16.84	4491.35	1579.37	2911.98	2829.68	82.30	2
14.94	4696.14	1655.98	3040.15	2948.36	91.79	2
13.04	4900.45	1733.35	3167.10	3066.57	100.52	2
11.15	5104.28	1811.75	3292.52	3184.31	108.22	2
9.28	5307.63	1891.51	3416.12	3301.56	114.56	2
7.40	5510.48	1973.01	3537.47	3418.31	119.16	2
5.54	5712.82	2082.66	3630.16	3534.56	95.60	2
3.69	5914.67	2203.52	3711.15	3650.30	60.84	2
1.84	6116.02	2321.29	3794.74	3765.56	29.17	2
.00	6316.90	2436.32	3880.59	3880.34	.24	2

Time = 4320. Degree of Consolidation = 84.%

Total Settlement = 1.023

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 4320. = 1.023

Settlement caused by Secondary Compression at time 4320. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.70	2.62	1.36
2.03	1.96	1.02
1.35	1.30	.68
.68	.65	.34
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
2.62	.00	.00
1.96	77.63	29.93

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
47.71	41.47	6.24	1

1.30	154.71	62.57	92.14	82.38	9.76	1
.65	231.58	95.41	136.17	123.09	13.08	1
.00	308.35	132.14	176.21	163.70	12.52	1

Time = 4320. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 4320. = .077

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .20

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.54	21.42	6.50	6.10	6.06	6
60.02	59.01	21.35	6.49	6.08	6.05	6
59.45	58.47	21.27	6.47	6.06	6.04	6
58.89	57.94	21.20	6.46	6.05	6.02	6
58.33	57.41	21.12	6.44	6.03	6.01	6
57.76	56.88	21.05	6.43	6.01	5.99	6
57.20	56.35	20.97	6.42	5.99	5.98	6
56.64	55.82	20.90	6.40	5.97	5.97	6
56.08	55.30	20.82	6.39	5.95	5.95	6
56.08	55.30	20.82	4.51	4.15	4.15	5
54.82	54.11	20.59	4.44	4.09	4.09	5
53.56	52.94	20.36	4.38	4.02	4.02	5
52.32	51.78	20.12	4.32	3.96	3.96	5
51.10	50.64	19.89	4.25	3.89	3.89	5
49.88	49.51	19.66	4.19	3.83	3.83	5
48.69	48.40	19.43	4.13	3.77	3.77	5
48.69	48.40	19.43	1.93	1.91	1.91	4
46.69	46.42	18.75	1.92	1.89	1.89	4
44.70	44.44	18.06	1.91	1.88	1.88	4
42.72	42.48	17.38	1.89	1.86	1.86	4
40.75	40.53	16.70	1.88	1.85	1.84	4
38.79	38.59	16.01	1.86	1.83	1.82	4
36.85	36.67	15.33	1.84	1.81	1.80	4
34.91	34.75	14.65	1.82	1.79	1.78	4
33.00	32.85	13.97	1.80	1.77	1.76	4
31.09	30.97	13.28	1.78	1.75	1.73	4
31.09	30.97	13.28	1.47	1.46	1.45	3
29.70	29.58	12.72	1.46	1.45	1.44	3
28.32	28.21	12.16	1.45	1.44	1.43	3
26.94	26.84	11.59	1.44	1.43	1.42	3
25.57	25.48	11.03	1.43	1.42	1.41	3
24.21	24.12	10.47	1.42	1.41	1.40	3
22.84	22.77	9.90	1.41	1.40	1.39	3
21.49	21.42	9.34	1.40	1.39	1.38	3
20.14	20.08	8.78	1.39	1.38	1.37	3

18.80	18.74	8.21	1.38	1.37	1.36	3
18.80	18.74	8.21	1.34	1.33	1.32	2
16.88	16.83	7.39	1.33	1.32	1.31	2
14.97	14.93	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.54	308.35	132.14	176.21	163.70	12.52	6
59.01	346.41	138.26	208.14	197.13	11.01	6
58.47	384.38	144.37	240.00	230.48	9.52	6
57.94	422.26	150.47	271.79	263.74	8.05	6
57.41	460.05	156.55	303.50	296.92	6.59	6
56.88	497.76	162.61	335.14	330.00	5.14	6
56.35	535.38	168.66	366.72	363.00	3.71	6
55.82	572.92	174.70	398.22	395.92	2.30	6
55.30	610.37	180.72	429.65	428.75	.90	6
55.30	610.37	180.72	429.65	428.75	.90	5
54.11	710.16	207.37	502.79	502.79	.00	5
52.94	809.02	233.12	575.90	575.90	.00	5
51.78	906.96	258.87	648.09	648.09	.00	5
50.64	1003.97	284.62	719.35	719.35	.00	5
49.51	1100.06	310.37	789.69	789.69	.00	5
48.40	1195.22	336.12	859.10	859.11	.00	5
48.40	1195.22	336.12	859.10	859.11	.00	4
46.42	1394.68	409.21	985.47	982.71	2.77	4
44.44	1593.66	487.84	1105.83	1105.83	.00	4
42.48	1791.98	554.23	1237.75	1228.29	9.46	4
40.53	1989.56	616.51	1373.05	1350.01	23.04	4
38.59	2186.39	679.75	1506.64	1470.98	35.66	4
36.67	2382.46	744.49	1637.97	1591.19	46.78	4
34.75	2577.74	811.48	1766.26	1710.61	55.65	4
32.85	2772.21	881.84	1890.37	1829.22	61.15	4
30.97	2965.80	958.12	2007.68	1946.95	60.73	4
30.97	2965.80	958.12	2007.68	1946.95	60.73	3
29.58	3113.85	1019.98	2093.86	2033.14	60.72	3
28.21	3261.51	1087.02	2174.49	2118.95	55.54	3
26.84	3408.81	1152.20	2256.60	2204.38	52.22	3
25.48	3555.74	1215.72	2340.02	2289.46	50.56	3
24.12	3702.32	1277.76	2424.56	2374.18	50.38	3
22.77	3848.56	1338.50	2510.06	2458.56	51.50	3
21.42	3994.45	1398.10	2596.36	2542.59	53.76	3
20.08	4140.02	1456.47	2683.55	2626.30	57.25	3
18.74	4285.26	1513.30	2771.96	2709.68	62.28	3
18.74	4285.26	1513.30	2771.96	2709.68	62.28	2
16.83	4490.46	1588.49	2901.97	2828.78	73.19	2
14.93	4695.19	1664.20	3030.99	2947.41	83.57	2
13.04	4899.45	1740.67	3158.78	3065.58	93.20	2
11.15	5103.24	1818.15	3285.09	3183.27	101.82	2
9.27	5306.55	1896.96	3409.59	3300.48	109.10	2
7.40	5509.37	1977.49	3531.89	3417.20	114.68	2
5.54	5711.69	2087.73	3623.96	3533.43	90.53	2
3.69	5913.52	2206.83	3706.69	3649.16	57.54	2
1.84	6114.87	2322.91	3791.96	3764.41	27.55	2

.00	6315.74	2436.33	3879.41	3879.18	.23	2

Time = 5040. Degree of Consolidation = 86.%

Total Settlement = 1.041

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 5040. = 1.041

Settlement caused by Secondary Compression at time 5040. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.93	47.71	41.47	6.24	1
1.30	154.71	62.57	92.14	82.38	9.76	1
.65	231.58	95.41	136.17	123.09	13.08	1
.00	308.35	132.14	176.21	163.70	12.52	1

Time = 5040. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 5040. = .077

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .18

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.53	21.42	6.50	6.10	6.06	6

60.02	59.00	21.35	6.49	6.08	6.05	6
59.45	58.46	21.27	6.47	6.06	6.04	6
58.89	57.93	21.20	6.46	6.05	6.02	6
58.33	57.40	21.12	6.44	6.03	6.01	6
57.76	56.87	21.05	6.43	6.01	5.99	6
57.20	56.34	20.97	6.42	5.99	5.98	6
56.64	55.81	20.90	6.40	5.97	5.97	6
56.08	55.28	20.82	6.39	5.95	5.95	6
56.08	55.28	20.82	4.51	4.15	4.15	5
54.82	54.10	20.59	4.44	4.09	4.09	5
53.56	52.93	20.36	4.38	4.02	4.02	5
52.32	51.77	20.12	4.32	3.96	3.96	5
51.10	50.63	19.89	4.25	3.89	3.89	5
49.88	49.50	19.66	4.19	3.83	3.83	5
48.69	48.39	19.43	4.13	3.77	3.77	5
48.69	48.39	19.43	1.93	1.91	1.91	4
46.69	46.41	18.75	1.92	1.89	1.89	4
44.70	44.43	18.06	1.91	1.88	1.88	4
42.72	42.47	17.38	1.89	1.86	1.86	4
40.75	40.52	16.70	1.88	1.85	1.84	4
38.79	38.58	16.01	1.86	1.83	1.82	4
36.85	36.66	15.33	1.84	1.81	1.80	4
34.91	34.74	14.65	1.82	1.79	1.78	4
33.00	32.84	13.97	1.80	1.77	1.76	4
31.09	30.96	13.28	1.78	1.75	1.73	4
31.09	30.96	13.28	1.47	1.46	1.45	3
29.70	29.58	12.72	1.46	1.45	1.44	3
28.32	28.20	12.16	1.45	1.44	1.43	3
26.94	26.83	11.59	1.44	1.42	1.42	3
25.57	25.47	11.03	1.43	1.41	1.41	3
24.21	24.11	10.47	1.42	1.40	1.40	3
22.84	22.76	9.90	1.41	1.39	1.39	3
21.49	21.42	9.34	1.40	1.39	1.38	3
20.14	20.07	8.78	1.39	1.38	1.37	3
18.80	18.74	8.21	1.38	1.37	1.36	3
18.80	18.74	8.21	1.34	1.33	1.32	2
16.88	16.83	7.39	1.33	1.32	1.31	2
14.97	14.93	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.53	308.35	132.14	176.21	163.70	12.52	6
59.00	346.41	138.26	208.14	197.13	11.01	6
58.46	384.38	144.37	240.00	230.48	9.52	6
57.93	422.26	150.47	271.79	263.74	8.05	6
57.40	460.05	156.55	303.50	296.92	6.59	6
56.87	497.76	162.61	335.14	330.00	5.14	6
56.34	535.38	168.66	366.72	363.00	3.71	6
55.81	572.92	174.70	398.22	395.92	2.30	6
55.28	610.37	180.72	429.65	428.75	.90	6
55.28	610.37	180.72	429.65	428.75	.90	5
54.10	710.16	207.37	502.79	502.79	.00	5
52.93	809.02	233.12	575.90	575.90	.00	5

51.77	906.96	258.87	648.09	648.09	.00	5
50.63	1003.97	284.62	719.35	719.35	.00	5
49.50	1100.06	310.37	789.69	789.69	.00	5
48.39	1195.22	336.12	859.10	859.11	.00	5
48.39	1195.22	336.12	859.10	859.11	.00	4
46.41	1394.68	409.21	985.47	982.71	2.77	4
44.43	1593.67	487.84	1105.83	1105.83	.00	4
42.47	1791.98	554.70	1237.28	1228.28	9.00	4
40.52	1989.55	617.48	1372.07	1350.00	22.07	4
38.58	2186.37	681.29	1505.08	1470.95	34.13	4
36.66	2382.41	746.66	1635.75	1591.14	44.61	4
34.74	2577.67	814.40	1763.26	1710.53	52.73	4
32.84	2772.09	885.68	1886.41	1829.10	57.31	4
30.96	2965.63	963.17	2002.46	1946.78	55.68	4
30.96	2965.63	963.17	2002.46	1946.78	55.68	3
29.58	3113.64	1026.32	2087.32	2032.93	54.39	3
28.20	3261.27	1093.47	2167.81	2118.71	49.10	3
26.83	3408.53	1158.65	2249.88	2204.11	45.78	3
25.47	3555.43	1222.17	2333.26	2289.14	44.12	3
24.11	3701.97	1284.21	2417.77	2373.83	43.94	3
22.76	3848.17	1344.94	2503.23	2458.17	45.06	3
21.42	3994.03	1404.54	2589.49	2542.17	47.32	3
20.07	4139.56	1462.47	2677.09	2625.84	51.25	3
18.74	4284.77	1518.88	2765.89	2709.19	56.70	3
18.74	4284.77	1518.88	2765.89	2709.19	56.70	2
16.83	4489.93	1593.57	2896.37	2828.26	68.11	2
14.93	4694.64	1668.78	3025.85	2946.86	78.99	2
13.04	4898.87	1744.74	3154.13	3065.00	89.13	2
11.15	5102.64	1821.71	3280.93	3182.67	98.26	2
9.27	5305.93	1900.00	3405.93	3299.86	106.07	2
7.40	5508.73	1979.98	3528.75	3416.57	112.19	2
5.54	5711.04	2090.55	3620.49	3532.78	87.72	2
3.69	5912.86	2208.66	3704.20	3648.50	55.70	2
1.84	6114.20	2323.81	3790.39	3763.74	26.65	2
.00	6315.07	2436.34	3878.73	3878.51	.22	2

Time = 5475. Degree of Consolidation = 86.%

Total Settlement = 1.052

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 5475. = 1.052

Settlement caused by Secondary Compression at time 5475. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

XI	Total Stresses	Effective Stresses	Total Pore Pressures	Static Pore Pressures	Excess Pore Pressures	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.93	47.71	41.47	6.24	1
1.30	154.71	62.57	92.14	82.38	9.76	1
.65	231.58	95.41	136.17	123.09	13.08	1
.00	308.35	132.14	176.21	163.70	12.52	1

Time = 5475. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 5475. = .077

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .17

**********Current Conditions in Compressible Foundation**********

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.51	21.42	6.50	6.10	6.06	6
60.02	58.97	21.35	6.49	6.08	6.05	6
59.45	58.44	21.27	6.47	6.06	6.04	6
58.89	57.90	21.20	6.46	6.05	6.02	6
58.33	57.37	21.12	6.44	6.03	6.01	6
57.76	56.84	21.05	6.43	6.01	5.99	6
57.20	56.31	20.97	6.42	5.99	5.98	6
56.64	55.79	20.90	6.40	5.97	5.97	6
56.08	55.26	20.82	6.39	5.95	5.95	6
56.08	55.26	20.82	4.51	4.15	4.15	5
54.82	54.07	20.59	4.44	4.09	4.09	5
53.56	52.90	20.36	4.38	4.02	4.02	5
52.32	51.74	20.12	4.32	3.96	3.96	5
51.10	50.60	19.89	4.25	3.89	3.89	5
49.88	49.47	19.66	4.19	3.83	3.83	5
48.69	48.36	19.43	4.13	3.77	3.77	5
48.69	48.36	19.43	1.93	1.91	1.91	4
46.69	46.38	18.75	1.92	1.89	1.89	4
44.70	44.41	18.06	1.91	1.88	1.88	4
42.72	42.45	17.38	1.89	1.86	1.86	4
40.75	40.50	16.70	1.88	1.85	1.84	4
38.79	38.56	16.01	1.86	1.83	1.82	4
36.85	36.63	15.33	1.84	1.81	1.80	4
34.91	34.72	14.65	1.82	1.79	1.78	4
33.00	32.82	13.97	1.80	1.77	1.76	4
31.09	30.94	13.28	1.78	1.75	1.73	4
31.09	30.94	13.28	1.47	1.45	1.45	3
29.70	29.56	12.72	1.46	1.44	1.44	3
28.32	28.19	12.16	1.45	1.43	1.43	3
26.94	26.82	11.59	1.44	1.42	1.42	3

25.57	25.46	11.03	1.43	1.41	1.41	3
24.21	24.10	10.47	1.42	1.40	1.40	3
22.84	22.75	9.90	1.41	1.39	1.39	3
21.49	21.41	9.34	1.40	1.38	1.38	3
20.14	20.07	8.78	1.39	1.37	1.37	3
18.80	18.73	8.21	1.38	1.36	1.36	3
18.80	18.73	8.21	1.34	1.33	1.32	2
16.88	16.83	7.39	1.33	1.32	1.31	2
14.97	14.93	6.57	1.32	1.31	1.30	2
13.07	13.03	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.51	308.35	132.14	176.21	163.70	12.52	6
58.97	346.41	138.26	208.14	197.13	11.01	6
58.44	384.38	144.37	240.00	230.48	9.52	6
57.90	422.26	150.47	271.79	263.74	8.05	6
57.37	460.05	156.55	303.50	296.92	6.59	6
56.84	497.76	162.61	335.14	330.00	5.14	6
56.31	535.38	168.66	366.72	363.00	3.71	6
55.79	572.92	174.70	398.22	395.92	2.30	6
55.26	610.37	180.72	429.65	428.75	.90	6
55.26	610.37	180.72	429.65	428.75	.90	5
54.07	710.16	207.37	502.79	502.79	.00	5
52.90	809.02	233.12	575.90	575.90	.00	5
51.74	906.96	258.87	648.09	648.09	.00	5
50.60	1003.97	284.62	719.35	719.35	.00	5
49.47	1100.06	310.37	789.69	789.69	.00	5
48.36	1195.22	336.12	859.10	859.11	.00	5
48.36	1195.22	336.12	859.10	859.11	.00	4
46.38	1394.68	409.21	985.47	982.71	2.77	4
44.41	1593.67	487.84	1105.83	1105.83	.00	4
42.45	1791.97	555.78	1236.19	1228.28	7.91	4
40.50	1989.53	619.76	1369.76	1349.97	19.79	4
38.56	2186.31	684.89	1501.41	1470.89	30.52	4
36.63	2382.30	751.78	1630.52	1591.03	39.49	4
34.72	2577.48	821.30	1756.18	1710.35	45.83	4
32.82	2771.81	894.77	1877.04	1828.82	48.22	4
30.94	2965.23	975.21	1990.02	1946.38	43.64	4
30.94	2965.23	975.21	1990.02	1946.38	43.64	3
29.56	3113.16	1040.86	2072.30	2032.45	39.85	3
28.19	3260.71	1108.36	2152.35	2118.14	34.21	3
26.82	3407.88	1173.54	2234.35	2203.46	30.89	3
25.46	3554.70	1237.06	2317.64	2288.41	29.23	3
24.10	3701.16	1299.10	2402.06	2373.01	29.05	3
22.75	3847.27	1359.83	2487.44	2457.27	30.17	3
21.41	3993.05	1419.10	2573.94	2541.19	32.76	3
20.07	4138.50	1476.73	2661.76	2624.78	36.98	3
18.73	4283.63	1532.87	2750.76	2708.05	42.70	3
18.73	4283.63	1532.87	2750.76	2708.05	42.70	2
16.83	4488.71	1606.31	2882.39	2827.03	55.36	2
14.93	4693.33	1680.27	3013.07	2945.56	67.50	2
13.03	4897.50	1754.96	3142.55	3063.63	78.91	2
11.15	5101.21	1830.63	3270.58	3181.24	89.34	2

9.27	5304.45	1907.59	3396.86	3298.38	98.47	2
7.40	5507.21	1986.21	3521.00	3415.05	105.96	2
5.54	5709.49	2097.59	3611.90	3531.22	80.67	2
3.69	5911.28	2213.25	3698.03	3646.92	51.11	2
1.84	6112.61	2326.06	3786.54	3762.15	24.40	2
.00	6313.48	2436.36	3877.12	3876.92	.20	2

Time = 6480. Degree of Consolidation = 89.%

Total Settlement = 1.078

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 6480. = 1.078

Settlement caused by Secondary Compression at time 6480. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1
1.35	1.30	.68	.98	.92	.92	1
.68	.65	.34	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.93	47.71	41.47	6.24	1
1.30	154.71	62.57	92.14	82.38	9.76	1
.65	231.58	95.41	136.17	123.09	13.08	1
.00	308.35	132.14	176.21	163.70	12.52	1

Time = 6480. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 6480. = .077

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .15

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.49	21.42	6.50	6.10	6.06	6
60.02	58.95	21.35	6.49	6.08	6.05	6
59.45	58.42	21.27	6.47	6.06	6.04	6
58.89	57.88	21.20	6.46	6.05	6.02	6
58.33	57.35	21.12	6.44	6.03	6.01	6
57.76	56.82	21.05	6.43	6.01	5.99	6
57.20	56.29	20.97	6.42	5.99	5.98	6
56.64	55.77	20.90	6.40	5.97	5.97	6
56.08	55.24	20.82	6.39	5.95	5.95	6
56.08	55.24	20.82	4.51	4.15	4.15	5
54.82	54.05	20.59	4.44	4.09	4.09	5
53.56	52.88	20.36	4.38	4.02	4.02	5
52.32	51.72	20.12	4.32	3.96	3.96	5
51.10	50.58	19.89	4.25	3.89	3.89	5
49.88	49.46	19.66	4.19	3.83	3.83	5
48.69	48.34	19.43	4.13	3.77	3.77	5
48.69	48.34	19.43	1.93	1.91	1.91	4
46.69	46.36	18.75	1.92	1.89	1.89	4
44.70	44.39	18.06	1.91	1.88	1.88	4
42.72	42.43	17.38	1.89	1.86	1.86	4
40.75	40.48	16.70	1.88	1.85	1.84	4
38.79	38.54	16.01	1.86	1.83	1.82	4
36.85	36.61	15.33	1.84	1.81	1.80	4
34.91	34.70	14.65	1.82	1.79	1.78	4
33.00	32.81	13.97	1.80	1.77	1.76	4
31.09	30.92	13.28	1.78	1.74	1.73	4
31.09	30.92	13.28	1.47	1.45	1.45	3
29.70	29.55	12.72	1.46	1.44	1.44	3
28.32	28.17	12.16	1.45	1.43	1.43	3
26.94	26.81	11.59	1.44	1.42	1.42	3
25.57	25.45	11.03	1.43	1.41	1.41	3
24.21	24.09	10.47	1.42	1.40	1.40	3
22.84	22.74	9.90	1.41	1.39	1.39	3
21.49	21.40	9.34	1.40	1.38	1.38	3
20.14	20.06	8.78	1.39	1.37	1.37	3
18.80	18.73	8.21	1.38	1.36	1.36	3
18.80	18.73	8.21	1.34	1.32	1.32	2
16.88	16.82	7.39	1.33	1.32	1.31	2
14.97	14.92	6.57	1.32	1.31	1.30	2
13.07	13.03	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.49	308.35	132.14	176.21	163.70	12.52	6
58.95	346.41	138.26	208.14	197.13	11.01	6
58.42	384.38	144.37	240.00	230.48	9.52	6
57.88	422.26	150.47	271.79	263.74	8.05	6
57.35	460.05	156.55	303.50	296.92	6.59	6
56.82	497.76	162.61	335.14	330.00	5.14	6
56.29	535.38	168.66	366.72	363.00	3.71	6

55.77	572.92	174.70	398.22	395.92	2.30	6
55.24	610.37	180.72	429.65	428.75	.90	6
55.24	610.37	180.72	429.65	428.75	.90	5
54.05	710.16	207.37	502.79	502.79	.00	5
52.88	809.02	233.12	575.90	575.90	.00	5
51.72	906.96	258.87	648.09	648.09	.00	5
50.58	1003.97	284.62	719.35	719.35	.00	5
49.46	1100.06	310.37	789.69	789.69	.00	5
48.34	1195.22	336.12	859.10	859.11	.00	5
48.34	1195.22	336.12	859.10	859.11	.00	4
46.36	1394.68	409.21	985.47	982.71	2.77	4
44.39	1593.67	487.84	1105.83	1105.83	.00	4
42.43	1791.97	556.60	1235.37	1228.28	7.09	4
40.48	1989.51	621.48	1368.02	1349.95	18.07	4
38.54	2186.26	687.62	1498.65	1470.85	27.80	4
36.61	2382.22	755.65	1626.56	1590.94	35.62	4
34.70	2577.34	826.53	1750.81	1710.21	40.60	4
32.81	2771.60	901.72	1869.89	1828.61	41.27	4
30.92	2964.92	984.22	1980.70	1946.07	34.63	4
30.92	2964.92	984.22	1980.70	1946.07	34.63	3
29.55	3112.79	1052.06	2060.73	2032.09	28.65	3
28.17	3260.28	1120.12	2140.16	2117.71	22.45	3
26.81	3407.38	1185.68	2221.70	2202.96	18.74	3
25.45	3554.13	1249.20	2304.93	2287.85	17.08	3
24.09	3700.52	1311.24	2389.28	2372.38	16.90	3
22.74	3846.57	1371.62	2474.95	2456.57	18.38	3
21.40	3992.28	1430.24	2562.04	2540.42	21.62	3
20.06	4137.67	1487.25	2650.43	2623.95	26.47	3
18.73	4282.74	1542.79	2739.95	2707.17	32.78	3
18.73	4282.74	1542.79	2739.95	2707.17	32.78	2
16.82	4487.76	1615.34	2872.42	2826.09	46.33	2
14.92	4692.34	1688.40	3003.94	2944.57	59.37	2
13.03	4896.46	1762.19	3134.27	3062.59	71.68	2
11.15	5100.13	1836.94	3263.19	3180.16	83.03	2
9.27	5303.33	1912.96	3390.37	3297.26	93.10	2
7.40	5506.06	1990.60	3515.46	3413.90	101.56	2
5.54	5708.31	2102.55	3605.76	3530.05	75.71	2
3.69	5910.09	2216.48	3693.61	3645.73	47.88	2
1.84	6111.41	2327.65	3783.76	3760.95	22.81	2
.00	6312.27	2436.37	3875.90	3875.71	.19	2

Time = 7300. Degree of Consolidation = 90.%

Total Settlement = 1.097

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 7300. = 1.097

Settlement caused by Secondary Compression at time 7300. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.70	2.62	1.36	.98	.98	.98	1
2.03	1.96	1.02	.98	.93	.93	1

1.35	1.30	.68	.98	.92	1
.68	.65	.34	.98	.91	1
.00	.00	.00	.98	.91	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.62	.00	.00	.00	.00	.00	1
1.96	77.63	29.93	47.71	41.47	6.24	1
1.30	154.71	62.57	92.14	82.38	9.76	1
.65	231.58	95.41	136.17	123.09	13.08	1
.00	308.35	132.14	176.21	163.70	12.52	1

Time = 7300. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 7300. = .077

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .13

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.47	21.42	6.50	6.10	6.06	6
60.02	58.94	21.35	6.49	6.08	6.05	6
59.45	58.40	21.27	6.47	6.06	6.04	6
58.89	57.87	21.20	6.46	6.05	6.02	6
58.33	57.34	21.12	6.44	6.03	6.01	6
57.76	56.81	21.05	6.43	6.01	5.99	6
57.20	56.28	20.97	6.42	5.99	5.98	6
56.64	55.75	20.90	6.40	5.97	5.97	6
56.08	55.23	20.82	6.39	5.95	5.95	6
56.08	55.23	20.82	4.51	4.15	4.15	5
54.82	54.04	20.59	4.44	4.09	4.09	5
53.56	52.87	20.36	4.38	4.02	4.02	5
52.32	51.71	20.12	4.32	3.96	3.96	5
51.10	50.57	19.89	4.25	3.89	3.89	5
49.88	49.44	19.66	4.19	3.83	3.83	5
48.69	48.33	19.43	4.13	3.77	3.77	5
48.69	48.33	19.43	1.93	1.91	1.91	4
46.69	46.35	18.75	1.92	1.89	1.89	4
44.70	44.37	18.06	1.91	1.88	1.88	4
42.72	42.41	17.38	1.89	1.86	1.86	4
40.75	40.46	16.70	1.88	1.85	1.84	4
38.79	38.53	16.01	1.86	1.83	1.82	4
36.85	36.60	15.33	1.84	1.81	1.80	4
34.91	34.69	14.65	1.82	1.79	1.78	4
33.00	32.79	13.97	1.80	1.77	1.76	4

31.09	30.91	13.28	1.78	1.74	1.73	4
31.09	30.91	13.28	1.47	1.45	1.45	3
29.70	29.54	12.72	1.46	1.44	1.44	3
28.32	28.16	12.16	1.45	1.43	1.43	3
26.94	26.80	11.59	1.44	1.42	1.42	3
25.57	25.44	11.03	1.43	1.41	1.41	3
24.21	24.09	10.47	1.42	1.40	1.40	3
22.84	22.74	9.90	1.41	1.39	1.39	3
21.49	21.39	9.34	1.40	1.38	1.38	3
20.14	20.06	8.78	1.39	1.37	1.37	3
18.80	18.72	8.21	1.38	1.36	1.36	3
18.80	18.72	8.21	1.34	1.32	1.32	2
16.88	16.82	7.39	1.33	1.32	1.31	2
14.97	14.92	6.57	1.32	1.31	1.30	2
13.07	13.03	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.47	308.35	132.14	176.21	163.70	12.52	6
58.94	346.41	138.26	208.14	197.13	11.01	6
58.40	384.38	144.37	240.00	230.48	9.52	6
57.87	422.26	150.47	271.79	263.74	8.05	6
57.34	460.05	156.55	303.50	296.92	6.59	6
56.81	497.76	162.61	335.14	330.00	5.14	6
56.28	535.38	168.66	366.72	363.00	3.71	6
55.75	572.92	174.70	398.22	395.92	2.30	6
55.23	610.37	180.72	429.65	428.75	.90	6
55.23	610.37	180.72	429.65	428.75	.90	5
54.04	710.16	207.37	502.79	502.79	.00	5
52.87	809.02	233.12	575.90	575.90	.00	5
51.71	906.96	258.87	648.09	648.09	.00	5
50.57	1003.97	284.62	719.35	719.35	.00	5
49.44	1100.06	310.37	789.69	789.69	.00	5
48.33	1195.22	336.12	859.10	859.11	.00	5
48.33	1195.22	336.12	859.10	859.11	.00	4
46.35	1394.68	409.21	985.47	982.71	2.77	4
44.37	1593.67	487.84	1105.83	1105.83	.00	4
42.41	1791.97	557.19	1234.78	1228.27	6.51	4
40.46	1989.49	622.72	1366.77	1349.94	16.83	4
38.53	2186.23	689.58	1496.65	1470.82	25.84	4
36.60	2382.16	758.44	1623.71	1590.88	32.83	4
34.69	2577.24	830.32	1746.93	1710.11	36.82	4
32.79	2771.45	906.75	1864.70	1828.46	36.24	4
30.91	2964.70	990.44	1974.26	1945.85	28.41	4
30.91	2964.70	990.44	1974.26	1945.85	28.41	3
29.54	3112.53	1060.00	2052.53	2031.82	20.70	3
28.16	3259.97	1128.63	2131.34	2117.40	13.94	3
26.80	3407.03	1194.77	2212.25	2202.60	9.65	3
25.44	3553.72	1258.64	2295.08	2287.44	7.64	3
24.09	3700.06	1320.42	2379.64	2371.92	7.72	3
22.74	3846.06	1380.30	2465.76	2456.06	9.70	3
21.39	3991.72	1438.44	2553.29	2539.86	13.42	3
20.06	4137.07	1494.99	2642.07	2623.35	18.73	3
18.72	4282.10	1550.12	2731.98	2706.52	25.46	3

18.72	4282.10	1550.12	2731.98	2706.52	25.46	2
16.82	4487.07	1622.01	2865.07	2825.40	39.67	2
14.92	4691.61	1694.40	2997.21	2943.84	53.37	2
13.03	4895.70	1767.52	3128.18	3061.83	66.35	2
11.15	5099.33	1841.59	3257.74	3179.36	78.38	2
9.27	5302.51	1916.92	3385.59	3296.44	89.15	2
7.40	5505.22	1993.84	3511.38	3413.05	98.32	2
5.54	5707.45	2106.21	3601.24	3529.19	72.06	2
3.69	5909.22	2218.87	3690.35	3644.85	45.50	2
1.84	6110.53	2328.82	3781.71	3760.07	21.64	2
.00	6311.39	2436.38	3875.01	3874.83	.18	2

Time = 9125. Degree of Consolidation = 91.%

Total Settlement = 1.111

Settlement at End of Primary Consolidation = 1.217

Settlement caused by Primary Consolidation at time 9125. = 1.111

Settlement caused by Secondary Compression at time 9125. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.70	2.62	1.36
2.03	1.96	1.02
1.35	1.30	.68
.68	.65	.34
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
2.62	.00	.00
1.96	77.63	29.93
1.30	154.71	62.57
.65	231.58	95.41
.00	308.35	132.14

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
47.71	41.47	6.24	1
92.14	82.38	9.76	1
136.17	123.09	13.08	1
176.21	163.70	12.52	1

Time = 9125. Degree of Consolidation = 96.%

Total Settlement = .077

Settlement at End of Primary Consolidation = .079

Settlement caused by Primary Consolidation at time 9125. = .077

Settlement caused by Secondary Compression at time 9125. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .11

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou Dupont - 3ft fill with Equivalent fill height of 4.9 f

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	4.9	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.164	.570	.30000E-03	z = .06

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	5.71	6
60.02	60.02	21.35	6.49	6.49	5.70	6
59.45	59.45	21.27	6.47	6.47	5.69	6
58.89	58.89	21.20	6.46	6.46	5.67	6

58.33	58.33	21.12	6.44	6.44	5.66	6
57.76	57.76	21.05	6.43	6.43	5.64	6
57.20	57.20	20.97	6.42	6.42	5.63	6
56.64	56.64	20.90	6.40	6.40	5.62	6
56.08	56.08	20.82	6.39	6.39	5.60	6
56.08	56.08	20.82	4.51	4.51	3.86	5
54.82	54.82	20.59	4.44	4.44	3.80	5
53.56	53.56	20.36	4.38	4.38	3.73	5
52.32	52.32	20.12	4.32	4.32	3.67	5
51.10	51.10	19.89	4.25	4.25	3.61	5
49.88	49.88	19.66	4.19	4.19	3.54	5
48.69	48.69	19.43	4.13	4.13	3.48	5
48.69	48.69	19.43	1.93	1.93	1.89	4
46.69	46.69	18.75	1.92	1.92	1.87	4
44.70	44.70	18.06	1.91	1.91	1.85	4
42.72	42.72	17.38	1.89	1.89	1.83	4
40.75	40.75	16.70	1.88	1.88	1.81	4
38.79	38.79	16.01	1.86	1.86	1.79	4
36.85	36.85	15.33	1.84	1.84	1.77	4
34.91	34.91	14.65	1.82	1.82	1.74	4
33.00	33.00	13.97	1.80	1.80	1.72	4
31.09	31.09	13.28	1.78	1.78	1.70	4
31.09	31.09	13.28	1.47	1.47	1.43	3
29.70	29.70	12.72	1.46	1.46	1.42	3
28.32	28.32	12.16	1.45	1.45	1.41	3
26.94	26.94	11.59	1.44	1.44	1.40	3
25.57	25.57	11.03	1.43	1.43	1.39	3
24.21	24.21	10.47	1.42	1.42	1.38	3
22.84	22.84	9.90	1.41	1.41	1.37	3
21.49	21.49	9.34	1.40	1.40	1.36	3
20.14	20.14	8.78	1.39	1.39	1.35	3
18.80	18.80	8.21	1.38	1.38	1.34	3
18.80	18.80	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.43	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.25	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	563.64	.00	563.64	303.26	260.38	6
60.02	603.59	4.62	598.97	338.59	260.38	6
59.45	643.47	9.24	634.23	373.85	260.38	6
58.89	683.29	13.86	669.43	409.05	260.38	6
58.33	723.04	18.48	704.56	444.18	260.38	6
57.76	762.72	23.10	739.62	479.24	260.38	6
57.20	802.34	27.72	774.62	514.24	260.38	6
56.64	841.89	32.34	809.55	549.17	260.38	6
56.08	881.38	36.96	844.42	584.04	260.38	6
56.08	881.38	36.96	844.42	584.04	260.38	5
54.82	986.35	62.71	923.64	663.26	260.38	5
53.56	1090.40	88.46	1001.94	741.56	260.38	5
52.32	1193.53	114.21	1079.32	818.94	260.38	5
51.10	1295.73	139.96	1155.77	895.39	260.38	5
49.88	1397.01	165.71	1231.30	970.92	260.38	5

48.69	1497.36	191.46	1305.90	1045.52	260.38	5
48.69	1497.36	191.46	1305.90	1045.52	260.38	4
46.69	1697.80	267.32	1430.48	1170.10	260.38	4
44.70	1897.74	343.18	1554.56	1294.19	260.38	4
42.72	2097.14	419.04	1678.10	1417.72	260.38	4
40.75	2296.09	494.90	1801.19	1540.81	260.38	4
38.79	2494.28	570.76	1923.52	1663.15	260.38	4
36.85	2691.58	646.62	2044.97	1784.59	260.38	4
34.91	2887.98	722.48	2165.50	1905.12	260.38	4
33.00	3083.47	798.34	2285.13	2024.75	260.38	4
31.09	3278.05	874.19	2403.86	2143.48	260.38	4
31.09	3278.05	874.19	2403.86	2143.48	260.38	3
29.70	3426.62	936.05	2490.57	2230.19	260.38	3
28.32	3574.79	997.91	2576.88	2316.50	260.38	3
26.94	3722.60	1059.77	2662.83	2402.45	260.38	3
25.57	3870.06	1121.63	2748.43	2488.05	260.38	3
24.21	4017.17	1183.49	2833.68	2573.30	260.38	3
22.84	4163.93	1245.35	2918.59	2658.21	260.38	3
21.49	4310.35	1307.21	3003.14	2742.77	260.38	3
20.14	4456.42	1369.06	3087.35	2826.97	260.38	3
18.80	4602.14	1430.92	3171.21	2910.83	260.38	3
18.80	4602.14	1430.92	3171.21	2910.83	260.38	2
16.88	4807.80	1517.02	3290.78	3030.40	260.38	2
14.97	5012.94	1603.12	3409.82	3149.44	260.38	2
13.07	5217.55	1689.22	3528.33	3267.96	260.38	2
11.18	5421.63	1775.31	3646.32	3385.94	260.38	2
9.30	5625.18	1861.41	3763.77	3503.39	260.38	2
7.43	5828.20	1947.51	3880.69	3620.31	260.38	2
5.56	6030.71	2033.61	3997.10	3736.72	260.38	2
3.70	6232.83	2119.71	4113.12	3852.74	260.38	2
1.85	6434.59	2205.80	4228.79	3968.41	260.38	2
.00	6636.00	2291.90	4344.10	4083.72	260.38	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.86	2.45	.98	.98	.98	1
3.64	3.64	1.84	.98	.98	.92	1
2.43	2.43	1.23	.98	.98	.91	1
1.22	1.22	.61	.98	.98	.90	1
.00	.00	.00	.98	.98	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

4.86	.00	.00	.00	.00	.00	1
3.64	140.91	.00	140.91	75.82	65.09	1
2.43	281.82	.00	281.82	151.63	130.19	1
1.22	422.73	.00	422.73	227.45	195.28	1
.00	563.64	.00	563.64	303.26	260.38	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.49	21.42	6.50	6.00	5.71	6
60.02	59.96	21.35	6.49	6.15	5.70	6
59.45	59.41	21.27	6.47	6.27	5.69	6
58.89	58.86	21.20	6.46	6.35	5.67	6
58.33	58.30	21.12	6.44	6.39	5.66	6
57.76	57.75	21.05	6.43	6.41	5.64	6
57.20	57.19	20.97	6.42	6.41	5.63	6
56.64	56.63	20.90	6.40	6.40	5.62	6
56.08	56.07	20.82	6.39	6.39	5.60	6
56.08	56.07	20.82	4.51	4.51	3.86	5
54.82	54.80	20.59	4.44	4.44	3.80	5
53.56	53.54	20.36	4.38	4.38	3.73	5
52.32	52.31	20.12	4.32	4.31	3.67	5
51.10	51.08	19.89	4.25	4.25	3.61	5
49.88	49.87	19.66	4.19	4.19	3.54	5
48.69	48.68	19.43	4.13	4.12	3.48	5
48.69	48.68	19.43	1.93	1.93	1.89	4
46.69	46.68	18.75	1.92	1.92	1.87	4
44.70	44.69	18.06	1.91	1.91	1.85	4
42.72	42.71	17.38	1.89	1.89	1.83	4
40.75	40.74	16.70	1.88	1.88	1.81	4
38.79	38.78	16.01	1.86	1.86	1.79	4
36.85	36.83	15.33	1.84	1.84	1.77	4
34.91	34.90	14.65	1.82	1.82	1.74	4
33.00	32.99	13.97	1.80	1.80	1.72	4
31.09	31.08	13.28	1.78	1.78	1.70	4
31.09	31.08	13.28	1.47	1.47	1.43	3
29.70	29.69	12.72	1.46	1.46	1.42	3
28.32	28.31	12.16	1.45	1.45	1.41	3
26.94	26.93	11.59	1.44	1.44	1.40	3
25.57	25.56	11.03	1.43	1.43	1.39	3
24.21	24.20	10.47	1.42	1.42	1.38	3
22.84	22.84	9.90	1.41	1.41	1.37	3
21.49	21.48	9.34	1.40	1.40	1.36	3
20.14	20.13	8.78	1.39	1.39	1.35	3
18.80	18.79	8.21	1.38	1.38	1.34	3
18.80	18.79	8.21	1.34	1.34	1.31	2

16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.49	553.98	165.97	388.01	293.61	94.41	6
59.96	591.98	114.84	477.13	326.98	150.16	6
59.41	630.62	75.39	555.23	361.00	194.23	6
58.86	669.73	49.56	620.17	395.49	224.68	6
58.30	709.11	35.83	673.28	430.25	243.03	6
57.75	748.62	30.77	717.86	465.15	252.71	6
57.19	788.17	30.92	757.25	500.07	257.18	6
56.63	827.69	33.80	793.89	534.97	258.92	6
56.07	867.16	38.04	829.12	569.82	259.30	6
56.07	867.16	38.04	829.12	569.82	259.30	5
54.80	972.10	63.58	908.52	649.01	259.51	5
53.54	1076.12	89.33	986.79	727.28	259.51	5
52.31	1179.21	115.12	1064.10	804.62	259.48	5
51.08	1281.38	140.89	1140.50	881.04	259.45	5
49.87	1382.63	166.62	1216.01	956.54	259.47	5
48.68	1482.95	192.28	1290.67	1031.11	259.56	5
48.68	1482.95	192.28	1290.67	1031.11	259.56	4
46.68	1683.39	267.32	1416.07	1155.69	260.38	4
44.69	1883.31	343.18	1540.13	1279.76	260.38	4
42.71	2082.72	421.73	1660.98	1403.30	257.68	4
40.74	2281.55	507.74	1773.81	1526.28	247.54	4
38.78	2479.67	573.60	1906.08	1648.54	257.54	4
36.83	2676.96	646.64	2030.32	1769.97	260.35	4
34.90	2873.36	722.48	2150.88	1890.50	260.38	4
32.99	3068.85	798.34	2270.51	2010.13	260.38	4
31.08	3263.43	874.20	2389.24	2128.86	260.38	4
31.08	3263.43	874.20	2389.24	2128.86	260.38	3
29.69	3412.00	936.05	2475.95	2215.57	260.38	3
28.31	3560.18	997.91	2562.26	2301.89	260.38	3
26.93	3707.98	1060.98	2647.00	2387.83	259.17	3
25.56	3855.43	1123.18	2732.25	2473.42	258.83	3
24.20	4002.53	1185.01	2817.53	2558.67	258.86	3
22.84	4149.29	1246.81	2902.47	2643.56	258.91	3
21.48	4295.69	1308.58	2987.12	2728.11	259.01	3
20.13	4441.75	1370.28	3071.47	2812.31	259.16	3
18.79	4587.47	1431.78	3155.68	2896.17	259.52	3
18.79	4587.47	1431.78	3155.68	2896.17	259.52	2
16.87	4793.13	1517.20	3275.93	3015.73	260.20	2
14.96	4998.27	1603.17	3395.10	3134.77	260.33	2
13.06	5202.88	1689.22	3513.66	3253.28	260.38	2
11.17	5406.96	1775.31	3631.64	3371.27	260.38	2
9.29	5610.51	1861.41	3749.10	3488.72	260.38	2
7.42	5813.53	1947.51	3866.02	3605.64	260.38	2
5.55	6016.05	2033.61	3982.45	3722.07	260.38	2
3.69	6218.15	2123.61	4094.54	3838.06	256.48	2
1.84	6419.86	2245.26	4174.61	3953.68	220.93	2
.00	6620.75	2550.41	4070.35	4068.47	1.87	2

Time = 30. Degree of Consolidation = 4.%

Total Settlement = .090

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 30. = .090

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
4.86	4.71	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.34	1.23	.98	.91	.91	1
1.22	1.17	.61	.98	.91	.90	1
.00	.00	.00	.98	.90	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
4.71	.00	.00	.00	.00	.00	1
3.51	139.47	50.09	89.38	74.38	15.00	1
2.34	277.86	104.96	172.89	147.67	25.23	1
1.17	415.97	147.59	268.38	220.69	47.69	1
.00	553.98	165.97	388.01	293.61	94.41	1

Time = 30. Degree of Consolidation = 95.%

Total Settlement = .155

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 30. = .155

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 3.22

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.44	21.42	6.50	5.94	5.71	6
60.02	59.91	21.35	6.49	6.06	5.70	6
59.45	59.38	21.27	6.47	6.17	5.69	6
58.89	58.83	21.20	6.46	6.25	5.67	6
58.33	58.28	21.12	6.44	6.31	5.66	6

57.76	57.73	21.05	6.43	6.35	5.64	6
57.20	57.17	20.97	6.42	6.37	5.63	6
56.64	56.61	20.90	6.40	6.37	5.62	6
56.08	56.06	20.82	6.39	6.37	5.60	6
56.08	56.06	20.82	4.51	4.49	3.86	5
54.82	54.79	20.59	4.44	4.44	3.80	5
53.56	53.54	20.36	4.38	4.37	3.73	5
52.32	52.30	20.12	4.32	4.31	3.67	5
51.10	51.07	19.89	4.25	4.25	3.61	5
49.88	49.86	19.66	4.19	4.18	3.54	5
48.69	48.67	19.43	4.13	4.12	3.48	5
48.69	48.67	19.43	1.93	1.93	1.89	4
46.69	46.67	18.75	1.92	1.92	1.87	4
44.70	44.68	18.06	1.91	1.91	1.85	4
42.72	42.71	17.38	1.89	1.89	1.83	4
40.75	40.74	16.70	1.88	1.88	1.81	4
38.79	38.78	16.01	1.86	1.86	1.79	4
36.85	36.83	15.33	1.84	1.84	1.77	4
34.91	34.90	14.65	1.82	1.82	1.74	4
33.00	32.98	13.97	1.80	1.80	1.72	4
31.09	31.08	13.28	1.78	1.78	1.70	4
31.09	31.08	13.28	1.47	1.47	1.43	3
29.70	29.69	12.72	1.46	1.46	1.42	3
28.32	28.31	12.16	1.45	1.45	1.41	3
26.94	26.93	11.59	1.44	1.44	1.40	3
25.57	25.56	11.03	1.43	1.43	1.39	3
24.21	24.19	10.47	1.42	1.42	1.38	3
22.84	22.83	9.90	1.41	1.41	1.37	3
21.49	21.48	9.34	1.40	1.40	1.36	3
20.14	20.13	8.78	1.39	1.39	1.35	3
18.80	18.78	8.21	1.38	1.38	1.34	3
18.80	18.78	8.21	1.34	1.34	1.31	2
16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.41	3.29	1.28	1.28	1.25	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.44	553.83	183.98	369.85	293.46	76.40	6
59.91	591.48	144.59	446.88	326.48	120.40	6
59.38	629.65	110.51	519.14	360.03	159.10	6
58.83	668.26	83.32	584.94	394.02	190.92	6
58.28	707.20	63.60	643.61	428.34	215.26	6
57.73	746.38	50.92	695.45	462.90	232.56	6
57.17	785.69	44.15	741.53	497.59	243.95	6
56.61	825.06	41.85	783.21	532.34	250.87	6
56.06	864.44	42.58	821.86	567.10	254.76	6
56.06	864.44	42.58	821.86	567.10	254.76	5
54.79	969.26	66.08	903.18	646.17	257.01	5
53.54	1073.21	90.84	982.36	724.37	258.00	5
52.30	1176.26	116.21	1060.04	801.66	258.38	5
51.07	1278.39	141.81	1136.58	878.05	258.53	5
49.86	1379.60	167.45	1212.15	953.51	258.64	5
48.67	1479.90	193.03	1286.87	1028.06	258.82	5

48.67	1479.90	193.03	1286.87	1028.06	258.82	4
46.67	1680.33	267.32	1413.01	1152.63	260.38	4
44.68	1880.26	343.57	1536.69	1276.70	259.99	4
42.71	2079.65	426.41	1653.24	1400.23	253.01	4
40.74	2278.43	512.81	1765.62	1523.15	242.47	4
38.78	2476.50	577.04	1899.46	1645.36	254.09	4
36.83	2673.76	647.56	2026.20	1766.77	259.43	4
34.90	2870.15	722.48	2147.68	1887.30	260.38	4
32.98	3065.65	798.34	2267.31	2006.93	260.38	4
31.08	3260.23	874.20	2386.03	2125.66	260.38	4
31.08	3260.23	874.20	2386.03	2125.66	260.38	3
29.69	3408.80	936.05	2472.75	2212.37	260.38	3
28.31	3556.97	997.91	2559.06	2298.68	260.38	3
26.93	3704.77	1061.84	2642.94	2384.62	258.31	3
25.56	3852.22	1124.49	2727.73	2470.21	257.52	3
24.19	3999.31	1186.46	2812.85	2555.45	257.40	3
22.83	4146.06	1248.19	2897.86	2640.33	257.53	3
21.48	4292.46	1309.84	2982.62	2724.88	257.74	3
20.13	4438.51	1371.37	3067.14	2809.07	258.07	3
18.78	4584.22	1432.63	3151.59	2892.92	258.68	3
18.78	4584.22	1432.62	3151.59	2892.92	258.68	2
16.87	4789.88	1517.55	3272.34	3012.48	259.85	2
14.96	4995.02	1603.34	3391.68	3131.52	260.16	2
13.06	5199.63	1689.22	3510.41	3250.03	260.38	2
11.17	5403.71	1775.31	3628.39	3368.01	260.38	2
9.29	5607.26	1861.41	3745.85	3485.47	260.38	2
7.41	5810.28	1947.51	3862.77	3602.39	260.38	2
5.55	6012.79	2033.61	3979.18	3718.80	260.38	2
3.69	6214.89	2131.53	4083.35	3834.80	248.55	2
1.84	6416.52	2274.51	4142.01	3950.33	191.67	2
.00	6617.32	2550.66	4066.66	4065.04	1.63	2

Time = 60. Degree of Consolidation = 6.%

Total Settlement = .142

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 60. = .142

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.86	4.70	2.45
3.64	3.51	1.84
2.43	2.34	1.23
1.22	1.17	.61
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.70	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

3.51	139.46	53.28	86.17	74.36	11.81	1
2.34	277.81	114.50	163.31	147.62	15.69	1
1.17	415.88	161.38	254.50	220.60	33.90	1
.00	553.83	183.98	369.85	293.46	76.40	1

Time = 60. Degree of Consolidation = 96.%

Total Settlement = .157

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 60. = .157

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 3.16

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.36	21.42	6.50	5.89	5.71	6
60.02	59.83	21.35	6.49	5.98	5.70	6
59.45	59.30	21.27	6.47	6.06	5.69	6
58.89	58.77	21.20	6.46	6.13	5.67	6
58.33	58.22	21.12	6.44	6.19	5.66	6
57.76	57.68	21.05	6.43	6.24	5.64	6
57.20	57.13	20.97	6.42	6.28	5.63	6
56.64	56.58	20.90	6.40	6.31	5.62	6
56.08	56.03	20.82	6.39	6.33	5.60	6
56.08	56.03	20.82	4.51	4.46	3.86	5
54.82	54.77	20.59	4.44	4.41	3.80	5
53.56	53.52	20.36	4.38	4.36	3.73	5
52.32	52.28	20.12	4.32	4.30	3.67	5
51.10	51.06	19.89	4.25	4.24	3.61	5
49.88	49.85	19.66	4.19	4.18	3.54	5
48.69	48.66	19.43	4.13	4.11	3.48	5
48.69	48.66	19.43	1.93	1.93	1.89	4
46.69	46.66	18.75	1.92	1.92	1.87	4
44.70	44.68	18.06	1.91	1.90	1.85	4
42.72	42.70	17.38	1.89	1.89	1.83	4
40.75	40.73	16.70	1.88	1.87	1.81	4
38.79	38.77	16.01	1.86	1.86	1.79	4
36.85	36.83	15.33	1.84	1.84	1.77	4
34.91	34.89	14.65	1.82	1.82	1.74	4
33.00	32.98	13.97	1.80	1.80	1.72	4
31.09	31.07	13.28	1.78	1.78	1.70	4
31.09	31.07	13.28	1.47	1.47	1.43	3
29.70	29.68	12.72	1.46	1.46	1.42	3
28.32	28.30	12.16	1.45	1.45	1.41	3
26.94	26.92	11.59	1.44	1.44	1.40	3
25.57	25.55	11.03	1.43	1.43	1.39	3
24.21	24.19	10.47	1.42	1.42	1.38	3
22.84	22.83	9.90	1.41	1.41	1.37	3
21.49	21.47	9.34	1.40	1.40	1.36	3
20.14	20.12	8.78	1.39	1.39	1.35	3
18.80	18.78	8.21	1.38	1.38	1.34	3

18.80	18.78	8.21	1.34	1.31	2
16.88	16.86	7.39	1.33	1.30	2
14.97	14.96	6.57	1.32	1.29	2
13.07	13.06	5.75	1.31	1.28	2
11.18	11.17	4.93	1.30	1.27	2
9.30	9.28	4.11	1.29	1.26	2
7.43	7.41	3.29	1.28	1.25	2
5.56	5.54	2.46	1.27	1.25	2
3.70	3.69	1.64	1.26	1.24	2
1.85	1.84	.82	1.25	1.23	2
.00	.00	.00	1.25	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.36	553.70	200.69	353.01	293.33	59.68	6
59.83	591.04	171.73	419.31	326.04	93.27	6
59.30	628.76	144.98	483.78	359.15	124.64	6
58.77	666.85	121.25	545.60	392.61	152.99	6
58.22	705.25	101.12	604.14	426.39	177.74	6
57.68	743.92	84.83	659.09	460.44	198.65	6
57.13	782.78	72.32	710.46	494.68	215.78	6
56.58	821.80	63.23	758.57	529.08	229.49	6
56.03	860.93	56.99	803.94	563.59	240.35	6
56.03	860.93	56.99	803.94	563.59	240.35	5
54.77	965.31	76.31	888.99	642.21	246.78	5
53.52	1068.95	97.87	971.07	720.11	250.97	5
52.28	1171.79	121.03	1050.75	797.20	253.56	5
51.06	1273.77	145.26	1128.51	873.43	255.08	5
49.85	1374.88	170.20	1204.68	948.79	255.90	5
48.66	1475.08	195.62	1279.46	1023.24	256.22	5
48.66	1475.08	195.62	1279.46	1023.24	256.22	4
46.66	1675.50	268.59	1406.91	1147.80	259.11	4
44.68	1875.41	347.10	1528.31	1271.86	256.45	4
42.70	2074.77	433.98	1640.78	1395.35	245.43	4
40.73	2273.48	518.97	1754.51	1518.21	236.31	4
38.77	2471.48	582.39	1889.09	1640.34	248.75	4
36.83	2668.69	650.37	2018.32	1761.70	256.62	4
34.89	2865.07	722.58	2142.49	1882.22	260.27	4
32.98	3060.56	798.34	2262.23	2001.85	260.38	4
31.07	3255.15	874.20	2380.95	2120.57	260.38	4
31.07	3255.15	874.20	2380.95	2120.57	260.38	3
29.68	3403.72	936.05	2467.66	2207.28	260.38	3
28.30	3551.89	997.91	2553.98	2293.60	260.38	3
26.92	3699.69	1063.07	2636.61	2379.54	257.08	3
25.55	3847.12	1126.62	2720.50	2465.11	255.39	3
24.19	3994.20	1189.03	2805.17	2550.34	254.83	3
22.83	4140.93	1250.80	2890.14	2635.21	254.93	3
21.47	4287.32	1312.30	2975.02	2719.74	255.28	3
20.12	4433.36	1373.51	3059.85	2803.92	255.93	3
18.78	4579.06	1434.31	3144.75	2887.76	256.99	3
18.78	4579.06	1434.31	3144.75	2887.76	256.99	2
16.86	4784.71	1518.34	3266.37	3007.31	259.06	2
14.96	4989.84	1603.70	3386.14	3126.35	259.79	2
13.06	5194.45	1689.35	3505.10	3244.86	260.24	2
11.17	5398.53	1775.31	3623.22	3362.84	260.38	2
9.28	5602.09	1861.41	3740.68	3480.30	260.38	2
7.41	5805.10	1947.51	3857.59	3597.21	260.38	2
5.54	6007.62	2034.15	3973.47	3713.63	259.84	2
3.69	6209.68	2150.47	4059.21	3829.60	229.61	2
1.84	6411.18	2313.23	4097.96	3945.00	152.96	2
.00	6611.88	2550.98	4060.89	4059.59	1.30	2

Time = 120. Degree of Consolidation = 10.%

Total Settlement = .227

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 120. = .227

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.34	1.23	.98	.91	.91	1
1.22	1.17	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.44	55.90	83.54	74.35	9.19	1
2.34	277.78	122.46	155.32	147.59	7.73	1
1.17	415.81	173.30	242.51	220.53	21.99	1
.00	553.70	200.69	353.01	293.33	59.68	1

Time = 120. Degree of Consolidation = 97.%

Total Settlement = .159

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 120. = .159

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.07

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.22	21.42	6.50	5.86	5.71	6
60.02	59.70	21.35	6.49	5.92	5.70	6

59.45	59.18	21.27	6.47	5.98	5.69	6
58.89	58.65	21.20	6.46	6.03	5.67	6
58.33	58.12	21.12	6.44	6.09	5.66	6
57.76	57.58	21.05	6.43	6.13	5.64	6
57.20	57.04	20.97	6.42	6.18	5.63	6
56.64	56.49	20.90	6.40	6.22	5.62	6
56.08	55.95	20.82	6.39	6.25	5.60	6
56.08	55.95	20.82	4.51	4.39	3.86	5
54.82	54.70	20.59	4.44	4.35	3.80	5
53.56	53.46	20.36	4.38	4.31	3.73	5
52.32	52.24	20.12	4.32	4.26	3.67	5
51.10	51.03	19.89	4.25	4.20	3.61	5
49.88	49.83	19.66	4.19	4.14	3.54	5
48.69	48.64	19.43	4.13	4.08	3.48	5
48.69	48.64	19.43	1.93	1.93	1.89	4
46.69	46.65	18.75	1.92	1.92	1.87	4
44.70	44.66	18.06	1.91	1.90	1.85	4
42.72	42.68	17.38	1.89	1.89	1.83	4
40.75	40.72	16.70	1.88	1.87	1.81	4
38.79	38.76	16.01	1.86	1.85	1.79	4
36.85	36.82	15.33	1.84	1.84	1.77	4
34.91	34.89	14.65	1.82	1.82	1.74	4
33.00	32.97	13.97	1.80	1.80	1.72	4
31.09	31.07	13.28	1.78	1.78	1.70	4
31.09	31.07	13.28	1.47	1.47	1.43	3
29.70	29.68	12.72	1.46	1.46	1.42	3
28.32	28.29	12.16	1.45	1.45	1.41	3
26.94	26.92	11.59	1.44	1.44	1.40	3
25.57	25.54	11.03	1.43	1.43	1.39	3
24.21	24.18	10.47	1.42	1.42	1.38	3
22.84	22.82	9.90	1.41	1.41	1.37	3
21.49	21.47	9.34	1.40	1.40	1.36	3
20.14	20.12	8.78	1.39	1.39	1.35	3
18.80	18.77	8.21	1.38	1.38	1.34	3
18.80	18.77	8.21	1.34	1.34	1.31	2
16.88	16.86	7.39	1.33	1.33	1.30	2
14.97	14.95	6.57	1.32	1.32	1.29	2
13.07	13.05	5.75	1.31	1.31	1.28	2
11.18	11.16	4.93	1.30	1.30	1.27	2
9.30	9.28	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.25	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.68	1.64	1.26	1.26	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.22	553.65	213.36	340.29	293.27	47.02	6
59.70	590.74	192.83	397.90	325.74	72.16	6
59.18	628.11	173.04	455.07	358.49	96.58	6
58.65	665.76	154.29	511.47	391.52	119.95	6
58.12	703.67	136.84	566.84	424.81	142.02	6
57.58	741.82	120.89	620.93	458.34	162.59	6
57.04	780.18	106.56	673.62	492.08	181.54	6
56.49	818.74	93.92	724.82	526.02	198.80	6
55.95	857.46	82.93	774.53	560.12	214.41	6
55.95	857.46	82.93	774.53	560.12	214.41	5
54.70	960.96	99.27	861.69	637.87	223.82	5
53.46	1063.84	117.70	946.14	714.99	231.14	5
52.24	1166.02	138.04	1027.97	791.42	236.55	5

51.03	1267.43	160.13	1107.30	867.09	240.21	5
49.83	1368.03	183.83	1184.20	941.94	242.26	5
48.64	1467.75	209.01	1258.74	1015.91	242.83	5
48.64	1467.75	209.01	1258.74	1015.91	242.83	4
46.65	1668.09	279.86	1388.23	1140.39	247.84	4
44.66	1867.93	358.27	1509.66	1264.37	245.29	4
42.68	2067.20	446.68	1620.51	1387.78	232.74	4
40.72	2265.82	526.92	1738.90	1510.54	228.36	4
38.76	2463.73	589.51	1874.22	1632.59	241.63	4
36.82	2660.87	655.41	2005.45	1753.87	251.58	4
34.89	2857.20	724.93	2132.27	1874.35	257.93	4
32.97	3052.68	798.34	2254.34	1993.96	260.38	4
31.07	3247.27	874.20	2373.07	2112.69	260.38	4
31.07	3247.27	874.20	2373.07	2112.69	260.38	3
29.68	3395.83	936.05	2459.78	2199.40	260.38	3
28.29	3544.01	997.91	2546.10	2285.72	260.38	3
26.92	3691.80	1064.81	2626.99	2371.65	255.34	3
25.54	3839.22	1129.70	2709.52	2457.22	252.30	3
24.18	3986.28	1192.99	2793.30	2542.42	250.88	3
22.82	4132.99	1255.16	2877.83	2627.27	250.57	3
21.47	4279.35	1316.53	2962.82	2711.77	251.05	3
20.12	4425.37	1377.35	3048.02	2795.93	252.09	3
18.77	4571.05	1437.57	3133.48	2879.75	253.73	3
18.77	4571.05	1437.57	3133.48	2879.75	253.73	2
16.86	4776.69	1520.42	3256.27	2999.29	256.98	2
14.95	4981.81	1604.72	3377.09	3118.31	258.77	2
13.05	5186.41	1689.87	3496.54	3236.82	259.73	2
11.16	5390.49	1775.35	3615.14	3354.80	260.34	2
9.28	5594.04	1861.41	3732.63	3472.25	260.38	2
7.40	5797.06	1947.51	3849.55	3589.17	260.38	2
5.54	5999.56	2044.83	3954.74	3705.57	249.16	2
3.68	6201.54	2183.04	4018.50	3821.45	197.05	2
1.83	6402.88	2352.65	4050.23	3936.70	113.53	2
.00	6603.47	2551.31	4052.16	4051.19	.97	2

Time = 240. Degree of Consolidation = 16.%

Total Settlement = .361

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 240. = .361

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1
1.22	1.17	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.44	57.02	82.42	74.34	8.07	1
2.33	277.76	125.90	151.86	147.57	4.29	1
1.17	415.78	178.58	237.19	220.49	16.70	1
.00	553.65	213.36	340.29	293.27	47.02	1

Time = 240. Degree of Consolidation = 98.%

Total Settlement = .160

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 240. = .160

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.94

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.11	21.42	6.50	5.84	5.71	6
60.02	59.59	21.35	6.49	5.89	5.70	6
59.45	59.07	21.27	6.47	5.94	5.69	6
58.89	58.54	21.20	6.46	5.99	5.67	6
58.33	58.01	21.12	6.44	6.03	5.66	6
57.76	57.48	21.05	6.43	6.08	5.64	6
57.20	56.94	20.97	6.42	6.12	5.63	6
56.64	56.40	20.90	6.40	6.15	5.62	6
56.08	55.86	20.82	6.39	6.19	5.60	6
56.08	55.86	20.82	4.51	4.34	3.86	5
54.82	54.63	20.59	4.44	4.30	3.80	5
53.56	53.40	20.36	4.38	4.26	3.73	5
52.32	52.19	20.12	4.32	4.21	3.67	5
51.10	50.99	19.89	4.25	4.15	3.61	5
49.88	49.80	19.66	4.19	4.10	3.54	5
48.69	48.63	19.43	4.13	4.03	3.48	5
48.69	48.63	19.43	1.93	1.92	1.89	4
46.69	46.63	18.75	1.92	1.91	1.87	4
44.70	44.65	18.06	1.91	1.90	1.85	4
42.72	42.67	17.38	1.89	1.89	1.83	4
40.75	40.71	16.70	1.88	1.87	1.81	4
38.79	38.75	16.01	1.86	1.85	1.79	4
36.85	36.81	15.33	1.84	1.84	1.77	4
34.91	34.88	14.65	1.82	1.82	1.74	4
33.00	32.96	13.97	1.80	1.80	1.72	4
31.09	31.06	13.28	1.78	1.78	1.70	4
31.09	31.06	13.28	1.47	1.47	1.43	3
29.70	29.67	12.72	1.46	1.46	1.42	3
28.32	28.29	12.16	1.45	1.45	1.41	3
26.94	26.91	11.59	1.44	1.44	1.40	3
25.57	25.54	11.03	1.43	1.43	1.39	3

24.21	24.17	10.47	1.42	1.42	1.38	3
22.84	22.81	9.90	1.41	1.41	1.37	3
21.49	21.46	9.34	1.40	1.40	1.36	3
20.14	20.11	8.78	1.39	1.39	1.35	3
18.80	18.77	8.21	1.38	1.38	1.34	3
18.80	18.77	8.21	1.34	1.34	1.31	2
16.88	16.85	7.39	1.33	1.33	1.30	2
14.97	14.95	6.57	1.32	1.32	1.29	2
13.07	13.05	5.75	1.31	1.31	1.28	2
11.18	11.16	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.25	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.11	553.62	219.24	334.38	293.24	41.14	6
59.59	590.60	202.39	388.21	325.60	62.60	6
59.07	627.82	185.94	441.88	358.20	83.68	6
58.54	665.26	170.04	495.22	391.02	104.20	6
58.01	702.93	154.87	548.06	424.07	123.99	6
57.48	740.81	140.57	600.24	457.33	142.91	6
56.94	778.88	127.28	651.61	490.78	160.82	6
56.40	817.14	115.10	702.04	524.42	177.62	6
55.86	855.56	104.14	751.42	558.22	193.20	6
55.86	855.56	104.14	751.42	558.22	193.20	5
54.63	958.30	120.36	837.94	635.21	202.73	5
53.40	1060.43	138.38	922.05	711.58	210.46	5
52.19	1161.87	158.18	1003.69	787.28	216.41	5
50.99	1262.58	179.74	1082.84	862.24	220.60	5
49.80	1362.48	203.01	1159.47	936.39	223.08	5
48.63	1461.51	227.95	1233.57	1009.67	223.89	5
48.63	1461.51	227.95	1233.57	1009.67	223.89	4
46.63	1661.74	296.60	1365.14	1134.04	231.10	4
44.65	1861.46	373.34	1488.13	1257.90	230.22	4
42.67	2060.63	460.80	1599.84	1381.22	218.62	4
40.71	2259.17	534.29	1724.87	1503.89	220.98	4
38.75	2456.99	595.53	1861.46	1625.86	235.61	4
36.81	2654.07	659.87	1994.20	1747.07	247.13	4
34.88	2850.36	727.50	2122.86	1867.50	255.35	4
32.96	3045.82	798.74	2247.08	1987.11	259.98	4
31.06	3240.41	874.39	2366.02	2105.83	260.18	4
31.06	3240.41	874.39	2366.02	2105.83	260.18	3
29.67	3388.98	936.05	2452.92	2192.54	260.38	3
28.29	3537.15	997.91	2539.24	2278.86	260.38	3
26.91	3684.94	1066.01	2618.93	2364.79	254.14	3
25.54	3832.35	1132.05	2700.30	2450.34	249.96	3
24.17	3979.40	1196.10	2783.30	2535.53	247.76	3
22.81	4126.09	1258.73	2867.35	2620.36	246.99	3
21.46	4272.43	1320.19	2952.23	2704.84	247.39	3
20.11	4418.42	1380.84	3037.58	2788.98	248.60	3
18.77	4564.08	1440.66	3123.43	2872.78	250.64	3
18.77	4564.08	1440.66	3123.43	2872.78	250.64	2
16.85	4769.70	1522.70	3247.01	2992.31	254.70	2
14.95	4974.82	1606.24	3368.57	3111.32	257.25	2
13.05	5179.41	1690.63	3488.78	3229.82	258.97	2
11.16	5383.49	1775.81	3607.68	3347.79	259.89	2
9.27	5587.03	1861.55	3725.48	3465.24	260.24	2

7.40	5790.05	1948.48	3841.57	3582.16	259.41	2
5.54	5992.53	2058.06	3934.46	3698.54	235.93	2
3.68	6194.42	2206.29	3988.13	3814.34	173.79	2
1.83	6395.67	2372.66	4023.02	3929.49	93.53	2
.00	6596.22	2551.48	4044.74	4043.94	.80	2

Time = 365. Degree of Consolidation = 22.%

Total Settlement = .477

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 365. = .477

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1
1.22	1.17	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.44	57.51	81.92	74.34	7.58	1
2.33	277.75	127.42	150.33	147.56	2.77	1
1.17	415.76	180.95	234.81	220.48	14.33	1
.00	553.62	219.24	334.38	293.24	41.14	1

Time = 365. Degree of Consolidation = 98.%

Total Settlement = .161

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 365. = .161

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.82

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.96	21.42	6.50	5.82	5.71	6
60.02	59.45	21.35	6.49	5.86	5.70	6
59.45	58.93	21.27	6.47	5.90	5.69	6
58.89	58.40	21.20	6.46	5.94	5.67	6
58.33	57.88	21.12	6.44	5.98	5.66	6
57.76	57.35	21.05	6.43	6.02	5.64	6
57.20	56.82	20.97	6.42	6.05	5.63	6
56.64	56.28	20.90	6.40	6.08	5.62	6
56.08	55.75	20.82	6.39	6.11	5.60	6
56.08	55.75	20.82	4.51	4.28	3.86	5
54.82	54.53	20.59	4.44	4.24	3.80	5
53.56	53.32	20.36	4.38	4.19	3.73	5
52.32	52.12	20.12	4.32	4.14	3.67	5
51.10	50.94	19.89	4.25	4.09	3.61	5
49.88	49.76	19.66	4.19	4.03	3.54	5
48.69	48.60	19.43	4.13	3.97	3.48	5
48.69	48.60	19.43	1.93	1.92	1.89	4
46.69	46.61	18.75	1.92	1.91	1.87	4
44.70	44.63	18.06	1.91	1.90	1.85	4
42.72	42.66	17.38	1.89	1.88	1.83	4
40.75	40.69	16.70	1.88	1.87	1.81	4
38.79	38.74	16.01	1.86	1.85	1.79	4
36.85	36.80	15.33	1.84	1.83	1.77	4
34.91	34.87	14.65	1.82	1.82	1.74	4
33.00	32.95	13.97	1.80	1.80	1.72	4
31.09	31.05	13.28	1.78	1.77	1.70	4
31.09	31.05	13.28	1.47	1.47	1.43	3
29.70	29.66	12.72	1.46	1.46	1.42	3
28.32	28.28	12.16	1.45	1.45	1.41	3
26.94	26.90	11.59	1.44	1.44	1.40	3
25.57	25.53	11.03	1.43	1.43	1.39	3
24.21	24.17	10.47	1.42	1.42	1.38	3
22.84	22.81	9.90	1.41	1.41	1.37	3
21.49	21.45	9.34	1.40	1.40	1.36	3
20.14	20.11	8.78	1.39	1.39	1.35	3
18.80	18.76	8.21	1.38	1.38	1.34	3
18.80	18.76	8.21	1.34	1.34	1.31	2
16.88	16.85	7.39	1.33	1.33	1.30	2
14.97	14.94	6.57	1.32	1.32	1.29	2
13.07	13.04	5.75	1.31	1.31	1.28	2
11.18	11.15	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.25	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.96	553.60	224.37	329.23	293.22	36.01	6
59.45	590.48	210.61	379.87	325.48	54.39	6
58.93	627.56	197.13	430.43	357.94	72.49	6
58.40	664.83	184.06	480.77	390.59	90.18	6
57.88	702.28	171.50	530.77	423.42	107.36	6
57.35	739.90	159.60	580.30	456.42	123.88	6
56.82	777.69	148.46	629.23	489.59	139.64	6
56.28	815.63	138.19	677.44	522.91	154.53	6

55.75	853.71	128.90	724.81	556.37	168.44	6
55.75	853.71	128.90	724.81	556.37	168.44	5
54.53	955.54	146.01	809.53	632.45	177.08	5
53.32	1056.74	164.62	892.12	707.90	184.22	5
52.12	1157.24	184.76	972.48	782.65	189.83	5
50.94	1256.98	206.44	1050.55	856.64	193.90	5
49.76	1355.93	229.66	1126.27	929.84	196.43	5
48.60	1454.01	254.39	1199.62	1002.17	197.45	5
48.60	1454.01	254.39	1199.62	1002.17	197.45	4
46.61	1654.06	321.18	1332.88	1126.36	206.52	4
44.63	1853.63	396.13	1457.50	1250.07	207.43	4
42.66	2052.65	482.03	1570.62	1373.23	197.39	4
40.69	2251.04	545.06	1705.98	1495.76	210.22	4
38.74	2448.75	604.17	1844.58	1617.61	226.97	4
36.80	2645.74	666.41	1979.32	1738.74	240.58	4
34.87	2841.96	732.04	2109.92	1859.11	250.81	4
32.95	3037.38	801.51	2235.87	1978.66	257.21	4
31.05	3231.94	875.73	2356.22	2097.37	258.85	4
31.05	3231.94	875.72	2356.22	2097.37	258.85	3
29.66	3380.51	936.05	2444.45	2184.07	260.38	3
28.28	3528.69	997.91	2530.77	2270.40	260.38	3
26.90	3676.47	1067.36	2609.11	2356.32	252.79	3
25.53	3823.87	1134.53	2689.34	2441.86	247.48	3
24.17	3970.90	1199.45	2771.44	2527.03	244.41	3
22.81	4117.57	1262.61	2854.96	2611.84	243.12	3
21.45	4263.88	1324.36	2939.53	2696.30	243.22	3
20.11	4409.86	1384.90	3024.96	2780.42	244.54	3
18.76	4555.50	1444.37	3111.13	2864.19	246.93	3
18.76	4555.50	1444.37	3111.13	2864.19	246.93	2
16.85	4761.10	1525.74	3235.36	2983.70	251.66	2
14.94	4966.19	1608.37	3357.82	3102.69	255.13	2
13.04	5170.78	1692.21	3478.57	3221.18	257.39	2
11.15	5374.84	1777.14	3597.70	3339.15	258.55	2
9.27	5578.38	1863.80	3714.58	3456.59	257.99	2
7.40	5781.38	1953.94	3827.43	3573.49	253.95	2
5.53	5983.80	2074.06	3909.74	3689.81	219.93	2
3.68	6185.62	2226.62	3959.00	3805.54	153.46	2
1.83	6386.80	2387.43	3999.37	3920.61	78.76	2
.00	6587.31	2551.60	4035.70	4035.02	.68	2

Time = 540. Degree of Consolidation = 28.%

Total Settlement = .619

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 540. = .619

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1

1.22	1.17	.61	.98	.90	1
.00	.00	.00	.98	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.44	57.93	81.50	74.34	7.16	1
2.33	277.75	128.71	149.03	147.56	1.48	1
1.17	415.75	182.97	232.78	220.47	12.31	1
.00	553.60	224.37	329.23	293.22	36.01	1

Time = 540. Degree of Consolidation = 98.%

Total Settlement = .161

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 540. = .161

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.68

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.83	21.42	6.50	5.81	5.71	6
60.02	59.31	21.35	6.49	5.84	5.70	6
59.45	58.79	21.27	6.47	5.88	5.69	6
58.89	58.27	21.20	6.46	5.91	5.67	6
58.33	57.75	21.12	6.44	5.94	5.66	6
57.76	57.22	21.05	6.43	5.97	5.64	6
57.20	56.70	20.97	6.42	5.99	5.63	6
56.64	56.17	20.90	6.40	6.02	5.62	6
56.08	55.64	20.82	6.39	6.04	5.60	6
56.08	55.64	20.82	4.51	4.22	3.86	5
54.82	54.43	20.59	4.44	4.18	3.80	5
53.56	53.24	20.36	4.38	4.13	3.73	5
52.32	52.05	20.12	4.32	4.08	3.67	5
51.10	50.88	19.89	4.25	4.02	3.61	5
49.88	49.72	19.66	4.19	3.97	3.54	5
48.69	48.58	19.43	4.13	3.90	3.48	5
48.69	48.58	19.43	1.93	1.92	1.89	4
46.69	46.59	18.75	1.92	1.90	1.87	4
44.70	44.61	18.06	1.91	1.89	1.85	4
42.72	42.64	17.38	1.89	1.88	1.83	4
40.75	40.68	16.70	1.88	1.86	1.81	4
38.79	38.73	16.01	1.86	1.85	1.79	4
36.85	36.79	15.33	1.84	1.83	1.77	4
34.91	34.86	14.65	1.82	1.81	1.74	4
33.00	32.95	13.97	1.80	1.79	1.72	4
31.09	31.05	13.28	1.78	1.77	1.70	4

31.09	31.05	13.28	1.47	1.47	1.43	3
29.70	29.66	12.72	1.46	1.46	1.42	3
28.32	28.27	12.16	1.45	1.45	1.41	3
26.94	26.90	11.59	1.44	1.44	1.40	3
25.57	25.53	11.03	1.43	1.43	1.39	3
24.21	24.16	10.47	1.42	1.42	1.38	3
22.84	22.80	9.90	1.41	1.41	1.37	3
21.49	21.45	9.34	1.40	1.40	1.36	3
20.14	20.10	8.78	1.39	1.39	1.35	3
18.80	18.76	8.21	1.38	1.38	1.34	3
18.80	18.76	8.21	1.34	1.34	1.31	2
16.88	16.84	7.39	1.33	1.33	1.30	2
14.97	14.94	6.57	1.32	1.32	1.29	2
13.07	13.04	5.75	1.31	1.31	1.28	2
11.18	11.15	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.39	3.29	1.28	1.27	1.25	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.83	553.58	228.82	324.76	293.20	31.56	6
59.31	590.38	217.63	372.75	325.38	47.37	6
58.79	627.34	206.69	420.65	357.72	62.93	6
58.27	664.45	196.11	468.35	390.22	78.13	6
57.75	701.72	185.98	515.74	422.86	92.88	6
57.22	739.12	176.41	562.71	455.64	107.07	6
56.70	776.65	167.50	609.15	488.55	120.60	6
56.17	814.30	159.35	654.96	521.58	133.37	6
55.64	852.07	152.04	700.03	554.73	145.30	6
55.64	852.07	152.04	700.03	554.73	145.30	5
54.43	953.05	170.27	782.78	629.96	152.82	5
53.24	1053.36	189.74	863.62	704.52	159.10	5
52.05	1152.94	210.49	942.45	778.35	164.10	5
50.88	1251.76	232.54	1019.22	851.42	167.80	5
49.72	1349.77	255.90	1093.87	923.68	170.20	5
48.58	1446.91	280.53	1166.38	995.07	171.31	5
48.58	1446.91	280.53	1166.38	995.07	171.31	4
46.59	1646.78	346.45	1300.33	1119.08	181.25	4
44.61	1846.18	420.46	1425.71	1242.62	183.09	4
42.64	2045.04	503.06	1541.98	1365.62	176.36	4
40.68	2243.28	557.11	1686.16	1488.00	198.16	4
38.73	2440.86	614.11	1826.74	1609.72	217.02	4
36.79	2637.74	674.30	1963.44	1730.74	232.70	4
34.86	2833.88	737.93	2095.94	1851.02	244.92	4
32.95	3029.24	805.49	2223.74	1970.52	253.22	4
31.05	3223.76	877.91	2345.85	2089.19	256.66	4
31.05	3223.76	877.91	2345.85	2089.19	256.66	3
29.66	3372.32	936.57	2435.76	2175.89	259.87	3
28.27	3520.50	998.32	2522.17	2262.21	259.97	3
26.90	3668.28	1068.53	2599.75	2348.13	251.62	3
25.53	3815.67	1136.44	2679.23	2433.66	245.57	3
24.16	3962.68	1202.10	2760.59	2518.82	241.77	3
22.80	4109.34	1265.74	2843.59	2603.61	239.98	3
21.45	4255.64	1327.75	2927.88	2688.05	239.83	3
20.10	4401.59	1388.30	3013.29	2772.15	241.14	3
18.76	4547.21	1447.55	3099.66	2855.91	243.75	3
18.76	4547.21	1447.55	3099.66	2855.91	243.75	2

16.84	4752.79	1528.51	3224.28	2975.39	248.89	2
14.94	4957.87	1610.73	3347.14	3094.37	252.77	2
13.04	5162.44	1694.51	3467.93	3212.85	255.08	2
11.15	5366.49	1780.14	3586.35	3330.80	255.55	2
9.27	5570.01	1868.20	3701.81	3448.22	253.59	2
7.39	5772.97	1960.87	3812.10	3565.08	247.02	2
5.53	5975.34	2087.92	3887.42	3681.36	206.07	2
3.68	6177.10	2240.61	3936.49	3797.02	139.47	2
1.83	6378.23	2396.29	3981.94	3912.05	69.89	2
.00	6578.72	2551.68	4027.04	4026.44	.61	2

Time = 730. Degree of Consolidation = 34.%

Total Settlement = .757

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 730. = .757

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1
1.22	1.17	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.43	58.28	81.15	74.34	6.81	1
2.33	277.74	129.80	147.94	147.55	.39	1
1.17	415.74	184.69	231.05	220.46	10.59	1
.00	553.58	228.82	324.76	293.20	31.56	1

Time = 730. Degree of Consolidation = 99.%

Total Settlement = .161

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 730. = .161

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.54

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.61	21.42	6.50	5.80	5.71	6
60.02	59.10	21.35	6.49	5.82	5.70	6
59.45	58.58	21.27	6.47	5.84	5.69	6
58.89	58.06	21.20	6.46	5.86	5.67	6
58.33	57.55	21.12	6.44	5.88	5.66	6
57.76	57.03	21.05	6.43	5.90	5.64	6
57.20	56.50	20.97	6.42	5.91	5.63	6
56.64	55.98	20.90	6.40	5.92	5.62	6
56.08	55.46	20.82	6.39	5.94	5.60	6
56.08	55.46	20.82	4.51	4.14	3.86	5
54.82	54.27	20.59	4.44	4.09	3.80	5
53.56	53.10	20.36	4.38	4.03	3.73	5
52.32	51.94	20.12	4.32	3.98	3.67	5
51.10	50.79	19.89	4.25	3.92	3.61	5
49.88	49.66	19.66	4.19	3.86	3.54	5
48.69	48.54	19.43	4.13	3.80	3.48	5
48.69	48.54	19.43	1.93	1.91	1.89	4
46.69	46.55	18.75	1.92	1.90	1.87	4
44.70	44.58	18.06	1.91	1.89	1.85	4
42.72	42.61	17.38	1.89	1.87	1.83	4
40.75	40.65	16.70	1.88	1.86	1.81	4
38.79	38.71	16.01	1.86	1.84	1.79	4
36.85	36.77	15.33	1.84	1.83	1.77	4
34.91	34.85	14.65	1.82	1.81	1.74	4
33.00	32.93	13.97	1.80	1.79	1.72	4
31.09	31.03	13.28	1.78	1.77	1.70	4
31.09	31.03	13.28	1.47	1.47	1.43	3
29.70	29.64	12.72	1.46	1.46	1.42	3
28.32	28.26	12.16	1.45	1.45	1.41	3
26.94	26.89	11.59	1.44	1.44	1.40	3
25.57	25.52	11.03	1.43	1.43	1.39	3
24.21	24.15	10.47	1.42	1.42	1.38	3
22.84	22.79	9.90	1.41	1.41	1.37	3
21.49	21.44	9.34	1.40	1.40	1.36	3
20.14	20.09	8.78	1.39	1.39	1.35	3
18.80	18.75	8.21	1.38	1.38	1.34	3
18.80	18.75	8.21	1.34	1.34	1.31	2
16.88	16.84	7.39	1.33	1.33	1.30	2
14.97	14.93	6.57	1.32	1.32	1.29	2
13.07	13.03	5.75	1.31	1.31	1.28	2
11.18	11.14	4.93	1.30	1.30	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.25	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.61	553.43	231.19	322.24	293.05	29.19	6
59.10	590.16	224.51	365.65	325.16	40.49	6
58.58	626.99	218.01	408.98	357.37	51.61	6

58.06	663.91	211.76	452.16	389.67	62.48	6
57.55	700.92	205.82	495.10	422.06	73.04	6
57.03	738.01	200.29	537.72	454.53	83.19	6
56.50	775.18	195.23	579.95	487.07	92.87	6
55.98	812.41	190.73	621.68	519.69	101.99	6
55.46	849.70	186.86	662.84	552.36	110.48	6
55.46	849.70	186.86	662.84	552.36	110.48	5
54.27	949.40	207.13	742.27	626.31	115.96	5
53.10	1048.35	228.23	820.12	699.51	120.61	5
51.94	1146.53	250.21	896.32	771.94	124.38	5
50.79	1243.91	273.08	970.83	843.57	127.26	5
49.66	1340.45	296.86	1043.59	914.36	129.23	5
48.54	1436.12	321.55	1114.58	984.28	130.30	5
48.54	1436.12	321.55	1114.58	984.28	130.30	4
46.55	1635.71	387.89	1247.82	1108.01	139.81	4
44.58	1834.83	462.37	1372.46	1231.27	141.19	4
42.61	2033.40	526.27	1507.13	1353.98	153.14	4
40.65	2231.38	577.92	1653.46	1476.10	177.36	4
38.71	2428.73	632.35	1796.38	1597.59	198.79	4
36.77	2625.40	689.85	1935.55	1718.41	217.14	4
34.85	2821.38	750.85	2070.52	1838.52	232.00	4
32.93	3016.60	816.11	2200.49	1957.88	242.61	4
31.03	3211.01	886.77	2324.23	2076.43	247.80	4
31.03	3211.01	886.77	2324.23	2076.43	247.80	3
29.64	3359.51	943.79	2415.72	2163.08	252.64	3
28.26	3507.65	1004.79	2502.86	2249.36	253.50	3
26.89	3655.39	1074.16	2581.24	2335.24	245.99	3
25.52	3802.75	1141.54	2661.21	2420.75	240.47	3
24.15	3949.74	1207.06	2742.68	2505.88	236.80	3
22.79	4096.37	1270.77	2825.59	2590.64	234.95	3
21.44	4242.64	1332.86	2909.78	2675.05	234.72	3
20.09	4388.56	1393.49	2995.07	2759.12	235.95	3
18.75	4534.15	1452.84	3081.31	2842.85	238.46	3
18.75	4534.15	1452.84	3081.31	2842.85	238.46	2
16.84	4739.70	1534.03	3205.67	2962.30	243.37	2
14.93	4944.75	1616.50	3328.25	3081.25	247.00	2
13.03	5149.28	1700.57	3448.71	3199.68	249.02	2
11.14	5353.29	1786.96	3566.33	3317.60	248.73	2
9.26	5556.76	1876.77	3679.99	3434.97	245.02	2
7.39	5759.66	1971.73	3787.94	3551.77	236.16	2
5.53	5961.96	2105.98	3855.98	3667.98	188.01	2
3.68	6163.66	2256.14	3907.52	3783.57	123.95	2
1.83	6364.73	2405.24	3959.49	3898.55	60.94	2
.00	6565.20	2551.75	4013.45	4012.92	.53	2

Time = 1080. Degree of Consolidation = 44.%

Total Settlement = .971

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 1080. = .971

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1
1.22	1.16	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.38	65.09	74.28	74.28	.00	1
2.33	277.67	130.19	147.48	147.48	.00	1
1.16	415.65	195.28	220.37	220.37	.00	1
.00	553.43	260.38	293.05	293.05	.00	1

Time = 1080. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 1080. = .164

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.33

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.41	21.42	6.50	5.76	5.71	6
60.02	58.90	21.35	6.49	5.77	5.70	6
59.45	58.39	21.27	6.47	5.79	5.69	6
58.89	57.88	21.20	6.46	5.80	5.67	6
58.33	57.36	21.12	6.44	5.81	5.66	6
57.76	56.85	21.05	6.43	5.82	5.64	6
57.20	56.33	20.97	6.42	5.83	5.63	6
56.64	55.81	20.90	6.40	5.84	5.62	6
56.08	55.30	20.82	6.39	5.84	5.60	6
56.08	55.30	20.82	4.51	4.06	3.86	5
54.82	54.13	20.59	4.44	4.01	3.80	5
53.56	52.98	20.36	4.38	3.95	3.73	5
52.32	51.83	20.12	4.32	3.90	3.67	5
51.10	50.71	19.89	4.25	3.84	3.61	5
49.88	49.59	19.66	4.19	3.78	3.54	5
48.69	48.49	19.43	4.13	3.72	3.48	5
48.69	48.49	19.43	1.93	1.90	1.89	4
46.69	46.51	18.75	1.92	1.89	1.87	4
44.70	44.54	18.06	1.91	1.88	1.85	4
42.72	42.58	17.38	1.89	1.87	1.83	4
40.75	40.62	16.70	1.88	1.85	1.81	4

38.79	38.68	16.01	1.86	1.79	4	
36.85	36.75	15.33	1.84	1.82	1.77	4
34.91	34.83	14.65	1.82	1.81	1.74	4
33.00	32.92	13.97	1.80	1.79	1.72	4
31.09	31.02	13.28	1.78	1.77	1.70	4
31.09	31.02	13.28	1.47	1.47	1.43	3
29.70	29.63	12.72	1.46	1.46	1.42	3
28.32	28.25	12.16	1.45	1.45	1.41	3
26.94	26.88	11.59	1.44	1.44	1.40	3
25.57	25.51	11.03	1.43	1.43	1.39	3
24.21	24.14	10.47	1.42	1.42	1.38	3
22.84	22.78	9.90	1.41	1.41	1.37	3
21.49	21.43	9.34	1.40	1.40	1.36	3
20.14	20.09	8.78	1.39	1.39	1.35	3
18.80	18.74	8.21	1.38	1.38	1.34	3
18.80	18.74	8.21	1.34	1.33	1.31	2
16.88	16.83	7.39	1.33	1.33	1.30	2
14.97	14.93	6.57	1.32	1.32	1.29	2
13.07	13.03	5.75	1.31	1.31	1.28	2
11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.25	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.41	553.42	244.64	308.78	293.05	15.73	6
58.90	589.95	240.14	349.82	324.95	24.86	6
58.39	626.55	235.81	390.73	356.93	33.81	6
57.88	663.20	231.75	431.45	388.96	42.49	6
57.36	699.90	228.00	471.91	421.04	50.86	6
56.85	736.66	224.64	512.02	453.18	58.84	6
56.33	773.47	221.73	551.74	485.37	66.37	6
55.81	810.31	219.33	590.98	517.59	73.39	6
55.30	847.18	217.49	629.69	549.84	79.85	6
55.30	847.18	217.49	629.69	549.84	79.85	5
54.13	945.75	238.99	706.77	622.66	84.10	5
52.98	1043.54	261.12	782.42	694.70	87.72	5
51.83	1140.53	283.92	856.61	765.94	90.67	5
50.71	1236.69	307.40	929.29	836.35	92.94	5
49.59	1331.99	331.55	1000.43	905.90	94.54	5
48.49	1426.41	356.38	1070.03	974.57	95.46	5
48.49	1426.41	356.38	1070.03	974.57	95.46	4
46.51	1625.76	424.08	1201.69	1098.06	103.62	4
44.54	1824.63	500.09	1324.53	1221.07	103.47	4
42.58	2022.94	547.91	1475.03	1343.52	131.51	4
40.62	2220.67	598.10	1622.57	1465.39	157.18	4
38.68	2417.78	650.88	1766.90	1586.65	180.26	4
36.75	2614.25	706.68	1907.57	1707.25	200.32	4
34.83	2810.03	765.97	2044.06	1827.18	216.88	4
32.92	3005.08	829.68	2175.40	1946.36	229.04	4
31.02	3199.33	899.13	2300.21	2064.76	235.44	4
31.02	3199.33	899.13	2300.21	2064.76	235.44	3
29.63	3347.77	954.96	2392.80	2151.34	241.47	3
28.25	3495.84	1015.87	2479.97	2237.55	242.42	3
26.88	3643.52	1083.54	2559.98	2323.37	236.61	3
25.51	3790.84	1149.73	2641.10	2408.83	232.28	3
24.14	3937.78	1214.41	2723.37	2493.91	229.45	3

22.78	4084.36	1277.60	2806.76	2578.64	228.12	3
21.43	4230.60	1339.43	2891.17	2663.01	228.16	3
20.09	4376.49	1400.05	2976.44	2747.04	229.39	3
18.74	4522.04	1459.42	3062.62	2830.74	231.88	3
18.74	4522.04	1459.42	3062.62	2830.74	231.88	2
16.83	4727.55	1540.59	3186.96	2950.15	236.81	2
14.93	4932.55	1623.05	3309.50	3069.05	240.44	2
13.03	5137.04	1707.44	3429.60	3187.45	242.15	2
11.14	5341.01	1794.75	3546.26	3305.32	240.95	2
9.26	5544.43	1885.57	3658.86	3422.64	236.22	2
7.39	5747.27	1980.79	3766.48	3539.39	227.10	2
5.53	5949.52	2119.10	3830.42	3655.53	174.89	2
3.67	6151.16	2266.36	3884.80	3771.08	113.73	2
1.83	6352.21	2411.00	3941.21	3886.02	55.18	2
.00	6552.67	2551.80	4000.87	4000.38	.48	2

Time = 1440. Degree of Consolidation = 53.%

Total Settlement = 1.172

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 1440. = 1.172

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.86	4.70	2.45
3.64	3.51	1.84
2.43	2.33	1.23
1.22	1.16	.61
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.70	.00	.00
3.51	139.38	65.09
2.33	277.67	130.19
1.16	415.65	195.28
.00	553.42	260.38

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
74.28	74.28	.00	1
147.48	147.48	.00	1
220.37	220.37	.00	1
293.05	293.05	.00	1

Time = 1440. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 1440. = .164

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.12

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.23	21.42	6.50	5.75	5.71	6
60.02	58.72	21.35	6.49	5.75	5.70	6
59.45	58.21	21.27	6.47	5.76	5.69	6
58.89	57.70	21.20	6.46	5.76	5.67	6
58.33	57.19	21.12	6.44	5.76	5.66	6
57.76	56.68	21.05	6.43	5.76	5.64	6
57.20	56.17	20.97	6.42	5.77	5.63	6
56.64	55.66	20.90	6.40	5.77	5.62	6
56.08	55.15	20.82	6.39	5.76	5.60	6
56.08	55.15	20.82	4.51	4.00	3.86	5
54.82	54.00	20.59	4.44	3.94	3.80	5
53.56	52.86	20.36	4.38	3.88	3.73	5
52.32	51.73	20.12	4.32	3.82	3.67	5
51.10	50.62	19.89	4.25	3.76	3.61	5
49.88	49.53	19.66	4.19	3.70	3.54	5
48.69	48.44	19.43	4.13	3.64	3.48	5
48.69	48.44	19.43	1.93	1.90	1.89	4
46.69	46.47	18.75	1.92	1.89	1.87	4
44.70	44.50	18.06	1.91	1.87	1.85	4
42.72	42.54	17.38	1.89	1.86	1.83	4
40.75	40.59	16.70	1.88	1.85	1.81	4
38.79	38.65	16.01	1.86	1.83	1.79	4
36.85	36.72	15.33	1.84	1.82	1.77	4
34.91	34.81	14.65	1.82	1.80	1.74	4
33.00	32.90	13.97	1.80	1.78	1.72	4
31.09	31.00	13.28	1.78	1.76	1.70	4
31.09	31.00	13.28	1.47	1.47	1.43	3
29.70	29.62	12.72	1.46	1.46	1.42	3
28.32	28.24	12.16	1.45	1.45	1.41	3
26.94	26.86	11.59	1.44	1.43	1.40	3
25.57	25.50	11.03	1.43	1.42	1.39	3
24.21	24.13	10.47	1.42	1.41	1.38	3
22.84	22.78	9.90	1.41	1.40	1.37	3
21.49	21.42	9.34	1.40	1.39	1.36	3
20.14	20.08	8.78	1.39	1.38	1.35	3
18.80	18.74	8.21	1.38	1.38	1.34	3
18.80	18.74	8.21	1.34	1.33	1.31	2
16.88	16.83	7.39	1.33	1.32	1.30	2
14.97	14.92	6.57	1.32	1.31	1.29	2
13.07	13.02	5.75	1.31	1.30	1.28	2
11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.25	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.23	553.42	249.47	303.95	293.04	10.91	6
58.72	589.86	247.88	341.98	324.86	17.12	6
58.21	626.32	246.43	379.89	356.70	23.18	6
57.70	662.80	245.20	417.61	388.56	29.04	6
57.19	699.30	244.21	455.09	420.44	34.65	6
56.68	735.81	243.53	492.28	452.33	39.95	6
56.17	772.32	243.21	529.12	484.22	44.89	6
55.66	808.84	243.29	565.55	516.12	49.43	6
55.15	845.35	243.82	601.53	548.01	53.52	6
55.15	845.35	243.82	601.53	548.01	53.52	5
54.00	942.96	266.83	676.13	619.87	56.27	5
52.86	1039.73	290.23	749.50	690.89	58.61	5
51.73	1135.65	314.05	821.60	761.06	60.54	5
50.62	1230.71	338.30	892.41	830.37	62.04	5
49.53	1324.89	362.99	961.90	898.80	63.10	5
48.44	1418.18	388.11	1030.07	966.34	63.73	5
48.44	1418.18	388.11	1030.07	966.34	63.73	4
46.47	1617.31	458.43	1158.88	1089.61	69.27	4
44.50	1815.93	520.65	1295.28	1212.37	82.91	4
42.54	2014.00	568.12	1445.88	1334.58	111.30	4
40.59	2211.49	617.59	1593.90	1456.21	137.69	4
38.65	2408.38	669.44	1738.94	1577.24	161.70	4
36.72	2604.63	724.11	1880.52	1697.63	182.89	4
34.81	2800.21	782.35	2017.86	1817.35	200.51	4
32.90	2995.07	845.08	2149.99	1936.35	213.63	4
31.00	3189.14	913.80	2275.35	2054.57	220.78	4
31.00	3189.14	913.80	2275.35	2054.57	220.78	3
29.62	3337.49	968.89	2368.59	2141.05	227.54	3
28.24	3485.47	1030.25	2455.22	2227.18	228.04	3
26.86	3633.08	1096.10	2536.99	2312.93	224.05	3
25.50	3780.33	1160.76	2619.57	2398.32	221.25	3
24.13	3927.21	1224.20	2703.01	2483.35	219.66	3
22.78	4073.75	1286.50	2787.25	2568.02	219.23	3
21.42	4219.93	1347.69	2872.24	2652.35	219.89	3
20.08	4365.77	1407.82	2957.96	2736.33	221.62	3
18.74	4511.28	1466.94	3044.34	2819.98	224.36	3
18.74	4511.28	1466.94	3044.34	2819.98	224.36	2
16.83	4716.75	1547.60	3169.15	2939.35	229.80	2
14.92	4921.71	1630.07	3291.64	3058.21	233.43	2
13.02	5126.16	1714.64	3411.51	3176.56	234.95	2
11.14	5330.08	1802.15	3527.93	3294.39	233.54	2
9.26	5533.45	1893.23	3640.23	3411.66	228.57	2
7.39	5736.25	1988.66	3747.59	3528.36	219.23	2
5.53	5938.45	2129.51	3808.94	3644.46	164.48	2
3.67	6140.06	2273.53	3866.52	3759.97	106.55	2
1.83	6341.08	2414.59	3926.49	3874.89	51.60	2
.00	6541.53	2551.83	3989.70	3989.25	.45	2

Time = 1825. Degree of Consolidation = 61.%

Total Settlement = 1.350

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 1825. = 1.350

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1
1.22	1.16	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.38	65.09	74.28	74.28	.00	1
2.33	277.67	130.19	147.48	147.48	.00	1
1.16	415.65	195.28	220.37	220.37	.00	1
.00	553.42	260.38	293.04	293.04	.00	1

Time = 1825. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 1825. = .164

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.95

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.97	21.42	6.50	5.73	5.71	6
60.02	58.46	21.35	6.49	5.72	5.70	6
59.45	57.96	21.27	6.47	5.71	5.69	6
58.89	57.45	21.20	6.46	5.70	5.67	6
58.33	56.94	21.12	6.44	5.69	5.66	6
57.76	56.44	21.05	6.43	5.69	5.64	6
57.20	55.93	20.97	6.42	5.68	5.63	6
56.64	55.43	20.90	6.40	5.67	5.62	6
56.08	54.93	20.82	6.39	5.65	5.60	6
56.08	54.93	20.82	4.51	3.91	3.86	5
54.82	53.80	20.59	4.44	3.84	3.80	5
53.56	52.68	20.36	4.38	3.78	3.73	5
52.32	51.58	20.12	4.32	3.72	3.67	5
51.10	50.49	19.89	4.25	3.65	3.61	5
49.88	49.42	19.66	4.19	3.59	3.54	5
48.69	48.36	19.43	4.13	3.53	3.48	5

48.69	48.36	19.43	1.93	1.89	1.89	4
46.69	46.39	18.75	1.92	1.88	1.87	4
44.70	44.43	18.06	1.91	1.87	1.85	4
42.72	42.48	17.38	1.89	1.85	1.83	4
40.75	40.54	16.70	1.88	1.84	1.81	4
38.79	38.60	16.01	1.86	1.82	1.79	4
36.85	36.68	15.33	1.84	1.81	1.77	4
34.91	34.77	14.65	1.82	1.79	1.74	4
33.00	32.86	13.97	1.80	1.78	1.72	4
31.09	30.97	13.28	1.78	1.76	1.70	4
31.09	30.97	13.28	1.47	1.46	1.43	3
29.70	29.59	12.72	1.46	1.45	1.42	3
28.32	28.21	12.16	1.45	1.44	1.41	3
26.94	26.84	11.59	1.44	1.43	1.40	3
25.57	25.48	11.03	1.43	1.42	1.39	3
24.21	24.12	10.47	1.42	1.41	1.38	3
22.84	22.76	9.90	1.41	1.40	1.37	3
21.49	21.41	9.34	1.40	1.39	1.36	3
20.14	20.07	8.78	1.39	1.38	1.35	3
18.80	18.73	8.21	1.38	1.37	1.34	3
18.80	18.73	8.21	1.34	1.33	1.31	2
16.88	16.82	7.39	1.33	1.32	1.30	2
14.97	14.91	6.57	1.32	1.31	1.29	2
13.07	13.02	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.97	553.42	256.46	296.97	293.04	3.92	6
58.46	589.73	258.84	330.90	324.74	6.16	6
57.96	626.01	261.32	364.69	356.39	8.30	6
57.45	662.25	263.94	398.32	388.01	10.30	6
56.94	698.45	266.72	431.73	419.60	12.14	6
56.44	734.62	269.72	464.90	451.14	13.76	6
55.93	770.73	272.95	497.79	482.63	15.15	6
55.43	806.80	276.44	530.36	514.08	16.28	6
54.93	842.82	280.24	562.59	545.48	17.11	6
54.93	842.82	280.24	562.58	545.48	17.11	5
53.80	939.08	305.42	633.66	615.99	17.67	5
52.68	1034.43	330.65	703.77	685.59	18.19	5
51.58	1128.87	355.95	772.92	754.28	18.64	5
50.49	1222.41	381.30	841.11	822.07	19.05	5
49.42	1315.04	406.67	908.36	888.95	19.42	5
48.36	1406.75	432.05	974.70	954.91	19.79	5
48.36	1406.75	432.05	974.70	954.91	19.79	4
46.39	1605.56	504.68	1100.88	1077.86	23.02	4
44.43	1803.82	551.10	1252.73	1200.26	52.46	4
42.48	2001.53	598.72	1402.81	1322.11	80.70	4
40.54	2198.66	647.95	1550.71	1443.38	107.33	4
38.60	2395.18	699.29	1695.90	1564.05	131.85	4
36.68	2591.08	753.30	1837.78	1684.09	153.69	4
34.77	2786.32	810.76	1975.56	1803.47	172.09	4
32.86	2980.84	872.78	2108.06	1922.13	185.93	4
30.97	3174.59	941.06	2233.53	2040.02	193.51	4
30.97	3174.59	941.06	2233.53	2040.02	193.51	3

29.59	3322.76	995.64	2327.12	2126.33	200.79	3
28.21	3470.58	1058.68	2411.90	2212.29	199.61	3
26.84	3618.04	1121.73	2496.31	2297.89	198.42	3
25.48	3765.15	1183.96	2581.19	2383.14	198.05	3
24.12	3911.91	1245.31	2666.60	2468.05	198.55	3
22.76	4058.33	1305.92	2752.42	2552.61	199.81	3
21.41	4204.41	1365.73	2838.68	2636.83	201.85	3
20.07	4350.16	1424.92	2925.24	2720.71	204.52	3
18.73	4495.57	1483.43	3012.14	2804.27	207.87	3
18.73	4495.57	1483.43	3012.14	2804.27	207.87	2
16.82	4700.94	1562.79	3138.15	2923.54	214.61	2
14.91	4905.81	1644.29	3261.52	3042.31	219.21	2
13.02	5110.17	1728.29	3381.88	3160.58	221.30	2
11.13	5314.01	1815.28	3498.73	3278.32	220.41	2
9.25	5517.30	1905.89	3611.41	3395.51	215.90	2
7.38	5720.03	2000.63	3719.39	3512.14	207.26	2
5.52	5922.16	2143.93	3778.23	3628.17	150.06	2
3.67	6123.72	2284.22	3839.50	3743.63	95.87	2
1.83	6324.70	2420.55	3904.15	3858.52	45.63	2
.00	6525.14	2551.88	3973.26	3972.86	.40	2

Time = 2520. Degree of Consolidation = 73.%

Total Settlement = 1.613

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 2520. = 1.613

Settlement caused by Secondary Compression at time 2520. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.86	4.70	2.45
3.64	3.51	1.84
2.43	2.33	1.23
1.22	1.16	.61
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.70	.00	.00
3.51	139.38	65.09
2.33	277.67	130.19
1.16	415.65	195.28
.00	553.42	260.38

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
74.28	74.28	.00	1
147.48	147.48	.00	1
220.37	220.37	.00	1
293.04	293.04	.00	1

Time = 2520. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 2520. = .164

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.68

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.85	21.42	6.50	5.71	5.71	6
60.02	58.34	21.35	6.49	5.70	5.70	6
59.45	57.83	21.27	6.47	5.68	5.69	6
58.89	57.33	21.20	6.46	5.67	5.67	6
58.33	56.83	21.12	6.44	5.66	5.66	6
57.76	56.32	21.05	6.43	5.64	5.64	6
57.20	55.82	20.97	6.42	5.63	5.63	6
56.64	55.32	20.90	6.40	5.61	5.62	6
56.08	54.82	20.82	6.39	5.60	5.60	6
56.08	54.82	20.82	4.51	3.86	3.86	5
54.82	53.70	20.59	4.44	3.80	3.80	5
53.56	52.60	20.36	4.38	3.73	3.73	5
52.32	51.51	20.12	4.32	3.67	3.67	5
51.10	50.43	19.89	4.25	3.61	3.61	5
49.88	49.37	19.66	4.19	3.54	3.54	5
48.69	48.32	19.43	4.13	3.48	3.48	5
48.69	48.32	19.43	1.93	1.89	1.89	4
46.69	46.36	18.75	1.92	1.88	1.87	4
44.70	44.40	18.06	1.91	1.86	1.85	4
42.72	42.45	17.38	1.89	1.85	1.83	4
40.75	40.51	16.70	1.88	1.83	1.81	4
38.79	38.58	16.01	1.86	1.82	1.79	4
36.85	36.65	15.33	1.84	1.81	1.77	4
34.91	34.74	14.65	1.82	1.79	1.74	4
33.00	32.85	13.97	1.80	1.77	1.72	4
31.09	30.96	13.28	1.78	1.75	1.70	4
31.09	30.96	13.28	1.47	1.46	1.43	3
29.70	29.58	12.72	1.46	1.45	1.42	3
28.32	28.20	12.16	1.45	1.44	1.41	3
26.94	26.83	11.59	1.44	1.43	1.40	3
25.57	25.47	11.03	1.43	1.42	1.39	3
24.21	24.11	10.47	1.42	1.41	1.38	3
22.84	22.75	9.90	1.41	1.40	1.37	3
21.49	21.40	9.34	1.40	1.39	1.36	3
20.14	20.06	8.78	1.39	1.38	1.35	3
18.80	18.72	8.21	1.38	1.37	1.34	3
18.80	18.72	8.21	1.34	1.33	1.31	2
16.88	16.81	7.39	1.33	1.32	1.30	2
14.97	14.91	6.57	1.32	1.31	1.29	2
13.07	13.01	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2

1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.85	553.42	260.38	293.04	293.04	.00	6
58.34	589.66	265.00	324.66	324.66	.00	6
57.83	625.83	269.62	356.21	356.21	.00	6
57.33	661.93	274.24	387.69	387.69	.00	6
56.83	697.97	278.86	419.11	419.11	.00	6
56.32	733.94	283.48	450.46	450.46	.00	6
55.82	769.85	288.10	481.75	481.75	.00	6
55.32	805.69	292.72	512.97	512.97	.00	6
54.82	841.46	297.34	544.12	544.12	.00	6
54.82	841.46	297.34	544.12	544.12	.00	5
53.70	937.09	323.09	614.00	614.00	.00	5
52.60	1031.79	348.84	682.95	682.95	.00	5
51.51	1125.58	374.59	750.98	750.98	.00	5
50.43	1218.43	400.34	818.09	818.09	.00	5
49.37	1310.37	426.09	884.28	884.28	.00	5
48.32	1401.38	451.84	949.54	949.54	.00	5
48.32	1401.38	451.84	949.54	949.54	.00	4
46.36	1600.03	517.61	1082.43	1072.34	10.09	4
44.40	1798.14	564.40	1233.75	1194.58	39.16	4
42.45	1995.69	612.12	1383.57	1316.27	67.30	4
40.51	2192.66	661.44	1531.21	1437.38	93.83	4
38.58	2389.02	712.94	1676.08	1557.89	118.20	4
36.65	2584.76	767.11	1817.65	1677.76	139.89	4
34.74	2779.83	824.73	1955.10	1796.97	158.12	4
32.85	2974.19	887.11	2087.07	1915.47	171.60	4
30.96	3167.76	956.27	2211.49	2033.19	178.30	4
30.96	3167.76	956.27	2211.49	2033.19	178.30	3
29.58	3315.83	1011.65	2304.19	2119.40	184.79	3
28.20	3463.56	1074.16	2389.40	2205.27	184.13	3
26.83	3610.94	1135.98	2474.96	2290.79	184.17	3
25.47	3757.97	1197.05	2560.92	2375.96	184.96	3
24.11	3904.66	1257.50	2647.16	2460.79	186.36	3
22.75	4051.01	1317.30	2733.72	2545.29	188.43	3
21.40	4197.03	1376.41	2820.62	2629.45	191.18	3
20.06	4342.72	1434.93	2907.79	2713.28	194.51	3
18.72	4488.08	1493.01	2995.06	2796.78	198.29	3
18.72	4488.08	1493.01	2995.06	2796.78	198.29	2
16.81	4693.39	1571.53	3121.85	2915.99	205.87	2
14.91	4898.21	1652.48	3245.73	3034.71	211.02	2
13.01	5102.52	1735.93	3366.59	3152.93	213.66	2
11.13	5306.32	1822.38	3483.93	3270.62	213.31	2
9.25	5509.57	1912.45	3597.12	3387.78	209.34	2
7.38	5712.25	2008.97	3703.28	3504.36	198.92	2
5.52	5914.36	2150.49	3763.87	3620.37	143.50	2
3.67	6115.89	2288.50	3827.39	3735.80	91.59	2
1.83	6316.86	2422.66	3894.21	3850.68	43.53	2
.00	6517.29	2551.90	3965.40	3965.01	.38	2

Time = 2880. Degree of Consolidation = 79.%

Total Settlement = 1.739

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 2880. = 1.738

Settlement caused by Secondary Compression at time 2880. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1
1.22	1.16	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.38	65.09	74.28	74.28	.00	1
2.33	277.67	130.19	147.48	147.48	.00	1
1.16	415.65	195.28	220.37	220.37	.00	1
.00	553.42	260.38	293.04	293.04	.00	1

Time = 2880. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 2880. = .164

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.56

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.81	21.42	6.50	5.71	5.71	6
60.02	58.30	21.35	6.49	5.70	5.70	6
59.45	57.80	21.27	6.47	5.68	5.69	6
58.89	57.29	21.20	6.46	5.67	5.67	6
58.33	56.79	21.12	6.44	5.65	5.66	6
57.76	56.29	21.05	6.43	5.64	5.64	6
57.20	55.79	20.97	6.42	5.63	5.63	6
56.64	55.29	20.90	6.40	5.61	5.62	6
56.08	54.79	20.82	6.39	5.60	5.60	6
56.08	54.79	20.82	4.51	3.86	3.86	5
54.82	53.67	20.59	4.44	3.80	3.80	5

53.56	52.56	20.36	4.38	3.73	3.73	5
52.32	51.47	20.12	4.32	3.67	3.67	5
51.10	50.40	19.89	4.25	3.61	3.61	5
49.88	49.34	19.66	4.19	3.54	3.54	5
48.69	48.29	19.43	4.13	3.48	3.48	5
48.69	48.29	19.43	1.93	1.89	1.89	4
46.69	46.32	18.75	1.92	1.87	1.87	4
44.70	44.36	18.06	1.91	1.86	1.85	4
42.72	42.42	17.38	1.89	1.85	1.83	4
40.75	40.48	16.70	1.88	1.83	1.81	4
38.79	38.55	16.01	1.86	1.82	1.79	4
36.85	36.63	15.33	1.84	1.80	1.77	4
34.91	34.72	14.65	1.82	1.79	1.74	4
33.00	32.83	13.97	1.80	1.77	1.72	4
31.09	30.94	13.28	1.78	1.75	1.70	4
31.09	30.94	13.28	1.47	1.45	1.43	3
29.70	29.56	12.72	1.46	1.45	1.42	3
28.32	28.19	12.16	1.45	1.44	1.41	3
26.94	26.82	11.59	1.44	1.43	1.40	3
25.57	25.45	11.03	1.43	1.42	1.39	3
24.21	24.10	10.47	1.42	1.41	1.38	3
22.84	22.74	9.90	1.41	1.40	1.37	3
21.49	21.40	9.34	1.40	1.39	1.36	3
20.14	20.05	8.78	1.39	1.38	1.35	3
18.80	18.72	8.21	1.38	1.37	1.34	3
18.80	18.72	8.21	1.34	1.33	1.31	2
16.88	16.81	7.39	1.33	1.32	1.30	2
14.97	14.90	6.57	1.32	1.31	1.29	2
13.07	13.01	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.81	553.42	260.38	293.04	293.04	.00	6
58.30	589.65	265.00	324.65	324.65	.00	6
57.80	625.81	269.62	356.19	356.19	.00	6
57.29	661.90	274.24	387.67	387.67	.00	6
56.79	697.93	278.86	419.07	419.07	.00	6
56.29	733.89	283.48	450.41	450.41	.00	6
55.79	769.79	288.10	481.69	481.69	.00	6
55.29	805.62	292.72	512.90	512.90	.00	6
54.79	841.38	297.34	544.04	544.04	.00	6
54.79	841.38	297.34	544.04	544.04	.00	5
53.67	937.01	323.09	613.92	613.92	.00	5
52.56	1031.70	348.84	682.86	682.86	.00	5
51.47	1125.48	374.59	750.89	750.89	.00	5
50.40	1218.33	400.34	817.99	817.99	.00	5
49.34	1310.25	426.09	884.16	884.16	.00	5
48.29	1401.26	451.84	949.41	949.41	.00	5
48.29	1401.26	451.84	949.41	949.41	.00	4
46.32	1599.89	520.97	1078.92	1072.19	6.73	4
44.36	1797.94	570.92	1227.02	1194.38	32.64	4
42.42	1995.39	621.19	1374.21	1315.98	58.23	4
40.48	2192.24	672.34	1519.90	1436.96	82.93	4
38.55	2388.47	725.04	1663.43	1557.33	106.10	4

36.63	2584.06	780.11	1803.95	1677.06	126.89	4
34.72	2778.97	838.53	1940.44	1796.11	144.33	4
32.83	2973.15	901.85	2071.31	1914.44	156.87	4
30.94	3166.54	972.47	2194.07	2031.97	162.10	4
30.94	3166.54	972.47	2194.07	2031.97	162.10	3
29.56	3314.52	1029.23	2285.29	2118.08	167.20	3
28.19	3462.15	1090.31	2371.84	2203.86	167.98	3
26.82	3609.44	1150.78	2458.66	2289.29	169.37	3
25.45	3756.39	1210.79	2545.60	2374.38	171.22	3
24.10	3903.01	1270.27	2632.74	2459.14	173.59	3
22.74	4049.29	1329.16	2720.13	2543.57	176.57	3
21.40	4195.24	1387.58	2807.66	2627.66	180.00	3
20.05	4340.87	1445.52	2895.35	2711.43	183.93	3
18.72	4486.17	1503.05	2983.12	2794.87	188.25	3
18.72	4486.17	1503.05	2983.12	2794.87	188.25	2
16.81	4691.42	1580.47	3110.95	2914.02	196.92	2
14.90	4896.19	1660.79	3235.40	3032.69	202.71	2
13.01	5100.46	1743.65	3356.81	3150.86	205.94	2
11.13	5304.20	1829.51	3474.69	3268.51	206.18	2
9.25	5507.41	1919.00	3588.41	3385.62	202.79	2
7.38	5710.06	2017.30	3692.76	3502.17	190.59	2
5.52	5912.13	2157.04	3755.09	3618.15	136.94	2
3.67	6113.64	2292.77	3820.87	3733.56	87.32	2
1.83	6314.60	2424.75	3889.85	3848.42	41.43	2
.00	6515.03	2551.91	3963.12	3962.75	.37	2

Time = 3240. Degree of Consolidation = 81.%

Total Settlement = 1.775

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 3240. = 1.772

Settlement caused by Secondary Compression at time 3240. = .003

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.86	4.70	2.45
3.64	3.51	1.84
2.43	2.33	1.23
1.22	1.16	.61
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.70	.00	.00
3.51	139.38	65.09
2.33	277.67	130.19
1.16	415.65	195.28
.00	553.42	260.38

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
74.28	74.28	.00	1
147.48	147.48	.00	1
220.37	220.37	.00	1
293.04	293.04	.00	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 3240. = .164

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.52

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.77	21.42	6.50	5.71	5.71	6
60.02	58.27	21.35	6.49	5.69	5.70	6
59.45	57.76	21.27	6.47	5.68	5.69	6
58.89	57.26	21.20	6.46	5.67	5.67	6
58.33	56.75	21.12	6.44	5.65	5.66	6
57.76	56.25	21.05	6.43	5.64	5.64	6
57.20	55.75	20.97	6.42	5.62	5.63	6
56.64	55.25	20.90	6.40	5.61	5.62	6
56.08	54.75	20.82	6.39	5.60	5.60	6
56.08	54.75	20.82	4.51	3.86	3.86	5
54.82	53.63	20.59	4.44	3.80	3.80	5
53.56	52.53	20.36	4.38	3.73	3.73	5
52.32	51.44	20.12	4.32	3.67	3.67	5
51.10	50.36	19.89	4.25	3.61	3.61	5
49.88	49.30	19.66	4.19	3.54	3.54	5
48.69	48.26	19.43	4.13	3.48	3.48	5
48.69	48.26	19.43	1.93	1.89	1.89	4
46.69	46.29	18.75	1.92	1.87	1.87	4
44.70	44.33	18.06	1.91	1.86	1.85	4
42.72	42.38	17.38	1.89	1.84	1.83	4
40.75	40.45	16.70	1.88	1.83	1.81	4
38.79	38.52	16.01	1.86	1.81	1.79	4
36.85	36.60	15.33	1.84	1.80	1.77	4
34.91	34.70	14.65	1.82	1.78	1.74	4
33.00	32.80	13.97	1.80	1.76	1.72	4
31.09	30.92	13.28	1.78	1.74	1.70	4
31.09	30.92	13.28	1.47	1.45	1.43	3
29.70	29.54	12.72	1.46	1.44	1.42	3
28.32	28.17	12.16	1.45	1.43	1.41	3
26.94	26.80	11.59	1.44	1.42	1.40	3
25.57	25.44	11.03	1.43	1.41	1.39	3
24.21	24.09	10.47	1.42	1.40	1.38	3
22.84	22.73	9.90	1.41	1.40	1.37	3
21.49	21.39	9.34	1.40	1.39	1.36	3
20.14	20.05	8.78	1.39	1.38	1.35	3
18.80	18.71	8.21	1.38	1.37	1.34	3
18.80	18.71	8.21	1.34	1.33	1.31	2
16.88	16.80	7.39	1.33	1.32	1.30	2
14.97	14.90	6.57	1.32	1.31	1.29	2
13.07	13.01	5.75	1.31	1.30	1.28	2

11.18	11.12	4.93	1.30	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.77	553.42	260.38	293.04	293.04	.00	6
58.27	589.65	265.00	324.65	324.65	.00	6
57.76	625.80	269.62	356.18	356.18	.00	6
57.26	661.88	274.24	387.64	387.64	.00	6
56.75	697.90	278.86	419.04	419.04	.00	6
56.25	733.85	283.48	450.37	450.37	.00	6
55.75	769.74	288.10	481.64	481.64	.00	6
55.25	805.56	292.72	512.84	512.84	.00	6
54.75	841.31	297.34	543.97	543.97	.00	6
54.75	841.31	297.34	543.97	543.97	.00	5
53.63	936.93	323.09	613.84	613.84	.00	5
52.53	1031.61	348.84	682.77	682.77	.00	5
51.44	1125.38	374.59	750.79	750.79	.00	5
50.36	1218.22	400.34	817.88	817.88	.00	5
49.30	1310.14	426.09	884.05	884.05	.00	5
48.26	1401.13	451.84	949.29	949.29	.00	5
48.26	1401.13	451.84	949.29	949.29	.00	4
46.29	1599.76	523.12	1076.64	1072.06	4.58	4
44.33	1797.77	575.28	1222.49	1194.21	28.28	4
42.38	1995.16	627.68	1367.48	1315.74	51.74	4
40.45	2191.91	680.86	1511.06	1436.64	74.42	4
38.52	2388.03	735.45	1652.58	1556.89	95.69	4
36.60	2583.48	792.20	1791.29	1676.48	114.80	4
34.70	2778.24	852.26	1925.98	1795.38	130.60	4
32.80	2972.25	917.25	2055.00	1913.54	141.46	4
30.92	3165.44	989.83	2175.62	2030.87	144.75	4
30.92	3165.44	989.83	2175.62	2030.87	144.75	3
29.54	3313.31	1048.45	2264.86	2116.88	147.98	3
28.17	3460.84	1108.37	2352.46	2202.55	149.92	3
26.80	3608.03	1167.76	2440.27	2287.88	152.39	3
25.44	3754.89	1226.72	2528.17	2372.88	155.29	3
24.09	3901.42	1285.21	2616.20	2457.55	158.65	3
22.73	4047.62	1343.22	2704.40	2541.89	162.51	3
21.39	4193.49	1400.82	2792.68	2625.91	166.77	3
20.05	4339.05	1458.15	2880.90	2709.60	171.29	3
18.71	4484.28	1515.13	2969.15	2792.98	176.17	3
18.71	4484.28	1515.13	2969.15	2792.98	176.17	2
16.80	4689.46	1591.49	3097.97	2912.06	185.91	2
14.90	4894.16	1670.75	3223.41	3030.67	192.75	2
13.01	5098.37	1752.61	3345.76	3148.78	196.98	2
11.12	5302.07	1837.47	3464.60	3266.37	198.22	2
9.25	5505.23	1925.93	3579.30	3383.44	195.86	2
7.38	5707.84	2025.84	3682.00	3499.95	182.05	2
5.52	5909.88	2163.44	3746.44	3615.89	130.55	2
3.67	6111.37	2296.94	3814.43	3731.28	83.14	2
1.83	6312.32	2426.80	3885.51	3846.13	39.38	2
.00	6512.74	2551.93	3960.81	3960.46	.35	2

Time = 3650. Degree of Consolidation = 82.%

Total Settlement = 1.812

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 3650. = 1.807

Settlement caused by Secondary Compression at time 3650. = .005

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1
1.22	1.16	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.38	65.09	74.28	74.28	.00	1
2.33	277.67	130.19	147.48	147.48	.00	1
1.16	415.65	195.28	220.37	220.37	.00	1
.00	553.42	260.38	293.04	293.04	.00	1

Time = 3650. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 3650. = .164

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.48

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.72	21.42	6.50	5.71	5.71	6
60.02	58.21	21.35	6.49	5.69	5.70	6
59.45	57.71	21.27	6.47	5.68	5.69	6
58.89	57.20	21.20	6.46	5.66	5.67	6
58.33	56.70	21.12	6.44	5.65	5.66	6
57.76	56.20	21.05	6.43	5.64	5.64	6

57.20	55.70	20.97	6.42	5.62	5.63	6
56.64	55.20	20.90	6.40	5.61	5.62	6
56.08	54.70	20.82	6.39	5.59	5.60	6
56.08	54.70	20.82	4.51	3.86	3.86	5
54.82	53.58	20.59	4.44	3.80	3.80	5
53.56	52.48	20.36	4.38	3.73	3.73	5
52.32	51.39	20.12	4.32	3.67	3.67	5
51.10	50.31	19.89	4.25	3.60	3.61	5
49.88	49.25	19.66	4.19	3.54	3.54	5
48.69	48.21	19.43	4.13	3.48	3.48	5
48.69	48.21	19.43	1.93	1.89	1.89	4
46.69	46.24	18.75	1.92	1.87	1.87	4
44.70	44.28	18.06	1.91	1.86	1.85	4
42.72	42.34	17.38	1.89	1.84	1.83	4
40.75	40.40	16.70	1.88	1.83	1.81	4
38.79	38.47	16.01	1.86	1.81	1.79	4
36.85	36.56	15.33	1.84	1.79	1.77	4
34.91	34.66	14.65	1.82	1.78	1.74	4
33.00	32.77	13.97	1.80	1.76	1.72	4
31.09	30.89	13.28	1.78	1.74	1.70	4
31.09	30.89	13.28	1.47	1.45	1.43	3
29.70	29.52	12.72	1.46	1.44	1.42	3
28.32	28.15	12.16	1.45	1.43	1.41	3
26.94	26.78	11.59	1.44	1.42	1.40	3
25.57	25.42	11.03	1.43	1.41	1.39	3
24.21	24.07	10.47	1.42	1.40	1.38	3
22.84	22.72	9.90	1.41	1.39	1.37	3
21.49	21.37	9.34	1.40	1.38	1.36	3
20.14	20.03	8.78	1.39	1.37	1.35	3
18.80	18.70	8.21	1.38	1.36	1.34	3
18.80	18.70	8.21	1.34	1.33	1.31	2
16.88	16.79	7.39	1.33	1.32	1.30	2
14.97	14.89	6.57	1.32	1.31	1.29	2
13.07	13.00	5.75	1.31	1.30	1.28	2
11.18	11.12	4.93	1.30	1.29	1.27	2
9.30	9.24	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.72	553.42	260.38	293.04	293.04	.00	6
58.21	589.64	265.00	324.64	324.64	.00	6
57.71	625.78	269.62	356.16	356.16	.00	6
57.20	661.86	274.24	387.62	387.62	.00	6
56.70	697.87	278.86	419.01	419.01	.00	6
56.20	733.81	283.48	450.33	450.33	.00	6
55.70	769.69	288.10	481.59	481.59	.00	6
55.20	805.50	292.72	512.78	512.78	.00	6
54.70	841.24	297.34	543.90	543.90	.00	6
54.70	841.24	297.34	543.90	543.90	.00	5
53.58	936.84	323.09	613.75	613.75	.00	5
52.48	1031.52	348.84	682.68	682.68	.00	5
51.39	1125.27	374.59	750.68	750.68	.00	5
50.31	1218.09	400.34	817.75	817.75	.00	5
49.25	1310.00	426.09	883.91	883.91	.00	5
48.21	1400.98	451.84	949.14	949.14	.00	5
48.21	1400.98	451.84	949.14	949.14	.00	4

46.24	1599.59	525.51	1074.08	1071.89	2.19	4
44.28	1797.56	580.30	1217.26	1194.00	23.26	4
42.34	1994.87	635.37	1359.49	1315.45	44.04	4
40.40	2191.52	691.18	1500.34	1436.24	64.10	4
38.47	2387.49	748.42	1639.07	1556.36	82.72	4
36.56	2582.77	807.86	1774.91	1675.78	99.13	4
34.66	2777.33	870.71	1906.62	1794.47	112.14	4
32.77	2971.10	938.75	2032.35	1912.39	119.96	4
30.89	3164.02	1013.71	2150.31	2029.45	120.86	4
30.89	3164.02	1013.71	2150.31	2029.45	120.86	3
29.52	3311.74	1074.69	2237.05	2115.31	121.74	3
28.15	3459.12	1134.48	2324.64	2200.83	123.81	3
26.78	3606.17	1193.36	2412.81	2286.02	126.79	3
25.42	3752.88	1251.46	2501.42	2370.88	130.55	3
24.07	3899.28	1308.95	2590.33	2455.41	134.92	3
22.72	4045.35	1365.96	2679.39	2539.62	139.76	3
21.37	4191.10	1422.64	2768.46	2623.52	144.94	3
20.03	4336.53	1479.00	2857.54	2707.09	150.45	3
18.70	4481.65	1535.06	2946.59	2790.35	156.24	3
18.70	4481.65	1535.06	2946.59	2790.35	156.24	2
16.79	4686.71	1609.59	3077.13	2909.32	167.81	2
14.89	4891.31	1687.03	3204.29	3027.82	176.47	2
13.00	5095.42	1767.17	3328.25	3145.83	182.43	2
11.12	5299.04	1850.29	3448.75	3263.34	185.41	2
9.24	5502.12	1936.97	3565.16	3380.33	184.82	2
7.38	5704.67	2039.23	3665.44	3496.78	168.66	2
5.52	5906.67	2173.24	3733.43	3612.68	120.75	2
3.67	6108.12	2303.33	3804.79	3728.04	76.75	2
1.83	6309.05	2429.94	3879.11	3842.87	36.24	2
.00	6509.47	2551.96	3957.51	3957.19	.32	2

Time = 4320. Degree of Consolidation = 85.%

Total Settlement = 1.864

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 4320. = 1.857

Settlement caused by Secondary Compression at time 4320. = .007

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.86	4.70	2.45
3.64	3.51	1.84
2.43	2.33	1.23
1.22	1.16	.61
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.70	.00	.00
3.51	139.38	65.09

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
74.28	74.28	.00	1

2.33	277.67	130.19	147.48	147.48	.00	1
1.16	415.65	195.28	220.37	220.37	.00	1
.00	553.42	260.38	293.04	293.04	.00	1

Time = 4320. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 4320. = .164

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.43

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.67	21.42	6.50	5.71	5.71	6
60.02	58.17	21.35	6.49	5.69	5.70	6
59.45	57.66	21.27	6.47	5.68	5.69	6
58.89	57.16	21.20	6.46	5.66	5.67	6
58.33	56.66	21.12	6.44	5.65	5.66	6
57.76	56.15	21.05	6.43	5.63	5.64	6
57.20	55.65	20.97	6.42	5.62	5.63	6
56.64	55.15	20.90	6.40	5.61	5.62	6
56.08	54.65	20.82	6.39	5.59	5.60	6
56.08	54.65	20.82	4.51	3.86	3.86	5
54.82	53.54	20.59	4.44	3.80	3.80	5
53.56	52.43	20.36	4.38	3.73	3.73	5
52.32	51.34	20.12	4.32	3.67	3.67	5
51.10	50.27	19.89	4.25	3.60	3.61	5
49.88	49.21	19.66	4.19	3.54	3.54	5
48.69	48.16	19.43	4.13	3.48	3.48	5
48.69	48.16	19.43	1.93	1.89	1.89	4
46.69	46.19	18.75	1.92	1.87	1.87	4
44.70	44.24	18.06	1.91	1.86	1.85	4
42.72	42.29	17.38	1.89	1.84	1.83	4
40.75	40.36	16.70	1.88	1.82	1.81	4
38.79	38.44	16.01	1.86	1.81	1.79	4
36.85	36.52	15.33	1.84	1.79	1.77	4
34.91	34.62	14.65	1.82	1.77	1.74	4
33.00	32.74	13.97	1.80	1.75	1.72	4
31.09	30.87	13.28	1.78	1.73	1.70	4
31.09	30.87	13.28	1.47	1.44	1.43	3
29.70	29.49	12.72	1.46	1.43	1.42	3
28.32	28.12	12.16	1.45	1.43	1.41	3
26.94	26.76	11.59	1.44	1.42	1.40	3
25.57	25.40	11.03	1.43	1.41	1.39	3
24.21	24.05	10.47	1.42	1.40	1.38	3
22.84	22.70	9.90	1.41	1.39	1.37	3
21.49	21.36	9.34	1.40	1.38	1.36	3
20.14	20.02	8.78	1.39	1.37	1.35	3

18.80	18.69	8.21	1.38	1.36	1.34	3
18.80	18.69	8.21	1.34	1.32	1.31	2
16.88	16.78	7.39	1.33	1.31	1.30	2
14.97	14.89	6.57	1.32	1.31	1.29	2
13.07	13.00	5.75	1.31	1.30	1.28	2
11.18	11.12	4.93	1.30	1.29	1.27	2
9.30	9.24	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.67	553.42	260.38	293.04	293.04	.00	6
58.17	589.63	265.00	324.63	324.63	.00	6
57.66	625.76	269.62	356.15	356.15	.00	6
57.16	661.83	274.24	387.59	387.59	.00	6
56.66	697.83	278.86	418.97	418.97	.00	6
56.15	733.76	283.48	450.28	450.28	.00	6
55.65	769.63	288.10	481.53	481.53	.00	6
55.15	805.43	292.72	512.71	512.71	.00	6
54.65	841.17	297.34	543.83	543.83	.00	6
54.65	841.17	297.34	543.83	543.83	.00	5
53.54	936.75	323.09	613.66	613.66	.00	5
52.43	1031.41	348.84	682.57	682.57	.00	5
51.34	1125.15	374.59	750.55	750.56	.00	5
50.27	1217.96	400.34	817.62	817.62	.00	5
49.21	1309.85	426.09	883.75	883.75	.00	5
48.16	1400.81	451.84	948.97	948.97	.00	5
48.16	1400.81	451.84	948.97	948.97	.00	4
46.19	1599.41	527.43	1071.98	1071.71	.27	4
44.24	1797.34	584.20	1213.14	1193.78	19.36	4
42.29	1994.59	641.35	1353.25	1315.18	38.07	4
40.36	2191.16	699.34	1491.82	1435.88	55.94	4
38.44	2387.03	758.80	1628.23	1555.89	72.34	4
36.52	2582.17	820.56	1761.61	1675.17	86.44	4
34.62	2776.56	885.86	1890.70	1793.70	97.00	4
32.74	2970.13	956.64	2013.50	1911.42	102.08	4
30.87	3162.83	1032.80	2130.03	2028.25	101.77	4
30.87	3162.83	1032.80	2130.03	2028.25	101.77	3
29.49	3310.44	1094.96	2215.48	2114.00	101.47	3
28.12	3457.70	1155.60	2302.10	2199.41	102.69	3
26.76	3604.63	1214.91	2389.72	2284.48	105.24	3
25.40	3751.22	1273.19	2478.03	2369.21	108.82	3
24.05	3897.49	1330.66	2566.83	2453.63	113.21	3
22.70	4043.44	1387.46	2655.98	2537.72	118.26	3
21.36	4189.07	1443.73	2745.34	2621.49	123.85	3
20.02	4334.39	1499.60	2834.79	2704.95	129.85	3
18.69	4479.39	1554.98	2924.41	2788.09	136.32	3
18.69	4479.39	1554.98	2924.41	2788.09	136.32	2
16.78	4684.34	1628.01	3056.33	2906.94	149.39	2
14.89	4888.83	1703.94	3184.88	3025.33	159.55	2
13.00	5092.84	1782.38	3310.46	3143.25	167.21	2
11.12	5296.36	1863.78	3432.58	3260.67	171.91	2
9.24	5499.38	1948.58	3550.80	3377.58	173.22	2
7.38	5701.86	2053.29	3648.57	3493.97	154.60	2
5.52	5903.80	2183.54	3720.26	3609.82	110.45	2
3.67	6105.22	2310.06	3795.17	3725.14	70.03	2
1.83	6306.13	2433.25	3872.88	3839.95	32.94	2

.00	6506.54	2551.99	3954.56	3954.26	.30	2

Time = 5040. Degree of Consolidation = 87.%

Total Settlement = 1.911

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 5040. = 1.901

Settlement caused by Secondary Compression at time 5040. = .010

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1
1.22	1.16	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.38	65.09	74.28	74.28	.00	1
2.33	277.67	130.19	147.48	147.48	.00	1
1.16	415.65	195.28	220.37	220.37	.00	1
.00	553.42	260.38	293.04	293.04	.00	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 5040. = .164

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.39

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.65	21.42	6.50	5.71	5.71	6

60.02	58.14	21.35	6.49	5.69	5.70	6
59.45	57.64	21.27	6.47	5.68	5.69	6
58.89	57.13	21.20	6.46	5.66	5.67	6
58.33	56.63	21.12	6.44	5.65	5.66	6
57.76	56.13	21.05	6.43	5.63	5.64	6
57.20	55.63	20.97	6.42	5.62	5.63	6
56.64	55.13	20.90	6.40	5.61	5.62	6
56.08	54.63	20.82	6.39	5.59	5.60	6
56.08	54.63	20.82	4.51	3.86	3.86	5
54.82	53.51	20.59	4.44	3.80	3.80	5
53.56	52.41	20.36	4.38	3.73	3.73	5
52.32	51.32	20.12	4.32	3.67	3.67	5
51.10	50.24	19.89	4.25	3.60	3.61	5
49.88	49.18	19.66	4.19	3.54	3.54	5
48.69	48.14	19.43	4.13	3.48	3.48	5
48.69	48.14	19.43	1.93	1.89	1.89	4
46.69	46.17	18.75	1.92	1.87	1.87	4
44.70	44.22	18.06	1.91	1.86	1.85	4
42.72	42.27	17.38	1.89	1.84	1.83	4
40.75	40.34	16.70	1.88	1.82	1.81	4
38.79	38.41	16.01	1.86	1.81	1.79	4
36.85	36.50	15.33	1.84	1.79	1.77	4
34.91	34.61	14.65	1.82	1.77	1.74	4
33.00	32.72	13.97	1.80	1.75	1.72	4
31.09	30.85	13.28	1.78	1.73	1.70	4
31.09	30.85	13.28	1.47	1.44	1.43	3
29.70	29.48	12.72	1.46	1.43	1.42	3
28.32	28.11	12.16	1.45	1.42	1.41	3
26.94	26.75	11.59	1.44	1.41	1.40	3
25.57	25.39	11.03	1.43	1.40	1.39	3
24.21	24.04	10.47	1.42	1.40	1.38	3
22.84	22.69	9.90	1.41	1.39	1.37	3
21.49	21.35	9.34	1.40	1.38	1.36	3
20.14	20.01	8.78	1.39	1.37	1.35	3
18.80	18.68	8.21	1.38	1.36	1.34	3
18.80	18.68	8.21	1.34	1.32	1.31	2
16.88	16.78	7.39	1.33	1.31	1.30	2
14.97	14.88	6.57	1.32	1.30	1.29	2
13.07	12.99	5.75	1.31	1.30	1.28	2
11.18	11.11	4.93	1.30	1.29	1.27	2
9.30	9.24	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.25	1.25	2
3.70	3.67	1.64	1.26	1.24	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.65	553.42	260.38	293.04	293.04	.00	6
58.14	589.63	265.00	324.63	324.63	.00	6
57.64	625.75	269.62	356.14	356.14	.00	6
57.13	661.81	274.24	387.57	387.57	.00	6
56.63	697.81	278.86	418.95	418.95	.00	6
56.13	733.73	283.48	450.25	450.25	.00	6
55.63	769.60	288.10	481.50	481.50	.00	6
55.13	805.39	292.72	512.67	512.67	.00	6
54.63	841.12	297.34	543.78	543.78	.00	6
54.63	841.12	297.34	543.78	543.78	.00	5
53.51	936.70	323.09	613.61	613.61	.00	5
52.41	1031.36	348.84	682.52	682.52	.00	5

51.32	1125.09	374.59	750.50	750.50	.00	5
50.24	1217.89	400.34	817.55	817.55	.00	5
49.18	1309.77	426.09	883.68	883.68	.00	5
48.14	1400.73	451.84	948.89	948.89	.00	5
48.14	1400.73	451.84	948.89	948.89	.00	4
46.17	1599.33	527.70	1071.63	1071.63	.00	4
44.22	1797.25	585.67	1211.58	1193.69	17.89	4
42.27	1994.48	644.00	1350.48	1315.06	35.42	4
40.34	2191.00	703.16	1487.84	1435.73	52.11	4
38.41	2386.82	763.79	1623.03	1555.68	67.35	4
36.50	2581.89	826.72	1755.17	1674.90	80.27	4
34.61	2776.20	893.26	1882.95	1793.35	89.60	4
32.72	2969.68	965.43	2004.26	1910.97	93.29	4
30.85	3162.26	1042.27	2119.99	2027.69	92.30	4
30.85	3162.26	1042.27	2119.99	2027.69	92.30	3
29.48	3309.82	1105.10	2204.71	2113.39	91.33	3
28.11	3457.02	1166.30	2290.72	2198.73	91.99	3
26.75	3603.89	1226.16	2377.73	2283.74	93.99	3
25.39	3750.42	1284.85	2465.57	2368.41	97.16	3
24.04	3896.62	1342.53	2554.09	2452.76	101.34	3
22.69	4042.50	1399.35	2643.16	2536.78	106.38	3
21.35	4188.07	1455.49	2732.58	2620.49	112.10	3
20.01	4333.32	1511.05	2822.27	2703.88	118.39	3
18.68	4478.26	1566.17	2912.09	2786.96	125.13	3
18.68	4478.26	1566.17	2912.09	2786.96	125.13	2
16.78	4683.14	1638.57	3044.56	2905.74	138.82	2
14.88	4887.57	1713.63	3173.94	3024.07	149.87	2
12.99	5091.52	1791.19	3300.33	3141.93	158.41	2
11.11	5294.99	1871.71	3423.29	3259.30	163.99	2
9.24	5497.96	1955.38	3542.58	3376.17	166.41	2
7.38	5700.40	2061.54	3638.87	3492.51	146.35	2
5.52	5902.32	2189.59	3712.73	3608.33	104.40	2
3.67	6103.72	2314.02	3789.70	3723.63	66.07	2
1.83	6304.62	2435.19	3869.42	3838.43	30.99	2
.00	6505.02	2552.00	3953.02	3952.74	.28	2

Time = 5475. Degree of Consolidation = 88.%

Total Settlement = 1.935

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 5475. = 1.924

Settlement caused by Secondary Compression at time 5475. = .011

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1
1.22	1.16	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

XI	***** Stresses ***** Total	Effective	***** Pore Pressures ***** Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.38	65.09	74.28	74.28	.00	1
2.33	277.67	130.19	147.48	147.48	.00	1
1.16	415.65	195.28	220.37	220.37	.00	1
.00	553.42	260.38	293.04	293.04	.00	1

Time = 5475. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 5475. = .164

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.36

**********Current Conditions in Compressible Foundation**********

A	***** Coordinates ***** XI	Z	***** Void Ratios ***** Einitial	E	Eeop	Material
60.58	58.60	21.42	6.50	5.71	5.71	6
60.02	58.10	21.35	6.49	5.69	5.70	6
59.45	57.59	21.27	6.47	5.67	5.69	6
58.89	57.09	21.20	6.46	5.66	5.67	6
58.33	56.59	21.12	6.44	5.64	5.66	6
57.76	56.08	21.05	6.43	5.63	5.64	6
57.20	55.58	20.97	6.42	5.62	5.63	6
56.64	55.08	20.90	6.40	5.60	5.62	6
56.08	54.59	20.82	6.39	5.59	5.60	6
56.08	54.59	20.82	4.51	3.86	3.86	5
54.82	53.47	20.59	4.44	3.80	3.80	5
53.56	52.36	20.36	4.38	3.73	3.73	5
52.32	51.27	20.12	4.32	3.67	3.67	5
51.10	50.20	19.89	4.25	3.60	3.61	5
49.88	49.14	19.66	4.19	3.54	3.54	5
48.69	48.09	19.43	4.13	3.48	3.48	5
48.69	48.09	19.43	1.93	1.89	1.89	4
46.69	46.13	18.75	1.92	1.87	1.87	4
44.70	44.17	18.06	1.91	1.86	1.85	4
42.72	42.23	17.38	1.89	1.84	1.83	4
40.75	40.29	16.70	1.88	1.82	1.81	4
38.79	38.37	16.01	1.86	1.80	1.79	4
36.85	36.46	15.33	1.84	1.79	1.77	4
34.91	34.57	14.65	1.82	1.77	1.74	4
33.00	32.69	13.97	1.80	1.75	1.72	4
31.09	30.82	13.28	1.78	1.72	1.70	4
31.09	30.82	13.28	1.47	1.44	1.43	3
29.70	29.45	12.72	1.46	1.43	1.42	3
28.32	28.08	12.16	1.45	1.42	1.41	3
26.94	26.72	11.59	1.44	1.41	1.40	3

25.57	25.37	11.03	1.43	1.40	1.39	3
24.21	24.02	10.47	1.42	1.39	1.38	3
22.84	22.67	9.90	1.41	1.38	1.37	3
21.49	21.33	9.34	1.40	1.37	1.36	3
20.14	20.00	8.78	1.39	1.36	1.35	3
18.80	18.67	8.21	1.38	1.36	1.34	3
18.80	18.67	8.21	1.34	1.32	1.31	2
16.88	16.77	7.39	1.33	1.31	1.30	2
14.97	14.87	6.57	1.32	1.30	1.29	2
13.07	12.99	5.75	1.31	1.29	1.28	2
11.18	11.11	4.93	1.30	1.28	1.27	2
9.30	9.24	4.11	1.29	1.27	1.26	2
7.43	7.37	3.29	1.28	1.26	1.25	2
5.56	5.52	2.46	1.27	1.25	1.25	2
3.70	3.67	1.64	1.26	1.24	1.24	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.60	553.42	260.38	293.04	293.04	.00	6
58.10	589.62	265.00	324.62	324.62	.00	6
57.59	625.73	269.62	356.11	356.11	.00	6
57.09	661.78	274.24	387.54	387.54	.00	6
56.59	697.76	278.86	418.90	418.90	.00	6
56.08	733.67	283.48	450.19	450.19	.00	6
55.58	769.52	288.10	481.42	481.42	.00	6
55.08	805.30	292.72	512.58	512.58	.00	6
54.59	841.02	297.34	543.67	543.67	.00	6
54.59	841.02	297.34	543.67	543.67	.00	5
53.47	936.60	323.09	613.51	613.51	.00	5
52.36	1031.25	348.84	682.41	682.41	.00	5
51.27	1124.98	374.59	750.39	750.39	.00	5
50.20	1217.79	400.34	817.45	817.45	.00	5
49.14	1309.67	426.09	883.58	883.58	.00	5
48.09	1400.62	451.84	948.78	948.78	.00	5
48.09	1400.62	451.84	948.78	948.78	.00	4
46.13	1599.22	527.70	1071.52	1071.53	.00	4
44.17	1797.13	587.60	1209.53	1193.58	15.96	4
42.23	1994.33	647.94	1346.39	1314.91	31.48	4
40.29	2190.80	709.24	1481.56	1435.52	46.04	4
38.37	2386.52	772.08	1614.44	1555.39	59.05	4
36.46	2581.49	837.36	1744.13	1674.49	69.64	4
34.57	2775.65	906.45	1869.21	1792.80	76.41	4
32.69	2968.96	981.60	1987.35	1910.24	77.11	4
30.82	3161.33	1060.07	2101.26	2026.76	74.51	4
30.82	3161.33	1060.07	2101.26	2026.76	74.51	3
29.45	3308.78	1124.41	2184.37	2112.35	72.02	3
28.08	3455.87	1186.79	2269.08	2197.58	71.50	3
26.72	3602.62	1247.55	2355.07	2282.47	72.60	3
25.37	3749.03	1306.92	2442.10	2367.02	75.08	3
24.02	3895.11	1365.09	2530.02	2451.24	78.78	3
22.67	4040.86	1422.19	2618.67	2535.14	83.54	3
21.33	4186.30	1478.38	2707.92	2618.71	89.20	3
20.00	4331.42	1533.80	2797.62	2701.98	95.64	3
18.67	4476.23	1588.58	2887.65	2784.93	102.72	3
18.67	4476.23	1588.58	2887.65	2784.93	102.72	2
16.77	4680.98	1660.17	3020.80	2903.58	117.22	2
14.87	4885.27	1733.93	3151.34	3021.78	129.56	2
12.99	5089.11	1810.23	3278.88	3139.51	139.37	2
11.11	5292.47	1889.10	3403.37	3256.78	146.59	2

9.24	5495.33	1970.51	3524.82	3373.54	151.28	2
7.37	5697.69	2080.21	3617.48	3489.80	127.68	2
5.52	5899.54	2203.38	3696.16	3605.56	90.60	2
3.67	6100.90	2323.18	3777.72	3720.81	56.91	2
1.83	6301.76	2439.69	3862.07	3835.58	26.49	2
.00	6502.16	2552.04	3950.12	3949.88	.24	2

Time = 6480. Degree of Consolidation = 90.%

Total Settlement = 1.981

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 6480. = 1.968

Settlement caused by Secondary Compression at time 6480. = .013

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1
2.43	2.33	1.23	.98	.91	.91	1
1.22	1.16	.61	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.38	65.09	74.28	74.28	.00	1
2.33	277.67	130.19	147.48	147.48	.00	1
1.16	415.65	195.28	220.37	220.37	.00	1
.00	553.42	260.38	293.04	293.04	.00	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 6480. = .164

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.32

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.57	21.42	6.50	5.71	5.71	6
60.02	58.07	21.35	6.49	5.68	5.70	6
59.45	57.56	21.27	6.47	5.67	5.69	6
58.89	57.06	21.20	6.46	5.66	5.67	6
58.33	56.56	21.12	6.44	5.64	5.66	6
57.76	56.06	21.05	6.43	5.63	5.64	6
57.20	55.55	20.97	6.42	5.61	5.63	6
56.64	55.06	20.90	6.40	5.60	5.62	6
56.08	54.56	20.82	6.39	5.59	5.60	6
56.08	54.56	20.82	4.51	3.86	3.86	5
54.82	53.44	20.59	4.44	3.80	3.80	5
53.56	52.33	20.36	4.38	3.73	3.73	5
52.32	51.24	20.12	4.32	3.67	3.67	5
51.10	50.17	19.89	4.25	3.60	3.61	5
49.88	49.11	19.66	4.19	3.54	3.54	5
48.69	48.07	19.43	4.13	3.48	3.48	5
48.69	48.07	19.43	1.93	1.89	1.89	4
46.69	46.10	18.75	1.92	1.87	1.87	4
44.70	44.14	18.06	1.91	1.86	1.85	4
42.72	42.20	17.38	1.89	1.84	1.83	4
40.75	40.27	16.70	1.88	1.82	1.81	4
38.79	38.35	16.01	1.86	1.80	1.79	4
36.85	36.44	15.33	1.84	1.78	1.77	4
34.91	34.54	14.65	1.82	1.76	1.74	4
33.00	32.66	13.97	1.80	1.74	1.72	4
31.09	30.80	13.28	1.78	1.72	1.70	4
31.09	30.80	13.28	1.47	1.44	1.43	3
29.70	29.43	12.72	1.46	1.43	1.42	3
28.32	28.06	12.16	1.45	1.42	1.41	3
26.94	26.70	11.59	1.44	1.41	1.40	3
25.57	25.35	11.03	1.43	1.40	1.39	3
24.21	24.00	10.47	1.42	1.39	1.38	3
22.84	22.66	9.90	1.41	1.38	1.37	3
21.49	21.32	9.34	1.40	1.37	1.36	3
20.14	19.99	8.78	1.39	1.36	1.35	3
18.80	18.66	8.21	1.38	1.35	1.34	3
18.80	18.66	8.21	1.34	1.32	1.31	2
16.88	16.76	7.39	1.33	1.31	1.30	2
14.97	14.87	6.57	1.32	1.30	1.29	2
13.07	12.98	5.75	1.31	1.29	1.28	2
11.18	11.10	4.93	1.30	1.28	1.27	2
9.30	9.23	4.11	1.29	1.27	1.26	2
7.43	7.37	3.29	1.28	1.26	1.25	2
5.56	5.52	2.46	1.27	1.25	1.25	2
3.70	3.67	1.64	1.26	1.24	1.24	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.57	553.42	260.38	293.04	293.04	.00	6
58.07	589.61	265.00	324.61	324.61	.00	6
57.56	625.71	269.62	356.09	356.09	.00	6
57.06	661.75	274.24	387.51	387.51	.00	6
56.56	697.72	278.86	418.86	418.86	.00	6
56.06	733.62	283.48	450.14	450.14	.00	6
55.55	769.45	288.10	481.35	481.35	.00	6

55.06	805.22	292.72	512.50	512.50	.00	6
54.56	840.93	297.34	543.59	543.59	.00	6
54.56	840.93	297.34	543.59	543.59	.00	5
53.44	936.51	323.09	613.42	613.42	.00	5
52.33	1031.17	348.84	682.32	682.32	.00	5
51.24	1124.90	374.59	750.30	750.30	.00	5
50.17	1217.70	400.34	817.36	817.36	.00	5
49.11	1309.58	426.09	883.49	883.49	.00	5
48.07	1400.54	451.84	948.69	948.69	.00	5
48.07	1400.54	451.84	948.69	948.69	.00	4
46.10	1599.14	527.70	1071.44	1071.44	.00	4
44.14	1797.04	588.66	1208.39	1193.48	14.90	4
42.20	1994.22	650.14	1344.08	1314.80	29.28	4
40.27	2190.65	712.63	1478.02	1435.37	42.65	4
38.35	2386.33	776.78	1609.55	1555.19	54.36	4
36.44	2581.23	843.51	1737.72	1674.23	63.49	4
34.54	2775.31	914.20	1861.11	1792.46	68.66	4
32.66	2968.51	991.30	1977.21	1909.80	67.41	4
30.80	3160.76	1070.92	2089.84	2026.19	63.65	4
30.80	3160.76	1070.92	2089.84	2026.19	63.65	3
29.43	3308.15	1136.38	2171.76	2111.71	60.05	3
28.06	3455.17	1199.73	2255.44	2196.88	58.56	3
26.70	3601.84	1261.30	2340.54	2281.69	58.85	3
25.35	3748.17	1321.29	2426.88	2366.16	60.72	3
24.00	3894.17	1379.84	2514.32	2450.30	64.02	3
22.66	4039.84	1437.13	2602.71	2534.11	68.60	3
21.32	4185.19	1493.32	2691.87	2617.61	74.26	3
19.99	4330.23	1548.74	2781.49	2700.79	80.70	3
18.66	4474.96	1603.49	2871.47	2783.66	87.81	3
18.66	4474.96	1603.49	2871.47	2783.66	87.81	2
16.76	4679.61	1675.11	3004.50	2902.21	102.28	2
14.87	4883.81	1748.87	3134.94	3020.32	114.62	2
12.98	5087.56	1824.38	3263.18	3137.97	125.22	2
11.10	5290.84	1901.96	3388.88	3255.14	133.73	2
9.23	5493.63	1982.07	3511.56	3371.84	139.72	2
7.37	5695.92	2095.15	3600.77	3488.03	112.73	2
5.52	5897.72	2214.49	3683.22	3603.73	79.49	2
3.67	6099.03	2330.65	3768.39	3718.95	49.44	2
1.83	6299.88	2443.36	3856.52	3833.69	22.82	2
.00	6500.27	2552.07	3948.20	3947.99	.21	2

Time = 7300. Degree of Consolidation = 91.%

Total Settlement = 2.011

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 7300. = 1.997

Settlement caused by Secondary Compression at time 7300. = .014

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
4.86	4.70	2.45	.98	.98	.98	1
3.64	3.51	1.84	.98	.92	.92	1

2.43	2.33	1.23	.98	.91	1
1.22	1.16	.61	.98	.90	1
.00	.00	.00	.98	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
4.70	.00	.00	.00	.00	.00	1
3.51	139.38	65.09	74.28	74.28	.00	1
2.33	277.67	130.19	147.48	147.48	.00	1
1.16	415.65	195.28	220.37	220.37	.00	1
.00	553.42	260.38	293.04	293.04	.00	1

Time = 7300. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 7300. = .164

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.28

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.52	21.42	6.50	5.71	5.71	6
60.02	58.02	21.35	6.49	5.68	5.70	6
59.45	57.51	21.27	6.47	5.66	5.69	6
58.89	57.01	21.20	6.46	5.65	5.67	6
58.33	56.51	21.12	6.44	5.64	5.66	6
57.76	56.01	21.05	6.43	5.62	5.64	6
57.20	55.51	20.97	6.42	5.61	5.63	6
56.64	55.01	20.90	6.40	5.59	5.62	6
56.08	54.51	20.82	6.39	5.58	5.60	6
56.08	54.51	20.82	4.51	3.86	3.86	5
54.82	53.39	20.59	4.44	3.80	3.80	5
53.56	52.29	20.36	4.38	3.73	3.73	5
52.32	51.20	20.12	4.32	3.67	3.67	5
51.10	50.12	19.89	4.25	3.60	3.61	5
49.88	49.06	19.66	4.19	3.54	3.54	5
48.69	48.02	19.43	4.13	3.48	3.48	5
48.69	48.02	19.43	1.93	1.89	1.89	4
46.69	46.05	18.75	1.92	1.87	1.87	4
44.70	44.09	18.06	1.91	1.85	1.85	4
42.72	42.15	17.38	1.89	1.84	1.83	4
40.75	40.22	16.70	1.88	1.82	1.81	4
38.79	38.30	16.01	1.86	1.80	1.79	4
36.85	36.39	15.33	1.84	1.78	1.77	4
34.91	34.50	14.65	1.82	1.76	1.74	4
33.00	32.62	13.97	1.80	1.74	1.72	4

31.09	30.76	13.28	1.78	1.71	1.70	4
31.09	30.76	13.28	1.47	1.44	1.43	3
29.70	29.39	12.72	1.46	1.43	1.42	3
28.32	28.03	12.16	1.45	1.41	1.41	3
26.94	26.67	11.59	1.44	1.40	1.40	3
25.57	25.32	11.03	1.43	1.39	1.39	3
24.21	23.97	10.47	1.42	1.39	1.38	3
22.84	22.63	9.90	1.41	1.38	1.37	3
21.49	21.30	9.34	1.40	1.37	1.36	3
20.14	19.97	8.78	1.39	1.36	1.35	3
18.80	18.64	8.21	1.38	1.35	1.34	3
18.80	18.64	8.21	1.34	1.31	1.31	2
16.88	16.74	7.39	1.33	1.31	1.30	2
14.97	14.85	6.57	1.32	1.30	1.29	2
13.07	12.97	5.75	1.31	1.29	1.28	2
11.18	11.10	4.93	1.30	1.28	1.27	2
9.30	9.23	4.11	1.29	1.27	1.26	2
7.43	7.37	3.29	1.28	1.26	1.25	2
5.56	5.52	2.46	1.27	1.25	1.25	2
3.70	3.67	1.64	1.26	1.24	1.24	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.52	553.42	260.38	293.04	293.04	.00	6
58.02	589.60	265.00	324.60	324.60	.00	6
57.51	625.67	269.62	356.05	356.05	.00	6
57.01	661.68	274.24	387.44	387.44	.00	6
56.51	697.62	278.86	418.76	418.76	.00	6
56.01	733.50	283.48	450.02	450.02	.00	6
55.51	769.31	288.10	481.21	481.21	.00	6
55.01	805.06	292.72	512.34	512.34	.00	6
54.51	840.74	297.34	543.40	543.40	.00	6
54.51	840.74	297.34	543.40	543.40	.00	5
53.39	936.32	323.09	613.23	613.23	.00	5
52.29	1030.97	348.84	682.13	682.13	.00	5
51.20	1124.70	374.59	750.11	750.11	.00	5
50.12	1217.51	400.34	817.17	817.17	.00	5
49.06	1309.39	426.09	883.30	883.30	.00	5
48.02	1400.34	451.84	948.50	948.50	.00	5
48.02	1400.34	451.84	948.50	948.50	.00	4
46.05	1598.95	527.70	1071.25	1071.25	.00	4
44.09	1796.84	590.29	1206.55	1193.29	13.27	4
42.15	1993.99	653.57	1340.42	1314.57	25.85	4
40.22	2190.37	717.98	1472.39	1435.09	37.30	4
38.30	2385.97	784.27	1601.71	1554.84	46.87	4
36.39	2580.77	853.44	1727.33	1673.77	53.56	4
34.50	2774.72	927.00	1847.72	1791.86	55.86	4
32.62	2967.74	1007.05	1960.70	1909.03	51.67	4
30.76	3159.79	1088.61	2071.18	2025.21	45.97	4
30.76	3159.79	1088.61	2071.18	2025.21	45.97	3
29.39	3307.07	1155.92	2151.15	2110.63	40.51	3
28.03	3453.97	1220.92	2233.05	2195.68	37.37	3
26.67	3600.52	1283.93	2316.60	2280.37	36.22	3
25.32	3746.72	1345.12	2401.60	2364.71	36.89	3
23.97	3892.58	1404.68	2487.90	2448.72	39.18	3
22.63	4038.11	1462.77	2575.34	2532.39	42.96	3
21.30	4183.32	1519.53	2663.78	2615.73	48.05	3
19.97	4328.21	1575.13	2753.08	2698.76	54.32	3
18.64	4472.79	1629.69	2843.10	2781.49	61.61	3

18.64	4472.79	1629.69	2843.10	2781.49	61.61	2
16.74	4677.28	1701.19	2976.09	2899.88	76.21	2
14.85	4881.33	1773.92	3107.40	3017.83	89.57	2
12.97	5084.92	1848.41	3236.51	3135.33	101.19	2
11.10	5288.05	1924.80	3363.25	3252.36	110.89	2
9.23	5490.71	2004.05	3486.66	3368.92	117.74	2
7.37	5692.89	2120.45	3572.43	3485.00	87.44	2
5.52	5894.59	2233.63	3660.97	3600.60	60.36	2
3.67	6095.84	2343.75	3752.09	3715.75	36.34	2
1.83	6296.65	2449.80	3846.85	3830.46	16.39	2
.00	6497.02	2552.12	3944.90	3944.74	.16	2

Time = 9125. Degree of Consolidation = 94.%

Total Settlement = 2.063

Settlement at End of Primary Consolidation = 2.200

Settlement caused by Primary Consolidation at time 9125. = 2.046

Settlement caused by Secondary Compression at time 9125. = .017

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.86	4.70	2.45
3.64	3.51	1.84
2.43	2.33	1.23
1.22	1.16	.61
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.70	.00	.00
3.51	139.38	65.09
2.33	277.67	130.19
1.16	415.65	195.28
.00	553.42	260.38

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
74.28	74.28	.00	1
147.48	147.48	.00	1
220.37	220.37	.00	1
293.04	293.04	.00	1

Time = 9125. Degree of Consolidation = 100.%

Total Settlement = .164

Settlement at End of Primary Consolidation = .164

Settlement caused by Primary Consolidation at time 9125. = .164

Settlement caused by Secondary Compression at time 9125. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.23

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou Dupont - 4ft fill with Equivalent fill height of 7.0 f

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	7.0	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.342	.570	.30000E-03	z = .06

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	5.36	6
60.02	60.02	21.35	6.49	6.49	5.35	6
59.45	59.45	21.27	6.47	6.47	5.33	6
58.89	58.89	21.20	6.46	6.46	5.32	6

58.33	58.33	21.12	6.44	6.44	5.31	6
57.76	57.76	21.05	6.43	6.43	5.29	6
57.20	57.20	20.97	6.42	6.42	5.28	6
56.64	56.64	20.90	6.40	6.40	5.26	6
56.08	56.08	20.82	6.39	6.39	5.25	6
56.08	56.08	20.82	4.51	4.51	3.57	5
54.82	54.82	20.59	4.44	4.44	3.51	5
53.56	53.56	20.36	4.38	4.38	3.45	5
52.32	52.32	20.12	4.32	4.32	3.38	5
51.10	51.10	19.89	4.25	4.25	3.34	5
49.88	49.88	19.66	4.19	4.19	3.31	5
48.69	48.69	19.43	4.13	4.13	3.28	5
48.69	48.69	19.43	1.93	1.93	1.86	4
46.69	46.69	18.75	1.92	1.92	1.84	4
44.70	44.70	18.06	1.91	1.91	1.82	4
42.72	42.72	17.38	1.89	1.89	1.80	4
40.75	40.75	16.70	1.88	1.88	1.78	4
38.79	38.79	16.01	1.86	1.86	1.75	4
36.85	36.85	15.33	1.84	1.84	1.73	4
34.91	34.91	14.65	1.82	1.82	1.71	4
33.00	33.00	13.97	1.80	1.80	1.69	4
31.09	31.09	13.28	1.78	1.78	1.67	4
31.09	31.09	13.28	1.47	1.47	1.41	3
29.70	29.70	12.72	1.46	1.46	1.40	3
28.32	28.32	12.16	1.45	1.45	1.39	3
26.94	26.94	11.59	1.44	1.44	1.38	3
25.57	25.57	11.03	1.43	1.43	1.37	3
24.21	24.21	10.47	1.42	1.42	1.36	3
22.84	22.84	9.90	1.41	1.41	1.35	3
21.49	21.49	9.34	1.40	1.40	1.34	3
20.14	20.14	8.78	1.39	1.39	1.33	3
18.80	18.80	8.21	1.38	1.38	1.32	3
18.80	18.80	8.21	1.34	1.34	1.29	2
16.88	16.88	7.39	1.33	1.33	1.28	2
14.97	14.97	6.57	1.32	1.32	1.27	2
13.07	13.07	5.75	1.31	1.31	1.26	2
11.18	11.18	4.93	1.30	1.30	1.26	2
9.30	9.30	4.11	1.29	1.29	1.25	2
7.43	7.43	3.29	1.28	1.28	1.24	2
5.56	5.56	2.46	1.27	1.27	1.24	2
3.70	3.70	1.64	1.26	1.26	1.23	2
1.85	1.85	.82	1.25	1.25	1.22	2
.00	.00	.00	1.25	1.25	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	815.31	.00	815.31	438.67	376.64	6
60.02	855.26	4.62	850.64	474.00	376.64	6
59.45	895.14	9.24	885.90	509.26	376.64	6
58.89	934.95	13.86	921.09	544.46	376.64	6
58.33	974.70	18.48	956.22	579.59	376.64	6
57.76	1014.39	23.10	991.29	614.65	376.64	6
57.20	1054.01	27.72	1026.29	649.65	376.64	6
56.64	1093.56	32.34	1061.22	684.58	376.64	6
56.08	1133.05	36.96	1096.08	719.45	376.64	6
56.08	1133.05	36.96	1096.08	719.45	376.64	5
54.82	1238.02	62.71	1175.31	798.67	376.64	5
53.56	1342.07	88.46	1253.61	876.97	376.64	5
52.32	1445.19	114.21	1330.98	954.34	376.64	5
51.10	1547.40	139.96	1407.43	1030.80	376.64	5
49.88	1648.67	165.71	1482.96	1106.32	376.64	5

48.69	1749.03	191.46	1557.57	1180.93	376.64	5
48.69	1749.03	191.46	1557.57	1180.93	376.64	4
46.69	1949.47	267.32	1682.15	1305.51	376.64	4
44.70	2149.41	343.18	1806.23	1429.59	376.64	4
42.72	2348.81	419.04	1929.77	1553.13	376.64	4
40.75	2547.75	494.90	2052.85	1676.22	376.64	4
38.79	2745.95	570.76	2175.19	1798.55	376.64	4
36.85	2943.25	646.62	2296.63	1919.99	376.64	4
34.91	3139.65	722.48	2417.17	2040.53	376.64	4
33.00	3335.14	798.34	2536.80	2160.16	376.64	4
31.09	3529.72	874.19	2655.53	2278.89	376.64	4
31.09	3529.72	874.19	2655.53	2278.89	376.64	3
29.70	3678.29	936.05	2742.24	2365.60	376.64	3
28.32	3826.46	997.91	2828.55	2451.91	376.64	3
26.94	3974.27	1059.77	2914.50	2537.86	376.64	3
25.57	4121.73	1121.63	3000.10	2623.46	376.64	3
24.21	4268.84	1183.49	3085.35	2708.71	376.64	3
22.84	4415.60	1245.35	3170.26	2793.62	376.64	3
21.49	4562.02	1307.21	3254.81	2878.17	376.64	3
20.14	4708.08	1369.06	3339.02	2962.38	376.64	3
18.80	4853.80	1430.92	3422.88	3046.24	376.64	3
18.80	4853.80	1430.92	3422.88	3046.24	376.64	2
16.88	5059.47	1517.02	3542.45	3165.81	376.64	2
14.97	5264.61	1603.12	3661.49	3284.85	376.64	2
13.07	5469.22	1689.22	3780.00	3403.36	376.64	2
11.18	5673.30	1775.31	3897.98	3521.34	376.64	2
9.30	5876.85	1861.41	4015.44	3638.80	376.64	2
7.43	6079.87	1947.51	4132.36	3755.72	376.64	2
5.56	6282.38	2033.61	4248.77	3872.13	376.64	2
3.70	6484.49	2119.71	4364.79	3988.15	376.64	2
1.85	6686.26	2205.80	4480.46	4103.82	376.64	2
.00	6887.67	2291.90	4595.77	4219.13	376.64	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	7.03	3.55	.98	.98	.98	1
5.27	5.27	2.66	.98	.98	.91	1
3.52	3.52	1.78	.98	.98	.90	1
1.76	1.76	.89	.98	.98	.89	1
.00	.00	.00	.98	.98	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

7.03	.00	.00	.00	.00	.00	1
5.27	203.83	.00	203.83	109.67	94.16	1
3.52	407.65	.00	407.65	219.34	188.32	1
1.76	611.48	.00	611.48	329.00	282.48	1
.00	815.31	.00	815.31	438.67	376.64	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.48	21.42	6.50	5.94	5.36	6
60.02	59.95	21.35	6.49	6.12	5.35	6
59.45	59.41	21.27	6.47	6.25	5.33	6
58.89	58.86	21.20	6.46	6.34	5.32	6
58.33	58.30	21.12	6.44	6.39	5.31	6
57.76	57.74	21.05	6.43	6.40	5.29	6
57.20	57.18	20.97	6.42	6.41	5.28	6
56.64	56.62	20.90	6.40	6.40	5.26	6
56.08	56.06	20.82	6.39	6.39	5.25	6
56.08	56.06	20.82	4.51	4.51	3.57	5
54.82	54.79	20.59	4.44	4.44	3.51	5
53.56	53.54	20.36	4.38	4.38	3.45	5
52.32	52.30	20.12	4.32	4.31	3.38	5
51.10	51.08	19.89	4.25	4.25	3.34	5
49.88	49.87	19.66	4.19	4.19	3.31	5
48.69	48.67	19.43	4.13	4.12	3.28	5
48.69	48.67	19.43	1.93	1.93	1.86	4
46.69	46.67	18.75	1.92	1.92	1.84	4
44.70	44.69	18.06	1.91	1.91	1.82	4
42.72	42.71	17.38	1.89	1.89	1.80	4
40.75	40.74	16.70	1.88	1.88	1.78	4
38.79	38.78	16.01	1.86	1.86	1.75	4
36.85	36.83	15.33	1.84	1.84	1.73	4
34.91	34.90	14.65	1.82	1.82	1.71	4
33.00	32.98	13.97	1.80	1.80	1.69	4
31.09	31.08	13.28	1.78	1.78	1.67	4
31.09	31.08	13.28	1.47	1.47	1.41	3
29.70	29.69	12.72	1.46	1.46	1.40	3
28.32	28.31	12.16	1.45	1.45	1.39	3
26.94	26.93	11.59	1.44	1.44	1.38	3
25.57	25.56	11.03	1.43	1.43	1.37	3
24.21	24.19	10.47	1.42	1.42	1.36	3
22.84	22.83	9.90	1.41	1.41	1.35	3
21.49	21.48	9.34	1.40	1.40	1.34	3
20.14	20.13	8.78	1.39	1.39	1.33	3
18.80	18.78	8.21	1.38	1.38	1.32	3
18.80	18.78	8.21	1.34	1.34	1.29	2

16.88	16.87	7.39	1.33	1.33	1.28	2
14.97	14.96	6.57	1.32	1.32	1.27	2
13.07	13.06	5.75	1.31	1.31	1.26	2
11.18	11.17	4.93	1.30	1.30	1.26	2
9.30	9.29	4.11	1.29	1.29	1.25	2
7.43	7.41	3.29	1.28	1.28	1.24	2
5.56	5.55	2.46	1.27	1.27	1.24	2
3.70	3.69	1.64	1.26	1.26	1.23	2
1.85	1.84	.82	1.25	1.25	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.48	800.26	184.12	616.14	423.62	192.52	6
59.95	838.03	127.21	710.83	456.78	254.05	6
59.41	876.54	83.15	793.39	490.66	302.73	6
58.86	915.56	53.92	861.64	525.06	336.58	6
58.30	954.90	38.00	916.90	559.78	357.12	6
57.74	994.39	31.72	962.68	594.65	368.02	6
57.18	1033.93	31.28	1002.65	629.57	373.08	6
56.62	1073.45	33.92	1039.52	664.47	375.06	6
56.06	1112.91	38.08	1074.84	699.31	375.52	6
56.06	1112.91	38.08	1074.84	699.31	375.52	5
54.79	1217.85	63.59	1154.26	778.50	375.76	5
53.54	1321.87	89.33	1232.54	856.77	375.77	5
52.30	1424.97	115.12	1309.85	934.12	375.73	5
51.08	1527.13	140.89	1386.24	1010.53	375.71	5
49.87	1628.38	166.62	1461.76	1086.03	375.73	5
48.67	1728.70	192.27	1536.43	1160.60	375.83	5
48.67	1728.70	192.27	1536.43	1160.60	375.83	4
46.67	1929.14	267.32	1661.82	1285.18	376.64	4
44.69	2129.07	343.18	1785.89	1409.25	376.64	4
42.71	2328.47	421.74	1906.73	1532.79	373.94	4
40.74	2527.31	507.76	2019.54	1655.77	363.78	4
38.78	2725.43	573.60	2151.83	1778.03	373.80	4
36.83	2922.72	646.64	2276.07	1899.46	376.61	4
34.90	3119.11	722.48	2396.63	2020.00	376.64	4
32.98	3314.60	798.34	2516.27	2139.63	376.64	4
31.08	3509.19	874.19	2634.99	2258.35	376.64	4
31.08	3509.19	874.20	2634.99	2258.35	376.64	3
29.69	3657.76	936.05	2721.70	2345.07	376.64	3
28.31	3805.93	997.91	2808.02	2431.38	376.64	3
26.93	3953.73	1060.99	2892.75	2517.32	375.42	3
25.56	4101.18	1123.18	2978.00	2602.92	375.08	3
24.19	4248.28	1185.03	3063.26	2688.16	375.10	3
22.83	4395.04	1246.80	3148.24	2773.05	375.19	3
21.48	4541.45	1308.56	3232.88	2857.60	375.28	3
20.13	4687.51	1370.27	3317.23	2941.80	375.43	3
18.78	4833.22	1431.78	3401.43	3025.66	375.78	3
18.78	4833.22	1431.78	3401.44	3025.66	375.78	2
16.87	5038.88	1517.22	3521.66	3145.23	376.44	2
14.96	5244.02	1603.21	3640.82	3264.27	376.55	2
13.06	5448.63	1689.22	3759.41	3382.78	376.64	2
11.17	5652.71	1775.31	3877.40	3500.76	376.64	2
9.29	5856.27	1861.41	3994.85	3618.21	376.64	2
7.41	6059.28	1947.51	4111.77	3735.13	376.64	2
5.55	6261.81	2033.61	4228.21	3851.57	376.64	2
3.69	6463.90	2125.02	4338.88	3967.55	371.33	2
1.84	6665.59	2262.79	4402.80	4083.15	319.65	2
.00	6866.24	2668.54	4197.71	4197.70	.00	2

Time = 30. Degree of Consolidation = 3.%

Total Settlement = .102

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 30. = .102

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	6.79	3.55	.98	.98	.98	1
5.27	5.07	2.66	.98	.91	.91	1
3.52	3.38	1.78	.98	.90	.90	1
1.76	1.69	.89	.98	.90	.89	1
.00	.00	.00	.98	.90	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
6.79	.00	.00	.00	.00	.00	1
5.07	201.38	94.16	107.22	107.22	.00	1
3.38	401.18	155.36	245.82	212.86	32.96	1
1.69	600.75	175.98	424.77	318.27	106.50	1
.00	800.26	184.12	616.14	423.62	192.52	1

Time = 30. Degree of Consolidation = 94.%

Total Settlement = .241

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 30. = .241

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 5.29

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.42	21.42	6.50	5.88	5.36	6
60.02	59.90	21.35	6.49	6.02	5.35	6
59.45	59.36	21.27	6.47	6.13	5.33	6
58.89	58.82	21.20	6.46	6.22	5.32	6
58.33	58.27	21.12	6.44	6.29	5.31	6

57.76	57.72	21.05	6.43	6.34	5.29	6
57.20	57.16	20.97	6.42	6.36	5.28	6
56.64	56.61	20.90	6.40	6.37	5.26	6
56.08	56.05	20.82	6.39	6.37	5.25	6
56.08	56.05	20.82	4.51	4.49	3.57	5
54.82	54.78	20.59	4.44	4.44	3.51	5
53.56	53.53	20.36	4.38	4.37	3.45	5
52.32	52.29	20.12	4.32	4.31	3.38	5
51.10	51.07	19.89	4.25	4.25	3.34	5
49.88	49.86	19.66	4.19	4.18	3.31	5
48.69	48.66	19.43	4.13	4.12	3.28	5
48.69	48.66	19.43	1.93	1.93	1.86	4
46.69	46.67	18.75	1.92	1.92	1.84	4
44.70	44.68	18.06	1.91	1.91	1.82	4
42.72	42.70	17.38	1.89	1.89	1.80	4
40.75	40.73	16.70	1.88	1.88	1.78	4
38.79	38.77	16.01	1.86	1.86	1.75	4
36.85	36.83	15.33	1.84	1.84	1.73	4
34.91	34.89	14.65	1.82	1.82	1.71	4
33.00	32.98	13.97	1.80	1.80	1.69	4
31.09	31.07	13.28	1.78	1.78	1.67	4
31.09	31.07	13.28	1.47	1.47	1.41	3
29.70	29.68	12.72	1.46	1.46	1.40	3
28.32	28.30	12.16	1.45	1.45	1.39	3
26.94	26.92	11.59	1.44	1.44	1.38	3
25.57	25.55	11.03	1.43	1.43	1.37	3
24.21	24.19	10.47	1.42	1.42	1.36	3
22.84	22.83	9.90	1.41	1.41	1.35	3
21.49	21.47	9.34	1.40	1.40	1.34	3
20.14	20.12	8.78	1.39	1.39	1.33	3
18.80	18.78	8.21	1.38	1.38	1.32	3
18.80	18.78	8.21	1.34	1.34	1.29	2
16.88	16.86	7.39	1.33	1.33	1.28	2
14.97	14.95	6.57	1.32	1.32	1.27	2
13.07	13.06	5.75	1.31	1.31	1.26	2
11.18	11.16	4.93	1.30	1.30	1.26	2
9.30	9.28	4.11	1.29	1.29	1.25	2
7.43	7.41	3.29	1.28	1.28	1.24	2
5.56	5.54	2.46	1.27	1.27	1.24	2
3.70	3.68	1.64	1.26	1.26	1.23	2
1.85	1.83	.82	1.25	1.25	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.42	800.08	204.29	595.80	423.45	172.35	6
59.90	837.47	160.27	677.21	456.22	220.99	6
59.36	875.45	122.13	753.32	489.57	263.75	6
58.82	913.92	91.49	822.44	523.42	299.01	6
58.27	952.77	69.02	883.75	557.65	326.10	6
57.72	991.88	54.32	937.56	592.14	345.42	6
57.16	1031.15	46.15	985.01	626.79	358.21	6
56.61	1070.50	42.93	1027.57	661.52	366.05	6
56.05	1109.87	43.10	1066.77	696.27	370.50	6
56.05	1109.87	43.10	1066.77	696.27	370.50	5
54.78	1214.68	66.30	1148.38	775.33	373.05	5
53.53	1318.62	90.93	1227.69	853.52	374.17	5
52.29	1421.67	116.25	1305.42	930.82	374.60	5
51.07	1523.80	141.83	1381.97	1007.20	374.77	5
49.86	1625.01	167.45	1457.56	1082.66	374.90	5
48.66	1725.31	193.02	1532.28	1157.21	375.08	5

48.66	1725.31	193.03	1532.28	1157.21	375.07	4
46.67	1925.74	267.32	1658.42	1281.79	376.64	4
44.68	2125.67	343.58	1782.09	1405.85	376.24	4
42.70	2325.06	426.45	1898.61	1529.38	369.23	4
40.73	2523.84	512.85	2010.99	1652.30	358.69	4
38.77	2721.91	577.07	2144.84	1774.51	370.33	4
36.83	2919.17	647.57	2271.60	1895.92	375.69	4
34.89	3115.56	722.48	2393.09	2016.45	376.64	4
32.98	3311.06	798.34	2512.72	2136.08	376.64	4
31.07	3505.64	874.19	2631.45	2254.81	376.64	4
31.07	3505.64	874.20	2631.44	2254.81	376.64	3
29.68	3654.21	936.05	2718.16	2341.52	376.64	3
28.30	3802.38	997.91	2804.47	2427.83	376.64	3
26.92	3950.18	1061.85	2888.34	2513.78	374.56	3
25.55	4097.63	1124.51	2973.11	2599.36	373.75	3
24.19	4244.72	1186.49	3058.23	2684.60	373.63	3
22.83	4391.47	1248.23	3143.24	2769.48	373.76	3
21.47	4537.87	1309.87	3228.00	2854.02	373.97	3
20.12	4683.92	1371.40	3312.52	2938.22	374.30	3
18.78	4829.63	1432.63	3396.99	3022.07	374.93	3
18.78	4829.63	1432.63	3396.99	3022.07	374.93	2
16.86	5035.29	1517.53	3517.76	3141.63	376.13	2
14.95	5240.43	1603.29	3637.13	3260.67	376.46	2
13.06	5445.04	1689.25	3755.78	3379.18	376.60	2
11.16	5649.11	1775.31	3873.80	3497.16	376.64	2
9.28	5852.67	1861.41	3991.26	3614.62	376.64	2
7.41	6055.69	1947.51	4108.17	3731.54	376.64	2
5.54	6258.20	2033.61	4224.60	3847.96	376.64	2
3.68	6460.29	2136.36	4323.93	3963.94	359.98	2
1.83	6661.86	2305.39	4356.47	4079.42	277.06	2
.00	6862.38	2668.54	4193.85	4193.84	.00	2

Time = 60. Degree of Consolidation = 5.%

Total Settlement = .161

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 60. = .161

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
7.03	6.79	3.55
5.27	5.07	2.66
3.52	3.38	1.78
1.76	1.69	.89
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.89	1
.98	.90	.89	1

***** Stresses *****

XI	Total	Effective
6.79	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

5.07	201.39	94.16	107.23	107.23	.00	1
3.38	401.16	164.18	236.98	212.84	24.14	1
1.69	600.67	190.67	410.00	318.19	91.81	1
.00	800.08	204.29	595.80	423.45	172.35	1

Time = 60. Degree of Consolidation = 95.%

Total Settlement = .244

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 60. = .244

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 5.22

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.33	21.42	6.50	5.82	5.36	6
60.02	59.81	21.35	6.49	5.92	5.35	6
59.45	59.28	21.27	6.47	6.01	5.33	6
58.89	58.75	21.20	6.46	6.10	5.32	6
58.33	58.21	21.12	6.44	6.17	5.31	6
57.76	57.67	21.05	6.43	6.22	5.29	6
57.20	57.12	20.97	6.42	6.27	5.28	6
56.64	56.57	20.90	6.40	6.30	5.26	6
56.08	56.02	20.82	6.39	6.32	5.25	6
56.08	56.02	20.82	4.51	4.45	3.57	5
54.82	54.76	20.59	4.44	4.41	3.51	5
53.56	53.51	20.36	4.38	4.36	3.45	5
52.32	52.27	20.12	4.32	4.30	3.38	5
51.10	51.05	19.89	4.25	4.24	3.34	5
49.88	49.85	19.66	4.19	4.18	3.31	5
48.69	48.65	19.43	4.13	4.11	3.28	5
48.69	48.65	19.43	1.93	1.93	1.86	4
46.69	46.66	18.75	1.92	1.92	1.84	4
44.70	44.67	18.06	1.91	1.90	1.82	4
42.72	42.69	17.38	1.89	1.89	1.80	4
40.75	40.72	16.70	1.88	1.87	1.78	4
38.79	38.76	16.01	1.86	1.86	1.75	4
36.85	36.82	15.33	1.84	1.84	1.73	4
34.91	34.89	14.65	1.82	1.82	1.71	4
33.00	32.97	13.97	1.80	1.80	1.69	4
31.09	31.07	13.28	1.78	1.78	1.67	4
31.09	31.07	13.28	1.47	1.47	1.41	3
29.70	29.68	12.72	1.46	1.46	1.40	3
28.32	28.29	12.16	1.45	1.45	1.39	3
26.94	26.92	11.59	1.44	1.44	1.38	3
25.57	25.55	11.03	1.43	1.43	1.37	3
24.21	24.18	10.47	1.42	1.42	1.36	3
22.84	22.82	9.90	1.41	1.41	1.35	3
21.49	21.46	9.34	1.40	1.40	1.34	3
20.14	20.12	8.78	1.39	1.39	1.33	3
18.80	18.77	8.21	1.38	1.38	1.32	3

18.80	18.77	8.21	1.34	1.29	2	
16.88	16.86	7.39	1.33	1.28	2	
14.97	14.95	6.57	1.32	1.27	2	
13.07	13.05	5.75	1.31	1.26	2	
11.18	11.16	4.93	1.30	1.26	2	
9.30	9.28	4.11	1.29	1.25	2	
7.43	7.40	3.29	1.28	1.24	2	
5.56	5.54	2.46	1.27	1.24	2	
3.70	3.68	1.64	1.26	1.23	2	
1.85	1.83	.82	1.25	1.24	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.33	799.98	223.93	576.05	423.34	152.71	6
59.81	837.00	191.02	645.98	455.75	190.24	6
59.28	874.48	160.67	713.82	488.61	225.21	6
58.75	912.37	133.68	778.69	521.87	256.81	6
58.21	950.62	110.68	839.94	555.50	284.44	6
57.67	989.16	91.94	897.22	589.42	307.80	6
57.12	1027.94	77.38	950.56	623.58	326.98	6
56.57	1066.90	66.62	1000.28	657.92	342.36	6
56.02	1105.99	59.00	1046.99	692.39	354.60	6
56.02	1105.99	59.00	1046.99	692.39	354.60	5
54.76	1210.31	77.53	1132.78	770.96	361.82	5
53.51	1313.92	98.59	1215.33	848.82	366.51	5
52.27	1416.74	121.43	1295.31	925.89	369.42	5
51.05	1518.71	145.48	1373.23	1002.11	371.12	5
49.85	1619.81	170.32	1449.49	1077.46	372.03	5
48.65	1720.01	195.73	1524.28	1151.91	372.37	5
48.65	1720.01	195.73	1524.28	1151.91	372.37	4
46.66	1920.44	268.63	1651.81	1276.48	375.33	4
44.67	2120.34	347.12	1773.23	1400.53	372.70	4
42.69	2319.70	434.00	1885.69	1524.02	361.67	4
40.72	2518.41	518.99	1999.43	1646.88	352.55	4
38.76	2716.41	582.40	2134.01	1769.02	364.99	4
36.82	2913.62	650.39	2263.24	1890.37	372.87	4
34.89	3110.00	722.58	2387.42	2010.89	376.53	4
32.97	3305.49	798.34	2507.16	2130.52	376.64	4
31.07	3500.07	874.19	2625.88	2249.24	376.64	4
31.07	3500.07	874.20	2625.88	2249.24	376.64	3
29.68	3648.64	936.05	2712.59	2335.95	376.64	3
28.29	3796.82	997.91	2798.91	2422.27	376.64	3
26.92	3944.62	1063.11	2881.51	2508.21	373.30	3
25.55	4092.05	1126.67	2965.38	2593.78	371.60	3
24.18	4239.13	1189.07	3050.06	2679.01	371.06	3
22.82	4385.86	1250.87	3135.00	2763.88	371.12	3
21.46	4532.25	1312.33	3219.92	2848.40	371.52	3
20.12	4678.29	1373.51	3304.78	2932.59	372.19	3
18.77	4823.98	1434.31	3389.68	3016.42	373.25	3
18.77	4823.98	1434.31	3389.68	3016.42	373.25	2
16.86	5029.64	1518.33	3511.31	3135.98	375.32	2
14.95	5234.77	1603.62	3631.15	3255.02	376.14	2
13.05	5439.38	1689.42	3749.96	3373.52	376.44	2
11.16	5643.46	1775.31	3868.14	3491.51	376.64	2
9.28	5847.02	1861.41	3985.61	3608.97	376.64	2
7.40	6050.03	1947.51	4102.52	3725.88	376.64	2
5.54	6252.54	2036.04	4216.50	3842.29	374.21	2
3.68	6454.58	2163.62	4290.96	3958.24	332.72	2
1.83	6655.97	2361.08	4294.89	4073.53	221.36	2
.00	6856.34	2668.54	4187.80	4187.79	.00	2

Time = 120. Degree of Consolidation = 8.%

Total Settlement = .256

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 120. = .256

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
7.03	6.78	3.55	.98	.98	.98	1
5.27	5.07	2.66	.98	.91	.91	1
3.52	3.37	1.78	.98	.90	.90	1
1.76	1.69	.89	.98	.90	.89	1
.00	.00	.00	.98	.90	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
6.78	.00	.00	.00	.00	.00	1
5.07	201.39	94.16	107.23	107.23	.00	1
3.37	401.15	169.13	232.02	212.83	19.19	1
1.69	600.62	199.54	401.08	318.14	82.93	1
.00	799.98	223.93	576.05	423.34	152.71	1

Time = 120. Degree of Consolidation = 96.%

Total Settlement = .246

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 120. = .246

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 5.13

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.17	21.42	6.50	5.76	5.36	6
60.02	59.66	21.35	6.49	5.83	5.35	6

59.45	59.14	21.27	6.47	5.91	5.33	6
58.89	58.62	21.20	6.46	5.98	5.32	6
58.33	58.09	21.12	6.44	6.04	5.31	6
57.76	57.55	21.05	6.43	6.10	5.29	6
57.20	57.01	20.97	6.42	6.15	5.28	6
56.64	56.47	20.90	6.40	6.19	5.26	6
56.08	55.93	20.82	6.39	6.23	5.25	6
56.08	55.93	20.82	4.51	4.38	3.57	5
54.82	54.68	20.59	4.44	4.34	3.51	5
53.56	53.45	20.36	4.38	4.30	3.45	5
52.32	52.23	20.12	4.32	4.25	3.38	5
51.10	51.01	19.89	4.25	4.20	3.34	5
49.88	49.82	19.66	4.19	4.14	3.31	5
48.69	48.63	19.43	4.13	4.08	3.28	5
48.69	48.63	19.43	1.93	1.93	1.86	4
46.69	46.64	18.75	1.92	1.92	1.84	4
44.70	44.65	18.06	1.91	1.90	1.82	4
42.72	42.67	17.38	1.89	1.89	1.80	4
40.75	40.71	16.70	1.88	1.87	1.78	4
38.79	38.75	16.01	1.86	1.85	1.75	4
36.85	36.81	15.33	1.84	1.84	1.73	4
34.91	34.87	14.65	1.82	1.82	1.71	4
33.00	32.96	13.97	1.80	1.80	1.69	4
31.09	31.06	13.28	1.78	1.78	1.67	4
31.09	31.06	13.28	1.47	1.47	1.41	3
29.70	29.67	12.72	1.46	1.46	1.40	3
28.32	28.28	12.16	1.45	1.45	1.39	3
26.94	26.91	11.59	1.44	1.44	1.38	3
25.57	25.53	11.03	1.43	1.43	1.37	3
24.21	24.17	10.47	1.42	1.42	1.36	3
22.84	22.81	9.90	1.41	1.41	1.35	3
21.49	21.45	9.34	1.40	1.40	1.34	3
20.14	20.11	8.78	1.39	1.39	1.33	3
18.80	18.76	8.21	1.38	1.38	1.32	3
18.80	18.76	8.21	1.34	1.34	1.29	2
16.88	16.85	7.39	1.33	1.33	1.28	2
14.97	14.94	6.57	1.32	1.32	1.27	2
13.07	13.04	5.75	1.31	1.31	1.26	2
11.18	11.15	4.93	1.30	1.30	1.26	2
9.30	9.27	4.11	1.29	1.29	1.25	2
7.43	7.39	3.29	1.28	1.28	1.24	2
5.56	5.53	2.46	1.27	1.27	1.24	2
3.70	3.67	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.24	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.17	799.85	245.66	554.19	423.21	130.98	6
59.66	836.51	220.42	616.09	455.25	160.84	6
59.14	873.53	196.35	677.18	487.65	189.53	6
58.62	910.87	173.71	737.16	520.38	216.78	6
58.09	948.53	152.77	795.76	553.41	242.35	6
57.55	986.48	133.68	852.79	586.74	266.05	6
57.01	1024.68	116.56	908.11	620.32	287.80	6
56.47	1063.11	101.42	961.69	654.13	307.56	6
55.93	1101.74	88.19	1013.55	688.14	325.41	6
55.93	1101.74	88.19	1013.55	688.14	325.41	5
54.68	1205.08	103.17	1101.91	765.73	336.18	5
53.45	1307.83	120.57	1187.26	842.73	344.53	5
52.23	1409.92	140.17	1269.75	919.07	350.68	5

51.01	1511.27	161.76	1349.51	994.67	354.84	5
49.82	1611.82	185.17	1426.64	1069.47	357.18	5
48.63	1711.49	210.26	1501.23	1143.39	357.84	5
48.63	1711.49	210.26	1501.23	1143.39	357.84	4
46.64	1911.83	280.56	1631.26	1267.87	363.40	4
44.65	2111.66	358.65	1753.01	1391.84	361.17	4
42.67	2310.93	446.90	1864.03	1515.25	348.78	4
40.71	2509.55	526.99	1982.56	1638.01	344.54	4
38.75	2707.46	589.56	2117.90	1760.06	357.84	4
36.81	2904.59	655.45	2249.14	1881.34	367.80	4
34.87	3100.93	724.97	2375.96	2001.81	374.15	4
32.96	3296.40	798.34	2498.07	2121.43	376.64	4
31.06	3490.99	874.19	2616.80	2240.16	376.64	4
31.06	3490.99	874.20	2616.80	2240.16	376.64	3
29.67	3639.56	936.05	2703.51	2326.87	376.64	3
28.28	3787.74	997.91	2789.82	2413.19	376.64	3
26.91	3935.53	1064.85	2870.68	2499.12	371.56	3
25.53	4082.95	1129.81	2953.14	2584.68	368.46	3
24.17	4230.01	1193.11	3036.90	2669.88	367.02	3
22.81	4376.72	1255.27	3121.44	2754.73	366.71	3
21.45	4523.08	1316.64	3206.44	2839.23	367.21	3
20.11	4669.09	1377.38	3291.71	2923.39	368.32	3
18.76	4814.77	1437.55	3377.22	3007.21	370.01	3
18.76	4814.77	1437.55	3377.22	3007.21	370.01	2
16.85	5020.41	1520.34	3500.07	3126.75	373.32	2
14.94	5225.53	1604.61	3620.92	3245.78	375.14	2
13.04	5430.14	1689.78	3740.36	3364.28	376.08	2
11.15	5634.21	1775.42	3858.79	3482.26	376.53	2
9.27	5837.77	1861.41	3976.35	3599.72	376.64	2
7.39	6040.78	1947.69	4093.09	3716.63	376.46	2
5.53	6243.27	2054.15	4189.12	3833.02	356.10	2
3.67	6445.17	2211.73	4233.44	3948.83	284.61	2
1.83	6646.33	2418.07	4228.26	4063.89	164.38	2
.00	6846.55	2668.54	4178.01	4178.01	.00	2

Time = 240. Degree of Consolidation = 13.%

Total Settlement = .411

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 240. = .411

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	6.78	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1
3.52	3.37	1.78	.98	.90	.90	1
1.76	1.68	.89	.98	.90	.89	1
.00	.00	.00	.98	.90	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
6.78	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.37	401.14	174.23	226.91	212.82	14.09	1
1.68	600.57	215.83	384.73	318.09	66.64	1
.00	799.85	245.66	554.19	423.21	130.98	1

Time = 240. Degree of Consolidation = 97.%

Total Settlement = .248

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 240. = .248

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.97

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.04	21.42	6.50	5.72	5.36	6
60.02	59.53	21.35	6.49	5.79	5.35	6
59.45	59.01	21.27	6.47	5.85	5.33	6
58.89	58.49	21.20	6.46	5.91	5.32	6
58.33	57.97	21.12	6.44	5.97	5.31	6
57.76	57.44	21.05	6.43	6.02	5.29	6
57.20	56.91	20.97	6.42	6.07	5.28	6
56.64	56.37	20.90	6.40	6.12	5.26	6
56.08	55.83	20.82	6.39	6.16	5.25	6
56.08	55.83	20.82	4.51	4.32	3.57	5
54.82	54.60	20.59	4.44	4.28	3.51	5
53.56	53.38	20.36	4.38	4.24	3.45	5
52.32	52.17	20.12	4.32	4.20	3.38	5
51.10	50.97	19.89	4.25	4.14	3.34	5
49.88	49.79	19.66	4.19	4.09	3.31	5
48.69	48.61	19.43	4.13	4.03	3.28	5
48.69	48.61	19.43	1.93	1.92	1.86	4
46.69	46.62	18.75	1.92	1.91	1.84	4
44.70	44.63	18.06	1.91	1.90	1.82	4
42.72	42.66	17.38	1.89	1.89	1.80	4
40.75	40.69	16.70	1.88	1.87	1.78	4
38.79	38.74	16.01	1.86	1.85	1.75	4
36.85	36.80	15.33	1.84	1.84	1.73	4
34.91	34.87	14.65	1.82	1.82	1.71	4
33.00	32.95	13.97	1.80	1.80	1.69	4
31.09	31.05	13.28	1.78	1.78	1.67	4
31.09	31.05	13.28	1.47	1.47	1.41	3
29.70	29.66	12.72	1.46	1.46	1.40	3
28.32	28.27	12.16	1.45	1.45	1.39	3
26.94	26.90	11.59	1.44	1.44	1.38	3
25.57	25.53	11.03	1.43	1.43	1.37	3

24.21	24.16	10.47	1.42	1.42	1.36	3
22.84	22.80	9.90	1.41	1.41	1.35	3
21.49	21.45	9.34	1.40	1.40	1.34	3
20.14	20.10	8.78	1.39	1.39	1.33	3
18.80	18.76	8.21	1.38	1.38	1.32	3
18.80	18.76	8.21	1.34	1.34	1.29	2
16.88	16.84	7.39	1.33	1.33	1.28	2
14.97	14.93	6.57	1.32	1.32	1.27	2
13.07	13.03	5.75	1.31	1.31	1.26	2
11.18	11.14	4.93	1.30	1.30	1.26	2
9.30	9.26	4.11	1.29	1.29	1.25	2
7.43	7.39	3.29	1.28	1.28	1.24	2
5.56	5.52	2.46	1.27	1.26	1.24	2
3.70	3.67	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.04	799.78	257.42	542.36	423.14	119.22	6
59.53	836.25	235.99	600.26	454.99	145.27	6
59.01	873.02	215.22	657.80	487.14	170.66	6
58.49	910.08	195.27	714.81	519.58	195.23	6
57.97	947.41	176.30	771.11	552.29	218.82	6
57.44	985.01	158.47	826.54	585.27	241.27	6
56.91	1022.85	141.90	880.95	618.50	262.45	6
56.37	1060.92	126.70	934.22	651.94	282.28	6
55.83	1099.20	112.94	986.26	685.60	300.66	6
55.83	1099.20	112.94	986.26	685.60	300.66	5
54.60	1201.66	127.41	1074.25	762.31	311.94	5
53.38	1303.55	144.04	1159.51	838.45	321.06	5
52.17	1404.82	162.81	1242.01	913.97	328.04	5
50.97	1505.37	183.64	1321.73	988.77	332.96	5
49.79	1605.14	206.47	1398.67	1062.79	335.88	5
48.61	1704.06	231.24	1472.81	1135.96	336.86	5
48.61	1704.06	231.24	1472.81	1135.96	336.86	4
46.62	1904.26	298.70	1605.56	1260.30	345.26	4
44.63	2103.98	374.64	1729.34	1384.16	345.18	4
42.66	2303.14	461.56	1841.58	1507.46	334.12	4
40.69	2501.67	534.54	1967.13	1630.13	337.00	4
38.74	2699.49	595.68	2103.81	1752.10	351.71	4
36.80	2896.57	659.95	2236.62	1873.31	363.30	4
34.87	3092.86	727.53	2365.33	1993.74	371.59	4
32.95	3288.32	798.74	2489.58	2113.34	376.23	4
31.05	3482.90	874.39	2608.52	2232.07	376.44	4
31.05	3482.90	874.39	2608.52	2232.07	376.44	3
29.66	3631.47	936.05	2695.42	2318.78	376.64	3
28.27	3779.65	997.91	2781.74	2405.10	376.64	3
26.90	3927.44	1066.10	2861.34	2491.03	370.31	3
25.53	4074.85	1132.15	2942.70	2576.58	366.11	3
24.16	4221.89	1196.24	3025.65	2661.77	363.89	3
22.80	4368.58	1258.85	3109.74	2746.60	363.14	3
21.45	4514.92	1320.30	3194.62	2831.08	363.54	3
20.10	4660.92	1380.86	3280.06	2915.22	364.84	3
18.76	4806.58	1440.60	3365.98	2999.02	366.96	3
18.76	4806.58	1440.60	3365.98	2999.02	366.96	2
16.84	5012.20	1522.51	3489.69	3118.54	371.14	2
14.93	5217.31	1606.03	3611.28	3237.56	373.73	2
13.03	5421.91	1690.54	3731.37	3356.05	375.32	2
11.14	5625.98	1775.91	3850.08	3474.03	376.05	2
9.26	5829.53	1862.47	3967.06	3591.48	375.59	2

7.39	6032.53	1952.33	4080.20	3708.38	371.81	2
5.52	6234.96	2075.74	4159.23	3824.72	334.51	2
3.67	6436.75	2246.37	4190.38	3940.40	249.98	2
1.83	6637.77	2447.18	4190.59	4055.32	135.26	2
.00	6837.92	2668.54	4169.38	4169.38	.00	2

Time = 365. Degree of Consolidation = 17.%

Total Settlement = .548

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 365. = .548

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
7.03	6.78	3.55
5.27	5.06	2.66
3.52	3.37	1.78
1.76	1.68	.89
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.89	1
.98	.90	.89	1

***** Stresses *****

XI	Total	Effective
6.78	.00	.00
5.06	201.40	94.16
3.37	401.14	176.77
1.68	600.54	224.69
.00	799.78	257.42

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
107.24	107.24	.00	1
224.37	212.82	11.55	1
375.85	318.06	57.79	1
542.36	423.14	119.22	1

Time = 365. Degree of Consolidation = 97.%

Total Settlement = .249

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 365. = .249

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.83

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.86	21.42	6.50	5.69	5.36	6
60.02	59.36	21.35	6.49	5.75	5.35	6
59.45	58.85	21.27	6.47	5.80	5.33	6
58.89	58.33	21.20	6.46	5.85	5.32	6
58.33	57.81	21.12	6.44	5.90	5.31	6
57.76	57.29	21.05	6.43	5.95	5.29	6
57.20	56.76	20.97	6.42	5.99	5.28	6
56.64	56.23	20.90	6.40	6.03	5.26	6
56.08	55.70	20.82	6.39	6.07	5.25	6
56.08	55.70	20.82	4.51	4.25	3.57	5
54.82	54.49	20.59	4.44	4.21	3.51	5
53.56	53.28	20.36	4.38	4.17	3.45	5
52.32	52.09	20.12	4.32	4.12	3.38	5
51.10	50.91	19.89	4.25	4.07	3.34	5
49.88	49.74	19.66	4.19	4.01	3.31	5
48.69	48.59	19.43	4.13	3.95	3.28	5
48.69	48.59	19.43	1.93	1.92	1.86	4
46.69	46.60	18.75	1.92	1.91	1.84	4
44.70	44.61	18.06	1.91	1.90	1.82	4
42.72	42.64	17.38	1.89	1.88	1.80	4
40.75	40.68	16.70	1.88	1.87	1.78	4
38.79	38.72	16.01	1.86	1.85	1.75	4
36.85	36.78	15.33	1.84	1.83	1.73	4
34.91	34.85	14.65	1.82	1.81	1.71	4
33.00	32.94	13.97	1.80	1.80	1.69	4
31.09	31.04	13.28	1.78	1.77	1.67	4
31.09	31.04	13.28	1.47	1.47	1.41	3
29.70	29.65	12.72	1.46	1.46	1.40	3
28.32	28.26	12.16	1.45	1.45	1.39	3
26.94	26.89	11.59	1.44	1.44	1.38	3
25.57	25.52	11.03	1.43	1.43	1.37	3
24.21	24.15	10.47	1.42	1.42	1.36	3
22.84	22.79	9.90	1.41	1.41	1.35	3
21.49	21.44	9.34	1.40	1.40	1.34	3
20.14	20.09	8.78	1.39	1.39	1.33	3
18.80	18.75	8.21	1.38	1.38	1.32	3
18.80	18.75	8.21	1.34	1.34	1.29	2
16.88	16.83	7.39	1.33	1.33	1.28	2
14.97	14.93	6.57	1.32	1.32	1.27	2
13.07	13.03	5.75	1.31	1.31	1.26	2
11.18	11.14	4.93	1.30	1.30	1.26	2
9.30	9.25	4.11	1.29	1.29	1.25	2
7.43	7.38	3.29	1.28	1.27	1.24	2
5.56	5.52	2.46	1.27	1.26	1.24	2
3.70	3.67	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.86	799.72	267.98	531.74	423.08	108.66	6
59.36	836.02	249.83	586.19	454.76	131.43	6
58.85	872.57	232.14	640.42	486.69	153.73	6
58.33	909.36	215.04	694.32	518.86	175.46	6
57.81	946.40	198.64	747.76	551.28	196.48	6
57.29	983.66	183.08	800.59	583.92	216.66	6
56.76	1021.14	168.46	852.68	616.78	235.89	6
56.23	1058.82	154.92	903.90	649.84	254.06	6

55.70	1096.68	142.56	954.12	683.08	271.04	6
55.70	1096.68	142.56	954.12	683.08	271.04	5
54.49	1198.07	157.68	1040.38	758.72	281.67	5
53.28	1298.87	174.68	1124.19	833.77	290.42	5
52.09	1399.03	193.56	1205.47	908.18	297.29	5
50.91	1498.48	214.33	1284.15	981.88	302.27	5
49.74	1597.15	236.97	1360.18	1054.80	305.38	5
48.59	1694.98	261.45	1433.53	1126.88	306.65	5
48.59	1694.98	261.45	1433.53	1126.88	306.65	4
46.60	1894.99	326.26	1568.73	1251.03	317.70	4
44.61	2094.52	399.68	1694.84	1374.71	320.14	4
42.64	2293.52	484.43	1809.10	1497.85	311.25	4
40.68	2491.91	545.93	1945.97	1620.37	325.60	4
38.72	2689.61	604.66	2084.95	1742.21	342.74	4
36.78	2886.59	666.67	2219.92	1863.33	356.59	4
34.85	3082.81	732.16	2350.66	1983.70	366.96	4
32.94	3278.23	801.56	2476.67	2103.26	373.41	4
31.04	3472.79	875.74	2597.05	2221.96	375.09	4
31.04	3472.79	875.74	2597.05	2221.96	375.09	3
29.65	3621.36	936.05	2685.30	2308.66	376.64	3
28.26	3769.53	997.91	2771.62	2394.98	376.64	3
26.89	3917.32	1067.37	2849.95	2480.91	369.04	3
25.52	4064.72	1134.53	2930.19	2566.45	363.73	3
24.15	4211.75	1199.49	3012.26	2651.62	360.64	3
22.79	4358.42	1262.65	3095.77	2736.43	359.34	3
21.44	4504.73	1324.36	3180.38	2820.89	359.49	3
20.09	4650.71	1384.85	3265.86	2905.01	360.86	3
18.75	4796.34	1444.27	3352.07	2988.78	363.29	3
18.75	4796.34	1444.27	3352.07	2988.78	363.29	2
16.83	5001.95	1525.56	3476.39	3108.29	368.10	2
14.93	5207.04	1608.29	3598.76	3227.29	371.47	2
13.03	5411.63	1692.41	3719.22	3345.77	373.45	2
11.14	5615.69	1778.32	3837.36	3463.74	373.63	2
9.25	5819.21	1867.38	3951.84	3581.16	370.67	2
7.38	6022.17	1962.84	4059.33	3698.02	361.31	2
5.52	6224.51	2102.35	4122.16	3814.27	307.89	2
3.67	6426.17	2277.81	4148.36	3929.83	218.53	2
1.83	6627.08	2469.29	4157.79	4044.64	113.15	2
.00	6827.18	2668.54	4158.64	4158.64	.00	2

Time = 540. Degree of Consolidation = 23.%

Total Settlement = .720

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 540. = .720

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	6.78	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1
3.52	3.37	1.78	.98	.90	.90	1

1.76	1.68	.89	.98	.90	.89	1
.00	.00	.00	.98	.90	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
6.78	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.37	401.13	178.91	222.22	212.81	9.41	1
1.68	600.51	232.50	368.01	318.03	49.98	1
.00	799.72	267.98	531.74	423.08	108.66	1

Time = 540. Degree of Consolidation = 98.%

Total Settlement = .250

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 540. = .250

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.66

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.70	21.42	6.50	5.66	5.36	6
60.02	59.19	21.35	6.49	5.71	5.35	6
59.45	58.68	21.27	6.47	5.76	5.33	6
58.89	58.17	21.20	6.46	5.80	5.32	6
58.33	57.66	21.12	6.44	5.84	5.31	6
57.76	57.14	21.05	6.43	5.88	5.29	6
57.20	56.62	20.97	6.42	5.92	5.28	6
56.64	56.09	20.90	6.40	5.95	5.26	6
56.08	55.57	20.82	6.39	5.98	5.25	6
56.08	55.57	20.82	4.51	4.18	3.57	5
54.82	54.37	20.59	4.44	4.14	3.51	5
53.56	53.18	20.36	4.38	4.09	3.45	5
52.32	52.01	20.12	4.32	4.04	3.38	5
51.10	50.85	19.89	4.25	3.99	3.34	5
49.88	49.69	19.66	4.19	3.94	3.31	5
48.69	48.56	19.43	4.13	3.88	3.28	5
48.69	48.56	19.43	1.93	1.91	1.86	4
46.69	46.57	18.75	1.92	1.90	1.84	4
44.70	44.59	18.06	1.91	1.89	1.82	4
42.72	42.62	17.38	1.89	1.88	1.80	4
40.75	40.66	16.70	1.88	1.86	1.78	4
38.79	38.71	16.01	1.86	1.85	1.75	4
36.85	36.77	15.33	1.84	1.83	1.73	4
34.91	34.84	14.65	1.82	1.81	1.71	4
33.00	32.93	13.97	1.80	1.79	1.69	4
31.09	31.03	13.28	1.78	1.77	1.67	4

31.09	31.03	13.28	1.47	1.47	1.41	3
29.70	29.64	12.72	1.46	1.46	1.40	3
28.32	28.25	12.16	1.45	1.45	1.39	3
26.94	26.88	11.59	1.44	1.44	1.38	3
25.57	25.51	11.03	1.43	1.43	1.37	3
24.21	24.14	10.47	1.42	1.42	1.36	3
22.84	22.78	9.90	1.41	1.41	1.35	3
21.49	21.43	9.34	1.40	1.40	1.34	3
20.14	20.08	8.78	1.39	1.39	1.33	3
18.80	18.74	8.21	1.38	1.38	1.32	3
18.80	18.74	8.21	1.34	1.34	1.29	2
16.88	16.83	7.39	1.33	1.33	1.28	2
14.97	14.92	6.57	1.32	1.32	1.27	2
13.07	13.02	5.75	1.31	1.31	1.26	2
11.18	11.13	4.93	1.30	1.30	1.26	2
9.30	9.25	4.11	1.29	1.29	1.25	2
7.43	7.38	3.29	1.28	1.27	1.24	2
5.56	5.52	2.46	1.27	1.26	1.24	2
3.70	3.67	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.70	799.67	277.03	522.64	423.03	99.61	6
59.19	835.82	261.58	574.24	454.56	119.68	6
58.68	872.18	246.54	625.64	486.30	139.34	6
58.17	908.76	232.00	676.75	518.26	158.50	6
57.66	945.53	218.08	727.46	550.41	177.04	6
57.14	982.50	204.87	777.63	582.76	194.87	6
56.62	1019.65	192.50	827.16	615.29	211.86	6
56.09	1056.98	181.05	875.93	648.00	227.93	6
55.57	1094.45	170.63	923.82	680.85	242.97	6
55.57	1094.45	170.63	923.82	680.85	242.97	5
54.37	1194.81	186.79	1008.02	755.46	252.56	5
53.18	1294.56	204.56	1089.99	829.45	260.54	5
52.01	1393.63	223.97	1169.67	902.78	266.88	5
50.85	1491.99	245.02	1246.97	975.39	271.58	5
49.69	1589.56	267.71	1321.84	1047.21	274.64	5
48.56	1686.28	292.03	1394.25	1118.18	276.07	5
48.56	1686.28	292.03	1394.25	1118.18	276.07	4
46.57	1886.09	355.33	1530.76	1242.13	288.63	4
44.59	2085.43	427.22	1658.21	1365.61	292.60	4
42.62	2284.25	505.89	1778.36	1488.57	289.79	4
40.66	2482.46	559.02	1923.44	1610.92	312.51	4
38.71	2680.02	615.37	2064.65	1732.63	332.02	4
36.77	2876.89	675.08	2201.81	1853.63	348.17	4
34.84	3073.02	738.38	2334.65	1973.91	360.74	4
32.93	3268.38	805.75	2462.63	2093.41	369.23	4
31.03	3462.90	878.07	2584.83	2212.07	372.76	4
31.03	3462.90	878.07	2584.83	2212.07	372.76	3
29.64	3611.46	936.66	2674.80	2298.77	376.04	3
28.25	3759.64	998.38	2761.25	2385.09	376.17	3
26.88	3907.41	1068.61	2838.80	2471.01	367.80	3
25.51	4054.81	1136.55	2918.26	2556.54	361.72	3
24.14	4201.82	1202.16	2999.66	2641.70	357.97	3
22.78	4348.47	1265.80	3082.67	2726.49	356.18	3
21.43	4494.77	1327.80	3166.97	2810.93	356.05	3
20.08	4640.73	1388.35	3252.38	2895.02	357.35	3
18.74	4786.34	1447.70	3338.64	2978.78	359.86	3
18.74	4786.34	1447.70	3338.64	2978.78	359.86	2

16.83	4991.92	1528.85	3463.07	3098.27	364.81	2
14.92	5197.00	1611.38	3585.62	3217.25	368.38	2
13.02	5401.57	1695.81	3705.75	3335.71	370.04	2
11.13	5605.60	1783.11	3822.50	3453.65	368.85	2
9.25	5809.09	1874.99	3934.10	3571.04	363.06	2
7.38	6011.99	1974.58	4037.41	3687.84	349.57	2
5.52	6214.25	2125.19	4089.06	3804.00	285.06	2
3.67	6415.81	2299.99	4115.83	3919.47	196.36	2
1.83	6616.64	2483.16	4133.48	4034.20	99.28	2
.00	6816.72	2668.54	4148.18	4148.17	.00	2

Time = 730. Degree of Consolidation = 28.%

Total Settlement = .887

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 730. = .887

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	6.78	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1
3.52	3.37	1.78	.98	.90	.90	1
1.76	1.68	.89	.98	.90	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
6.78	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.37	401.13	180.64	220.49	212.81	7.67	1
1.68	600.49	239.09	361.40	318.01	43.39	1
.00	799.67	277.03	522.64	423.03	99.61	1

Time = 730. Degree of Consolidation = 98.%

Total Settlement = .251

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 730. = .251

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.49

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.43	21.42	6.50	5.62	5.36	6
60.02	58.92	21.35	6.49	5.65	5.35	6
59.45	58.42	21.27	6.47	5.69	5.33	6
58.89	57.91	21.20	6.46	5.72	5.32	6
58.33	57.40	21.12	6.44	5.75	5.31	6
57.76	56.89	21.05	6.43	5.78	5.29	6
57.20	56.38	20.97	6.42	5.81	5.28	6
56.64	55.86	20.90	6.40	5.83	5.26	6
56.08	55.35	20.82	6.39	5.85	5.25	6
56.08	55.35	20.82	4.51	4.07	3.57	5
54.82	54.18	20.59	4.44	4.02	3.51	5
53.56	53.02	20.36	4.38	3.98	3.45	5
52.32	51.87	20.12	4.32	3.92	3.38	5
51.10	50.74	19.89	4.25	3.87	3.34	5
49.88	49.61	19.66	4.19	3.81	3.31	5
48.69	48.50	19.43	4.13	3.75	3.28	5
48.69	48.50	19.43	1.93	1.91	1.86	4
46.69	46.52	18.75	1.92	1.90	1.84	4
44.70	44.55	18.06	1.91	1.88	1.82	4
42.72	42.59	17.38	1.89	1.87	1.80	4
40.75	40.63	16.70	1.88	1.86	1.78	4
38.79	38.68	16.01	1.86	1.84	1.75	4
36.85	36.75	15.33	1.84	1.83	1.73	4
34.91	34.82	14.65	1.82	1.81	1.71	4
33.00	32.91	13.97	1.80	1.79	1.69	4
31.09	31.01	13.28	1.78	1.77	1.67	4
31.09	31.01	13.28	1.47	1.47	1.41	3
29.70	29.62	12.72	1.46	1.46	1.40	3
28.32	28.24	12.16	1.45	1.45	1.39	3
26.94	26.86	11.59	1.44	1.44	1.38	3
25.57	25.49	11.03	1.43	1.43	1.37	3
24.21	24.13	10.47	1.42	1.42	1.36	3
22.84	22.77	9.90	1.41	1.41	1.35	3
21.49	21.42	9.34	1.40	1.40	1.34	3
20.14	20.07	8.78	1.39	1.39	1.33	3
18.80	18.73	8.21	1.38	1.38	1.32	3
18.80	18.73	8.21	1.34	1.34	1.29	2
16.88	16.81	7.39	1.33	1.33	1.28	2
14.97	14.91	6.57	1.32	1.32	1.27	2
13.07	13.01	5.75	1.31	1.31	1.26	2
11.18	11.12	4.93	1.30	1.29	1.26	2
9.30	9.24	4.11	1.29	1.28	1.25	2
7.43	7.37	3.29	1.28	1.27	1.24	2
5.56	5.51	2.46	1.27	1.26	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.43	799.59	291.34	508.25	422.96	85.29	6
58.92	835.51	279.92	555.59	454.25	101.34	6
58.42	871.58	268.86	602.72	485.70	117.02	6

57.91	907.81	258.24	649.57	517.31	132.26	6
57.40	944.19	248.15	696.04	549.07	146.97	6
56.89	980.70	238.67	742.03	580.96	161.07	6
56.38	1017.35	229.88	787.47	612.99	174.48	6
55.86	1054.11	221.86	832.25	645.13	187.12	6
55.35	1090.99	214.69	876.29	677.39	198.91	6
55.35	1090.99	214.69	876.29	677.39	198.91	5
54.18	1189.72	232.69	957.03	750.37	206.66	5
53.02	1287.80	251.92	1035.87	822.70	213.18	5
51.87	1385.16	272.41	1112.75	894.31	218.44	5
50.74	1481.76	294.16	1187.60	965.16	222.44	5
49.61	1577.56	317.18	1260.37	1035.21	225.17	5
48.50	1672.51	341.46	1331.05	1104.41	226.64	5
48.50	1672.51	341.46	1331.05	1104.41	226.64	4
46.52	1871.98	404.40	1467.58	1228.02	239.56	4
44.55	2070.99	476.03	1594.96	1351.17	243.79	4
42.59	2269.48	532.52	1736.96	1473.80	263.16	4
40.63	2467.39	582.53	1884.86	1595.85	289.00	4
38.68	2664.69	635.68	2029.01	1717.29	311.71	4
36.75	2861.33	692.22	2169.11	1838.08	331.04	4
34.82	3057.28	752.51	2304.77	1958.17	346.61	4
32.91	3252.49	817.24	2435.24	2077.51	357.73	4
31.01	3446.88	887.64	2559.25	2196.05	363.19	4
31.01	3446.88	887.64	2559.25	2196.05	363.20	3
29.62	3595.39	944.40	2650.98	2282.69	368.29	3
28.24	3743.52	1005.28	2738.24	2368.97	369.27	3
26.86	3891.26	1074.51	2816.75	2454.85	361.90	3
25.49	4038.62	1141.87	2896.75	2540.35	356.40	3
24.13	4185.61	1207.38	2978.23	2625.48	352.75	3
22.77	4332.23	1271.19	3061.04	2710.24	350.80	3
21.42	4478.50	1333.39	3145.10	2794.65	350.45	3
20.07	4624.42	1394.17	3230.25	2878.72	351.54	3
18.73	4770.00	1453.72	3316.28	2962.44	353.84	3
18.73	4770.00	1453.72	3316.28	2962.44	353.84	2
16.81	4975.55	1535.26	3440.29	3081.89	358.40	2
14.91	5180.58	1618.64	3561.94	3200.82	361.11	2
13.01	5385.10	1704.62	3680.48	3319.24	361.23	2
11.12	5589.07	1794.49	3794.58	3437.12	357.46	2
9.24	5792.48	1889.89	3902.59	3554.43	348.16	2
7.37	5995.28	1993.36	4001.91	3671.13	330.78	2
5.51	6197.41	2155.56	4041.86	3787.17	254.69	2
3.66	6398.86	2325.68	4073.18	3902.51	170.67	2
1.83	6599.60	2497.94	4101.66	4017.16	84.50	2
.00	6799.65	2668.54	4131.11	4131.10	.00	2

Time = 1080. Degree of Consolidation = 37.%

Total Settlement = 1.159

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 1080. = 1.159

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	6.78	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1
3.52	3.37	1.78	.98	.90	.90	1
1.76	1.68	.89	.98	.90	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
6.78	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.37	401.13	183.21	217.92	212.81	5.11	1
1.68	600.46	249.31	351.15	317.98	33.16	1
.00	799.59	291.34	508.25	422.96	85.29	1

Time = 1080. Degree of Consolidation = 98.%

Total Settlement = .252

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 1080. = .252

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.22

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.18	21.42	6.50	5.58	5.36	6
60.02	58.68	21.35	6.49	5.61	5.35	6
59.45	58.18	21.27	6.47	5.63	5.33	6
58.89	57.68	21.20	6.46	5.65	5.32	6
58.33	57.18	21.12	6.44	5.67	5.31	6
57.76	56.67	21.05	6.43	5.69	5.29	6
57.20	56.17	20.97	6.42	5.71	5.28	6
56.64	55.66	20.90	6.40	5.72	5.26	6
56.08	55.15	20.82	6.39	5.74	5.25	6
56.08	55.15	20.82	4.51	3.97	3.57	5
54.82	54.00	20.59	4.44	3.93	3.51	5
53.56	52.87	20.36	4.38	3.87	3.45	5
52.32	51.74	20.12	4.32	3.82	3.38	5
51.10	50.63	19.89	4.25	3.77	3.34	5
49.88	49.53	19.66	4.19	3.71	3.31	5
48.69	48.45	19.43	4.13	3.65	3.28	5
48.69	48.45	19.43	1.93	1.90	1.86	4
46.69	46.47	18.75	1.92	1.89	1.84	4
44.70	44.51	18.06	1.91	1.88	1.82	4
42.72	42.55	17.38	1.89	1.86	1.80	4
40.75	40.59	16.70	1.88	1.85	1.78	4

38.79	38.65	16.01	1.86	1.75	4	
36.85	36.72	15.33	1.84	1.82	1.73	4
34.91	34.80	14.65	1.82	1.80	1.71	4
33.00	32.89	13.97	1.80	1.79	1.69	4
31.09	30.99	13.28	1.78	1.77	1.67	4
31.09	30.99	13.28	1.47	1.47	1.41	3
29.70	29.61	12.72	1.46	1.46	1.40	3
28.32	28.22	12.16	1.45	1.45	1.39	3
26.94	26.85	11.59	1.44	1.44	1.38	3
25.57	25.48	11.03	1.43	1.43	1.37	3
24.21	24.12	10.47	1.42	1.42	1.36	3
22.84	22.76	9.90	1.41	1.41	1.35	3
21.49	21.41	9.34	1.40	1.40	1.34	3
20.14	20.06	8.78	1.39	1.39	1.33	3
18.80	18.72	8.21	1.38	1.38	1.32	3
18.80	18.72	8.21	1.34	1.33	1.29	2
16.88	16.80	7.39	1.33	1.32	1.28	2
14.97	14.90	6.57	1.32	1.31	1.27	2
13.07	13.00	5.75	1.31	1.30	1.26	2
11.18	11.11	4.93	1.30	1.29	1.26	2
9.30	9.24	4.11	1.29	1.28	1.25	2
7.43	7.37	3.29	1.28	1.27	1.24	2
5.56	5.51	2.46	1.27	1.26	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.18	799.53	304.17	495.36	422.89	72.47	6
58.68	835.23	296.08	539.16	453.98	85.18	6
58.18	871.05	288.32	582.73	485.18	97.56	6
57.68	906.98	280.96	626.03	516.48	109.54	6
57.18	943.01	274.05	668.96	547.89	121.07	6
56.67	979.14	267.67	711.47	579.40	132.07	6
56.17	1015.35	261.88	753.47	610.99	142.48	6
55.66	1051.64	256.74	794.89	642.66	152.24	6
55.15	1087.99	252.31	835.68	674.39	161.29	6
55.15	1087.99	252.31	835.68	674.39	161.29	5
54.00	1185.35	271.96	913.39	746.00	167.39	5
52.87	1281.99	292.53	989.46	816.89	172.57	5
51.74	1377.87	314.06	1063.82	887.02	176.79	5
50.63	1472.97	336.55	1136.42	956.37	180.05	5
49.53	1567.24	360.01	1207.23	1024.89	182.34	5
48.45	1660.65	384.43	1276.22	1092.55	183.67	5
48.45	1660.65	384.43	1276.22	1092.55	183.67	4
46.47	1859.82	448.70	1411.12	1215.86	195.26	4
44.51	2058.52	512.13	1546.39	1338.71	207.69	4
42.55	2256.71	557.57	1699.13	1461.03	238.10	4
40.59	2454.33	605.68	1848.66	1582.80	265.86	4
38.65	2651.37	656.72	1994.65	1703.97	290.68	4
36.72	2847.78	711.10	2136.68	1824.52	312.16	4
34.80	3043.51	769.34	2274.18	1944.40	329.78	4
32.89	3238.52	832.24	2406.28	2063.55	342.73	4
30.99	3432.75	901.23	2531.52	2181.92	349.60	4
30.99	3432.75	901.23	2531.52	2181.92	349.60	3
29.61	3581.17	956.63	2624.55	2268.48	356.06	3
28.22	3729.23	1017.31	2711.92	2354.68	357.24	3
26.85	3876.91	1084.62	2792.29	2440.51	351.79	3
25.48	4024.22	1150.56	2873.66	2525.95	347.71	3
24.12	4171.16	1215.11	2956.05	2611.03	345.01	3

22.76	4317.74	1278.34	3039.40	2695.76	343.64	3
21.41	4463.97	1340.33	3123.64	2780.13	343.52	3
20.06	4609.85	1401.15	3208.70	2864.15	344.55	3
18.72	4755.40	1460.98	3294.42	2947.84	346.58	3
18.72	4755.40	1460.98	3294.42	2947.84	346.58	2
16.80	4960.89	1543.08	3417.82	3067.24	350.58	2
14.90	5165.88	1627.51	3538.37	3186.12	352.25	2
13.00	5370.33	1714.97	3655.36	3304.48	350.88	2
11.11	5574.24	1806.60	3767.64	3422.29	345.35	2
9.24	5777.57	1903.96	3873.60	3539.52	334.09	2
7.37	5980.27	2012.91	3967.36	3656.12	311.24	2
5.51	6182.32	2177.22	4005.10	3772.07	233.03	2
3.66	6383.68	2342.44	4041.25	3887.34	153.91	2
1.83	6584.38	2507.05	4077.33	4001.93	75.40	2
.00	6784.40	2668.54	4115.86	4115.86	.00	2

Time = 1440. Degree of Consolidation = 44.%

Total Settlement = 1.402

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 1440. = 1.402

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
7.03	6.78	3.55
5.27	5.06	2.66
3.52	3.37	1.78
1.76	1.68	.89
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
6.78	.00	.00
5.06	201.40	94.16
3.37	401.12	185.32
1.68	600.44	258.23
.00	799.53	304.17

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
107.24	107.24	.00	1
215.80	212.80	3.00	1
342.20	317.96	24.24	1
495.36	422.89	72.47	1

Time = 1440. Degree of Consolidation = 99.%

Total Settlement = .253

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 1440. = .253

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.97

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.95	21.42	6.50	5.54	5.36	6
60.02	58.46	21.35	6.49	5.56	5.35	6
59.45	57.96	21.27	6.47	5.57	5.33	6
58.89	57.46	21.20	6.46	5.59	5.32	6
58.33	56.97	21.12	6.44	5.60	5.31	6
57.76	56.47	21.05	6.43	5.61	5.29	6
57.20	55.97	20.97	6.42	5.62	5.28	6
56.64	55.47	20.90	6.40	5.63	5.26	6
56.08	54.97	20.82	6.39	5.63	5.25	6
56.08	54.97	20.82	4.51	3.89	3.57	5
54.82	53.84	20.59	4.44	3.84	3.51	5
53.56	52.72	20.36	4.38	3.78	3.45	5
52.32	51.62	20.12	4.32	3.73	3.38	5
51.10	50.53	19.89	4.25	3.67	3.34	5
49.88	49.46	19.66	4.19	3.61	3.31	5
48.69	48.39	19.43	4.13	3.55	3.28	5
48.69	48.39	19.43	1.93	1.89	1.86	4
46.69	46.42	18.75	1.92	1.88	1.84	4
44.70	44.46	18.06	1.91	1.87	1.82	4
42.72	42.50	17.38	1.89	1.86	1.80	4
40.75	40.56	16.70	1.88	1.84	1.78	4
38.79	38.62	16.01	1.86	1.83	1.75	4
36.85	36.69	15.33	1.84	1.82	1.73	4
34.91	34.77	14.65	1.82	1.80	1.71	4
33.00	32.87	13.97	1.80	1.78	1.69	4
31.09	30.97	13.28	1.78	1.76	1.67	4
31.09	30.97	13.28	1.47	1.46	1.41	3
29.70	29.59	12.72	1.46	1.46	1.40	3
28.32	28.21	12.16	1.45	1.44	1.39	3
26.94	26.83	11.59	1.44	1.43	1.38	3
25.57	25.46	11.03	1.43	1.42	1.37	3
24.21	24.10	10.47	1.42	1.41	1.36	3
22.84	22.75	9.90	1.41	1.40	1.35	3
21.49	21.39	9.34	1.40	1.39	1.34	3
20.14	20.05	8.78	1.39	1.38	1.33	3
18.80	18.71	8.21	1.38	1.37	1.32	3
18.80	18.71	8.21	1.34	1.33	1.29	2
16.88	16.80	7.39	1.33	1.32	1.28	2
14.97	14.89	6.57	1.32	1.31	1.27	2
13.07	13.00	5.75	1.31	1.30	1.26	2
11.18	11.11	4.93	1.30	1.29	1.26	2
9.30	9.23	4.11	1.29	1.28	1.25	2
7.43	7.36	3.29	1.28	1.27	1.24	2
5.56	5.51	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
58.95	799.46	316.44	483.02	422.83	60.20	6
58.46	834.98	311.28	523.70	453.72	69.98	6
57.96	870.56	306.42	564.14	484.68	79.46	6
57.46	906.21	301.91	604.30	515.71	88.59	6
56.97	941.92	297.81	644.11	546.80	97.31	6
56.47	977.69	294.15	683.53	577.95	105.58	6
55.97	1013.50	291.01	722.49	609.14	113.35	6
55.47	1049.36	288.42	760.94	640.38	120.56	6
54.97	1085.25	286.43	798.82	671.65	127.17	6
54.97	1085.25	286.43	798.82	671.65	127.17	5
53.84	1181.35	307.61	873.75	742.00	131.74	5
52.72	1276.69	329.47	947.22	811.59	135.63	5
51.62	1371.23	352.03	1019.19	880.38	138.82	5
50.53	1464.94	375.31	1089.63	948.34	141.29	5
49.46	1557.81	399.31	1158.50	1015.46	143.04	5
48.39	1649.81	424.01	1225.79	1081.71	144.09	5
48.39	1649.81	424.01	1225.79	1081.71	144.09	4
46.42	1848.70	490.84	1357.85	1204.74	153.12	4
44.46	2047.11	536.83	1510.28	1327.29	182.99	4
42.50	2245.00	581.37	1663.63	1449.33	214.31	4
40.56	2442.35	628.37	1813.98	1570.82	243.16	4
38.62	2639.13	678.15	1960.97	1691.73	269.24	4
36.69	2835.28	731.16	2104.13	1812.03	292.10	4
34.77	3030.79	788.03	2242.76	1931.67	311.09	4
32.87	3225.59	849.73	2375.86	2050.61	325.25	4
30.97	3419.61	917.74	2501.87	2168.78	333.09	4
30.97	3419.61	917.74	2501.87	2168.78	333.09	3
29.59	3567.93	972.18	2595.75	2255.24	340.51	3
28.21	3715.89	1033.23	2682.66	2341.34	341.32	3
26.83	3863.49	1098.48	2765.01	2427.08	337.93	3
25.46	4010.73	1162.76	2847.96	2512.46	335.50	3
24.10	4157.60	1226.05	2931.55	2597.48	334.07	3
22.75	4304.12	1288.41	3015.72	2682.14	333.58	3
21.39	4450.30	1349.85	3100.44	2766.45	333.99	3
20.05	4596.13	1410.47	3185.65	2850.43	335.23	3
18.71	4741.62	1470.39	3271.23	2934.06	337.17	3
18.71	4741.62	1470.39	3271.23	2934.06	337.17	2
16.80	4947.06	1552.67	3394.39	3053.40	340.99	2
14.89	5151.98	1637.66	3514.32	3172.22	342.10	2
13.00	5356.37	1726.15	3630.22	3290.52	339.71	2
11.11	5560.21	1818.92	3741.29	3408.25	333.04	2
9.23	5763.46	1917.14	3846.31	3525.40	320.91	2
7.36	5966.08	2032.62	3933.46	3641.93	291.53	2
5.51	6168.05	2194.13	3973.92	3757.80	216.12	2
3.66	6369.35	2355.04	4014.31	3873.01	141.31	2
1.83	6570.00	2513.74	4056.27	3987.56	68.71	2
.00	6770.01	2668.54	4101.47	4101.47	.00	2

Time = 1825. Degree of Consolidation = 52.%

Total Settlement = 1.632

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 1825. = 1.632

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	6.78	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1
3.52	3.37	1.78	.98	.90	.90	1
1.76	1.68	.89	.98	.90	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
6.78	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.37	401.12	187.19	213.93	212.80	1.13	1
1.68	600.41	266.52	333.89	317.93	15.96	1
.00	799.46	316.44	483.02	422.83	60.20	1

Time = 1825. Degree of Consolidation = 99.%

Total Settlement = .254

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 1825. = .254

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.74

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.65	21.42	6.50	5.52	5.36	6
60.02	58.15	21.35	6.49	5.52	5.35	6
59.45	57.66	21.27	6.47	5.52	5.33	6
58.89	57.17	21.20	6.46	5.51	5.32	6
58.33	56.68	21.12	6.44	5.51	5.31	6
57.76	56.18	21.05	6.43	5.51	5.29	6
57.20	55.69	20.97	6.42	5.51	5.28	6
56.64	55.20	20.90	6.40	5.51	5.26	6
56.08	54.71	20.82	6.39	5.50	5.25	6
56.08	54.71	20.82	4.51	3.78	3.57	5
54.82	53.61	20.59	4.44	3.72	3.51	5
53.56	52.52	20.36	4.38	3.67	3.45	5
52.32	51.44	20.12	4.32	3.61	3.38	5
51.10	50.38	19.89	4.25	3.55	3.34	5
49.88	49.33	19.66	4.19	3.49	3.31	5
48.69	48.30	19.43	4.13	3.43	3.28	5

48.69	48.30	19.43	1.93	1.88	1.86	4
46.69	46.33	18.75	1.92	1.87	1.84	4
44.70	44.38	18.06	1.91	1.86	1.82	4
42.72	42.43	17.38	1.89	1.85	1.80	4
40.75	40.49	16.70	1.88	1.83	1.78	4
38.79	38.55	16.01	1.86	1.82	1.75	4
36.85	36.63	15.33	1.84	1.81	1.73	4
34.91	34.72	14.65	1.82	1.79	1.71	4
33.00	32.82	13.97	1.80	1.77	1.69	4
31.09	30.93	13.28	1.78	1.75	1.67	4
31.09	30.93	13.28	1.47	1.46	1.41	3
29.70	29.55	12.72	1.46	1.45	1.40	3
28.32	28.18	12.16	1.45	1.44	1.39	3
26.94	26.80	11.59	1.44	1.43	1.38	3
25.57	25.44	11.03	1.43	1.42	1.37	3
24.21	24.08	10.47	1.42	1.41	1.36	3
22.84	22.72	9.90	1.41	1.40	1.35	3
21.49	21.37	9.34	1.40	1.39	1.34	3
20.14	20.03	8.78	1.39	1.38	1.33	3
18.80	18.69	8.21	1.38	1.37	1.32	3
18.80	18.69	8.21	1.34	1.33	1.29	2
16.88	16.78	7.39	1.33	1.32	1.28	2
14.97	14.88	6.57	1.32	1.31	1.27	2
13.07	12.99	5.75	1.31	1.30	1.26	2
11.18	11.10	4.93	1.30	1.29	1.26	2
9.30	9.23	4.11	1.29	1.28	1.25	2
7.43	7.36	3.29	1.28	1.27	1.24	2
5.56	5.51	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.65	799.34	325.76	473.58	422.70	50.88	6
58.15	834.68	325.85	508.83	453.42	55.41	6
57.66	870.02	325.99	544.03	484.14	59.89	6
57.17	905.36	326.21	579.14	514.86	64.28	6
56.68	940.69	326.57	614.12	545.57	68.55	6
56.18	976.02	327.09	648.93	576.28	72.65	6
55.69	1011.33	327.81	683.52	606.97	76.55	6
55.20	1046.64	328.78	717.86	637.66	80.20	6
54.71	1081.93	330.02	751.91	668.33	83.58	6
54.71	1081.93	330.02	751.91	668.33	83.58	5
53.61	1176.43	353.36	823.08	737.08	85.99	5
52.52	1270.10	376.71	893.39	805.00	88.39	5
51.44	1362.93	400.09	962.84	872.08	90.76	5
50.38	1454.91	423.50	1031.41	938.31	93.10	5
49.33	1546.06	446.93	1099.13	1003.71	95.42	5
48.30	1636.37	470.34	1166.03	1068.27	97.76	5
48.30	1636.37	470.34	1166.03	1068.27	97.76	4
46.33	1834.92	525.70	1309.21	1190.96	118.26	4
44.38	2032.94	570.05	1462.90	1313.12	149.77	4
42.43	2230.43	615.63	1614.80	1434.76	180.05	4
40.49	2427.37	662.90	1764.47	1555.83	208.64	4
38.55	2623.73	712.38	1911.36	1676.34	235.02	4
36.63	2819.49	764.69	2054.80	1796.23	258.57	4
34.72	3014.60	820.68	2193.92	1915.48	278.44	4
32.82	3209.01	881.53	2327.48	2034.04	293.45	4
30.93	3402.66	949.21	2453.45	2151.83	301.62	4
30.93	3402.66	949.21	2453.45	2151.83	301.62	3

29.55	3550.78	1003.23	2547.55	2238.09	309.46	3
28.18	3698.55	1065.84	2632.72	2324.00	308.71	3
26.80	3845.98	1128.00	2717.98	2409.57	308.41	3
25.44	3993.05	1189.67	2803.38	2494.79	308.60	3
24.08	4139.78	1250.85	2888.93	2579.66	309.27	3
22.72	4286.17	1311.53	2974.64	2664.19	310.45	3
21.37	4432.22	1371.75	3060.46	2748.37	312.09	3
20.03	4577.93	1431.57	3146.36	2832.23	314.13	3
18.69	4723.30	1491.12	3232.18	2915.74	316.43	3
18.69	4723.30	1491.13	3232.18	2915.74	316.43	2
16.78	4928.61	1572.63	3355.98	3034.96	321.03	2
14.88	5133.42	1657.57	3475.85	3153.66	322.19	2
12.99	5337.68	1746.24	3591.45	3271.83	319.62	2
11.10	5541.39	1839.18	3702.22	3389.44	312.77	2
9.23	5744.52	1937.28	3807.24	3506.47	300.77	2
7.36	5947.02	2060.39	3886.64	3622.87	263.76	2
5.51	6148.89	2216.96	3931.93	3738.64	193.29	2
3.66	6350.11	2371.15	3978.96	3853.77	125.20	2
1.83	6550.71	2521.99	4028.72	3968.27	60.45	2
.00	6750.70	2668.54	4082.16	4082.16	.00	2

Time = 2520. Degree of Consolidation = 61.%

Total Settlement = 1.939

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 2520. = 1.939

Settlement caused by Secondary Compression at time 2520. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
7.03	6.77	3.55
5.27	5.06	2.66
3.52	3.36	1.78
1.76	1.68	.89
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
6.77	.00	.00
5.06	201.40	94.16
3.36	401.12	188.32
1.68	600.38	282.48
.00	799.34	350.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
107.24	107.24	.00	1
212.80	212.80	.00	1
317.90	317.90	.00	1
449.34	422.70	26.64	1

Time = 2520. Degree of Consolidation = 100.%

Total Settlement = .256

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 2520. = .256

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.43

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.53	21.42	6.50	5.49	5.36	6
60.02	58.04	21.35	6.49	5.49	5.35	6
59.45	57.55	21.27	6.47	5.49	5.33	6
58.89	57.06	21.20	6.46	5.48	5.32	6
58.33	56.57	21.12	6.44	5.48	5.31	6
57.76	56.08	21.05	6.43	5.48	5.29	6
57.20	55.59	20.97	6.42	5.47	5.28	6
56.64	55.11	20.90	6.40	5.47	5.26	6
56.08	54.62	20.82	6.39	5.46	5.25	6
56.08	54.62	20.82	4.51	3.75	3.57	5
54.82	53.52	20.59	4.44	3.69	3.51	5
53.56	52.44	20.36	4.38	3.63	3.45	5
52.32	51.38	20.12	4.32	3.57	3.38	5
51.10	50.32	19.89	4.25	3.51	3.34	5
49.88	49.28	19.66	4.19	3.46	3.31	5
48.69	48.26	19.43	4.13	3.40	3.28	5
48.69	48.26	19.43	1.93	1.88	1.86	4
46.69	46.29	18.75	1.92	1.87	1.84	4
44.70	44.34	18.06	1.91	1.86	1.82	4
42.72	42.39	17.38	1.89	1.84	1.80	4
40.75	40.45	16.70	1.88	1.83	1.78	4
38.79	38.52	16.01	1.86	1.82	1.75	4
36.85	36.60	15.33	1.84	1.80	1.73	4
34.91	34.70	14.65	1.82	1.79	1.71	4
33.00	32.80	13.97	1.80	1.77	1.69	4
31.09	30.91	13.28	1.78	1.75	1.67	4
31.09	30.91	13.28	1.47	1.46	1.41	3
29.70	29.53	12.72	1.46	1.45	1.40	3
28.32	28.16	12.16	1.45	1.44	1.39	3
26.94	26.79	11.59	1.44	1.43	1.38	3
25.57	25.43	11.03	1.43	1.42	1.37	3
24.21	24.07	10.47	1.42	1.41	1.36	3
22.84	22.71	9.90	1.41	1.40	1.35	3
21.49	21.36	9.34	1.40	1.39	1.34	3
20.14	20.02	8.78	1.39	1.38	1.33	3
18.80	18.69	8.21	1.38	1.37	1.32	3
18.80	18.69	8.21	1.34	1.33	1.29	2
16.88	16.78	7.39	1.33	1.32	1.28	2
14.97	14.87	6.57	1.32	1.31	1.27	2
13.07	12.98	5.75	1.31	1.30	1.26	2
11.18	11.10	4.93	1.30	1.29	1.26	2
9.30	9.22	4.11	1.29	1.28	1.25	2
7.43	7.36	3.29	1.28	1.26	1.24	2
5.56	5.50	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2

1.85	1.83	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.53	799.34	335.26	464.08	422.70	41.38	6
58.04	834.54	335.58	498.96	453.28	45.68	6
57.55	869.74	336.09	533.65	483.86	49.79	6
57.06	904.93	336.78	568.15	514.43	53.72	6
56.57	940.11	337.67	602.44	544.99	57.45	6
56.08	975.27	338.78	636.50	575.53	60.96	6
55.59	1010.42	340.11	670.31	606.06	64.25	6
55.11	1045.55	341.68	703.87	636.57	67.30	6
54.62	1080.65	343.50	737.15	667.05	70.10	6
54.62	1080.65	343.50	737.15	667.05	70.10	5
53.52	1174.66	367.22	807.45	735.31	72.13	5
52.44	1267.83	390.82	877.00	802.73	74.28	5
51.38	1360.14	414.31	945.84	869.29	76.54	5
50.32	1451.62	437.65	1013.97	935.02	78.95	5
49.28	1542.27	460.84	1081.43	999.92	81.51	5
48.26	1632.08	483.84	1148.24	1063.98	84.26	5
48.26	1632.08	483.84	1148.24	1063.98	84.26	4
46.29	1830.52	535.62	1294.91	1186.56	108.34	4
44.34	2028.42	581.50	1446.92	1308.60	138.31	4
42.39	2225.77	628.35	1597.41	1430.09	167.32	4
40.45	2422.55	676.63	1745.92	1551.01	194.91	4
38.52	2618.74	726.91	1891.83	1671.34	220.49	4
36.60	2814.32	779.89	2034.43	1791.06	243.37	4
34.70	3009.24	836.54	2172.70	1910.13	262.58	4
32.80	3203.46	898.29	2305.17	2028.49	276.68	4
30.91	3396.90	967.51	2429.39	2146.07	283.32	4
30.91	3396.90	967.51	2429.39	2146.07	283.32	3
29.53	3544.91	1022.93	2521.98	2232.22	289.76	3
28.16	3692.58	1083.91	2608.67	2318.03	290.64	3
26.79	3839.90	1144.64	2695.26	2403.49	291.77	3
25.43	3986.89	1205.07	2781.82	2488.62	293.20	3
24.07	4133.53	1265.23	2868.30	2573.41	294.89	3
22.71	4279.84	1325.07	2954.77	2657.86	296.91	3
21.36	4425.82	1384.62	3041.20	2741.97	299.22	3
20.02	4571.45	1443.92	3127.54	2825.75	301.79	3
18.69	4716.76	1503.09	3213.67	2909.20	304.47	3
18.69	4716.76	1503.09	3213.67	2909.20	304.47	2
16.78	4922.00	1583.85	3338.15	3028.34	309.81	2
14.87	5126.74	1668.06	3458.68	3146.98	311.70	2
12.98	5330.94	1756.28	3574.66	3265.09	309.57	2
11.10	5534.59	1848.81	3685.78	3382.64	303.14	2
9.22	5737.66	1946.50	3791.16	3499.61	291.55	2
7.36	5940.11	2072.55	3867.56	3615.96	251.60	2
5.50	6141.93	2226.35	3915.57	3731.68	183.89	2
3.66	6343.12	2377.41	3965.71	3846.78	118.93	2
1.83	6543.70	2525.13	4018.58	3961.26	57.32	2
.00	6743.69	2668.54	4075.15	4075.15	.00	2

Time = 2880. Degree of Consolidation = 65.%

Total Settlement = 2.051

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 2880. = 2.051

Settlement caused by Secondary Compression at time 2880. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	6.77	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1
3.52	3.36	1.78	.98	.90	.90	1
1.76	1.68	.89	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
6.77	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.36	401.12	188.32	212.80	212.80	.00	1
1.68	600.38	282.48	317.90	317.90	.00	1
.00	799.34	350.00	449.34	422.70	26.64	1

Time = 2880. Degree of Consolidation = 100.%

Total Settlement = .256

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 2880. = .256

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.32

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.44	21.42	6.50	5.47	5.36	6
60.02	57.95	21.35	6.49	5.46	5.35	6
59.45	57.46	21.27	6.47	5.46	5.33	6
58.89	56.97	21.20	6.46	5.46	5.32	6
58.33	56.48	21.12	6.44	5.45	5.31	6
57.76	56.00	21.05	6.43	5.45	5.29	6
57.20	55.51	20.97	6.42	5.44	5.28	6
56.64	55.02	20.90	6.40	5.44	5.26	6
56.08	54.54	20.82	6.39	5.43	5.25	6
56.08	54.54	20.82	4.51	3.72	3.57	5
54.82	53.45	20.59	4.44	3.66	3.51	5

53.56	52.38	20.36	4.38	3.60	3.45	5
52.32	51.32	20.12	4.32	3.54	3.38	5
51.10	50.27	19.89	4.25	3.49	3.34	5
49.88	49.23	19.66	4.19	3.43	3.31	5
48.69	48.21	19.43	4.13	3.37	3.28	5
48.69	48.21	19.43	1.93	1.88	1.86	4
46.69	46.25	18.75	1.92	1.87	1.84	4
44.70	44.30	18.06	1.91	1.85	1.82	4
42.72	42.35	17.38	1.89	1.84	1.80	4
40.75	40.42	16.70	1.88	1.83	1.78	4
38.79	38.49	16.01	1.86	1.81	1.75	4
36.85	36.57	15.33	1.84	1.80	1.73	4
34.91	34.67	14.65	1.82	1.78	1.71	4
33.00	32.78	13.97	1.80	1.76	1.69	4
31.09	30.89	13.28	1.78	1.74	1.67	4
31.09	30.89	13.28	1.47	1.45	1.41	3
29.70	29.52	12.72	1.46	1.44	1.40	3
28.32	28.14	12.16	1.45	1.43	1.39	3
26.94	26.77	11.59	1.44	1.42	1.38	3
25.57	25.41	11.03	1.43	1.41	1.37	3
24.21	24.05	10.47	1.42	1.41	1.36	3
22.84	22.70	9.90	1.41	1.40	1.35	3
21.49	21.36	9.34	1.40	1.39	1.34	3
20.14	20.01	8.78	1.39	1.38	1.33	3
18.80	18.68	8.21	1.38	1.37	1.32	3
18.80	18.68	8.21	1.34	1.33	1.29	2
16.88	16.77	7.39	1.33	1.32	1.28	2
14.97	14.87	6.57	1.32	1.31	1.27	2
13.07	12.98	5.75	1.31	1.30	1.26	2
11.18	11.09	4.93	1.30	1.29	1.26	2
9.30	9.22	4.11	1.29	1.28	1.25	2
7.43	7.36	3.29	1.28	1.26	1.24	2
5.56	5.50	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.82	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.44	799.34	341.89	457.44	422.70	34.75	6
57.95	834.44	342.90	491.54	453.18	38.36	6
57.46	869.53	344.04	525.49	483.65	41.84	6
56.97	904.60	345.33	559.27	514.10	45.17	6
56.48	939.66	346.78	592.87	544.54	48.34	6
56.00	974.69	348.40	626.29	574.95	51.34	6
55.51	1009.69	350.19	659.50	605.34	54.17	6
55.02	1044.67	352.17	692.51	635.70	56.81	6
54.54	1079.63	354.33	725.29	666.03	59.27	6
54.54	1079.63	354.33	725.29	666.03	59.27	5
53.45	1173.24	378.29	794.95	733.89	61.06	5
52.38	1266.01	402.03	863.98	800.91	63.07	5
51.32	1357.92	425.52	932.40	867.07	65.33	5
50.27	1449.00	448.77	1000.23	932.40	67.83	5
49.23	1539.25	471.75	1067.50	996.90	70.60	5
48.21	1628.68	494.45	1134.23	1060.58	73.65	5
48.21	1628.68	494.45	1134.23	1060.58	73.65	4
46.25	1827.03	543.55	1283.48	1183.07	100.41	4
44.30	2024.83	590.87	1433.96	1305.01	128.95	4
42.35	2222.06	639.02	1583.04	1426.38	156.66	4
40.42	2418.70	688.48	1730.23	1547.17	183.06	4
38.49	2614.75	739.83	1874.91	1667.35	207.56	4

36.57	2810.16	793.86	2016.30	1786.91	229.39	4
34.67	3004.91	851.64	2153.27	1905.80	247.47	4
32.78	3198.94	914.72	2284.22	2023.97	260.25	4
30.89	3392.18	985.79	2406.39	2141.35	265.04	4
30.89	3392.18	985.79	2406.39	2141.35	265.04	3
29.52	3540.07	1042.95	2497.12	2227.38	269.74	3
28.14	3687.63	1102.52	2585.11	2313.08	272.03	3
26.77	3834.86	1161.94	2672.92	2398.45	274.47	3
25.41	3981.75	1221.22	2760.52	2483.48	277.04	3
24.05	4128.31	1280.34	2847.96	2568.18	279.78	3
22.70	4274.53	1339.30	2935.23	2652.55	282.68	3
21.36	4420.43	1398.13	3022.29	2736.58	285.71	3
20.01	4565.99	1456.87	3109.12	2820.29	288.83	3
18.68	4711.23	1515.56	3195.66	2903.67	292.00	3
18.68	4711.23	1515.56	3195.66	2903.67	292.00	2
16.77	4916.40	1595.34	3321.05	3022.74	298.32	2
14.87	5121.06	1678.84	3442.22	3141.31	300.92	2
12.98	5325.20	1766.36	3558.84	3259.35	299.49	2
11.09	5528.79	1858.22	3670.57	3376.84	293.73	2
9.22	5731.80	1955.01	3776.79	3493.75	283.04	2
7.36	5934.20	2083.59	3850.61	3610.06	240.56	2
5.50	6135.98	2234.97	3901.01	3725.74	175.28	2
3.66	6337.15	2383.52	3953.63	3840.80	112.83	2
1.82	6537.71	2528.26	4009.45	3955.27	54.18	2
.00	6737.69	2668.54	4069.15	4069.15	.00	2

Time = 3240. Degree of Consolidation = 68.%

Total Settlement = 2.148

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 3240. = 2.148

Settlement caused by Secondary Compression at time 3240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
7.03	6.77	3.55
5.27	5.06	2.66
3.52	3.36	1.78
1.76	1.68	.89
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
6.77	.00	.00
5.06	201.40	94.16
3.36	401.12	188.32
1.68	600.38	282.48
.00	799.34	350.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
107.24	107.24	.00	1
212.80	212.80	.00	1
317.90	317.90	.00	1
449.34	422.70	26.64	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .256

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 3240. = .256

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.23

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.35	21.42	6.50	5.45	5.36	6
60.02	57.86	21.35	6.49	5.44	5.35	6
59.45	57.37	21.27	6.47	5.44	5.33	6
58.89	56.89	21.20	6.46	5.43	5.32	6
58.33	56.40	21.12	6.44	5.43	5.31	6
57.76	55.92	21.05	6.43	5.42	5.29	6
57.20	55.43	20.97	6.42	5.42	5.28	6
56.64	54.95	20.90	6.40	5.41	5.26	6
56.08	54.46	20.82	6.39	5.40	5.25	6
56.08	54.46	20.82	4.51	3.70	3.57	5
54.82	53.38	20.59	4.44	3.64	3.51	5
53.56	52.31	20.36	4.38	3.58	3.45	5
52.32	51.26	20.12	4.32	3.52	3.38	5
51.10	50.21	19.89	4.25	3.47	3.34	5
49.88	49.19	19.66	4.19	3.41	3.31	5
48.69	48.17	19.43	4.13	3.36	3.28	5
48.69	48.17	19.43	1.93	1.88	1.86	4
46.69	46.21	18.75	1.92	1.87	1.84	4
44.70	44.25	18.06	1.91	1.85	1.82	4
42.72	42.31	17.38	1.89	1.84	1.80	4
40.75	40.38	16.70	1.88	1.82	1.78	4
38.79	38.45	16.01	1.86	1.81	1.75	4
36.85	36.54	15.33	1.84	1.79	1.73	4
34.91	34.64	14.65	1.82	1.78	1.71	4
33.00	32.75	13.97	1.80	1.76	1.69	4
31.09	30.87	13.28	1.78	1.74	1.67	4
31.09	30.87	13.28	1.47	1.45	1.41	3
29.70	29.49	12.72	1.46	1.44	1.40	3
28.32	28.12	12.16	1.45	1.43	1.39	3
26.94	26.76	11.59	1.44	1.42	1.38	3
25.57	25.40	11.03	1.43	1.41	1.37	3
24.21	24.04	10.47	1.42	1.40	1.36	3
22.84	22.69	9.90	1.41	1.39	1.35	3
21.49	21.34	9.34	1.40	1.38	1.34	3
20.14	20.00	8.78	1.39	1.37	1.33	3
18.80	18.67	8.21	1.38	1.37	1.32	3
18.80	18.67	8.21	1.34	1.33	1.29	2
16.88	16.76	7.39	1.33	1.32	1.28	2
14.97	14.86	6.57	1.32	1.31	1.27	2
13.07	12.97	5.75	1.31	1.30	1.26	2

11.18	11.09	4.93	1.30	1.29	1.26	2
9.30	9.22	4.11	1.29	1.27	1.25	2
7.43	7.36	3.29	1.28	1.26	1.24	2
5.56	5.50	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.82	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.35	799.33	347.74	451.59	422.70	28.90	6
57.86	834.35	349.35	485.00	453.09	31.91	6
57.37	869.35	351.06	518.29	483.47	34.82	6
56.89	904.31	352.87	551.45	513.82	37.63	6
56.40	939.26	354.78	584.48	544.14	40.34	6
55.92	974.17	356.80	617.38	574.43	42.94	6
55.43	1009.06	358.92	650.13	604.70	45.44	6
54.95	1043.91	361.16	682.75	634.93	47.82	6
54.46	1078.73	363.50	715.23	665.13	50.10	6
54.46	1078.73	363.50	715.23	665.13	50.10	5
53.38	1172.02	387.57	784.45	732.67	51.78	5
52.31	1264.45	411.22	853.23	799.35	53.88	5
51.26	1356.04	434.41	921.63	865.19	56.44	5
50.21	1446.81	457.11	989.70	930.21	59.49	5
49.19	1536.77	479.27	1057.50	994.42	63.08	5
48.17	1625.95	501.94	1124.01	1057.85	66.16	5
48.17	1625.95	501.94	1124.01	1057.85	66.16	4
46.21	1824.23	550.77	1273.46	1180.27	93.19	4
44.25	2021.93	599.77	1422.16	1302.11	120.05	4
42.31	2219.04	649.44	1569.60	1423.37	146.24	4
40.38	2415.56	700.31	1715.25	1544.02	171.23	4
38.45	2611.45	753.04	1858.41	1664.05	194.35	4
36.54	2806.70	808.46	1998.25	1783.45	214.80	4
34.64	3001.27	867.71	2133.56	1902.15	231.40	4
32.75	3195.10	932.59	2262.51	2020.12	242.39	4
30.87	3388.11	1005.62	2382.48	2137.27	245.21	4
30.87	3388.11	1005.62	2382.48	2137.27	245.21	3
29.49	3535.88	1064.69	2471.18	2223.19	248.00	3
28.12	3683.32	1123.33	2559.99	2308.77	251.22	3
26.76	3830.43	1181.72	2648.70	2394.02	254.68	3
25.40	3977.21	1239.97	2737.24	2478.94	258.30	3
24.04	4123.67	1298.11	2825.56	2563.54	262.02	3
22.69	4269.80	1356.16	2913.63	2647.81	265.82	3
21.34	4415.60	1414.15	3001.45	2731.75	269.70	3
20.00	4561.07	1472.18	3088.90	2815.37	273.53	3
18.67	4706.22	1530.31	3175.92	2898.66	277.25	3
18.67	4706.22	1530.31	3175.91	2898.66	277.25	2
16.76	4911.31	1608.95	3302.35	3017.65	284.71	2
14.86	5115.89	1691.46	3424.43	3136.14	288.29	2
12.97	5319.96	1778.03	3541.93	3254.10	287.83	2
11.09	5523.48	1868.93	3654.55	3371.53	283.02	2
9.22	5726.43	1964.62	3761.81	3488.38	273.44	2
7.36	5928.77	2095.76	3833.01	3604.62	228.39	2
5.50	6130.51	2244.10	3886.41	3720.26	166.15	2
3.66	6331.64	2389.57	3942.07	3835.30	106.77	2
1.82	6532.19	2531.38	4000.80	3949.74	51.06	2
.00	6732.16	2668.54	4063.62	4063.61	.00	2

Time = 3650. Degree of Consolidation = 71.%

Total Settlement = 2.236

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 3650. = 2.236

Settlement caused by Secondary Compression at time 3650. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	6.77	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1
3.52	3.36	1.78	.98	.90	.90	1
1.76	1.68	.89	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
6.77	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.36	401.12	188.32	212.80	212.80	.00	1
1.68	600.38	282.48	317.90	317.90	.00	1
.00	799.33	350.00	449.33	422.70	26.64	1

Time = 3650. Degree of Consolidation = 100.%

Total Settlement = .256

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 3650. = .256

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.14

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.27	21.42	6.50	5.44	5.36	6
60.02	57.78	21.35	6.49	5.43	5.35	6
59.45	57.30	21.27	6.47	5.43	5.33	6
58.89	56.81	21.20	6.46	5.42	5.32	6
58.33	56.32	21.12	6.44	5.41	5.31	6
57.76	55.84	21.05	6.43	5.41	5.29	6

57.20	55.36	20.97	6.42	5.40	5.28	6
56.64	54.87	20.90	6.40	5.40	5.26	6
56.08	54.39	20.82	6.39	5.39	5.25	6
56.08	54.39	20.82	4.51	3.69	3.57	5
54.82	53.31	20.59	4.44	3.63	3.51	5
53.56	52.24	20.36	4.38	3.57	3.45	5
52.32	51.19	20.12	4.32	3.51	3.38	5
51.10	50.15	19.89	4.25	3.46	3.34	5
49.88	49.12	19.66	4.19	3.41	3.31	5
48.69	48.11	19.43	4.13	3.36	3.28	5
48.69	48.11	19.43	1.93	1.88	1.86	4
46.69	46.15	18.75	1.92	1.86	1.84	4
44.70	44.19	18.06	1.91	1.85	1.82	4
42.72	42.25	17.38	1.89	1.83	1.80	4
40.75	40.32	16.70	1.88	1.82	1.78	4
38.79	38.40	16.01	1.86	1.80	1.75	4
36.85	36.49	15.33	1.84	1.79	1.73	4
34.91	34.59	14.65	1.82	1.77	1.71	4
33.00	32.71	13.97	1.80	1.75	1.69	4
31.09	30.84	13.28	1.78	1.73	1.67	4
31.09	30.84	13.28	1.47	1.44	1.41	3
29.70	29.46	12.72	1.46	1.44	1.40	3
28.32	28.09	12.16	1.45	1.43	1.39	3
26.94	26.73	11.59	1.44	1.42	1.38	3
25.57	25.37	11.03	1.43	1.41	1.37	3
24.21	24.02	10.47	1.42	1.40	1.36	3
22.84	22.67	9.90	1.41	1.39	1.35	3
21.49	21.33	9.34	1.40	1.38	1.34	3
20.14	19.99	8.78	1.39	1.37	1.33	3
18.80	18.66	8.21	1.38	1.36	1.32	3
18.80	18.66	8.21	1.34	1.32	1.29	2
16.88	16.75	7.39	1.33	1.31	1.28	2
14.97	14.85	6.57	1.32	1.30	1.27	2
13.07	12.97	5.75	1.31	1.29	1.26	2
11.18	11.09	4.93	1.30	1.28	1.26	2
9.30	9.21	4.11	1.29	1.27	1.25	2
7.43	7.35	3.29	1.28	1.26	1.24	2
5.56	5.50	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.82	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.27	799.33	351.48	447.86	422.69	25.16	6
57.78	834.29	353.47	480.82	453.04	27.79	6
57.30	869.23	355.47	513.75	483.35	30.40	6
56.81	904.13	357.49	546.64	513.63	33.01	6
56.32	939.01	359.52	579.49	543.89	35.60	6
55.84	973.85	361.55	612.30	574.12	38.18	6
55.36	1008.67	363.60	645.07	604.31	40.76	6
54.87	1043.46	365.66	677.80	634.48	43.32	6
54.39	1078.22	367.73	710.49	664.62	45.87	6
54.39	1078.22	367.73	710.49	664.62	45.87	5
53.31	1171.36	391.59	779.77	732.01	47.76	5
52.24	1263.65	414.86	848.79	798.55	50.24	5
51.19	1355.12	437.53	917.59	864.27	53.32	5
50.15	1445.79	459.58	986.21	929.19	57.02	5
49.12	1535.67	481.02	1054.66	993.32	61.34	5
48.11	1624.80	504.07	1120.73	1056.70	64.03	5
48.11	1624.80	504.07	1120.73	1056.70	64.03	4

46.15	1823.04	556.38	1266.66	1179.08	87.58	4
44.19	2020.65	608.69	1411.97	1300.83	111.13	4
42.25	2217.64	661.46	1556.18	1421.96	134.22	4
40.32	2413.99	715.23	1698.76	1542.45	156.31	4
38.40	2609.69	770.67	1839.02	1662.29	176.73	4
36.49	2804.71	828.71	1976.01	1781.46	194.55	4
34.59	2999.03	890.63	2108.40	1899.91	208.49	4
32.71	3192.56	958.45	2234.12	2017.59	216.53	4
30.84	3385.25	1032.32	2352.93	2134.42	218.51	4
30.84	3385.25	1032.32	2352.93	2134.42	218.51	3
29.46	3532.87	1092.23	2440.64	2220.18	220.46	3
28.09	3680.15	1151.31	2528.84	2305.60	223.24	3
26.73	3827.11	1209.73	2617.38	2390.70	226.68	3
25.37	3973.73	1267.65	2706.08	2475.46	230.62	3
24.02	4120.03	1325.23	2794.80	2559.91	234.89	3
22.67	4266.01	1382.58	2883.44	2644.03	239.41	3
21.33	4411.67	1439.82	2971.84	2727.82	244.02	3
19.99	4557.00	1497.04	3059.96	2811.30	248.66	3
18.66	4702.02	1554.32	3147.69	2894.45	253.24	3
18.66	4702.02	1554.32	3147.69	2894.45	253.24	2
16.75	4906.95	1631.22	3275.74	3013.30	262.44	2
14.85	5111.41	1711.98	3399.43	3131.65	267.78	2
12.97	5315.35	1796.82	3518.54	3249.50	269.04	2
11.09	5518.76	1885.99	3632.77	3366.81	265.96	2
9.21	5721.61	1979.91	3741.71	3483.56	258.14	2
7.35	5923.87	2114.73	3809.14	3599.72	209.42	2
5.50	6125.54	2258.43	3867.11	3715.29	151.82	2
3.66	6326.62	2398.96	3927.67	3830.28	97.39	2
1.82	6527.14	2535.98	3991.16	3944.70	46.47	2
.00	6727.10	2668.54	4058.56	4058.56	.00	2

Time = 4320. Degree of Consolidation = 73.%

Total Settlement = 2.317

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 4320. = 2.317

Settlement caused by Secondary Compression at time 4320. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
7.03	6.77	3.55
5.27	5.06	2.66
3.52	3.36	1.78
1.76	1.68	.89
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
6.77	.00	.00
5.06	201.40	94.16

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
107.24	107.24	.00	1

3.36	401.12	188.32	212.80	212.80	.00	1
1.68	600.38	282.48	317.90	317.90	.00	1
.00	799.33	350.00	449.33	422.69	26.64	1

Time = 4320. Degree of Consolidation = 100.%

Total Settlement = .256

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 4320. = .256

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.06

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.21	21.42	6.50	5.44	5.36	6
60.02	57.72	21.35	6.49	5.43	5.35	6
59.45	57.24	21.27	6.47	5.42	5.33	6
58.89	56.75	21.20	6.46	5.42	5.32	6
58.33	56.27	21.12	6.44	5.41	5.31	6
57.76	55.78	21.05	6.43	5.41	5.29	6
57.20	55.30	20.97	6.42	5.40	5.28	6
56.64	54.82	20.90	6.40	5.39	5.26	6
56.08	54.33	20.82	6.39	5.39	5.25	6
56.08	54.33	20.82	4.51	3.69	3.57	5
54.82	53.25	20.59	4.44	3.63	3.51	5
53.56	52.19	20.36	4.38	3.57	3.45	5
52.32	51.13	20.12	4.32	3.51	3.38	5
51.10	50.09	19.89	4.25	3.46	3.34	5
49.88	49.07	19.66	4.19	3.41	3.31	5
48.69	48.05	19.43	4.13	3.35	3.28	5
48.69	48.05	19.43	1.93	1.88	1.86	4
46.69	46.09	18.75	1.92	1.86	1.84	4
44.70	44.14	18.06	1.91	1.85	1.82	4
42.72	42.20	17.38	1.89	1.83	1.80	4
40.75	40.27	16.70	1.88	1.82	1.78	4
38.79	38.35	16.01	1.86	1.80	1.75	4
36.85	36.45	15.33	1.84	1.78	1.73	4
34.91	34.55	14.65	1.82	1.77	1.71	4
33.00	32.67	13.97	1.80	1.75	1.69	4
31.09	30.80	13.28	1.78	1.72	1.67	4
31.09	30.80	13.28	1.47	1.44	1.41	3
29.70	29.43	12.72	1.46	1.43	1.40	3
28.32	28.06	12.16	1.45	1.42	1.39	3
26.94	26.70	11.59	1.44	1.41	1.38	3
25.57	25.35	11.03	1.43	1.40	1.37	3
24.21	23.99	10.47	1.42	1.39	1.36	3
22.84	22.65	9.90	1.41	1.38	1.35	3
21.49	21.31	9.34	1.40	1.38	1.34	3
20.14	19.97	8.78	1.39	1.37	1.33	3

18.80	18.64	8.21	1.38	1.36	1.32	3
18.80	18.64	8.21	1.34	1.32	1.29	2
16.88	16.74	7.39	1.33	1.31	1.28	2
14.97	14.85	6.57	1.32	1.30	1.27	2
13.07	12.96	5.75	1.31	1.29	1.26	2
11.18	11.08	4.93	1.30	1.28	1.26	2
9.30	9.21	4.11	1.29	1.27	1.25	2
7.43	7.35	3.29	1.28	1.26	1.24	2
5.56	5.50	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.82	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.21	799.33	352.12	447.22	422.69	24.52	6
57.72	834.28	354.18	480.11	453.03	27.08	6
57.24	869.21	356.24	512.97	483.33	29.64	6
56.75	904.10	358.29	545.81	513.60	32.21	6
56.27	938.96	360.34	578.62	543.85	34.78	6
55.78	973.80	362.39	611.41	574.06	37.35	6
55.30	1008.61	364.43	644.17	604.25	39.93	6
54.82	1043.38	366.47	676.91	634.40	42.51	6
54.33	1078.13	368.51	709.62	664.53	45.09	6
54.33	1078.13	368.51	709.62	664.53	45.09	5
53.25	1171.24	392.34	778.90	731.89	47.01	5
52.19	1263.51	415.56	847.95	798.41	49.54	5
51.13	1354.95	438.16	916.80	864.10	52.69	5
50.09	1445.60	460.12	985.48	929.00	56.48	5
49.07	1535.47	481.45	1054.02	993.12	60.90	5
48.05	1624.58	504.80	1119.78	1056.48	63.30	5
48.05	1624.58	504.80	1119.78	1056.48	63.30	4
46.09	1822.80	559.63	1263.17	1178.84	84.33	4
44.14	2020.36	614.52	1405.83	1300.54	105.30	4
42.20	2217.26	669.90	1547.36	1421.58	125.78	4
40.27	2413.49	726.27	1687.22	1541.95	145.27	4
38.35	2609.04	784.31	1824.73	1661.65	163.08	4
36.45	2803.89	844.99	1958.90	1780.63	178.27	4
34.55	2997.99	909.62	2088.37	1898.88	189.49	4
32.67	3191.28	980.44	2210.84	2016.31	194.53	4
30.80	3383.69	1055.40	2328.30	2132.86	195.43	4
30.80	3383.69	1055.40	2328.30	2132.86	195.43	3
29.43	3531.18	1116.38	2414.80	2218.49	196.31	3
28.06	3678.33	1176.21	2502.11	2303.78	198.34	3
26.70	3825.14	1235.09	2590.05	2388.73	201.32	3
25.35	3971.62	1293.18	2678.44	2473.35	205.08	3
23.99	4117.78	1350.73	2767.05	2557.65	209.40	3
22.65	4263.61	1407.86	2855.75	2641.63	214.12	3
21.31	4409.13	1464.73	2944.40	2725.29	219.11	3
19.97	4554.32	1521.48	3032.85	2808.62	224.23	3
18.64	4699.20	1578.13	3121.07	2891.64	229.43	3
18.64	4699.20	1578.14	3121.07	2891.64	229.42	2
16.74	4904.00	1653.75	3250.25	3010.34	239.91	2
14.85	5108.32	1732.93	3375.39	3128.56	246.82	2
12.96	5312.14	1815.80	3496.34	3246.29	250.06	2
11.08	5515.44	1903.00	3612.44	3363.49	248.95	2
9.21	5718.19	1994.91	3723.28	3480.14	243.14	2
7.35	5920.37	2133.54	3786.82	3596.22	190.60	2
5.50	6121.96	2272.42	3849.55	3711.72	137.83	2
3.66	6323.00	2408.36	3914.64	3826.66	87.98	2
1.82	6523.49	2540.58	3982.91	3941.04	41.86	2

.00	6723.44	2668.54	4054.90	4054.90	.00	2

Time = 5040. Degree of Consolidation = 75.%

Total Settlement = 2.376

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 5040. = 2.376

Settlement caused by Secondary Compression at time 5040. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	6.77	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1
3.52	3.36	1.78	.98	.90	.90	1
1.76	1.68	.89	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
6.77	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.36	401.12	188.32	212.80	212.80	.00	1
1.68	600.38	282.48	317.90	317.90	.00	1
.00	799.33	350.00	449.33	422.69	26.64	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .256

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 5040. = .256

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.00

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.18	21.42	6.50	5.44	5.36	6

60.02	57.69	21.35	6.49	5.43	5.35	6
59.45	57.21	21.27	6.47	5.42	5.33	6
58.89	56.72	21.20	6.46	5.42	5.32	6
58.33	56.24	21.12	6.44	5.41	5.31	6
57.76	55.75	21.05	6.43	5.41	5.29	6
57.20	55.27	20.97	6.42	5.40	5.28	6
56.64	54.79	20.90	6.40	5.39	5.26	6
56.08	54.30	20.82	6.39	5.39	5.25	6
56.08	54.30	20.82	4.51	3.69	3.57	5
54.82	53.22	20.59	4.44	3.63	3.51	5
53.56	52.16	20.36	4.38	3.57	3.45	5
52.32	51.11	20.12	4.32	3.51	3.38	5
51.10	50.07	19.89	4.25	3.46	3.34	5
49.88	49.04	19.66	4.19	3.41	3.31	5
48.69	48.02	19.43	4.13	3.35	3.28	5
48.69	48.02	19.43	1.93	1.88	1.86	4
46.69	46.06	18.75	1.92	1.86	1.84	4
44.70	44.11	18.06	1.91	1.85	1.82	4
42.72	42.17	17.38	1.89	1.83	1.80	4
40.75	40.24	16.70	1.88	1.82	1.78	4
38.79	38.33	16.01	1.86	1.80	1.75	4
36.85	36.42	15.33	1.84	1.78	1.73	4
34.91	34.53	14.65	1.82	1.76	1.71	4
33.00	32.65	13.97	1.80	1.74	1.69	4
31.09	30.78	13.28	1.78	1.72	1.67	4
31.09	30.78	13.28	1.47	1.44	1.41	3
29.70	29.41	12.72	1.46	1.43	1.40	3
28.32	28.05	12.16	1.45	1.42	1.39	3
26.94	26.69	11.59	1.44	1.41	1.38	3
25.57	25.33	11.03	1.43	1.40	1.37	3
24.21	23.98	10.47	1.42	1.39	1.36	3
22.84	22.64	9.90	1.41	1.38	1.35	3
21.49	21.30	9.34	1.40	1.37	1.34	3
20.14	19.96	8.78	1.39	1.36	1.33	3
18.80	18.63	8.21	1.38	1.36	1.32	3
18.80	18.63	8.21	1.34	1.32	1.29	2
16.88	16.73	7.39	1.33	1.31	1.28	2
14.97	14.84	6.57	1.32	1.30	1.27	2
13.07	12.95	5.75	1.31	1.29	1.26	2
11.18	11.08	4.93	1.30	1.28	1.26	2
9.30	9.21	4.11	1.29	1.27	1.25	2
7.43	7.35	3.29	1.28	1.26	1.24	2
5.56	5.50	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.82	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.18	799.33	352.26	447.08	422.69	24.38	6
57.69	834.28	354.33	479.95	453.02	26.93	6
57.21	869.20	356.40	512.80	483.32	29.48	6
56.72	904.09	358.47	545.63	513.60	32.03	6
56.24	938.96	360.52	578.43	543.84	34.60	6
55.75	973.79	362.57	611.22	574.05	37.17	6
55.27	1008.59	364.62	643.98	604.23	39.74	6
54.79	1043.37	366.65	676.71	634.39	42.33	6
54.30	1078.11	368.68	709.43	664.51	44.92	6
54.30	1078.11	368.68	709.43	664.51	44.92	5
53.22	1171.22	392.51	778.71	731.87	46.84	5
52.16	1263.48	415.72	847.76	798.38	49.38	5

51.11	1354.92	438.30	916.62	864.07	52.55	5
50.07	1445.56	460.26	985.30	928.96	56.34	5
49.04	1535.42	481.57	1053.85	993.07	60.78	5
48.02	1624.53	505.05	1119.48	1056.43	63.05	5
48.02	1624.53	505.05	1119.48	1056.43	63.05	4
46.06	1822.74	561.04	1261.69	1178.78	82.92	4
44.11	2020.27	617.14	1403.13	1300.45	102.67	4
42.17	2217.13	673.76	1543.37	1421.46	121.91	4
40.24	2413.31	731.41	1681.91	1541.78	140.13	4
38.33	2608.80	790.74	1818.06	1661.40	156.65	4
36.42	2803.56	852.76	1950.80	1780.30	170.49	4
34.53	2997.56	918.88	2078.68	1898.44	180.24	4
32.65	3190.73	991.42	2199.31	2015.76	183.55	4
30.78	3383.00	1067.11	2315.89	2132.17	183.72	4
30.78	3383.00	1067.11	2315.89	2132.17	183.72	3
29.41	3530.42	1128.80	2401.62	2217.73	183.89	3
28.05	3677.49	1189.17	2488.32	2302.94	185.38	3
26.69	3824.23	1248.45	2575.78	2387.82	187.96	3
25.33	3970.64	1306.84	2663.80	2472.37	191.43	3
23.98	4116.72	1364.49	2752.23	2556.59	195.64	3
22.64	4262.48	1421.64	2840.84	2640.49	200.35	3
21.30	4407.92	1478.43	2929.48	2724.07	205.41	3
19.96	4553.04	1535.01	3018.02	2807.33	210.69	3
18.63	4697.84	1591.43	3106.40	2890.28	216.13	3
18.63	4697.84	1591.44	3106.40	2890.28	216.13	2
16.73	4902.55	1666.46	3236.10	3008.89	227.20	2
14.84	5106.80	1744.91	3361.89	3127.04	234.84	2
12.95	5310.55	1827.08	3483.47	3244.69	238.78	2
11.08	5513.78	1913.15	3600.63	3361.83	238.80	2
9.21	5716.47	2005.66	3710.81	3478.42	232.39	2
7.35	5918.60	2144.27	3774.32	3594.45	179.88	2
5.50	6120.16	2280.40	3839.76	3709.91	129.85	2
3.66	6321.17	2413.73	3907.44	3824.82	82.62	2
1.82	6521.64	2543.21	3978.43	3939.20	39.23	2
.00	6721.59	2668.54	4053.05	4053.04	.00	2

Time = 5475. Degree of Consolidation = 76.%

Total Settlement = 2.406

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 5475. = 2.406

Settlement caused by Secondary Compression at time 5475. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
7.03	6.77	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1
3.52	3.36	1.78	.98	.90	.90	1
1.76	1.68	.89	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

XI	Total Stresses	Effective Stresses	Total Pore Pressures	Static Pore Pressures	Excess Pore Pressures	Material
6.77	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.36	401.12	188.32	212.80	212.80	.00	1
1.68	600.38	282.48	317.90	317.90	.00	1
.00	799.33	350.00	449.33	422.69	26.64	1

Time = 5475. Degree of Consolidation = 100.%

Total Settlement = .256

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 5475. = .256

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.97

**********Current Conditions in Compressible Foundation**********

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.12	21.42	6.50	5.44	5.36	6
60.02	57.63	21.35	6.49	5.43	5.35	6
59.45	57.15	21.27	6.47	5.42	5.33	6
58.89	56.66	21.20	6.46	5.42	5.32	6
58.33	56.18	21.12	6.44	5.41	5.31	6
57.76	55.69	21.05	6.43	5.40	5.29	6
57.20	55.21	20.97	6.42	5.40	5.28	6
56.64	54.73	20.90	6.40	5.39	5.26	6
56.08	54.25	20.82	6.39	5.39	5.25	6
56.08	54.25	20.82	4.51	3.69	3.57	5
54.82	53.17	20.59	4.44	3.63	3.51	5
53.56	52.10	20.36	4.38	3.57	3.45	5
52.32	51.05	20.12	4.32	3.51	3.38	5
51.10	50.01	19.89	4.25	3.46	3.34	5
49.88	48.98	19.66	4.19	3.41	3.31	5
48.69	47.97	19.43	4.13	3.35	3.28	5
48.69	47.97	19.43	1.93	1.88	1.86	4
46.69	46.00	18.75	1.92	1.86	1.84	4
44.70	44.06	18.06	1.91	1.85	1.82	4
42.72	42.12	17.38	1.89	1.83	1.80	4
40.75	40.19	16.70	1.88	1.81	1.78	4
38.79	38.28	16.01	1.86	1.80	1.75	4
36.85	36.37	15.33	1.84	1.78	1.73	4
34.91	34.48	14.65	1.82	1.76	1.71	4
33.00	32.61	13.97	1.80	1.74	1.69	4
31.09	30.74	13.28	1.78	1.71	1.67	4
31.09	30.74	13.28	1.47	1.44	1.41	3
29.70	29.38	12.72	1.46	1.43	1.40	3
28.32	28.01	12.16	1.45	1.42	1.39	3
26.94	26.65	11.59	1.44	1.41	1.38	3

25.57	25.30	11.03	1.43	1.40	1.37	3
24.21	23.95	10.47	1.42	1.39	1.36	3
22.84	22.61	9.90	1.41	1.38	1.35	3
21.49	21.28	9.34	1.40	1.37	1.34	3
20.14	19.94	8.78	1.39	1.36	1.33	3
18.80	18.62	8.21	1.38	1.35	1.32	3
18.80	18.62	8.21	1.34	1.32	1.29	2
16.88	16.72	7.39	1.33	1.31	1.28	2
14.97	14.83	6.57	1.32	1.30	1.27	2
13.07	12.95	5.75	1.31	1.29	1.26	2
11.18	11.07	4.93	1.30	1.28	1.26	2
9.30	9.20	4.11	1.29	1.27	1.25	2
7.43	7.35	3.29	1.28	1.26	1.24	2
5.56	5.50	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.82	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.12	799.33	352.40	446.94	422.69	24.24	6
57.63	834.28	354.49	479.79	453.02	26.77	6
57.15	869.20	356.57	512.62	483.32	29.30	6
56.66	904.09	358.65	545.43	513.59	31.85	6
56.18	938.95	360.72	578.22	543.83	34.40	6
55.69	973.78	362.79	610.99	574.04	36.95	6
55.21	1008.58	364.85	643.73	604.22	39.51	6
54.73	1043.35	366.90	676.45	634.37	42.08	6
54.25	1078.09	368.94	709.15	664.49	44.66	6
54.25	1078.09	368.94	709.15	664.49	44.66	5
53.17	1171.18	392.77	778.42	731.83	46.58	5
52.10	1263.44	415.97	847.46	798.34	49.13	5
51.05	1354.87	438.55	916.32	864.02	52.30	5
50.01	1445.50	460.49	985.01	928.90	56.11	5
48.98	1535.36	481.80	1053.56	993.01	60.55	5
47.97	1624.46	505.51	1118.94	1056.36	62.59	5
47.97	1624.46	505.51	1118.94	1056.36	62.59	4
46.00	1822.64	563.53	1259.12	1178.68	80.43	4
44.06	2020.14	621.74	1398.39	1300.32	98.08	4
42.12	2216.93	680.60	1536.33	1421.25	115.08	4
40.19	2413.02	740.59	1672.43	1541.48	130.95	4
38.28	2608.38	802.45	1805.93	1660.98	144.95	4
36.37	2802.98	867.22	1935.76	1779.72	156.03	4
34.48	2996.79	936.51	2060.28	1897.67	162.60	4
32.61	3189.73	1011.89	2177.84	2014.76	163.08	4
30.74	3381.74	1089.29	2292.45	2130.91	161.54	4
30.74	3381.74	1089.29	2292.45	2130.91	161.54	3
29.38	3529.03	1152.63	2376.40	2216.34	160.06	3
28.01	3675.96	1214.33	2461.63	2301.41	160.22	3
26.65	3822.56	1274.69	2547.87	2386.15	161.72	3
25.30	3968.81	1333.86	2634.96	2470.55	164.41	3
23.95	4114.74	1392.11	2722.63	2554.62	168.02	3
22.61	4260.34	1449.59	2810.75	2638.36	172.39	3
21.28	4405.62	1506.46	2899.17	2721.78	177.39	3
19.94	4550.58	1562.89	2987.70	2804.88	182.81	3
18.62	4695.23	1619.01	3076.22	2887.67	188.55	3
18.62	4695.23	1619.02	3076.21	2887.67	188.54	2
16.72	4899.78	1693.39	3206.39	3006.12	200.27	2
14.83	5103.86	1770.65	3333.21	3124.10	209.11	2
12.95	5307.46	1851.26	3456.20	3241.60	214.59	2
11.07	5510.55	1935.38	3575.17	3358.60	216.57	2

9.20	5713.11	2034.53	3678.58	3475.06	203.52	2
7.35	5915.13	2167.28	3747.85	3590.98	156.87	2
5.50	6116.61	2297.80	3818.81	3706.36	112.45	2
3.66	6317.56	2425.07	3892.49	3821.21	71.28	2
1.82	6517.99	2548.76	3969.23	3935.55	33.68	2
.00	6717.93	2668.54	4049.39	4049.39	.00	2

Time = 6480. Degree of Consolidation = 78.%

Total Settlement = 2.464

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 6480. = 2.464

Settlement caused by Secondary Compression at time 6480. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
7.03	6.77	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1
3.52	3.36	1.78	.98	.90	.90	1
1.76	1.68	.89	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
6.77	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.36	401.12	188.32	212.80	212.80	.00	1
1.68	600.38	282.48	317.90	317.90	.00	1
.00	799.33	350.00	449.33	422.69	26.64	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .256

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 6480. = .256

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.91

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
60.58	58.08	21.42
60.02	57.59	21.35
59.45	57.11	21.27
58.89	56.62	21.20
58.33	56.14	21.12
57.76	55.66	21.05
57.20	55.17	20.97
56.64	54.69	20.90
56.08	54.21	20.82
56.08	54.21	20.82
54.82	53.13	20.59
53.56	52.06	20.36
52.32	51.01	20.12
51.10	49.97	19.89
49.88	48.94	19.66
48.69	47.93	19.43
48.69	47.93	19.43
46.69	45.97	18.75
44.70	44.02	18.06
42.72	42.08	17.38
40.75	40.15	16.70
38.79	38.24	16.01
36.85	36.34	15.33
34.91	34.45	14.65
33.00	32.58	13.97
31.09	30.72	13.28
31.09	30.72	13.28
29.70	29.35	12.72
28.32	27.99	12.16
26.94	26.63	11.59
25.57	25.28	11.03
24.21	23.94	10.47
22.84	22.60	9.90
21.49	21.26	9.34
20.14	19.93	8.78
18.80	18.61	8.21
18.80	18.61	8.21
16.88	16.71	7.39
14.97	14.82	6.57
13.07	12.94	5.75
11.18	11.07	4.93
9.30	9.20	4.11
7.43	7.34	3.29
5.56	5.50	2.46
3.70	3.66	1.64
1.85	1.82	.82
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
6.50	5.44	5.36	6
6.49	5.43	5.35	6
6.47	5.42	5.33	6
6.46	5.42	5.32	6
6.44	5.41	5.31	6
6.43	5.40	5.29	6
6.42	5.40	5.28	6
6.40	5.39	5.26	6
6.39	5.39	5.25	6
4.51	3.68	3.57	5
4.44	3.63	3.51	5
4.38	3.57	3.45	5
4.32	3.51	3.38	5
4.25	3.46	3.34	5
4.19	3.40	3.31	5
4.13	3.35	3.28	5
1.93	1.88	1.86	4
1.92	1.86	1.84	4
1.91	1.85	1.82	4
1.89	1.83	1.80	4
1.88	1.81	1.78	4
1.86	1.79	1.75	4
1.84	1.77	1.73	4
1.82	1.75	1.71	4
1.80	1.73	1.69	4
1.78	1.71	1.67	4
1.47	1.43	1.41	3
1.46	1.42	1.40	3
1.45	1.41	1.39	3
1.44	1.40	1.38	3
1.43	1.39	1.37	3
1.42	1.38	1.36	3
1.41	1.38	1.35	3
1.40	1.37	1.34	3
1.39	1.36	1.33	3
1.38	1.35	1.32	3
1.34	1.31	1.29	2
1.33	1.30	1.28	2
1.32	1.30	1.27	2
1.31	1.29	1.26	2
1.30	1.28	1.26	2
1.29	1.27	1.25	2
1.28	1.26	1.24	2
1.27	1.25	1.24	2
1.26	1.24	1.23	2
1.25	1.23	1.22	2
1.25	1.22	1.22	2

***** Stresses *****

XI	Total	Effective
58.08	799.33	352.40
57.59	834.28	354.49
57.11	869.20	356.58
56.62	904.09	358.66
56.14	938.95	360.74
55.66	973.77	362.81
55.17	1008.57	364.87

***** Pore Pressures *****

Total	Static	Excess	Material
446.93	422.69	24.24	6
479.79	453.02	26.76	6
512.62	483.32	29.30	6
545.42	513.59	31.83	6
578.21	543.83	34.38	6
610.97	574.04	36.93	6
643.71	604.21	39.49	6

54.69	1043.34	366.92	676.42	634.36	42.06	6
54.21	1078.09	368.97	709.12	664.49	44.63	6
54.21	1078.09	368.97	709.12	664.49	44.63	5
53.13	1171.18	392.81	778.37	731.83	46.54	5
52.06	1263.43	416.03	847.41	798.33	49.07	5
51.01	1354.86	438.62	916.24	864.01	52.23	5
49.97	1445.49	460.57	984.92	928.89	56.03	5
48.94	1535.34	481.89	1053.46	992.99	60.46	5
47.93	1624.44	505.74	1118.70	1056.34	62.36	5
47.93	1624.44	505.74	1118.70	1056.34	62.36	4
45.97	1822.62	565.05	1257.57	1178.66	78.91	4
44.02	2020.08	624.66	1395.42	1300.26	95.15	4
42.08	2216.83	684.99	1531.85	1421.16	110.69	4
40.15	2412.86	746.57	1666.29	1541.32	124.96	4
38.24	2608.14	810.19	1797.94	1660.74	137.20	4
36.34	2802.64	876.98	1925.65	1779.38	146.27	4
34.45	2996.31	948.65	2047.66	1897.20	150.46	4
32.58	3189.10	1025.67	2163.42	2014.12	149.30	4
30.72	3380.93	1104.16	2276.77	2130.10	146.67	4
30.72	3380.93	1104.16	2276.77	2130.10	146.67	3
29.35	3528.13	1168.56	2359.57	2215.44	144.13	3
27.99	3674.97	1231.23	2443.74	2300.42	143.32	3
26.63	3821.47	1292.34	2529.13	2385.06	144.07	3
25.28	3967.63	1352.16	2615.47	2469.36	146.11	3
23.94	4113.45	1410.87	2702.58	2553.32	149.26	3
22.60	4258.94	1468.61	2790.33	2636.96	153.37	3
21.26	4404.12	1525.62	2878.49	2720.27	158.22	3
19.93	4548.97	1582.07	2966.90	2803.27	163.63	3
18.61	4693.51	1638.08	3055.43	2885.95	169.48	3
18.61	4693.51	1638.08	3055.43	2885.95	169.48	2
16.71	4897.94	1712.24	3185.70	3004.28	181.41	2
14.82	5101.91	1788.95	3312.96	3122.15	190.81	2
12.94	5305.40	1868.64	3436.76	3239.54	197.22	2
11.07	5508.38	1951.71	3556.67	3356.43	200.24	2
9.20	5710.85	2056.15	3654.70	3472.80	181.91	2
7.34	5912.79	2184.67	3728.12	3588.64	139.48	2
5.50	6114.21	2310.53	3803.67	3703.96	99.72	2
3.66	6315.11	2433.37	3881.74	3818.77	62.98	2
1.82	6515.52	2552.83	3962.70	3933.08	29.62	2
.00	6715.45	2668.54	4046.91	4046.91	.00	2

Time = 7300. Degree of Consolidation = 79.%

Total Settlement = 2.504

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 7300. = 2.504

Settlement caused by Secondary Compression at time 7300. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
7.03	6.77	3.55	.98	.98	.98	1
5.27	5.06	2.66	.98	.91	.91	1

3.52	3.36	1.78	.98	.90	1
1.76	1.68	.89	.98	.89	1
.00	.00	.00	.98	.89	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
6.77	.00	.00	.00	.00	.00	1
5.06	201.40	94.16	107.24	107.24	.00	1
3.36	401.12	188.32	212.80	212.80	.00	1
1.68	600.38	282.48	317.90	317.90	.00	1
.00	799.33	350.00	449.33	422.69	26.64	1

Time = 7300. Degree of Consolidation = 100.%

Total Settlement = .256

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 7300. = .256

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.87

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.01	21.42	6.50	5.44	5.36	6
60.02	57.52	21.35	6.49	5.43	5.35	6
59.45	57.04	21.27	6.47	5.42	5.33	6
58.89	56.55	21.20	6.46	5.42	5.32	6
58.33	56.07	21.12	6.44	5.41	5.31	6
57.76	55.58	21.05	6.43	5.40	5.29	6
57.20	55.10	20.97	6.42	5.40	5.28	6
56.64	54.62	20.90	6.40	5.39	5.26	6
56.08	54.13	20.82	6.39	5.39	5.25	6
56.08	54.13	20.82	4.51	3.68	3.57	5
54.82	53.06	20.59	4.44	3.63	3.51	5
53.56	51.99	20.36	4.38	3.57	3.45	5
52.32	50.94	20.12	4.32	3.51	3.38	5
51.10	49.90	19.89	4.25	3.46	3.34	5
49.88	48.87	19.66	4.19	3.40	3.31	5
48.69	47.86	19.43	4.13	3.35	3.28	5
48.69	47.86	19.43	1.93	1.88	1.86	4
46.69	45.90	18.75	1.92	1.86	1.84	4
44.70	43.95	18.06	1.91	1.84	1.82	4
42.72	42.01	17.38	1.89	1.83	1.80	4
40.75	40.09	16.70	1.88	1.81	1.78	4
38.79	38.18	16.01	1.86	1.79	1.75	4
36.85	36.28	15.33	1.84	1.77	1.73	4
34.91	34.39	14.65	1.82	1.75	1.71	4
33.00	32.52	13.97	1.80	1.73	1.69	4

31.09	30.67	13.28	1.78	1.70	1.67	4
31.09	30.67	13.28	1.47	1.43	1.41	3
29.70	29.30	12.72	1.46	1.42	1.40	3
28.32	27.95	12.16	1.45	1.41	1.39	3
26.94	26.59	11.59	1.44	1.40	1.38	3
25.57	25.24	11.03	1.43	1.39	1.37	3
24.21	23.90	10.47	1.42	1.38	1.36	3
22.84	22.56	9.90	1.41	1.37	1.35	3
21.49	21.23	9.34	1.40	1.36	1.34	3
20.14	19.90	8.78	1.39	1.35	1.33	3
18.80	18.58	8.21	1.38	1.34	1.32	3
18.80	18.58	8.21	1.34	1.31	1.29	2
16.88	16.69	7.39	1.33	1.30	1.28	2
14.97	14.80	6.57	1.32	1.29	1.27	2
13.07	12.93	5.75	1.31	1.28	1.26	2
11.18	11.06	4.93	1.30	1.27	1.26	2
9.30	9.19	4.11	1.29	1.26	1.25	2
7.43	7.34	3.29	1.28	1.25	1.24	2
5.56	5.49	2.46	1.27	1.24	1.24	2
3.70	3.66	1.64	1.26	1.23	1.23	2
1.85	1.82	.82	1.25	1.23	1.22	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.01	799.33	352.52	446.82	422.69	24.12	6
57.52	834.28	354.62	479.66	453.02	26.64	6
57.04	869.19	356.72	512.47	483.32	29.16	6
56.55	904.08	358.81	545.27	513.58	31.69	6
56.07	938.94	360.90	578.04	543.82	34.22	6
55.58	973.76	362.97	610.79	574.03	36.77	6
55.10	1008.56	365.04	643.52	604.20	39.32	6
54.62	1043.33	367.11	676.22	634.35	41.87	6
54.13	1078.07	369.16	708.90	664.47	44.44	6
54.13	1078.07	369.16	708.90	664.47	44.44	5
53.06	1171.16	393.00	778.16	731.81	46.35	5
51.99	1263.40	416.22	847.18	798.30	48.88	5
50.94	1354.82	438.80	916.02	863.97	52.05	5
49.90	1445.44	460.76	984.69	928.84	55.84	5
48.87	1535.29	482.07	1053.22	992.94	60.28	5
47.86	1624.38	506.14	1118.24	1056.28	61.96	5
47.86	1624.38	506.14	1118.24	1056.28	61.96	4
45.90	1822.54	567.62	1254.93	1178.58	76.34	4
43.95	2019.96	629.58	1390.39	1300.14	90.24	4
42.01	2216.64	692.42	1524.22	1420.96	103.26	4
40.09	2412.56	756.75	1655.81	1541.02	114.79	4
38.18	2607.70	823.42	1784.28	1660.30	123.98	4
36.28	2802.02	893.77	1908.25	1778.77	129.48	4
34.39	2995.47	969.89	2025.58	1896.36	129.22	4
32.52	3187.98	1049.98	2138.00	2013.01	125.00	4
30.67	3379.49	1130.55	2248.95	2128.66	120.28	4
30.67	3379.49	1130.55	2248.95	2128.66	120.28	3
29.30	3526.54	1196.78	2329.76	2213.85	115.91	3
27.95	3673.22	1261.07	2412.15	2298.67	113.48	3
26.59	3819.55	1323.61	2495.94	2383.14	112.80	3
25.24	3965.52	1384.57	2580.95	2467.26	113.69	3
23.90	4111.16	1444.23	2666.93	2551.03	115.90	3
22.56	4256.47	1502.75	2753.72	2634.48	119.23	3
21.23	4401.44	1560.29	2841.15	2717.60	123.55	3
19.90	4546.10	1617.00	2929.10	2800.40	128.70	3
18.58	4690.44	1673.03	3017.42	2882.88	134.53	3

18.58	4690.44	1673.03	3017.42	2882.88	134.53	2
16.69	4894.66	1746.87	3147.79	3001.00	146.79	2
14.80	5098.42	1822.67	3275.74	3118.66	157.08	2
12.93	5301.70	1900.68	3401.02	3235.85	165.17	2
11.06	5504.50	1981.37	3523.13	3352.55	170.58	2
9.19	5706.80	2095.04	3611.76	3468.75	143.01	2
7.34	5908.59	2216.21	3692.38	3584.44	107.94	2
5.49	6109.89	2334.37	3775.52	3699.65	75.87	2
3.66	6310.72	2449.26	3861.46	3814.37	47.09	2
1.82	6511.08	2560.77	3950.31	3928.64	21.67	2
.00	6710.99	2668.54	4042.45	4042.45	.00	2

Time = 9125. Degree of Consolidation = 81.%

Total Settlement = 2.575

Settlement at End of Primary Consolidation = 3.168

Settlement caused by Primary Consolidation at time 9125. = 2.575

Settlement caused by Secondary Compression at time 9125. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
7.03	6.77	3.55
5.27	5.06	2.66
3.52	3.36	1.78
1.76	1.68	.89
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
6.77	.00	.00
5.06	201.40	94.16
3.36	401.12	188.32
1.68	600.38	282.48
.00	799.33	350.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
107.24	107.24	.00	1
212.80	212.80	.00	1
317.90	317.90	.00	1
449.33	422.69	26.64	1

Time = 9125. Degree of Consolidation = 100.%

Total Settlement = .256

Settlement at End of Primary Consolidation = .256

Settlement caused by Primary Consolidation at time 9125. = .256

Settlement caused by Secondary Compression at time 9125. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.80

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou Dupont - 5ft fill with Equivalent fill height of 9.2 f

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	9.2	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.585	.570	.30000E-03	z = .06

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	5.01	6
60.02	60.02	21.35	6.49	6.49	5.00	6
59.45	59.45	21.27	6.47	6.47	4.99	6
58.89	58.89	21.20	6.46	6.46	4.98	6

58.33	58.33	21.12	6.44	6.44	4.97	6
57.76	57.76	21.05	6.43	6.43	4.97	6
57.20	57.20	20.97	6.42	6.42	4.96	6
56.64	56.64	20.90	6.40	6.40	4.95	6
56.08	56.08	20.82	6.39	6.39	4.95	6
56.08	56.08	20.82	4.51	4.51	3.33	5
54.82	54.82	20.59	4.44	4.44	3.30	5
53.56	53.56	20.36	4.38	4.38	3.27	5
52.32	52.32	20.12	4.32	4.32	3.24	5
51.10	51.10	19.89	4.25	4.25	3.21	5
49.88	49.88	19.66	4.19	4.19	3.18	5
48.69	48.69	19.43	4.13	4.13	3.15	5
48.69	48.69	19.43	1.93	1.93	1.83	4
46.69	46.69	18.75	1.92	1.92	1.81	4
44.70	44.70	18.06	1.91	1.91	1.79	4
42.72	42.72	17.38	1.89	1.89	1.76	4
40.75	40.75	16.70	1.88	1.88	1.74	4
38.79	38.79	16.01	1.86	1.86	1.72	4
36.85	36.85	15.33	1.84	1.84	1.70	4
34.91	34.91	14.65	1.82	1.82	1.68	4
33.00	33.00	13.97	1.80	1.80	1.66	4
31.09	31.09	13.28	1.78	1.78	1.63	4
31.09	31.09	13.28	1.47	1.47	1.39	3
29.70	29.70	12.72	1.46	1.46	1.38	3
28.32	28.32	12.16	1.45	1.45	1.37	3
26.94	26.94	11.59	1.44	1.44	1.36	3
25.57	25.57	11.03	1.43	1.43	1.35	3
24.21	24.21	10.47	1.42	1.42	1.34	3
22.84	22.84	9.90	1.41	1.41	1.33	3
21.49	21.49	9.34	1.40	1.40	1.32	3
20.14	20.14	8.78	1.39	1.39	1.31	3
18.80	18.80	8.21	1.38	1.38	1.30	3
18.80	18.80	8.21	1.34	1.34	1.28	2
16.88	16.88	7.39	1.33	1.33	1.27	2
14.97	14.97	6.57	1.32	1.32	1.26	2
13.07	13.07	5.75	1.31	1.31	1.26	2
11.18	11.18	4.93	1.30	1.30	1.25	2
9.30	9.30	4.11	1.29	1.29	1.24	2
7.43	7.43	3.29	1.28	1.28	1.23	2
5.56	5.56	2.46	1.27	1.27	1.23	2
3.70	3.70	1.64	1.26	1.26	1.22	2
1.85	1.85	.82	1.25	1.25	1.21	2
.00	.00	.00	1.25	1.25	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	1065.82	.00	1065.82	573.46	492.36	6
60.02	1105.76	4.62	1101.14	608.78	492.36	6
59.45	1145.65	9.24	1136.41	644.04	492.36	6
58.89	1185.46	13.86	1171.60	679.24	492.36	6
58.33	1225.21	18.48	1206.73	714.37	492.36	6
57.76	1264.90	23.10	1241.79	749.43	492.36	6
57.20	1304.51	27.72	1276.79	784.43	492.36	6
56.64	1344.07	32.34	1311.72	819.36	492.36	6
56.08	1383.55	36.96	1346.59	854.23	492.36	6
56.08	1383.55	36.96	1346.59	854.23	492.36	5
54.82	1488.53	62.71	1425.81	933.45	492.36	5
53.56	1592.58	88.46	1504.11	1011.75	492.36	5
52.32	1695.70	114.21	1581.49	1089.13	492.36	5
51.10	1797.90	139.96	1657.94	1165.58	492.36	5
49.88	1899.18	165.71	1733.47	1241.11	492.36	5

48.69	1999.54	191.46	1808.07	1315.71	492.36	5
48.69	1999.54	191.46	1808.07	1315.71	492.36	4
46.69	2199.98	267.32	1932.66	1440.30	492.36	4
44.70	2399.92	343.18	2056.74	1564.38	492.36	4
42.72	2599.31	419.04	2180.27	1687.91	492.36	4
40.75	2798.26	494.90	2303.36	1811.00	492.36	4
38.79	2996.46	570.76	2425.70	1933.34	492.36	4
36.85	3193.76	646.62	2547.14	2054.78	492.36	4
34.91	3390.15	722.48	2667.68	2175.31	492.36	4
33.00	3585.64	798.34	2787.31	2294.95	492.36	4
31.09	3780.23	874.19	2906.03	2413.67	492.36	4
31.09	3780.23	874.19	2906.03	2413.67	492.36	3
29.70	3928.80	936.05	2992.74	2500.38	492.36	3
28.32	4076.97	997.91	3079.06	2586.70	492.36	3
26.94	4224.78	1059.77	3165.01	2672.64	492.36	3
25.57	4372.23	1121.63	3250.61	2758.24	492.36	3
24.21	4519.35	1183.49	3335.86	2843.50	492.36	3
22.84	4666.11	1245.35	3420.76	2928.40	492.36	3
21.49	4812.52	1307.21	3505.32	3012.96	492.36	3
20.14	4958.59	1369.06	3589.53	3097.17	492.36	3
18.80	5104.31	1430.92	3673.39	3181.03	492.36	3
18.80	5104.31	1430.92	3673.39	3181.03	492.36	2
16.88	5309.98	1517.02	3792.96	3300.60	492.36	2
14.97	5515.12	1603.12	3912.00	3419.64	492.36	2
13.07	5719.73	1689.22	4030.51	3538.15	492.36	2
11.18	5923.80	1775.31	4148.49	3656.13	492.36	2
9.30	6127.36	1861.41	4265.95	3773.58	492.36	2
7.43	6330.38	1947.51	4382.86	3890.50	492.36	2
5.56	6532.88	2033.61	4499.27	4006.91	492.36	2
3.70	6735.00	2119.71	4615.29	4122.93	492.36	2
1.85	6936.77	2205.80	4730.96	4238.60	492.36	2
.00	7138.18	2291.90	4846.28	4353.92	492.36	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	9.19	4.64	.98	.98	.98	1
6.89	6.89	3.48	.98	.98	.91	1
4.59	4.59	2.32	.98	.98	.90	1
2.30	2.30	1.16	.98	.98	.89	1
.00	.00	.00	.98	.98	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

9.19	.00	.00	.00	.00	.00	1
6.89	266.45	.00	266.45	143.36	123.09	1
4.59	532.91	.00	532.91	286.73	246.18	1
2.30	799.36	.00	799.36	430.09	369.27	1
.00	1065.82	.00	1065.82	573.46	492.36	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.46	21.42	6.50	5.84	5.01	6
60.02	59.94	21.35	6.49	6.04	5.00	6
59.45	59.40	21.27	6.47	6.20	4.99	6
58.89	58.85	21.20	6.46	6.31	4.98	6
58.33	58.29	21.12	6.44	6.37	4.97	6
57.76	57.74	21.05	6.43	6.40	4.97	6
57.20	57.18	20.97	6.42	6.40	4.96	6
56.64	56.62	20.90	6.40	6.40	4.95	6
56.08	56.06	20.82	6.39	6.38	4.95	6
56.08	56.06	20.82	4.51	4.51	3.33	5
54.82	54.79	20.59	4.44	4.44	3.30	5
53.56	53.54	20.36	4.38	4.38	3.27	5
52.32	52.30	20.12	4.32	4.31	3.24	5
51.10	51.07	19.89	4.25	4.25	3.21	5
49.88	49.86	19.66	4.19	4.19	3.18	5
48.69	48.67	19.43	4.13	4.12	3.15	5
48.69	48.67	19.43	1.93	1.93	1.83	4
46.69	46.67	18.75	1.92	1.92	1.81	4
44.70	44.68	18.06	1.91	1.91	1.79	4
42.72	42.70	17.38	1.89	1.89	1.76	4
40.75	40.73	16.70	1.88	1.88	1.74	4
38.79	38.77	16.01	1.86	1.86	1.72	4
36.85	36.83	15.33	1.84	1.84	1.70	4
34.91	34.90	14.65	1.82	1.82	1.68	4
33.00	32.98	13.97	1.80	1.80	1.66	4
31.09	31.08	13.28	1.78	1.78	1.63	4
31.09	31.08	13.28	1.47	1.47	1.39	3
29.70	29.69	12.72	1.46	1.46	1.38	3
28.32	28.30	12.16	1.45	1.45	1.37	3
26.94	26.93	11.59	1.44	1.44	1.36	3
25.57	25.55	11.03	1.43	1.43	1.35	3
24.21	24.19	10.47	1.42	1.42	1.34	3
22.84	22.83	9.90	1.41	1.41	1.33	3
21.49	21.47	9.34	1.40	1.40	1.32	3
20.14	20.12	8.78	1.39	1.39	1.31	3
18.80	18.78	8.21	1.38	1.38	1.30	3
18.80	18.78	8.21	1.34	1.34	1.28	2

16.88	16.86	7.39	1.33	1.33	1.27	2
14.97	14.95	6.57	1.32	1.32	1.26	2
13.07	13.06	5.75	1.31	1.31	1.26	2
11.18	11.16	4.93	1.30	1.30	1.25	2
9.30	9.28	4.11	1.29	1.29	1.24	2
7.43	7.41	3.29	1.28	1.28	1.23	2
5.56	5.54	2.46	1.27	1.27	1.23	2
3.70	3.68	1.64	1.26	1.26	1.22	2
1.85	1.83	.82	1.25	1.25	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.46	1044.72	220.13	824.58	552.35	272.23	6
59.94	1082.05	153.41	928.64	585.07	343.57	6
59.40	1120.24	100.19	1020.06	618.64	401.41	6
58.85	1159.08	63.61	1095.47	652.86	442.62	6
58.29	1198.32	42.78	1155.54	687.48	468.06	6
57.74	1237.76	33.76	1204.01	722.30	481.71	6
57.18	1277.28	32.03	1245.25	757.20	488.05	6
56.62	1316.79	34.17	1282.63	792.09	490.54	6
56.06	1356.26	38.16	1318.10	826.94	491.17	6
56.06	1356.26	38.16	1318.10	826.94	491.17	5
54.79	1461.20	63.61	1397.59	906.12	491.47	5
53.54	1565.22	89.34	1475.87	984.39	491.48	5
52.30	1668.31	115.13	1553.18	1061.74	491.45	5
51.07	1770.48	140.90	1629.58	1138.15	491.43	5
49.86	1871.72	166.62	1705.10	1213.65	491.45	5
48.67	1972.05	192.27	1779.78	1288.22	491.56	5
48.67	1972.05	192.27	1779.78	1288.22	491.56	4
46.67	2172.49	267.32	1905.17	1412.80	492.36	4
44.68	2372.41	343.18	2029.23	1536.87	492.36	4
42.70	2571.81	421.79	2150.02	1660.41	489.61	4
40.73	2770.65	507.85	2262.80	1783.39	479.41	4
38.77	2968.77	573.63	2395.13	1905.65	489.49	4
36.83	3166.06	646.64	2519.41	2027.08	492.34	4
34.90	3362.45	722.48	2639.98	2147.62	492.36	4
32.98	3557.94	798.34	2759.61	2267.25	492.36	4
31.08	3752.53	874.19	2878.33	2385.97	492.36	4
31.08	3752.53	874.19	2878.33	2385.97	492.36	3
29.69	3901.10	936.05	2965.04	2472.68	492.36	3
28.30	4049.27	997.91	3051.36	2559.00	492.36	3
26.93	4197.07	1061.00	3136.08	2644.94	491.14	3
25.55	4344.52	1123.20	3221.32	2730.53	490.79	3
24.19	4491.63	1185.05	3306.58	2815.78	490.80	3
22.83	4638.38	1246.82	3391.56	2900.67	490.89	3
21.47	4784.79	1308.58	3476.21	2985.22	490.99	3
20.12	4930.85	1370.28	3560.57	3069.42	491.14	3
18.78	5076.56	1431.78	3644.78	3153.28	491.50	3
18.78	5076.56	1431.78	3644.78	3153.28	491.50	2
16.86	5282.23	1517.22	3765.01	3272.84	492.16	2
14.95	5487.36	1603.20	3884.16	3391.88	492.28	2
13.06	5691.97	1689.25	4002.73	3510.39	492.33	2
11.16	5896.05	1775.31	4120.74	3628.38	492.36	2
9.28	6099.61	1861.41	4238.19	3745.83	492.36	2
7.41	6302.62	1947.51	4355.11	3862.75	492.36	2
5.54	6505.16	2033.61	4471.55	3979.19	492.36	2
3.68	6707.24	2126.38	4580.86	4095.17	485.69	2
1.83	6908.91	2279.93	4628.98	4210.74	418.24	2
.00	7109.33	2784.26	4325.07	4325.07	.00	2

Time = 30. Degree of Consolidation = 3.%

Total Settlement = .124

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 30. = .124

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
9.19	8.85	4.64	.98	.98	.98	1
6.89	6.61	3.48	.98	.91	.91	1
4.59	4.40	2.32	.98	.90	.90	1
2.30	2.20	1.16	.98	.90	.89	1
.00	.00	.00	.98	.90	.89	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
8.85	.00	.00	.00	.00	.00	1
6.61	263.17	123.09	140.08	140.08	.00	1
4.40	523.92	246.18	277.74	277.74	.00	1
2.20	784.27	265.86	518.42	415.00	103.41	1
.00	1044.72	220.13	824.58	552.35	272.23	1

Time = 30. Degree of Consolidation = 97.%

Total Settlement = .338

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 30. = .338

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 7.33

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.39	21.42	6.50	5.78	5.01	6
60.02	59.87	21.35	6.49	5.93	5.00	6
59.45	59.35	21.27	6.47	6.07	4.99	6
58.89	58.81	21.20	6.46	6.18	4.98	6
58.33	58.26	21.12	6.44	6.26	4.97	6

57.76	57.71	21.05	6.43	6.32	4.97	6
57.20	57.16	20.97	6.42	6.35	4.96	6
56.64	56.60	20.90	6.40	6.36	4.95	6
56.08	56.04	20.82	6.39	6.37	4.95	6
56.08	56.04	20.82	4.51	4.49	3.33	5
54.82	54.78	20.59	4.44	4.43	3.30	5
53.56	53.53	20.36	4.38	4.37	3.27	5
52.32	52.29	20.12	4.32	4.31	3.24	5
51.10	51.06	19.89	4.25	4.25	3.21	5
49.88	49.85	19.66	4.19	4.18	3.18	5
48.69	48.66	19.43	4.13	4.12	3.15	5
48.69	48.66	19.43	1.93	1.93	1.83	4
46.69	46.66	18.75	1.92	1.92	1.81	4
44.70	44.67	18.06	1.91	1.91	1.79	4
42.72	42.69	17.38	1.89	1.89	1.76	4
40.75	40.72	16.70	1.88	1.88	1.74	4
38.79	38.77	16.01	1.86	1.86	1.72	4
36.85	36.82	15.33	1.84	1.84	1.70	4
34.91	34.89	14.65	1.82	1.82	1.68	4
33.00	32.97	13.97	1.80	1.80	1.66	4
31.09	31.07	13.28	1.78	1.78	1.63	4
31.09	31.07	13.28	1.47	1.47	1.39	3
29.70	29.68	12.72	1.46	1.46	1.38	3
28.32	28.30	12.16	1.45	1.45	1.37	3
26.94	26.92	11.59	1.44	1.44	1.36	3
25.57	25.55	11.03	1.43	1.43	1.35	3
24.21	24.18	10.47	1.42	1.42	1.34	3
22.84	22.82	9.90	1.41	1.41	1.33	3
21.49	21.47	9.34	1.40	1.40	1.32	3
20.14	20.12	8.78	1.39	1.39	1.31	3
18.80	18.77	8.21	1.38	1.38	1.30	3
18.80	18.77	8.21	1.34	1.34	1.28	2
16.88	16.86	7.39	1.33	1.33	1.27	2
14.97	14.95	6.57	1.32	1.32	1.26	2
13.07	13.05	5.75	1.31	1.31	1.26	2
11.18	11.16	4.93	1.30	1.30	1.25	2
9.30	9.28	4.11	1.29	1.29	1.24	2
7.43	7.40	3.29	1.28	1.28	1.23	2
5.56	5.54	2.46	1.27	1.27	1.23	2
3.70	3.68	1.64	1.26	1.26	1.22	2
1.85	1.83	.82	1.25	1.24	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.39	1044.68	239.56	805.12	552.32	252.80	6
59.87	1081.62	188.66	892.96	584.64	308.32	6
59.35	1119.24	143.82	975.42	617.64	357.78	6
58.81	1157.45	107.07	1050.38	651.23	399.15	6
58.26	1196.11	79.51	1116.61	685.27	431.34	6
57.71	1235.10	60.90	1174.20	719.64	454.56	6
57.16	1274.30	49.99	1224.31	754.22	470.09	6
56.60	1313.61	45.00	1268.61	788.91	479.71	6
56.04	1352.96	44.06	1308.90	823.64	485.26	6
56.04	1352.96	44.06	1308.90	823.64	485.26	5
54.78	1457.74	66.70	1391.05	902.67	488.38	5
53.53	1561.68	91.08	1470.60	980.85	489.75	5
52.29	1664.72	116.29	1548.43	1058.15	490.28	5
51.06	1766.85	141.83	1625.02	1134.53	490.49	5
49.85	1868.07	167.45	1700.62	1209.99	490.63	5
48.66	1968.36	193.01	1775.35	1284.54	490.81	5

48.66	1968.36	193.01	1775.35	1284.54	490.81	4
46.66	2168.80	267.32	1901.48	1409.11	492.36	4
44.67	2368.72	343.58	2025.14	1533.18	491.96	4
42.69	2568.11	426.46	2141.65	1656.71	484.94	4
40.72	2766.89	512.87	2254.03	1779.63	474.39	4
38.77	2964.96	577.08	2387.88	1901.84	486.04	4
36.82	3162.23	647.57	2514.66	2023.25	491.41	4
34.89	3358.62	722.48	2636.14	2143.78	492.36	4
32.97	3554.11	798.34	2755.77	2263.41	492.36	4
31.07	3748.69	874.19	2874.50	2382.14	492.36	4
31.07	3748.69	874.20	2874.50	2382.14	492.36	3
29.68	3897.26	936.05	2961.21	2468.85	492.36	3
28.30	4045.44	997.91	3047.52	2555.16	492.36	3
26.92	4193.24	1061.85	3131.39	2641.10	490.28	3
25.55	4340.68	1124.52	3216.16	2726.69	489.47	3
24.18	4487.77	1186.50	3301.28	2811.92	489.35	3
22.82	4634.52	1248.24	3386.28	2896.81	489.47	3
21.47	4780.92	1309.88	3471.04	2981.35	489.68	3
20.12	4926.97	1371.40	3555.57	3065.55	490.03	3
18.77	5072.68	1432.63	3640.05	3149.40	490.66	3
18.77	5072.68	1432.63	3640.06	3149.40	490.66	2
16.86	5278.34	1517.52	3760.82	3268.96	491.86	2
14.95	5483.48	1603.30	3880.18	3388.00	492.18	2
13.05	5688.09	1689.30	3998.79	3506.51	492.28	2
11.16	5892.17	1775.31	4116.85	3624.49	492.36	2
9.28	6095.72	1861.41	4234.31	3741.95	492.36	2
7.40	6298.74	1947.51	4351.23	3858.86	492.36	2
5.54	6501.26	2033.61	4467.65	3975.29	492.36	2
3.68	6703.33	2140.85	4562.48	4091.27	471.22	2
1.83	6904.85	2335.02	4569.83	4206.68	363.15	2
.00	7105.10	2784.26	4320.84	4320.84	.00	2

Time = 60. Degree of Consolidation = 5.%

Total Settlement = .191

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 60. = .191

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
9.19	8.85	4.64
6.89	6.61	3.48
4.59	4.40	2.32
2.30	2.20	1.16
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.89	1
.98	.90	.89	1

***** Stresses *****

XI	Total	Effective
8.85	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

6.61	263.17	123.09	140.08	140.08	.00	1
4.40	523.92	246.18	277.74	277.74	.00	1
2.20	784.28	265.86	518.42	415.01	103.41	1
.00	1044.68	239.56	805.12	552.32	252.80	1

Time = 60. Degree of Consolidation = 97.%

Total Settlement = .339

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 60. = .339

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 7.26

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.28	21.42	6.50	5.72	5.01	6
60.02	59.77	21.35	6.49	5.83	5.00	6
59.45	59.25	21.27	6.47	5.94	4.99	6
58.89	58.72	21.20	6.46	6.03	4.98	6
58.33	58.19	21.12	6.44	6.12	4.97	6
57.76	57.65	21.05	6.43	6.18	4.97	6
57.20	57.10	20.97	6.42	6.24	4.96	6
56.64	56.56	20.90	6.40	6.28	4.95	6
56.08	56.00	20.82	6.39	6.31	4.95	6
56.08	56.00	20.82	4.51	4.44	3.33	5
54.82	54.75	20.59	4.44	4.40	3.30	5
53.56	53.50	20.36	4.38	4.35	3.27	5
52.32	52.27	20.12	4.32	4.30	3.24	5
51.10	51.04	19.89	4.25	4.24	3.21	5
49.88	49.84	19.66	4.19	4.18	3.18	5
48.69	48.64	19.43	4.13	4.11	3.15	5
48.69	48.64	19.43	1.93	1.93	1.83	4
46.69	46.65	18.75	1.92	1.92	1.81	4
44.70	44.66	18.06	1.91	1.90	1.79	4
42.72	42.68	17.38	1.89	1.89	1.76	4
40.75	40.71	16.70	1.88	1.87	1.74	4
38.79	38.76	16.01	1.86	1.86	1.72	4
36.85	36.81	15.33	1.84	1.84	1.70	4
34.91	34.88	14.65	1.82	1.82	1.68	4
33.00	32.96	13.97	1.80	1.80	1.66	4
31.09	31.06	13.28	1.78	1.78	1.63	4
31.09	31.06	13.28	1.47	1.47	1.39	3
29.70	29.67	12.72	1.46	1.46	1.38	3
28.32	28.29	12.16	1.45	1.45	1.37	3
26.94	26.91	11.59	1.44	1.44	1.36	3
25.57	25.54	11.03	1.43	1.43	1.35	3
24.21	24.17	10.47	1.42	1.42	1.34	3
22.84	22.81	9.90	1.41	1.41	1.33	3
21.49	21.46	9.34	1.40	1.40	1.32	3
20.14	20.11	8.78	1.39	1.39	1.31	3
18.80	18.76	8.21	1.38	1.38	1.30	3

18.80	18.76	8.21	1.34	1.28		2
16.88	16.85	7.39	1.33	1.27		2
14.97	14.94	6.57	1.32	1.26		2
13.07	13.04	5.75	1.31	1.26		2
11.18	11.15	4.93	1.30	1.25		2
9.30	9.27	4.11	1.29	1.24		2
7.43	7.40	3.29	1.28	1.23		2
5.56	5.53	2.46	1.27	1.23		2
3.70	3.67	1.64	1.26	1.22		2
1.85	1.83	.82	1.25	1.24	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.28	1044.65	258.38	786.27	552.29	233.98	6
59.77	1081.22	220.92	860.30	584.24	276.06	6
59.25	1118.31	185.99	932.32	616.71	315.61	6
58.72	1155.87	154.51	1001.36	649.65	351.71	6
58.19	1193.85	127.26	1066.59	683.01	383.59	6
57.65	1232.19	104.64	1127.55	716.72	410.82	6
57.10	1270.81	86.66	1184.15	750.73	433.42	6
56.56	1309.66	72.95	1236.70	784.96	451.75	6
56.00	1348.68	62.83	1285.85	819.35	466.49	6
56.00	1348.68	62.83	1285.85	819.35	466.49	5
54.75	1452.89	79.93	1372.96	897.81	475.14	5
53.50	1556.43	100.01	1456.41	975.60	480.81	5
52.27	1659.21	122.25	1536.96	1052.63	484.33	5
51.04	1761.16	145.94	1615.22	1128.84	486.38	5
49.84	1862.25	170.61	1691.64	1204.17	487.46	5
48.64	1962.43	195.97	1766.46	1278.61	487.85	5
48.64	1962.43	195.97	1766.46	1278.61	487.85	4
46.65	2162.86	268.72	1894.14	1403.18	490.97	4
44.66	2362.77	347.17	2015.60	1527.23	488.37	4
42.68	2562.12	434.06	2128.06	1650.72	477.34	4
40.71	2760.84	519.03	2241.81	1773.58	468.23	4
38.76	2958.83	582.44	2376.40	1895.71	480.68	4
36.81	3156.05	650.40	2505.64	2017.07	488.58	4
34.88	3352.42	722.59	2629.84	2137.58	492.25	4
32.96	3547.91	798.34	2749.58	2257.22	492.36	4
31.06	3742.50	874.19	2868.30	2375.94	492.36	4
31.06	3742.50	874.20	2868.30	2375.94	492.36	3
29.67	3891.07	936.05	2955.01	2462.65	492.36	3
28.29	4039.24	997.91	3041.33	2548.97	492.36	3
26.91	4187.04	1063.12	3123.92	2634.91	489.01	3
25.54	4334.47	1126.69	3207.78	2720.48	487.30	3
24.17	4481.55	1189.10	3292.46	2805.70	486.75	3
22.81	4628.28	1250.90	3377.38	2890.58	486.81	3
21.46	4774.67	1312.36	3462.31	2975.10	487.21	3
20.11	4920.71	1373.53	3547.18	3059.28	487.90	3
18.76	5066.41	1434.31	3632.09	3143.12	488.97	3
18.76	5066.41	1434.31	3632.10	3143.12	488.97	2
16.85	5272.06	1518.32	3753.74	3262.68	491.06	2
14.94	5477.19	1603.62	3873.57	3381.71	491.86	2
13.04	5681.80	1689.40	3992.40	3500.22	492.18	2
11.15	5885.88	1775.31	4110.57	3618.20	492.36	2
9.27	6089.44	1861.41	4228.03	3735.67	492.36	2
7.40	6292.45	1947.51	4344.94	3852.58	492.36	2
5.53	6494.96	2038.26	4456.70	3968.99	487.71	2
3.67	6696.97	2176.61	4520.36	4084.90	435.46	2
1.83	6898.25	2408.08	4490.17	4200.08	290.09	2
.00	7098.30	2784.26	4314.03	4314.03	.00	2

Time = 121. Degree of Consolidation = 8.%

Total Settlement = .300

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 121. = .300

Settlement caused by Secondary Compression at time 121. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
9.19	8.85	4.64	.98	.98	.98	1
6.89	6.61	3.48	.98	.91	.91	1
4.59	4.40	2.32	.98	.90	.90	1
2.30	2.20	1.16	.98	.90	.89	1
.00	.00	.00	.98	.90	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
8.85	.00	.00	.00	.00	.00	1
6.61	263.17	123.09	140.08	140.08	.00	1
4.40	523.92	246.18	277.74	277.74	.00	1
2.20	784.28	265.86	518.42	415.01	103.41	1
.00	1044.65	258.38	786.27	552.29	233.98	1

Time = 121. Degree of Consolidation = 97.%

Total Settlement = .339

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 121. = .339

Settlement caused by Secondary Compression at time 121. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 7.15

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.11	21.42	6.50	5.67	5.01	6
60.02	59.61	21.35	6.49	5.75	5.00	6

59.45	59.09	21.27	6.47	5.83	4.99	6
58.89	58.58	21.20	6.46	5.91	4.98	6
58.33	58.05	21.12	6.44	5.98	4.97	6
57.76	57.52	21.05	6.43	6.05	4.97	6
57.20	56.99	20.97	6.42	6.11	4.96	6
56.64	56.45	20.90	6.40	6.16	4.95	6
56.08	55.90	20.82	6.39	6.21	4.95	6
56.08	55.90	20.82	4.51	4.36	3.33	5
54.82	54.66	20.59	4.44	4.33	3.30	5
53.56	53.43	20.36	4.38	4.29	3.27	5
52.32	52.21	20.12	4.32	4.24	3.24	5
51.10	51.00	19.89	4.25	4.19	3.21	5
49.88	49.80	19.66	4.19	4.14	3.18	5
48.69	48.62	19.43	4.13	4.07	3.15	5
48.69	48.62	19.43	1.93	1.93	1.83	4
46.69	46.63	18.75	1.92	1.91	1.81	4
44.70	44.64	18.06	1.91	1.90	1.79	4
42.72	42.66	17.38	1.89	1.89	1.76	4
40.75	40.69	16.70	1.88	1.87	1.74	4
38.79	38.74	16.01	1.86	1.85	1.72	4
36.85	36.80	15.33	1.84	1.84	1.70	4
34.91	34.86	14.65	1.82	1.82	1.68	4
33.00	32.95	13.97	1.80	1.80	1.66	4
31.09	31.04	13.28	1.78	1.78	1.63	4
31.09	31.04	13.28	1.47	1.47	1.39	3
29.70	29.66	12.72	1.46	1.46	1.38	3
28.32	28.27	12.16	1.45	1.45	1.37	3
26.94	26.89	11.59	1.44	1.44	1.36	3
25.57	25.52	11.03	1.43	1.43	1.35	3
24.21	24.16	10.47	1.42	1.42	1.34	3
22.84	22.80	9.90	1.41	1.41	1.33	3
21.49	21.44	9.34	1.40	1.40	1.32	3
20.14	20.10	8.78	1.39	1.39	1.31	3
18.80	18.75	8.21	1.38	1.38	1.30	3
18.80	18.75	8.21	1.34	1.34	1.28	2
16.88	16.84	7.39	1.33	1.33	1.27	2
14.97	14.93	6.57	1.32	1.32	1.26	2
13.07	13.03	5.75	1.31	1.31	1.26	2
11.18	11.14	4.93	1.30	1.30	1.25	2
9.30	9.26	4.11	1.29	1.29	1.24	2
7.43	7.38	3.29	1.28	1.28	1.23	2
5.56	5.52	2.46	1.27	1.26	1.23	2
3.70	3.66	1.64	1.26	1.25	1.22	2
1.85	1.82	.82	1.25	1.23	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.11	1044.60	275.74	768.85	552.24	216.62	6
59.61	1080.85	247.88	832.97	583.87	249.10	6
59.09	1117.50	221.09	896.40	615.89	280.51	6
58.58	1154.51	195.64	958.87	648.29	310.59	6
58.05	1191.88	171.79	1020.09	681.03	339.05	6
57.52	1229.57	149.77	1079.80	714.11	365.70	6
56.99	1267.56	129.72	1137.85	747.48	390.37	6
56.45	1305.83	111.71	1194.12	781.12	413.00	6
55.90	1344.33	95.72	1248.61	815.01	433.60	6
55.90	1344.33	95.72	1248.61	815.01	433.60	5
54.66	1447.43	109.01	1338.42	892.36	446.06	5
53.43	1550.00	125.05	1424.96	969.18	455.78	5
52.21	1651.95	143.61	1508.34	1045.38	462.97	5

51.00	1753.19	164.47	1588.72	1120.87	467.85	5
49.80	1853.65	187.45	1666.20	1195.57	470.63	5
48.62	1953.24	212.39	1740.85	1269.42	471.44	5
48.62	1953.24	212.39	1740.85	1269.42	471.44	4
46.63	2153.57	281.77	1871.80	1393.88	477.91	4
44.64	2353.39	359.28	1994.11	1517.85	476.26	4
42.66	2552.66	447.22	2105.44	1641.26	464.19	4
40.69	2751.28	527.08	2224.20	1764.02	460.18	4
38.74	2949.19	589.60	2359.59	1886.07	473.52	4
36.80	3146.32	655.47	2490.85	2007.34	483.50	4
34.86	3342.66	724.98	2617.67	2127.82	489.85	4
32.95	3538.13	798.34	2739.80	2247.44	492.36	4
31.04	3732.72	874.19	2858.53	2366.16	492.36	4
31.04	3732.72	874.20	2858.53	2366.16	492.36	3
29.66	3881.29	936.05	2945.24	2452.88	492.36	3
28.27	4029.47	997.91	3031.55	2539.19	492.36	3
26.89	4177.26	1064.86	3112.39	2625.13	487.27	3
25.52	4324.68	1129.84	3194.84	2710.69	484.15	3
24.16	4471.74	1193.15	3278.59	2795.89	482.70	3
22.80	4618.45	1255.31	3363.14	2880.74	482.40	3
21.44	4764.81	1316.67	3448.14	2965.24	482.90	3
20.10	4910.82	1377.40	3533.42	3049.40	484.02	3
18.75	5056.50	1437.55	3618.95	3133.22	485.74	3
18.75	5056.50	1437.55	3618.95	3133.22	485.74	2
16.84	5262.14	1520.29	3741.85	3252.76	489.09	2
14.93	5467.26	1604.59	3862.67	3371.78	490.89	2
13.03	5671.87	1689.78	3982.09	3490.29	491.80	2
11.14	5875.94	1775.45	4100.49	3608.27	492.23	2
9.26	6079.49	1861.48	4218.01	3725.72	492.29	2
7.38	6282.51	1948.77	4333.74	3842.64	491.10	2
5.52	6484.97	2063.52	4421.45	3959.00	462.45	2
3.66	6686.81	2239.89	4446.92	4074.74	372.18	2
1.82	6887.78	2482.34	4405.44	4189.61	215.83	2
.00	7087.64	2784.26	4303.37	4303.37	.00	2

Time = 240. Degree of Consolidation = 12.%

Total Settlement = .470

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 240. = .470

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.85	4.64	.98	.98	.98	1
6.89	6.61	3.48	.98	.91	.91	1
4.59	4.40	2.32	.98	.90	.90	1
2.30	2.20	1.16	.98	.90	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
8.85	.00	.00	.00	.00	.00	1
6.61	263.17	123.09	140.08	140.08	.00	1
4.40	523.92	246.18	277.74	277.74	.00	1
2.20	784.27	270.11	514.16	415.00	99.16	1
.00	1044.60	275.74	768.85	552.24	216.62	1

Time = 240. Degree of Consolidation = 97.%

Total Settlement = .340

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 240. = .340

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.98

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.96	21.42	6.50	5.63	5.01	6
60.02	59.46	21.35	6.49	5.70	5.00	6
59.45	58.95	21.27	6.47	5.78	4.99	6
58.89	58.44	21.20	6.46	5.84	4.98	6
58.33	57.92	21.12	6.44	5.91	4.97	6
57.76	57.39	21.05	6.43	5.97	4.97	6
57.20	56.86	20.97	6.42	6.03	4.96	6
56.64	56.33	20.90	6.40	6.08	4.95	6
56.08	55.79	20.82	6.39	6.13	4.95	6
56.08	55.79	20.82	4.51	4.30	3.33	5
54.82	54.57	20.59	4.44	4.26	3.30	5
53.56	53.35	20.36	4.38	4.23	3.27	5
52.32	52.15	20.12	4.32	4.18	3.24	5
51.10	50.95	19.89	4.25	4.13	3.21	5
49.88	49.77	19.66	4.19	4.08	3.18	5
48.69	48.60	19.43	4.13	4.02	3.15	5
48.69	48.60	19.43	1.93	1.92	1.83	4
46.69	46.61	18.75	1.92	1.91	1.81	4
44.70	44.62	18.06	1.91	1.90	1.79	4
42.72	42.65	17.38	1.89	1.89	1.76	4
40.75	40.68	16.70	1.88	1.87	1.74	4
38.79	38.73	16.01	1.86	1.85	1.72	4
36.85	36.78	15.33	1.84	1.84	1.70	4
34.91	34.85	14.65	1.82	1.82	1.68	4
33.00	32.94	13.97	1.80	1.80	1.66	4
31.09	31.03	13.28	1.78	1.78	1.63	4
31.09	31.03	13.28	1.47	1.47	1.39	3
29.70	29.64	12.72	1.46	1.46	1.38	3
28.32	28.26	12.16	1.45	1.45	1.37	3
26.94	26.88	11.59	1.44	1.44	1.36	3
25.57	25.51	11.03	1.43	1.43	1.35	3

24.21	24.15	10.47	1.42	1.42	1.34	3
22.84	22.79	9.90	1.41	1.41	1.33	3
21.49	21.43	9.34	1.40	1.40	1.32	3
20.14	20.09	8.78	1.39	1.39	1.31	3
18.80	18.74	8.21	1.38	1.38	1.30	3
18.80	18.74	8.21	1.34	1.34	1.28	2
16.88	16.83	7.39	1.33	1.33	1.27	2
14.97	14.92	6.57	1.32	1.32	1.26	2
13.07	13.02	5.75	1.31	1.31	1.26	2
11.18	11.13	4.93	1.30	1.30	1.25	2
9.30	9.25	4.11	1.29	1.29	1.24	2
7.43	7.38	3.29	1.28	1.28	1.23	2
5.56	5.51	2.46	1.27	1.26	1.23	2
3.70	3.66	1.64	1.26	1.25	1.22	2
1.85	1.82	.82	1.25	1.23	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.96	1044.52	287.22	757.30	552.16	205.14	6
59.46	1080.58	263.27	817.31	583.60	233.71	6
58.95	1116.98	239.97	877.01	615.38	261.63	6
58.44	1153.70	217.46	936.24	647.48	288.76	6
57.92	1190.74	195.93	994.80	679.90	314.91	6
57.39	1228.08	175.55	1052.52	712.61	339.91	6
56.86	1265.69	156.47	1109.23	745.61	363.62	6
56.33	1303.57	138.80	1164.78	778.87	385.91	6
55.79	1341.70	122.65	1219.05	812.37	406.68	6
55.79	1341.70	122.65	1219.05	812.37	406.68	5
54.57	1443.83	135.60	1308.23	888.76	419.48	5
53.35	1545.46	150.97	1394.49	964.64	429.85	5
52.15	1646.49	168.73	1477.77	1039.92	437.85	5
50.95	1746.85	188.82	1558.03	1114.52	443.50	5
49.77	1846.44	211.18	1635.26	1188.37	446.90	5
48.60	1945.19	235.74	1709.45	1261.37	448.09	5
48.60	1945.19	235.74	1709.45	1261.37	448.09	4
46.61	2145.37	301.75	1843.62	1385.69	457.93	4
44.62	2345.07	376.62	1968.45	1509.53	458.93	4
42.65	2544.22	462.77	2081.45	1632.82	448.63	4
40.68	2742.74	534.94	2207.81	1755.48	452.32	4
38.73	2940.56	595.89	2344.68	1877.45	467.23	4
36.78	3137.64	660.05	2477.59	1998.66	478.93	4
34.85	3333.93	727.57	2606.36	2119.09	487.27	4
32.94	3529.39	798.75	2730.64	2238.69	491.94	4
31.03	3723.97	874.39	2849.58	2357.42	492.16	4
31.03	3723.97	874.39	2849.58	2357.42	492.16	3
29.64	3872.54	936.05	2936.49	2444.13	492.36	3
28.26	4020.72	997.91	3022.81	2530.45	492.36	3
26.88	4168.51	1066.12	3102.38	2616.38	486.01	3
25.51	4315.92	1132.19	3183.73	2701.93	481.81	3
24.15	4462.96	1196.28	3266.69	2787.11	479.57	3
22.79	4609.65	1258.88	3350.77	2871.94	478.83	3
21.43	4755.99	1320.33	3435.66	2956.42	479.24	3
20.09	4901.99	1380.85	3521.14	3040.56	480.57	3
18.74	5047.65	1440.56	3607.09	3124.36	482.72	3
18.74	5047.65	1440.56	3607.09	3124.36	482.72	2
16.83	5253.27	1522.45	3730.82	3243.89	486.94	2
14.92	5458.38	1605.94	3852.45	3362.90	489.54	2
13.02	5662.98	1690.55	3972.43	3481.40	491.03	2
11.13	5867.05	1776.20	4090.85	3599.38	491.48	2
9.25	6070.59	1863.73	4206.86	3716.82	490.04	2

7.38	6273.58	1956.67	4316.92	3833.71	483.21	2
5.51	6475.96	2093.53	4382.44	3949.99	432.44	2
3.66	6677.64	2285.89	4391.75	4065.57	326.18	2
1.82	6878.43	2520.58	4357.85	4180.26	177.59	2
.00	7078.19	2784.26	4293.93	4293.93	.00	2

Time = 365. Degree of Consolidation = 16.%

Total Settlement = .620

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 365. = .620

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.85	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.40	2.32	.98	.90	.90	1
2.30	2.20	1.16	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
8.85	.00	.00	.00	.00	.00	1
6.60	263.17	123.09	140.08	140.08	.00	1
4.40	523.92	246.18	277.74	277.74	.00	1
2.20	784.25	280.07	504.18	414.98	89.20	1
.00	1044.52	287.22	757.30	552.16	205.14	1

Time = 365. Degree of Consolidation = 97.%

Total Settlement = .341

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 365. = .341

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.83

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.78	21.42	6.50	5.60	5.01	6
60.02	59.28	21.35	6.49	5.66	5.00	6
59.45	58.77	21.27	6.47	5.72	4.99	6
58.89	58.26	21.20	6.46	5.78	4.98	6
58.33	57.74	21.12	6.44	5.84	4.97	6
57.76	57.23	21.05	6.43	5.89	4.97	6
57.20	56.70	20.97	6.42	5.94	4.96	6
56.64	56.18	20.90	6.40	5.99	4.95	6
56.08	55.65	20.82	6.39	6.03	4.95	6
56.08	55.65	20.82	4.51	4.22	3.33	5
54.82	54.44	20.59	4.44	4.18	3.30	5
53.56	53.25	20.36	4.38	4.14	3.27	5
52.32	52.06	20.12	4.32	4.10	3.24	5
51.10	50.88	19.89	4.25	4.05	3.21	5
49.88	49.72	19.66	4.19	3.99	3.18	5
48.69	48.57	19.43	4.13	3.93	3.15	5
48.69	48.57	19.43	1.93	1.92	1.83	4
46.69	46.58	18.75	1.92	1.91	1.81	4
44.70	44.60	18.06	1.91	1.90	1.79	4
42.72	42.62	17.38	1.89	1.88	1.76	4
40.75	40.66	16.70	1.88	1.87	1.74	4
38.79	38.71	16.01	1.86	1.85	1.72	4
36.85	36.77	15.33	1.84	1.83	1.70	4
34.91	34.84	14.65	1.82	1.81	1.68	4
33.00	32.92	13.97	1.80	1.80	1.66	4
31.09	31.02	13.28	1.78	1.77	1.63	4
31.09	31.02	13.28	1.47	1.47	1.39	3
29.70	29.63	12.72	1.46	1.46	1.38	3
28.32	28.25	12.16	1.45	1.45	1.37	3
26.94	26.87	11.59	1.44	1.44	1.36	3
25.57	25.50	11.03	1.43	1.43	1.35	3
24.21	24.14	10.47	1.42	1.42	1.34	3
22.84	22.78	9.90	1.41	1.41	1.33	3
21.49	21.42	9.34	1.40	1.40	1.32	3
20.14	20.07	8.78	1.39	1.39	1.31	3
18.80	18.73	8.21	1.38	1.38	1.30	3
18.80	18.73	8.21	1.34	1.34	1.28	2
16.88	16.82	7.39	1.33	1.33	1.27	2
14.97	14.91	6.57	1.32	1.32	1.26	2
13.07	13.01	5.75	1.31	1.31	1.26	2
11.18	11.12	4.93	1.30	1.30	1.25	2
9.30	9.24	4.11	1.29	1.29	1.24	2
7.43	7.37	3.29	1.28	1.27	1.23	2
5.56	5.51	2.46	1.27	1.26	1.23	2
3.70	3.66	1.64	1.26	1.24	1.22	2
1.85	1.82	.82	1.25	1.23	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.78	1044.44	298.05	746.38	552.07	194.31	6
59.28	1080.32	277.63	802.69	583.34	219.36	6
58.77	1116.49	257.67	858.82	614.89	243.93	6
58.26	1152.94	238.30	914.64	646.72	267.92	6
57.74	1189.66	219.65	970.01	678.82	291.19	6
57.23	1226.64	201.86	1024.78	711.18	313.60	6
56.70	1263.87	185.07	1078.80	743.78	335.01	6
56.18	1301.32	169.41	1131.92	776.62	355.30	6

55.65	1339.00	154.99	1184.00	809.67	374.33	6
55.65	1339.00	154.99	1184.00	809.67	374.33	5
54.44	1439.96	168.76	1271.20	884.88	386.32	5
53.25	1540.39	184.61	1355.78	959.56	396.22	5
52.06	1640.21	202.57	1437.64	1033.63	404.00	5
50.88	1739.35	222.65	1516.70	1107.02	409.68	5
49.72	1837.73	244.82	1592.91	1179.66	413.26	5
48.57	1935.28	269.04	1666.24	1251.46	414.78	5
48.57	1935.28	269.04	1666.24	1251.46	414.78	4
46.58	2135.24	332.03	1803.21	1375.56	427.65	4
44.60	2334.75	403.95	1930.80	1499.20	431.59	4
42.62	2533.72	487.50	2046.22	1622.32	423.90	4
40.66	2732.08	547.13	2184.95	1744.82	440.13	4
38.71	2929.77	605.38	2324.39	1866.66	457.74	4
36.77	3126.75	667.08	2459.67	1987.77	471.90	4
34.84	3322.97	732.38	2590.59	2108.13	482.46	4
32.92	3518.38	801.67	2716.71	2227.69	489.02	4
31.02	3712.94	875.80	2837.15	2346.39	490.76	4
31.02	3712.94	875.80	2837.15	2346.39	490.76	3
29.63	3861.51	936.05	2925.46	2433.09	492.36	3
28.25	4009.69	997.91	3011.78	2519.41	492.36	3
26.87	4157.47	1067.40	3090.07	2605.34	484.73	3
25.50	4304.87	1134.58	3170.29	2690.88	479.41	3
24.14	4451.90	1199.56	3252.34	2776.05	476.29	3
22.78	4598.57	1262.71	3335.85	2860.86	474.99	3
21.42	4744.89	1324.40	3420.49	2945.32	475.17	3
20.07	4890.86	1384.85	3506.01	3029.43	476.57	3
18.73	5036.50	1444.24	3592.26	3113.21	479.04	3
18.73	5036.50	1444.24	3592.26	3113.21	479.04	2
16.82	5242.10	1525.49	3716.61	3232.72	483.89	2
14.91	5447.20	1608.33	3838.87	3351.72	487.15	2
13.01	5651.78	1692.86	3958.92	3470.20	488.72	2
11.12	5855.83	1779.80	4076.04	3588.16	487.88	2
9.24	6059.34	1871.26	4188.08	3705.57	482.51	2
7.37	6262.26	1971.97	4290.29	3822.39	467.90	2
5.51	6464.52	2130.64	4333.88	3938.55	395.33	2
3.66	6666.02	2328.51	4337.52	4053.96	283.56	2
1.82	6866.66	2550.20	4316.46	4168.50	147.96	2
.00	7066.36	2784.26	4282.10	4282.10	.00	2

Time = 541. Degree of Consolidation = 20.%

Total Settlement = .808

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 541. = .808

Settlement caused by Secondary Compression at time 541. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.85	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.40	2.32	.98	.90	.90	1

2.30	2.20	1.16	.98	.89	1
.00	.00	.00	.98	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
8.85	.00	.00	.00	.00	.00	1
6.60	263.16	123.09	140.07	140.07	.00	1
4.40	523.92	246.18	277.74	277.74	.00	1
2.20	784.23	289.94	494.29	414.95	79.33	1
.00	1044.44	298.05	746.38	552.07	194.31	1

Time = 541. Degree of Consolidation = 98.%

Total Settlement = .343

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 541. = .343

Settlement caused by Secondary Compression at time 541. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.64

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.59	21.42	6.50	5.57	5.01	6
60.02	59.09	21.35	6.49	5.62	5.00	6
59.45	58.59	21.27	6.47	5.68	4.99	6
58.89	58.09	21.20	6.46	5.73	4.98	6
58.33	57.58	21.12	6.44	5.77	4.97	6
57.76	57.06	21.05	6.43	5.82	4.97	6
57.20	56.55	20.97	6.42	5.86	4.96	6
56.64	56.03	20.90	6.40	5.90	4.95	6
56.08	55.50	20.82	6.39	5.94	4.95	6
56.08	55.50	20.82	4.51	4.14	3.33	5
54.82	54.32	20.59	4.44	4.10	3.30	5
53.56	53.14	20.36	4.38	4.06	3.27	5
52.32	51.97	20.12	4.32	4.02	3.24	5
51.10	50.81	19.89	4.25	3.96	3.21	5
49.88	49.67	19.66	4.19	3.91	3.18	5
48.69	48.54	19.43	4.13	3.85	3.15	5
48.69	48.54	19.43	1.93	1.91	1.83	4
46.69	46.55	18.75	1.92	1.90	1.81	4
44.70	44.57	18.06	1.91	1.89	1.79	4
42.72	42.60	17.38	1.89	1.88	1.76	4
40.75	40.64	16.70	1.88	1.86	1.74	4
38.79	38.69	16.01	1.86	1.85	1.72	4
36.85	36.75	15.33	1.84	1.83	1.70	4
34.91	34.83	14.65	1.82	1.81	1.68	4
33.00	32.91	13.97	1.80	1.79	1.66	4
31.09	31.01	13.28	1.78	1.77	1.63	4

31.09	31.01	13.28	1.47	1.47	1.39	3
29.70	29.62	12.72	1.46	1.46	1.38	3
28.32	28.24	12.16	1.45	1.45	1.37	3
26.94	26.86	11.59	1.44	1.44	1.36	3
25.57	25.49	11.03	1.43	1.43	1.35	3
24.21	24.12	10.47	1.42	1.42	1.34	3
22.84	22.77	9.90	1.41	1.41	1.33	3
21.49	21.41	9.34	1.40	1.40	1.32	3
20.14	20.06	8.78	1.39	1.39	1.31	3
18.80	18.72	8.21	1.38	1.38	1.30	3
18.80	18.72	8.21	1.34	1.34	1.28	2
16.88	16.81	7.39	1.33	1.33	1.27	2
14.97	14.90	6.57	1.32	1.32	1.26	2
13.07	13.00	5.75	1.31	1.31	1.26	2
11.18	11.11	4.93	1.30	1.30	1.25	2
9.30	9.23	4.11	1.29	1.28	1.24	2
7.43	7.36	3.29	1.28	1.27	1.23	2
5.56	5.50	2.46	1.27	1.26	1.23	2
3.70	3.65	1.64	1.26	1.24	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.59	1044.36	307.52	736.84	552.00	184.84	6
59.09	1080.09	290.01	790.07	583.11	206.97	6
58.59	1116.06	272.94	843.12	614.46	228.66	6
58.09	1152.27	256.38	895.89	646.05	249.84	6
57.58	1188.72	240.45	948.26	677.87	270.39	6
57.06	1225.38	225.28	1000.10	709.92	290.18	6
56.55	1262.26	210.98	1051.27	742.17	309.10	6
56.03	1299.33	197.67	1101.66	774.63	327.04	6
55.50	1336.58	185.45	1151.13	807.26	343.87	6
55.50	1336.58	185.45	1151.13	807.26	343.87	5
54.32	1436.43	200.38	1236.05	881.36	354.70	5
53.14	1535.71	217.10	1318.61	954.88	363.72	5
51.97	1634.35	235.65	1398.70	1027.78	370.92	5
50.81	1732.30	256.05	1476.25	1099.98	376.27	5
49.67	1829.48	278.29	1551.20	1171.41	379.79	5
48.54	1925.83	302.33	1623.50	1242.01	381.49	5
48.54	1925.83	302.33	1623.50	1242.01	381.49	4
46.55	2125.57	363.65	1761.92	1365.89	396.03	4
44.57	2324.87	433.88	1890.99	1489.33	401.66	4
42.60	2523.64	508.80	2014.84	1612.24	402.60	4
40.64	2721.83	561.07	2160.76	1734.57	426.19	4
38.69	2919.37	616.77	2302.59	1856.25	446.35	4
36.75	3116.22	675.99	2440.23	1977.24	462.99	4
34.83	3312.35	738.95	2573.40	2097.51	475.89	4
32.91	3507.70	806.09	2701.61	2217.00	484.61	4
31.01	3702.22	878.30	2823.92	2335.66	488.25	4
31.01	3702.22	878.30	2823.92	2335.66	488.26	3
29.62	3850.77	936.78	2914.00	2422.36	491.64	3
28.24	3998.95	998.44	3000.51	2508.68	491.83	3
26.86	4146.73	1068.64	3078.09	2594.60	483.49	3
25.49	4294.12	1136.57	3157.55	2680.13	477.42	3
24.12	4441.13	1202.19	3238.94	2765.29	473.66	3
22.77	4587.79	1265.86	3321.92	2850.08	471.85	3
21.41	4734.08	1327.84	3406.24	2934.52	471.72	3
20.06	4880.04	1388.42	3491.62	3018.61	473.00	3
18.72	5025.66	1447.80	3577.86	3102.37	475.49	3
18.72	5025.66	1447.80	3577.86	3102.37	475.49	2

16.81	5231.24	1528.99	3702.25	3221.85	480.39	2
14.90	5436.31	1611.90	3824.41	3340.83	483.58	2
13.00	5640.87	1697.26	3943.61	3459.29	484.32	2
11.11	5844.89	1786.43	4058.46	3577.22	481.24	2
9.23	6048.35	1882.05	4166.30	3694.58	471.72	2
7.36	6251.19	1988.55	4262.64	3811.32	451.32	2
5.50	6453.33	2162.30	4291.03	3927.36	363.67	2
3.65	6654.70	2358.79	4295.91	4042.63	253.28	2
1.82	6855.23	2569.01	4286.23	4157.07	129.16	2
.00	7054.89	2784.26	4270.63	4270.63	.00	2

Time = 730. Degree of Consolidation = 25.%

Total Settlement = .991

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 730. = .991

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.85	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.40	2.32	.98	.90	.90	1
2.30	2.20	1.16	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
8.85	.00	.00	.00	.00	.00	1
6.60	263.15	123.09	140.06	140.06	.00	1
4.40	523.92	246.18	277.74	277.74	.00	1
2.20	784.20	299.17	485.03	414.93	70.10	1
.00	1044.36	307.52	736.84	552.00	184.84	1

Time = 730. Degree of Consolidation = 98.%

Total Settlement = .344

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 730. = .344

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.46

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
60.58	59.29	21.42
60.02	58.80	21.35
59.45	58.30	21.27
58.89	57.80	21.20
58.33	57.30	21.12
57.76	56.79	21.05
57.20	56.29	20.97
56.64	55.78	20.90
56.08	55.26	20.82
56.08	55.26	20.82
54.82	54.10	20.59
53.56	52.95	20.36
52.32	51.82	20.12
51.10	50.69	19.89
49.88	49.58	19.66
48.69	48.48	19.43
48.69	48.48	19.43
46.69	46.50	18.75
44.70	44.52	18.06
42.72	42.56	17.38
40.75	40.60	16.70
38.79	38.66	16.01
36.85	36.72	15.33
34.91	34.80	14.65
33.00	32.89	13.97
31.09	30.99	13.28
31.09	30.99	13.28
29.70	29.60	12.72
28.32	28.22	12.16
26.94	26.84	11.59
25.57	25.47	11.03
24.21	24.11	10.47
22.84	22.75	9.90
21.49	21.40	9.34
20.14	20.05	8.78
18.80	18.71	8.21
18.80	18.71	8.21
16.88	16.79	7.39
14.97	14.89	6.57
13.07	12.99	5.75
11.18	11.10	4.93
9.30	9.22	4.11
7.43	7.35	3.29
5.56	5.50	2.46
3.70	3.65	1.64
1.85	1.82	.82
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
6.50	5.52	5.01	6
6.49	5.56	5.00	6
6.47	5.60	4.99	6
6.46	5.64	4.98	6
6.44	5.68	4.97	6
6.43	5.71	4.97	6
6.42	5.74	4.96	6
6.40	5.77	4.95	6
6.39	5.80	4.95	6
4.51	4.02	3.33	5
4.44	3.98	3.30	5
4.38	3.93	3.27	5
4.32	3.88	3.24	5
4.25	3.83	3.21	5
4.19	3.78	3.18	5
4.13	3.72	3.15	5
1.93	1.90	1.83	4
1.92	1.89	1.81	4
1.91	1.88	1.79	4
1.89	1.87	1.76	4
1.88	1.86	1.74	4
1.86	1.84	1.72	4
1.84	1.83	1.70	4
1.82	1.81	1.68	4
1.80	1.79	1.66	4
1.78	1.77	1.63	4
1.47	1.47	1.39	3
1.46	1.46	1.38	3
1.45	1.45	1.37	3
1.44	1.44	1.36	3
1.43	1.43	1.35	3
1.42	1.42	1.34	3
1.41	1.41	1.33	3
1.40	1.40	1.32	3
1.39	1.39	1.31	3
1.38	1.38	1.30	3
1.34	1.34	1.28	2
1.33	1.33	1.27	2
1.32	1.32	1.26	2
1.31	1.30	1.26	2
1.30	1.29	1.25	2
1.29	1.28	1.24	2
1.28	1.27	1.23	2
1.27	1.25	1.23	2
1.26	1.24	1.22	2
1.25	1.22	1.21	2
1.25	1.21	1.21	2

***** Stresses *****

XI	Total	Effective
59.29	1044.22	322.94
58.80	1079.70	309.77
58.30	1115.36	297.00

***** Pore Pressures *****

Total	Static	Excess	Material
721.28	551.86	169.42	6
769.93	582.72	187.22	6
818.36	613.76	204.60	6

57.80	1151.20	284.70	866.50	644.98	221.52	6
57.30	1187.21	272.96	914.25	676.37	237.88	6
56.79	1223.38	261.86	961.52	707.92	253.60	6
56.29	1259.71	251.51	1008.20	739.63	268.58	6
55.78	1296.18	241.97	1054.20	771.47	282.73	6
55.26	1332.77	233.35	1099.43	803.45	295.98	6
55.26	1332.77	233.35	1099.43	803.45	295.98	5
54.10	1430.86	250.30	1180.57	875.79	304.78	5
52.95	1528.32	268.62	1259.70	947.50	312.20	5
51.82	1625.10	288.36	1336.73	1018.52	318.21	5
50.69	1721.14	309.53	1411.61	1088.81	322.80	5
49.58	1816.39	332.12	1484.27	1158.32	325.96	5
48.48	1910.81	356.12	1554.69	1226.99	327.71	5
48.48	1910.81	356.12	1554.69	1226.99	327.71	4
46.50	2110.19	416.95	1693.24	1350.51	342.74	4
44.52	2309.12	486.79	1822.33	1473.58	348.75	4
42.56	2507.54	537.60	1969.94	1596.14	373.80	4
40.60	2705.40	586.42	2118.98	1718.14	400.84	4
38.66	2902.66	638.61	2264.05	1839.54	424.51	4
36.72	3099.28	694.36	2404.91	1960.30	444.61	4
34.80	3295.20	754.06	2541.14	2080.36	460.77	4
32.89	3490.39	818.38	2672.01	2199.69	472.31	4
30.99	3684.78	888.51	2796.26	2318.22	478.04	4
30.99	3684.78	888.51	2796.26	2318.22	478.04	3
29.60	3833.27	945.04	2888.23	2404.86	483.38	3
28.22	3981.40	1005.77	2975.63	2491.13	484.50	3
26.84	4129.14	1074.84	3054.30	2577.01	477.29	3
25.47	4276.50	1142.11	3134.39	2662.51	471.88	3
24.11	4423.48	1207.61	3215.87	2747.64	468.24	3
22.75	4570.11	1271.43	3298.67	2832.40	466.28	3
21.40	4716.37	1333.71	3382.66	2916.81	465.86	3
20.05	4862.29	1394.64	3467.65	3000.87	466.78	3
18.71	5007.87	1454.43	3553.45	3084.59	468.86	3
18.71	5007.87	1454.43	3553.45	3084.59	468.86	2
16.79	5213.41	1536.44	3676.97	3204.03	472.94	2
14.89	5418.44	1620.83	3797.60	3322.96	474.65	2
12.99	5622.93	1708.75	3914.19	3441.35	472.83	2
11.10	5826.87	1801.90	4024.97	3559.20	465.77	2
9.22	6030.22	1902.88	4127.34	3676.45	450.89	2
7.35	6232.91	2022.13	4210.79	3793.04	417.75	2
5.50	6434.88	2204.25	4230.63	3908.91	321.72	2
3.65	6636.09	2394.31	4241.78	4024.02	217.76	2
1.82	6836.51	2589.42	4247.08	4138.34	108.74	2
.00	7036.12	2784.26	4251.86	4251.86	.00	2

Time = 1080. Degree of Consolidation = 32.%

Total Settlement = 1.289

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 1080. = 1.289

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.84	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.39	2.32	.98	.90	.90	1
2.30	2.20	1.16	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
8.84	.00	.00	.00	.00	.00	1
6.60	263.14	123.09	140.05	140.05	.00	1
4.39	523.92	246.18	277.74	277.74	.00	1
2.20	784.16	316.98	467.18	414.89	52.29	1
.00	1044.22	322.94	721.28	551.86	169.42	1

Time = 1080. Degree of Consolidation = 99.%

Total Settlement = .346

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 1080. = .346

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.15

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.03	21.42	6.50	5.49	5.01	6
60.02	58.54	21.35	6.49	5.51	5.00	6
59.45	58.04	21.27	6.47	5.54	4.99	6
58.89	57.55	21.20	6.46	5.57	4.98	6
58.33	57.05	21.12	6.44	5.59	4.97	6
57.76	56.55	21.05	6.43	5.61	4.97	6
57.20	56.05	20.97	6.42	5.63	4.96	6
56.64	55.55	20.90	6.40	5.65	4.95	6
56.08	55.05	20.82	6.39	5.67	4.95	6
56.08	55.05	20.82	4.51	3.92	3.33	5
54.82	53.91	20.59	4.44	3.87	3.30	5
53.56	52.79	20.36	4.38	3.82	3.27	5
52.32	51.68	20.12	4.32	3.77	3.24	5
51.10	50.58	19.89	4.25	3.72	3.21	5
49.88	49.49	19.66	4.19	3.66	3.18	5
48.69	48.41	19.43	4.13	3.60	3.15	5
48.69	48.41	19.43	1.93	1.90	1.83	4
46.69	46.44	18.75	1.92	1.89	1.81	4
44.70	44.47	18.06	1.91	1.87	1.79	4
42.72	42.51	17.38	1.89	1.86	1.76	4
40.75	40.56	16.70	1.88	1.85	1.74	4

38.79	38.62	16.01	1.86	1.83	1.72	4
36.85	36.69	15.33	1.84	1.82	1.70	4
34.91	34.77	14.65	1.82	1.80	1.68	4
33.00	32.86	13.97	1.80	1.79	1.66	4
31.09	30.97	13.28	1.78	1.77	1.63	4
31.09	30.97	13.28	1.47	1.47	1.39	3
29.70	29.58	12.72	1.46	1.46	1.38	3
28.32	28.20	12.16	1.45	1.45	1.37	3
26.94	26.82	11.59	1.44	1.44	1.36	3
25.57	25.45	11.03	1.43	1.43	1.35	3
24.21	24.09	10.47	1.42	1.42	1.34	3
22.84	22.73	9.90	1.41	1.41	1.33	3
21.49	21.38	9.34	1.40	1.40	1.32	3
20.14	20.03	8.78	1.39	1.39	1.31	3
18.80	18.69	8.21	1.38	1.38	1.30	3
18.80	18.69	8.21	1.34	1.33	1.28	2
16.88	16.78	7.39	1.33	1.32	1.27	2
14.97	14.87	6.57	1.32	1.31	1.26	2
13.07	12.98	5.75	1.31	1.30	1.26	2
11.18	11.09	4.93	1.30	1.29	1.25	2
9.30	9.21	4.11	1.29	1.28	1.24	2
7.43	7.35	3.29	1.28	1.27	1.23	2
5.56	5.49	2.46	1.27	1.25	1.23	2
3.70	3.65	1.64	1.26	1.24	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.03	1043.96	335.36	708.60	551.60	157.00	6
58.54	1079.23	326.58	752.65	582.25	170.40	6
58.04	1114.62	317.91	796.71	613.02	183.69	6
57.55	1150.14	309.47	840.66	643.91	196.75	6
57.05	1185.77	301.38	884.39	674.93	209.46	6
56.55	1221.51	293.74	927.78	706.05	221.72	6
56.05	1257.36	286.65	970.71	737.28	233.43	6
55.55	1293.31	280.22	1013.09	768.60	244.49	6
55.05	1329.34	274.51	1054.82	800.02	254.81	6
55.05	1329.34	274.51	1054.82	800.02	254.81	5
53.91	1425.92	293.20	1132.72	870.85	261.88	5
52.79	1521.81	312.94	1208.87	940.99	267.89	5
51.68	1616.98	333.77	1283.20	1010.40	272.80	5
50.58	1711.37	355.72	1355.65	1079.05	276.61	5
49.49	1804.96	378.78	1426.18	1146.89	279.29	5
48.41	1897.70	402.95	1494.76	1213.88	280.88	5
48.41	1897.70	402.95	1494.76	1213.88	280.88	4
46.44	2096.75	465.30	1631.46	1337.07	294.39	4
44.47	2295.35	520.39	1774.96	1459.81	315.15	4
42.51	2493.45	564.33	1929.12	1582.05	347.07	4
40.56	2691.00	611.15	2079.85	1703.74	376.11	4
38.62	2887.98	661.11	2226.87	1824.86	402.01	4
36.69	3084.34	714.58	2369.76	1945.36	424.40	4
34.77	3280.04	772.08	2507.96	2065.20	442.76	4
32.86	3475.02	834.43	2640.59	2184.32	456.27	4
30.97	3669.22	903.03	2766.20	2302.67	463.53	4
30.97	3669.22	903.03	2766.20	2302.67	463.53	3
29.58	3817.64	958.07	2859.56	2389.22	470.34	3
28.20	3965.69	1018.58	2947.10	2475.41	471.69	3
26.82	4113.36	1085.58	3027.78	2561.23	466.55	3
25.45	4260.66	1151.36	3109.31	2646.67	462.63	3
24.09	4407.60	1215.88	3191.72	2731.75	459.97	3

22.73	4554.17	1279.18	3275.00	2816.47	458.53	3
21.38	4700.40	1341.33	3359.07	2900.83	458.24	3
20.03	4846.27	1402.46	3443.82	2984.85	458.97	3
18.69	4991.81	1462.77	3529.04	3068.53	460.51	3
18.69	4991.81	1462.77	3529.04	3068.53	460.51	2
16.78	5197.29	1545.83	3651.46	3187.91	463.55	2
14.87	5402.26	1631.95	3770.31	3306.78	463.53	2
12.98	5606.68	1722.29	3884.39	3425.10	459.29	2
11.09	5810.53	1818.41	3992.11	3542.85	449.26	2
9.21	6013.76	1922.50	4091.26	3659.99	431.27	2
7.35	6216.33	2053.95	4162.38	3776.45	385.92	2
5.49	6418.17	2233.82	4184.35	3892.20	292.15	2
3.65	6619.27	2417.31	4201.96	4007.20	194.76	2
1.82	6819.61	2601.97	4217.64	4121.45	96.19	2
.00	7019.20	2784.26	4234.94	4234.94	.00	2

Time = 1440. Degree of Consolidation = 39.%

Total Settlement = 1.556

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 1440. = 1.556

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.84	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.39	2.32	.98	.90	.90	1
2.30	2.19	1.16	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
8.84	.00	.00	.00	.00	.00	1
6.60	263.11	123.09	140.02	140.02	.00	1
4.39	523.92	246.18	277.74	277.74	.00	1
2.19	784.08	350.00	434.08	414.81	19.27	1
.00	1043.96	350.00	693.96	551.60	142.36	1

Time = 1440. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 1440. = .350

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 5.88

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.79	21.42	6.50	5.47	5.01	6
60.02	58.30	21.35	6.49	5.48	5.00	6
59.45	57.81	21.27	6.47	5.50	4.99	6
58.89	57.32	21.20	6.46	5.51	4.98	6
58.33	56.83	21.12	6.44	5.53	4.97	6
57.76	56.33	21.05	6.43	5.54	4.97	6
57.20	55.84	20.97	6.42	5.55	4.96	6
56.64	55.34	20.90	6.40	5.56	4.95	6
56.08	54.85	20.82	6.39	5.57	4.95	6
56.08	54.85	20.82	4.51	3.83	3.33	5
54.82	53.73	20.59	4.44	3.78	3.30	5
53.56	52.63	20.36	4.38	3.73	3.27	5
52.32	51.54	20.12	4.32	3.67	3.24	5
51.10	50.46	19.89	4.25	3.62	3.21	5
49.88	49.40	19.66	4.19	3.56	3.18	5
48.69	48.35	19.43	4.13	3.50	3.15	5
48.69	48.35	19.43	1.93	1.89	1.83	4
46.69	46.38	18.75	1.92	1.88	1.81	4
44.70	44.42	18.06	1.91	1.87	1.79	4
42.72	42.47	17.38	1.89	1.85	1.76	4
40.75	40.52	16.70	1.88	1.84	1.74	4
38.79	38.58	16.01	1.86	1.83	1.72	4
36.85	36.66	15.33	1.84	1.81	1.70	4
34.91	34.74	14.65	1.82	1.80	1.68	4
33.00	32.83	13.97	1.80	1.78	1.66	4
31.09	30.94	13.28	1.78	1.76	1.63	4
31.09	30.94	13.28	1.47	1.46	1.39	3
29.70	29.56	12.72	1.46	1.45	1.38	3
28.32	28.18	12.16	1.45	1.44	1.37	3
26.94	26.80	11.59	1.44	1.43	1.36	3
25.57	25.43	11.03	1.43	1.42	1.35	3
24.21	24.07	10.47	1.42	1.41	1.34	3
22.84	22.72	9.90	1.41	1.40	1.33	3
21.49	21.37	9.34	1.40	1.39	1.32	3
20.14	20.02	8.78	1.39	1.38	1.31	3
18.80	18.68	8.21	1.38	1.37	1.30	3
18.80	18.68	8.21	1.34	1.33	1.28	2
16.88	16.77	7.39	1.33	1.32	1.27	2
14.97	14.86	6.57	1.32	1.31	1.26	2
13.07	12.97	5.75	1.31	1.30	1.26	2
11.18	11.08	4.93	1.30	1.29	1.25	2
9.30	9.21	4.11	1.29	1.28	1.24	2
7.43	7.34	3.29	1.28	1.26	1.23	2
5.56	5.49	2.46	1.27	1.25	1.23	2
3.70	3.65	1.64	1.26	1.24	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
58.79	1043.96	342.35	701.61	551.60	150.01	6
58.30	1079.11	336.56	742.54	582.13	160.42	6
57.81	1114.34	331.19	783.15	612.73	170.41	6
57.32	1149.64	326.23	823.41	643.41	179.99	6
56.83	1185.00	321.71	863.29	674.16	189.13	6
56.33	1220.43	317.68	902.75	704.97	197.78	6
55.84	1255.92	314.17	941.74	735.83	205.91	6
55.34	1291.44	311.23	980.22	766.74	213.47	6
54.85	1327.01	308.89	1018.12	797.69	220.44	6
54.85	1327.01	308.89	1018.12	797.69	220.44	5
53.73	1422.32	329.75	1092.57	867.24	225.33	5
52.63	1516.86	351.28	1165.59	936.04	229.54	5
51.54	1610.63	373.49	1237.14	1004.05	233.09	5
50.46	1703.58	396.36	1307.22	1071.26	235.96	5
49.40	1795.70	419.88	1375.82	1137.63	238.20	5
48.35	1886.97	443.98	1442.98	1203.14	239.84	5
48.35	1886.97	443.99	1442.98	1203.14	239.84	4
46.38	2085.73	505.70	1580.02	1326.04	253.98	4
44.42	2284.01	546.67	1737.34	1448.47	288.87	4
42.47	2481.80	589.79	1892.01	1570.40	321.61	4
40.52	2679.06	635.45	2043.61	1691.80	351.81	4
38.58	2875.75	684.04	2191.71	1812.63	379.08	4
36.66	3071.84	736.03	2335.82	1932.87	402.95	4
34.74	3267.30	792.06	2475.24	2052.46	422.78	4
32.83	3462.05	853.08	2608.97	2171.35	437.62	4
30.94	3656.04	920.66	2735.38	2289.48	445.89	4
30.94	3656.04	920.66	2735.38	2289.48	445.89	3
29.56	3804.34	974.68	2829.66	2375.93	453.73	3
28.18	3952.29	1035.64	2916.65	2462.02	454.63	3
26.80	4099.88	1100.49	2999.39	2547.74	451.64	3
25.43	4247.10	1164.57	3082.53	2633.11	449.42	3
24.07	4393.96	1227.84	3166.12	2718.11	448.01	3
22.72	4540.47	1290.32	3250.16	2802.77	447.39	3
21.37	4686.64	1352.07	3334.57	2887.07	447.50	3
20.02	4832.45	1413.20	3419.25	2971.03	448.22	3
18.68	4977.93	1473.85	3504.08	3054.64	449.43	3
18.68	4977.93	1473.85	3504.08	3054.64	449.43	2
16.77	5183.34	1557.59	3625.76	3173.96	451.80	2
14.86	5388.23	1644.94	3743.29	3292.75	450.55	2
12.97	5592.56	1736.94	3855.62	3410.99	444.64	2
11.08	5796.32	1834.92	3961.40	3528.64	432.76	2
9.21	5999.45	1940.60	4058.85	3645.67	413.18	2
7.34	6201.90	2081.04	4120.85	3762.03	358.83	2
5.49	6403.64	2257.28	4146.35	3877.67	268.69	2
3.65	6604.65	2434.64	4170.01	3992.58	177.43	2
1.82	6804.94	2611.13	4193.81	4106.77	87.04	2
.00	7004.51	2784.26	4220.25	4220.25	.00	2

Time = 1825. Degree of Consolidation = 45.%

Total Settlement = 1.792

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 1825. = 1.792

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.84	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.39	2.32	.98	.90	.90	1
2.30	2.19	1.16	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
8.84	.00	.00	.00	.00	.00	1
6.60	263.11	123.09	140.02	140.02	.00	1
4.39	523.92	246.18	277.74	277.74	.00	1
2.19	784.08	350.00	434.08	414.81	19.27	1
.00	1043.96	350.00	693.96	551.60	142.36	1

Time = 1825. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 1825. = .350

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 5.65

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.46	21.42	6.50	5.37	5.01	6
60.02	57.98	21.35	6.49	5.38	5.00	6
59.45	57.49	21.27	6.47	5.39	4.99	6
58.89	57.01	21.20	6.46	5.40	4.98	6
58.33	56.53	21.12	6.44	5.41	4.97	6
57.76	56.04	21.05	6.43	5.42	4.97	6
57.20	55.56	20.97	6.42	5.42	4.96	6
56.64	55.07	20.90	6.40	5.42	4.95	6
56.08	54.59	20.82	6.39	5.43	4.95	6
56.08	54.59	20.82	4.51	3.72	3.33	5
54.82	53.50	20.59	4.44	3.67	3.30	5
53.56	52.42	20.36	4.38	3.61	3.27	5
52.32	51.36	20.12	4.32	3.56	3.24	5
51.10	50.31	19.89	4.25	3.50	3.21	5
49.88	49.27	19.66	4.19	3.45	3.18	5
48.69	48.25	19.43	4.13	3.39	3.15	5

48.69	48.25	19.43	1.93	1.88	1.83	4
46.69	46.28	18.75	1.92	1.87	1.81	4
44.70	44.33	18.06	1.91	1.86	1.79	4
42.72	42.38	17.38	1.89	1.85	1.76	4
40.75	40.44	16.70	1.88	1.83	1.74	4
38.79	38.51	16.01	1.86	1.82	1.72	4
36.85	36.59	15.33	1.84	1.80	1.70	4
34.91	34.68	14.65	1.82	1.79	1.68	4
33.00	32.78	13.97	1.80	1.77	1.66	4
31.09	30.90	13.28	1.78	1.75	1.63	4
31.09	30.90	13.28	1.47	1.46	1.39	3
29.70	29.52	12.72	1.46	1.45	1.38	3
28.32	28.14	12.16	1.45	1.44	1.37	3
26.94	26.77	11.59	1.44	1.43	1.36	3
25.57	25.40	11.03	1.43	1.42	1.35	3
24.21	24.04	10.47	1.42	1.41	1.34	3
22.84	22.69	9.90	1.41	1.40	1.33	3
21.49	21.34	9.34	1.40	1.39	1.32	3
20.14	20.00	8.78	1.39	1.38	1.31	3
18.80	18.66	8.21	1.38	1.37	1.30	3
18.80	18.66	8.21	1.34	1.33	1.28	2
16.88	16.75	7.39	1.33	1.32	1.27	2
14.97	14.85	6.57	1.32	1.31	1.26	2
13.07	12.96	5.75	1.31	1.30	1.26	2
11.18	11.07	4.93	1.30	1.29	1.25	2
9.30	9.20	4.11	1.29	1.27	1.24	2
7.43	7.34	3.29	1.28	1.26	1.23	2
5.56	5.49	2.46	1.27	1.25	1.23	2
3.70	3.65	1.64	1.26	1.23	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.46	1043.96	372.73	671.22	551.60	119.63	6
57.98	1078.66	369.33	709.32	581.67	127.65	6
57.49	1113.40	366.26	747.14	611.80	135.34	6
57.01	1148.18	363.51	784.67	641.96	142.71	6
56.53	1183.01	361.11	821.90	672.16	149.73	6
56.04	1217.86	359.07	858.79	702.40	156.40	6
55.56	1252.74	357.40	895.34	732.66	162.68	6
55.07	1287.64	356.12	931.52	762.94	168.58	6
54.59	1322.56	355.25	967.31	793.23	174.08	6
54.59	1322.56	355.25	967.31	793.23	174.08	5
53.50	1416.18	376.99	1039.20	861.11	178.09	5
52.42	1509.03	398.92	1110.11	928.20	181.90	5
51.36	1601.08	421.03	1180.05	994.51	185.54	5
50.31	1692.34	443.30	1249.04	1060.01	189.02	5
49.27	1782.79	465.69	1317.10	1124.72	192.38	5
48.25	1872.45	488.17	1384.28	1188.62	195.66	5
48.25	1872.45	488.17	1384.28	1188.62	195.66	4
46.28	2070.87	535.48	1535.40	1311.19	224.21	4
44.33	2268.79	578.98	1689.81	1433.25	256.56	4
42.38	2466.18	623.79	1842.39	1554.78	287.61	4
40.44	2663.02	670.33	1992.69	1675.76	316.93	4
38.51	2859.30	719.14	2140.16	1796.18	343.98	4
36.59	3054.98	770.87	2284.11	1916.00	368.11	4
34.68	3250.01	826.39	2423.63	2035.18	388.45	4
32.78	3444.36	886.97	2557.39	2153.66	403.72	4
30.90	3637.94	954.77	2683.17	2271.39	411.78	4
30.90	3637.94	954.77	2683.17	2271.39	411.78	3

29.52	3786.03	1008.87	2777.16	2357.62	419.54	3
28.14	3933.78	1070.84	2862.94	2443.50	419.43	3
26.77	4081.17	1132.58	2948.59	2529.04	419.55	3
25.40	4228.22	1194.07	3034.16	2614.23	419.93	3
24.04	4374.93	1255.26	3119.66	2699.08	420.58	3
22.69	4521.29	1316.20	3205.09	2783.58	421.51	3
21.34	4667.31	1376.95	3290.36	2867.74	422.62	3
20.00	4812.99	1437.55	3375.44	2951.56	423.87	3
18.66	4958.33	1498.11	3460.21	3035.04	425.17	3
18.66	4958.33	1498.11	3460.21	3035.04	425.17	2
16.75	5163.59	1581.67	3581.92	3154.21	427.71	2
14.85	5368.33	1669.59	3698.74	3272.85	425.89	2
12.96	5572.51	1762.54	3809.97	3390.93	419.04	2
11.07	5776.10	1861.45	3914.66	3508.43	406.23	2
9.20	5979.07	1967.54	4011.53	3625.29	386.23	2
7.34	6181.36	2118.81	4062.55	3741.48	321.06	2
5.49	6382.96	2288.23	4094.72	3856.98	237.74	2
3.65	6583.86	2456.62	4127.24	3971.79	155.45	2
1.82	6784.08	2622.49	4161.59	4085.91	75.68	2
.00	6983.63	2784.26	4199.37	4199.36	.00	2

Time = 2520. Degree of Consolidation = 53.%

Total Settlement = 2.126

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 2520. = 2.126

Settlement caused by Secondary Compression at time 2520. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
9.19	8.84	4.64
6.89	6.60	3.48
4.59	4.39	2.32
2.30	2.19	1.16
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
8.84	.00	.00
6.60	263.11	123.09
4.39	523.92	246.18
2.19	784.08	350.00
.00	1043.96	350.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
140.02	140.02	.00	1
277.74	277.74	.00	1
434.08	414.81	19.27	1
693.96	551.60	142.36	1

Time = 2520. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 2520. = .350

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 5.31

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.33	21.42	6.50	5.34	5.01	6
60.02	57.85	21.35	6.49	5.35	5.00	6
59.45	57.37	21.27	6.47	5.35	4.99	6
58.89	56.89	21.20	6.46	5.36	4.98	6
58.33	56.41	21.12	6.44	5.36	4.97	6
57.76	55.93	21.05	6.43	5.37	4.97	6
57.20	55.44	20.97	6.42	5.37	4.96	6
56.64	54.96	20.90	6.40	5.37	4.95	6
56.08	54.48	20.82	6.39	5.38	4.95	6
56.08	54.48	20.82	4.51	3.68	3.33	5
54.82	53.40	20.59	4.44	3.62	3.30	5
53.56	52.34	20.36	4.38	3.57	3.27	5
52.32	51.28	20.12	4.32	3.51	3.24	5
51.10	50.24	19.89	4.25	3.46	3.21	5
49.88	49.22	19.66	4.19	3.41	3.18	5
48.69	48.20	19.43	4.13	3.36	3.15	5
48.69	48.20	19.43	1.93	1.88	1.83	4
46.69	46.24	18.75	1.92	1.87	1.81	4
44.70	44.28	18.06	1.91	1.85	1.79	4
42.72	42.34	17.38	1.89	1.84	1.76	4
40.75	40.40	16.70	1.88	1.83	1.74	4
38.79	38.48	16.01	1.86	1.81	1.72	4
36.85	36.56	15.33	1.84	1.80	1.70	4
34.91	34.65	14.65	1.82	1.78	1.68	4
33.00	32.76	13.97	1.80	1.77	1.66	4
31.09	30.87	13.28	1.78	1.75	1.63	4
31.09	30.87	13.28	1.47	1.45	1.39	3
29.70	29.49	12.72	1.46	1.45	1.38	3
28.32	28.12	12.16	1.45	1.44	1.37	3
26.94	26.75	11.59	1.44	1.43	1.36	3
25.57	25.39	11.03	1.43	1.42	1.35	3
24.21	24.03	10.47	1.42	1.41	1.34	3
22.84	22.68	9.90	1.41	1.40	1.33	3
21.49	21.33	9.34	1.40	1.39	1.32	3
20.14	19.99	8.78	1.39	1.38	1.31	3
18.80	18.65	8.21	1.38	1.37	1.30	3
18.80	18.65	8.21	1.34	1.33	1.28	2
16.88	16.74	7.39	1.33	1.32	1.27	2
14.97	14.84	6.57	1.32	1.31	1.26	2
13.07	12.95	5.75	1.31	1.30	1.26	2
11.18	11.07	4.93	1.30	1.29	1.25	2
9.30	9.20	4.11	1.29	1.27	1.24	2
7.43	7.34	3.29	1.28	1.26	1.23	2
5.56	5.49	2.46	1.27	1.25	1.23	2
3.70	3.65	1.64	1.26	1.23	1.22	2

1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.33	1043.96	384.47	659.49	551.60	107.89	6
57.85	1078.48	382.00	696.48	581.50	114.99	6
57.37	1113.04	379.78	733.26	611.44	121.82	6
56.89	1147.63	377.82	769.81	641.40	128.41	6
56.41	1182.24	376.12	806.12	671.40	134.72	6
55.93	1216.87	374.71	842.17	701.41	140.76	6
55.44	1251.53	373.57	877.95	731.44	146.51	6
54.96	1286.19	372.73	913.47	761.49	151.98	6
54.48	1320.87	372.17	948.71	791.55	157.16	6
54.48	1320.87	372.17	948.71	791.55	157.16	5
53.40	1413.89	394.08	1019.81	858.81	160.99	5
52.34	1506.12	415.92	1090.20	925.30	164.91	5
51.28	1597.57	437.62	1159.95	991.00	168.95	5
50.24	1688.24	459.12	1229.13	1055.92	173.21	5
49.22	1778.15	480.31	1297.84	1120.08	177.76	5
48.20	1867.31	502.44	1364.87	1183.48	181.38	5
48.20	1867.31	502.44	1364.87	1183.48	181.38	4
46.24	2065.61	546.66	1518.96	1305.93	213.02	4
44.28	2263.39	591.44	1671.95	1427.85	244.10	4
42.34	2460.62	637.30	1823.32	1549.22	274.10	4
40.40	2657.30	684.74	1972.56	1670.04	302.52	4
38.48	2853.40	734.34	2119.06	1790.28	328.78	4
36.56	3048.89	786.80	2262.09	1909.91	352.18	4
34.65	3243.73	843.14	2400.60	2028.90	371.70	4
32.76	3437.87	904.84	2533.03	2147.18	385.85	4
30.87	3631.24	974.43	2656.80	2264.68	392.12	4
30.87	3631.24	974.43	2656.80	2264.68	392.12	3
29.49	3779.20	1030.19	2749.02	2350.79	398.23	3
28.12	3926.83	1090.50	2836.33	2436.56	399.77	3
26.75	4074.12	1150.81	2923.31	2521.99	401.32	3
25.39	4221.07	1211.07	3010.00	2607.08	402.92	3
24.03	4367.68	1271.28	3096.40	2691.83	404.57	3
22.68	4513.96	1331.42	3182.54	2776.25	406.29	3
21.33	4659.89	1391.58	3268.32	2860.33	407.99	3
19.99	4805.49	1451.77	3353.72	2944.07	409.66	3
18.65	4950.75	1512.08	3438.67	3027.47	411.21	3
18.65	4950.75	1512.08	3438.67	3027.47	411.21	2
16.74	5155.93	1595.09	3560.84	3146.55	414.29	2
14.84	5360.59	1682.68	3677.91	3265.11	412.80	2
12.95	5564.69	1775.39	3789.30	3383.11	406.19	2
11.07	5768.20	1873.94	3894.26	3500.53	393.73	2
9.20	5971.09	1979.52	3991.57	3617.32	374.25	2
7.34	6173.31	2134.86	4038.45	3733.44	305.01	2
5.49	6374.85	2300.93	4073.92	3848.88	225.04	2
3.65	6575.71	2465.40	4110.31	3963.64	146.67	2
1.82	6775.90	2627.00	4148.90	4077.74	71.17	2
.00	6975.44	2784.26	4191.18	4191.18	.00	2

Time = 2880. Degree of Consolidation = 57.%

Total Settlement = 2.258

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 2880. = 2.258

Settlement caused by Secondary Compression at time 2880. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.84	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.39	2.32	.98	.90	.90	1
2.30	2.19	1.16	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
8.84	.00	.00	.00	.00	.00	1
6.60	263.11	123.09	140.02	140.02	.00	1
4.39	523.92	246.18	277.74	277.74	.00	1
2.19	784.08	350.00	434.08	414.81	19.27	1
.00	1043.96	350.00	693.96	551.60	142.36	1

Time = 2880. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 2880. = .350

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 5.18

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.25	21.42	6.50	5.32	5.01	6
60.02	57.77	21.35	6.49	5.32	5.00	6
59.45	57.29	21.27	6.47	5.33	4.99	6
58.89	56.81	21.20	6.46	5.33	4.98	6
58.33	56.33	21.12	6.44	5.34	4.97	6
57.76	55.86	21.05	6.43	5.34	4.97	6
57.20	55.38	20.97	6.42	5.34	4.96	6
56.64	54.90	20.90	6.40	5.35	4.95	6
56.08	54.42	20.82	6.39	5.35	4.95	6
56.08	54.42	20.82	4.51	3.66	3.33	5
54.82	53.34	20.59	4.44	3.60	3.30	5

53.56	52.28	20.36	4.38	3.55	3.27	5
52.32	51.23	20.12	4.32	3.50	3.24	5
51.10	50.20	19.89	4.25	3.45	3.21	5
49.88	49.17	19.66	4.19	3.40	3.18	5
48.69	48.16	19.43	4.13	3.35	3.15	5
48.69	48.16	19.43	1.93	1.88	1.83	4
46.69	46.19	18.75	1.92	1.87	1.81	4
44.70	44.24	18.06	1.91	1.85	1.79	4
42.72	42.30	17.38	1.89	1.84	1.76	4
40.75	40.36	16.70	1.88	1.82	1.74	4
38.79	38.44	16.01	1.86	1.81	1.72	4
36.85	36.53	15.33	1.84	1.80	1.70	4
34.91	34.62	14.65	1.82	1.78	1.68	4
33.00	32.73	13.97	1.80	1.76	1.66	4
31.09	30.85	13.28	1.78	1.74	1.63	4
31.09	30.85	13.28	1.47	1.45	1.39	3
29.70	29.47	12.72	1.46	1.44	1.38	3
28.32	28.10	12.16	1.45	1.43	1.37	3
26.94	26.73	11.59	1.44	1.42	1.36	3
25.57	25.37	11.03	1.43	1.41	1.35	3
24.21	24.01	10.47	1.42	1.40	1.34	3
22.84	22.66	9.90	1.41	1.39	1.33	3
21.49	21.32	9.34	1.40	1.38	1.32	3
20.14	19.98	8.78	1.39	1.38	1.31	3
18.80	18.64	8.21	1.38	1.37	1.30	3
18.80	18.64	8.21	1.34	1.33	1.28	2
16.88	16.73	7.39	1.33	1.32	1.27	2
14.97	14.83	6.57	1.32	1.31	1.26	2
13.07	12.94	5.75	1.31	1.30	1.26	2
11.18	11.06	4.93	1.30	1.28	1.25	2
9.30	9.19	4.11	1.29	1.27	1.24	2
7.43	7.33	3.29	1.28	1.26	1.23	2
5.56	5.48	2.46	1.27	1.25	1.23	2
3.70	3.65	1.64	1.26	1.23	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.25	1043.96	391.98	651.98	551.59	100.38	6
57.77	1078.37	390.10	688.27	581.39	106.88	6
57.29	1112.81	388.34	724.47	611.21	113.26	6
56.81	1147.27	386.69	760.58	641.05	119.53	6
56.33	1181.76	385.17	796.58	670.91	125.67	6
55.86	1216.26	383.77	832.49	700.80	131.69	6
55.38	1250.79	382.49	868.29	730.70	137.59	6
54.90	1285.33	381.33	904.00	760.63	143.37	6
54.42	1319.89	380.28	939.61	790.56	149.05	6
54.42	1319.89	380.28	939.61	790.56	149.05	5
53.34	1412.62	401.79	1010.83	857.55	153.28	5
52.28	1504.59	422.89	1081.69	923.76	157.93	5
51.23	1595.80	443.56	1152.24	989.23	163.01	5
50.20	1686.29	463.77	1222.52	1053.96	168.56	5
49.17	1776.06	483.48	1292.58	1117.98	174.60	5
48.16	1865.12	505.93	1359.19	1181.30	177.89	5
48.16	1865.12	505.93	1359.19	1181.30	177.89	4
46.19	2063.37	553.03	1510.34	1303.69	206.65	4
44.24	2261.05	600.23	1660.82	1425.51	235.31	4
42.30	2458.17	648.04	1810.13	1546.77	263.36	4
40.36	2654.71	697.05	1957.66	1667.45	290.21	4
38.44	2850.66	747.96	2102.69	1787.54	315.16	4

36.53	3045.98	801.63	2244.35	1907.00	337.35	4
34.62	3240.64	859.18	2381.46	2025.80	355.66	4
32.73	3434.58	922.35	2512.23	2143.88	368.35	4
30.85	3627.72	994.00	2633.72	2261.16	372.55	4
30.85	3627.72	994.00	2633.72	2261.16	372.55	3
29.47	3775.56	1051.72	2723.84	2347.15	376.69	3
28.10	3923.07	1110.64	2812.44	2432.80	379.64	3
26.73	4070.25	1169.69	2900.56	2518.12	382.44	3
25.37	4217.10	1228.84	2988.26	2603.11	385.15	3
24.01	4363.62	1288.10	3075.52	2687.77	387.75	3
22.66	4509.80	1347.45	3162.34	2772.09	390.25	3
21.32	4655.65	1406.95	3248.70	2856.08	392.62	3
19.98	4801.16	1466.65	3334.51	2939.73	394.78	3
18.64	4946.33	1526.58	3419.75	3023.05	396.70	3
18.64	4946.33	1526.58	3419.75	3023.05	396.70	2
16.73	5151.43	1608.86	3542.57	3142.05	400.52	2
14.83	5356.00	1695.82	3660.18	3260.52	399.66	2
12.94	5560.02	1787.94	3772.08	3378.45	393.64	2
11.06	5763.46	1885.93	3877.54	3495.79	381.75	2
9.19	5966.28	1990.74	3975.54	3612.51	363.04	2
7.33	6168.43	2149.43	4019.00	3728.56	290.44	2
5.48	6369.92	2312.31	4057.61	3843.95	213.66	2
3.65	6570.74	2473.11	4097.63	3958.67	138.96	2
1.82	6770.91	2630.82	4140.09	4072.74	67.34	2
.00	6970.44	2784.26	4186.18	4186.18	.00	2

Time = 3240. Degree of Consolidation = 59.%

Total Settlement = 2.338

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 3240. = 2.338

Settlement caused by Secondary Compression at time 3240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
9.19	8.84	4.64
6.89	6.60	3.48
4.59	4.39	2.32
2.30	2.19	1.16
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
8.84	.00	.00
6.60	263.11	123.09
4.39	523.92	246.18
2.19	784.08	350.00
.00	1043.96	350.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
140.02	140.02	.00	1
277.74	277.74	.00	1
434.08	414.81	19.27	1
693.96	551.59	142.36	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 3240. = .350

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 5.10

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.19	21.42	6.50	5.31	5.01	6
60.02	57.71	21.35	6.49	5.31	5.00	6
59.45	57.23	21.27	6.47	5.32	4.99	6
58.89	56.75	21.20	6.46	5.32	4.98	6
58.33	56.28	21.12	6.44	5.32	4.97	6
57.76	55.80	21.05	6.43	5.33	4.97	6
57.20	55.32	20.97	6.42	5.33	4.96	6
56.64	54.84	20.90	6.40	5.34	4.95	6
56.08	54.36	20.82	6.39	5.34	4.95	6
56.08	54.36	20.82	4.51	3.65	3.33	5
54.82	53.29	20.59	4.44	3.60	3.30	5
53.56	52.23	20.36	4.38	3.54	3.27	5
52.32	51.18	20.12	4.32	3.49	3.24	5
51.10	50.15	19.89	4.25	3.45	3.21	5
49.88	49.12	19.66	4.19	3.40	3.18	5
48.69	48.11	19.43	4.13	3.35	3.15	5
48.69	48.11	19.43	1.93	1.88	1.83	4
46.69	46.15	18.75	1.92	1.86	1.81	4
44.70	44.20	18.06	1.91	1.85	1.79	4
42.72	42.25	17.38	1.89	1.84	1.76	4
40.75	40.32	16.70	1.88	1.82	1.74	4
38.79	38.40	16.01	1.86	1.81	1.72	4
36.85	36.49	15.33	1.84	1.79	1.70	4
34.91	34.59	14.65	1.82	1.77	1.68	4
33.00	32.70	13.97	1.80	1.76	1.66	4
31.09	30.82	13.28	1.78	1.74	1.63	4
31.09	30.82	13.28	1.47	1.45	1.39	3
29.70	29.45	12.72	1.46	1.44	1.38	3
28.32	28.08	12.16	1.45	1.43	1.37	3
26.94	26.71	11.59	1.44	1.42	1.36	3
25.57	25.35	11.03	1.43	1.41	1.35	3
24.21	24.00	10.47	1.42	1.40	1.34	3
22.84	22.65	9.90	1.41	1.39	1.33	3
21.49	21.30	9.34	1.40	1.38	1.32	3
20.14	19.96	8.78	1.39	1.37	1.31	3
18.80	18.63	8.21	1.38	1.36	1.30	3
18.80	18.63	8.21	1.34	1.32	1.28	2
16.88	16.72	7.39	1.33	1.32	1.27	2
14.97	14.83	6.57	1.32	1.30	1.26	2
13.07	12.94	5.75	1.31	1.29	1.26	2

11.18	11.06	4.93	1.30	1.28	1.25	2
9.30	9.19	4.11	1.29	1.27	1.24	2
7.43	7.33	3.29	1.28	1.26	1.23	2
5.56	5.48	2.46	1.27	1.24	1.23	2
3.70	3.65	1.64	1.26	1.23	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.19	1043.96	395.29	648.66	551.59	97.07	6
57.71	1078.32	393.68	684.64	581.34	103.30	6
57.23	1112.70	392.10	720.60	611.10	109.50	6
56.75	1147.11	390.57	756.54	640.89	115.65	6
56.28	1181.54	389.09	792.46	670.70	121.76	6
55.80	1215.99	387.64	828.35	700.53	127.82	6
55.32	1250.46	386.25	864.22	730.38	133.84	6
54.84	1284.95	384.89	900.06	760.25	139.81	6
54.36	1319.46	383.58	935.89	790.14	145.75	6
54.36	1319.46	383.58	935.89	790.14	145.75	5
53.29	1412.08	404.88	1007.20	857.01	150.20	5
52.23	1503.94	425.66	1078.29	923.12	155.17	5
51.18	1595.07	445.91	1149.16	988.49	160.67	5
50.15	1685.48	465.61	1219.86	1053.15	166.71	5
49.12	1775.19	484.77	1290.42	1117.11	173.30	5
48.11	1864.22	507.51	1356.71	1180.40	176.31	5
48.11	1864.22	507.51	1356.71	1180.40	176.31	4
46.15	2062.43	557.16	1505.27	1302.75	202.52	4
44.20	2260.05	606.81	1653.24	1424.51	228.73	4
42.25	2457.08	656.91	1800.17	1545.68	254.49	4
40.32	2653.50	708.05	1945.45	1666.24	279.21	4
38.40	2849.30	760.94	2088.36	1786.18	302.18	4
36.49	3044.45	816.48	2227.98	1905.48	322.50	4
34.59	3238.93	875.95	2362.97	2024.09	338.89	4
32.70	3432.65	941.28	2491.37	2141.96	349.42	4
30.82	3625.56	1014.34	2611.21	2259.00	352.21	4
30.82	3625.56	1014.34	2611.21	2259.00	352.21	3
29.45	3773.28	1073.47	2699.81	2344.86	354.95	3
28.08	3920.67	1132.19	2788.47	2430.39	358.08	3
26.71	4067.73	1190.69	2877.04	2515.60	361.44	3
25.35	4214.46	1249.12	2965.34	2600.47	364.87	3
24.00	4360.86	1307.61	3053.26	2685.01	368.24	3
22.65	4506.94	1366.21	3140.73	2769.23	371.50	3
21.30	4652.68	1425.01	3227.67	2853.12	374.55	3
19.96	4798.09	1484.10	3314.00	2936.67	377.33	3
18.63	4943.17	1543.54	3399.64	3019.89	379.74	3
18.63	4943.17	1543.54	3399.64	3019.89	379.75	2
16.72	5148.17	1624.81	3523.36	3138.78	384.58	2
14.83	5352.65	1710.82	3641.83	3257.17	384.66	2
12.94	5556.58	1802.04	3754.54	3375.00	379.54	2
11.06	5759.93	1899.16	3860.78	3492.26	368.52	2
9.19	5962.67	2004.15	3958.52	3608.90	349.63	2
7.33	6164.76	2164.79	3999.97	3724.89	275.08	2
5.48	6366.19	2324.15	4042.04	3840.22	201.83	2
3.65	6566.97	2481.18	4085.79	3954.90	130.89	2
1.82	6767.11	2634.95	4132.16	4068.95	63.22	2
.00	6966.63	2784.26	4182.37	4182.37	.00	2

Time = 3650. Degree of Consolidation = 60.%

Total Settlement = 2.399

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 3650. = 2.399

Settlement caused by Secondary Compression at time 3650. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.84	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.39	2.32	.98	.90	.90	1
2.30	2.19	1.16	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
8.84	.00	.00	.00	.00	.00	1
6.60	263.11	123.09	140.02	140.02	.00	1
4.39	523.92	246.18	277.74	277.74	.00	1
2.19	784.08	350.00	434.08	414.81	19.27	1
.00	1043.95	350.00	693.95	551.59	142.36	1

Time = 3650. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 3650. = .350

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 5.04

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.11	21.42	6.50	5.30	5.01	6
60.02	57.64	21.35	6.49	5.31	5.00	6
59.45	57.16	21.27	6.47	5.31	4.99	6
58.89	56.68	21.20	6.46	5.32	4.98	6
58.33	56.21	21.12	6.44	5.32	4.97	6
57.76	55.73	21.05	6.43	5.32	4.97	6

57.20	55.25	20.97	6.42	5.33	4.96	6
56.64	54.77	20.90	6.40	5.33	4.95	6
56.08	54.29	20.82	6.39	5.34	4.95	6
56.08	54.29	20.82	4.51	3.64	3.33	5
54.82	53.22	20.59	4.44	3.59	3.30	5
53.56	52.16	20.36	4.38	3.54	3.27	5
52.32	51.12	20.12	4.32	3.49	3.24	5
51.10	50.08	19.89	4.25	3.44	3.21	5
49.88	49.06	19.66	4.19	3.40	3.18	5
48.69	48.04	19.43	4.13	3.35	3.15	5
48.69	48.04	19.43	1.93	1.88	1.83	4
46.69	46.08	18.75	1.92	1.86	1.81	4
44.70	44.13	18.06	1.91	1.85	1.79	4
42.72	42.19	17.38	1.89	1.83	1.76	4
40.75	40.26	16.70	1.88	1.82	1.74	4
38.79	38.34	16.01	1.86	1.80	1.72	4
36.85	36.44	15.33	1.84	1.79	1.70	4
34.91	34.54	14.65	1.82	1.77	1.68	4
33.00	32.65	13.97	1.80	1.75	1.66	4
31.09	30.78	13.28	1.78	1.73	1.63	4
31.09	30.78	13.28	1.47	1.44	1.39	3
29.70	29.41	12.72	1.46	1.43	1.38	3
28.32	28.04	12.16	1.45	1.42	1.37	3
26.94	26.68	11.59	1.44	1.41	1.36	3
25.57	25.32	11.03	1.43	1.41	1.35	3
24.21	23.97	10.47	1.42	1.40	1.34	3
22.84	22.62	9.90	1.41	1.39	1.33	3
21.49	21.28	9.34	1.40	1.38	1.32	3
20.14	19.94	8.78	1.39	1.37	1.31	3
18.80	18.61	8.21	1.38	1.36	1.30	3
18.80	18.61	8.21	1.34	1.32	1.28	2
16.88	16.71	7.39	1.33	1.31	1.27	2
14.97	14.82	6.57	1.32	1.30	1.26	2
13.07	12.93	5.75	1.31	1.29	1.26	2
11.18	11.05	4.93	1.30	1.28	1.25	2
9.30	9.19	4.11	1.29	1.27	1.24	2
7.43	7.33	3.29	1.28	1.25	1.23	2
5.56	5.48	2.46	1.27	1.24	1.23	2
3.70	3.64	1.64	1.26	1.23	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.11	1043.95	396.77	647.18	551.59	95.59	6
57.64	1078.30	395.27	683.02	581.31	101.71	6
57.16	1112.66	393.78	718.88	611.06	107.82	6
56.68	1147.04	392.31	754.74	640.82	113.92	6
56.21	1181.45	390.84	790.60	670.60	120.00	6
55.73	1215.87	389.39	826.48	700.41	126.07	6
55.25	1250.32	387.95	862.36	730.24	132.13	6
54.77	1284.79	386.53	898.25	760.08	138.17	6
54.29	1319.27	385.12	934.15	789.95	144.20	6
54.29	1319.27	385.12	934.15	789.95	144.20	5
53.22	1411.83	406.33	1005.50	856.76	148.74	5
52.16	1503.65	426.98	1076.67	922.82	153.84	5
51.12	1594.73	447.06	1147.67	988.15	159.52	5
50.08	1685.10	466.56	1218.54	1052.77	165.76	5
49.06	1774.78	485.49	1289.29	1116.71	172.58	5
48.04	1863.79	508.59	1355.20	1179.97	175.24	5
48.04	1863.79	508.59	1355.20	1179.97	175.24	4

46.08	2061.97	561.36	1500.61	1302.29	198.32	4
44.13	2259.52	614.14	1645.38	1423.98	221.40	4
42.19	2456.44	667.38	1789.06	1545.04	244.02	4
40.26	2652.72	721.62	1931.10	1665.46	265.64	4
38.34	2848.34	777.54	2070.80	1785.22	285.58	4
36.44	3043.28	836.11	2207.17	1904.30	302.87	4
34.54	3237.50	898.65	2338.84	2022.66	316.18	4
32.65	3430.93	967.33	2463.61	2140.24	323.37	4
30.78	3623.51	1041.53	2581.98	2256.95	325.03	4
30.78	3623.51	1041.53	2581.98	2256.95	325.03	3
29.41	3771.08	1101.78	2669.29	2342.66	326.63	3
28.04	3918.30	1161.23	2757.07	2428.03	329.04	3
26.68	4065.20	1220.12	2845.08	2513.07	332.01	3
25.32	4211.77	1278.59	2933.17	2597.78	335.40	3
23.97	4358.01	1336.86	3021.15	2682.16	338.99	3
22.62	4503.92	1395.06	3108.85	2766.21	342.65	3
21.28	4649.50	1453.34	3196.16	2849.93	346.23	3
19.94	4794.75	1511.78	3282.98	2933.33	349.65	3
18.61	4939.68	1570.52	3369.16	3016.40	352.76	3
18.61	4939.68	1570.52	3369.16	3016.40	352.76	2
16.71	5144.51	1650.35	3494.17	3135.13	359.04	2
14.82	5348.84	1734.95	3613.89	3253.36	360.54	2
12.93	5552.63	1824.66	3727.96	3371.05	356.92	2
11.05	5755.85	1920.07	3835.78	3488.17	347.61	2
9.19	5958.46	2032.04	3926.43	3604.69	321.74	2
7.33	6160.45	2187.58	3972.86	3720.57	252.29	2
5.48	6361.79	2341.50	4020.29	3835.82	184.47	2
3.64	6562.52	2492.79	4069.73	3950.45	119.28	2
1.82	6762.62	2640.64	4121.98	4064.46	57.53	2
.00	6962.13	2784.26	4177.87	4177.87	.00	2

Time = 4321. Degree of Consolidation = 62.%

Total Settlement = 2.471

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 4321. = 2.471

Settlement caused by Secondary Compression at time 4321. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
9.19	8.84	4.64
6.89	6.60	3.48
4.59	4.39	2.32
2.30	2.19	1.16
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
8.84	.00	.00
6.60	263.11	123.09

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
140.02	140.02	.00	1

4.39	523.92	246.18	277.74	277.74	.00	1
2.19	784.08	350.00	434.08	414.81	19.27	1
.00	1043.95	350.00	693.95	551.59	142.36	1

Time = 4321. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 4321. = .350

Settlement caused by Secondary Compression at time 4321. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.97

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.05	21.42	6.50	5.30	5.01	6
60.02	57.58	21.35	6.49	5.31	5.00	6
59.45	57.10	21.27	6.47	5.31	4.99	6
58.89	56.62	21.20	6.46	5.31	4.98	6
58.33	56.15	21.12	6.44	5.32	4.97	6
57.76	55.67	21.05	6.43	5.32	4.97	6
57.20	55.19	20.97	6.42	5.33	4.96	6
56.64	54.71	20.90	6.40	5.33	4.95	6
56.08	54.23	20.82	6.39	5.34	4.95	6
56.08	54.23	20.82	4.51	3.64	3.33	5
54.82	53.16	20.59	4.44	3.59	3.30	5
53.56	52.10	20.36	4.38	3.54	3.27	5
52.32	51.06	20.12	4.32	3.49	3.24	5
51.10	50.02	19.89	4.25	3.44	3.21	5
49.88	49.00	19.66	4.19	3.40	3.18	5
48.69	47.98	19.43	4.13	3.35	3.15	5
48.69	47.98	19.43	1.93	1.88	1.83	4
46.69	46.02	18.75	1.92	1.86	1.81	4
44.70	44.08	18.06	1.91	1.85	1.79	4
42.72	42.14	17.38	1.89	1.83	1.76	4
40.75	40.21	16.70	1.88	1.81	1.74	4
38.79	38.29	16.01	1.86	1.80	1.72	4
36.85	36.39	15.33	1.84	1.78	1.70	4
34.91	34.49	14.65	1.82	1.76	1.68	4
33.00	32.61	13.97	1.80	1.74	1.66	4
31.09	30.75	13.28	1.78	1.72	1.63	4
31.09	30.75	13.28	1.47	1.44	1.39	3
29.70	29.37	12.72	1.46	1.43	1.38	3
28.32	28.01	12.16	1.45	1.42	1.37	3
26.94	26.65	11.59	1.44	1.41	1.36	3
25.57	25.29	11.03	1.43	1.40	1.35	3
24.21	23.94	10.47	1.42	1.39	1.34	3
22.84	22.60	9.90	1.41	1.38	1.33	3
21.49	21.26	9.34	1.40	1.37	1.32	3
20.14	19.93	8.78	1.39	1.36	1.31	3

18.80	18.60	8.21	1.38	1.35	1.30	3
18.80	18.60	8.21	1.34	1.32	1.28	2
16.88	16.70	7.39	1.33	1.31	1.27	2
14.97	14.80	6.57	1.32	1.30	1.26	2
13.07	12.92	5.75	1.31	1.29	1.26	2
11.18	11.05	4.93	1.30	1.28	1.25	2
9.30	9.18	4.11	1.29	1.27	1.24	2
7.43	7.33	3.29	1.28	1.25	1.23	2
5.56	5.48	2.46	1.27	1.24	1.23	2
3.70	3.64	1.64	1.26	1.23	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.05	1043.95	397.13	646.82	551.59	95.23	6
57.58	1078.29	395.66	682.63	581.31	101.32	6
57.10	1112.65	394.19	718.45	611.04	107.41	6
56.62	1147.02	392.74	754.29	640.80	113.49	6
56.15	1181.42	391.29	790.14	670.58	119.56	6
55.67	1215.84	389.84	826.00	700.38	125.62	6
55.19	1250.28	388.41	861.87	730.20	131.68	6
54.71	1284.74	386.98	897.76	760.04	137.72	6
54.23	1319.22	385.56	933.66	789.90	143.77	6
54.23	1319.22	385.56	933.66	789.90	143.77	5
53.16	1411.77	406.76	1005.01	856.69	148.32	5
52.10	1503.56	427.38	1076.18	922.74	153.44	5
51.06	1594.63	447.43	1147.20	988.06	159.14	5
50.02	1684.99	466.90	1218.09	1052.67	165.42	5
49.00	1774.66	485.79	1288.87	1116.59	172.28	5
47.98	1863.66	509.16	1354.50	1179.84	174.66	5
47.98	1863.66	509.16	1354.50	1179.84	174.66	4
46.02	2061.82	564.33	1497.49	1302.14	195.35	4
44.08	2259.32	619.58	1639.74	1423.78	215.96	4
42.14	2456.16	675.35	1780.81	1544.76	236.05	4
40.21	2652.33	732.17	1920.16	1665.07	255.09	4
38.29	2847.81	790.73	2057.07	1784.69	272.39	4
36.39	3042.57	852.02	2190.55	1903.59	286.96	4
34.49	3236.58	917.46	2319.12	2021.75	297.38	4
32.61	3429.78	989.47	2440.31	2139.08	301.23	4
30.75	3622.07	1065.09	2556.99	2255.52	301.47	4
30.75	3622.07	1065.09	2556.99	2255.52	301.47	3
29.37	3769.50	1126.72	2642.78	2341.09	301.69	3
28.01	3916.59	1187.22	2729.36	2426.31	303.05	3
26.65	4063.34	1246.88	2816.46	2511.20	305.26	3
25.29	4209.75	1305.89	2903.86	2595.76	308.10	3
23.94	4355.83	1364.43	2991.40	2679.98	311.42	3
22.60	4501.59	1422.69	3078.90	2763.88	315.02	3
21.26	4647.02	1480.83	3166.18	2847.45	318.73	3
19.93	4792.12	1539.01	3253.11	2930.69	322.42	3
18.60	4936.89	1597.33	3339.56	3013.61	325.96	3
18.60	4936.89	1597.33	3339.56	3013.61	325.96	2
16.70	5141.56	1676.27	3465.29	3132.18	333.12	2
14.80	5345.73	1759.58	3586.15	3250.25	335.90	2
12.92	5549.37	1847.75	3701.62	3367.79	333.83	2
11.05	5752.46	1941.40	3811.06	3484.78	326.28	2
9.18	5954.95	2059.95	3895.00	3601.17	293.82	2
7.33	6156.83	2209.90	3946.93	3716.96	229.97	2
5.48	6358.10	2358.15	3999.95	3832.13	167.82	2
3.64	6558.76	2503.85	4054.92	3946.69	108.22	2
1.82	6758.84	2646.15	4112.68	4060.67	52.02	2

.00	6958.33	2784.26	4174.07	4174.07	.00	2

Time = 5040. Degree of Consolidation = 64.%

Total Settlement = 2.532

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 5040. = 2.532

Settlement caused by Secondary Compression at time 5040. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.84	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.39	2.32	.98	.90	.90	1
2.30	2.19	1.16	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
8.84	.00	.00	.00	.00	.00	1
6.60	263.11	123.09	140.02	140.02	.00	1
4.39	523.92	246.18	277.74	277.74	.00	1
2.19	784.08	350.00	434.08	414.81	19.27	1
.00	1043.95	350.00	693.95	551.59	142.36	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 5040. = .350

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.91

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.02	21.42	6.50	5.30	5.01	6

60.02	57.54	21.35	6.49	5.30	5.00	6
59.45	57.07	21.27	6.47	5.31	4.99	6
58.89	56.59	21.20	6.46	5.31	4.98	6
58.33	56.11	21.12	6.44	5.32	4.97	6
57.76	55.64	21.05	6.43	5.32	4.97	6
57.20	55.16	20.97	6.42	5.33	4.96	6
56.64	54.68	20.90	6.40	5.33	4.95	6
56.08	54.20	20.82	6.39	5.34	4.95	6
56.08	54.20	20.82	4.51	3.64	3.33	5
54.82	53.13	20.59	4.44	3.59	3.30	5
53.56	52.07	20.36	4.38	3.54	3.27	5
52.32	51.03	20.12	4.32	3.49	3.24	5
51.10	49.99	19.89	4.25	3.44	3.21	5
49.88	48.97	19.66	4.19	3.39	3.18	5
48.69	47.95	19.43	4.13	3.35	3.15	5
48.69	47.95	19.43	1.93	1.88	1.83	4
46.69	45.99	18.75	1.92	1.86	1.81	4
44.70	44.04	18.06	1.91	1.85	1.79	4
42.72	42.11	17.38	1.89	1.83	1.76	4
40.75	40.18	16.70	1.88	1.81	1.74	4
38.79	38.26	16.01	1.86	1.80	1.72	4
36.85	36.36	15.33	1.84	1.78	1.70	4
34.91	34.47	14.65	1.82	1.76	1.68	4
33.00	32.59	13.97	1.80	1.74	1.66	4
31.09	30.73	13.28	1.78	1.72	1.63	4
31.09	30.73	13.28	1.47	1.44	1.39	3
29.70	29.35	12.72	1.46	1.43	1.38	3
28.32	27.99	12.16	1.45	1.42	1.37	3
26.94	26.63	11.59	1.44	1.41	1.36	3
25.57	25.28	11.03	1.43	1.40	1.35	3
24.21	23.93	10.47	1.42	1.39	1.34	3
22.84	22.59	9.90	1.41	1.38	1.33	3
21.49	21.25	9.34	1.40	1.37	1.32	3
20.14	19.92	8.78	1.39	1.36	1.31	3
18.80	18.59	8.21	1.38	1.35	1.30	3
18.80	18.59	8.21	1.34	1.32	1.28	2
16.88	16.69	7.39	1.33	1.31	1.27	2
14.97	14.80	6.57	1.32	1.30	1.26	2
13.07	12.92	5.75	1.31	1.29	1.26	2
11.18	11.04	4.93	1.30	1.28	1.25	2
9.30	9.18	4.11	1.29	1.26	1.24	2
7.43	7.32	3.29	1.28	1.25	1.23	2
5.56	5.48	2.46	1.27	1.24	1.23	2
3.70	3.64	1.64	1.26	1.23	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.02	1043.95	397.24	646.71	551.59	95.12	6
57.54	1078.28	395.77	682.51	581.30	101.21	6
57.07	1112.64	394.31	718.33	611.04	107.29	6
56.59	1147.02	392.85	754.16	640.79	113.37	6
56.11	1181.41	391.41	790.01	670.57	119.44	6
55.64	1215.83	389.96	825.87	700.37	125.50	6
55.16	1250.27	388.53	861.74	730.19	131.56	6
54.68	1284.73	387.10	897.63	760.02	137.60	6
54.20	1319.21	385.68	933.53	789.88	143.65	6
54.20	1319.21	385.68	933.53	789.88	143.65	5
53.13	1411.75	406.88	1004.87	856.68	148.19	5
52.07	1503.54	427.51	1076.03	922.72	153.31	5

51.03	1594.60	447.56	1147.05	988.03	159.02	5
49.99	1684.96	467.02	1217.93	1052.63	165.30	5
48.97	1774.62	485.91	1288.71	1116.55	172.16	5
47.95	1863.62	509.41	1354.21	1179.80	174.41	5
47.95	1863.62	509.41	1354.21	1179.80	174.41	4
45.99	2061.77	565.70	1496.07	1302.09	193.99	4
44.04	2259.25	622.13	1637.12	1423.71	213.41	4
42.11	2456.05	679.13	1776.92	1544.65	232.27	4
40.18	2652.16	737.23	1914.94	1664.90	250.03	4
38.26	2847.57	797.12	2050.46	1784.45	266.00	4
36.36	3042.25	859.80	2182.46	1903.27	279.18	4
34.47	3236.16	926.81	2309.35	2021.33	288.02	4
32.59	3429.23	1000.66	2428.58	2138.54	290.04	4
30.73	3621.39	1077.16	2544.23	2254.83	289.39	4
30.73	3621.39	1077.16	2544.23	2254.83	289.39	3
29.35	3768.75	1139.67	2629.08	2340.33	288.75	3
27.99	3915.76	1200.89	2714.87	2425.49	289.38	3
26.63	4062.43	1261.09	2801.33	2510.30	291.04	3
25.28	4208.76	1320.50	2888.26	2594.77	293.49	3
23.93	4354.76	1379.33	2975.43	2678.91	296.52	3
22.59	4500.43	1437.73	3062.71	2762.72	299.98	3
21.25	4645.78	1495.90	3149.87	2846.21	303.66	3
19.92	4790.79	1554.01	3236.78	2929.37	307.42	3
18.59	4935.48	1612.17	3323.31	3012.20	311.11	3
18.59	4935.48	1612.17	3323.31	3012.20	311.11	2
16.69	5140.06	1690.77	3449.29	3130.68	318.62	2
14.80	5344.14	1773.53	3570.62	3248.66	321.95	2
12.92	5547.70	1860.94	3686.76	3366.12	320.64	2
11.04	5750.71	1953.61	3797.10	3483.03	314.07	2
9.18	5953.13	2075.87	3877.26	3599.36	277.90	2
7.32	6154.95	2222.79	3932.16	3715.08	217.08	2
5.48	6356.17	2367.93	3988.24	3830.20	158.04	2
3.64	6556.80	2510.44	4046.36	3944.73	101.63	2
1.82	6756.86	2649.48	4107.38	4058.69	48.69	2
.00	6956.35	2784.26	4172.09	4172.08	.00	2

Time = 5475. Degree of Consolidation = 64.%

Total Settlement = 2.564

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 5475. = 2.564

Settlement caused by Secondary Compression at time 5475. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
9.19	8.84	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.39	2.32	.98	.90	.90	1
2.30	2.19	1.16	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
8.84	.00	.00	.00	.00	.00	1
6.60	263.11	123.09	140.02	140.02	.00	1
4.39	523.92	246.18	277.74	277.74	.00	1
2.19	784.08	350.00	434.08	414.81	19.27	1
.00	1043.95	350.00	693.95	551.59	142.36	1

Time = 5475. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 5475. = .350

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.88

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	57.96	21.42	6.50	5.30	5.01	6
60.02	57.48	21.35	6.49	5.30	5.00	6
59.45	57.00	21.27	6.47	5.31	4.99	6
58.89	56.53	21.20	6.46	5.31	4.98	6
58.33	56.05	21.12	6.44	5.32	4.97	6
57.76	55.57	21.05	6.43	5.32	4.97	6
57.20	55.10	20.97	6.42	5.33	4.96	6
56.64	54.62	20.90	6.40	5.33	4.95	6
56.08	54.14	20.82	6.39	5.33	4.95	6
56.08	54.14	20.82	4.51	3.64	3.33	5
54.82	53.07	20.59	4.44	3.59	3.30	5
53.56	52.01	20.36	4.38	3.54	3.27	5
52.32	50.96	20.12	4.32	3.49	3.24	5
51.10	49.93	19.89	4.25	3.44	3.21	5
49.88	48.90	19.66	4.19	3.39	3.18	5
48.69	47.89	19.43	4.13	3.35	3.15	5
48.69	47.89	19.43	1.93	1.88	1.83	4
46.69	45.93	18.75	1.92	1.86	1.81	4
44.70	43.98	18.06	1.91	1.84	1.79	4
42.72	42.05	17.38	1.89	1.83	1.76	4
40.75	40.12	16.70	1.88	1.81	1.74	4
38.79	38.21	16.01	1.86	1.79	1.72	4
36.85	36.30	15.33	1.84	1.77	1.70	4
34.91	34.42	14.65	1.82	1.76	1.68	4
33.00	32.54	13.97	1.80	1.73	1.66	4
31.09	30.68	13.28	1.78	1.71	1.63	4
31.09	30.68	13.28	1.47	1.43	1.39	3
29.70	29.31	12.72	1.46	1.42	1.38	3
28.32	27.95	12.16	1.45	1.41	1.37	3
26.94	26.60	11.59	1.44	1.40	1.36	3

25.57	25.24	11.03	1.43	1.39	1.35	3
24.21	23.90	10.47	1.42	1.38	1.34	3
22.84	22.56	9.90	1.41	1.38	1.33	3
21.49	21.22	9.34	1.40	1.37	1.32	3
20.14	19.89	8.78	1.39	1.36	1.31	3
18.80	18.57	8.21	1.38	1.35	1.30	3
18.80	18.57	8.21	1.34	1.31	1.28	2
16.88	16.67	7.39	1.33	1.30	1.27	2
14.97	14.79	6.57	1.32	1.29	1.26	2
13.07	12.91	5.75	1.31	1.28	1.26	2
11.18	11.03	4.93	1.30	1.27	1.25	2
9.30	9.17	4.11	1.29	1.26	1.24	2
7.43	7.32	3.29	1.28	1.25	1.23	2
5.56	5.48	2.46	1.27	1.24	1.23	2
3.70	3.64	1.64	1.26	1.23	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
57.96	1043.95	397.40	646.55	551.59	94.96	6
57.48	1078.28	395.94	682.34	581.30	101.04	6
57.00	1112.63	394.49	718.14	611.03	107.11	6
56.53	1147.01	393.04	753.96	640.78	113.18	6
56.05	1181.40	391.60	789.80	670.56	119.24	6
55.57	1215.82	390.17	825.65	700.35	125.29	6
55.10	1250.25	388.74	861.51	730.17	131.35	6
54.62	1284.71	387.31	897.39	760.00	137.39	6
54.14	1319.18	385.89	933.29	789.86	143.43	6
54.14	1319.18	385.89	933.29	789.86	143.43	5
53.07	1411.72	407.09	1004.62	856.64	147.98	5
52.01	1503.50	427.72	1075.78	922.68	153.11	5
50.96	1594.56	447.76	1146.79	987.98	158.81	5
49.93	1684.90	467.23	1217.68	1052.58	165.10	5
48.90	1774.56	486.11	1288.45	1116.49	171.97	5
47.89	1863.55	509.84	1353.71	1179.73	173.98	5
47.89	1863.55	509.84	1353.71	1179.73	173.98	4
45.93	2061.68	568.21	1493.48	1302.00	191.48	4
43.98	2259.12	626.85	1632.26	1423.58	208.69	4
42.05	2455.85	686.19	1769.66	1544.45	225.21	4
40.12	2651.86	746.78	1905.09	1664.60	240.48	4
38.21	2847.15	809.39	2037.76	1784.03	253.73	4
36.30	3041.66	875.16	2166.50	1902.68	263.82	4
34.42	3235.37	945.88	2289.49	2020.53	268.96	4
32.54	3428.19	1022.29	2405.90	2137.49	268.41	4
30.68	3620.06	1100.64	2519.42	2253.51	265.91	4
30.68	3620.06	1100.64	2519.42	2253.51	265.91	3
29.31	3767.28	1164.92	2602.37	2338.87	263.50	3
27.95	3914.15	1227.66	2686.49	2423.88	262.62	3
26.60	4060.66	1289.14	2771.52	2508.53	262.99	3
25.24	4206.84	1349.57	2857.26	2592.85	264.42	3
23.90	4352.67	1409.15	2943.52	2676.82	266.70	3
22.56	4498.17	1468.09	3030.09	2760.46	269.62	3
21.22	4643.34	1526.54	3116.80	2843.78	273.03	3
19.89	4788.19	1584.70	3203.49	2926.76	276.73	3
18.57	4932.71	1642.72	3289.99	3009.42	280.57	3
18.57	4932.71	1642.72	3289.99	3009.42	280.57	2
16.67	5137.10	1720.90	3416.19	3127.72	288.48	2
14.79	5341.00	1802.73	3538.27	3245.52	292.75	2
12.91	5544.38	1888.68	3655.70	3362.80	292.90	2
11.03	5747.22	1979.41	3767.81	3479.55	288.26	2

9.17	5949.49	2109.71	3839.78	3595.72	244.06	2
7.32	6151.19	2249.97	3901.22	3711.32	189.90	2
5.48	6352.31	2388.24	3964.08	3826.34	137.73	2
3.64	6552.88	2523.77	4029.10	3940.81	88.30	2
1.82	6752.89	2656.04	4096.85	4054.72	42.13	2
.00	6952.37	2784.26	4168.10	4168.10	.00	2

Time = 6480. Degree of Consolidation = 66.%

Total Settlement = 2.627

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 6480. = 2.627

Settlement caused by Secondary Compression at time 6480. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.84	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1
4.59	4.39	2.32	.98	.90	.90	1
2.30	2.19	1.16	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
8.84	.00	.00	.00	.00	.00	1
6.60	263.11	123.09	140.02	140.02	.00	1
4.39	523.92	246.18	277.74	277.74	.00	1
2.19	784.08	350.00	434.08	414.81	19.27	1
.00	1043.95	350.00	693.95	551.59	142.36	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 6480. = .350

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.81

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	57.91	21.42	6.50	5.30	5.01	6
60.02	57.44	21.35	6.49	5.30	5.00	6
59.45	56.96	21.27	6.47	5.31	4.99	6
58.89	56.48	21.20	6.46	5.31	4.98	6
58.33	56.01	21.12	6.44	5.32	4.97	6
57.76	55.53	21.05	6.43	5.32	4.97	6
57.20	55.05	20.97	6.42	5.33	4.96	6
56.64	54.57	20.90	6.40	5.33	4.95	6
56.08	54.09	20.82	6.39	5.33	4.95	6
56.08	54.09	20.82	4.51	3.64	3.33	5
54.82	53.02	20.59	4.44	3.59	3.30	5
53.56	51.97	20.36	4.38	3.54	3.27	5
52.32	50.92	20.12	4.32	3.49	3.24	5
51.10	49.88	19.89	4.25	3.44	3.21	5
49.88	48.86	19.66	4.19	3.39	3.18	5
48.69	47.85	19.43	4.13	3.35	3.15	5
48.69	47.85	19.43	1.93	1.88	1.83	4
46.69	45.89	18.75	1.92	1.86	1.81	4
44.70	43.94	18.06	1.91	1.84	1.79	4
42.72	42.00	17.38	1.89	1.83	1.76	4
40.75	40.08	16.70	1.88	1.81	1.74	4
38.79	38.17	16.01	1.86	1.79	1.72	4
36.85	36.27	15.33	1.84	1.77	1.70	4
34.91	34.38	14.65	1.82	1.75	1.68	4
33.00	32.51	13.97	1.80	1.73	1.66	4
31.09	30.65	13.28	1.78	1.71	1.63	4
31.09	30.65	13.28	1.47	1.43	1.39	3
29.70	29.29	12.72	1.46	1.42	1.38	3
28.32	27.93	12.16	1.45	1.41	1.37	3
26.94	26.57	11.59	1.44	1.40	1.36	3
25.57	25.22	11.03	1.43	1.39	1.35	3
24.21	23.88	10.47	1.42	1.38	1.34	3
22.84	22.54	9.90	1.41	1.37	1.33	3
21.49	21.21	9.34	1.40	1.36	1.32	3
20.14	19.88	8.78	1.39	1.35	1.31	3
18.80	18.55	8.21	1.38	1.34	1.30	3
18.80	18.55	8.21	1.34	1.31	1.28	2
16.88	16.66	7.39	1.33	1.30	1.27	2
14.97	14.78	6.57	1.32	1.29	1.26	2
13.07	12.90	5.75	1.31	1.28	1.26	2
11.18	11.03	4.93	1.30	1.27	1.25	2
9.30	9.17	4.11	1.29	1.26	1.24	2
7.43	7.32	3.29	1.28	1.25	1.23	2
5.56	5.48	2.46	1.27	1.24	1.23	2
3.70	3.64	1.64	1.26	1.23	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
57.91	1043.95	397.46	646.49	551.59	94.90	6
57.44	1078.28	396.01	682.27	581.30	100.97	6
56.96	1112.63	394.56	718.07	611.03	107.04	6
56.48	1147.00	393.13	753.88	640.78	113.10	6
56.01	1181.40	391.69	789.70	670.55	119.15	6
55.53	1215.81	390.26	825.54	700.35	125.20	6
55.05	1250.24	388.84	861.40	730.16	131.24	6

54.57	1284.70	387.42	897.27	759.99	137.28	6
54.09	1319.17	386.01	933.16	789.85	143.31	6
54.09	1319.17	386.01	933.16	789.85	143.31	5
53.02	1411.70	407.22	1004.48	856.63	147.85	5
51.97	1503.48	427.85	1075.63	922.66	152.97	5
50.92	1594.53	447.90	1146.63	987.96	158.68	5
49.88	1684.87	467.36	1217.51	1052.55	164.96	5
48.86	1774.53	486.24	1288.28	1116.45	171.83	5
47.85	1863.51	510.14	1353.37	1179.69	173.68	5
47.85	1863.51	510.14	1353.37	1179.69	173.68	4
45.89	2061.63	569.88	1491.75	1301.95	189.80	4
43.94	2259.04	629.99	1629.05	1423.50	205.56	4
42.00	2455.72	690.88	1764.84	1544.32	220.52	4
40.08	2651.67	753.18	1898.49	1664.41	234.08	4
38.17	2846.87	817.70	2029.16	1783.75	245.42	4
36.27	3041.27	885.65	2155.61	1902.29	253.32	4
34.38	3234.83	959.01	2275.82	2020.00	255.82	4
32.51	3427.48	1037.25	2390.23	2136.79	253.44	4
30.65	3619.16	1116.85	2502.32	2252.61	249.71	4
30.65	3619.16	1116.85	2502.32	2252.61	249.71	3
29.29	3766.29	1182.30	2583.99	2337.88	246.11	3
27.93	3913.05	1246.08	2666.98	2422.78	244.20	3
26.57	4059.46	1308.42	2751.04	2507.33	243.71	3
25.22	4205.53	1369.58	2835.95	2591.53	244.41	3
23.88	4351.25	1429.74	2921.51	2675.40	246.11	3
22.54	4496.63	1489.10	3007.53	2758.92	248.61	3
21.21	4641.68	1547.82	3093.87	2842.12	251.75	3
19.88	4786.41	1606.10	3180.31	2924.98	255.33	3
18.55	4930.81	1664.09	3266.71	3007.52	259.19	3
18.55	4930.81	1664.09	3266.71	3007.52	259.19	2
16.66	5135.07	1742.19	3392.88	3125.68	267.19	2
14.78	5338.84	1823.53	3515.30	3243.35	271.95	2
12.90	5542.09	1908.62	3633.47	3360.52	272.96	2
11.03	5744.82	1998.01	3746.80	3477.14	269.66	2
9.17	5946.98	2134.10	3812.88	3593.21	219.67	2
7.32	6148.58	2269.68	3878.90	3708.71	170.19	2
5.48	6349.64	2403.18	3946.46	3823.67	122.79	2
3.64	6550.15	2533.75	4016.40	3938.08	78.32	2
1.82	6750.13	2660.93	4089.20	4051.96	37.24	2
.00	6949.60	2784.26	4165.34	4165.33	.00	2

Time = 7300. Degree of Consolidation = 67.%

Total Settlement = 2.672

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 7300. = 2.672

Settlement caused by Secondary Compression at time 7300. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
9.19	8.84	4.64	.98	.98	.98	1
6.89	6.60	3.48	.98	.91	.91	1

4.59	4.39	2.32	.98	.90	1
2.30	2.19	1.16	.98	.89	1
.00	.00	.00	.98	.89	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
8.84	.00	.00	.00	.00	.00	1
6.60	263.11	123.09	140.02	140.02	.00	1
4.39	523.92	246.18	277.74	277.74	.00	1
2.19	784.08	350.00	434.08	414.81	19.27	1
.00	1043.95	350.00	693.95	551.59	142.36	1

Time = 7300. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 7300. = .350

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.77

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	57.83	21.42	6.50	5.30	5.01	6
60.02	57.36	21.35	6.49	5.30	5.00	6
59.45	56.88	21.27	6.47	5.31	4.99	6
58.89	56.40	21.20	6.46	5.31	4.98	6
58.33	55.93	21.12	6.44	5.32	4.97	6
57.76	55.45	21.05	6.43	5.32	4.97	6
57.20	54.97	20.97	6.42	5.33	4.96	6
56.64	54.49	20.90	6.40	5.33	4.95	6
56.08	54.02	20.82	6.39	5.33	4.95	6
56.08	54.02	20.82	4.51	3.64	3.33	5
54.82	52.95	20.59	4.44	3.59	3.30	5
53.56	51.89	20.36	4.38	3.54	3.27	5
52.32	50.84	20.12	4.32	3.49	3.24	5
51.10	49.81	19.89	4.25	3.44	3.21	5
49.88	48.78	19.66	4.19	3.39	3.18	5
48.69	47.77	19.43	4.13	3.35	3.15	5
48.69	47.77	19.43	1.93	1.88	1.83	4
46.69	45.81	18.75	1.92	1.86	1.81	4
44.70	43.86	18.06	1.91	1.84	1.79	4
42.72	41.93	17.38	1.89	1.82	1.76	4
40.75	40.01	16.70	1.88	1.81	1.74	4
38.79	38.10	16.01	1.86	1.79	1.72	4
36.85	36.20	15.33	1.84	1.77	1.70	4
34.91	34.32	14.65	1.82	1.74	1.68	4
33.00	32.45	13.97	1.80	1.72	1.66	4

31.09	30.60	13.28	1.78	1.70	1.63	4
31.09	30.60	13.28	1.47	1.43	1.39	3
29.70	29.23	12.72	1.46	1.42	1.38	3
28.32	27.88	12.16	1.45	1.41	1.37	3
26.94	26.53	11.59	1.44	1.40	1.36	3
25.57	25.18	11.03	1.43	1.39	1.35	3
24.21	23.84	10.47	1.42	1.38	1.34	3
22.84	22.50	9.90	1.41	1.37	1.33	3
21.49	21.17	9.34	1.40	1.36	1.32	3
20.14	19.85	8.78	1.39	1.35	1.31	3
18.80	18.53	8.21	1.38	1.34	1.30	3
18.80	18.53	8.21	1.34	1.31	1.28	2
16.88	16.64	7.39	1.33	1.30	1.27	2
14.97	14.76	6.57	1.32	1.29	1.26	2
13.07	12.88	5.75	1.31	1.28	1.26	2
11.18	11.02	4.93	1.30	1.27	1.25	2
9.30	9.16	4.11	1.29	1.26	1.24	2
7.43	7.31	3.29	1.28	1.25	1.23	2
5.56	5.47	2.46	1.27	1.24	1.23	2
3.70	3.64	1.64	1.26	1.23	1.22	2
1.85	1.82	.82	1.25	1.22	1.21	2
.00	.00	.00	1.25	1.21	1.21	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
57.83	1043.95	397.61	646.34	551.59	94.75	6
57.36	1078.28	396.17	682.11	581.29	100.81	6
56.88	1112.63	394.73	717.89	611.02	106.87	6
56.40	1147.00	393.30	753.69	640.77	112.92	6
55.93	1181.39	391.88	789.51	670.54	118.96	6
55.45	1215.80	390.46	825.34	700.33	125.00	6
54.97	1250.23	389.04	861.18	730.14	131.04	6
54.49	1284.68	387.63	897.04	759.98	137.07	6
54.02	1319.15	386.23	932.92	789.83	143.09	6
54.02	1319.15	386.23	932.92	789.83	143.09	5
52.95	1411.67	407.44	1004.23	856.60	147.63	5
51.89	1503.44	428.07	1075.37	922.62	152.75	5
50.84	1594.49	448.12	1146.37	987.91	158.45	5
49.81	1684.82	467.58	1217.24	1052.50	164.74	5
48.78	1774.47	486.46	1288.00	1116.39	171.61	5
47.77	1863.44	510.63	1352.81	1179.62	173.19	5
47.77	1863.44	510.63	1352.81	1179.62	173.19	4
45.81	2061.54	572.69	1488.86	1301.86	186.99	4
43.86	2258.90	635.27	1623.63	1423.36	200.27	4
41.93	2455.51	698.87	1756.64	1544.11	212.53	4
40.01	2651.34	764.15	1887.19	1664.08	223.11	4
38.10	2846.39	832.01	2014.38	1783.27	231.11	4
36.20	3040.60	903.89	2136.71	1901.62	235.09	4
34.32	3233.92	982.16	2251.75	2019.08	232.67	4
32.45	3426.26	1063.80	2362.46	2135.57	226.90	4
30.60	3617.60	1145.66	2471.94	2251.04	220.90	4
30.60	3617.60	1145.66	2471.94	2251.04	220.89	3
29.23	3764.56	1213.18	2551.37	2336.14	215.23	3
27.88	3911.14	1278.79	2632.35	2420.87	211.48	3
26.53	4057.36	1342.74	2714.62	2505.23	209.39	3
25.18	4203.23	1405.21	2798.01	2589.24	208.78	3
23.84	4348.75	1466.45	2882.29	2672.90	209.39	3
22.50	4493.92	1526.63	2967.29	2756.21	211.08	3
21.17	4638.76	1585.92	3052.84	2839.19	213.65	3
19.85	4783.27	1644.53	3138.74	2921.84	216.89	3
18.53	4927.45	1702.61	3224.84	3004.17	220.67	3

18.53	4927.45	1702.61	3224.84	3004.17	220.67	2
16.64	5131.47	1780.83	3350.64	3122.09	228.55	2
14.76	5335.01	1861.65	3473.36	3239.53	233.83	2
12.88	5538.03	1945.51	3592.53	3356.46	236.07	2
11.02	5740.54	2048.02	3692.52	3472.86	219.66	2
9.16	5942.51	2177.98	3764.53	3588.73	175.80	2
7.31	6143.95	2305.49	3838.45	3704.07	134.38	2
5.47	6344.87	2430.13	3914.74	3818.90	95.84	2
3.64	6545.29	2551.77	3993.52	3933.22	60.30	2
1.82	6745.22	2669.98	4075.24	4047.05	28.19	2
.00	6944.67	2784.26	4160.40	4160.40	.00	2

Time = 9125. Degree of Consolidation = 69.%

Total Settlement = 2.751

Settlement at End of Primary Consolidation = 3.976

Settlement caused by Primary Consolidation at time 9125. = 2.751

Settlement caused by Secondary Compression at time 9125. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
9.19	8.84	4.64
6.89	6.60	3.48
4.59	4.39	2.32
2.30	2.19	1.16
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
8.84	.00	.00
6.60	263.11	123.09
4.39	523.92	246.18
2.19	784.08	350.00
.00	1043.95	350.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
140.02	140.02	.00	1
277.74	277.74	.00	1
434.08	414.81	19.27	1
693.95	551.59	142.36	1

Time = 9125. Degree of Consolidation = 100.%

Total Settlement = .350

Settlement at End of Primary Consolidation = .350

Settlement caused by Primary Consolidation at time 9125. = .350

Settlement caused by Secondary Compression at time 9125. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 4.69

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou Dupont - 6ft fill with Equivalent fill height of 11.4

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	11.4	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.894	.570	.30000E-03	z = .06

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	4.83	6
60.02	60.02	21.35	6.49	6.49	4.82	6
59.45	59.45	21.27	6.47	6.47	4.81	6
58.89	58.89	21.20	6.46	6.46	4.81	6

58.33	58.33	21.12	6.44	6.44	4.80	6
57.76	57.76	21.05	6.43	6.43	4.79	6
57.20	57.20	20.97	6.42	6.42	4.79	6
56.64	56.64	20.90	6.40	6.40	4.78	6
56.08	56.08	20.82	6.39	6.39	4.77	6
56.08	56.08	20.82	4.51	4.51	3.19	5
54.82	54.82	20.59	4.44	4.44	3.16	5
53.56	53.56	20.36	4.38	4.38	3.14	5
52.32	52.32	20.12	4.32	4.32	3.11	5
51.10	51.10	19.89	4.25	4.25	3.08	5
49.88	49.88	19.66	4.19	4.19	3.05	5
48.69	48.69	19.43	4.13	4.13	3.02	5
48.69	48.69	19.43	1.93	1.93	1.80	4
46.69	46.69	18.75	1.92	1.92	1.77	4
44.70	44.70	18.06	1.91	1.91	1.75	4
42.72	42.72	17.38	1.89	1.89	1.73	4
40.75	40.75	16.70	1.88	1.88	1.71	4
38.79	38.79	16.01	1.86	1.86	1.69	4
36.85	36.85	15.33	1.84	1.84	1.67	4
34.91	34.91	14.65	1.82	1.82	1.64	4
33.00	33.00	13.97	1.80	1.80	1.62	4
31.09	31.09	13.28	1.78	1.78	1.60	4
31.09	31.09	13.28	1.47	1.47	1.37	3
29.70	29.70	12.72	1.46	1.46	1.36	3
28.32	28.32	12.16	1.45	1.45	1.35	3
26.94	26.94	11.59	1.44	1.44	1.34	3
25.57	25.57	11.03	1.43	1.43	1.33	3
24.21	24.21	10.47	1.42	1.42	1.32	3
22.84	22.84	9.90	1.41	1.41	1.31	3
21.49	21.49	9.34	1.40	1.40	1.30	3
20.14	20.14	8.78	1.39	1.39	1.29	3
18.80	18.80	8.21	1.38	1.38	1.29	3
18.80	18.80	8.21	1.34	1.34	1.27	2
16.88	16.88	7.39	1.33	1.33	1.26	2
14.97	14.97	6.57	1.32	1.32	1.25	2
13.07	13.07	5.75	1.31	1.31	1.25	2
11.18	11.18	4.93	1.30	1.30	1.24	2
9.30	9.30	4.11	1.29	1.29	1.23	2
7.43	7.43	3.29	1.28	1.28	1.23	2
5.56	5.56	2.46	1.27	1.27	1.22	2
3.70	3.70	1.64	1.26	1.26	1.21	2
1.85	1.85	.82	1.25	1.25	1.20	2
.00	.00	.00	1.25	1.25	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	1317.48	.00	1317.48	708.86	608.62	6
60.02	1357.43	4.62	1352.81	744.19	608.62	6
59.45	1397.31	9.24	1388.07	779.45	608.62	6
58.89	1437.13	13.86	1423.27	814.65	608.62	6
58.33	1476.88	18.48	1458.40	849.78	608.62	6
57.76	1516.56	23.10	1493.46	884.84	608.62	6
57.20	1556.18	27.72	1528.46	919.84	608.62	6
56.64	1595.73	32.34	1563.39	954.77	608.62	6
56.08	1635.22	36.96	1598.26	989.64	608.62	6
56.08	1635.22	36.96	1598.26	989.64	608.62	5
54.82	1740.19	62.71	1677.48	1068.86	608.62	5
53.56	1844.24	88.46	1755.78	1147.16	608.62	5
52.32	1947.37	114.21	1833.16	1224.54	608.62	5
51.10	2049.57	139.96	1909.61	1300.99	608.62	5
49.88	2150.85	165.71	1985.14	1376.52	608.62	5

48.69	2251.20	191.46	2059.74	1451.12	608.62	5
48.69	2251.20	191.46	2059.74	1451.12	608.62	4
46.69	2451.65	267.32	2184.33	1575.70	608.62	4
44.70	2651.59	343.18	2308.41	1699.79	608.62	4
42.72	2850.98	419.04	2431.94	1823.32	608.62	4
40.75	3049.93	494.90	2555.03	1946.41	608.62	4
38.79	3248.12	570.76	2677.37	2068.75	608.62	4
36.85	3445.43	646.62	2798.81	2190.19	608.62	4
34.91	3641.82	722.48	2919.34	2310.72	608.62	4
33.00	3837.31	798.34	3038.98	2430.35	608.62	4
31.09	4031.90	874.19	3157.70	2549.08	608.62	4
31.09	4031.90	874.19	3157.70	2549.08	608.62	3
29.70	4180.47	936.05	3244.41	2635.79	608.62	3
28.32	4328.64	997.91	3330.72	2722.10	608.62	3
26.94	4476.44	1059.77	3416.67	2808.05	608.62	3
25.57	4623.90	1121.63	3502.27	2893.65	608.62	3
24.21	4771.01	1183.49	3587.53	2978.90	608.62	3
22.84	4917.78	1245.35	3672.43	3063.81	608.62	3
21.49	5064.19	1307.21	3756.99	3148.37	608.62	3
20.14	5210.26	1369.06	3841.19	3232.57	608.62	3
18.80	5355.98	1430.92	3925.06	3316.43	608.62	3
18.80	5355.98	1430.92	3925.05	3316.43	608.62	2
16.88	5561.65	1517.02	4044.63	3436.00	608.62	2
14.97	5766.78	1603.12	4163.67	3555.04	608.62	2
13.07	5971.39	1689.22	4282.18	3673.56	608.62	2
11.18	6175.47	1775.31	4400.16	3791.54	608.62	2
9.30	6379.03	1861.41	4517.61	3908.99	608.62	2
7.43	6582.04	1947.51	4634.53	4025.91	608.62	2
5.56	6784.55	2033.61	4750.94	4142.32	608.62	2
3.70	6986.67	2119.71	4866.96	4258.34	608.62	2
1.85	7188.43	2205.80	4982.63	4374.01	608.62	2
.00	7389.85	2291.90	5097.95	4489.32	608.62	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	11.36	5.74	.98	.98	.98	1
8.52	8.52	4.30	.98	.98	.90	1
5.68	5.68	2.87	.98	.98	.89	1
2.84	2.84	1.43	.98	.98	.89	1
.00	.00	.00	.98	.98	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

11.36	.00	.00	.00	.00	.00	1
8.52	329.37	.00	329.37	177.22	152.16	1
5.68	658.74	.00	658.74	354.43	304.31	1
2.84	988.11	.00	988.11	531.65	456.47	1
.00	1317.48	.00	1317.48	708.86	608.62	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.46	21.42	6.50	5.82	4.83	6
60.02	59.93	21.35	6.49	6.03	4.82	6
59.45	59.39	21.27	6.47	6.20	4.81	6
58.89	58.85	21.20	6.46	6.31	4.81	6
58.33	58.29	21.12	6.44	6.37	4.80	6
57.76	57.73	21.05	6.43	6.40	4.79	6
57.20	57.17	20.97	6.42	6.40	4.79	6
56.64	56.61	20.90	6.40	6.40	4.78	6
56.08	56.06	20.82	6.39	6.39	4.77	6
56.08	56.06	20.82	4.51	4.51	3.19	5
54.82	54.79	20.59	4.44	4.44	3.16	5
53.56	53.53	20.36	4.38	4.38	3.14	5
52.32	52.29	20.12	4.32	4.31	3.11	5
51.10	51.07	19.89	4.25	4.25	3.08	5
49.88	49.86	19.66	4.19	4.19	3.05	5
48.69	48.66	19.43	4.13	4.12	3.02	5
48.69	48.66	19.43	1.93	1.93	1.80	4
46.69	46.67	18.75	1.92	1.92	1.77	4
44.70	44.68	18.06	1.91	1.91	1.75	4
42.72	42.70	17.38	1.89	1.89	1.73	4
40.75	40.73	16.70	1.88	1.88	1.71	4
38.79	38.77	16.01	1.86	1.86	1.69	4
36.85	36.82	15.33	1.84	1.84	1.67	4
34.91	34.89	14.65	1.82	1.82	1.64	4
33.00	32.97	13.97	1.80	1.80	1.62	4
31.09	31.07	13.28	1.78	1.78	1.60	4
31.09	31.07	13.28	1.47	1.47	1.37	3
29.70	29.68	12.72	1.46	1.46	1.36	3
28.32	28.30	12.16	1.45	1.45	1.35	3
26.94	26.92	11.59	1.44	1.44	1.34	3
25.57	25.55	11.03	1.43	1.43	1.33	3
24.21	24.18	10.47	1.42	1.42	1.32	3
22.84	22.82	9.90	1.41	1.41	1.31	3
21.49	21.47	9.34	1.40	1.40	1.30	3
20.14	20.12	8.78	1.39	1.39	1.29	3
18.80	18.77	8.21	1.38	1.38	1.29	3
18.80	18.77	8.21	1.34	1.34	1.27	2

16.88	16.86	7.39	1.33	1.33	1.26	2
14.97	14.95	6.57	1.32	1.32	1.25	2
13.07	13.05	5.75	1.31	1.31	1.25	2
11.18	11.16	4.93	1.30	1.30	1.24	2
9.30	9.28	4.11	1.29	1.29	1.23	2
7.43	7.40	3.29	1.28	1.28	1.23	2
5.56	5.54	2.46	1.27	1.27	1.22	2
3.70	3.68	1.64	1.26	1.26	1.21	2
1.85	1.83	.82	1.25	1.25	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.46	1290.59	224.43	1066.16	681.97	384.19	6
59.93	1327.88	154.87	1173.01	714.64	458.37	6
59.39	1366.07	100.12	1265.95	748.20	517.74	6
58.85	1404.91	62.87	1342.03	782.43	559.61	6
58.29	1444.16	41.97	1402.18	817.06	585.13	6
57.73	1483.62	33.15	1450.46	851.89	598.57	6
57.17	1523.14	31.67	1491.47	886.80	604.68	6
56.61	1562.66	33.97	1528.69	921.69	606.99	6
56.06	1602.12	38.04	1564.08	956.54	607.54	6
56.06	1602.12	38.04	1564.08	956.54	607.54	5
54.79	1707.06	63.57	1643.50	1035.73	607.76	5
53.53	1811.08	89.33	1721.75	1114.00	607.75	5
52.29	1914.18	115.12	1799.06	1191.34	607.71	5
51.07	2016.35	140.89	1875.46	1267.76	607.69	5
49.86	2117.59	166.61	1950.98	1343.26	607.72	5
48.66	2217.91	192.25	2025.66	1417.83	607.83	5
48.66	2217.91	192.25	2025.66	1417.83	607.83	4
46.67	2418.35	267.32	2151.03	1542.41	608.62	4
44.68	2618.28	343.18	2275.10	1666.48	608.62	4
42.70	2817.68	421.79	2395.89	1790.02	605.87	4
40.73	3016.52	507.87	2508.65	1913.00	595.65	4
38.77	3214.64	573.63	2641.00	2035.26	605.75	4
36.82	3411.93	646.64	2765.28	2156.69	608.60	4
34.89	3608.32	722.48	2885.84	2277.22	608.62	4
32.97	3803.81	798.34	3005.48	2396.85	608.62	4
31.07	3998.40	874.19	3124.20	2515.58	608.62	4
31.07	3998.40	874.19	3124.20	2515.58	608.62	3
29.68	4146.97	936.05	3210.91	2602.29	608.62	3
28.30	4295.14	997.91	3297.23	2688.61	608.62	3
26.92	4442.94	1061.00	3381.94	2774.55	607.39	3
25.55	4590.39	1123.20	3467.19	2860.14	607.05	3
24.18	4737.49	1185.05	3552.45	2945.39	607.06	3
22.82	4884.25	1246.82	3637.43	3030.28	607.15	3
21.47	5030.66	1308.58	3722.08	3114.83	607.25	3
20.12	5176.72	1370.28	3806.44	3199.03	607.41	3
18.77	5322.43	1431.77	3890.66	3282.89	607.77	3
18.77	5322.43	1431.77	3890.66	3282.89	607.77	2
16.86	5528.09	1517.21	4010.88	3402.45	608.43	2
14.95	5733.23	1603.20	4130.04	3521.49	608.54	2
13.05	5937.84	1689.25	4248.59	3640.00	608.59	2
11.16	6141.92	1775.31	4366.60	3757.98	608.62	2
9.28	6345.48	1861.41	4484.06	3875.44	608.62	2
7.40	6548.49	1947.51	4600.98	3992.36	608.62	2
5.54	6751.04	2033.61	4717.43	4108.81	608.62	2
3.68	6953.11	2127.49	4825.61	4224.78	600.84	2
1.83	7154.76	2295.89	4858.87	4340.33	518.54	2
.00	7354.95	2900.52	4454.43	4454.42	.00	2

Time = 30. Degree of Consolidation = 3.%

Total Settlement = .128

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 30. = .128

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
11.36	10.93	5.74	.98	.98	.98	1
8.52	8.16	4.30	.98	.90	.90	1
5.68	5.43	2.87	.98	.89	.89	1
2.84	2.72	1.43	.98	.89	.89	1
.00	.00	.00	.98	.90	.89	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.93	.00	.00	.00	.00	.00	1
8.16	325.18	152.15	173.03	173.03	.00	1
5.43	647.17	304.31	342.86	342.86	.00	1
2.72	968.73	294.52	674.21	512.26	161.95	1
.00	1290.59	224.43	1066.16	681.97	384.19	1

Time = 30. Degree of Consolidation = 97.%

Total Settlement = .431

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 30. = .431

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 9.40

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.38	21.42	6.50	5.76	4.83	6
60.02	59.87	21.35	6.49	5.92	4.82	6
59.45	59.34	21.27	6.47	6.06	4.81	6
58.89	58.80	21.20	6.46	6.17	4.81	6
58.33	58.26	21.12	6.44	6.26	4.80	6

57.76	57.71	21.05	6.43	6.31	4.79	6
57.20	57.15	20.97	6.42	6.35	4.79	6
56.64	56.60	20.90	6.40	6.36	4.78	6
56.08	56.04	20.82	6.39	6.37	4.77	6
56.08	56.04	20.82	4.51	4.49	3.19	5
54.82	54.77	20.59	4.44	4.43	3.16	5
53.56	53.52	20.36	4.38	4.37	3.14	5
52.32	52.28	20.12	4.32	4.31	3.11	5
51.10	51.06	19.89	4.25	4.25	3.08	5
49.88	49.85	19.66	4.19	4.18	3.05	5
48.69	48.65	19.43	4.13	4.12	3.02	5
48.69	48.65	19.43	1.93	1.93	1.80	4
46.69	46.66	18.75	1.92	1.92	1.77	4
44.70	44.67	18.06	1.91	1.91	1.75	4
42.72	42.69	17.38	1.89	1.89	1.73	4
40.75	40.72	16.70	1.88	1.88	1.71	4
38.79	38.76	16.01	1.86	1.86	1.69	4
36.85	36.81	15.33	1.84	1.84	1.67	4
34.91	34.88	14.65	1.82	1.82	1.64	4
33.00	32.97	13.97	1.80	1.80	1.62	4
31.09	31.06	13.28	1.78	1.78	1.60	4
31.09	31.06	13.28	1.47	1.47	1.37	3
29.70	29.67	12.72	1.46	1.46	1.36	3
28.32	28.29	12.16	1.45	1.45	1.35	3
26.94	26.91	11.59	1.44	1.44	1.34	3
25.57	25.54	11.03	1.43	1.43	1.33	3
24.21	24.18	10.47	1.42	1.42	1.32	3
22.84	22.82	9.90	1.41	1.41	1.31	3
21.49	21.46	9.34	1.40	1.40	1.30	3
20.14	20.11	8.78	1.39	1.39	1.29	3
18.80	18.77	8.21	1.38	1.38	1.29	3
18.80	18.77	8.21	1.34	1.34	1.27	2
16.88	16.85	7.39	1.33	1.33	1.26	2
14.97	14.94	6.57	1.32	1.32	1.25	2
13.07	13.04	5.75	1.31	1.31	1.25	2
11.18	11.15	4.93	1.30	1.30	1.24	2
9.30	9.27	4.11	1.29	1.29	1.23	2
7.43	7.40	3.29	1.28	1.28	1.23	2
5.56	5.53	2.46	1.27	1.27	1.22	2
3.70	3.67	1.64	1.26	1.26	1.21	2
1.85	1.83	.82	1.25	1.24	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.38	1290.54	246.20	1044.34	681.92	362.42	6
59.87	1327.40	193.27	1134.13	714.16	419.97	6
59.34	1364.97	146.90	1218.07	747.11	470.96	6
58.80	1403.14	108.97	1294.16	780.66	513.51	6
58.26	1441.78	80.57	1361.21	814.68	546.53	6
57.71	1480.76	61.41	1419.35	849.04	570.32	6
57.15	1519.95	50.17	1469.79	883.61	586.18	6
56.60	1559.26	44.99	1514.27	918.30	595.97	6
56.04	1598.61	43.96	1554.65	953.03	601.62	6
56.04	1598.61	43.96	1554.65	953.03	601.62	5
54.77	1703.40	66.62	1636.78	1032.07	604.71	5
53.52	1807.34	91.04	1716.30	1110.25	606.04	5
52.28	1910.38	116.28	1794.10	1187.55	606.56	5
51.06	2012.51	141.83	1870.68	1263.93	606.76	5
49.85	2113.72	167.44	1946.28	1339.39	606.89	5
48.65	2214.02	193.00	2021.02	1413.94	607.08	5

48.65	2214.02	193.00	2021.02	1413.94	607.08	4
46.66	2414.46	267.32	2147.14	1538.51	608.62	4
44.67	2614.38	343.60	2270.78	1662.58	608.20	4
42.69	2813.77	426.56	2387.21	1786.11	601.10	4
40.72	3012.55	512.96	2499.60	1909.03	590.56	4
38.76	3210.62	577.14	2633.48	2031.24	602.24	4
36.81	3407.88	647.59	2760.29	2152.64	607.65	4
34.88	3604.27	722.48	2881.80	2273.18	608.62	4
32.97	3799.76	798.34	3001.43	2392.81	608.62	4
31.06	3994.35	874.19	3120.15	2511.53	608.62	4
31.06	3994.35	874.19	3120.15	2511.53	608.62	3
29.67	4142.92	936.05	3206.87	2598.24	608.62	3
28.29	4291.09	997.91	3293.18	2684.56	608.62	3
26.91	4438.89	1061.87	3377.03	2770.50	606.53	3
25.54	4586.34	1124.54	3461.79	2856.09	605.71	3
24.18	4733.43	1186.53	3546.90	2941.32	605.58	3
22.82	4880.18	1248.26	3631.91	3026.21	605.70	3
21.46	5026.58	1309.90	3716.67	3110.75	605.92	3
20.11	5172.63	1371.41	3801.21	3194.94	606.27	3
18.77	5318.34	1432.63	3885.71	3278.79	606.91	3
18.77	5318.34	1432.63	3885.71	3278.79	606.91	2
16.85	5524.00	1517.52	4006.48	3398.36	608.12	2
14.94	5729.13	1603.30	4125.83	3517.40	608.44	2
13.04	5933.74	1689.28	4244.46	3635.91	608.55	2
11.15	6137.82	1775.31	4362.51	3753.89	608.62	2
9.27	6341.38	1861.41	4479.97	3871.35	608.62	2
7.40	6544.39	1947.51	4596.88	3988.26	608.62	2
5.53	6746.92	2033.64	4713.28	4104.69	608.59	2
3.67	6948.98	2145.50	4803.48	4220.66	582.82	2
1.83	7150.44	2365.32	4785.12	4336.02	449.11	2
.00	7350.42	2900.52	4449.90	4449.90	.00	2

Time = 61. Degree of Consolidation = 4.%

Total Settlement = .200

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 61. = .200

Settlement caused by Secondary Compression at time 61. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
11.36	10.93	5.74
8.52	8.16	4.30
5.68	5.43	2.87
2.84	2.72	1.43
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1
.98	.90	.89	1

***** Stresses *****

XI	Total	Effective
10.93	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

8.16	325.19	152.15	173.03	173.03	.00	1
5.43	647.17	304.31	342.86	342.86	.00	1
2.72	968.73	294.52	674.22	512.27	161.95	1
.00	1290.54	246.20	1044.34	681.92	362.42	1

Time = 61. Degree of Consolidation = 98.%

Total Settlement = .432

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 61. = .432

Settlement caused by Secondary Compression at time 61. = .000

Surface Elevation = 9.33

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.27	21.42	6.50	5.69	4.83	6
60.02	59.76	21.35	6.49	5.81	4.82	6
59.45	59.24	21.27	6.47	5.92	4.81	6
58.89	58.71	21.20	6.46	6.02	4.81	6
58.33	58.18	21.12	6.44	6.11	4.80	6
57.76	57.64	21.05	6.43	6.18	4.79	6
57.20	57.10	20.97	6.42	6.23	4.79	6
56.64	56.55	20.90	6.40	6.28	4.78	6
56.08	56.00	20.82	6.39	6.31	4.77	6
56.08	56.00	20.82	4.51	4.44	3.19	5
54.82	54.74	20.59	4.44	4.40	3.16	5
53.56	53.49	20.36	4.38	4.35	3.14	5
52.32	52.26	20.12	4.32	4.30	3.11	5
51.10	51.04	19.89	4.25	4.24	3.08	5
49.88	49.83	19.66	4.19	4.18	3.05	5
48.69	48.64	19.43	4.13	4.11	3.02	5
48.69	48.64	19.43	1.93	1.93	1.80	4
46.69	46.64	18.75	1.92	1.92	1.77	4
44.70	44.65	18.06	1.91	1.90	1.75	4
42.72	42.67	17.38	1.89	1.89	1.73	4
40.75	40.70	16.70	1.88	1.87	1.71	4
38.79	38.75	16.01	1.86	1.86	1.69	4
36.85	36.80	15.33	1.84	1.84	1.67	4
34.91	34.87	14.65	1.82	1.82	1.64	4
33.00	32.95	13.97	1.80	1.80	1.62	4
31.09	31.05	13.28	1.78	1.78	1.60	4
31.09	31.05	13.28	1.47	1.47	1.37	3
29.70	29.66	12.72	1.46	1.46	1.36	3
28.32	28.28	12.16	1.45	1.45	1.35	3
26.94	26.90	11.59	1.44	1.44	1.34	3
25.57	25.53	11.03	1.43	1.43	1.33	3
24.21	24.16	10.47	1.42	1.42	1.32	3
22.84	22.80	9.90	1.41	1.41	1.31	3
21.49	21.45	9.34	1.40	1.40	1.30	3
20.14	20.10	8.78	1.39	1.39	1.29	3
18.80	18.76	8.21	1.38	1.38	1.29	3

18.80	18.76	8.21	1.34	1.27	2	
16.88	16.84	7.39	1.33	1.33	1.26	2
14.97	14.93	6.57	1.32	1.32	1.25	2
13.07	13.03	5.75	1.31	1.31	1.25	2
11.18	11.14	4.93	1.30	1.30	1.24	2
9.30	9.26	4.11	1.29	1.29	1.23	2
7.43	7.39	3.29	1.28	1.28	1.23	2
5.56	5.52	2.46	1.27	1.27	1.22	2
3.70	3.66	1.64	1.26	1.25	1.21	2
1.85	1.82	.82	1.25	1.23	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.27	1290.50	266.70	1023.80	681.88	341.92	6
59.76	1326.97	227.53	1099.43	713.73	385.71	6
59.24	1363.97	191.13	1172.84	746.11	426.73	6
58.71	1401.47	158.36	1243.11	778.99	464.12	6
58.18	1439.40	130.02	1309.38	812.30	497.09	6
57.64	1477.70	106.51	1371.19	845.98	525.21	6
57.10	1516.30	87.84	1428.47	879.96	548.51	6
56.55	1555.14	73.59	1481.55	914.18	567.38	6
56.00	1594.15	63.05	1531.11	948.57	582.54	6
56.00	1594.15	63.05	1531.11	948.57	582.54	5
54.74	1698.36	79.98	1618.38	1027.02	591.35	5
53.49	1801.90	99.99	1701.91	1104.82	597.10	5
52.26	1904.68	122.19	1782.49	1181.85	600.65	5
51.04	2006.64	145.87	1860.77	1258.05	602.71	5
49.83	2107.72	170.53	1937.20	1333.39	603.81	5
48.64	2207.92	195.87	2012.04	1407.83	604.21	5
48.64	2207.92	195.87	2012.04	1407.83	604.21	4
46.64	2408.34	268.67	2139.67	1532.40	607.27	4
44.65	2608.25	347.16	2261.09	1656.45	604.64	4
42.67	2807.60	434.09	2373.51	1779.94	593.57	4
40.70	3006.32	519.05	2487.26	1902.80	584.47	4
38.75	3204.31	582.46	2621.85	2024.94	596.92	4
36.80	3401.53	650.42	2751.11	2146.29	604.82	4
34.87	3597.90	722.59	2875.31	2266.81	608.51	4
32.95	3793.39	798.34	2995.06	2386.44	608.62	4
31.05	3987.98	874.19	3113.78	2505.16	608.62	4
31.05	3987.98	874.19	3113.78	2505.16	608.62	3
29.66	4136.55	936.05	3200.49	2591.87	608.62	3
28.28	4284.72	997.91	3286.81	2678.19	608.62	3
26.90	4432.52	1063.13	3369.39	2764.13	605.26	3
25.53	4579.95	1126.70	3453.25	2849.70	603.55	3
24.16	4727.03	1189.11	3537.92	2934.92	603.00	3
22.80	4873.76	1250.91	3622.85	3019.80	603.06	3
21.45	5020.15	1312.37	3707.78	3104.32	603.46	3
20.10	5166.19	1373.53	3792.66	3188.50	604.15	3
18.76	5311.89	1434.30	3877.58	3272.34	605.24	3
18.76	5311.89	1434.30	3877.58	3272.34	605.24	2
16.84	5517.54	1518.32	3999.22	3391.90	607.33	2
14.93	5722.67	1603.61	4119.07	3510.93	608.13	2
13.03	5927.28	1689.38	4237.90	3629.44	608.46	2
11.14	6131.36	1775.31	4356.05	3747.42	608.62	2
9.26	6334.92	1861.41	4473.51	3864.89	608.62	2
7.39	6537.93	1947.51	4590.42	3981.80	608.62	2
5.52	6740.43	2040.58	4699.86	4098.20	601.65	2
3.66	6942.42	2189.43	4752.99	4214.09	538.89	2
1.82	7143.59	2454.94	4688.65	4329.16	359.49	2
.00	7343.31	2900.52	4442.79	4442.79	.00	2

Time = 121. Degree of Consolidation = 7.%

Total Settlement = .313

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 121. = .313

Settlement caused by Secondary Compression at time 121. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
11.36	10.93	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.43	2.87	.98	.89	.89	1
2.84	2.72	1.43	.98	.89	.89	1
.00	.00	.00	.98	.90	.89	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.93	.00	.00	.00	.00	.00	1
8.15	325.19	152.15	173.04	173.04	.00	1
5.43	647.17	304.31	342.86	342.86	.00	1
2.72	968.74	294.52	674.22	512.27	161.95	1
.00	1290.50	266.70	1023.80	681.88	341.92	1

Time = 121. Degree of Consolidation = 98.%

Total Settlement = .432

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 121. = .432

Settlement caused by Secondary Compression at time 121. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 9.21

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.09	21.42	6.50	5.64	4.83	6
60.02	59.59	21.35	6.49	5.73	4.82	6

59.45	59.08	21.27	6.47	5.81	4.81	6
58.89	58.56	21.20	6.46	5.89	4.81	6
58.33	58.04	21.12	6.44	5.97	4.80	6
57.76	57.51	21.05	6.43	6.04	4.79	6
57.20	56.97	20.97	6.42	6.10	4.79	6
56.64	56.43	20.90	6.40	6.16	4.78	6
56.08	55.89	20.82	6.39	6.21	4.77	6
56.08	55.89	20.82	4.51	4.36	3.19	5
54.82	54.65	20.59	4.44	4.33	3.16	5
53.56	53.42	20.36	4.38	4.29	3.14	5
52.32	52.20	20.12	4.32	4.24	3.11	5
51.10	50.99	19.89	4.25	4.19	3.08	5
49.88	49.79	19.66	4.19	4.13	3.05	5
48.69	48.61	19.43	4.13	4.07	3.02	5
48.69	48.61	19.43	1.93	1.93	1.80	4
46.69	46.62	18.75	1.92	1.91	1.77	4
44.70	44.63	18.06	1.91	1.90	1.75	4
42.72	42.65	17.38	1.89	1.89	1.73	4
40.75	40.68	16.70	1.88	1.87	1.71	4
38.79	38.73	16.01	1.86	1.85	1.69	4
36.85	36.78	15.33	1.84	1.84	1.67	4
34.91	34.85	14.65	1.82	1.82	1.64	4
33.00	32.94	13.97	1.80	1.80	1.62	4
31.09	31.03	13.28	1.78	1.78	1.60	4
31.09	31.03	13.28	1.47	1.47	1.37	3
29.70	29.65	12.72	1.46	1.46	1.36	3
28.32	28.26	12.16	1.45	1.45	1.35	3
26.94	26.88	11.59	1.44	1.44	1.34	3
25.57	25.51	11.03	1.43	1.43	1.33	3
24.21	24.15	10.47	1.42	1.42	1.32	3
22.84	22.79	9.90	1.41	1.41	1.31	3
21.49	21.43	9.34	1.40	1.40	1.30	3
20.14	20.09	8.78	1.39	1.39	1.29	3
18.80	18.74	8.21	1.38	1.38	1.29	3
18.80	18.74	8.21	1.34	1.34	1.27	2
16.88	16.83	7.39	1.33	1.33	1.26	2
14.97	14.92	6.57	1.32	1.32	1.25	2
13.07	13.02	5.75	1.31	1.31	1.25	2
11.18	11.13	4.93	1.30	1.30	1.24	2
9.30	9.25	4.11	1.29	1.29	1.23	2
7.43	7.37	3.29	1.28	1.28	1.23	2
5.56	5.51	2.46	1.27	1.26	1.22	2
3.70	3.66	1.64	1.26	1.25	1.21	2
1.85	1.82	.82	1.25	1.23	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.09	1290.47	284.45	1006.01	681.85	324.17	6
59.59	1326.60	255.76	1070.84	713.36	357.48	6
59.08	1363.14	228.02	1135.11	745.28	389.84	6
58.56	1400.06	201.56	1198.50	777.58	420.92	6
58.04	1437.35	176.70	1260.66	810.25	450.41	6
57.51	1474.98	153.69	1321.29	843.26	478.03	6
56.97	1512.93	132.72	1380.21	876.58	503.62	6
56.43	1551.15	113.85	1437.31	910.19	527.11	6
55.89	1589.64	97.08	1492.56	944.05	548.51	6
55.89	1589.64	97.08	1492.56	944.05	548.51	5
54.65	1692.69	109.93	1582.76	1021.36	561.41	5
53.42	1795.24	125.63	1669.60	1098.15	571.45	5
52.20	1897.17	143.95	1753.22	1174.34	578.88	5

50.99	1998.40	164.65	1833.75	1249.82	583.94	5
49.79	2098.85	187.51	1911.34	1324.52	586.82	5
48.61	2198.45	212.39	1986.06	1398.36	587.70	5
48.61	2198.45	212.39	1986.06	1398.36	587.70	4
46.62	2398.77	281.72	2117.05	1522.83	594.22	4
44.63	2598.60	359.23	2239.37	1646.80	592.57	4
42.65	2797.86	447.18	2350.68	1770.20	580.48	4
40.68	2996.49	527.08	2469.41	1892.97	576.44	4
38.73	3194.39	589.60	2604.79	2015.01	589.78	4
36.78	3391.53	655.48	2736.05	2136.29	599.76	4
34.85	3587.86	724.99	2862.87	2256.76	606.11	4
32.94	3783.34	798.34	2985.00	2376.38	608.62	4
31.03	3977.93	874.19	3103.73	2495.11	608.62	4
31.03	3977.93	874.20	3103.73	2495.11	608.62	3
29.65	4126.49	936.05	3190.44	2581.82	608.62	3
28.26	4274.67	997.91	3276.76	2668.14	608.62	3
26.88	4422.46	1064.87	3357.60	2754.07	603.52	3
25.51	4569.88	1129.85	3440.04	2839.63	600.40	3
24.15	4716.94	1193.15	3523.79	2924.83	598.96	3
22.79	4863.65	1255.31	3608.34	3009.68	598.66	3
21.43	5010.01	1316.67	3693.34	3094.18	599.16	3
20.09	5156.03	1377.40	3778.63	3178.34	600.29	3
18.74	5301.70	1437.53	3864.17	3262.16	602.01	3
18.74	5301.70	1437.53	3864.17	3262.16	602.01	2
16.83	5507.34	1520.27	3987.07	3381.70	605.37	2
14.92	5712.47	1604.57	4107.89	3500.73	607.17	2
13.02	5917.07	1689.76	4227.31	3619.23	608.07	2
11.13	6121.15	1775.44	4345.71	3737.21	608.50	2
9.25	6324.70	1861.68	4463.02	3854.67	608.35	2
7.37	6527.71	1950.21	4577.50	3971.58	605.92	2
5.51	6730.15	2073.05	4657.10	4087.92	569.18	2
3.66	6931.91	2268.01	4663.90	4203.58	460.31	2
1.82	7132.70	2546.71	4586.00	4318.28	267.72	2
.00	7332.19	2900.52	4431.67	4431.67	.00	2

Time = 240. Degree of Consolidation = 11.%

Total Settlement = .491

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 240. = .491

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.93	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.43	2.87	.98	.89	.89	1
2.84	2.72	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.93	.00	.00	.00	.00	.00	1
8.15	325.20	152.15	173.04	173.04	.00	1
5.43	647.17	304.31	342.86	342.86	.00	1
2.72	968.74	294.52	674.23	512.28	161.95	1
.00	1290.47	284.45	1006.01	681.85	324.17	1

Time = 240. Degree of Consolidation = 98.%

Total Settlement = .433

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 240. = .433

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 9.04

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.94	21.42	6.50	5.61	4.83	6
60.02	59.44	21.35	6.49	5.69	4.82	6
59.45	58.93	21.27	6.47	5.76	4.81	6
58.89	58.42	21.20	6.46	5.83	4.81	6
58.33	57.90	21.12	6.44	5.89	4.80	6
57.76	57.37	21.05	6.43	5.96	4.79	6
57.20	56.85	20.97	6.42	6.02	4.79	6
56.64	56.31	20.90	6.40	6.07	4.78	6
56.08	55.78	20.82	6.39	6.12	4.77	6
56.08	55.78	20.82	4.51	4.29	3.19	5
54.82	54.55	20.59	4.44	4.26	3.16	5
53.56	53.34	20.36	4.38	4.22	3.14	5
52.32	52.13	20.12	4.32	4.18	3.11	5
51.10	50.94	19.89	4.25	4.13	3.08	5
49.88	49.76	19.66	4.19	4.07	3.05	5
48.69	48.59	19.43	4.13	4.01	3.02	5
48.69	48.59	19.43	1.93	1.92	1.80	4
46.69	46.59	18.75	1.92	1.91	1.77	4
44.70	44.61	18.06	1.91	1.90	1.75	4
42.72	42.63	17.38	1.89	1.89	1.73	4
40.75	40.67	16.70	1.88	1.87	1.71	4
38.79	38.71	16.01	1.86	1.85	1.69	4
36.85	36.77	15.33	1.84	1.84	1.67	4
34.91	34.84	14.65	1.82	1.82	1.64	4
33.00	32.92	13.97	1.80	1.80	1.62	4
31.09	31.02	13.28	1.78	1.78	1.60	4
31.09	31.02	13.28	1.47	1.47	1.37	3
29.70	29.63	12.72	1.46	1.46	1.36	3
28.32	28.25	12.16	1.45	1.45	1.35	3
26.94	26.87	11.59	1.44	1.44	1.34	3
25.57	25.50	11.03	1.43	1.43	1.33	3

24.21	24.13	10.47	1.42	1.42	1.32	3
22.84	22.78	9.90	1.41	1.41	1.31	3
21.49	21.42	9.34	1.40	1.40	1.30	3
20.14	20.07	8.78	1.39	1.39	1.29	3
18.80	18.73	8.21	1.38	1.38	1.29	3
18.80	18.73	8.21	1.34	1.34	1.27	2
16.88	16.81	7.39	1.33	1.33	1.26	2
14.97	14.91	6.57	1.32	1.32	1.25	2
13.07	13.01	5.75	1.31	1.31	1.25	2
11.18	11.12	4.93	1.30	1.30	1.24	2
9.30	9.24	4.11	1.29	1.29	1.23	2
7.43	7.36	3.29	1.28	1.27	1.23	2
5.56	5.50	2.46	1.27	1.26	1.22	2
3.70	3.65	1.64	1.26	1.24	1.21	2
1.85	1.82	.82	1.25	1.22	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.94	1290.45	293.11	997.34	681.83	315.51	6
59.44	1326.43	269.04	1057.39	713.19	344.20	6
58.93	1362.75	245.47	1117.28	744.88	372.39	6
58.42	1399.40	222.57	1176.82	776.91	399.91	6
57.90	1436.36	200.56	1235.81	809.26	426.54	6
57.37	1473.64	179.61	1294.03	841.92	452.11	6
56.85	1511.20	159.90	1351.30	874.86	476.44	6
56.31	1549.04	141.58	1407.46	908.08	499.39	6
55.78	1587.13	124.76	1462.36	941.54	520.82	6
55.78	1587.13	124.76	1462.36	941.54	520.82	5
54.55	1689.19	137.32	1551.87	1017.86	534.01	5
53.34	1790.77	152.35	1638.41	1093.68	544.73	5
52.13	1891.76	169.83	1721.93	1168.92	553.01	5
50.94	1992.07	189.69	1802.38	1243.49	558.89	5
49.76	2091.64	211.90	1879.74	1317.31	562.44	5
48.59	2190.37	236.36	1954.00	1390.28	563.72	5
48.59	2190.37	236.36	1954.00	1390.28	563.72	4
46.59	2390.54	302.12	2088.42	1514.60	573.82	4
44.61	2590.24	376.83	2213.41	1638.44	574.97	4
42.63	2789.39	462.89	2326.50	1761.73	564.77	4
40.67	2987.91	534.97	2452.94	1884.39	568.55	4
38.71	3185.73	595.91	2589.82	2006.35	583.47	4
36.77	3382.81	660.06	2722.74	2127.57	595.17	4
34.84	3579.09	727.58	2851.52	2248.00	603.52	4
32.92	3774.55	798.76	2975.80	2367.60	608.20	4
31.02	3969.14	874.39	3094.75	2486.32	608.42	4
31.02	3969.14	874.39	3094.75	2486.32	608.42	3
29.63	4117.71	936.05	3181.66	2573.03	608.62	3
28.25	4265.89	997.91	3267.97	2659.35	608.62	3
26.87	4413.67	1066.14	3347.53	2745.28	602.25	3
25.50	4561.08	1132.21	3428.88	2830.83	598.04	3
24.13	4708.13	1196.30	3511.82	2916.02	595.80	3
22.78	4854.82	1258.90	3595.91	3000.85	595.06	3
21.42	5001.16	1320.35	3680.80	3085.33	595.47	3
20.07	5147.15	1380.88	3766.27	3169.47	596.80	3
18.73	5292.81	1440.60	3852.22	3253.27	598.95	3
18.73	5292.81	1440.60	3852.22	3253.27	598.95	2
16.81	5498.43	1522.50	3975.94	3372.79	603.14	2
14.91	5703.55	1605.95	4097.60	3491.81	605.79	2
13.01	5908.14	1690.63	4217.52	3610.31	607.21	2
11.12	6112.22	1776.57	4335.64	3728.28	607.36	2
9.24	6315.75	1865.16	4450.59	3845.72	604.88	2

7.36	6518.73	1961.24	4557.48	3962.59	594.89	2
5.50	6721.06	2111.72	4609.34	4078.83	530.51	2
3.65	6922.61	2325.79	4596.82	4194.29	402.54	2
1.82	7123.18	2594.40	4528.78	4308.75	220.03	2
.00	7322.55	2900.52	4422.03	4422.03	.00	2

Time = 366. Degree of Consolidation = 14.%

Total Settlement = .645

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 366. = .645

Settlement caused by Secondary Compression at time 366. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.93	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.43	2.87	.98	.89	.89	1
2.84	2.72	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.93	.00	.00	.00	.00	.00	1
8.15	325.20	152.15	173.04	173.04	.00	1
5.43	647.17	304.31	342.86	342.86	.00	1
2.72	968.75	294.52	674.23	512.28	161.95	1
.00	1290.45	293.11	997.34	681.83	315.51	1

Time = 366. Degree of Consolidation = 98.%

Total Settlement = .433

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 366. = .433

Settlement caused by Secondary Compression at time 366. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 8.88

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.75	21.42	6.50	5.59	4.83	6
60.02	59.25	21.35	6.49	5.65	4.82	6
59.45	58.74	21.27	6.47	5.71	4.81	6
58.89	58.23	21.20	6.46	5.77	4.81	6
58.33	57.72	21.12	6.44	5.83	4.80	6
57.76	57.20	21.05	6.43	5.88	4.79	6
57.20	56.68	20.97	6.42	5.93	4.79	6
56.64	56.16	20.90	6.40	5.98	4.78	6
56.08	55.63	20.82	6.39	6.03	4.77	6
56.08	55.63	20.82	4.51	4.21	3.19	5
54.82	54.42	20.59	4.44	4.18	3.16	5
53.56	53.23	20.36	4.38	4.14	3.14	5
52.32	52.04	20.12	4.32	4.09	3.11	5
51.10	50.87	19.89	4.25	4.04	3.08	5
49.88	49.70	19.66	4.19	3.99	3.05	5
48.69	48.55	19.43	4.13	3.93	3.02	5
48.69	48.55	19.43	1.93	1.92	1.80	4
46.69	46.56	18.75	1.92	1.91	1.77	4
44.70	44.58	18.06	1.91	1.90	1.75	4
42.72	42.61	17.38	1.89	1.88	1.73	4
40.75	40.65	16.70	1.88	1.87	1.71	4
38.79	38.69	16.01	1.86	1.85	1.69	4
36.85	36.75	15.33	1.84	1.83	1.67	4
34.91	34.82	14.65	1.82	1.81	1.64	4
33.00	32.91	13.97	1.80	1.80	1.62	4
31.09	31.01	13.28	1.78	1.77	1.60	4
31.09	31.01	13.28	1.47	1.47	1.37	3
29.70	29.62	12.72	1.46	1.46	1.36	3
28.32	28.23	12.16	1.45	1.45	1.35	3
26.94	26.86	11.59	1.44	1.44	1.34	3
25.57	25.48	11.03	1.43	1.43	1.33	3
24.21	24.12	10.47	1.42	1.42	1.32	3
22.84	22.76	9.90	1.41	1.41	1.31	3
21.49	21.41	9.34	1.40	1.40	1.30	3
20.14	20.06	8.78	1.39	1.39	1.29	3
18.80	18.72	8.21	1.38	1.38	1.29	3
18.80	18.72	8.21	1.34	1.34	1.27	2
16.88	16.80	7.39	1.33	1.33	1.26	2
14.97	14.89	6.57	1.32	1.32	1.25	2
13.07	13.00	5.75	1.31	1.31	1.25	2
11.18	11.11	4.93	1.30	1.30	1.24	2
9.30	9.22	4.11	1.29	1.28	1.23	2
7.43	7.35	3.29	1.28	1.27	1.23	2
5.56	5.49	2.46	1.27	1.26	1.22	2
3.70	3.65	1.64	1.26	1.24	1.21	2
1.85	1.81	.82	1.25	1.22	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.75	1290.37	302.58	987.78	681.75	306.04	6
59.25	1326.19	281.92	1044.27	712.95	331.32	6
58.74	1362.30	261.72	1100.58	744.44	356.14	6
58.23	1398.69	242.08	1156.61	776.21	380.40	6
57.72	1435.36	223.14	1212.22	808.26	403.96	6
57.20	1472.30	205.04	1267.25	840.57	426.68	6
56.68	1509.48	187.92	1321.56	873.14	448.42	6
56.16	1546.90	171.90	1374.99	905.94	469.06	6

55.63	1584.54	157.13	1427.41	938.96	488.45	6
55.63	1584.54	157.13	1427.41	938.96	488.45	5
54.42	1685.43	170.68	1514.74	1014.09	500.65	5
53.23	1785.79	186.33	1599.46	1088.71	510.75	5
52.04	1885.55	204.12	1681.44	1162.72	518.72	5
50.87	1984.64	224.04	1760.60	1236.06	524.55	5
49.70	2082.98	246.08	1836.89	1308.64	528.25	5
48.55	2180.48	270.22	1910.26	1380.40	529.87	5
48.55	2180.48	270.22	1910.27	1380.40	529.87	4
46.56	2380.44	332.88	2047.55	1504.49	543.06	4
44.58	2579.93	404.53	2175.40	1628.13	547.27	4
42.61	2778.91	487.89	2291.01	1751.25	539.77	4
40.65	2977.27	547.27	2430.00	1873.75	556.25	4
38.69	3174.96	605.45	2569.50	1995.58	573.93	4
36.75	3371.93	667.12	2704.81	2116.69	588.12	4
34.82	3568.15	732.39	2835.76	2237.05	598.71	4
32.91	3763.57	801.68	2961.89	2356.61	605.28	4
31.01	3958.13	875.80	3082.33	2475.31	607.02	4
31.01	3958.13	875.80	3082.33	2475.31	607.02	3
29.62	4106.69	936.05	3170.64	2562.02	608.62	3
28.23	4254.87	997.91	3256.96	2648.34	608.62	3
26.86	4402.65	1067.42	3335.23	2734.26	600.97	3
25.48	4550.05	1134.61	3415.44	2819.80	595.64	3
24.12	4697.08	1199.58	3497.50	2904.97	592.52	3
22.76	4843.75	1262.75	3581.00	2989.78	591.22	3
21.41	4990.07	1324.44	3665.63	3074.24	591.38	3
20.06	5136.04	1384.91	3751.13	3158.36	592.78	3
18.72	5281.68	1444.32	3837.36	3242.13	595.22	3
18.72	5281.68	1444.32	3837.36	3242.13	595.22	2
16.80	5487.28	1525.61	3961.66	3361.64	600.03	2
14.89	5692.37	1608.57	4083.81	3480.64	603.17	2
13.00	5896.96	1693.46	4203.50	3599.12	604.38	2
11.11	6101.00	1781.39	4319.61	3717.07	602.54	2
9.22	6304.50	1875.26	4429.23	3834.46	594.77	2
7.35	6507.38	1981.25	4526.13	3951.25	574.88	2
5.49	6709.55	2159.16	4550.39	4067.32	483.07	2
3.65	6910.90	2379.40	4531.49	4182.57	348.92	2
1.81	7111.26	2631.41	4479.86	4296.84	183.02	2
.00	7310.56	2900.52	4410.04	4410.04	.00	2

Time = 541. Degree of Consolidation = 18.%

Total Settlement = .836

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 541. = .836

Settlement caused by Secondary Compression at time 541. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
11.36	10.93	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.43	2.87	.98	.89	.89	1

2.84	2.72	1.43	.98	.89	1
.00	.00	.00	.98	.89	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.93	.00	.00	.00	.00	.00	1
8.15	325.19	152.15	173.04	173.04	.00	1
5.43	647.17	304.31	342.86	342.86	.00	1
2.72	968.72	302.24	666.48	512.26	154.22	1
.00	1290.37	302.58	987.79	681.75	306.04	1

Time = 541. Degree of Consolidation = 98.%

Total Settlement = .435

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 541. = .435

Settlement caused by Secondary Compression at time 541. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 8.69

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.56	21.42	6.50	5.56	4.83	6
60.02	59.06	21.35	6.49	5.61	4.82	6
59.45	58.56	21.27	6.47	5.66	4.81	6
58.89	58.06	21.20	6.46	5.71	4.81	6
58.33	57.55	21.12	6.44	5.76	4.80	6
57.76	57.04	21.05	6.43	5.81	4.79	6
57.20	56.52	20.97	6.42	5.85	4.79	6
56.64	56.00	20.90	6.40	5.90	4.78	6
56.08	55.48	20.82	6.39	5.93	4.77	6
56.08	55.48	20.82	4.51	4.13	3.19	5
54.82	54.29	20.59	4.44	4.10	3.16	5
53.56	53.11	20.36	4.38	4.06	3.14	5
52.32	51.95	20.12	4.32	4.01	3.11	5
51.10	50.79	19.89	4.25	3.96	3.08	5
49.88	49.65	19.66	4.19	3.91	3.05	5
48.69	48.52	19.43	4.13	3.85	3.02	5
48.69	48.52	19.43	1.93	1.91	1.80	4
46.69	46.53	18.75	1.92	1.90	1.77	4
44.70	44.55	18.06	1.91	1.89	1.75	4
42.72	42.58	17.38	1.89	1.88	1.73	4
40.75	40.62	16.70	1.88	1.86	1.71	4
38.79	38.67	16.01	1.86	1.85	1.69	4
36.85	36.73	15.33	1.84	1.83	1.67	4
34.91	34.81	14.65	1.82	1.81	1.64	4
33.00	32.89	13.97	1.80	1.79	1.62	4
31.09	30.99	13.28	1.78	1.77	1.60	4

31.09	30.99	13.28	1.47	1.47	1.37	3
29.70	29.60	12.72	1.46	1.46	1.36	3
28.32	28.22	12.16	1.45	1.45	1.35	3
26.94	26.84	11.59	1.44	1.44	1.34	3
25.57	25.47	11.03	1.43	1.43	1.33	3
24.21	24.11	10.47	1.42	1.42	1.32	3
22.84	22.75	9.90	1.41	1.41	1.31	3
21.49	21.39	9.34	1.40	1.40	1.30	3
20.14	20.05	8.78	1.39	1.39	1.29	3
18.80	18.70	8.21	1.38	1.38	1.29	3
18.80	18.70	8.21	1.34	1.34	1.27	2
16.88	16.79	7.39	1.33	1.33	1.26	2
14.97	14.88	6.57	1.32	1.32	1.25	2
13.07	12.98	5.75	1.31	1.31	1.25	2
11.18	11.09	4.93	1.30	1.30	1.24	2
9.30	9.21	4.11	1.29	1.28	1.23	2
7.43	7.34	3.29	1.28	1.27	1.23	2
5.56	5.49	2.46	1.27	1.25	1.22	2
3.70	3.64	1.64	1.26	1.24	1.21	2
1.85	1.81	.82	1.25	1.22	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.56	1290.27	311.99	978.27	681.64	296.63	6
59.06	1325.93	294.20	1031.73	712.69	319.04	6
58.56	1361.85	276.86	1084.99	743.98	341.01	6
58.06	1398.00	260.02	1137.98	775.52	362.46	6
57.55	1434.40	243.82	1190.58	807.30	383.28	6
57.04	1471.02	228.37	1242.65	839.30	403.35	6
56.52	1507.85	213.79	1294.06	871.51	422.55	6
56.00	1544.89	200.20	1344.69	903.92	440.77	6
55.48	1582.11	187.70	1394.41	936.52	457.88	6
55.48	1582.11	187.70	1394.41	936.52	457.88	5
54.29	1681.87	202.46	1479.42	1010.54	468.88	5
53.11	1781.08	219.03	1562.05	1084.00	478.06	5
51.95	1879.66	237.44	1642.22	1156.83	485.39	5
50.79	1977.54	257.72	1719.83	1228.96	490.87	5
49.65	2074.67	279.85	1794.82	1300.33	494.48	5
48.52	2170.96	303.81	1867.15	1370.88	496.27	5
48.52	2170.96	303.82	1867.15	1370.88	496.27	4
46.53	2370.70	364.86	2005.84	1494.75	511.08	4
44.55	2569.98	434.86	2135.12	1618.18	516.94	4
42.58	2768.75	509.23	2259.52	1741.09	518.43	4
40.62	2966.93	561.37	2405.57	1863.41	542.15	4
38.67	3164.47	616.96	2547.51	1985.09	562.42	4
36.73	3361.32	676.11	2685.22	2106.08	579.13	4
34.81	3557.45	739.01	2818.43	2226.35	592.08	4
32.89	3752.80	806.12	2946.67	2345.84	600.83	4
30.99	3947.32	878.32	3069.00	2464.50	604.50	4
30.99	3947.32	878.32	3069.00	2464.50	604.50	3
29.60	4095.87	936.79	3159.09	2551.20	607.89	3
28.22	4244.05	998.45	3245.60	2637.51	608.08	3
26.84	4391.83	1068.66	3323.17	2723.44	599.73	3
25.47	4539.22	1136.60	3402.62	2808.97	593.65	3
24.11	4686.23	1202.25	3483.98	2894.12	589.86	3
22.75	4832.88	1265.93	3566.95	2978.92	588.04	3
21.39	4979.18	1327.94	3651.24	3063.36	587.88	3
20.05	5125.14	1388.55	3736.58	3147.45	589.13	3
18.70	5270.75	1447.98	3822.77	3231.21	591.56	3
18.70	5270.75	1447.98	3822.77	3231.21	591.56	2

16.79	5476.33	1529.31	3947.02	3350.69	596.33	2
14.88	5681.40	1612.62	4068.78	3469.66	599.12	2
12.98	5885.95	1698.87	4187.08	3588.12	598.96	2
11.09	6089.96	1789.93	4300.04	3706.03	594.01	2
9.21	6293.39	1889.24	4404.15	3823.35	580.79	2
7.34	6496.16	2003.99	4492.17	3940.03	552.14	2
5.49	6698.18	2199.71	4498.47	4055.95	442.52	2
3.64	6899.36	2417.87	4481.49	4171.03	310.46	2
1.81	7099.60	2655.20	4444.40	4285.17	159.23	2
.00	7298.84	2900.52	4398.32	4398.32	.00	2

Time = 730. Degree of Consolidation = 22.%

Total Settlement = 1.022

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 730. = 1.022

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
11.36	10.92	5.74
8.52	8.15	4.30
5.68	5.43	2.87
2.84	2.72	1.43
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
10.92	.00	.00
8.15	325.18	152.15
5.43	647.17	304.31
2.72	968.69	312.87
.00	1290.27	311.99

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
173.03	173.03	.00	1
342.86	342.86	.00	1
655.82	512.23	143.59	1
978.27	681.64	296.63	1

Time = 730. Degree of Consolidation = 99.%

Total Settlement = .436

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 730. = .436

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 8.50

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.26	21.42	6.50	5.51	4.83	6
60.02	58.76	21.35	6.49	5.55	4.82	6
59.45	58.27	21.27	6.47	5.59	4.81	6
58.89	57.77	21.20	6.46	5.63	4.81	6
58.33	57.27	21.12	6.44	5.66	4.80	6
57.76	56.76	21.05	6.43	5.70	4.79	6
57.20	56.25	20.97	6.42	5.73	4.79	6
56.64	55.74	20.90	6.40	5.76	4.78	6
56.08	55.23	20.82	6.39	5.79	4.77	6
56.08	55.23	20.82	4.51	4.01	3.19	5
54.82	54.07	20.59	4.44	3.97	3.16	5
53.56	52.93	20.36	4.38	3.93	3.14	5
52.32	51.79	20.12	4.32	3.88	3.11	5
51.10	50.66	19.89	4.25	3.83	3.08	5
49.88	49.55	19.66	4.19	3.77	3.05	5
48.69	48.45	19.43	4.13	3.71	3.02	5
48.69	48.45	19.43	1.93	1.90	1.80	4
46.69	46.47	18.75	1.92	1.89	1.77	4
44.70	44.50	18.06	1.91	1.88	1.75	4
42.72	42.54	17.38	1.89	1.87	1.73	4
40.75	40.58	16.70	1.88	1.86	1.71	4
38.79	38.64	16.01	1.86	1.84	1.69	4
36.85	36.70	15.33	1.84	1.83	1.67	4
34.91	34.78	14.65	1.82	1.81	1.64	4
33.00	32.86	13.97	1.80	1.79	1.62	4
31.09	30.97	13.28	1.78	1.77	1.60	4
31.09	30.97	13.28	1.47	1.47	1.37	3
29.70	29.58	12.72	1.46	1.46	1.36	3
28.32	28.19	12.16	1.45	1.45	1.35	3
26.94	26.82	11.59	1.44	1.44	1.34	3
25.57	25.45	11.03	1.43	1.43	1.33	3
24.21	24.08	10.47	1.42	1.42	1.32	3
22.84	22.73	9.90	1.41	1.41	1.31	3
21.49	21.37	9.34	1.40	1.40	1.30	3
20.14	20.03	8.78	1.39	1.39	1.29	3
18.80	18.68	8.21	1.38	1.38	1.29	3
18.80	18.68	8.21	1.34	1.34	1.27	2
16.88	16.77	7.39	1.33	1.33	1.26	2
14.97	14.86	6.57	1.32	1.32	1.25	2
13.07	12.97	5.75	1.31	1.30	1.25	2
11.18	11.08	4.93	1.30	1.29	1.24	2
9.30	9.20	4.11	1.29	1.28	1.23	2
7.43	7.33	3.29	1.28	1.27	1.23	2
5.56	5.48	2.46	1.27	1.25	1.22	2
3.70	3.64	1.64	1.26	1.23	1.21	2
1.85	1.81	.82	1.25	1.22	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.26	1290.05	327.67	962.38	681.43	280.95	6
58.76	1325.46	314.18	1011.28	712.22	299.06	6
58.27	1361.06	301.13	1059.93	743.20	316.73	6

57.77	1396.84	288.55	1108.29	774.36	333.93	6
57.27	1432.80	276.55	1156.26	805.70	350.56	6
56.76	1468.93	265.19	1203.74	837.20	366.53	6
56.25	1505.21	254.58	1250.63	868.86	381.76	6
55.74	1541.63	244.79	1296.84	900.67	396.17	6
55.23	1578.19	235.93	1342.27	932.61	409.66	6
55.23	1578.19	235.93	1342.27	932.61	409.66	5
54.07	1676.19	252.72	1423.47	1004.86	418.62	5
52.93	1773.56	270.91	1502.66	1076.48	426.18	5
51.79	1870.26	290.53	1579.73	1147.43	432.31	5
50.66	1966.22	311.59	1654.64	1217.64	437.00	5
49.55	2061.41	334.09	1727.32	1287.07	440.25	5
48.45	2155.76	358.01	1797.75	1355.68	442.07	5
48.45	2155.76	358.01	1797.75	1355.68	442.07	4
46.47	2355.12	418.59	1936.53	1479.18	457.35	4
44.50	2554.04	488.22	2065.83	1602.24	463.59	4
42.54	2752.46	538.28	2214.18	1724.80	489.38	4
40.58	2950.31	586.95	2363.36	1846.79	516.57	4
38.64	3147.56	639.00	2508.56	1968.18	540.38	4
36.70	3344.17	694.65	2649.53	2088.94	560.59	4
34.78	3540.10	754.26	2785.83	2209.00	576.83	4
32.86	3735.28	818.52	2916.76	2328.33	588.43	4
30.97	3929.67	888.62	3041.05	2446.85	594.20	4
30.97	3929.67	888.62	3041.05	2446.85	594.20	3
29.58	4078.16	945.12	3133.05	2533.49	599.56	3
28.19	4226.29	1005.85	3220.45	2619.76	600.69	3
26.82	4374.03	1074.91	3299.13	2705.64	593.49	3
25.45	4521.39	1142.19	3379.20	2791.14	588.06	3
24.08	4668.38	1207.73	3460.65	2876.27	584.38	3
22.73	4815.00	1271.62	3543.37	2961.03	582.35	3
21.37	4961.26	1334.03	3627.23	3045.43	581.80	3
20.03	5107.18	1395.13	3712.04	3129.49	582.55	3
18.68	5252.76	1455.19	3797.57	3213.21	584.35	3
18.68	5252.76	1455.19	3797.57	3213.21	584.36	2
16.77	5458.29	1537.75	3920.54	3332.65	587.89	2
14.86	5663.30	1623.23	4040.08	3451.56	588.51	2
12.97	5867.78	1713.11	4154.67	3569.94	584.73	2
11.08	6071.68	1809.69	4261.99	3687.75	574.24	2
9.20	6274.96	1916.32	4358.65	3804.93	553.72	2
7.33	6477.55	2054.63	4422.92	3921.42	501.50	2
5.48	6679.36	2252.88	4426.47	4037.13	389.35	2
3.64	6880.33	2463.00	4417.33	4152.00	265.33	2
1.81	7080.41	2681.16	4399.25	4265.99	133.27	2
.00	7279.60	2900.52	4379.08	4379.08	.00	2

Time = 1081. Degree of Consolidation = 29.%

Total Settlement = 1.327

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 1081. = 1.327

Settlement caused by Secondary Compression at time 1081. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.43	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.16	152.15	173.00	173.00	.00	1
5.43	647.17	304.31	342.86	342.86	.00	1
2.71	968.62	336.15	632.47	512.15	120.32	1
.00	1290.05	327.67	962.38	681.43	280.95	1

Time = 1081. Degree of Consolidation = 99.%

Total Settlement = .440

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 1081. = .440

Settlement caused by Secondary Compression at time 1081. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 8.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.99	21.42	6.50	5.50	4.83	6
60.02	58.50	21.35	6.49	5.52	4.82	6
59.45	58.01	21.27	6.47	5.54	4.81	6
58.89	57.51	21.20	6.46	5.57	4.81	6
58.33	57.02	21.12	6.44	5.59	4.80	6
57.76	56.52	21.05	6.43	5.61	4.79	6
57.20	56.02	20.97	6.42	5.63	4.79	6
56.64	55.51	20.90	6.40	5.65	4.78	6
56.08	55.01	20.82	6.39	5.67	4.77	6
56.08	55.01	20.82	4.51	3.91	3.19	5
54.82	53.88	20.59	4.44	3.87	3.16	5
53.56	52.75	20.36	4.38	3.82	3.14	5
52.32	51.64	20.12	4.32	3.77	3.11	5
51.10	50.54	19.89	4.25	3.71	3.08	5
49.88	49.46	19.66	4.19	3.66	3.05	5
48.69	48.39	19.43	4.13	3.60	3.02	5
48.69	48.39	19.43	1.93	1.90	1.80	4
46.69	46.41	18.75	1.92	1.89	1.77	4
44.70	44.45	18.06	1.91	1.87	1.75	4
42.72	42.49	17.38	1.89	1.86	1.73	4
40.75	40.54	16.70	1.88	1.85	1.71	4

38.79	38.60	16.01	1.86	1.83	1.69	4
36.85	36.67	15.33	1.84	1.82	1.67	4
34.91	34.74	14.65	1.82	1.80	1.64	4
33.00	32.84	13.97	1.80	1.79	1.62	4
31.09	30.94	13.28	1.78	1.77	1.60	4
31.09	30.94	13.28	1.47	1.47	1.37	3
29.70	29.55	12.72	1.46	1.46	1.36	3
28.32	28.17	12.16	1.45	1.45	1.35	3
26.94	26.80	11.59	1.44	1.44	1.34	3
25.57	25.43	11.03	1.43	1.43	1.33	3
24.21	24.06	10.47	1.42	1.42	1.32	3
22.84	22.71	9.90	1.41	1.41	1.31	3
21.49	21.35	9.34	1.40	1.40	1.30	3
20.14	20.01	8.78	1.39	1.39	1.29	3
18.80	18.67	8.21	1.38	1.38	1.29	3
18.80	18.67	8.21	1.34	1.33	1.27	2
16.88	16.75	7.39	1.33	1.32	1.26	2
14.97	14.85	6.57	1.32	1.31	1.25	2
13.07	12.95	5.75	1.31	1.30	1.25	2
11.18	11.07	4.93	1.30	1.29	1.24	2
9.30	9.19	4.11	1.29	1.28	1.23	2
7.43	7.33	3.29	1.28	1.26	1.23	2
5.56	5.48	2.46	1.27	1.25	1.22	2
3.70	3.64	1.64	1.26	1.23	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.99	1289.89	332.67	957.22	681.27	275.96	6
58.50	1325.19	324.58	1000.61	711.95	288.66	6
58.01	1360.61	316.59	1044.01	742.75	301.27	6
57.51	1396.14	308.80	1087.33	773.65	313.68	6
57.02	1431.77	301.31	1130.47	804.67	325.79	6
56.52	1467.51	294.20	1173.31	835.79	337.52	6
56.02	1503.35	287.59	1215.76	867.01	348.75	6
55.51	1539.28	281.56	1257.72	898.32	359.40	6
55.01	1575.29	276.21	1299.08	929.71	369.37	6
55.01	1575.29	276.21	1299.08	929.71	369.37	5
53.88	1671.81	295.14	1376.67	1000.47	376.19	5
52.75	1767.63	315.04	1452.58	1070.54	382.04	5
51.64	1862.71	335.96	1526.75	1139.88	386.87	5
50.54	1957.03	357.94	1599.09	1208.45	390.64	5
49.46	2050.54	380.99	1669.54	1276.21	393.34	5
48.39	2143.20	405.12	1738.09	1343.12	394.97	5
48.39	2143.20	405.12	1738.09	1343.12	394.97	4
46.41	2342.24	467.36	1874.88	1466.30	408.58	4
44.45	2540.82	521.46	2019.37	1589.02	430.34	4
42.49	2738.91	565.22	2173.69	1711.25	462.44	4
40.54	2936.45	611.88	2324.57	1832.93	491.64	4
38.60	3133.42	661.70	2471.72	1954.04	517.68	4
36.67	3329.77	715.05	2614.73	2074.54	540.19	4
34.74	3525.47	772.45	2753.02	2194.37	558.65	4
32.84	3720.45	834.72	2885.72	2313.49	572.23	4
30.94	3914.65	903.29	3011.36	2431.83	579.53	4
30.94	3914.65	903.29	3011.36	2431.83	579.53	3
29.55	4063.06	958.31	3104.74	2518.38	586.36	3
28.17	4211.11	1018.84	3192.27	2604.57	587.70	3
26.80	4358.78	1085.85	3272.93	2690.39	582.54	3
25.43	4506.08	1151.69	3354.39	2775.83	578.56	3
24.06	4653.01	1216.34	3436.68	2860.90	575.77	3

22.71	4799.59	1279.82	3519.77	2945.62	574.15	3
21.35	4945.81	1342.25	3603.55	3029.98	573.57	3
20.01	5091.68	1403.78	3687.89	3113.99	573.90	3
18.67	5237.20	1464.63	3772.57	3197.66	574.91	3
18.67	5237.20	1464.63	3772.57	3197.66	574.91	2
16.75	5442.67	1548.77	3893.90	3317.03	576.87	2
14.85	5647.61	1636.72	4010.89	3435.87	575.02	2
12.95	5851.99	1729.95	4122.04	3554.16	567.89	2
11.07	6055.78	1830.54	4225.24	3671.85	553.40	2
9.19	6258.92	1941.36	4317.57	3788.89	528.68	2
7.33	6461.35	2095.39	4365.96	3905.21	460.75	2
5.48	6662.99	2290.67	4372.32	4020.76	351.56	2
3.64	6863.82	2492.35	4371.47	4135.49	235.98	2
1.81	7063.81	2697.19	4366.63	4249.39	117.24	2
.00	7262.97	2900.52	4362.45	4362.45	.00	2

Time = 1441. Degree of Consolidation = 34.%

Total Settlement = 1.591

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 1441. = 1.591

Settlement caused by Secondary Compression at time 1441. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.14	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.11	106.47	1
.00	1289.89	350.00	939.89	681.27	258.62	1

Time = 1441. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 1441. = .442

Settlement caused by Secondary Compression at time 1441. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 7.93

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.76	21.42	6.50	5.47	4.83	6
60.02	58.27	21.35	6.49	5.49	4.82	6
59.45	57.78	21.27	6.47	5.50	4.81	6
58.89	57.29	21.20	6.46	5.52	4.81	6
58.33	56.79	21.12	6.44	5.53	4.80	6
57.76	56.30	21.05	6.43	5.54	4.79	6
57.20	55.81	20.97	6.42	5.55	4.79	6
56.64	55.31	20.90	6.40	5.56	4.78	6
56.08	54.82	20.82	6.39	5.57	4.77	6
56.08	54.82	20.82	4.51	3.83	3.19	5
54.82	53.70	20.59	4.44	3.78	3.16	5
53.56	52.60	20.36	4.38	3.73	3.14	5
52.32	51.51	20.12	4.32	3.67	3.11	5
51.10	50.43	19.89	4.25	3.62	3.08	5
49.88	49.37	19.66	4.19	3.56	3.05	5
48.69	48.32	19.43	4.13	3.50	3.02	5
48.69	48.32	19.43	1.93	1.89	1.80	4
46.69	46.35	18.75	1.92	1.88	1.77	4
44.70	44.39	18.06	1.91	1.87	1.75	4
42.72	42.43	17.38	1.89	1.85	1.73	4
40.75	40.49	16.70	1.88	1.84	1.71	4
38.79	38.55	16.01	1.86	1.83	1.69	4
36.85	36.63	15.33	1.84	1.81	1.67	4
34.91	34.71	14.65	1.82	1.80	1.64	4
33.00	32.80	13.97	1.80	1.78	1.62	4
31.09	30.91	13.28	1.78	1.76	1.60	4
31.09	30.91	13.28	1.47	1.46	1.37	3
29.70	29.53	12.72	1.46	1.45	1.36	3
28.32	28.15	12.16	1.45	1.44	1.35	3
26.94	26.77	11.59	1.44	1.43	1.34	3
25.57	25.40	11.03	1.43	1.42	1.33	3
24.21	24.04	10.47	1.42	1.41	1.32	3
22.84	22.69	9.90	1.41	1.40	1.31	3
21.49	21.34	9.34	1.40	1.39	1.30	3
20.14	19.99	8.78	1.39	1.38	1.29	3
18.80	18.65	8.21	1.38	1.37	1.29	3
18.80	18.65	8.21	1.34	1.33	1.27	2
16.88	16.74	7.39	1.33	1.32	1.26	2
14.97	14.84	6.57	1.32	1.31	1.25	2
13.07	12.94	5.75	1.31	1.30	1.25	2
11.18	11.06	4.93	1.30	1.29	1.24	2
9.30	9.18	4.11	1.29	1.27	1.23	2
7.43	7.32	3.29	1.28	1.26	1.23	2
5.56	5.47	2.46	1.27	1.24	1.22	2
3.70	3.64	1.64	1.26	1.23	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
58.76	1289.89	341.62	948.27	681.27	267.00	6
58.27	1325.05	335.90	989.14	711.80	277.34	6
57.78	1360.28	330.64	1029.64	742.42	287.22	6
57.29	1395.59	325.82	1069.77	773.11	296.67	6
56.79	1430.96	321.45	1109.51	803.86	305.65	6
56.30	1466.39	317.59	1148.80	834.67	314.13	6
55.81	1501.87	314.26	1187.62	865.53	322.08	6
55.31	1537.40	311.49	1225.91	896.44	329.47	6
54.82	1572.96	309.32	1263.64	927.38	336.26	6
54.82	1572.96	309.32	1263.64	927.38	336.26	5
53.70	1668.25	330.32	1337.93	996.92	341.01	5
52.60	1762.78	351.96	1410.82	1065.69	345.12	5
51.51	1856.51	374.24	1482.27	1133.68	348.59	5
50.43	1949.44	397.16	1552.28	1200.86	351.42	5
49.37	2041.53	420.67	1620.86	1267.20	353.66	5
48.32	2132.77	444.74	1688.03	1332.69	355.35	5
48.32	2132.77	444.74	1688.03	1332.69	355.35	4
46.35	2331.52	506.31	1825.22	1455.58	369.64	4
44.39	2529.80	547.36	1982.44	1578.00	404.44	4
42.43	2727.58	590.50	2137.08	1699.92	437.16	4
40.49	2924.83	636.13	2288.69	1821.31	467.39	4
38.55	3121.51	684.67	2436.85	1942.13	494.71	4
36.63	3317.60	736.59	2581.01	2062.36	518.65	4
34.71	3513.05	792.56	2720.49	2181.95	538.54	4
32.80	3707.79	853.54	2854.26	2300.84	553.42	4
30.91	3901.78	921.12	2980.66	2418.96	561.70	4
30.91	3901.78	921.12	2980.66	2418.96	561.70	3
29.53	4050.07	975.16	3074.92	2505.40	569.51	3
28.15	4198.02	1036.23	3161.79	2591.49	570.30	3
26.77	4345.60	1101.16	3244.44	2677.21	567.23	3
25.40	4492.82	1165.40	3327.42	2762.57	564.85	3
24.04	4639.68	1228.92	3410.76	2847.57	563.18	3
22.69	4786.19	1291.76	3494.42	2932.22	562.20	3
21.34	4932.34	1354.00	3578.34	3016.51	561.83	3
19.99	5078.14	1415.75	3662.40	3100.46	561.94	3
18.65	5223.60	1477.20	3746.40	3184.06	562.34	3
18.65	5223.60	1477.20	3746.40	3184.06	562.35	2
16.74	5428.99	1562.55	3866.44	3303.35	563.09	2
14.84	5633.84	1652.38	3981.46	3422.10	559.36	2
12.94	5838.12	1748.00	4090.12	3540.28	549.84	2
11.06	6041.79	1851.16	4190.63	3657.85	532.78	2
9.18	6244.80	1964.22	4280.57	3774.76	505.81	2
7.32	6447.08	2129.86	4317.21	3890.94	426.27	2
5.47	6648.59	2320.60	4327.99	4006.36	321.63	2
3.64	6849.31	2514.49	4334.82	4120.98	213.84	2
1.81	7049.23	2708.92	4340.31	4234.81	105.51	2
.00	7248.36	2900.52	4347.84	4347.84	.00	2

Time = 1825. Degree of Consolidation = 39.%

Total Settlement = 1.825

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 1825. = 1.825

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.14	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.11	106.47	1
.00	1289.89	350.00	939.89	681.27	258.62	1

Time = 1825. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 1825. = .442

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 7.69

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.42	21.42	6.50	5.37	4.83	6
60.02	57.94	21.35	6.49	5.38	4.82	6
59.45	57.45	21.27	6.47	5.39	4.81	6
58.89	56.97	21.20	6.46	5.40	4.81	6
58.33	56.49	21.12	6.44	5.41	4.80	6
57.76	56.00	21.05	6.43	5.41	4.79	6
57.20	55.52	20.97	6.42	5.42	4.79	6
56.64	55.03	20.90	6.40	5.42	4.78	6
56.08	54.55	20.82	6.39	5.43	4.77	6
56.08	54.55	20.82	4.51	3.72	3.19	5
54.82	53.46	20.59	4.44	3.66	3.16	5
53.56	52.38	20.36	4.38	3.61	3.14	5
52.32	51.32	20.12	4.32	3.56	3.11	5
51.10	50.27	19.89	4.25	3.50	3.08	5
49.88	49.24	19.66	4.19	3.44	3.05	5
48.69	48.21	19.43	4.13	3.39	3.02	5

48.69	48.21	19.43	1.93	1.88	1.80	4
46.69	46.25	18.75	1.92	1.87	1.77	4
44.70	44.29	18.06	1.91	1.86	1.75	4
42.72	42.34	17.38	1.89	1.85	1.73	4
40.75	40.41	16.70	1.88	1.83	1.71	4
38.79	38.48	16.01	1.86	1.82	1.69	4
36.85	36.56	15.33	1.84	1.80	1.67	4
34.91	34.65	14.65	1.82	1.79	1.64	4
33.00	32.75	13.97	1.80	1.77	1.62	4
31.09	30.86	13.28	1.78	1.75	1.60	4
31.09	30.86	13.28	1.47	1.46	1.37	3
29.70	29.48	12.72	1.46	1.45	1.36	3
28.32	28.10	12.16	1.45	1.44	1.35	3
26.94	26.73	11.59	1.44	1.43	1.34	3
25.57	25.37	11.03	1.43	1.42	1.33	3
24.21	24.01	10.47	1.42	1.41	1.32	3
22.84	22.65	9.90	1.41	1.40	1.31	3
21.49	21.31	9.34	1.40	1.39	1.30	3
20.14	19.96	8.78	1.39	1.38	1.29	3
18.80	18.63	8.21	1.38	1.37	1.29	3
18.80	18.63	8.21	1.34	1.33	1.27	2
16.88	16.72	7.39	1.33	1.32	1.26	2
14.97	14.82	6.57	1.32	1.31	1.25	2
13.07	12.92	5.75	1.31	1.30	1.25	2
11.18	11.04	4.93	1.30	1.28	1.24	2
9.30	9.17	4.11	1.29	1.27	1.23	2
7.43	7.32	3.29	1.28	1.26	1.23	2
5.56	5.47	2.46	1.27	1.24	1.22	2
3.70	3.63	1.64	1.26	1.23	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.42	1289.88	374.47	915.42	681.26	234.15	6
57.94	1324.56	370.83	953.73	711.32	242.41	6
57.45	1359.28	367.56	991.73	741.42	250.31	6
56.97	1394.05	364.63	1029.42	771.57	257.85	6
56.49	1428.86	362.07	1066.79	801.76	265.03	6
56.00	1463.70	359.89	1103.81	831.98	271.84	6
55.52	1498.57	358.09	1140.47	862.23	278.25	6
55.03	1533.46	356.70	1176.76	892.50	284.26	6
54.55	1568.37	355.72	1212.65	922.79	289.86	6
54.55	1568.37	355.72	1212.65	922.79	289.86	5
53.46	1661.98	377.40	1284.58	990.65	293.93	5
52.38	1754.81	399.28	1355.53	1057.73	297.80	5
51.32	1846.85	421.35	1425.50	1124.02	301.48	5
50.27	1938.10	443.59	1494.51	1189.51	305.00	5
49.24	2028.54	465.95	1562.59	1254.21	308.38	5
48.21	2118.19	488.41	1629.78	1318.10	311.67	5
48.21	2118.19	488.41	1629.78	1318.10	311.67	4
46.25	2316.61	535.69	1780.92	1440.67	340.25	4
44.29	2514.52	579.27	1935.25	1562.72	372.53	4
42.34	2711.91	624.15	2087.76	1684.25	403.51	4
40.41	2908.75	670.76	2237.99	1805.23	432.76	4
38.48	3105.02	719.65	2385.37	1925.64	459.73	4
36.56	3300.69	771.46	2529.23	2045.45	483.78	4
34.65	3495.72	827.08	2668.64	2164.62	504.01	4
32.75	3690.06	887.85	2802.21	2283.10	519.11	4
30.86	3883.63	955.97	2927.66	2400.81	526.85	4
30.86	3883.63	955.97	2927.66	2400.81	526.85	3

29.48	4031.71	1010.37	3021.34	2487.04	534.30	3
28.10	4179.45	1072.53	3106.92	2572.91	534.00	3
26.73	4326.83	1134.54	3192.29	2658.44	533.85	3
25.37	4473.87	1196.40	3277.47	2743.62	533.85	3
24.01	4620.56	1258.10	3362.46	2828.45	534.01	3
22.65	4766.91	1319.68	3447.22	2912.94	534.28	3
21.31	4912.90	1381.22	3531.69	2997.08	534.61	3
19.96	5058.55	1442.80	3615.75	3080.87	534.88	3
18.63	5203.86	1504.57	3699.29	3164.32	534.97	3
18.63	5203.86	1504.57	3699.29	3164.32	534.97	2
16.72	5409.08	1590.53	3818.55	3283.44	535.11	2
14.82	5613.75	1681.70	3932.05	3402.01	530.04	2
12.92	5817.84	1779.10	4038.75	3520.01	518.74	2
11.04	6021.32	1883.94	4137.38	3637.38	500.00	2
9.17	6224.12	1997.99	4226.14	3754.09	472.05	2
7.32	6426.20	2177.60	4248.60	3870.06	378.53	2
5.47	6627.53	2359.97	4267.56	3985.30	282.26	2
3.63	6828.11	2542.51	4285.60	4099.78	185.81	2
1.81	7027.95	2723.41	4304.54	4213.52	91.02	2
.00	7227.05	2900.52	4326.53	4326.53	.00	2

Time = 2521. Degree of Consolidation = 47.%

Total Settlement = 2.167

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 2521. = 2.167

Settlement caused by Secondary Compression at time 2521. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.14	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.11	106.47	1
.00	1289.88	350.00	939.88	681.26	258.62	1

Time = 2521. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 2521. = .442

Settlement caused by Secondary Compression at time 2521. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 7.35

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.28	21.42	6.50	5.33	4.83	6
60.02	57.80	21.35	6.49	5.34	4.82	6
59.45	57.32	21.27	6.47	5.35	4.81	6
58.89	56.84	21.20	6.46	5.35	4.81	6
58.33	56.36	21.12	6.44	5.36	4.80	6
57.76	55.88	21.05	6.43	5.36	4.79	6
57.20	55.40	20.97	6.42	5.37	4.79	6
56.64	54.92	20.90	6.40	5.37	4.78	6
56.08	54.44	20.82	6.39	5.37	4.77	6
56.08	54.44	20.82	4.51	3.67	3.19	5
54.82	53.36	20.59	4.44	3.62	3.16	5
53.56	52.30	20.36	4.38	3.57	3.14	5
52.32	51.24	20.12	4.32	3.51	3.11	5
51.10	50.20	19.89	4.25	3.46	3.08	5
49.88	49.18	19.66	4.19	3.41	3.05	5
48.69	48.16	19.43	4.13	3.36	3.02	5
48.69	48.16	19.43	1.93	1.88	1.80	4
46.69	46.20	18.75	1.92	1.87	1.77	4
44.70	44.24	18.06	1.91	1.85	1.75	4
42.72	42.30	17.38	1.89	1.84	1.73	4
40.75	40.36	16.70	1.88	1.83	1.71	4
38.79	38.44	16.01	1.86	1.81	1.69	4
36.85	36.52	15.33	1.84	1.80	1.67	4
34.91	34.61	14.65	1.82	1.78	1.64	4
33.00	32.72	13.97	1.80	1.77	1.62	4
31.09	30.83	13.28	1.78	1.75	1.60	4
31.09	30.83	13.28	1.47	1.45	1.37	3
29.70	29.45	12.72	1.46	1.44	1.36	3
28.32	28.08	12.16	1.45	1.44	1.35	3
26.94	26.71	11.59	1.44	1.43	1.34	3
25.57	25.35	11.03	1.43	1.42	1.33	3
24.21	23.99	10.47	1.42	1.41	1.32	3
22.84	22.64	9.90	1.41	1.40	1.31	3
21.49	21.29	9.34	1.40	1.39	1.30	3
20.14	19.95	8.78	1.39	1.38	1.29	3
18.80	18.61	8.21	1.38	1.37	1.29	3
18.80	18.61	8.21	1.34	1.33	1.27	2
16.88	16.71	7.39	1.33	1.32	1.26	2
14.97	14.81	6.57	1.32	1.31	1.25	2
13.07	12.92	5.75	1.31	1.29	1.25	2
11.18	11.04	4.93	1.30	1.28	1.24	2
9.30	9.17	4.11	1.29	1.27	1.23	2
7.43	7.31	3.29	1.28	1.25	1.23	2
5.56	5.47	2.46	1.27	1.24	1.22	2
3.70	3.63	1.64	1.26	1.23	1.21	2

1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.28	1289.88	387.47	902.41	681.26	221.15	6
57.80	1324.37	384.66	939.71	711.13	228.58	6
57.32	1358.89	382.14	976.75	741.03	235.72	6
56.84	1393.44	379.90	1013.55	770.96	242.59	6
56.36	1428.03	377.94	1050.09	800.93	249.16	6
55.88	1462.64	376.28	1086.36	830.92	255.44	6
55.40	1497.27	374.92	1122.35	860.93	261.42	6
54.92	1531.92	373.86	1158.07	890.96	267.11	6
54.44	1566.59	373.09	1193.50	921.00	272.50	6
54.44	1566.59	373.09	1193.50	921.00	272.50	5
53.36	1659.57	394.85	1264.72	988.24	276.48	5
52.30	1751.78	416.55	1335.23	1054.69	280.54	5
51.24	1843.21	438.12	1405.09	1120.37	284.72	5
50.20	1933.87	459.48	1474.39	1185.28	289.10	5
49.18	2023.76	480.54	1543.22	1249.43	293.79	5
48.16	2112.91	502.67	1610.24	1312.83	297.41	5
48.16	2112.91	502.67	1610.24	1312.83	297.41	4
46.20	2311.22	546.95	1764.27	1435.27	329.00	4
44.24	2508.99	591.78	1917.20	1557.18	360.02	4
42.30	2706.22	637.70	2068.51	1678.55	389.96	4
40.36	2902.89	685.22	2217.66	1799.37	418.30	4
38.44	3098.98	734.92	2364.06	1919.60	444.46	4
36.52	3294.47	787.52	2506.94	2039.23	467.71	4
34.61	3489.30	844.06	2645.24	2158.20	487.04	4
32.72	3683.43	906.05	2777.38	2276.47	500.91	4
30.83	3876.77	976.10	2900.67	2393.96	506.71	4
30.83	3876.77	976.10	2900.67	2393.96	506.72	3
29.45	4024.73	1032.32	2992.41	2480.05	512.35	3
28.08	4172.34	1092.90	3079.44	2565.81	513.63	3
26.71	4319.62	1153.59	3166.03	2651.23	514.80	3
25.35	4466.55	1214.33	3252.22	2736.30	515.92	3
23.99	4613.14	1275.16	3337.99	2821.04	516.95	3
22.64	4759.39	1336.08	3423.31	2905.43	517.89	3
21.29	4905.30	1397.14	3508.16	2989.48	518.69	3
19.95	5050.86	1458.44	3592.43	3073.18	519.25	3
18.61	5196.08	1520.07	3676.01	3156.54	519.48	3
18.61	5196.08	1520.07	3676.01	3156.54	519.47	2
16.71	5401.21	1605.79	3795.42	3275.56	519.85	2
14.81	5605.79	1696.94	3908.84	3394.05	514.80	2
12.92	5809.78	1794.42	4015.37	3511.95	503.42	2
11.04	6013.16	1899.35	4113.81	3629.23	484.58	2
9.17	6215.87	2019.31	4196.56	3745.84	450.72	2
7.31	6417.86	2197.33	4220.53	3861.73	358.80	2
5.47	6619.12	2375.83	4243.29	3976.89	266.40	2
3.63	6819.65	2553.56	4266.09	4091.32	174.77	2
1.81	7019.45	2729.07	4290.38	4205.02	85.36	2
.00	7218.54	2900.52	4318.02	4318.02	.00	2

Time = 2881. Degree of Consolidation = 50.%

Total Settlement = 2.303

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 2881. = 2.303

Settlement caused by Secondary Compression at time 2881. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.14	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.11	106.47	1
.00	1289.88	350.00	939.88	681.26	258.62	1

Time = 2881. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 2881. = .442

Settlement caused by Secondary Compression at time 2881. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 7.21

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.20	21.42	6.50	5.30	4.83	6
60.02	57.72	21.35	6.49	5.31	4.82	6
59.45	57.24	21.27	6.47	5.32	4.81	6
58.89	56.77	21.20	6.46	5.32	4.81	6
58.33	56.29	21.12	6.44	5.33	4.80	6
57.76	55.81	21.05	6.43	5.33	4.79	6
57.20	55.33	20.97	6.42	5.34	4.79	6
56.64	54.85	20.90	6.40	5.34	4.78	6
56.08	54.37	20.82	6.39	5.35	4.77	6
56.08	54.37	20.82	4.51	3.65	3.19	5
54.82	53.30	20.59	4.44	3.60	3.16	5

53.56	52.24	20.36	4.38	3.55	3.14	5
52.32	51.19	20.12	4.32	3.50	3.11	5
51.10	50.15	19.89	4.25	3.45	3.08	5
49.88	49.13	19.66	4.19	3.40	3.05	5
48.69	48.11	19.43	4.13	3.35	3.02	5
48.69	48.11	19.43	1.93	1.88	1.80	4
46.69	46.15	18.75	1.92	1.87	1.77	4
44.70	44.20	18.06	1.91	1.85	1.75	4
42.72	42.26	17.38	1.89	1.84	1.73	4
40.75	40.32	16.70	1.88	1.82	1.71	4
38.79	38.40	16.01	1.86	1.81	1.69	4
36.85	36.48	15.33	1.84	1.80	1.67	4
34.91	34.58	14.65	1.82	1.78	1.64	4
33.00	32.69	13.97	1.80	1.76	1.62	4
31.09	30.81	13.28	1.78	1.74	1.60	4
31.09	30.81	13.28	1.47	1.45	1.37	3
29.70	29.43	12.72	1.46	1.44	1.36	3
28.32	28.06	12.16	1.45	1.43	1.35	3
26.94	26.69	11.59	1.44	1.42	1.34	3
25.57	25.33	11.03	1.43	1.41	1.33	3
24.21	23.97	10.47	1.42	1.40	1.32	3
22.84	22.62	9.90	1.41	1.39	1.31	3
21.49	21.28	9.34	1.40	1.38	1.30	3
20.14	19.94	8.78	1.39	1.37	1.29	3
18.80	18.60	8.21	1.38	1.36	1.29	3
18.80	18.60	8.21	1.34	1.33	1.27	2
16.88	16.70	7.39	1.33	1.32	1.26	2
14.97	14.80	6.57	1.32	1.30	1.25	2
13.07	12.91	5.75	1.31	1.29	1.25	2
11.18	11.03	4.93	1.30	1.28	1.24	2
9.30	9.17	4.11	1.29	1.27	1.23	2
7.43	7.31	3.29	1.28	1.25	1.23	2
5.56	5.47	2.46	1.27	1.24	1.22	2
3.70	3.63	1.64	1.26	1.22	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.20	1289.88	395.93	893.95	681.26	212.69	6
57.72	1324.24	393.66	930.58	711.00	219.58	6
57.24	1358.63	391.53	967.10	740.77	226.33	6
56.77	1393.05	389.54	1003.51	770.57	232.94	6
56.29	1427.50	387.68	1039.82	800.40	239.43	6
55.81	1461.97	385.95	1076.02	830.25	245.77	6
55.33	1496.47	384.35	1112.11	860.13	251.99	6
54.85	1530.99	382.89	1148.10	890.02	258.07	6
54.37	1565.52	381.54	1183.98	919.94	264.04	6
54.37	1565.52	381.54	1183.98	919.94	264.04	5
53.30	1658.21	402.83	1255.38	986.88	268.50	5
52.24	1750.15	423.73	1326.42	1053.06	273.35	5
51.19	1841.34	444.21	1397.13	1118.51	278.63	5
50.15	1931.80	464.23	1467.57	1183.22	284.35	5
49.13	2021.56	483.77	1537.78	1247.22	290.56	5
48.11	2110.62	506.23	1604.39	1310.54	293.85	5
48.11	2110.62	506.23	1604.39	1310.54	293.85	4
46.15	2308.86	553.38	1755.48	1432.92	322.56	4
44.20	2506.54	600.63	1905.91	1554.74	351.17	4
42.26	2703.65	648.52	2055.13	1675.99	379.14	4
40.32	2900.18	697.64	2202.54	1796.66	405.88	4
38.40	3096.12	748.69	2347.43	1916.74	430.69	4

36.48	3291.43	802.53	2488.90	2036.20	452.70	4
34.58	3486.08	860.36	2625.72	2154.98	470.74	4
32.69	3680.01	923.92	2756.09	2273.05	483.04	4
30.81	3873.12	996.19	2876.93	2390.31	486.63	4
30.81	3873.12	996.19	2876.93	2390.31	486.63	3
29.43	4020.95	1054.54	2966.41	2476.28	490.14	3
28.06	4168.45	1113.82	3054.62	2561.91	492.71	3
26.69	4315.61	1173.34	3142.26	2647.22	495.05	3
25.33	4462.43	1233.08	3229.35	2732.18	497.17	3
23.97	4608.92	1293.05	3315.87	2816.81	499.06	3
22.62	4755.07	1353.28	3401.80	2901.11	500.69	3
21.28	4900.89	1413.82	3487.07	2985.06	502.01	3
19.94	5046.36	1474.73	3571.62	3068.67	502.95	3
18.60	5191.48	1536.13	3655.36	3151.94	503.42	3
18.60	5191.48	1536.13	3655.36	3151.94	503.42	2
16.70	5396.51	1621.35	3775.16	3270.87	504.29	2
14.80	5601.00	1712.18	3888.82	3389.26	499.56	2
12.91	5804.90	1809.39	3995.52	3507.06	488.45	2
11.03	6008.19	1914.03	4094.17	3624.25	469.91	2
9.17	6210.81	2039.80	4171.01	3740.78	430.24	2
7.31	6412.72	2214.78	4197.94	3856.59	341.35	2
5.47	6613.92	2389.60	4224.31	3971.69	252.63	2
3.63	6814.39	2563.06	4251.33	4086.07	165.27	2
1.81	7014.17	2733.90	4280.27	4199.74	80.53	2
.00	7213.25	2900.52	4312.73	4312.72	.00	2

Time = 3240. Degree of Consolidation = 51.%

Total Settlement = 2.388

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 3240. = 2.388

Settlement caused by Secondary Compression at time 3240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.14	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.11	106.47	1
.00	1289.88	350.00	939.88	681.26	258.62	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 3240. = .442

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 7.13

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.13	21.42	6.50	5.29	4.83	6
60.02	57.66	21.35	6.49	5.30	4.82	6
59.45	57.18	21.27	6.47	5.30	4.81	6
58.89	56.70	21.20	6.46	5.31	4.81	6
58.33	56.23	21.12	6.44	5.32	4.80	6
57.76	55.75	21.05	6.43	5.32	4.79	6
57.20	55.27	20.97	6.42	5.33	4.79	6
56.64	54.79	20.90	6.40	5.33	4.78	6
56.08	54.31	20.82	6.39	5.34	4.77	6
56.08	54.31	20.82	4.51	3.64	3.19	5
54.82	53.24	20.59	4.44	3.59	3.16	5
53.56	52.18	20.36	4.38	3.54	3.14	5
52.32	51.14	20.12	4.32	3.49	3.11	5
51.10	50.10	19.89	4.25	3.44	3.08	5
49.88	49.08	19.66	4.19	3.40	3.05	5
48.69	48.06	19.43	4.13	3.35	3.02	5
48.69	48.06	19.43	1.93	1.88	1.80	4
46.69	46.10	18.75	1.92	1.86	1.77	4
44.70	44.15	18.06	1.91	1.85	1.75	4
42.72	42.21	17.38	1.89	1.84	1.73	4
40.75	40.28	16.70	1.88	1.82	1.71	4
38.79	38.35	16.01	1.86	1.81	1.69	4
36.85	36.44	15.33	1.84	1.79	1.67	4
34.91	34.54	14.65	1.82	1.77	1.64	4
33.00	32.65	13.97	1.80	1.76	1.62	4
31.09	30.78	13.28	1.78	1.74	1.60	4
31.09	30.78	13.28	1.47	1.45	1.37	3
29.70	29.40	12.72	1.46	1.44	1.36	3
28.32	28.03	12.16	1.45	1.43	1.35	3
26.94	26.67	11.59	1.44	1.42	1.34	3
25.57	25.31	11.03	1.43	1.41	1.33	3
24.21	23.95	10.47	1.42	1.40	1.32	3
22.84	22.60	9.90	1.41	1.39	1.31	3
21.49	21.26	9.34	1.40	1.38	1.30	3
20.14	19.92	8.78	1.39	1.37	1.29	3
18.80	18.59	8.21	1.38	1.36	1.29	3
18.80	18.59	8.21	1.34	1.32	1.27	2
16.88	16.69	7.39	1.33	1.31	1.26	2
14.97	14.79	6.57	1.32	1.30	1.25	2
13.07	12.90	5.75	1.31	1.29	1.25	2

11.18	11.03	4.93	1.30	1.28	1.24	2
9.30	9.16	4.11	1.29	1.27	1.23	2
7.43	7.31	3.29	1.28	1.25	1.23	2
5.56	5.46	2.46	1.27	1.24	1.22	2
3.70	3.63	1.64	1.26	1.22	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.13	1289.88	399.88	890.00	681.26	208.75	6
57.66	1324.18	397.86	926.32	710.94	215.38	6
57.18	1358.51	395.89	962.62	740.65	221.97	6
56.70	1392.87	393.98	998.89	770.39	228.50	6
56.23	1427.25	392.12	1035.13	800.15	234.98	6
55.75	1461.66	390.31	1071.35	829.94	241.41	6
55.27	1496.10	388.55	1107.55	859.75	247.79	6
54.79	1530.56	386.84	1143.71	889.59	254.12	6
54.31	1565.04	385.18	1179.86	919.46	260.40	6
54.31	1565.04	385.18	1179.86	919.46	260.40	5
53.24	1657.61	406.22	1251.39	986.27	265.12	5
52.18	1749.42	426.74	1322.68	1052.34	270.34	5
51.14	1840.51	446.75	1393.76	1117.68	276.08	5
50.10	1930.90	466.23	1464.67	1182.31	282.35	5
49.08	2020.59	485.16	1535.43	1246.26	289.17	5
48.06	2109.61	507.91	1601.70	1309.53	292.17	5
48.06	2109.61	507.91	1601.70	1309.53	292.17	4
46.10	2307.82	557.63	1750.19	1431.88	318.31	4
44.15	2505.43	607.35	1898.08	1553.63	344.45	4
42.21	2702.45	657.56	2044.89	1674.79	370.10	4
40.28	2898.86	708.84	2190.02	1795.34	394.68	4
38.35	3094.65	761.91	2332.74	1915.27	417.47	4
36.44	3289.80	817.71	2472.08	2034.56	437.53	4
34.54	3484.25	877.54	2606.71	2153.15	453.56	4
32.65	3677.96	943.39	2734.56	2271.00	463.56	4
30.78	3870.83	1017.01	2853.82	2388.01	465.81	4
30.78	3870.83	1017.01	2853.82	2388.01	465.81	3
29.40	4018.53	1076.69	2941.85	2473.86	467.99	3
28.03	4165.90	1136.02	3029.88	2559.37	470.51	3
26.67	4312.94	1195.21	3117.73	2644.55	473.18	3
25.31	4459.65	1254.41	3205.23	2729.40	475.84	3
23.95	4606.02	1313.76	3292.26	2813.91	478.35	3
22.60	4752.05	1373.38	3378.68	2898.09	480.59	3
21.26	4897.76	1433.36	3464.39	2981.93	482.46	3
19.92	5043.12	1493.83	3549.29	3065.43	483.86	3
18.59	5188.14	1554.84	3633.29	3148.59	484.70	3
18.59	5188.14	1554.84	3633.29	3148.59	484.70	2
16.69	5393.05	1639.31	3753.74	3267.41	486.33	2
14.79	5597.43	1729.50	3867.92	3385.69	482.24	2
12.90	5801.23	1826.07	3975.16	3503.39	471.77	2
11.03	6004.42	1930.00	4074.42	3620.48	453.94	2
9.16	6206.94	2061.58	4145.37	3736.91	408.46	2
7.31	6408.77	2232.91	4175.86	3852.64	323.22	2
5.46	6609.90	2403.65	4206.25	3967.67	238.58	2
3.63	6810.33	2572.64	4237.69	4082.00	155.69	2
1.81	7010.07	2738.73	4271.35	4195.65	75.70	2
.00	7209.15	2900.52	4308.62	4308.62	.00	2

Time = 3650. Degree of Consolidation = 53.%

Total Settlement = 2.453

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 3650. = 2.453

Settlement caused by Secondary Compression at time 3650. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.15	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.11	106.47	1
.00	1289.88	350.00	939.88	681.26	258.62	1

Time = 3650. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 3650. = .442

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 7.06

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.05	21.42	6.50	5.29	4.83	6
60.02	57.58	21.35	6.49	5.29	4.82	6
59.45	57.10	21.27	6.47	5.30	4.81	6
58.89	56.63	21.20	6.46	5.30	4.81	6
58.33	56.15	21.12	6.44	5.31	4.80	6
57.76	55.67	21.05	6.43	5.31	4.79	6

57.20	55.20	20.97	6.42	5.32	4.79	6
56.64	54.72	20.90	6.40	5.33	4.78	6
56.08	54.24	20.82	6.39	5.33	4.77	6
56.08	54.24	20.82	4.51	3.64	3.19	5
54.82	53.17	20.59	4.44	3.59	3.16	5
53.56	52.11	20.36	4.38	3.54	3.14	5
52.32	51.07	20.12	4.32	3.49	3.11	5
51.10	50.03	19.89	4.25	3.44	3.08	5
49.88	49.01	19.66	4.19	3.39	3.05	5
48.69	47.99	19.43	4.13	3.35	3.02	5
48.69	47.99	19.43	1.93	1.88	1.80	4
46.69	46.03	18.75	1.92	1.86	1.77	4
44.70	44.08	18.06	1.91	1.85	1.75	4
42.72	42.14	17.38	1.89	1.83	1.73	4
40.75	40.21	16.70	1.88	1.82	1.71	4
38.79	38.29	16.01	1.86	1.80	1.69	4
36.85	36.39	15.33	1.84	1.79	1.67	4
34.91	34.49	14.65	1.82	1.77	1.64	4
33.00	32.61	13.97	1.80	1.75	1.62	4
31.09	30.74	13.28	1.78	1.73	1.60	4
31.09	30.74	13.28	1.47	1.44	1.37	3
29.70	29.36	12.72	1.46	1.43	1.36	3
28.32	27.99	12.16	1.45	1.42	1.35	3
26.94	26.63	11.59	1.44	1.41	1.34	3
25.57	25.28	11.03	1.43	1.40	1.33	3
24.21	23.92	10.47	1.42	1.39	1.32	3
22.84	22.58	9.90	1.41	1.39	1.31	3
21.49	21.24	9.34	1.40	1.38	1.30	3
20.14	19.90	8.78	1.39	1.37	1.29	3
18.80	18.57	8.21	1.38	1.36	1.29	3
18.80	18.57	8.21	1.34	1.32	1.27	2
16.88	16.67	7.39	1.33	1.31	1.26	2
14.97	14.78	6.57	1.32	1.30	1.25	2
13.07	12.89	5.75	1.31	1.29	1.25	2
11.18	11.02	4.93	1.30	1.28	1.24	2
9.30	9.16	4.11	1.29	1.26	1.23	2
7.43	7.30	3.29	1.28	1.25	1.23	2
5.56	5.46	2.46	1.27	1.24	1.22	2
3.70	3.63	1.64	1.26	1.22	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.05	1289.88	401.73	888.15	681.26	206.89	6
57.58	1324.15	399.83	924.32	710.91	213.41	6
57.10	1358.45	397.95	960.51	740.59	219.91	6
56.63	1392.78	396.08	996.70	770.30	226.40	6
56.15	1427.13	394.22	1032.91	800.03	232.88	6
55.67	1461.51	392.39	1069.13	829.79	239.34	6
55.20	1495.92	390.56	1105.36	859.58	245.78	6
54.72	1530.35	388.75	1141.60	889.39	252.21	6
54.24	1564.81	386.96	1177.85	919.23	258.62	6
54.24	1564.81	386.96	1177.85	919.23	258.62	5
53.17	1657.31	407.89	1249.43	985.98	263.45	5
52.11	1749.07	428.25	1320.82	1051.99	268.83	5
51.07	1840.11	448.06	1392.06	1117.28	274.78	5
50.03	1930.45	467.29	1463.16	1181.87	281.29	5
49.01	2020.11	485.96	1534.15	1245.78	288.37	5
47.99	2109.11	509.08	1600.04	1309.03	291.01	5
47.99	2109.11	509.08	1600.04	1309.03	291.01	4

46.03	2307.29	561.97	1745.31	1431.34	313.97	4
44.08	2504.83	614.90	1889.93	1553.03	336.90	4
42.14	2701.74	668.31	2033.43	1674.08	359.35	4
40.21	2898.00	722.75	2175.25	1794.48	380.77	4
38.29	3093.61	778.94	2314.67	1914.23	400.44	4
36.39	3288.53	837.85	2450.68	2033.29	417.39	4
34.49	3482.72	900.88	2581.84	2151.63	430.22	4
32.61	3676.13	970.27	2705.86	2269.17	436.69	4
30.74	3868.67	1045.19	2823.48	2385.85	437.63	4
30.74	3868.67	1045.19	2823.48	2385.85	437.63	3
29.36	4016.21	1106.15	2910.06	2471.54	438.52	3
27.99	4163.41	1166.40	2997.02	2556.88	440.14	3
26.63	4310.28	1226.14	3084.13	2641.89	442.25	3
25.28	4456.81	1285.61	3171.20	2726.56	444.64	3
23.92	4603.00	1344.98	3258.02	2810.89	447.13	3
22.58	4748.86	1404.42	3344.45	2894.90	449.55	3
21.24	4894.39	1464.08	3430.31	2978.56	451.75	3
19.90	5039.58	1524.10	3515.48	3061.90	453.59	3
18.57	5184.43	1584.62	3599.81	3144.89	454.92	3
18.57	5184.43	1584.62	3599.81	3144.89	454.92	2
16.67	5389.17	1668.06	3721.11	3263.52	457.58	2
14.78	5593.37	1757.05	3836.32	3381.63	454.69	2
12.89	5797.01	1852.29	3944.71	3499.17	445.54	2
11.02	6000.04	1954.68	4045.36	3616.10	429.26	2
9.16	6202.42	2094.47	4107.94	3732.38	375.56	2
7.30	6404.13	2259.75	4144.37	3847.99	296.38	2
5.46	6605.16	2424.09	4181.06	3962.93	218.14	2
3.63	6805.52	2586.42	4219.09	4077.19	141.90	2
1.81	7005.22	2745.58	4259.64	4190.79	68.85	2
.00	7204.27	2900.52	4303.75	4303.75	.00	2

Time = 4321. Degree of Consolidation = 55.%

Total Settlement = 2.532

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 4321. = 2.532

Settlement caused by Secondary Compression at time 4321. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
11.36	10.92	5.74
8.52	8.15	4.30
5.68	5.42	2.87
2.84	2.71	1.43
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.90	.90	1
.98	.89	.89	1
.98	.89	.89	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
10.92	.00	.00
8.15	325.15	152.15

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
172.99	172.99	.00	1

5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.11	106.47	1
.00	1289.88	350.00	939.88	681.26	258.62	1

Time = 4321. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 4321. = .442

Settlement caused by Secondary Compression at time 4321. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.99

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	57.99	21.42	6.50	5.29	4.83	6
60.02	57.51	21.35	6.49	5.29	4.82	6
59.45	57.04	21.27	6.47	5.30	4.81	6
58.89	56.56	21.20	6.46	5.30	4.81	6
58.33	56.08	21.12	6.44	5.31	4.80	6
57.76	55.61	21.05	6.43	5.31	4.79	6
57.20	55.13	20.97	6.42	5.32	4.79	6
56.64	54.65	20.90	6.40	5.32	4.78	6
56.08	54.17	20.82	6.39	5.33	4.77	6
56.08	54.17	20.82	4.51	3.64	3.19	5
54.82	53.10	20.59	4.44	3.59	3.16	5
53.56	52.05	20.36	4.38	3.54	3.14	5
52.32	51.00	20.12	4.32	3.49	3.11	5
51.10	49.97	19.89	4.25	3.44	3.08	5
49.88	48.94	19.66	4.19	3.39	3.05	5
48.69	47.93	19.43	4.13	3.35	3.02	5
48.69	47.93	19.43	1.93	1.88	1.80	4
46.69	45.97	18.75	1.92	1.86	1.77	4
44.70	44.02	18.06	1.91	1.85	1.75	4
42.72	42.08	17.38	1.89	1.83	1.73	4
40.75	40.15	16.70	1.88	1.81	1.71	4
38.79	38.24	16.01	1.86	1.80	1.69	4
36.85	36.33	15.33	1.84	1.78	1.67	4
34.91	34.44	14.65	1.82	1.76	1.64	4
33.00	32.56	13.97	1.80	1.74	1.62	4
31.09	30.69	13.28	1.78	1.72	1.60	4
31.09	30.69	13.28	1.47	1.44	1.37	3
29.70	29.32	12.72	1.46	1.43	1.36	3
28.32	27.96	12.16	1.45	1.42	1.35	3
26.94	26.60	11.59	1.44	1.41	1.34	3
25.57	25.24	11.03	1.43	1.40	1.33	3
24.21	23.89	10.47	1.42	1.39	1.32	3
22.84	22.55	9.90	1.41	1.38	1.31	3
21.49	21.21	9.34	1.40	1.37	1.30	3
20.14	19.88	8.78	1.39	1.36	1.29	3

18.80	18.55	8.21	1.38	1.35	1.29	3
18.80	18.55	8.21	1.34	1.32	1.27	2
16.88	16.65	7.39	1.33	1.31	1.26	2
14.97	14.76	6.57	1.32	1.30	1.25	2
13.07	12.88	5.75	1.31	1.28	1.25	2
11.18	11.01	4.93	1.30	1.27	1.24	2
9.30	9.15	4.11	1.29	1.26	1.23	2
7.43	7.30	3.29	1.28	1.25	1.23	2
5.56	5.46	2.46	1.27	1.23	1.22	2
3.70	3.63	1.64	1.26	1.22	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
57.99	1289.88	402.20	887.68	681.26	206.43	6
57.51	1324.14	400.33	923.82	710.90	212.92	6
57.04	1358.44	398.46	959.97	740.58	219.40	6
56.56	1392.76	396.61	996.15	770.28	225.87	6
56.08	1427.10	394.77	1032.34	800.00	232.34	6
55.61	1461.48	392.93	1068.55	829.75	238.79	6
55.13	1495.88	391.10	1104.77	859.53	245.24	6
54.65	1530.30	389.28	1141.02	889.34	251.68	6
54.17	1564.75	387.47	1177.28	919.17	258.11	6
54.17	1564.75	387.47	1177.28	919.17	258.11	5
53.10	1657.23	408.38	1248.86	985.90	262.96	5
52.05	1748.98	428.71	1320.26	1051.89	268.37	5
51.00	1840.00	448.48	1391.52	1117.17	274.35	5
49.97	1930.33	467.67	1462.65	1181.74	280.91	5
48.94	2019.97	486.29	1533.68	1245.64	288.04	5
47.93	2108.96	509.68	1599.28	1308.88	290.40	5
47.93	2108.96	509.68	1599.28	1308.88	290.40	4
45.97	2307.11	565.04	1742.07	1431.17	310.90	4
44.02	2504.60	620.51	1884.09	1552.80	331.29	4
42.08	2701.43	676.54	2024.89	1673.77	351.12	4
40.15	2897.58	733.65	2163.93	1794.06	369.87	4
38.24	3093.04	792.57	2300.47	1913.66	386.81	4
36.33	3287.78	854.32	2433.46	2032.54	400.92	4
34.44	3481.76	920.42	2561.35	2150.67	410.68	4
32.56	3674.92	993.38	2681.54	2267.96	413.58	4
30.69	3867.16	1069.89	2797.27	2384.34	412.93	4
30.69	3867.16	1069.89	2797.27	2384.34	412.93	3
29.32	4014.56	1132.41	2882.15	2469.89	412.26	3
27.96	4161.61	1193.89	2967.72	2555.08	412.64	3
26.60	4308.32	1254.60	3053.72	2639.93	413.79	3
25.24	4454.69	1314.74	3139.94	2724.44	415.51	3
23.89	4600.72	1374.55	3226.17	2808.61	417.56	3
22.55	4746.41	1434.21	3312.20	2892.44	419.76	3
21.21	4891.77	1493.88	3397.89	2975.94	421.94	3
19.88	5036.79	1553.76	3483.04	3059.11	423.93	3
18.55	5181.48	1613.96	3567.52	3141.93	425.59	3
18.55	5181.48	1613.96	3567.52	3141.93	425.59	2
16.65	5386.03	1696.75	3689.28	3260.39	428.89	2
14.76	5590.06	1784.74	3805.33	3378.32	427.00	2
12.88	5793.53	1878.64	3914.90	3495.70	419.20	2
11.01	5996.41	1979.27	4017.14	3612.47	404.67	2
9.15	6198.65	2126.91	4071.74	3728.61	343.13	2
7.30	6400.23	2285.95	4114.28	3844.10	270.18	2
5.46	6601.17	2443.86	4157.31	3958.94	198.37	2
3.63	6801.46	2599.56	4201.90	4073.13	128.76	2
1.81	7001.12	2752.09	4249.04	4186.70	62.34	2

.00	7200.17	2900.52	4299.64	4299.64	.00	2

Time = 5040. Degree of Consolidation = 56.%

Total Settlement = 2.597

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 5040. = 2.597

Settlement caused by Secondary Compression at time 5040. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.15	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.11	106.47	1
.00	1289.88	350.00	939.88	681.26	258.62	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 5040. = .442

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.92

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	57.95	21.42	6.50	5.28	4.83	6

60.02	57.48	21.35	6.49	5.29	4.82	6
59.45	57.00	21.27	6.47	5.30	4.81	6
58.89	56.53	21.20	6.46	5.30	4.81	6
58.33	56.05	21.12	6.44	5.31	4.80	6
57.76	55.57	21.05	6.43	5.31	4.79	6
57.20	55.10	20.97	6.42	5.32	4.79	6
56.64	54.62	20.90	6.40	5.32	4.78	6
56.08	54.14	20.82	6.39	5.33	4.77	6
56.08	54.14	20.82	4.51	3.64	3.19	5
54.82	53.07	20.59	4.44	3.59	3.16	5
53.56	52.01	20.36	4.38	3.54	3.14	5
52.32	50.97	20.12	4.32	3.49	3.11	5
51.10	49.93	19.89	4.25	3.44	3.08	5
49.88	48.91	19.66	4.19	3.39	3.05	5
48.69	47.90	19.43	4.13	3.35	3.02	5
48.69	47.90	19.43	1.93	1.88	1.80	4
46.69	45.94	18.75	1.92	1.86	1.77	4
44.70	43.99	18.06	1.91	1.85	1.75	4
42.72	42.05	17.38	1.89	1.83	1.73	4
40.75	40.12	16.70	1.88	1.81	1.71	4
38.79	38.21	16.01	1.86	1.80	1.69	4
36.85	36.30	15.33	1.84	1.78	1.67	4
34.91	34.41	14.65	1.82	1.76	1.64	4
33.00	32.53	13.97	1.80	1.74	1.62	4
31.09	30.67	13.28	1.78	1.72	1.60	4
31.09	30.67	13.28	1.47	1.44	1.37	3
29.70	29.30	12.72	1.46	1.43	1.36	3
28.32	27.94	12.16	1.45	1.42	1.35	3
26.94	26.58	11.59	1.44	1.41	1.34	3
25.57	25.23	11.03	1.43	1.40	1.33	3
24.21	23.88	10.47	1.42	1.39	1.32	3
22.84	22.54	9.90	1.41	1.38	1.31	3
21.49	21.20	9.34	1.40	1.37	1.30	3
20.14	19.87	8.78	1.39	1.36	1.29	3
18.80	18.54	8.21	1.38	1.35	1.29	3
18.80	18.54	8.21	1.34	1.31	1.27	2
16.88	16.65	7.39	1.33	1.30	1.26	2
14.97	14.76	6.57	1.32	1.29	1.25	2
13.07	12.88	5.75	1.31	1.28	1.25	2
11.18	11.01	4.93	1.30	1.27	1.24	2
9.30	9.15	4.11	1.29	1.26	1.23	2
7.43	7.30	3.29	1.28	1.25	1.23	2
5.56	5.46	2.46	1.27	1.23	1.22	2
3.70	3.63	1.64	1.26	1.22	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
57.95	1289.88	402.32	887.55	681.26	206.30	6
57.48	1324.14	400.46	923.68	710.90	212.78	6
57.00	1358.43	398.60	959.83	740.57	219.26	6
56.53	1392.75	396.75	996.00	770.27	225.73	6
56.05	1427.10	394.91	1032.18	799.99	232.19	6
55.57	1461.47	393.08	1068.39	829.74	238.64	6
55.10	1495.86	391.25	1104.61	859.52	245.09	6
54.62	1530.28	389.43	1140.85	889.32	251.53	6
54.14	1564.73	387.62	1177.12	919.15	257.97	6
54.14	1564.73	387.62	1177.12	919.15	257.97	5
53.07	1657.21	408.52	1248.69	985.88	262.81	5
52.01	1748.95	428.86	1320.09	1051.87	268.23	5

50.97	1839.97	448.62	1391.35	1117.14	274.21	5
49.93	1930.29	467.81	1462.48	1181.71	280.78	5
48.91	2019.93	486.42	1533.52	1245.60	287.92	5
47.90	2108.92	509.94	1598.97	1308.83	290.14	5
47.90	2108.92	509.94	1598.97	1308.83	290.14	4
45.94	2307.06	566.47	1740.59	1431.12	309.48	4
43.99	2504.52	623.16	1881.36	1552.72	328.64	4
42.05	2701.31	680.46	2020.85	1673.65	347.20	4
40.12	2897.41	738.90	2158.51	1793.89	364.62	4
38.21	3092.80	799.23	2293.57	1913.42	380.15	4
36.30	3287.45	862.50	2424.95	2032.21	392.74	4
34.41	3481.32	930.35	2550.97	2150.22	400.75	4
32.53	3674.34	1005.05	2669.29	2267.39	401.90	4
30.67	3866.44	1082.60	2783.84	2383.62	400.22	4
30.67	3866.44	1082.60	2783.84	2383.62	400.22	3
29.30	4013.76	1146.11	2867.65	2469.09	398.56	3
27.94	4160.73	1208.40	2952.33	2554.20	398.13	3
26.58	4307.36	1269.76	3037.60	2638.97	398.63	3
25.23	4453.64	1330.41	3123.23	2723.39	399.84	3
23.88	4599.58	1390.58	3209.00	2807.47	401.53	3
22.54	4745.18	1450.47	3294.71	2891.22	403.49	3
21.20	4890.45	1510.27	3380.18	2974.63	405.55	3
19.87	5035.38	1570.15	3465.23	3057.70	407.54	3
18.54	5179.98	1630.25	3549.72	3140.43	409.29	3
18.54	5179.98	1630.25	3549.72	3140.43	409.29	2
16.65	5384.43	1712.80	3671.63	3258.79	412.84	2
14.76	5588.36	1800.30	3788.06	3376.62	411.44	2
12.88	5791.74	1893.45	3898.29	3493.90	404.39	2
11.01	5994.53	1993.11	4001.42	3610.59	390.83	2
9.15	6196.68	2145.21	4051.48	3726.65	324.83	2
7.30	6398.20	2300.70	4097.50	3842.07	255.43	2
5.46	6599.09	2454.88	4144.20	3956.86	187.35	2
3.63	6799.34	2606.87	4192.47	4071.01	121.46	2
1.81	6998.98	2755.72	4243.26	4184.55	58.70	2
.00	7198.02	2900.52	4297.49	4297.49	.00	2

Time = 5476. Degree of Consolidation = 57.%

Total Settlement = 2.632

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 5476. = 2.632

Settlement caused by Secondary Compression at time 5476. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.15	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.11	106.47	1
.00	1289.88	350.00	939.88	681.26	258.62	1

Time = 5476. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 5476. = .442

Settlement caused by Secondary Compression at time 5476. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.89

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	57.88	21.42	6.50	5.28	4.83	6
60.02	57.41	21.35	6.49	5.29	4.82	6
59.45	56.93	21.27	6.47	5.30	4.81	6
58.89	56.46	21.20	6.46	5.30	4.81	6
58.33	55.98	21.12	6.44	5.31	4.80	6
57.76	55.50	21.05	6.43	5.31	4.79	6
57.20	55.03	20.97	6.42	5.32	4.79	6
56.64	54.55	20.90	6.40	5.32	4.78	6
56.08	54.07	20.82	6.39	5.33	4.77	6
56.08	54.07	20.82	4.51	3.64	3.19	5
54.82	53.00	20.59	4.44	3.59	3.16	5
53.56	51.94	20.36	4.38	3.54	3.14	5
52.32	50.90	20.12	4.32	3.49	3.11	5
51.10	49.86	19.89	4.25	3.44	3.08	5
49.88	48.84	19.66	4.19	3.39	3.05	5
48.69	47.83	19.43	4.13	3.35	3.02	5
48.69	47.83	19.43	1.93	1.88	1.80	4
46.69	45.87	18.75	1.92	1.86	1.77	4
44.70	43.92	18.06	1.91	1.84	1.75	4
42.72	41.98	17.38	1.89	1.83	1.73	4
40.75	40.06	16.70	1.88	1.81	1.71	4
38.79	38.14	16.01	1.86	1.79	1.69	4
36.85	36.24	15.33	1.84	1.77	1.67	4
34.91	34.36	14.65	1.82	1.75	1.64	4
33.00	32.48	13.97	1.80	1.73	1.62	4
31.09	30.62	13.28	1.78	1.71	1.60	4
31.09	30.62	13.28	1.47	1.43	1.37	3
29.70	29.26	12.72	1.46	1.42	1.36	3
28.32	27.90	12.16	1.45	1.41	1.35	3
26.94	26.54	11.59	1.44	1.40	1.34	3

25.57	25.19	11.03	1.43	1.39	1.33	3
24.21	23.84	10.47	1.42	1.38	1.32	3
22.84	22.51	9.90	1.41	1.37	1.31	3
21.49	21.17	9.34	1.40	1.36	1.30	3
20.14	19.84	8.78	1.39	1.35	1.29	3
18.80	18.52	8.21	1.38	1.34	1.29	3
18.80	18.52	8.21	1.34	1.31	1.27	2
16.88	16.63	7.39	1.33	1.30	1.26	2
14.97	14.74	6.57	1.32	1.29	1.25	2
13.07	12.87	5.75	1.31	1.28	1.25	2
11.18	11.00	4.93	1.30	1.27	1.24	2
9.30	9.14	4.11	1.29	1.26	1.23	2
7.43	7.29	3.29	1.28	1.24	1.23	2
5.56	5.46	2.46	1.27	1.23	1.22	2
3.70	3.63	1.64	1.26	1.22	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
57.88	1289.87	402.48	887.40	681.25	206.14	6
57.41	1324.14	400.63	923.51	710.90	212.62	6
56.93	1358.43	398.78	959.65	740.57	219.08	6
56.46	1392.74	396.94	995.80	770.26	225.54	6
55.98	1427.08	395.10	1031.98	799.98	232.00	6
55.50	1461.45	393.27	1068.18	829.73	238.45	6
55.03	1495.84	391.45	1104.39	859.50	244.89	6
54.55	1530.26	389.64	1140.63	889.30	251.33	6
54.07	1564.71	387.83	1176.88	919.13	257.75	6
54.07	1564.71	387.83	1176.88	919.13	257.75	5
53.00	1657.18	408.74	1248.44	985.85	262.59	5
51.94	1748.91	429.07	1319.84	1051.83	268.01	5
50.90	1839.92	448.84	1391.09	1117.09	274.00	5
49.86	1930.24	468.02	1462.21	1181.65	280.56	5
48.84	2019.87	486.63	1533.24	1245.54	287.70	5
47.83	2108.85	510.41	1598.44	1308.76	289.68	5
47.83	2108.85	510.41	1598.44	1308.76	289.68	4
45.87	2306.97	569.12	1737.85	1431.03	306.82	4
43.92	2504.39	628.15	1876.24	1552.59	323.65	4
41.98	2701.10	687.93	2013.17	1673.44	339.73	4
40.06	2897.10	749.05	2148.05	1793.58	354.47	4
38.14	3092.35	812.33	2280.01	1912.97	367.05	4
36.24	3286.82	878.95	2407.87	2031.58	376.29	4
34.36	3480.48	950.82	2529.65	2149.38	380.27	4
32.48	3673.23	1028.33	2644.90	2266.27	378.63	4
30.62	3865.02	1107.85	2757.17	2382.21	374.96	4
30.62	3865.02	1107.85	2757.17	2382.21	374.96	3
29.26	4012.20	1173.26	2838.94	2467.53	371.42	3
27.90	4159.01	1237.21	2921.81	2552.48	369.33	3
26.54	4305.47	1299.96	3005.51	2637.08	368.43	3
25.19	4451.58	1361.76	3089.82	2721.33	368.49	3
23.84	4597.34	1422.82	3174.52	2805.23	369.29	3
22.51	4742.76	1483.37	3259.40	2888.80	370.60	3
21.17	4887.84	1543.57	3344.28	2972.02	372.26	3
19.84	5032.59	1603.61	3428.98	3054.90	374.07	3
18.52	5176.99	1663.68	3513.31	3137.45	375.86	3
18.52	5176.99	1663.68	3513.31	3137.45	375.86	2
16.63	5381.24	1746.11	3635.13	3255.60	379.53	2
14.74	5584.97	1832.97	3752.00	3373.23	378.77	2
12.87	5788.15	1924.98	3863.18	3490.31	372.86	2
11.00	5990.75	2033.42	3957.33	3606.81	350.52	2

9.14	6192.74	2182.93	4009.80	3722.70	287.10	2
7.29	6394.12	2331.37	4062.75	3837.98	224.77	2
5.46	6594.89	2478.12	4116.77	3952.66	164.11	2
3.63	6795.06	2622.40	4172.66	4066.74	105.92	2
1.81	6994.66	2763.43	4231.22	4180.23	50.99	2
.00	7193.68	2900.52	4293.15	4293.15	.00	2

Time = 6481. Degree of Consolidation = 58.%

Total Settlement = 2.701

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 6481. = 2.701

Settlement caused by Secondary Compression at time 6481. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.15	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.12	106.47	1
.00	1289.87	350.00	939.87	681.25	258.62	1

Time = 6481. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 6481. = .442

Settlement caused by Secondary Compression at time 6481. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.82

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	57.83	21.42	6.50	5.28	4.83	6
60.02	57.36	21.35	6.49	5.29	4.82	6
59.45	56.88	21.27	6.47	5.30	4.81	6
58.89	56.41	21.20	6.46	5.30	4.81	6
58.33	55.93	21.12	6.44	5.31	4.80	6
57.76	55.46	21.05	6.43	5.31	4.79	6
57.20	54.98	20.97	6.42	5.32	4.79	6
56.64	54.50	20.90	6.40	5.32	4.78	6
56.08	54.02	20.82	6.39	5.33	4.77	6
56.08	54.02	20.82	4.51	3.64	3.19	5
54.82	52.95	20.59	4.44	3.59	3.16	5
53.56	51.90	20.36	4.38	3.54	3.14	5
52.32	50.85	20.12	4.32	3.49	3.11	5
51.10	49.82	19.89	4.25	3.44	3.08	5
49.88	48.79	19.66	4.19	3.39	3.05	5
48.69	47.78	19.43	4.13	3.35	3.02	5
48.69	47.78	19.43	1.93	1.88	1.80	4
46.69	45.82	18.75	1.92	1.86	1.77	4
44.70	43.87	18.06	1.91	1.84	1.75	4
42.72	41.94	17.38	1.89	1.83	1.73	4
40.75	40.01	16.70	1.88	1.81	1.71	4
38.79	38.10	16.01	1.86	1.79	1.69	4
36.85	36.20	15.33	1.84	1.77	1.67	4
34.91	34.32	14.65	1.82	1.75	1.64	4
33.00	32.45	13.97	1.80	1.73	1.62	4
31.09	30.59	13.28	1.78	1.70	1.60	4
31.09	30.59	13.28	1.47	1.43	1.37	3
29.70	29.23	12.72	1.46	1.42	1.36	3
28.32	27.87	12.16	1.45	1.41	1.35	3
26.94	26.51	11.59	1.44	1.40	1.34	3
25.57	25.16	11.03	1.43	1.39	1.33	3
24.21	23.82	10.47	1.42	1.38	1.32	3
22.84	22.48	9.90	1.41	1.37	1.31	3
21.49	21.15	9.34	1.40	1.36	1.30	3
20.14	19.83	8.78	1.39	1.35	1.29	3
18.80	18.51	8.21	1.38	1.34	1.29	3
18.80	18.51	8.21	1.34	1.31	1.27	2
16.88	16.61	7.39	1.33	1.30	1.26	2
14.97	14.73	6.57	1.32	1.29	1.25	2
13.07	12.86	5.75	1.31	1.28	1.25	2
11.18	10.99	4.93	1.30	1.26	1.24	2
9.30	9.14	4.11	1.29	1.25	1.23	2
7.43	7.29	3.29	1.28	1.24	1.23	2
5.56	5.45	2.46	1.27	1.23	1.22	2
3.70	3.63	1.64	1.26	1.22	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
57.83	1289.87	402.57	887.30	681.25	206.05	6
57.36	1324.13	400.73	923.41	710.89	212.51	6
56.88	1358.42	398.89	959.53	740.56	218.97	6
56.41	1392.74	397.05	995.68	770.25	225.43	6
55.93	1427.08	395.22	1031.85	799.97	231.88	6
55.46	1461.44	393.40	1068.04	829.72	238.32	6
54.98	1495.83	391.58	1104.25	859.49	244.76	6

54.50	1530.25	389.77	1140.48	889.29	251.19	6
54.02	1564.69	387.97	1176.73	919.11	257.62	6
54.02	1564.69	387.97	1176.73	919.11	257.62	5
52.95	1657.16	408.87	1248.29	985.83	262.46	5
51.90	1748.89	429.21	1319.67	1051.80	267.87	5
50.85	1839.89	448.97	1390.92	1117.06	273.86	5
49.82	1930.20	468.16	1462.04	1181.62	280.42	5
48.79	2019.83	486.77	1533.07	1245.50	287.57	5
47.78	2108.80	510.71	1598.09	1308.72	289.37	5
47.78	2108.80	510.71	1598.09	1308.72	289.37	4
45.82	2306.91	570.89	1736.02	1430.97	305.05	4
43.87	2504.30	631.48	1872.82	1552.50	320.32	4
41.94	2700.97	692.94	2008.02	1673.31	334.72	4
40.01	2896.89	755.90	2140.99	1793.37	347.62	4
38.10	3092.04	821.21	2270.83	1912.67	358.16	4
36.20	3286.40	890.20	2396.20	2031.16	365.04	4
34.32	3479.90	964.98	2514.93	2148.81	366.12	4
32.45	3672.47	1044.48	2628.00	2265.52	362.48	4
30.59	3864.06	1125.36	2738.70	2381.24	357.46	4
30.59	3864.06	1125.36	2738.70	2381.24	357.46	3
29.23	4011.13	1192.06	2819.07	2466.46	352.62	3
27.87	4157.84	1257.14	2900.69	2551.30	349.39	3
26.51	4304.18	1320.89	2983.29	2635.79	347.51	3
25.16	4450.17	1383.51	3066.66	2719.92	346.74	3
23.82	4595.81	1445.25	3150.55	2803.70	346.85	3
22.48	4741.10	1506.31	3234.79	2887.13	347.66	3
21.15	4886.05	1566.87	3319.18	2970.22	348.95	3
19.83	5030.66	1627.14	3403.52	3052.98	350.55	3
18.51	5174.93	1687.28	3487.66	3135.39	352.27	3
18.51	5174.93	1687.28	3487.66	3135.39	352.27	2
16.61	5379.04	1769.83	3609.21	3253.40	355.81	2
14.73	5582.62	1856.38	3726.24	3370.88	355.35	2
12.86	5785.66	1947.68	3837.98	3487.82	350.15	2
10.99	5988.12	2064.72	3923.41	3604.19	319.22	2
9.14	6189.99	2209.63	3980.37	3719.96	260.41	2
7.29	6391.27	2353.07	4038.20	3835.14	203.06	2
5.45	6591.97	2494.53	4097.44	3949.74	147.70	2
3.63	6792.09	2633.38	4158.70	4063.76	94.95	2
1.81	6991.64	2768.92	4222.72	4177.22	45.50	2
.00	7190.65	2900.52	4290.13	4290.13	.00	2

Time = 7301. Degree of Consolidation = 59.%

Total Settlement = 2.750

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 7301. = 2.750

Settlement caused by Secondary Compression at time 7301. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1

5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.15	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.12	106.47	1
.00	1289.87	350.00	939.87	681.25	258.62	1

Time = 7301. Degree of Consolidation = 100.%

Total Settlement = .442

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 7301. = .442

Settlement caused by Secondary Compression at time 7301. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.77

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	57.75	21.42	6.50	5.28	4.83	6
60.02	57.27	21.35	6.49	5.29	4.82	6
59.45	56.80	21.27	6.47	5.29	4.81	6
58.89	56.32	21.20	6.46	5.30	4.81	6
58.33	55.85	21.12	6.44	5.31	4.80	6
57.76	55.37	21.05	6.43	5.31	4.79	6
57.20	54.89	20.97	6.42	5.32	4.79	6
56.64	54.41	20.90	6.40	5.32	4.78	6
56.08	53.94	20.82	6.39	5.33	4.77	6
56.08	53.94	20.82	4.51	3.64	3.19	5
54.82	52.87	20.59	4.44	3.59	3.16	5
53.56	51.81	20.36	4.38	3.54	3.14	5
52.32	50.76	20.12	4.32	3.49	3.11	5
51.10	49.73	19.89	4.25	3.44	3.08	5
49.88	48.71	19.66	4.19	3.39	3.05	5
48.69	47.69	19.43	4.13	3.35	3.02	5
48.69	47.69	19.43	1.93	1.88	1.80	4
46.69	45.73	18.75	1.92	1.86	1.77	4
44.70	43.79	18.06	1.91	1.84	1.75	4
42.72	41.85	17.38	1.89	1.82	1.73	4
40.75	39.93	16.70	1.88	1.81	1.71	4
38.79	38.02	16.01	1.86	1.79	1.69	4
36.85	36.13	15.33	1.84	1.77	1.67	4
34.91	34.25	14.65	1.82	1.74	1.64	4
33.00	32.38	13.97	1.80	1.72	1.62	4

31.09	30.53	13.28	1.78	1.69	1.60	4
31.09	30.53	13.28	1.47	1.42	1.37	3
29.70	29.17	12.72	1.46	1.41	1.36	3
28.32	27.81	12.16	1.45	1.40	1.35	3
26.94	26.46	11.59	1.44	1.39	1.34	3
25.57	25.12	11.03	1.43	1.38	1.33	3
24.21	23.78	10.47	1.42	1.37	1.32	3
22.84	22.44	9.90	1.41	1.36	1.31	3
21.49	21.12	9.34	1.40	1.35	1.30	3
20.14	19.79	8.78	1.39	1.34	1.29	3
18.80	18.48	8.21	1.38	1.33	1.29	3
18.80	18.48	8.21	1.34	1.30	1.27	2
16.88	16.59	7.39	1.33	1.29	1.26	2
14.97	14.71	6.57	1.32	1.28	1.25	2
13.07	12.84	5.75	1.31	1.27	1.25	2
11.18	10.98	4.93	1.30	1.26	1.24	2
9.30	9.13	4.11	1.29	1.25	1.23	2
7.43	7.29	3.29	1.28	1.24	1.23	2
5.56	5.45	2.46	1.27	1.23	1.22	2
3.70	3.63	1.64	1.26	1.22	1.21	2
1.85	1.81	.82	1.25	1.21	1.20	2
.00	.00	.00	1.25	1.20	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
57.75	1289.87	402.71	887.16	681.25	205.91	6
57.27	1324.13	400.88	923.25	710.89	212.37	6
56.80	1358.41	399.04	959.37	740.55	218.82	6
56.32	1392.73	397.22	995.51	770.24	225.26	6
55.85	1427.06	395.40	1031.67	799.96	231.70	6
55.37	1461.43	393.58	1067.84	829.70	238.14	6
54.89	1495.82	391.77	1104.04	859.47	244.57	6
54.41	1530.23	389.97	1140.26	889.27	250.99	6
53.94	1564.67	388.17	1176.50	919.09	257.41	6
53.94	1564.67	388.17	1176.50	919.09	257.41	5
52.87	1657.13	409.09	1248.04	985.80	262.25	5
51.81	1748.85	429.43	1319.42	1051.76	267.66	5
50.76	1839.85	449.19	1390.65	1117.01	273.64	5
49.73	1930.15	468.38	1461.77	1181.56	280.20	5
48.71	2019.77	486.99	1532.78	1245.44	287.34	5
47.69	2108.73	511.22	1597.51	1308.65	288.86	5
47.69	2108.73	511.22	1597.51	1308.65	288.86	4
45.73	2306.82	573.89	1732.93	1430.88	302.05	4
43.79	2504.16	637.15	1867.01	1552.36	314.66	4
41.85	2700.74	701.50	1999.23	1673.08	326.16	4
39.93	2896.54	767.66	2128.88	1793.02	335.86	4
38.02	3091.53	836.60	2254.94	1912.16	342.78	4
36.13	3285.68	909.84	2375.84	2030.45	345.40	4
34.25	3478.92	990.06	2488.86	2147.82	341.04	4
32.38	3671.16	1073.32	2597.84	2264.20	333.63	4
30.53	3862.37	1156.68	2705.68	2379.55	326.13	4
30.53	3862.37	1156.68	2705.68	2379.55	326.13	3
29.17	4009.26	1225.68	2783.58	2464.59	319.00	3
27.81	4155.77	1292.81	2862.96	2549.24	313.72	3
26.46	4301.91	1358.35	2943.56	2633.52	310.04	3
25.12	4447.68	1422.52	3025.16	2717.43	307.73	3
23.78	4593.10	1485.54	3107.56	2800.99	306.57	3
22.44	4738.16	1547.60	3190.56	2884.19	306.37	3
21.12	4882.88	1608.90	3273.98	2967.05	306.93	3
19.79	5027.25	1669.62	3357.63	3049.56	308.07	3
18.48	5171.28	1729.95	3441.33	3131.74	309.59	3

18.48	5171.28	1729.95	3441.33	3131.74	309.59	2
16.59	5375.12	1812.86	3562.26	3249.48	312.78	2
14.71	5578.44	1899.00	3679.45	3366.70	312.74	2
12.84	5781.22	1989.06	3792.16	3483.39	308.77	2
10.98	5983.44	2121.63	3861.81	3599.50	262.31	2
9.13	6185.09	2258.26	3926.83	3715.06	211.77	2
7.29	6386.19	2392.65	3993.54	3830.06	163.48	2
5.45	6586.74	2524.49	4062.25	3944.51	117.74	2
3.63	6786.76	2653.33	4133.43	4058.43	75.00	2
1.81	6986.26	2778.81	4207.45	4171.83	35.62	2
.00	7185.25	2900.52	4284.72	4284.72	.00	2

Time = 9126. Degree of Consolidation = 61.%

Total Settlement = 2.836

Settlement at End of Primary Consolidation = 4.642

Settlement caused by Primary Consolidation at time 9126. = 2.836

Settlement caused by Secondary Compression at time 9126. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
11.36	10.92	5.74	.98	.98	.98	1
8.52	8.15	4.30	.98	.90	.90	1
5.68	5.42	2.87	.98	.89	.89	1
2.84	2.71	1.43	.98	.89	.89	1
.00	.00	.00	.98	.89	.89	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
10.92	.00	.00	.00	.00	.00	1
8.15	325.15	152.15	172.99	172.99	.00	1
5.42	647.17	304.31	342.86	342.86	.00	1
2.71	968.58	350.00	618.58	512.12	106.47	1
.00	1289.87	350.00	939.87	681.25	258.62	1

Time = 9126. Degree of Consolidation = 100.%

Total Settlement = .443

Settlement at End of Primary Consolidation = .442

Settlement caused by Primary Consolidation at time 9126. = .442

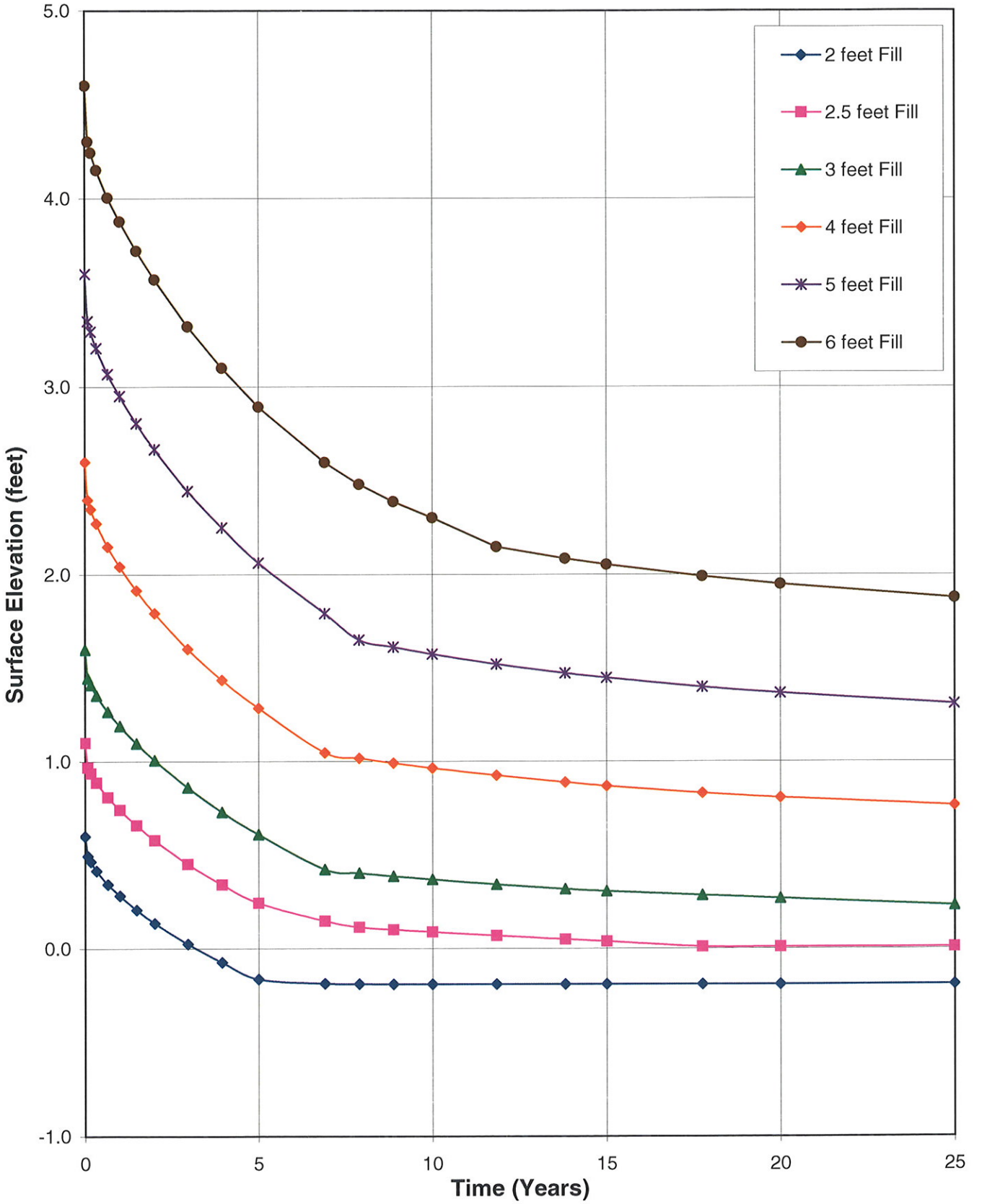
Settlement caused by Secondary Compression at time 9126. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 6.68

Figure No. 6

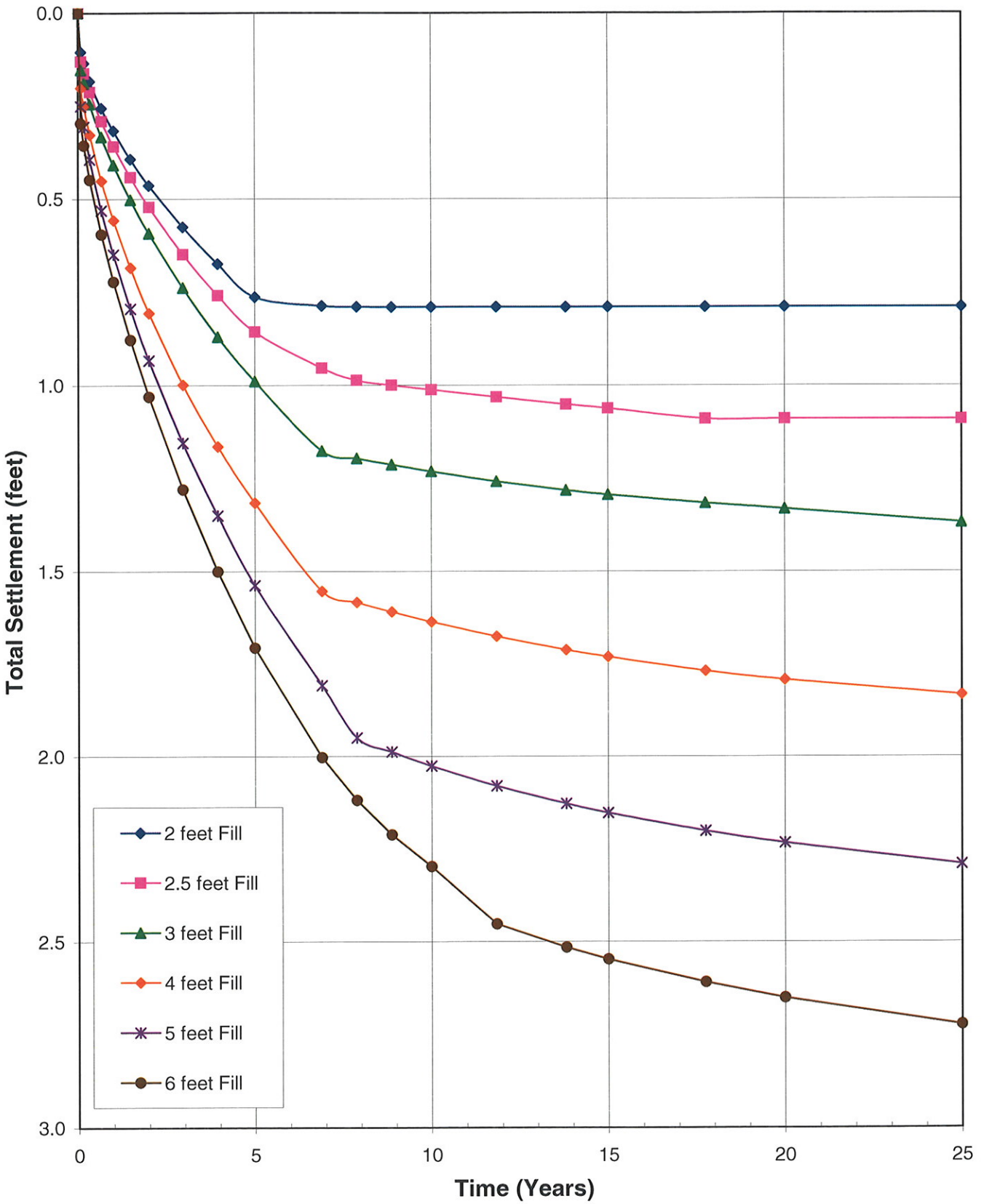
Surface Elevation due to Actual Dredged Fill Height from PSDDF



URS CORP.

Figure No. 7

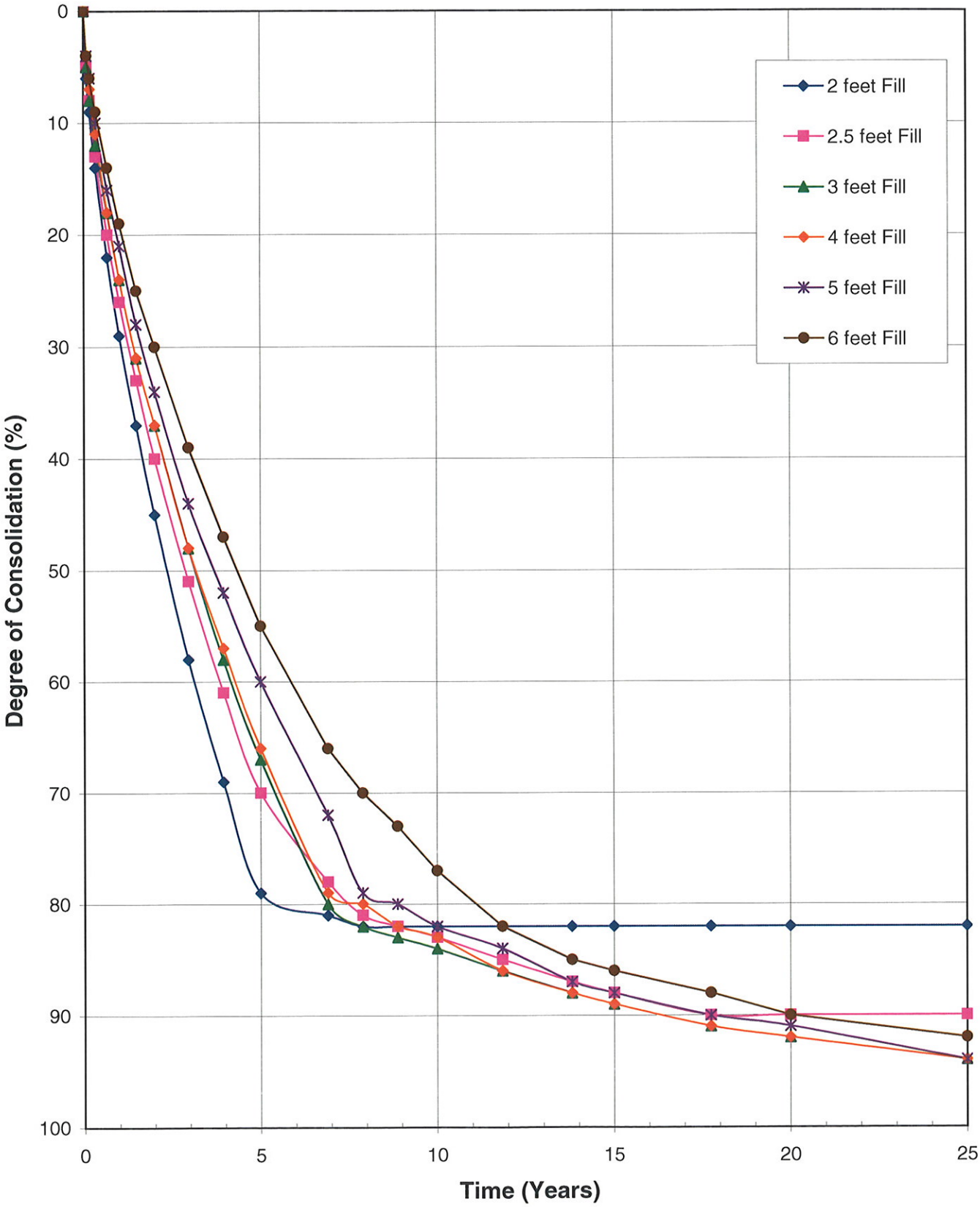
Total Settlement due to Actual Dredged Fill Height from PSDDF



URS CORP.

Figure No. 8

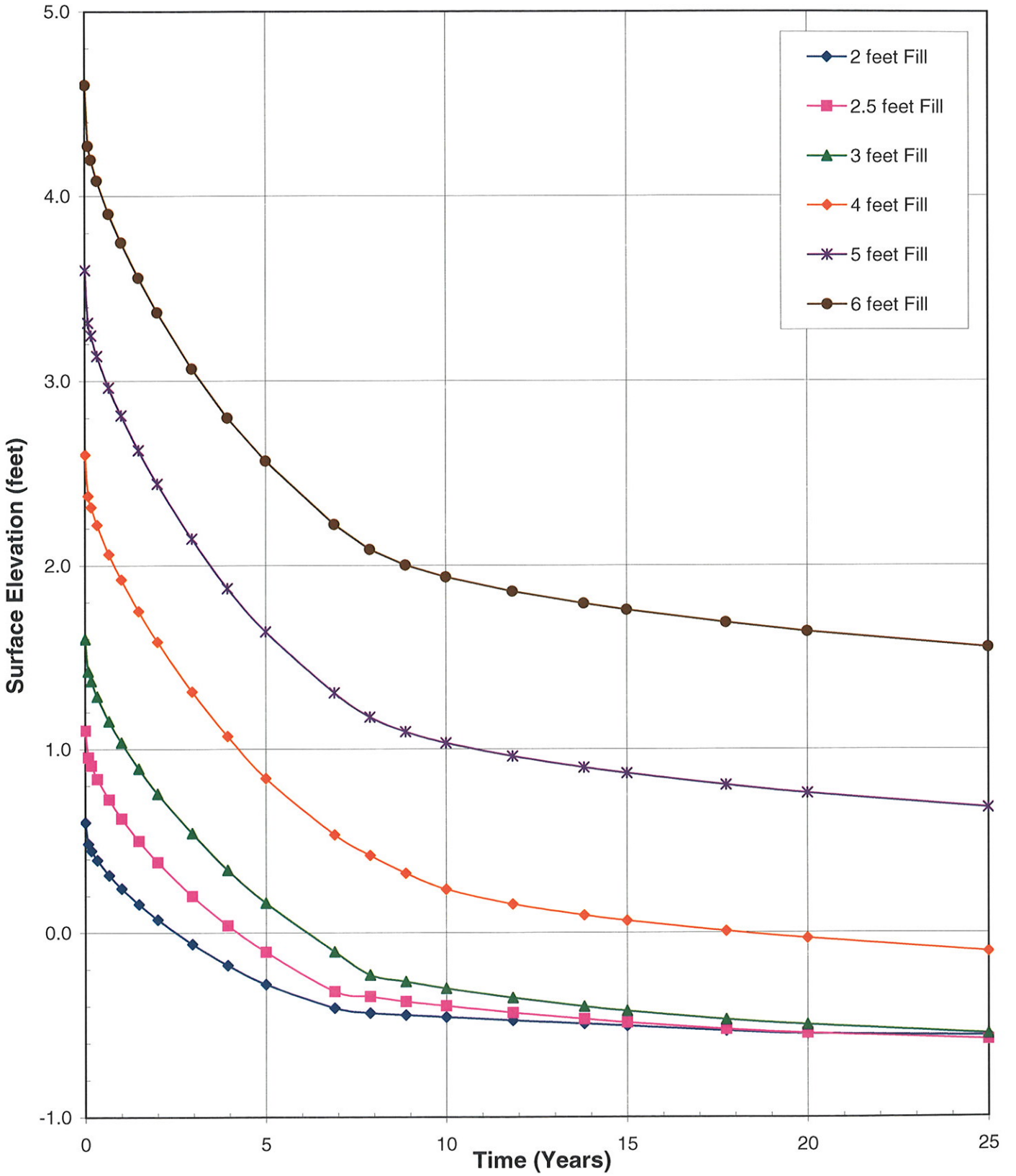
Degree of Consolidation of Compressible Layers due to Actual Dredged Fill Height from PSDDF



URS CORP.

Figure No. 9

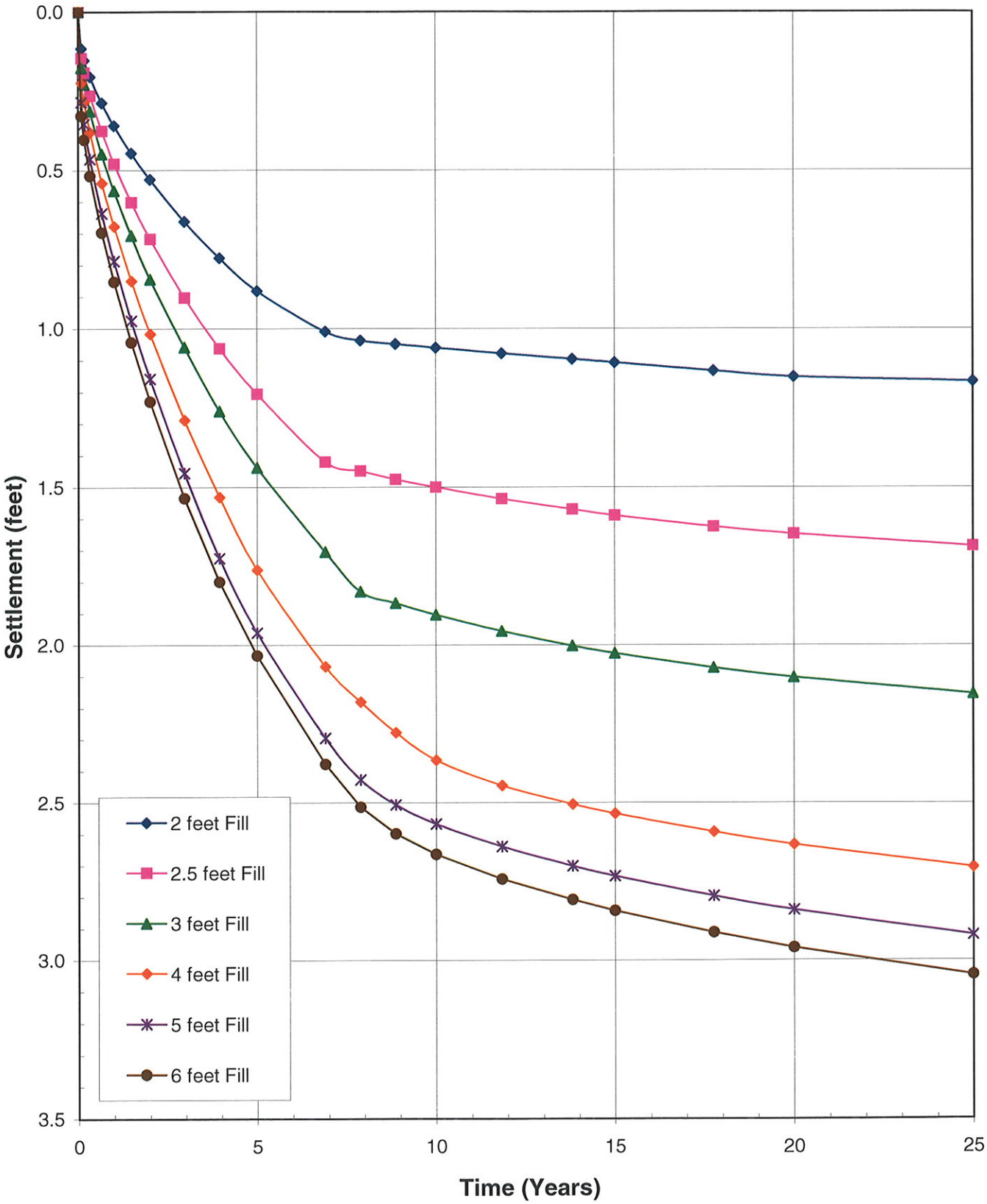
Surface Elevation due to Equivalent Dredged Fill Height from PSDDF



URS CORP.

Figure No. 10

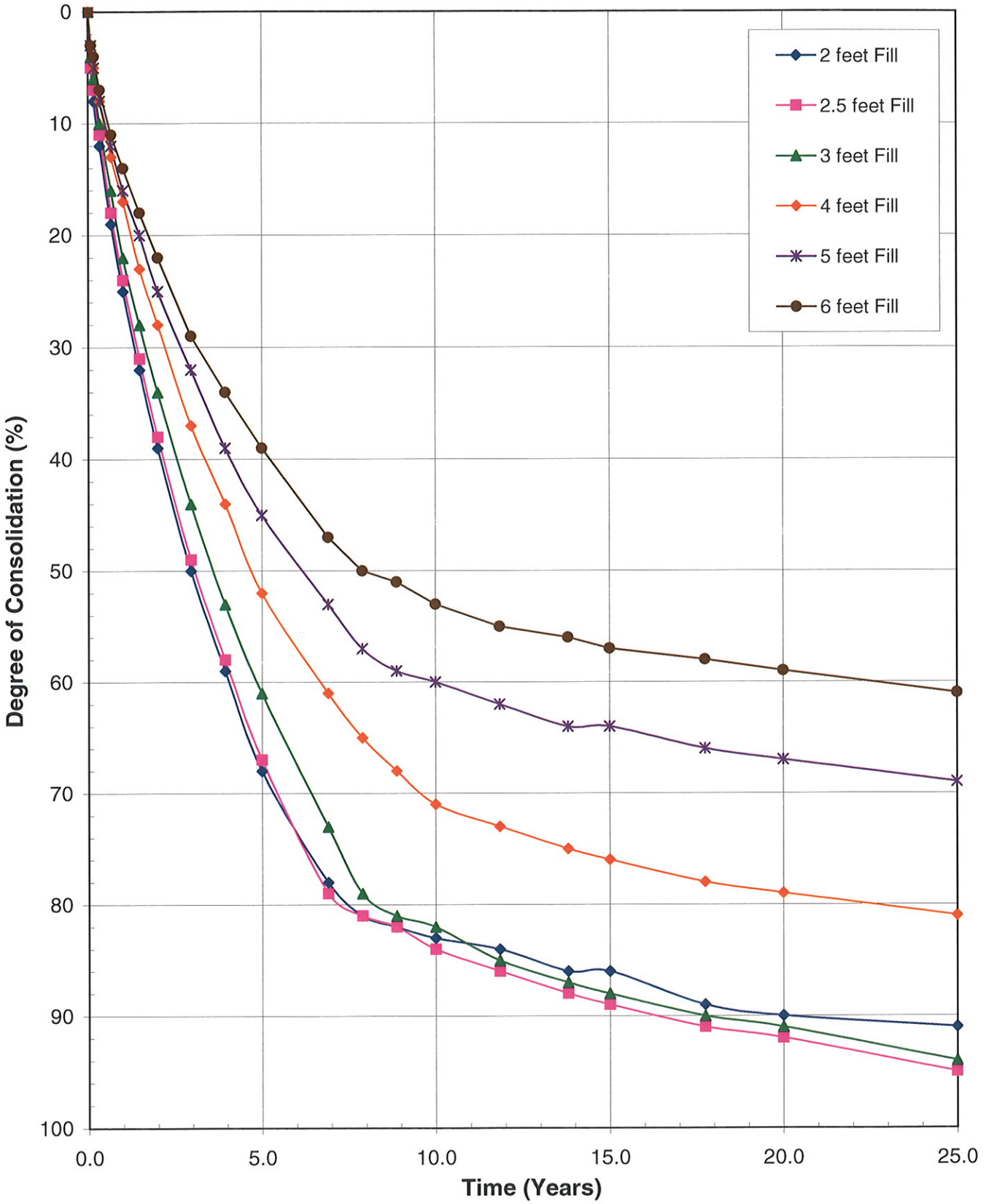
Total Settlement due to Equivalent Dredged Fill Height from PSDDF



URS CORP.

Figure No. 11

Degree of Consolidation of Compressible Layers due to Equivalent Dredged Fill Height from PSDDF



URS CORP.

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou Dupont - 2.5ft Fill Height

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	2.5	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.433E-01	.570	.30000E-03	z = .06

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	6.10	6
60.02	60.02	21.35	6.49	6.49	6.08	6
59.45	59.45	21.27	6.47	6.47	6.07	6
58.89	58.89	21.20	6.46	6.46	6.05	6

58.33	58.33	21.12	6.44	6.44	6.04	6
57.76	57.76	21.05	6.43	6.43	6.03	6
57.20	57.20	20.97	6.42	6.42	6.01	6
56.64	56.64	20.90	6.40	6.40	6.00	6
56.08	56.08	20.82	6.39	6.39	5.98	6
56.08	56.08	20.82	4.51	4.51	4.18	5
54.82	54.82	20.59	4.44	4.44	4.11	5
53.56	53.56	20.36	4.38	4.38	4.05	5
52.32	52.32	20.12	4.32	4.32	3.98	5
51.10	51.10	19.89	4.25	4.25	3.92	5
49.88	49.88	19.66	4.19	4.19	3.86	5
48.69	48.69	19.43	4.13	4.13	3.79	5
48.69	48.69	19.43	1.93	1.93	1.91	4
46.69	46.69	18.75	1.92	1.92	1.90	4
44.70	44.70	18.06	1.91	1.91	1.88	4
42.72	42.72	17.38	1.89	1.89	1.87	4
40.75	40.75	16.70	1.88	1.88	1.84	4
38.79	38.79	16.01	1.86	1.86	1.82	4
36.85	36.85	15.33	1.84	1.84	1.80	4
34.91	34.91	14.65	1.82	1.82	1.78	4
33.00	33.00	13.97	1.80	1.80	1.76	4
31.09	31.09	13.28	1.78	1.78	1.74	4
31.09	31.09	13.28	1.47	1.47	1.45	3
29.70	29.70	12.72	1.46	1.46	1.44	3
28.32	28.32	12.16	1.45	1.45	1.43	3
26.94	26.94	11.59	1.44	1.44	1.42	3
25.57	25.57	11.03	1.43	1.43	1.41	3
24.21	24.21	10.47	1.42	1.42	1.40	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.49	9.34	1.40	1.40	1.38	3
20.14	20.14	8.78	1.39	1.39	1.37	3
18.80	18.80	8.21	1.38	1.38	1.36	3
18.80	18.80	8.21	1.34	1.34	1.32	2
16.88	16.88	7.39	1.33	1.33	1.31	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.30	4.11	1.29	1.29	1.27	2
7.43	7.43	3.29	1.28	1.28	1.26	2
5.56	5.56	2.46	1.27	1.27	1.26	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.85	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.25	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	289.94	.00	289.94	156.00	133.94	6
60.02	329.89	4.62	325.27	191.33	133.94	6
59.45	369.77	9.24	360.53	226.59	133.94	6
58.89	409.58	13.86	395.72	261.78	133.94	6
58.33	449.33	18.48	430.85	296.91	133.94	6
57.76	489.02	23.10	465.92	331.98	133.94	6
57.20	528.64	27.72	500.92	366.98	133.94	6
56.64	568.19	32.34	535.85	401.91	133.94	6
56.08	607.68	36.96	570.71	436.77	133.94	6
56.08	607.68	36.96	570.71	436.77	133.94	5
54.82	712.65	62.71	649.94	516.00	133.94	5
53.56	816.70	88.46	728.24	594.30	133.94	5
52.32	919.82	114.21	805.61	671.67	133.94	5
51.10	1022.03	139.96	882.06	748.12	133.94	5
49.88	1123.30	165.71	957.59	823.65	133.94	5

48.69	1223.66	191.46	1032.20	898.26	133.94	5
48.69	1223.66	191.46	1032.20	898.26	133.94	4
46.69	1424.10	267.32	1156.78	1022.84	133.94	4
44.70	1624.04	343.18	1280.86	1146.92	133.94	4
42.72	1823.44	419.04	1404.40	1270.46	133.94	4
40.75	2022.38	494.90	1527.48	1393.54	133.94	4
38.79	2220.58	570.76	1649.82	1515.88	133.94	4
36.85	2417.88	646.62	1771.26	1637.32	133.94	4
34.91	2614.27	722.48	1891.80	1757.86	133.94	4
33.00	2809.77	798.34	2011.43	1877.49	133.94	4
31.09	3004.35	874.19	2130.16	1996.22	133.94	4
31.09	3004.35	874.19	2130.16	1996.22	133.94	3
29.70	3152.92	936.05	2216.87	2082.93	133.94	3
28.32	3301.09	997.91	2303.18	2169.24	133.94	3
26.94	3448.90	1059.77	2389.13	2255.19	133.94	3
25.57	3596.36	1121.63	2474.73	2340.79	133.94	3
24.21	3743.47	1183.49	2559.98	2426.04	133.94	3
22.84	3890.23	1245.35	2644.88	2510.94	133.94	3
21.49	4036.65	1307.21	2729.44	2595.50	133.94	3
20.14	4182.71	1369.06	2813.65	2679.71	133.94	3
18.80	4328.43	1430.92	2897.51	2763.57	133.94	3
18.80	4328.43	1430.92	2897.51	2763.57	133.94	2
16.88	4534.10	1517.02	3017.08	2883.14	133.94	2
14.97	4739.24	1603.12	3136.12	3002.18	133.94	2
13.07	4943.85	1689.22	3254.63	3120.69	133.94	2
11.18	5147.93	1775.31	3372.61	3238.67	133.94	2
9.30	5351.48	1861.41	3490.07	3356.13	133.94	2
7.43	5554.50	1947.51	3606.99	3473.05	133.94	2
5.56	5757.00	2033.61	3723.40	3589.46	133.94	2
3.70	5959.12	2119.71	3839.42	3705.48	133.94	2
1.85	6160.89	2205.80	3955.08	3821.14	133.94	2
.00	6362.30	2291.90	4070.40	3936.46	133.94	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.50	1.26	.98	.98	.98	1
1.88	1.88	.95	.98	.98	.93	1
1.25	1.25	.63	.98	.98	.92	1
.63	.63	.32	.98	.98	.91	1
.00	.00	.00	.98	.98	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

2.50	.00	.00	.00	.00	.00	1
1.88	72.48	.00	72.48	39.00	33.48	1
1.25	144.97	.00	144.97	78.00	66.97	1
.63	217.45	.00	217.45	117.00	100.45	1
.00	289.94	.00	289.94	156.00	133.94	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.52	21.42	6.50	6.18	6.10	6
60.02	59.98	21.35	6.49	6.26	6.08	6
59.45	59.43	21.27	6.47	6.33	6.07	6
58.89	58.87	21.20	6.46	6.38	6.05	6
58.33	58.31	21.12	6.44	6.41	6.04	6
57.76	57.75	21.05	6.43	6.41	6.03	6
57.20	57.19	20.97	6.42	6.41	6.01	6
56.64	56.63	20.90	6.40	6.40	6.00	6
56.08	56.07	20.82	6.39	6.39	5.98	6
56.08	56.07	20.82	4.51	4.51	4.18	5
54.82	54.80	20.59	4.44	4.44	4.11	5
53.56	53.55	20.36	4.38	4.38	4.05	5
52.32	52.31	20.12	4.32	4.31	3.98	5
51.10	51.09	19.89	4.25	4.25	3.92	5
49.88	49.88	19.66	4.19	4.19	3.86	5
48.69	48.68	19.43	4.13	4.12	3.79	5
48.69	48.68	19.43	1.93	1.93	1.91	4
46.69	46.68	18.75	1.92	1.92	1.90	4
44.70	44.70	18.06	1.91	1.91	1.88	4
42.72	42.72	17.38	1.89	1.89	1.87	4
40.75	40.74	16.70	1.88	1.88	1.84	4
38.79	38.79	16.01	1.86	1.86	1.82	4
36.85	36.84	15.33	1.84	1.84	1.80	4
34.91	34.91	14.65	1.82	1.82	1.78	4
33.00	32.99	13.97	1.80	1.80	1.76	4
31.09	31.09	13.28	1.78	1.78	1.74	4
31.09	31.09	13.28	1.47	1.47	1.45	3
29.70	29.70	12.72	1.46	1.46	1.44	3
28.32	28.32	12.16	1.45	1.45	1.43	3
26.94	26.94	11.59	1.44	1.44	1.42	3
25.57	25.57	11.03	1.43	1.43	1.41	3
24.21	24.20	10.47	1.42	1.42	1.40	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.14	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3
18.80	18.79	8.21	1.34	1.34	1.32	2

16.88	16.88	7.39	1.33	1.33	1.31	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.30	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.56	2.46	1.27	1.27	1.26	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.52	285.65	106.99	178.66	151.71	26.95	6
59.98	324.32	78.03	246.28	185.76	60.53	6
59.43	363.36	54.70	308.66	220.18	88.48	6
58.87	402.68	39.16	363.52	254.88	108.64	6
58.31	442.17	31.16	411.01	289.75	121.26	6
57.75	481.73	28.89	452.84	324.69	128.15	6
57.19	521.29	30.24	491.05	359.63	131.42	6
56.63	560.82	33.58	527.24	394.54	132.70	6
56.07	600.29	37.97	562.33	429.39	132.94	6
56.07	600.29	37.97	562.33	429.39	132.94	5
54.80	705.23	63.58	641.66	508.58	133.07	5
53.55	809.25	89.35	719.91	586.85	133.06	5
52.31	912.34	115.13	797.21	664.19	133.02	5
51.09	1014.51	140.90	873.62	740.61	133.01	5
49.88	1115.76	166.62	949.14	816.11	133.03	5
48.68	1216.08	192.28	1023.80	890.68	133.12	5
48.68	1216.08	192.28	1023.80	890.68	133.12	4
46.68	1416.52	267.32	1149.20	1015.26	133.94	4
44.70	1616.44	343.18	1273.26	1139.32	133.94	4
42.72	1815.85	421.71	1394.14	1262.87	131.27	4
40.74	2014.68	507.72	1506.96	1385.84	121.12	4
38.79	2212.81	573.57	1639.24	1508.11	131.13	4
36.84	2410.09	646.64	1763.45	1629.54	133.91	4
34.91	2606.49	722.48	1884.01	1750.07	133.94	4
32.99	2801.98	798.34	2003.64	1869.70	133.94	4
31.09	2996.56	874.19	2122.37	1988.43	133.94	4
31.09	2996.56	874.20	2122.37	1988.43	133.94	3
29.70	3145.14	936.05	2209.08	2075.14	133.94	3
28.32	3293.31	997.91	2295.40	2161.46	133.94	3
26.94	3441.11	1060.93	2380.18	2247.40	132.78	3
25.57	3588.56	1123.18	2465.38	2332.99	132.39	3
24.20	3735.66	1185.04	2550.62	2418.24	132.39	3
22.84	3882.42	1246.90	2635.52	2503.13	132.39	3
21.48	4028.82	1308.57	2720.26	2587.68	132.58	3
20.14	4174.88	1370.12	2804.77	2671.88	132.89	3
18.79	4320.60	1431.63	2888.97	2755.74	133.23	3
18.79	4320.60	1431.63	2888.97	2755.74	133.23	2
16.88	4526.27	1517.02	3009.25	2875.31	133.94	2
14.97	4731.40	1603.12	3128.29	2994.35	133.94	2
13.07	4936.01	1689.22	3246.80	3112.86	133.94	2
11.18	5140.09	1775.31	3364.78	3230.84	133.94	2
9.30	5343.65	1861.41	3482.23	3348.29	133.94	2
7.42	5546.66	1947.51	3599.15	3465.21	133.94	2
5.56	5749.18	2033.61	3715.57	3581.63	133.94	2
3.70	5951.29	2122.02	3829.26	3697.64	131.63	2
1.84	6153.02	2226.39	3926.63	3813.28	113.35	2
.00	6354.17	2424.91	3929.26	3928.32	.94	2

Time = 30. Degree of Consolidation = 5.%

Total Settlement = .062

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 30. = .062

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.82	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.82	71.90	27.86	44.04	38.41	5.63	1
1.21	143.30	52.97	90.33	76.33	14.00	1
.60	214.52	83.62	130.90	114.07	16.83	1
.00	285.65	106.99	178.66	151.71	26.94	1

Time = 30. Degree of Consolidation = 95.%

Total Settlement = .069

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 30. = .069

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = .97

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.49	21.42	6.50	6.16	6.10	6
60.02	59.95	21.35	6.49	6.23	6.08	6
59.45	59.40	21.27	6.47	6.28	6.07	6
58.89	58.85	21.20	6.46	6.32	6.05	6
58.33	58.29	21.12	6.44	6.35	6.04	6

57.76	57.74	21.05	6.43	6.37	6.03	6
57.20	57.18	20.97	6.42	6.38	6.01	6
56.64	56.62	20.90	6.40	6.38	6.00	6
56.08	56.06	20.82	6.39	6.38	5.98	6
56.08	56.06	20.82	4.51	4.50	4.18	5
54.82	54.80	20.59	4.44	4.44	4.11	5
53.56	53.54	20.36	4.38	4.38	4.05	5
52.32	52.30	20.12	4.32	4.31	3.98	5
51.10	51.08	19.89	4.25	4.25	3.92	5
49.88	49.87	19.66	4.19	4.18	3.86	5
48.69	48.68	19.43	4.13	4.12	3.79	5
48.69	48.68	19.43	1.93	1.93	1.91	4
46.69	46.68	18.75	1.92	1.92	1.90	4
44.70	44.69	18.06	1.91	1.91	1.88	4
42.72	42.71	17.38	1.89	1.89	1.87	4
40.75	40.74	16.70	1.88	1.88	1.84	4
38.79	38.78	16.01	1.86	1.86	1.82	4
36.85	36.84	15.33	1.84	1.84	1.80	4
34.91	34.91	14.65	1.82	1.82	1.78	4
33.00	32.99	13.97	1.80	1.80	1.76	4
31.09	31.09	13.28	1.78	1.78	1.74	4
31.09	31.09	13.28	1.47	1.47	1.45	3
29.70	29.70	12.72	1.46	1.46	1.44	3
28.32	28.31	12.16	1.45	1.45	1.43	3
26.94	26.94	11.59	1.44	1.44	1.42	3
25.57	25.56	11.03	1.43	1.43	1.41	3
24.21	24.20	10.47	1.42	1.42	1.40	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3
18.80	18.79	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.49	285.64	111.06	174.58	151.70	22.88	6
59.95	324.18	90.89	233.29	185.62	47.67	6
59.40	363.00	72.95	290.05	219.82	70.23	6
58.85	402.05	58.48	343.57	254.25	89.32	6
58.29	441.27	48.10	393.17	288.85	104.32	6
57.74	480.62	41.82	438.80	323.58	115.23	6
57.18	520.03	39.11	480.92	358.36	122.55	6
56.62	559.45	39.21	520.24	393.17	127.07	6
56.06	598.86	41.30	557.56	427.96	129.60	6
56.06	598.86	41.30	557.56	427.96	129.60	5
54.80	703.71	65.56	638.15	507.06	131.09	5
53.54	807.67	90.67	717.00	585.27	131.74	5
52.30	910.72	116.17	794.55	662.57	131.99	5
51.08	1012.85	141.80	871.05	738.95	132.10	5
49.87	1114.07	167.45	946.62	814.42	132.20	5
48.68	1214.36	193.03	1021.34	888.96	132.38	5

48.68	1214.36	193.03	1021.34	888.96	132.38	4
46.68	1414.80	267.32	1147.48	1013.54	133.94	4
44.69	1614.73	343.56	1271.17	1137.61	133.56	4
42.71	1814.11	426.38	1387.74	1261.13	126.60	4
40.74	2012.90	512.79	1500.11	1384.06	116.05	4
38.78	2210.97	577.01	1633.96	1506.27	127.69	4
36.84	2408.23	647.54	1760.69	1627.67	133.01	4
34.91	2604.62	722.48	1882.15	1748.21	133.94	4
32.99	2800.11	798.34	2001.78	1867.84	133.94	4
31.09	2994.70	874.19	2120.50	1986.56	133.94	4
31.09	2994.70	874.20	2120.50	1986.56	133.94	3
29.70	3143.27	936.05	2207.21	2073.27	133.94	3
28.31	3291.44	997.91	2293.53	2159.59	133.94	3
26.94	3439.24	1061.83	2377.42	2245.53	131.88	3
25.56	3586.69	1124.50	2462.18	2331.12	131.06	3
24.20	3733.78	1186.59	2547.19	2416.35	130.84	3
22.84	3880.53	1248.33	2632.19	2501.24	130.96	3
21.48	4026.92	1309.80	2717.13	2585.78	131.35	3
20.13	4172.98	1371.15	2801.83	2669.98	131.86	3
18.79	4318.69	1432.42	2886.27	2753.83	132.44	3
18.79	4318.69	1432.42	2886.27	2753.83	132.44	2
16.87	4524.35	1517.32	3007.03	2873.39	133.64	2
14.97	4729.49	1603.12	3126.37	2992.43	133.94	2
13.07	4934.10	1689.22	3244.88	3110.94	133.94	2
11.18	5138.18	1775.31	3362.86	3228.92	133.94	2
9.29	5341.73	1861.41	3480.32	3346.38	133.94	2
7.42	5544.75	1947.51	3597.24	3463.30	133.94	2
5.55	5747.26	2033.61	3713.65	3579.71	133.94	2
3.70	5949.36	2126.47	3822.90	3695.72	127.18	2
1.84	6151.06	2241.75	3909.31	3811.31	97.99	2
.00	6352.16	2425.03	3927.12	3926.31	.81	2

Time = 60. Degree of Consolidation = 8.%

Total Settlement = .094

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 60. = .094

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.50	2.43	1.26
1.88	1.82	.95
1.25	1.21	.63
.63	.60	.32
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
2.43	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

1.82	71.90	27.96	43.94	38.41	5.53	1
1.21	143.29	53.95	89.34	76.32	13.01	1
.60	214.51	85.19	129.32	114.06	15.26	1
.00	285.64	111.06	174.58	151.70	22.88	1

Time = 60. Degree of Consolidation = 95.%

Total Settlement = .069

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 60. = .069

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = .94

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.44	21.42	6.50	6.15	6.10	6
60.02	59.90	21.35	6.49	6.19	6.08	6
59.45	59.35	21.27	6.47	6.23	6.07	6
58.89	58.81	21.20	6.46	6.27	6.05	6
58.33	58.26	21.12	6.44	6.29	6.04	6
57.76	57.70	21.05	6.43	6.32	6.03	6
57.20	57.15	20.97	6.42	6.33	6.01	6
56.64	56.60	20.90	6.40	6.34	6.00	6
56.08	56.04	20.82	6.39	6.35	5.98	6
56.08	56.04	20.82	4.51	4.48	4.18	5
54.82	54.78	20.59	4.44	4.42	4.11	5
53.56	53.53	20.36	4.38	4.36	4.05	5
52.32	52.29	20.12	4.32	4.30	3.98	5
51.10	51.07	19.89	4.25	4.24	3.92	5
49.88	49.86	19.66	4.19	4.18	3.86	5
48.69	48.67	19.43	4.13	4.12	3.79	5
48.69	48.67	19.43	1.93	1.93	1.91	4
46.69	46.67	18.75	1.92	1.92	1.90	4
44.70	44.68	18.06	1.91	1.90	1.88	4
42.72	42.70	17.38	1.89	1.89	1.87	4
40.75	40.74	16.70	1.88	1.87	1.84	4
38.79	38.78	16.01	1.86	1.86	1.82	4
36.85	36.83	15.33	1.84	1.84	1.80	4
34.91	34.90	14.65	1.82	1.82	1.78	4
33.00	32.98	13.97	1.80	1.80	1.76	4
31.09	31.08	13.28	1.78	1.78	1.74	4
31.09	31.08	13.28	1.47	1.47	1.45	3
29.70	29.69	12.72	1.46	1.46	1.44	3
28.32	28.31	12.16	1.45	1.45	1.43	3
26.94	26.93	11.59	1.44	1.44	1.42	3
25.57	25.56	11.03	1.43	1.43	1.41	3
24.21	24.19	10.47	1.42	1.42	1.40	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3

18.80	18.79	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.44	285.62	114.32	171.30	151.68	19.62	6
59.90	324.07	101.00	223.07	185.51	37.56	6
59.35	362.70	88.53	274.17	219.52	54.65	6
58.81	401.50	77.43	324.07	253.70	70.37	6
58.26	440.45	68.11	372.34	288.03	84.31	6
57.70	479.52	60.78	418.73	322.48	96.26	6
57.15	518.67	55.50	463.17	357.01	106.16	6
56.60	557.89	52.13	505.76	391.61	114.15	6
56.04	597.14	50.40	546.74	426.24	120.50	6
56.04	597.14	50.40	546.74	426.24	120.50	5
54.78	701.70	72.39	629.31	505.05	124.26	5
53.53	805.45	95.65	709.80	583.05	126.75	5
52.29	908.35	119.82	788.53	660.20	128.33	5
51.07	1010.37	144.61	865.76	736.47	129.29	5
49.86	1111.49	169.80	941.70	811.84	129.86	5
48.67	1211.71	195.26	1016.44	886.30	130.14	5
48.67	1211.71	195.26	1016.44	886.30	130.14	4
46.67	1412.13	268.52	1143.62	1010.87	132.74	4
44.68	1612.04	347.09	1264.95	1134.92	130.03	4
42.70	1811.40	433.95	1377.44	1258.42	119.03	4
40.74	2010.11	518.94	1491.18	1381.28	109.90	4
38.78	2208.11	582.39	1625.73	1503.41	122.31	4
36.83	2405.32	650.41	1754.91	1624.77	130.14	4
34.90	2601.70	722.60	1879.10	1745.28	133.82	4
32.98	2797.19	798.34	1998.86	1864.92	133.94	4
31.08	2991.77	874.20	2117.58	1983.64	133.94	4
31.08	2991.77	874.20	2117.58	1983.64	133.94	3
29.69	3140.34	936.05	2204.29	2070.35	133.94	3
28.31	3288.52	997.91	2290.61	2156.67	133.94	3
26.93	3436.32	1062.87	2373.44	2242.61	130.84	3
25.56	3583.75	1126.52	2457.23	2328.18	129.04	3
24.19	3730.83	1188.73	2542.11	2413.41	128.70	3
22.83	3877.57	1250.44	2627.12	2498.28	128.84	3
21.48	4023.95	1311.89	2712.07	2582.81	129.26	3
20.13	4170.00	1373.21	2796.78	2666.99	129.79	3
18.79	4315.70	1434.09	2881.61	2750.83	130.77	3
18.79	4315.70	1434.09	2881.61	2750.83	130.77	2
16.87	4521.35	1518.17	3003.18	2870.39	132.79	2
14.96	4726.49	1603.12	3123.37	2989.43	133.94	2
13.06	4931.09	1689.22	3241.88	3107.94	133.94	2
11.17	5135.17	1775.31	3359.86	3225.92	133.94	2
9.29	5338.73	1861.41	3477.32	3343.38	133.94	2
7.42	5541.74	1947.51	3594.23	3460.29	133.94	2
5.55	5744.26	2033.61	3710.65	3576.71	133.94	2
3.69	5946.35	2136.79	3809.55	3692.70	116.85	2
1.84	6147.97	2262.16	3885.82	3808.23	77.59	2
.00	6349.01	2425.20	3923.81	3923.17	.64	2

Time = 120. Degree of Consolidation = 13.%

Total Settlement = .144

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 120. = .144

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.82	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.82	71.90	28.04	43.86	38.41	5.45	1
1.21	143.29	54.73	88.56	76.32	12.23	1
.60	214.51	86.44	128.06	114.05	14.01	1
.00	285.62	114.32	171.30	151.68	19.62	1

Time = 120. Degree of Consolidation = 96.%

Total Settlement = .069

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 120. = .069

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .89

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.36	21.42	6.50	6.15	6.10	6
60.02	59.82	21.35	6.49	6.17	6.08	6

59.45	59.28	21.27	6.47	6.20	6.07	6
58.89	58.73	21.20	6.46	6.22	6.05	6
58.33	58.19	21.12	6.44	6.24	6.04	6
57.76	57.64	21.05	6.43	6.26	6.03	6
57.20	57.09	20.97	6.42	6.28	6.01	6
56.64	56.54	20.90	6.40	6.29	6.00	6
56.08	55.99	20.82	6.39	6.30	5.98	6
56.08	55.99	20.82	4.51	4.44	4.18	5
54.82	54.73	20.59	4.44	4.39	4.11	5
53.56	53.49	20.36	4.38	4.33	4.05	5
52.32	52.26	20.12	4.32	4.28	3.98	5
51.10	51.04	19.89	4.25	4.22	3.92	5
49.88	49.84	19.66	4.19	4.16	3.86	5
48.69	48.65	19.43	4.13	4.09	3.79	5
48.69	48.65	19.43	1.93	1.93	1.91	4
46.69	46.66	18.75	1.92	1.92	1.90	4
44.70	44.67	18.06	1.91	1.90	1.88	4
42.72	42.69	17.38	1.89	1.89	1.87	4
40.75	40.73	16.70	1.88	1.87	1.84	4
38.79	38.77	16.01	1.86	1.86	1.82	4
36.85	36.83	15.33	1.84	1.84	1.80	4
34.91	34.90	14.65	1.82	1.82	1.78	4
33.00	32.98	13.97	1.80	1.80	1.76	4
31.09	31.08	13.28	1.78	1.78	1.74	4
31.09	31.08	13.28	1.47	1.47	1.45	3
29.70	29.69	12.72	1.46	1.46	1.44	3
28.32	28.30	12.16	1.45	1.45	1.43	3
26.94	26.93	11.59	1.44	1.44	1.42	3
25.57	25.56	11.03	1.43	1.43	1.41	3
24.21	24.19	10.47	1.42	1.42	1.40	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.36	285.62	116.70	168.92	151.68	17.24	6
59.82	323.99	108.24	215.75	185.43	30.32	6
59.28	362.49	100.06	262.43	219.31	43.12	6
58.73	401.10	92.35	308.75	253.30	55.45	6
58.19	439.82	85.27	354.55	287.40	67.15	6
57.64	478.63	78.94	399.69	321.59	78.10	6
57.09	517.53	73.47	444.06	355.87	88.19	6
56.54	556.50	68.90	487.59	390.21	97.38	6
55.99	595.52	65.27	530.25	424.62	105.63	6
55.99	595.52	65.27	530.25	424.62	105.63	5
54.73	699.57	86.09	613.48	502.92	110.56	5
53.49	802.85	107.95	694.91	580.45	114.45	5
52.26	905.34	130.82	774.52	657.18	117.33	5

51.04	1006.98	154.60	852.38	733.08	119.30	5
49.84	1107.76	179.24	928.51	808.10	120.41	5
48.65	1207.63	204.67	1002.96	882.23	120.73	5
48.65	1207.63	204.67	1002.96	882.23	120.73	4
46.66	1408.00	277.57	1130.43	1006.74	123.69	4
44.67	1607.84	357.00	1250.84	1130.72	120.12	4
42.69	1807.12	446.08	1361.04	1254.14	106.90	4
40.73	2005.75	526.72	1479.03	1376.91	102.12	4
38.77	2203.66	589.27	1614.39	1498.96	115.43	4
36.83	2400.80	655.31	1745.49	1620.24	125.25	4
34.90	2597.13	724.87	1872.26	1740.72	131.54	4
32.98	2792.61	798.34	1994.28	1860.34	133.94	4
31.08	2987.20	874.20	2113.00	1979.06	133.94	4
31.08	2987.20	874.20	2113.00	1979.06	133.94	3
29.69	3135.77	936.05	2199.71	2065.77	133.94	3
28.30	3283.94	997.91	2286.03	2152.09	133.94	3
26.93	3431.74	1064.74	2366.99	2238.03	128.97	3
25.56	3579.16	1129.44	2449.72	2323.59	126.13	3
24.19	3726.22	1192.65	2533.57	2408.79	124.77	3
22.83	3872.93	1254.57	2618.36	2493.65	124.71	3
21.48	4019.30	1316.02	2703.28	2578.15	125.13	3
20.13	4165.31	1377.20	2788.11	2662.31	125.80	3
18.78	4310.99	1437.56	2873.43	2746.13	127.30	3
18.78	4310.99	1437.56	2873.43	2746.13	127.30	2
16.87	4516.63	1520.52	2996.11	2865.67	130.44	2
14.96	4721.75	1604.31	3117.44	2984.70	132.75	2
13.06	4926.36	1689.22	3237.14	3103.20	133.94	2
11.17	5130.44	1775.31	3355.13	3221.19	133.94	2
9.29	5334.00	1861.41	3472.58	3338.64	133.94	2
7.42	5537.01	1947.51	3589.50	3455.56	133.94	2
5.55	5739.53	2035.72	3703.81	3571.98	131.83	2
3.69	5941.58	2152.67	3788.91	3687.93	100.98	2
1.84	6143.12	2282.62	3860.51	3803.38	57.13	2
.00	6344.11	2425.37	3918.74	3918.27	.47	2

Time = 240. Degree of Consolidation = 20.%

Total Settlement = .222

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 240. = .222

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.82	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.82	71.90	28.09	43.80	38.41	5.39	1
1.21	143.29	55.30	87.99	76.32	11.67	1
.60	214.50	87.35	127.15	114.05	13.10	1
.00	285.62	116.70	168.92	151.68	17.24	1

Time = 240. Degree of Consolidation = 96.%

Total Settlement = .069

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 240. = .069

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .81

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.29	21.42	6.50	6.14	6.10	6
60.02	59.75	21.35	6.49	6.16	6.08	6
59.45	59.21	21.27	6.47	6.18	6.07	6
58.89	58.67	21.20	6.46	6.20	6.05	6
58.33	58.12	21.12	6.44	6.22	6.04	6
57.76	57.58	21.05	6.43	6.23	6.03	6
57.20	57.03	20.97	6.42	6.25	6.01	6
56.64	56.48	20.90	6.40	6.26	6.00	6
56.08	55.93	20.82	6.39	6.27	5.98	6
56.08	55.93	20.82	4.51	4.41	4.18	5
54.82	54.69	20.59	4.44	4.36	4.11	5
53.56	53.45	20.36	4.38	4.30	4.05	5
52.32	52.23	20.12	4.32	4.25	3.98	5
51.10	51.02	19.89	4.25	4.19	3.92	5
49.88	49.82	19.66	4.19	4.13	3.86	5
48.69	48.64	19.43	4.13	4.06	3.79	5
48.69	48.64	19.43	1.93	1.93	1.91	4
46.69	46.65	18.75	1.92	1.91	1.90	4
44.70	44.66	18.06	1.91	1.90	1.88	4
42.72	42.69	17.38	1.89	1.89	1.87	4
40.75	40.72	16.70	1.88	1.87	1.84	4
38.79	38.76	16.01	1.86	1.85	1.82	4
36.85	36.82	15.33	1.84	1.84	1.80	4
34.91	34.89	14.65	1.82	1.82	1.78	4
33.00	32.98	13.97	1.80	1.80	1.76	4
31.09	31.07	13.28	1.78	1.78	1.74	4
31.09	31.07	13.28	1.47	1.47	1.45	3
29.70	29.68	12.72	1.46	1.46	1.44	3
28.32	28.30	12.16	1.45	1.45	1.43	3
26.94	26.92	11.59	1.44	1.44	1.42	3
25.57	25.55	11.03	1.43	1.43	1.41	3

24.21	24.19	10.47	1.42	1.42	1.40	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.29	285.61	117.75	167.86	151.67	16.19	6
59.75	323.96	111.41	212.55	185.40	27.15	6
59.21	362.40	105.23	257.17	219.22	37.95	6
58.67	400.92	99.32	301.61	253.12	48.48	6
58.12	439.53	93.78	345.74	287.11	58.64	6
57.58	478.21	88.73	389.48	321.17	68.31	6
57.03	516.96	84.23	432.73	355.30	77.43	6
56.48	555.77	80.37	475.40	389.49	85.92	6
55.93	594.63	77.21	517.42	423.73	93.69	6
55.93	594.63	77.21	517.42	423.73	93.69	5
54.69	698.24	98.28	599.97	501.59	98.37	5
53.45	801.09	120.20	680.89	578.69	102.20	5
52.23	903.13	143.01	760.12	654.98	105.14	5
51.02	1004.34	166.69	837.65	730.44	107.21	5
49.82	1104.68	191.23	913.46	805.03	108.42	5
48.64	1204.13	216.59	987.55	878.73	108.82	5
48.64	1204.13	216.59	987.55	878.73	108.82	4
46.65	1404.42	288.91	1115.50	1003.16	112.35	4
44.66	1604.19	368.27	1235.92	1127.07	108.85	4
42.69	1803.39	457.47	1345.91	1250.41	95.51	4
40.72	2001.94	533.09	1468.85	1373.10	95.75	4
38.76	2199.78	594.79	1604.98	1495.08	109.91	4
36.82	2396.86	659.42	1737.44	1616.30	121.14	4
34.89	2593.15	727.33	1865.82	1736.74	129.09	4
32.98	2788.62	798.72	1989.90	1856.34	133.56	4
31.07	2983.20	874.36	2108.84	1975.07	133.77	4
31.07	2983.20	874.36	2108.84	1975.07	133.77	3
29.68	3131.77	936.05	2195.72	2061.78	133.94	3
28.30	3279.95	997.91	2282.04	2148.10	133.94	3
26.92	3427.74	1065.85	2361.89	2234.03	127.86	3
25.55	3575.15	1131.62	2443.53	2319.58	123.95	3
24.19	3722.20	1195.77	2526.43	2404.77	121.66	3
22.83	3868.89	1258.61	2610.28	2489.60	120.67	3
21.47	4015.23	1320.32	2694.91	2574.08	120.83	3
20.12	4161.22	1381.05	2780.18	2658.22	121.96	3
18.78	4306.88	1440.97	2865.91	2742.02	123.89	3
18.78	4306.88	1440.97	2865.91	2742.02	123.89	2
16.87	4512.50	1523.06	2989.44	2861.54	127.90	2
14.96	4717.61	1605.94	3111.67	2980.55	131.11	2
13.06	4922.21	1689.92	3232.29	3099.05	133.24	2
11.17	5126.29	1775.31	3350.97	3217.03	133.94	2
9.29	5329.84	1861.41	3468.43	3334.49	133.94	2

7.41	5532.86	1947.51	3585.35	3451.41	133.94	2
5.55	5735.37	2040.02	3695.36	3567.82	127.53	2
3.69	5937.39	2163.19	3774.20	3683.74	90.46	2
1.84	6138.89	2292.65	3846.24	3799.15	47.10	2
.00	6339.85	2425.46	3914.40	3914.01	.39	2

Time = 365. Degree of Consolidation = 26.%

Total Settlement = .290

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 365. = .290

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.82	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.82	71.90	28.12	43.78	38.41	5.37	1
1.21	143.29	55.54	87.74	76.32	11.43	1
.60	214.50	87.75	126.75	114.04	12.70	1
.00	285.61	117.75	167.86	151.67	16.19	1

Time = 365. Degree of Consolidation = 96.%

Total Settlement = .069

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 365. = .069

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .74

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
60.58	60.21	21.42
60.02	59.67	21.35
59.45	59.13	21.27
58.89	58.59	21.20
58.33	58.05	21.12
57.76	57.50	21.05
57.20	56.96	20.97
56.64	56.41	20.90
56.08	55.87	20.82
56.08	55.87	20.82
54.82	54.63	20.59
53.56	53.40	20.36
52.32	52.19	20.12
51.10	50.99	19.89
49.88	49.80	19.66
48.69	48.63	19.43
48.69	48.63	19.43
46.69	46.64	18.75
44.70	44.65	18.06
42.72	42.68	17.38
40.75	40.71	16.70
38.79	38.76	16.01
36.85	36.82	15.33
34.91	34.89	14.65
33.00	32.97	13.97
31.09	31.07	13.28
31.09	31.07	13.28
29.70	29.68	12.72
28.32	28.30	12.16
26.94	26.92	11.59
25.57	25.55	11.03
24.21	24.18	10.47
22.84	22.82	9.90
21.49	21.47	9.34
20.14	20.12	8.78
18.80	18.78	8.21
18.80	18.78	8.21
16.88	16.86	7.39
14.97	14.96	6.57
13.07	13.06	5.75
11.18	11.17	4.93
9.30	9.29	4.11
7.43	7.41	3.29
5.56	5.55	2.46
3.70	3.69	1.64
1.85	1.84	.82
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
6.50	6.14	6.10	6
6.49	6.15	6.08	6
6.47	6.17	6.07	6
6.46	6.18	6.05	6
6.44	6.19	6.04	6
6.43	6.20	6.03	6
6.42	6.21	6.01	6
6.40	6.22	6.00	6
6.39	6.22	5.98	6
4.51	4.37	4.18	5
4.44	4.32	4.11	5
4.38	4.26	4.05	5
4.32	4.21	3.98	5
4.25	4.15	3.92	5
4.19	4.09	3.86	5
4.13	4.02	3.79	5
1.93	1.92	1.91	4
1.92	1.91	1.90	4
1.91	1.90	1.88	4
1.89	1.88	1.87	4
1.88	1.87	1.84	4
1.86	1.85	1.82	4
1.84	1.83	1.80	4
1.82	1.82	1.78	4
1.80	1.80	1.76	4
1.78	1.77	1.74	4
1.47	1.47	1.45	3
1.46	1.46	1.44	3
1.45	1.45	1.43	3
1.44	1.44	1.42	3
1.43	1.43	1.41	3
1.42	1.42	1.40	3
1.41	1.41	1.39	3
1.40	1.40	1.38	3
1.39	1.39	1.37	3
1.38	1.38	1.36	3
1.34	1.34	1.32	2
1.33	1.33	1.31	2
1.32	1.32	1.30	2
1.31	1.31	1.29	2
1.30	1.30	1.28	2
1.29	1.29	1.27	2
1.28	1.28	1.26	2
1.27	1.27	1.26	2
1.26	1.26	1.25	2
1.25	1.25	1.24	2
1.25	1.24	1.24	2

***** Stresses *****

XI	Total	Effective
60.21	285.61	118.71
59.67	323.93	114.28
59.13	362.31	109.99
58.59	400.76	105.89
58.05	439.26	102.09
57.50	477.81	98.65
56.96	516.41	95.65
56.41	555.04	93.16

***** Pore Pressures *****

Total	Static	Excess	Material
166.90	151.67	15.23	6
209.65	185.37	24.28	6
252.33	219.13	33.19	6
294.87	252.96	41.91	6
337.17	286.84	50.33	6
379.16	320.77	58.39	6
420.76	354.74	66.02	6
461.88	388.76	73.12	6

55.87	593.71	91.25	502.46	422.81	79.65	6
55.87	593.71	91.25	502.46	422.81	79.65	5
54.63	696.81	113.04	583.77	500.16	83.61	5
53.40	799.11	135.50	663.61	576.71	86.90	5
52.19	900.60	158.67	741.94	652.45	89.49	5
50.99	1001.24	182.57	818.68	727.34	91.33	5
49.80	1101.02	207.19	893.83	801.36	92.46	5
48.63	1199.89	232.51	967.38	874.49	92.89	5
48.63	1199.89	232.51	967.38	874.49	92.89	4
46.64	1400.07	304.46	1095.61	998.81	96.80	4
44.65	1599.74	383.59	1216.15	1122.62	93.53	4
42.68	1798.83	472.79	1326.04	1245.85	80.19	4
40.71	1997.28	541.41	1455.87	1368.44	87.43	4
38.76	2195.02	601.72	1593.30	1490.33	102.97	4
36.82	2392.03	664.82	1727.21	1611.48	115.73	4
34.89	2588.27	731.09	1857.19	1731.86	125.33	4
32.97	2783.70	801.01	1982.69	1851.42	131.26	4
31.07	2978.27	875.46	2102.81	1970.13	132.67	4
31.07	2978.27	875.46	2102.81	1970.13	132.67	3
29.68	3126.83	936.05	2190.78	2056.84	133.94	3
28.30	3275.01	997.91	2277.10	2143.16	133.94	3
26.92	3422.80	1067.12	2355.67	2229.09	126.59	3
25.55	3570.20	1134.14	2436.06	2314.63	121.43	3
24.18	3717.23	1198.78	2518.44	2399.80	118.64	3
22.82	3863.90	1261.62	2602.28	2484.62	117.66	3
21.47	4010.23	1323.33	2686.90	2569.08	117.82	3
20.12	4156.21	1384.06	2772.15	2653.20	118.94	3
18.78	4301.85	1443.67	2858.18	2736.98	121.20	3
18.78	4301.85	1443.67	2858.18	2736.98	121.20	2
16.86	4507.45	1525.11	2982.34	2856.49	125.85	2
14.96	4712.55	1607.34	3105.21	2975.49	129.72	2
13.06	4917.14	1690.63	3226.51	3093.99	132.52	2
11.17	5121.22	1775.31	3345.90	3211.97	133.94	2
9.29	5324.77	1861.41	3463.36	3329.42	133.94	2
7.41	5527.79	1947.51	3580.28	3446.34	133.94	2
5.55	5730.29	2046.04	3684.25	3562.74	121.51	2
3.69	5932.28	2171.09	3761.18	3678.63	82.55	2
1.84	6133.75	2298.92	3834.83	3794.00	40.82	2
.00	6334.69	2425.51	3909.19	3908.85	.34	2

Time = 540. Degree of Consolidation = 33.%

Total Settlement = .373

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 540. = .373

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1

.63	.60	.32	.98	.91	1
.00	.00	.00	.98	.91	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.90	28.14	43.76	38.41	5.34	1
1.21	143.29	55.77	87.52	76.32	11.20	1
.60	214.50	88.11	126.38	114.04	12.34	1
.00	285.61	118.71	166.90	151.67	15.23	1

Time = 540. Degree of Consolidation = 96.%

Total Settlement = .069

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 540. = .069

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .66

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.13	21.42	6.50	6.14	6.10	6
60.02	59.59	21.35	6.49	6.15	6.08	6
59.45	59.05	21.27	6.47	6.16	6.07	6
58.89	58.51	21.20	6.46	6.16	6.05	6
58.33	57.97	21.12	6.44	6.17	6.04	6
57.76	57.43	21.05	6.43	6.18	6.03	6
57.20	56.88	20.97	6.42	6.18	6.01	6
56.64	56.34	20.90	6.40	6.18	6.00	6
56.08	55.80	20.82	6.39	6.18	5.98	6
56.08	55.80	20.82	4.51	4.34	4.18	5
54.82	54.57	20.59	4.44	4.29	4.11	5
53.56	53.35	20.36	4.38	4.23	4.05	5
52.32	52.14	20.12	4.32	4.17	3.98	5
51.10	50.95	19.89	4.25	4.11	3.92	5
49.88	49.77	19.66	4.19	4.05	3.86	5
48.69	48.61	19.43	4.13	3.98	3.79	5
48.69	48.61	19.43	1.93	1.92	1.91	4
46.69	46.62	18.75	1.92	1.91	1.90	4
44.70	44.64	18.06	1.91	1.90	1.88	4
42.72	42.67	17.38	1.89	1.88	1.87	4
40.75	40.70	16.70	1.88	1.87	1.84	4
38.79	38.75	16.01	1.86	1.85	1.82	4
36.85	36.81	15.33	1.84	1.83	1.80	4
34.91	34.88	14.65	1.82	1.81	1.78	4
33.00	32.97	13.97	1.80	1.79	1.76	4
31.09	31.07	13.28	1.78	1.77	1.74	4

31.09	31.07	13.28	1.47	1.47	1.45	3
29.70	29.68	12.72	1.46	1.46	1.44	3
28.32	28.29	12.16	1.45	1.45	1.43	3
26.94	26.92	11.59	1.44	1.44	1.42	3
25.57	25.55	11.03	1.43	1.43	1.41	3
24.21	24.18	10.47	1.42	1.42	1.40	3
22.84	22.82	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.13	285.60	119.55	166.05	151.67	14.39	6
59.59	323.90	116.81	207.09	185.34	21.75	6
59.05	362.24	114.18	248.06	219.06	29.00	6
58.51	400.61	111.72	288.90	252.81	36.08	6
57.97	439.02	109.49	329.53	286.60	42.93	6
57.43	477.45	107.57	369.88	320.41	49.47	6
56.88	515.91	106.05	409.86	354.25	55.61	6
56.34	554.39	104.98	449.41	388.11	61.30	6
55.80	592.88	104.40	488.48	421.98	66.50	6
55.80	592.88	104.40	488.48	421.98	66.50	5
54.57	695.49	126.97	568.53	498.84	69.68	5
53.35	797.29	150.06	647.22	574.88	72.34	5
52.14	898.24	173.73	724.51	650.09	74.42	5
50.95	998.34	197.95	800.38	724.44	75.95	5
49.77	1097.55	222.76	874.79	797.90	76.89	5
48.61	1195.87	248.14	947.73	870.47	77.26	5
48.61	1195.87	248.14	947.73	870.47	77.26	4
46.62	1395.94	320.60	1075.34	994.68	80.66	4
44.64	1595.49	399.95	1195.55	1118.37	77.17	4
42.67	1794.48	489.15	1305.33	1241.50	63.83	4
40.70	1992.81	550.18	1442.64	1363.98	78.66	4
38.75	2190.46	609.20	1581.26	1485.77	95.50	4
36.81	2387.39	671.03	1716.36	1606.84	109.53	4
34.88	2583.56	735.94	1847.62	1727.15	120.47	4
32.97	2778.94	804.39	1974.55	1846.67	127.88	4
31.07	2973.48	877.16	2096.32	1965.34	130.98	4
31.07	2973.48	877.16	2096.32	1965.34	130.98	3
29.68	3122.04	936.05	2185.99	2052.05	133.94	3
28.29	3270.22	997.91	2272.31	2138.37	133.94	3
26.92	3418.00	1068.06	2349.94	2224.29	125.65	3
25.55	3565.40	1135.99	2429.40	2309.83	119.57	3
24.18	3712.41	1201.54	2510.88	2394.99	115.89	3
22.82	3859.07	1264.90	2594.17	2479.78	114.39	3
21.47	4005.38	1326.60	2678.78	2564.23	114.55	3
20.12	4151.34	1387.33	2764.01	2648.33	115.67	3
18.78	4296.96	1446.63	2850.32	2732.10	118.23	3
18.78	4296.96	1446.63	2850.32	2732.10	118.23	2

16.86	4502.55	1527.46	2975.09	2851.59	123.50	2
14.96	4707.64	1609.04	3098.59	2970.58	128.01	2
13.06	4912.22	1691.67	3220.55	3089.06	131.49	2
11.17	5116.29	1775.66	3340.63	3207.04	133.59	2
9.28	5319.84	1861.41	3458.43	3324.49	133.94	2
7.41	5522.86	1947.51	3575.35	3441.41	133.94	2
5.55	5725.35	2049.96	3675.39	3557.80	117.59	2
3.69	5927.32	2177.64	3749.68	3673.67	76.01	2
1.84	6128.77	2302.93	3825.84	3789.02	36.81	2
.00	6329.70	2425.54	3904.16	3903.86	.30	2

Time = 730. Degree of Consolidation = 40.%

Total Settlement = .453

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 730. = .453

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.90	28.16	43.74	38.41	5.32	1
1.21	143.29	55.96	87.32	76.32	11.01	1
.60	214.50	88.44	126.06	114.04	12.02	1
.00	285.60	119.55	166.05	151.67	14.39	1

Time = 730. Degree of Consolidation = 96.%

Total Settlement = .069

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 730. = .069

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .58

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.00	21.42	6.50	6.14	6.10	6
60.02	59.47	21.35	6.49	6.14	6.08	6
59.45	58.93	21.27	6.47	6.14	6.07	6
58.89	58.39	21.20	6.46	6.14	6.05	6
58.33	57.85	21.12	6.44	6.14	6.04	6
57.76	57.31	21.05	6.43	6.13	6.03	6
57.20	56.77	20.97	6.42	6.13	6.01	6
56.64	56.23	20.90	6.40	6.13	6.00	6
56.08	55.69	20.82	6.39	6.12	5.98	6
56.08	55.69	20.82	4.51	4.29	4.18	5
54.82	54.47	20.59	4.44	4.23	4.11	5
53.56	53.27	20.36	4.38	4.17	4.05	5
52.32	52.08	20.12	4.32	4.11	3.98	5
51.10	50.90	19.89	4.25	4.05	3.92	5
49.88	49.73	19.66	4.19	3.99	3.86	5
48.69	48.58	19.43	4.13	3.92	3.79	5
48.69	48.58	19.43	1.93	1.92	1.91	4
46.69	46.60	18.75	1.92	1.90	1.90	4
44.70	44.62	18.06	1.91	1.89	1.88	4
42.72	42.65	17.38	1.89	1.88	1.87	4
40.75	40.69	16.70	1.88	1.86	1.84	4
38.79	38.74	16.01	1.86	1.85	1.82	4
36.85	36.80	15.33	1.84	1.83	1.80	4
34.91	34.87	14.65	1.82	1.81	1.78	4
33.00	32.96	13.97	1.80	1.79	1.76	4
31.09	31.06	13.28	1.78	1.77	1.74	4
31.09	31.06	13.28	1.47	1.47	1.45	3
29.70	29.67	12.72	1.46	1.46	1.44	3
28.32	28.29	12.16	1.45	1.45	1.43	3
26.94	26.91	11.59	1.44	1.44	1.42	3
25.57	25.54	11.03	1.43	1.43	1.41	3
24.21	24.18	10.47	1.42	1.42	1.40	3
22.84	22.82	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.00	285.60	120.85	164.75	151.66	13.09	6
59.47	323.86	120.64	203.22	185.30	17.92	6
58.93	362.12	120.52	241.60	218.94	22.66	6

58.39	400.39	120.53	279.85	252.59	27.27	6
57.85	438.65	120.75	317.90	286.23	31.67	6
57.31	476.91	121.20	355.71	319.87	35.84	6
56.77	515.16	121.94	393.22	353.50	39.72	6
56.23	553.40	123.03	430.37	387.11	43.25	6
55.69	591.61	124.51	467.11	420.71	46.40	6
55.69	591.61	124.51	467.11	420.71	46.40	5
54.47	693.48	148.30	545.18	496.83	48.35	5
53.27	794.49	172.42	622.07	572.09	49.98	5
52.08	894.63	196.87	697.76	646.48	51.28	5
50.90	993.88	221.67	772.22	719.98	52.23	5
49.73	1092.24	246.79	845.46	792.59	52.86	5
48.58	1189.70	272.25	917.45	864.29	53.15	5
48.58	1189.70	272.25	917.45	864.29	53.15	4
46.60	1389.60	345.38	1044.22	988.34	55.88	4
44.62	1588.98	425.46	1163.52	1111.86	51.66	4
42.65	1787.79	508.76	1279.03	1234.81	44.22	4
40.69	1985.95	564.61	1421.34	1357.11	64.22	4
38.74	2183.43	622.47	1560.96	1478.74	82.22	4
36.80	2380.21	682.61	1697.60	1599.66	97.94	4
34.87	2576.26	745.77	1830.49	1719.84	110.65	4
32.96	2771.53	812.36	1959.17	1839.26	119.92	4
31.06	2965.98	883.80	2082.18	1957.85	124.33	4
31.06	2965.98	883.80	2082.18	1957.85	124.33	3
29.67	3114.50	941.67	2172.83	2044.51	128.32	3
28.29	3262.65	1003.37	2259.27	2130.80	128.48	3
26.91	3410.40	1073.85	2336.55	2216.69	119.86	3
25.54	3557.76	1141.85	2415.91	2302.19	113.72	3
24.18	3704.75	1207.47	2497.27	2387.32	109.95	3
22.82	3851.37	1270.92	2580.45	2472.08	108.37	3
21.47	3997.64	1332.62	2665.02	2556.50	108.52	3
20.12	4143.57	1393.18	2750.38	2640.56	109.82	3
18.78	4289.16	1452.08	2837.08	2724.30	112.78	3
18.78	4289.16	1452.08	2837.08	2724.30	112.78	2
16.86	4494.72	1531.88	2962.84	2843.76	119.08	2
14.96	4699.78	1612.42	3087.36	2962.72	124.64	2
13.06	4904.35	1693.97	3210.38	3081.19	129.19	2
11.17	5108.41	1776.84	3331.57	3199.15	132.41	2
9.28	5311.95	1861.41	3450.54	3316.60	133.94	2
7.41	5514.97	1947.51	3567.46	3433.52	133.94	2
5.55	5717.47	2050.30	3667.17	3549.92	117.25	2
3.69	5919.43	2178.31	3741.12	3665.78	75.34	2
1.84	6120.87	2303.26	3817.61	3781.13	36.49	2
.00	6321.81	2425.54	3896.27	3895.97	.30	2

Time = 1080. Degree of Consolidation = 51.%

Total Settlement = .579

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 1080. = .579

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.90	28.19	43.71	38.41	5.29	1
1.21	143.29	56.27	87.02	76.32	10.70	1
.60	214.49	88.93	125.57	114.04	11.53	1
.00	285.60	120.85	164.75	151.66	13.09	1

Time = 1080. Degree of Consolidation = 96.%

Total Settlement = .070

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 1080. = .070

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .45

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.90	21.42	6.50	6.13	6.10	6
60.02	59.36	21.35	6.49	6.13	6.08	6
59.45	58.82	21.27	6.47	6.12	6.07	6
58.89	58.28	21.20	6.46	6.11	6.05	6
58.33	57.74	21.12	6.44	6.11	6.04	6
57.76	57.21	21.05	6.43	6.10	6.03	6
57.20	56.67	20.97	6.42	6.09	6.01	6
56.64	56.13	20.90	6.40	6.08	6.00	6
56.08	55.60	20.82	6.39	6.07	5.98	6
56.08	55.60	20.82	4.51	4.25	4.18	5
54.82	54.39	20.59	4.44	4.19	4.11	5
53.56	53.19	20.36	4.38	4.13	4.05	5
52.32	52.01	20.12	4.32	4.06	3.98	5
51.10	50.85	19.89	4.25	4.00	3.92	5
49.88	49.69	19.66	4.19	3.94	3.86	5
48.69	48.56	19.43	4.13	3.87	3.79	5
48.69	48.56	19.43	1.93	1.91	1.91	4
46.69	46.57	18.75	1.92	1.90	1.90	4
44.70	44.59	18.06	1.91	1.89	1.88	4
42.72	42.63	17.38	1.89	1.87	1.87	4
40.75	40.67	16.70	1.88	1.86	1.84	4

38.79	38.72	16.01	1.86	1.84	1.82	4
36.85	36.79	15.33	1.84	1.83	1.80	4
34.91	34.86	14.65	1.82	1.81	1.78	4
33.00	32.95	13.97	1.80	1.79	1.76	4
31.09	31.05	13.28	1.78	1.77	1.74	4
31.09	31.05	13.28	1.47	1.47	1.45	3
29.70	29.66	12.72	1.46	1.46	1.44	3
28.32	28.28	12.16	1.45	1.45	1.43	3
26.94	26.91	11.59	1.44	1.44	1.42	3
25.57	25.54	11.03	1.43	1.43	1.41	3
24.21	24.17	10.47	1.42	1.42	1.40	3
22.84	22.82	9.90	1.41	1.41	1.39	3
21.49	21.46	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.90	285.60	121.92	163.68	151.66	12.02	6
59.36	323.83	123.78	200.04	185.27	14.78	6
58.82	362.03	125.72	236.31	218.85	17.46	6
58.28	400.21	127.77	272.44	252.41	20.03	6
57.74	438.35	129.96	308.40	285.93	22.46	6
57.21	476.47	132.34	344.12	319.42	24.70	6
56.67	514.54	134.95	379.59	352.88	26.71	6
56.13	552.58	137.82	414.76	386.30	28.46	6
55.60	590.58	141.00	449.58	419.68	29.90	6
55.60	590.58	141.00	449.58	419.68	29.90	5
54.39	691.84	165.85	525.99	495.18	30.81	5
53.19	792.20	190.84	601.36	569.80	31.56	5
52.01	891.66	216.00	675.66	643.51	32.15	5
50.85	990.22	241.30	748.92	716.32	32.60	5
49.69	1087.87	266.78	821.09	788.22	32.87	5
48.56	1184.60	292.40	892.20	859.20	33.00	5
48.56	1184.60	292.40	892.20	859.20	33.00	4
46.57	1384.36	367.18	1017.18	983.10	34.08	4
44.59	1583.59	449.38	1134.21	1106.47	27.74	4
42.63	1782.23	522.96	1259.26	1229.25	30.02	4
40.67	1980.22	578.09	1402.13	1351.39	50.75	4
38.72	2177.55	634.98	1542.57	1472.85	69.72	4
36.79	2374.19	694.17	1680.02	1593.63	86.39	4
34.86	2570.10	756.38	1813.72	1713.68	100.04	4
32.95	2765.25	822.40	1942.85	1832.97	109.87	4
31.05	2959.58	893.34	2066.24	1951.45	114.79	4
31.05	2959.58	893.34	2066.24	1951.45	114.79	3
29.66	3108.05	950.55	2157.50	2038.05	119.44	3
28.28	3256.14	1012.18	2243.96	2124.29	119.67	3
26.91	3403.85	1080.98	2322.87	2210.13	112.73	3
25.54	3551.17	1148.06	2403.10	2295.60	107.50	3
24.17	3698.12	1213.65	2484.47	2380.69	103.77	3

22.82	3844.71	1277.11	2567.60	2465.42	102.18	3
21.46	3990.94	1338.81	2652.13	2549.80	102.33	3
20.12	4136.84	1398.89	2737.95	2633.83	104.12	3
18.78	4282.40	1457.32	2825.08	2717.54	107.54	3
18.78	4282.40	1457.32	2825.08	2717.54	107.54	2
16.86	4487.93	1536.22	2951.71	2836.97	114.74	2
14.96	4692.97	1615.84	3077.13	2955.91	121.22	2
13.06	4897.52	1696.44	3201.08	3074.36	126.72	2
11.17	5101.56	1778.33	3323.24	3192.31	130.93	2
9.28	5305.10	1861.87	3443.24	3309.75	133.49	2
7.41	5508.12	1947.51	3560.61	3426.67	133.94	2
5.55	5710.62	2050.30	3660.32	3543.07	117.25	2
3.69	5912.58	2178.31	3734.27	3658.93	75.34	2
1.84	6114.02	2303.26	3810.76	3774.28	36.49	2
.00	6314.96	2425.54	3889.42	3889.12	.30	2

Time = 1440. Degree of Consolidation = 61.%

Total Settlement = .689

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 1440. = .689

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.90	28.22	43.68	38.41	5.27	1
1.21	143.29	56.51	86.77	76.32	10.46	1
.60	214.49	89.33	125.16	114.04	11.12	1
.00	285.60	121.92	163.68	151.66	12.02	1

Time = 1440. Degree of Consolidation = 96.%

Total Settlement = .070

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 1440. = .070

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .34

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.80	21.42	6.50	6.13	6.10	6
60.02	59.26	21.35	6.49	6.12	6.08	6
59.45	58.72	21.27	6.47	6.11	6.07	6
58.89	58.19	21.20	6.46	6.10	6.05	6
58.33	57.65	21.12	6.44	6.08	6.04	6
57.76	57.11	21.05	6.43	6.07	6.03	6
57.20	56.58	20.97	6.42	6.06	6.01	6
56.64	56.05	20.90	6.40	6.05	6.00	6
56.08	55.52	20.82	6.39	6.03	5.98	6
56.08	55.52	20.82	4.51	4.22	4.18	5
54.82	54.31	20.59	4.44	4.15	4.11	5
53.56	53.13	20.36	4.38	4.09	4.05	5
52.32	51.96	20.12	4.32	4.02	3.98	5
51.10	50.80	19.89	4.25	3.96	3.92	5
49.88	49.66	19.66	4.19	3.90	3.86	5
48.69	48.53	19.43	4.13	3.83	3.79	5
48.69	48.53	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.90	4
44.70	44.57	18.06	1.91	1.88	1.88	4
42.72	42.60	17.38	1.89	1.87	1.87	4
40.75	40.65	16.70	1.88	1.85	1.84	4
38.79	38.71	16.01	1.86	1.84	1.82	4
36.85	36.77	15.33	1.84	1.82	1.80	4
34.91	34.85	14.65	1.82	1.81	1.78	4
33.00	32.94	13.97	1.80	1.79	1.76	4
31.09	31.04	13.28	1.78	1.77	1.74	4
31.09	31.04	13.28	1.47	1.47	1.45	3
29.70	29.66	12.72	1.46	1.46	1.44	3
28.32	28.28	12.16	1.45	1.45	1.43	3
26.94	26.90	11.59	1.44	1.44	1.42	3
25.57	25.53	11.03	1.43	1.42	1.41	3
24.21	24.17	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.39	1.38	3
20.14	20.11	8.78	1.39	1.39	1.37	3
18.80	18.77	8.21	1.38	1.38	1.36	3
18.80	18.77	8.21	1.34	1.33	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.95	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.80	285.59	122.84	162.75	151.65	11.10	6
59.26	323.80	126.49	197.31	185.24	12.07	6
58.72	361.95	130.18	231.77	218.77	13.00	6
58.19	400.05	133.93	266.12	252.25	13.87	6
57.65	438.10	137.78	300.31	285.68	14.64	6
57.11	476.09	141.79	334.29	319.05	15.25	6
56.58	514.02	145.99	368.03	352.36	15.67	6
56.05	551.89	150.40	401.49	385.61	15.89	6
55.52	589.70	155.04	434.65	418.79	15.86	6
55.52	589.70	155.04	434.65	418.79	15.86	5
54.31	690.43	180.82	509.61	493.78	15.83	5
53.13	790.24	206.61	583.64	567.84	15.79	5
51.96	889.13	232.42	656.71	640.98	15.74	5
50.80	987.09	258.22	728.87	713.19	15.68	5
49.66	1084.12	284.03	800.09	784.47	15.62	5
48.53	1180.23	309.84	870.39	854.83	15.56	5
48.53	1180.23	309.84	870.39	854.83	15.56	4
46.54	1379.87	386.20	993.67	978.61	15.06	4
44.57	1578.96	469.96	1109.00	1101.84	7.16	4
42.60	1777.46	535.13	1242.33	1224.48	17.85	4
40.65	1975.31	589.95	1385.36	1346.47	38.88	4
38.71	2172.50	646.60	1525.90	1467.80	58.10	4
36.77	2369.00	705.60	1663.39	1588.44	74.95	4
34.85	2564.77	767.69	1797.08	1708.36	88.72	4
32.94	2759.79	833.32	1926.47	1827.51	98.96	4
31.04	2953.99	903.97	2050.02	1945.86	104.17	4
31.04	2953.99	903.97	2050.03	1945.86	104.17	3
29.66	3102.39	960.88	2141.51	2032.40	109.11	3
28.28	3250.42	1023.03	2227.39	2118.57	108.82	3
26.90	3398.07	1090.48	2307.59	2204.36	103.24	3
25.53	3545.34	1156.28	2389.06	2289.78	99.29	3
24.17	3692.25	1220.64	2471.62	2374.82	96.79	3
22.81	3838.80	1283.73	2555.07	2459.52	95.56	3
21.46	3985.00	1345.16	2639.84	2543.86	95.99	3
20.11	4130.86	1404.80	2726.06	2627.86	98.20	3
18.77	4276.39	1462.83	2813.56	2711.53	102.03	3
18.77	4276.39	1462.83	2813.56	2711.53	102.03	2
16.86	4481.89	1540.88	2941.01	2830.93	110.08	2
14.95	4686.90	1619.63	3067.27	2949.84	117.43	2
13.06	4891.43	1699.34	3192.09	3068.27	123.82	2
11.17	5095.46	1780.30	3315.16	3186.21	128.95	2
9.28	5298.99	1862.88	3436.11	3303.64	132.47	2
7.41	5502.01	1947.51	3554.50	3420.56	133.94	2
5.55	5704.50	2050.30	3654.20	3536.95	117.25	2
3.69	5906.47	2178.31	3728.16	3652.82	75.34	2
1.84	6107.91	2303.26	3804.65	3768.16	36.49	2
.00	6308.85	2425.54	3883.31	3883.00	.30	2

Time = 1825. Degree of Consolidation = 70.%

Total Settlement = .787

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 1825. = .787

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.90	28.24	43.66	38.41	5.25	1
1.21	143.28	56.73	86.56	76.31	10.24	1
.60	214.49	89.68	124.81	114.04	10.78	1
.00	285.59	122.84	162.75	151.65	11.10	1

Time = 1825. Degree of Consolidation = 96.%

Total Settlement = .070

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 1825. = .070

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .24

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.70	21.42	6.50	6.13	6.10	6
60.02	59.16	21.35	6.49	6.11	6.08	6
59.45	58.63	21.27	6.47	6.10	6.07	6
58.89	58.09	21.20	6.46	6.08	6.05	6
58.33	57.55	21.12	6.44	6.07	6.04	6
57.76	57.02	21.05	6.43	6.06	6.03	6
57.20	56.49	20.97	6.42	6.04	6.01	6
56.64	55.96	20.90	6.40	6.03	6.00	6
56.08	55.43	20.82	6.39	6.01	5.98	6
56.08	55.43	20.82	4.51	4.20	4.18	5
54.82	54.23	20.59	4.44	4.11	4.11	5
53.56	53.05	20.36	4.38	4.05	4.05	5
52.32	51.89	20.12	4.32	3.98	3.98	5
51.10	50.74	19.89	4.25	3.92	3.92	5
49.88	49.61	19.66	4.19	3.86	3.86	5
48.69	48.49	19.43	4.13	3.79	3.79	5

48.69	48.49	19.43	1.93	1.91	1.91	4
46.69	46.51	18.75	1.92	1.90	1.90	4
44.70	44.53	18.06	1.91	1.88	1.88	4
42.72	42.57	17.38	1.89	1.87	1.87	4
40.75	40.62	16.70	1.88	1.85	1.84	4
38.79	38.68	16.01	1.86	1.83	1.82	4
36.85	36.75	15.33	1.84	1.82	1.80	4
34.91	34.83	14.65	1.82	1.80	1.78	4
33.00	32.92	13.97	1.80	1.78	1.76	4
31.09	31.03	13.28	1.78	1.76	1.74	4
31.09	31.03	13.28	1.47	1.46	1.45	3
29.70	29.64	12.72	1.46	1.45	1.44	3
28.32	28.26	12.16	1.45	1.44	1.43	3
26.94	26.89	11.59	1.44	1.43	1.42	3
25.57	25.52	11.03	1.43	1.42	1.41	3
24.21	24.16	10.47	1.42	1.41	1.40	3
22.84	22.80	9.90	1.41	1.40	1.39	3
21.49	21.45	9.34	1.40	1.39	1.38	3
20.14	20.11	8.78	1.39	1.38	1.37	3
18.80	18.77	8.21	1.38	1.37	1.36	3
18.80	18.77	8.21	1.34	1.33	1.32	2
16.88	16.86	7.39	1.33	1.32	1.31	2
14.97	14.95	6.57	1.32	1.31	1.30	2
13.07	13.05	5.75	1.31	1.31	1.29	2
11.18	11.16	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.70	285.59	123.39	162.20	151.65	10.55	6
59.16	323.78	128.08	195.70	185.22	10.48	6
58.63	361.90	132.78	229.13	218.72	10.40	6
58.09	399.96	137.47	262.50	252.16	10.33	6
57.55	437.95	142.15	295.80	285.53	10.27	6
57.02	475.87	146.84	329.04	318.83	10.20	6
56.49	513.73	151.52	362.21	352.07	10.14	6
55.96	551.52	156.19	395.32	385.24	10.09	6
55.43	589.24	160.87	428.37	418.34	10.03	6
55.43	589.24	160.87	428.37	418.34	10.03	5
54.23	689.53	196.65	492.88	492.88	.00	5
53.05	788.77	222.40	566.37	566.37	.00	5
51.89	887.09	248.15	638.94	638.94	.00	5
50.74	984.49	273.90	710.59	710.59	.00	5
49.61	1080.96	299.65	781.31	781.31	.00	5
48.49	1176.51	325.40	851.11	851.11	.00	5
48.49	1176.51	325.40	851.11	851.11	.00	4
46.51	1376.05	398.54	977.51	974.79	2.72	4
44.53	1575.09	477.12	1097.97	1097.97	.00	4
42.57	1773.51	543.97	1229.54	1220.53	9.01	4
40.62	1971.23	602.21	1369.02	1342.40	26.62	4
38.68	2168.26	661.03	1507.23	1463.56	43.67	4
36.75	2364.58	721.34	1643.24	1584.02	59.22	4
34.83	2560.17	783.81	1776.35	1703.75	72.60	4
32.92	2754.99	849.38	1905.61	1822.71	82.90	4
31.03	2949.00	919.89	2029.11	1940.87	88.25	4
31.03	2949.00	919.89	2029.12	1940.87	88.25	3

29.64	3097.30	976.89	2120.41	2027.31	93.10	3
28.26	3245.23	1040.48	2204.74	2113.38	91.37	3
26.89	3392.78	1106.52	2286.27	2199.07	87.19	3
25.52	3539.97	1170.98	2368.99	2284.40	84.58	3
24.16	3686.80	1234.07	2452.73	2369.37	83.35	3
22.80	3833.28	1295.96	2537.31	2453.99	83.32	3
21.45	3979.41	1356.82	2622.59	2538.27	84.32	3
20.11	4125.21	1416.16	2709.04	2622.20	86.84	3
18.77	4270.67	1473.91	2796.76	2705.81	90.95	3
18.77	4270.67	1473.92	2796.75	2705.81	90.95	2
16.86	4476.10	1550.92	2925.18	2825.14	100.04	2
14.95	4681.06	1628.62	3052.44	2944.00	108.44	2
13.05	4885.53	1707.27	3178.27	3062.38	115.89	2
11.16	5089.52	1787.15	3302.37	3180.27	122.10	2
9.28	5293.01	1868.62	3424.39	3297.66	126.73	2
7.41	5496.00	1952.10	3543.90	3414.55	129.35	2
5.55	5698.47	2055.51	3642.96	3530.92	112.04	2
3.69	5900.41	2181.70	3718.71	3646.77	71.94	2
1.84	6101.85	2304.93	3796.92	3762.10	34.82	2
.00	6302.78	2425.56	3877.22	3876.94	.29	2

Time = 2520. Degree of Consolidation = 78.%

Total Settlement = .884

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 2520. = .886

Settlement caused by Secondary Compression at time 2520. = -.002

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.50	2.43	1.26
1.88	1.81	.95
1.25	1.21	.63
.63	.60	.32
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
2.43	.00	.00
1.81	71.90	28.25
1.21	143.28	56.85
.60	214.49	89.89
.00	285.59	123.39

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
43.65	38.41	5.23	1
86.43	76.31	10.12	1
124.60	114.03	10.57	1
162.20	151.65	10.55	1

Time = 2520. Degree of Consolidation = 96.%

Total Settlement = .070

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 2520. = .070

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .15

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.67	21.42	6.50	6.10	6.10	6
60.02	59.13	21.35	6.49	6.08	6.08	6
59.45	58.60	21.27	6.47	6.07	6.07	6
58.89	58.06	21.20	6.46	6.05	6.05	6
58.33	57.53	21.12	6.44	6.04	6.04	6
57.76	57.00	21.05	6.43	6.03	6.03	6
57.20	56.47	20.97	6.42	6.01	6.01	6
56.64	55.94	20.90	6.40	6.00	6.00	6
56.08	55.41	20.82	6.39	5.98	5.98	6
56.08	55.41	20.82	4.51	4.18	4.18	5
54.82	54.22	20.59	4.44	4.11	4.11	5
53.56	53.04	20.36	4.38	4.05	4.05	5
52.32	51.88	20.12	4.32	3.98	3.98	5
51.10	50.73	19.89	4.25	3.92	3.92	5
49.88	49.60	19.66	4.19	3.86	3.86	5
48.69	48.48	19.43	4.13	3.79	3.79	5
48.69	48.48	19.43	1.93	1.91	1.91	4
46.69	46.50	18.75	1.92	1.90	1.90	4
44.70	44.52	18.06	1.91	1.88	1.88	4
42.72	42.56	17.38	1.89	1.87	1.87	4
40.75	40.61	16.70	1.88	1.85	1.84	4
38.79	38.66	16.01	1.86	1.83	1.82	4
36.85	36.73	15.33	1.84	1.82	1.80	4
34.91	34.82	14.65	1.82	1.80	1.78	4
33.00	32.91	13.97	1.80	1.78	1.76	4
31.09	31.02	13.28	1.78	1.76	1.74	4
31.09	31.02	13.28	1.47	1.46	1.45	3
29.70	29.63	12.72	1.46	1.45	1.44	3
28.32	28.26	12.16	1.45	1.44	1.43	3
26.94	26.88	11.59	1.44	1.43	1.42	3
25.57	25.52	11.03	1.43	1.42	1.41	3
24.21	24.15	10.47	1.42	1.41	1.40	3
22.84	22.80	9.90	1.41	1.40	1.39	3
21.49	21.45	9.34	1.40	1.39	1.38	3
20.14	20.10	8.78	1.39	1.38	1.37	3
18.80	18.77	8.21	1.38	1.37	1.36	3
18.80	18.77	8.21	1.34	1.33	1.32	2
16.88	16.85	7.39	1.33	1.32	1.31	2
14.97	14.95	6.57	1.32	1.31	1.30	2
13.07	13.05	5.75	1.31	1.30	1.29	2
11.18	11.16	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2

1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.67	285.59	133.94	151.65	151.65	.00	6
59.13	323.63	138.56	185.07	185.07	.00	6
58.60	361.60	143.18	218.42	218.42	.00	6
58.06	399.51	147.80	251.71	251.71	.00	6
57.53	437.35	152.42	284.93	284.93	.00	6
57.00	475.13	157.04	318.09	318.09	.00	6
56.47	512.84	161.66	351.18	351.18	.00	6
55.94	550.48	166.28	384.20	384.20	.00	6
55.41	588.06	170.90	417.16	417.16	.00	6
55.41	588.06	170.90	417.16	417.16	.00	5
54.22	688.23	196.65	491.58	491.58	.00	5
53.04	787.47	222.40	565.07	565.07	.00	5
51.88	885.79	248.15	637.64	637.64	.00	5
50.73	983.19	273.90	709.29	709.29	.00	5
49.60	1079.66	299.65	780.01	780.01	.00	5
48.48	1175.21	325.40	849.81	849.81	.00	5
48.48	1175.21	325.40	849.81	849.81	.00	4
46.50	1374.75	398.54	976.21	973.49	2.72	4
44.52	1573.79	477.12	1096.67	1096.67	.00	4
42.56	1772.20	544.95	1227.25	1219.22	8.03	4
40.61	1969.91	604.27	1365.64	1341.07	24.57	4
38.66	2166.91	664.25	1502.65	1462.21	40.44	4
36.73	2363.18	725.33	1637.85	1582.62	55.23	4
34.82	2558.72	788.44	1770.28	1702.30	67.98	4
32.91	2753.48	854.78	1898.70	1821.20	77.50	4
31.02	2947.43	925.86	2021.57	1939.29	82.27	4
31.02	2947.43	925.86	2021.56	1939.29	82.27	3
29.63	3095.68	983.26	2112.42	2025.69	86.73	3
28.26	3243.57	1047.72	2195.85	2111.72	84.13	3
26.88	3391.09	1113.48	2277.61	2197.38	80.23	3
25.52	3538.23	1177.70	2360.54	2282.67	77.87	3
24.15	3685.03	1240.56	2444.47	2367.60	76.87	3
22.80	3831.47	1302.24	2529.23	2452.18	77.05	3
21.45	3977.57	1362.81	2614.75	2536.42	78.33	3
20.10	4123.33	1421.66	2701.67	2620.33	81.34	3
18.77	4268.76	1478.94	2789.82	2703.90	85.92	3
18.77	4268.76	1478.94	2789.82	2703.90	85.92	2
16.85	4474.17	1555.50	2918.67	2823.21	95.46	2
14.95	4679.10	1632.75	3046.34	2942.04	104.30	2
13.05	4883.55	1710.95	3172.60	3060.39	112.21	2
11.16	5087.51	1790.38	3297.14	3178.26	118.88	2
9.28	5290.99	1871.38	3419.61	3295.64	123.97	2
7.41	5493.96	1954.37	3539.59	3412.51	127.08	2
5.54	5696.41	2058.09	3638.32	3528.86	109.46	2
3.69	5898.35	2183.38	3714.97	3644.70	70.27	2
1.84	6099.78	2305.75	3794.03	3760.03	34.00	2
.00	6300.71	2425.56	3875.15	3874.87	.28	2

Time = 2880. Degree of Consolidation = 81.%

Total Settlement = .917

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 2880. = .917

Settlement caused by Secondary Compression at time 2880. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.90	28.25	43.64	38.41	5.23	1
1.21	143.28	56.89	86.39	76.31	10.08	1
.60	214.49	89.95	124.54	114.03	10.50	1
.00	285.59	123.56	162.03	151.65	10.38	1

Time = 2880. Degree of Consolidation = 96.%

Total Settlement = .070

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 2880. = .070

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .11

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.66	21.42	6.50	6.10	6.10	6
60.02	59.12	21.35	6.49	6.08	6.08	6
59.45	58.59	21.27	6.47	6.07	6.07	6
58.89	58.05	21.20	6.46	6.05	6.05	6
58.33	57.52	21.12	6.44	6.04	6.04	6
57.76	56.99	21.05	6.43	6.03	6.03	6
57.20	56.46	20.97	6.42	6.01	6.01	6
56.64	55.93	20.90	6.40	6.00	6.00	6
56.08	55.40	20.82	6.39	5.98	5.98	6
56.08	55.40	20.82	4.51	4.18	4.18	5
54.82	54.21	20.59	4.44	4.11	4.11	5

53.56	53.03	20.36	4.38	4.05	4.05	5
52.32	51.87	20.12	4.32	3.98	3.98	5
51.10	50.72	19.89	4.25	3.92	3.92	5
49.88	49.59	19.66	4.19	3.86	3.86	5
48.69	48.47	19.43	4.13	3.79	3.79	5
48.69	48.47	19.43	1.93	1.91	1.91	4
46.69	46.49	18.75	1.92	1.90	1.90	4
44.70	44.51	18.06	1.91	1.88	1.88	4
42.72	42.55	17.38	1.89	1.87	1.87	4
40.75	40.59	16.70	1.88	1.85	1.84	4
38.79	38.65	16.01	1.86	1.83	1.82	4
36.85	36.72	15.33	1.84	1.82	1.80	4
34.91	34.81	14.65	1.82	1.80	1.78	4
33.00	32.90	13.97	1.80	1.78	1.76	4
31.09	31.01	13.28	1.78	1.76	1.74	4
31.09	31.01	13.28	1.47	1.46	1.45	3
29.70	29.63	12.72	1.46	1.45	1.44	3
28.32	28.25	12.16	1.45	1.44	1.43	3
26.94	26.88	11.59	1.44	1.43	1.42	3
25.57	25.51	11.03	1.43	1.42	1.41	3
24.21	24.15	10.47	1.42	1.41	1.40	3
22.84	22.80	9.90	1.41	1.40	1.39	3
21.49	21.45	9.34	1.40	1.39	1.38	3
20.14	20.10	8.78	1.39	1.38	1.37	3
18.80	18.76	8.21	1.38	1.37	1.36	3
18.80	18.76	8.21	1.34	1.33	1.32	2
16.88	16.85	7.39	1.33	1.32	1.31	2
14.97	14.95	6.57	1.32	1.31	1.30	2
13.07	13.05	5.75	1.31	1.30	1.29	2
11.18	11.16	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.66	285.43	133.94	151.49	151.49	.00	6
59.12	323.47	138.56	184.91	184.91	.00	6
58.59	361.44	143.18	218.26	218.26	.00	6
58.05	399.35	147.80	251.55	251.55	.00	6
57.52	437.19	152.42	284.77	284.77	.00	6
56.99	474.97	157.04	317.93	317.93	.00	6
56.46	512.68	161.66	351.01	351.01	.00	6
55.93	550.32	166.28	384.04	384.04	.00	6
55.40	587.90	170.90	416.99	416.99	.00	6
55.40	587.90	170.90	416.99	416.99	.00	5
54.21	688.06	196.65	491.41	491.41	.00	5
53.03	787.31	222.40	564.91	564.91	.00	5
51.87	885.63	248.15	637.48	637.48	.00	5
50.72	983.03	273.90	709.12	709.12	.00	5
49.59	1079.50	299.65	779.85	779.85	.00	5
48.47	1175.05	325.40	849.65	849.65	.00	5
48.47	1175.05	325.40	849.65	849.65	.00	4
46.49	1374.58	398.54	976.04	973.32	2.72	4
44.51	1573.63	477.12	1096.51	1096.51	.00	4
42.55	1772.04	545.61	1226.42	1219.06	7.36	4
40.59	1969.73	605.66	1364.07	1340.89	23.18	4
38.65	2166.71	666.44	1500.27	1462.01	38.26	4

36.72	2362.95	728.40	1634.55	1582.39	52.15	4
34.81	2558.44	792.16	1766.28	1702.03	64.26	4
32.90	2753.16	859.01	1894.15	1820.88	73.26	4
31.01	2947.05	930.78	2016.27	1938.92	77.35	4
31.01	2947.05	930.78	2016.27	1938.92	77.35	3
29.63	3095.28	988.78	2106.49	2025.28	81.21	3
28.25	3243.13	1054.14	2188.98	2111.28	77.71	3
26.88	3390.61	1119.83	2270.78	2196.90	73.88	3
25.51	3537.72	1183.98	2353.74	2282.15	71.59	3
24.15	3684.48	1246.80	2437.68	2367.05	70.63	3
22.80	3830.88	1308.45	2522.44	2451.60	70.84	3
21.45	3976.95	1368.76	2608.19	2535.80	72.39	3
20.10	4122.68	1427.36	2695.31	2619.67	75.64	3
18.76	4268.08	1484.42	2783.66	2703.22	80.44	3
18.76	4268.08	1484.42	2783.66	2703.22	80.44	2
16.85	4473.45	1560.49	2912.96	2822.49	90.47	2
14.95	4678.35	1637.26	3041.09	2941.29	99.80	2
13.05	4882.78	1714.96	3167.81	3059.62	108.19	2
11.16	5086.72	1793.89	3292.83	3177.47	115.36	2
9.28	5290.17	1874.38	3415.80	3294.82	120.97	2
7.41	5493.13	1956.84	3536.29	3411.68	124.61	2
5.54	5695.57	2060.89	3634.68	3528.02	106.66	2
3.69	5897.50	2185.21	3712.29	3643.85	68.44	2
1.84	6098.92	2306.64	3792.28	3759.17	33.10	2
.00	6299.85	2425.57	3874.28	3874.01	.27	2

Time = 3240. Degree of Consolidation = 82.%

Total Settlement = .928

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 3240. = .928

Settlement caused by Secondary Compression at time 3240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.50	2.43	1.26
1.88	1.81	.95
1.25	1.21	.63
.63	.60	.32
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
2.43	.00	.00
1.81	71.85	33.48
1.21	143.19	66.97
.60	214.36	100.45
.00	285.43	133.94

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
38.37	38.37	.00	1
76.22	76.22	.00	1
113.90	113.90	.00	1
151.49	151.49	.00	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .072

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 3240. = .072

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .10

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.64	21.42	6.50	6.10	6.10	6
60.02	59.11	21.35	6.49	6.08	6.08	6
59.45	58.57	21.27	6.47	6.07	6.07	6
58.89	58.04	21.20	6.46	6.05	6.05	6
58.33	57.51	21.12	6.44	6.04	6.04	6
57.76	56.98	21.05	6.43	6.03	6.03	6
57.20	56.45	20.97	6.42	6.01	6.01	6
56.64	55.92	20.90	6.40	6.00	6.00	6
56.08	55.39	20.82	6.39	5.98	5.98	6
56.08	55.39	20.82	4.51	4.18	4.18	5
54.82	54.20	20.59	4.44	4.11	4.11	5
53.56	53.02	20.36	4.38	4.05	4.05	5
52.32	51.86	20.12	4.32	3.98	3.98	5
51.10	50.71	19.89	4.25	3.92	3.92	5
49.88	49.57	19.66	4.19	3.86	3.86	5
48.69	48.46	19.43	4.13	3.79	3.79	5
48.69	48.46	19.43	1.93	1.91	1.91	4
46.69	46.47	18.75	1.92	1.90	1.90	4
44.70	44.50	18.06	1.91	1.88	1.88	4
42.72	42.54	17.38	1.89	1.87	1.87	4
40.75	40.58	16.70	1.88	1.85	1.84	4
38.79	38.64	16.01	1.86	1.83	1.82	4
36.85	36.71	15.33	1.84	1.82	1.80	4
34.91	34.80	14.65	1.82	1.80	1.78	4
33.00	32.89	13.97	1.80	1.78	1.76	4
31.09	31.00	13.28	1.78	1.76	1.74	4
31.09	31.00	13.28	1.47	1.46	1.45	3
29.70	29.62	12.72	1.46	1.45	1.44	3
28.32	28.24	12.16	1.45	1.44	1.43	3
26.94	26.87	11.59	1.44	1.43	1.42	3
25.57	25.50	11.03	1.43	1.42	1.41	3
24.21	24.14	10.47	1.42	1.41	1.40	3
22.84	22.79	9.90	1.41	1.40	1.39	3
21.49	21.44	9.34	1.40	1.39	1.38	3
20.14	20.10	8.78	1.39	1.38	1.37	3
18.80	18.76	8.21	1.38	1.37	1.36	3
18.80	18.76	8.21	1.34	1.33	1.32	2
16.88	16.85	7.39	1.33	1.32	1.31	2
14.97	14.95	6.57	1.32	1.31	1.30	2
13.07	13.05	5.75	1.31	1.30	1.29	2

11.18	11.16	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.64	285.43	133.94	151.49	151.49	.00	6
59.11	323.47	138.56	184.91	184.91	.00	6
58.57	361.44	143.18	218.26	218.26	.00	6
58.04	399.35	147.80	251.55	251.55	.00	6
57.51	437.19	152.42	284.77	284.77	.00	6
56.98	474.97	157.04	317.93	317.93	.00	6
56.45	512.68	161.66	351.01	351.01	.00	6
55.92	550.32	166.28	384.04	384.04	.00	6
55.39	587.90	170.90	416.99	416.99	.00	6
55.39	587.90	170.90	416.99	416.99	.00	5
54.20	688.06	196.65	491.41	491.41	.00	5
53.02	787.31	222.40	564.91	564.91	.00	5
51.86	885.63	248.15	637.48	637.48	.00	5
50.71	983.03	273.90	709.12	709.12	.00	5
49.57	1079.50	299.65	779.85	779.85	.00	5
48.46	1175.05	325.40	849.65	849.65	.00	5
48.46	1175.05	325.40	849.65	849.65	.00	4
46.47	1374.58	398.54	976.04	973.32	2.72	4
44.50	1573.63	477.12	1096.51	1096.51	.00	4
42.54	1772.03	546.23	1225.81	1219.05	6.75	4
40.58	1969.72	606.94	1362.78	1340.88	21.90	4
38.64	2166.67	668.46	1498.21	1461.98	36.24	4
36.71	2362.89	731.25	1631.64	1582.33	49.31	4
34.80	2558.34	795.96	1762.38	1701.93	60.46	4
32.89	2753.01	863.52	1889.49	1820.73	68.76	4
31.00	2946.84	936.17	2010.68	1938.71	71.97	4
31.00	2946.84	936.16	2010.68	1938.71	71.97	3
29.62	3095.03	995.00	2100.03	2025.04	74.99	3
28.24	3242.84	1061.44	2181.40	2110.99	70.42	3
26.87	3390.28	1127.04	2263.24	2196.57	66.67	3
25.50	3537.35	1191.13	2346.22	2281.78	64.44	3
24.14	3684.07	1253.90	2430.17	2366.64	63.53	3
22.79	3830.43	1315.52	2514.92	2451.15	63.77	3
21.44	3976.46	1375.56	2600.90	2535.31	65.59	3
20.10	4122.15	1433.91	2688.25	2619.15	69.10	3
18.76	4267.52	1490.73	2776.79	2702.66	74.14	3
18.76	4267.52	1490.73	2776.79	2702.66	74.13	2
16.85	4472.85	1566.24	2906.61	2821.89	84.72	2
14.95	4677.72	1642.45	3035.27	2940.66	94.61	2
13.05	4882.11	1719.58	3162.53	3058.96	103.57	2
11.16	5086.03	1797.93	3288.10	3176.78	111.32	2
9.28	5289.46	1877.83	3411.63	3294.11	117.52	2
7.41	5492.40	1959.68	3532.72	3410.95	121.77	2
5.54	5694.82	2064.11	3630.71	3527.27	103.44	2
3.69	5896.74	2187.30	3709.43	3643.09	66.34	2
1.84	6098.16	2307.67	3790.48	3758.41	32.07	2
.00	6299.08	2425.58	3873.51	3873.24	.26	2

Time = 3650. Degree of Consolidation = 83.%

Total Settlement = .941

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 3650. = .941

Settlement caused by Secondary Compression at time 3650. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.85	33.48	38.37	38.37	.00	1
1.21	143.19	66.97	76.22	76.22	.00	1
.60	214.36	100.45	113.90	113.90	.00	1
.00	285.43	133.94	151.49	151.49	.00	1

Time = 3650. Degree of Consolidation = 100.%

Total Settlement = .072

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 3650. = .072

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .09

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.62	21.42	6.50	6.10	6.10	6
60.02	59.09	21.35	6.49	6.08	6.08	6
59.45	58.55	21.27	6.47	6.07	6.07	6
58.89	58.02	21.20	6.46	6.05	6.05	6
58.33	57.49	21.12	6.44	6.04	6.04	6
57.76	56.96	21.05	6.43	6.03	6.03	6

57.20	56.43	20.97	6.42	6.01	6.01	6
56.64	55.90	20.90	6.40	6.00	6.00	6
56.08	55.37	20.82	6.39	5.98	5.98	6
56.08	55.37	20.82	4.51	4.18	4.18	5
54.82	54.18	20.59	4.44	4.11	4.11	5
53.56	53.00	20.36	4.38	4.05	4.05	5
52.32	51.84	20.12	4.32	3.98	3.98	5
51.10	50.69	19.89	4.25	3.92	3.92	5
49.88	49.55	19.66	4.19	3.86	3.86	5
48.69	48.44	19.43	4.13	3.79	3.79	5
48.69	48.44	19.43	1.93	1.91	1.91	4
46.69	46.45	18.75	1.92	1.90	1.90	4
44.70	44.48	18.06	1.91	1.88	1.88	4
42.72	42.52	17.38	1.89	1.87	1.87	4
40.75	40.56	16.70	1.88	1.85	1.84	4
38.79	38.62	16.01	1.86	1.83	1.82	4
36.85	36.70	15.33	1.84	1.81	1.80	4
34.91	34.78	14.65	1.82	1.80	1.78	4
33.00	32.88	13.97	1.80	1.78	1.76	4
31.09	30.99	13.28	1.78	1.76	1.74	4
31.09	30.99	13.28	1.47	1.46	1.45	3
29.70	29.61	12.72	1.46	1.45	1.44	3
28.32	28.23	12.16	1.45	1.44	1.43	3
26.94	26.86	11.59	1.44	1.43	1.42	3
25.57	25.49	11.03	1.43	1.42	1.41	3
24.21	24.13	10.47	1.42	1.41	1.40	3
22.84	22.78	9.90	1.41	1.40	1.39	3
21.49	21.43	9.34	1.40	1.39	1.38	3
20.14	20.09	8.78	1.39	1.38	1.37	3
18.80	18.75	8.21	1.38	1.37	1.36	3
18.80	18.75	8.21	1.34	1.33	1.32	2
16.88	16.84	7.39	1.33	1.32	1.31	2
14.97	14.94	6.57	1.32	1.31	1.30	2
13.07	13.05	5.75	1.31	1.30	1.29	2
11.18	11.16	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.62	285.43	133.94	151.49	151.49	.00	6
59.09	323.47	138.56	184.91	184.91	.00	6
58.55	361.44	143.18	218.26	218.26	.00	6
58.02	399.35	147.80	251.55	251.55	.00	6
57.49	437.19	152.42	284.77	284.77	.00	6
56.96	474.97	157.04	317.93	317.93	.00	6
56.43	512.68	161.66	351.01	351.01	.00	6
55.90	550.32	166.28	384.04	384.04	.00	6
55.37	587.90	170.90	416.99	416.99	.00	6
55.37	587.90	170.90	416.99	416.99	.00	5
54.18	688.06	196.65	491.41	491.41	.00	5
53.00	787.31	222.40	564.91	564.91	.00	5
51.84	885.63	248.15	637.48	637.48	.00	5
50.69	983.03	273.90	709.12	709.12	.00	5
49.55	1079.50	299.65	779.85	779.85	.00	5
48.44	1175.05	325.40	849.65	849.65	.00	5
48.44	1175.05	325.40	849.65	849.65	.00	4

46.45	1374.58	398.54	976.04	973.32	2.72	4
44.48	1573.63	477.12	1096.51	1096.51	.00	4
42.52	1772.03	547.03	1225.00	1219.05	5.94	4
40.56	1969.70	608.64	1361.06	1340.86	20.20	4
38.62	2166.63	671.13	1495.50	1461.93	33.56	4
36.70	2362.81	735.02	1627.78	1582.25	45.53	4
34.78	2558.21	801.01	1757.20	1701.79	55.41	4
32.88	2752.80	870.11	1882.70	1820.53	62.17	4
30.99	2946.55	944.71	2001.83	1938.41	63.42	4
30.99	2946.55	944.71	2001.83	1938.41	63.42	3
29.61	3094.68	1005.16	2089.52	2024.68	64.84	3
28.23	3242.42	1072.97	2169.46	2110.57	58.89	3
26.86	3389.80	1138.57	2251.23	2196.09	55.14	3
25.49	3536.81	1202.66	2334.15	2281.24	52.91	3
24.13	3683.46	1265.43	2418.03	2366.03	52.00	3
22.78	3829.76	1326.94	2502.82	2450.47	52.35	3
21.43	3975.72	1386.63	2589.09	2534.58	54.51	3
20.09	4121.35	1444.66	2676.69	2618.35	58.34	3
18.75	4266.66	1501.19	2765.47	2701.80	63.67	3
18.75	4266.66	1501.19	2765.47	2701.80	63.67	2
16.84	4471.93	1575.77	2896.16	2820.97	75.19	2
14.94	4676.74	1651.04	3025.70	2939.69	86.02	2
13.05	4881.09	1727.23	3153.85	3057.93	95.92	2
11.16	5084.96	1804.62	3280.34	3175.71	104.63	2
9.28	5288.35	1883.54	3404.81	3293.00	111.81	2
7.41	5491.26	1964.38	3526.88	3409.81	117.07	2
5.54	5693.66	2069.44	3624.22	3526.11	98.11	2
3.69	5895.55	2190.77	3704.78	3641.91	62.87	2
1.84	6096.96	2309.38	3787.58	3757.22	30.37	2
.00	6297.89	2425.59	3872.29	3872.04	.25	2

Time = 4320. Degree of Consolidation = 85.%

Total Settlement = .960

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 4320. = .960

Settlement caused by Secondary Compression at time 4320. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.50	2.43	1.26
1.88	1.81	.95
1.25	1.21	.63
.63	.60	.32
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
2.43	.00	.00
1.81	71.85	33.48

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
38.37	38.37	.00	1

1.21	143.19	66.97	76.22	76.22	.00	1
.60	214.36	100.45	113.90	113.90	.00	1
.00	285.43	133.94	151.49	151.49	.00	1

Time = 4320. Degree of Consolidation = 100.%

Total Settlement = .072

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 4320. = .072

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .07

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.60	21.42	6.50	6.10	6.10	6
60.02	59.07	21.35	6.49	6.08	6.08	6
59.45	58.53	21.27	6.47	6.07	6.07	6
58.89	58.00	21.20	6.46	6.05	6.05	6
58.33	57.47	21.12	6.44	6.04	6.04	6
57.76	56.94	21.05	6.43	6.03	6.03	6
57.20	56.41	20.97	6.42	6.01	6.01	6
56.64	55.88	20.90	6.40	6.00	6.00	6
56.08	55.35	20.82	6.39	5.98	5.98	6
56.08	55.35	20.82	4.51	4.18	4.18	5
54.82	54.16	20.59	4.44	4.11	4.11	5
53.56	52.98	20.36	4.38	4.05	4.05	5
52.32	51.82	20.12	4.32	3.98	3.98	5
51.10	50.67	19.89	4.25	3.92	3.92	5
49.88	49.53	19.66	4.19	3.86	3.86	5
48.69	48.42	19.43	4.13	3.79	3.79	5
48.69	48.42	19.43	1.93	1.91	1.91	4
46.69	46.43	18.75	1.92	1.90	1.90	4
44.70	44.46	18.06	1.91	1.88	1.88	4
42.72	42.50	17.38	1.89	1.87	1.87	4
40.75	40.54	16.70	1.88	1.85	1.84	4
38.79	38.60	16.01	1.86	1.83	1.82	4
36.85	36.68	15.33	1.84	1.81	1.80	4
34.91	34.76	14.65	1.82	1.79	1.78	4
33.00	32.86	13.97	1.80	1.77	1.76	4
31.09	30.97	13.28	1.78	1.75	1.74	4
31.09	30.97	13.28	1.47	1.46	1.45	3
29.70	29.59	12.72	1.46	1.45	1.44	3
28.32	28.22	12.16	1.45	1.44	1.43	3
26.94	26.85	11.59	1.44	1.43	1.42	3
25.57	25.48	11.03	1.43	1.42	1.41	3
24.21	24.13	10.47	1.42	1.41	1.40	3
22.84	22.77	9.90	1.41	1.40	1.39	3
21.49	21.43	9.34	1.40	1.39	1.38	3
20.14	20.08	8.78	1.39	1.38	1.37	3

18.80	18.75	8.21	1.38	1.37	1.36	3
18.80	18.75	8.21	1.34	1.33	1.32	2
16.88	16.84	7.39	1.33	1.32	1.31	2
14.97	14.94	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.16	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.60	285.43	133.94	151.49	151.49	.00	6
59.07	323.47	138.56	184.91	184.91	.00	6
58.53	361.44	143.18	218.26	218.26	.00	6
58.00	399.35	147.80	251.55	251.55	.00	6
57.47	437.19	152.42	284.77	284.77	.00	6
56.94	474.97	157.04	317.93	317.93	.00	6
56.41	512.68	161.66	351.01	351.01	.00	6
55.88	550.32	166.28	384.04	384.04	.00	6
55.35	587.90	170.90	416.99	416.99	.00	6
55.35	587.90	170.90	416.99	416.99	.00	5
54.16	688.06	196.65	491.41	491.41	.00	5
52.98	787.31	222.40	564.91	564.91	.00	5
51.82	885.63	248.15	637.48	637.48	.00	5
50.67	983.03	273.90	709.12	709.12	.00	5
49.53	1079.50	299.65	779.85	779.85	.00	5
48.42	1175.05	325.40	849.65	849.65	.00	5
48.42	1175.05	325.40	849.65	849.65	.00	4
46.43	1374.58	398.54	976.04	973.32	2.72	4
44.46	1573.64	477.12	1096.51	1096.52	.00	4
42.50	1772.03	547.95	1224.07	1219.05	5.03	4
40.54	1969.68	610.57	1359.11	1340.84	18.27	4
38.60	2166.58	674.18	1492.40	1461.88	30.52	4
36.68	2362.71	739.33	1623.38	1582.15	41.22	4
34.76	2558.05	806.79	1751.26	1701.64	49.63	4
32.86	2752.57	877.68	1874.89	1820.30	54.59	4
30.97	2946.21	954.71	1991.50	1938.08	53.43	4
30.97	2946.21	954.71	1991.50	1938.08	53.43	3
29.59	3094.27	1017.22	2077.06	2024.28	52.78	3
28.22	3241.95	1085.31	2156.64	2110.10	46.54	3
26.85	3389.26	1150.91	2238.34	2195.55	42.80	3
25.48	3536.20	1215.00	2321.19	2280.63	40.56	3
24.13	3682.78	1277.77	2405.01	2365.35	39.66	3
22.77	3829.01	1338.73	2490.28	2449.73	40.56	3
21.43	3974.91	1397.90	2577.01	2533.76	43.24	3
20.08	4120.48	1455.45	2665.03	2617.47	47.55	3
18.75	4265.73	1511.53	2754.20	2700.86	53.33	3
18.75	4265.73	1511.53	2754.20	2700.86	53.33	2
16.84	4470.94	1585.19	2885.75	2819.98	65.77	2
14.94	4675.69	1659.53	3016.17	2938.63	77.53	2
13.04	4879.99	1734.78	3145.21	3056.83	88.38	2
11.16	5083.82	1811.22	3272.60	3174.56	98.03	2
9.28	5287.17	1889.16	3398.01	3291.82	106.19	2
7.41	5490.04	1969.00	3521.04	3408.59	112.45	2
5.54	5692.42	2074.67	3617.75	3524.87	92.88	2
3.69	5894.30	2194.18	3700.12	3640.65	59.47	2
1.84	6095.70	2311.05	3784.65	3755.95	28.70	2

.00	6296.62	2425.61	3871.01	3870.77	.24	2

Time = 5040. Degree of Consolidation = 87.%

Total Settlement = .980

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 5040. = .980

Settlement caused by Secondary Compression at time 5040. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.85	33.48	38.37	38.37	.00	1
1.21	143.19	66.97	76.22	76.22	.00	1
.60	214.36	100.45	113.90	113.90	.00	1
.00	285.43	133.94	151.49	151.49	.00	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .072

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 5040. = .072

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .05

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.59	21.42	6.50	6.10	6.10	6

60.02	59.06	21.35	6.49	6.08	6.08	6
59.45	58.52	21.27	6.47	6.07	6.07	6
58.89	57.99	21.20	6.46	6.05	6.05	6
58.33	57.46	21.12	6.44	6.04	6.04	6
57.76	56.93	21.05	6.43	6.03	6.03	6
57.20	56.40	20.97	6.42	6.01	6.01	6
56.64	55.87	20.90	6.40	6.00	6.00	6
56.08	55.34	20.82	6.39	5.98	5.98	6
56.08	55.34	20.82	4.51	4.18	4.18	5
54.82	54.15	20.59	4.44	4.11	4.11	5
53.56	52.97	20.36	4.38	4.05	4.05	5
52.32	51.80	20.12	4.32	3.98	3.98	5
51.10	50.66	19.89	4.25	3.92	3.92	5
49.88	49.52	19.66	4.19	3.86	3.86	5
48.69	48.40	19.43	4.13	3.79	3.79	5
48.69	48.40	19.43	1.93	1.91	1.91	4
46.69	46.42	18.75	1.92	1.90	1.90	4
44.70	44.45	18.06	1.91	1.88	1.88	4
42.72	42.48	17.38	1.89	1.87	1.87	4
40.75	40.53	16.70	1.88	1.85	1.84	4
38.79	38.59	16.01	1.86	1.83	1.82	4
36.85	36.67	15.33	1.84	1.81	1.80	4
34.91	34.75	14.65	1.82	1.79	1.78	4
33.00	32.85	13.97	1.80	1.77	1.76	4
31.09	30.96	13.28	1.78	1.75	1.74	4
31.09	30.96	13.28	1.47	1.46	1.45	3
29.70	29.58	12.72	1.46	1.45	1.44	3
28.32	28.21	12.16	1.45	1.44	1.43	3
26.94	26.84	11.59	1.44	1.42	1.42	3
25.57	25.48	11.03	1.43	1.41	1.41	3
24.21	24.12	10.47	1.42	1.40	1.40	3
22.84	22.77	9.90	1.41	1.39	1.39	3
21.49	21.42	9.34	1.40	1.39	1.38	3
20.14	20.08	8.78	1.39	1.38	1.37	3
18.80	18.75	8.21	1.38	1.37	1.36	3
18.80	18.75	8.21	1.34	1.33	1.32	2
16.88	16.84	7.39	1.33	1.32	1.31	2
14.97	14.94	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.16	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.59	285.43	133.94	151.49	151.49	.00	6
59.06	323.47	138.56	184.91	184.91	.00	6
58.52	361.44	143.18	218.26	218.26	.00	6
57.99	399.35	147.80	251.55	251.55	.00	6
57.46	437.19	152.42	284.77	284.77	.00	6
56.93	474.97	157.04	317.93	317.93	.00	6
56.40	512.68	161.66	351.01	351.01	.00	6
55.87	550.32	166.28	384.04	384.04	.00	6
55.34	587.90	170.90	416.99	416.99	.00	6
55.34	587.90	170.90	416.99	416.99	.00	5
54.15	688.06	196.65	491.41	491.41	.00	5
52.97	787.31	222.40	564.91	564.91	.00	5

51.80	885.63	248.15	637.48	637.48	.00	5
50.66	983.03	273.90	709.12	709.12	.00	5
49.52	1079.50	299.65	779.85	779.85	.00	5
48.40	1175.05	325.40	849.65	849.65	.00	5
48.40	1175.05	325.40	849.65	849.65	.00	4
46.42	1374.58	398.54	976.04	973.32	2.72	4
44.45	1573.64	477.12	1096.52	1096.52	.00	4
42.48	1772.02	548.46	1223.56	1219.04	4.51	4
40.53	1969.67	611.65	1358.02	1340.83	17.19	4
38.59	2166.55	675.88	1490.67	1461.85	28.81	4
36.67	2362.66	741.75	1620.91	1582.10	38.81	4
34.75	2557.97	810.03	1747.93	1701.55	46.38	4
32.85	2752.44	881.94	1870.50	1820.16	50.33	4
30.96	2946.02	960.14	1985.88	1937.89	48.00	4
30.96	2946.02	960.14	1985.88	1937.89	48.00	3
29.58	3094.05	1023.97	2070.08	2024.06	46.02	3
28.21	3241.69	1092.42	2149.27	2109.84	39.43	3
26.84	3388.95	1158.37	2230.58	2195.24	35.34	3
25.48	3535.85	1222.46	2313.39	2280.28	33.11	3
24.12	3682.39	1284.84	2397.55	2364.96	32.59	3
22.77	3828.59	1345.29	2483.30	2449.30	34.00	3
21.42	3974.45	1403.97	2570.47	2533.30	37.17	3
20.08	4119.98	1461.06	2658.92	2616.98	41.94	3
18.75	4265.20	1516.70	2748.50	2700.34	48.16	3
18.75	4265.20	1516.70	2748.50	2700.34	48.16	2
16.84	4470.38	1589.89	2880.49	2819.42	61.07	2
14.94	4675.11	1663.77	3011.34	2938.05	73.29	2
13.04	4879.38	1738.55	3140.83	3056.22	84.60	2
11.16	5083.19	1814.52	3268.67	3173.93	94.74	2
9.28	5286.53	1891.97	3394.55	3291.17	103.38	2
7.41	5489.38	1971.31	3518.07	3407.93	110.15	2
5.54	5691.74	2077.28	3614.46	3524.19	90.27	2
3.69	5893.61	2195.88	3697.73	3639.97	57.77	2
1.84	6095.01	2311.88	3783.12	3755.26	27.86	2
.00	6295.93	2425.61	3870.31	3870.08	.23	2

Time = 5475. Degree of Consolidation = 88.%

Total Settlement = .991

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 5475. = .991

Settlement caused by Secondary Compression at time 5475. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

XI	Total Stresses	Effective Stresses	Total Pore Pressures	Static Pore Pressures	Excess Pore Pressures	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.85	33.48	38.37	38.37	.00	1
1.21	143.19	66.97	76.22	76.22	.00	1
.60	214.36	100.45	113.90	113.90	.00	1
.00	285.43	133.94	151.49	151.49	.00	1

Time = 5475. Degree of Consolidation = 100.%

Total Settlement = .072

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 5475. = .072

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .04

**********Current Conditions in Compressible Foundation**********

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.57	21.42	6.50	6.10	6.10	6
60.02	59.03	21.35	6.49	6.08	6.08	6
59.45	58.50	21.27	6.47	6.07	6.07	6
58.89	57.96	21.20	6.46	6.05	6.05	6
58.33	57.43	21.12	6.44	6.04	6.04	6
57.76	56.90	21.05	6.43	6.03	6.03	6
57.20	56.37	20.97	6.42	6.01	6.01	6
56.64	55.84	20.90	6.40	6.00	6.00	6
56.08	55.31	20.82	6.39	5.98	5.98	6
56.08	55.31	20.82	4.51	4.18	4.18	5
54.82	54.12	20.59	4.44	4.11	4.11	5
53.56	52.94	20.36	4.38	4.05	4.05	5
52.32	51.78	20.12	4.32	3.98	3.98	5
51.10	50.63	19.89	4.25	3.92	3.92	5
49.88	49.50	19.66	4.19	3.86	3.86	5
48.69	48.38	19.43	4.13	3.79	3.79	5
48.69	48.38	19.43	1.93	1.91	1.91	4
46.69	46.39	18.75	1.92	1.90	1.90	4
44.70	44.42	18.06	1.91	1.88	1.88	4
42.72	42.46	17.38	1.89	1.87	1.87	4
40.75	40.51	16.70	1.88	1.85	1.84	4
38.79	38.57	16.01	1.86	1.83	1.82	4
36.85	36.64	15.33	1.84	1.81	1.80	4
34.91	34.73	14.65	1.82	1.79	1.78	4
33.00	32.83	13.97	1.80	1.77	1.76	4
31.09	30.94	13.28	1.78	1.75	1.74	4
31.09	30.94	13.28	1.47	1.45	1.45	3
29.70	29.56	12.72	1.46	1.44	1.44	3
28.32	28.19	12.16	1.45	1.43	1.43	3
26.94	26.82	11.59	1.44	1.42	1.42	3

25.57	25.46	11.03	1.43	1.41	1.41	3
24.21	24.11	10.47	1.42	1.40	1.40	3
22.84	22.76	9.90	1.41	1.39	1.39	3
21.49	21.41	9.34	1.40	1.38	1.38	3
20.14	20.07	8.78	1.39	1.37	1.37	3
18.80	18.74	8.21	1.38	1.36	1.36	3
18.80	18.74	8.21	1.34	1.33	1.32	2
16.88	16.83	7.39	1.33	1.32	1.31	2
14.97	14.93	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.57	285.43	133.94	151.49	151.49	.00	6
59.03	323.47	138.56	184.91	184.91	.00	6
58.50	361.44	143.18	218.26	218.26	.00	6
57.96	399.35	147.80	251.55	251.55	.00	6
57.43	437.19	152.42	284.77	284.77	.00	6
56.90	474.97	157.04	317.93	317.93	.00	6
56.37	512.68	161.66	351.01	351.01	.00	6
55.84	550.32	166.28	384.04	384.04	.00	6
55.31	587.90	170.90	416.99	416.99	.00	6
55.31	587.90	170.90	416.99	416.99	.00	5
54.12	688.06	196.65	491.41	491.41	.00	5
52.94	787.31	222.40	564.91	564.91	.00	5
51.78	885.63	248.15	637.48	637.48	.00	5
50.63	983.03	273.90	709.12	709.12	.00	5
49.50	1079.50	299.65	779.85	779.85	.00	5
48.38	1175.05	325.40	849.65	849.65	.00	5
48.38	1175.05	325.40	849.65	849.65	.00	4
46.39	1374.58	398.54	976.04	973.32	2.72	4
44.42	1573.64	477.12	1096.52	1096.52	.00	4
42.46	1772.02	549.64	1222.38	1219.04	3.34	4
40.51	1969.64	614.12	1355.52	1340.80	14.72	4
38.57	2166.49	679.80	1486.69	1461.79	24.90	4
36.64	2362.54	747.30	1615.24	1581.98	33.26	4
34.73	2557.77	817.52	1740.25	1701.35	38.90	4
32.83	2752.14	891.83	1860.31	1819.86	40.45	4
30.94	2945.58	973.33	1972.25	1937.45	34.80	4
30.94	2945.58	973.33	1972.25	1937.45	34.80	3
29.56	3093.52	1039.87	2053.65	2023.53	30.12	3
28.19	3241.07	1108.64	2132.43	2109.22	23.21	3
26.82	3388.24	1174.94	2213.30	2194.53	18.77	3
25.46	3535.05	1238.98	2296.07	2279.48	16.59	3
24.11	3681.50	1300.95	2380.54	2364.07	16.47	3
22.76	3827.60	1361.04	2466.56	2448.32	18.25	3
21.41	3973.38	1419.40	2553.97	2532.23	21.74	3
20.07	4118.83	1476.21	2642.62	2615.82	26.80	3
18.74	4263.96	1531.60	2732.36	2699.10	33.26	3
18.74	4263.96	1531.60	2732.36	2699.10	33.26	2
16.83	4469.05	1603.45	2865.60	2818.09	47.51	2
14.93	4673.70	1675.98	2997.72	2936.64	61.08	2
13.04	4877.90	1749.41	3128.49	3054.75	73.75	2
11.15	5081.65	1824.00	3257.65	3172.39	85.26	2

9.28	5284.93	1900.04	3384.89	3289.58	95.31	2
7.41	5487.74	1977.93	3509.81	3406.29	103.52	2
5.54	5690.07	2084.77	3605.30	3522.52	82.78	2
3.69	5891.91	2200.76	3691.15	3638.27	52.89	2
1.84	6093.29	2314.28	3779.01	3753.54	25.47	2
.00	6294.21	2425.63	3868.57	3868.36	.21	2

Time = 6480. Degree of Consolidation = 90.%

Total Settlement = 1.019

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 6480. = 1.019

Settlement caused by Secondary Compression at time 6480. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1
1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.85	33.48	38.37	38.37	.00	1
1.21	143.19	66.97	76.22	76.22	.00	1
.60	214.36	100.45	113.90	113.90	.00	1
.00	285.43	133.94	151.49	151.49	.00	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .072

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 6480. = .072

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .01

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.56	21.42	6.50	6.10	6.10	6
60.02	59.03	21.35	6.49	6.08	6.08	6
59.45	58.49	21.27	6.47	6.07	6.07	6
58.89	57.96	21.20	6.46	6.05	6.05	6
58.33	57.43	21.12	6.44	6.04	6.04	6
57.76	56.90	21.05	6.43	6.03	6.03	6
57.20	56.37	20.97	6.42	6.01	6.01	6
56.64	55.84	20.90	6.40	6.00	6.00	6
56.08	55.31	20.82	6.39	5.98	5.98	6
56.08	55.31	20.82	4.51	4.18	4.18	5
54.82	54.12	20.59	4.44	4.11	4.11	5
53.56	52.94	20.36	4.38	4.05	4.05	5
52.32	51.78	20.12	4.32	3.98	3.98	5
51.10	50.63	19.89	4.25	3.92	3.92	5
49.88	49.50	19.66	4.19	3.86	3.86	5
48.69	48.38	19.43	4.13	3.79	3.79	5
48.69	48.38	19.43	1.93	1.91	1.91	4
46.69	46.39	18.75	1.92	1.90	1.90	4
44.70	44.42	18.06	1.91	1.88	1.88	4
42.72	42.46	17.38	1.89	1.87	1.87	4
40.75	40.51	16.70	1.88	1.85	1.84	4
38.79	38.57	16.01	1.86	1.83	1.82	4
36.85	36.64	15.33	1.84	1.81	1.80	4
34.91	34.73	14.65	1.82	1.79	1.78	4
33.00	32.83	13.97	1.80	1.77	1.76	4
31.09	30.94	13.28	1.78	1.75	1.74	4
31.09	30.94	13.28	1.47	1.45	1.45	3
29.70	29.56	12.72	1.46	1.44	1.44	3
28.32	28.19	12.16	1.45	1.43	1.43	3
26.94	26.82	11.59	1.44	1.42	1.42	3
25.57	25.46	11.03	1.43	1.41	1.41	3
24.21	24.11	10.47	1.42	1.40	1.40	3
22.84	22.76	9.90	1.41	1.39	1.39	3
21.49	21.41	9.34	1.40	1.38	1.38	3
20.14	20.07	8.78	1.39	1.37	1.37	3
18.80	18.74	8.21	1.38	1.36	1.36	3
18.80	18.74	8.21	1.34	1.33	1.32	2
16.88	16.83	7.39	1.33	1.32	1.31	2
14.97	14.93	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.56	285.43	133.94	151.49	151.49	.00	6
59.03	323.47	138.56	184.91	184.91	.00	6
58.49	361.44	143.18	218.26	218.26	.00	6
57.96	399.35	147.80	251.55	251.55	.00	6
57.43	437.19	152.42	284.77	284.77	.00	6
56.90	474.97	157.04	317.93	317.93	.00	6
56.37	512.68	161.66	351.01	351.01	.00	6

55.84	550.32	166.28	384.04	384.04	.00	6
55.31	587.90	170.90	416.99	416.99	.00	6
55.31	587.90	170.90	416.99	416.99	.00	5
54.12	688.06	196.65	491.41	491.41	.00	5
52.94	787.31	222.40	564.91	564.91	.00	5
51.78	885.63	248.15	637.48	637.48	.00	5
50.63	983.03	273.90	709.12	709.12	.00	5
49.50	1079.50	299.65	779.85	779.85	.00	5
48.38	1175.05	325.40	849.65	849.65	.00	5
48.38	1175.05	325.40	849.65	849.65	.00	4
46.39	1374.58	398.54	976.04	973.32	2.72	4
44.42	1573.64	477.12	1096.52	1096.52	.00	4
42.46	1772.02	549.71	1222.31	1219.04	3.27	4
40.51	1969.64	614.27	1355.37	1340.80	14.57	4
38.57	2166.48	680.03	1486.45	1461.78	24.67	4
36.64	2362.53	747.63	1614.90	1581.97	32.92	4
34.73	2557.76	817.97	1739.78	1701.34	38.44	4
32.83	2752.12	892.43	1859.69	1819.84	39.85	4
30.94	2945.56	973.33	1972.23	1937.43	34.80	4
30.94	2945.56	973.33	1972.23	1937.43	34.80	3
29.56	3093.50	1039.87	2053.63	2023.51	30.12	3
28.19	3241.05	1108.65	2132.40	2109.20	23.21	3
26.82	3388.22	1174.95	2213.27	2194.51	18.76	3
25.46	3535.02	1238.99	2296.03	2279.46	16.58	3
24.11	3681.47	1300.96	2380.51	2364.05	16.46	3
22.76	3827.58	1361.05	2466.53	2448.29	18.24	3
21.41	3973.35	1419.41	2553.94	2532.21	21.73	3
20.07	4118.80	1476.21	2642.59	2615.80	26.79	3
18.74	4263.94	1531.60	2732.34	2699.08	33.26	3
18.74	4263.94	1531.60	2732.34	2699.08	33.26	2
16.83	4469.03	1603.45	2865.58	2818.07	47.51	2
14.93	4673.68	1675.98	2997.69	2936.62	61.07	2
13.04	4877.88	1749.41	3128.47	3054.72	73.74	2
11.15	5081.62	1824.00	3257.63	3172.37	85.26	2
9.28	5284.91	1900.05	3384.86	3289.55	95.31	2
7.41	5487.72	1977.93	3509.79	3406.27	103.52	2
5.54	5690.04	2084.77	3605.27	3522.49	82.78	2
3.69	5891.89	2200.76	3691.13	3638.24	52.88	2
1.84	6093.27	2314.28	3778.99	3753.52	25.47	2
.00	6294.18	2425.63	3868.55	3868.34	.21	2

Time = 7300. Degree of Consolidation = 90.%

Total Settlement = 1.019

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 7300. = 1.019

Settlement caused by Secondary Compression at time 7300. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.50	2.43	1.26	.98	.98	.98	1
1.88	1.81	.95	.98	.93	.93	1

1.25	1.21	.63	.98	.92	.92	1
.63	.60	.32	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.43	.00	.00	.00	.00	.00	1
1.81	71.85	33.48	38.37	38.37	.00	1
1.21	143.19	66.97	76.22	76.22	.00	1
.60	214.36	100.45	113.90	113.90	.00	1
.00	285.43	133.94	151.49	151.49	.00	1

Time = 7300. Degree of Consolidation = 100.%

Total Settlement = .072

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 7300. = .072

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .01

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.56	21.42	6.50	6.10	6.10	6
60.02	59.03	21.35	6.49	6.08	6.08	6
59.45	58.49	21.27	6.47	6.07	6.07	6
58.89	57.96	21.20	6.46	6.05	6.05	6
58.33	57.43	21.12	6.44	6.04	6.04	6
57.76	56.90	21.05	6.43	6.03	6.03	6
57.20	56.37	20.97	6.42	6.01	6.01	6
56.64	55.84	20.90	6.40	6.00	6.00	6
56.08	55.31	20.82	6.39	5.98	5.98	6
56.08	55.31	20.82	4.51	4.18	4.18	5
54.82	54.12	20.59	4.44	4.11	4.11	5
53.56	52.94	20.36	4.38	4.05	4.05	5
52.32	51.78	20.12	4.32	3.98	3.98	5
51.10	50.63	19.89	4.25	3.92	3.92	5
49.88	49.50	19.66	4.19	3.86	3.86	5
48.69	48.38	19.43	4.13	3.79	3.79	5
48.69	48.38	19.43	1.93	1.91	1.91	4
46.69	46.39	18.75	1.92	1.90	1.90	4
44.70	44.42	18.06	1.91	1.88	1.88	4
42.72	42.46	17.38	1.89	1.87	1.87	4
40.75	40.51	16.70	1.88	1.85	1.84	4
38.79	38.57	16.01	1.86	1.83	1.82	4
36.85	36.64	15.33	1.84	1.81	1.80	4
34.91	34.73	14.65	1.82	1.79	1.78	4
33.00	32.83	13.97	1.80	1.77	1.76	4

31.09	30.94	13.28	1.78	1.75	1.74	4
31.09	30.94	13.28	1.47	1.45	1.45	3
29.70	29.56	12.72	1.46	1.44	1.44	3
28.32	28.19	12.16	1.45	1.43	1.43	3
26.94	26.82	11.59	1.44	1.42	1.42	3
25.57	25.46	11.03	1.43	1.41	1.41	3
24.21	24.11	10.47	1.42	1.40	1.40	3
22.84	22.76	9.90	1.41	1.39	1.39	3
21.49	21.41	9.34	1.40	1.38	1.38	3
20.14	20.07	8.78	1.39	1.37	1.37	3
18.80	18.74	8.21	1.38	1.36	1.36	3
18.80	18.74	8.21	1.34	1.33	1.32	2
16.88	16.83	7.39	1.33	1.32	1.31	2
14.97	14.93	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.26	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.56	285.43	133.94	151.49	151.49	.00	6
59.03	323.47	138.56	184.91	184.91	.00	6
58.49	361.44	143.18	218.26	218.26	.00	6
57.96	399.35	147.80	251.55	251.55	.00	6
57.43	437.19	152.42	284.77	284.77	.00	6
56.90	474.97	157.04	317.93	317.93	.00	6
56.37	512.68	161.66	351.01	351.01	.00	6
55.84	550.32	166.28	384.04	384.04	.00	6
55.31	587.90	170.90	416.99	416.99	.00	6
55.31	587.90	170.90	416.99	416.99	.00	5
54.12	688.06	196.65	491.41	491.41	.00	5
52.94	787.31	222.40	564.91	564.91	.00	5
51.78	885.63	248.15	637.48	637.48	.00	5
50.63	983.03	273.90	709.12	709.12	.00	5
49.50	1079.50	299.65	779.85	779.85	.00	5
48.38	1175.05	325.40	849.65	849.65	.00	5
48.38	1175.05	325.40	849.65	849.65	.00	4
46.39	1374.58	398.54	976.04	973.32	2.72	4
44.42	1573.64	477.12	1096.52	1096.52	.00	4
42.46	1772.02	549.71	1222.31	1219.04	3.27	4
40.51	1969.64	614.27	1355.37	1340.80	14.57	4
38.57	2166.48	680.03	1486.45	1461.78	24.67	4
36.64	2362.53	747.63	1614.90	1581.97	32.92	4
34.73	2557.76	817.97	1739.78	1701.34	38.44	4
32.83	2752.12	892.43	1859.69	1819.84	39.85	4
30.94	2945.56	973.33	1972.23	1937.43	34.80	4
30.94	2945.56	973.33	1972.23	1937.43	34.80	3
29.56	3093.50	1039.87	2053.63	2023.51	30.12	3
28.19	3241.05	1108.65	2132.40	2109.20	23.21	3
26.82	3388.22	1174.95	2213.27	2194.51	18.76	3
25.46	3535.02	1238.99	2296.03	2279.46	16.58	3
24.11	3681.47	1300.96	2380.51	2364.05	16.46	3
22.76	3827.58	1361.05	2466.53	2448.29	18.24	3
21.41	3973.35	1419.41	2553.94	2532.21	21.73	3
20.07	4118.80	1476.21	2642.59	2615.80	26.79	3
18.74	4263.94	1531.60	2732.34	2699.08	33.26	3

18.74	4263.94	1531.60	2732.34	2699.08	33.26	2
16.83	4469.03	1603.45	2865.58	2818.07	47.51	2
14.93	4673.68	1675.98	2997.69	2936.62	61.07	2
13.04	4877.88	1749.41	3128.47	3054.72	73.74	2
11.15	5081.62	1824.00	3257.63	3172.37	85.26	2
9.28	5284.91	1900.05	3384.86	3289.55	95.31	2
7.41	5487.72	1977.93	3509.79	3406.27	103.52	2
5.54	5690.04	2084.77	3605.27	3522.49	82.78	2
3.69	5891.89	2200.76	3691.13	3638.24	52.88	2
1.84	6093.27	2314.28	3778.99	3753.52	25.47	2
.00	6294.18	2425.63	3868.55	3868.34	.21	2

Time = 9125. Degree of Consolidation = 90.%

Total Settlement = 1.019

Settlement at End of Primary Consolidation = 1.127

Settlement caused by Primary Consolidation at time 9125. = 1.019

Settlement caused by Secondary Compression at time 9125. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.50	2.43	1.26
1.88	1.81	.95
1.25	1.21	.63
.63	.60	.32
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
2.43	.00	.00
1.81	71.85	33.48
1.21	143.19	66.97
.60	214.36	100.45
.00	285.43	133.94

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
38.37	38.37	.00	1
76.22	76.22	.00	1
113.90	113.90	.00	1
151.49	151.49	.00	1

Time = 9125. Degree of Consolidation = 100.%

Total Settlement = .072

Settlement at End of Primary Consolidation = .072

Settlement caused by Primary Consolidation at time 9125. = .072

Settlement caused by Secondary Compression at time 9125. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .01

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou Dupont - 2ft Fill Height

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	2.0	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.277E-01	1.106	.30000E-04	z = .05

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	6.18	6
60.02	60.02	21.35	6.49	6.49	6.16	6
59.45	59.45	21.27	6.47	6.47	6.15	6
58.89	58.89	21.20	6.46	6.46	6.13	6

58.33	58.33	21.12	6.44	6.44	6.12	6
57.76	57.76	21.05	6.43	6.43	6.11	6
57.20	57.20	20.97	6.42	6.42	6.09	6
56.64	56.64	20.90	6.40	6.40	6.08	6
56.08	56.08	20.82	6.39	6.39	6.06	6
56.08	56.08	20.82	4.51	4.51	4.24	5
54.82	54.82	20.59	4.44	4.44	4.18	5
53.56	53.56	20.36	4.38	4.38	4.11	5
52.32	52.32	20.12	4.32	4.32	4.05	5
51.10	51.10	19.89	4.25	4.25	3.99	5
49.88	49.88	19.66	4.19	4.19	3.92	5
48.69	48.69	19.43	4.13	4.13	3.86	5
48.69	48.69	19.43	1.93	1.93	1.91	4
46.69	46.69	18.75	1.92	1.92	1.90	4
44.70	44.70	18.06	1.91	1.91	1.89	4
42.72	42.72	17.38	1.89	1.89	1.87	4
40.75	40.75	16.70	1.88	1.88	1.85	4
38.79	38.79	16.01	1.86	1.86	1.83	4
36.85	36.85	15.33	1.84	1.84	1.81	4
34.91	34.91	14.65	1.82	1.82	1.79	4
33.00	33.00	13.97	1.80	1.80	1.77	4
31.09	31.09	13.28	1.78	1.78	1.75	4
31.09	31.09	13.28	1.47	1.47	1.45	3
29.70	29.70	12.72	1.46	1.46	1.44	3
28.32	28.32	12.16	1.45	1.45	1.43	3
26.94	26.94	11.59	1.44	1.44	1.42	3
25.57	25.57	11.03	1.43	1.43	1.41	3
24.21	24.21	10.47	1.42	1.42	1.40	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.49	9.34	1.40	1.40	1.38	3
20.14	20.14	8.78	1.39	1.39	1.37	3
18.80	18.80	8.21	1.38	1.38	1.36	3
18.80	18.80	8.21	1.34	1.34	1.33	2
16.88	16.88	7.39	1.33	1.33	1.32	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.30	4.11	1.29	1.29	1.27	2
7.43	7.43	3.29	1.28	1.28	1.27	2
5.56	5.56	2.46	1.27	1.27	1.26	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.85	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.25	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	231.95	.00	231.95	124.80	107.15	6
60.02	271.90	4.62	267.28	160.13	107.15	6
59.45	311.78	9.24	302.54	195.39	107.15	6
58.89	351.60	13.86	337.74	230.58	107.15	6
58.33	391.35	18.48	372.87	265.71	107.15	6
57.76	431.03	23.10	407.93	300.78	107.15	6
57.20	470.65	27.72	442.93	335.78	107.15	6
56.64	510.20	32.34	477.86	370.71	107.15	6
56.08	549.69	36.96	512.73	405.57	107.15	6
56.08	549.69	36.96	512.73	405.57	107.15	5
54.82	654.66	62.71	591.95	484.80	107.15	5
53.56	758.71	88.46	670.25	563.10	107.15	5
52.32	861.84	114.21	747.62	640.47	107.15	5
51.10	964.04	139.96	824.08	716.92	107.15	5
49.88	1065.32	165.71	899.60	792.45	107.15	5

48.69	1165.67	191.46	974.21	867.06	107.15	5
48.69	1165.67	191.46	974.21	867.06	107.15	4
46.69	1366.11	267.32	1098.79	991.64	107.15	4
44.70	1566.05	343.18	1222.87	1115.72	107.15	4
42.72	1765.45	419.04	1346.41	1239.26	107.15	4
40.75	1964.40	494.90	1469.50	1362.34	107.15	4
38.79	2162.59	570.76	1591.83	1484.68	107.15	4
36.85	2359.89	646.62	1713.27	1606.12	107.15	4
34.91	2556.29	722.48	1833.81	1726.66	107.15	4
33.00	2751.78	798.34	1953.44	1846.29	107.15	4
31.09	2946.36	874.19	2072.17	1965.02	107.15	4
31.09	2946.36	874.19	2072.17	1965.02	107.15	3
29.70	3094.93	936.05	2158.88	2051.73	107.15	3
28.32	3243.10	997.91	2245.19	2138.04	107.15	3
26.94	3390.91	1059.77	2331.14	2223.99	107.15	3
25.57	3538.37	1121.63	2416.74	2309.59	107.15	3
24.21	3685.48	1183.49	2501.99	2394.84	107.15	3
22.84	3832.24	1245.35	2586.90	2479.74	107.15	3
21.49	3978.66	1307.21	2671.45	2564.30	107.15	3
20.14	4124.73	1369.06	2755.66	2648.51	107.15	3
18.80	4270.44	1430.92	2839.52	2732.37	107.15	3
18.80	4270.44	1430.92	2839.52	2732.37	107.15	2
16.88	4476.11	1517.02	2959.09	2851.94	107.15	2
14.97	4681.25	1603.12	3078.13	2970.98	107.15	2
13.07	4885.86	1689.22	3196.64	3089.49	107.15	2
11.18	5089.94	1775.31	3314.62	3207.47	107.15	2
9.30	5293.49	1861.41	3432.08	3324.93	107.15	2
7.43	5496.51	1947.51	3549.00	3441.85	107.15	2
5.56	5699.02	2033.61	3665.41	3558.26	107.15	2
3.70	5901.14	2119.71	3781.43	3674.28	107.15	2
1.85	6102.90	2205.80	3897.10	3789.94	107.15	2
.00	6304.31	2291.90	4012.41	3905.26	107.15	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	2.00	1.01	.98	.98	.98	1
1.50	1.50	.76	.98	.98	.93	1
1.00	1.00	.51	.98	.98	.92	1
.50	.50	.25	.98	.98	.91	1
.00	.00	.00	.98	.98	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

2.00	.00	.00	.00	.00	.00	1
1.50	57.99	.00	57.99	31.20	26.79	1
1.00	115.98	.00	115.98	62.40	53.58	1
.50	173.96	.00	173.96	93.60	80.36	1
.00	231.95	.00	231.95	124.80	107.15	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.53	21.42	6.50	6.22	6.18	6
60.02	59.98	21.35	6.49	6.29	6.16	6
59.45	59.43	21.27	6.47	6.35	6.15	6
58.89	58.87	21.20	6.46	6.39	6.13	6
58.33	58.31	21.12	6.44	6.41	6.12	6
57.76	57.75	21.05	6.43	6.41	6.11	6
57.20	57.19	20.97	6.42	6.41	6.09	6
56.64	56.63	20.90	6.40	6.40	6.08	6
56.08	56.07	20.82	6.39	6.39	6.06	6
56.08	56.07	20.82	4.51	4.51	4.24	5
54.82	54.81	20.59	4.44	4.44	4.18	5
53.56	53.55	20.36	4.38	4.38	4.11	5
52.32	52.31	20.12	4.32	4.31	4.05	5
51.10	51.09	19.89	4.25	4.25	3.99	5
49.88	49.88	19.66	4.19	4.19	3.92	5
48.69	48.68	19.43	4.13	4.12	3.86	5
48.69	48.68	19.43	1.93	1.93	1.91	4
46.69	46.69	18.75	1.92	1.92	1.90	4
44.70	44.70	18.06	1.91	1.91	1.89	4
42.72	42.72	17.38	1.89	1.89	1.87	4
40.75	40.75	16.70	1.88	1.88	1.85	4
38.79	38.79	16.01	1.86	1.86	1.83	4
36.85	36.84	15.33	1.84	1.84	1.81	4
34.91	34.91	14.65	1.82	1.82	1.79	4
33.00	32.99	13.97	1.80	1.80	1.77	4
31.09	31.09	13.28	1.78	1.78	1.75	4
31.09	31.09	13.28	1.47	1.47	1.45	3
29.70	29.70	12.72	1.46	1.46	1.44	3
28.32	28.32	12.16	1.45	1.45	1.43	3
26.94	26.94	11.59	1.44	1.44	1.42	3
25.57	25.57	11.03	1.43	1.43	1.41	3
24.21	24.20	10.47	1.42	1.42	1.40	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.49	9.34	1.40	1.40	1.38	3
20.14	20.14	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3
18.80	18.79	8.21	1.34	1.34	1.33	2

16.88	16.88	7.39	1.33	1.33	1.32	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.30	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.56	2.46	1.27	1.27	1.26	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.53	228.69	92.02	136.67	121.54	15.13	6
59.98	267.54	67.90	199.64	155.77	43.87	6
59.43	306.70	48.50	258.20	190.31	67.89	6
58.87	346.09	35.76	310.33	225.07	85.26	6
58.31	385.61	29.48	356.13	259.98	96.15	6
57.75	425.18	28.15	397.04	294.93	102.11	6
57.19	464.75	29.94	434.82	329.88	104.94	6
56.63	504.28	33.46	470.82	364.79	106.03	6
56.07	543.76	37.90	505.86	399.64	106.21	6
56.07	543.76	37.90	505.86	399.64	106.21	5
54.81	648.70	63.55	585.15	478.83	106.32	5
53.55	752.72	89.30	663.42	557.10	106.32	5
52.31	855.81	115.06	740.75	634.45	106.30	5
51.09	957.98	140.84	817.15	710.87	106.28	5
49.88	1059.23	166.60	892.64	786.37	106.27	5
48.68	1159.55	192.26	967.30	860.94	106.36	5
48.68	1159.55	192.26	967.30	860.94	106.36	4
46.69	1359.99	267.32	1092.67	985.52	107.15	4
44.70	1559.92	343.18	1216.74	1109.59	107.15	4
42.72	1759.32	421.74	1337.58	1233.13	104.45	4
40.75	1958.16	507.71	1450.44	1356.11	94.34	4
38.79	2156.28	573.61	1582.67	1478.37	104.30	4
36.84	2353.57	646.64	1706.93	1599.80	107.13	4
34.91	2549.96	722.48	1827.49	1720.34	107.15	4
32.99	2745.45	798.34	1947.12	1839.97	107.15	4
31.09	2940.04	874.19	2065.84	1958.69	107.15	4
31.09	2940.04	874.20	2065.84	1958.69	107.15	3
29.70	3088.61	936.05	2152.56	2045.40	107.15	3
28.32	3236.78	997.91	2238.87	2131.72	107.15	3
26.94	3384.58	1060.83	2323.75	2217.66	106.09	3
25.57	3532.04	1123.24	2408.79	2303.25	105.54	3
24.20	3679.14	1185.10	2494.04	2388.50	105.54	3
22.84	3825.89	1246.96	2578.93	2473.39	105.54	3
21.49	3972.30	1308.77	2663.52	2557.94	105.58	3
20.14	4118.36	1370.32	2748.03	2642.14	105.89	3
18.79	4264.07	1431.77	2832.30	2726.00	106.30	3
18.79	4264.07	1431.77	2832.30	2726.00	106.30	2
16.88	4469.74	1517.02	2952.71	2845.56	107.15	2
14.97	4674.87	1603.12	3071.76	2964.60	107.15	2
13.07	4879.48	1689.22	3190.27	3083.11	107.15	2
11.18	5083.56	1775.31	3308.25	3201.10	107.15	2
9.30	5287.12	1861.41	3425.70	3318.55	107.15	2
7.42	5490.13	1947.51	3542.62	3435.47	107.15	2
5.56	5692.65	2033.61	3659.04	3551.89	107.15	2
3.70	5894.76	2121.25	3773.51	3667.90	105.61	2
1.84	6096.51	2218.51	3878.00	3783.55	94.44	2
.00	6297.73	2390.81	3906.92	3898.67	8.25	2

Time = 30. Degree of Consolidation = 6.%

Total Settlement = .053

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 30. = .053

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.95	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.92	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.95	.00	.00	.00	.00	.00	1
1.45	57.56	22.67	34.89	30.77	4.12	1
.97	114.73	45.27	69.45	61.15	8.30	1
.48	171.75	70.22	101.53	91.39	10.15	1
.00	228.69	92.02	136.67	121.54	15.13	1

Time = 30. Degree of Consolidation = 96.%

Total Settlement = .052

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 30. = .052

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = .49

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.50	21.42	6.50	6.22	6.18	6
60.02	59.96	21.35	6.49	6.27	6.16	6
59.45	59.41	21.27	6.47	6.31	6.15	6
58.89	58.85	21.20	6.46	6.34	6.13	6
58.33	58.30	21.12	6.44	6.37	6.12	6

57.76	57.74	21.05	6.43	6.38	6.11	6
57.20	57.18	20.97	6.42	6.39	6.09	6
56.64	56.62	20.90	6.40	6.38	6.08	6
56.08	56.07	20.82	6.39	6.38	6.06	6
56.08	56.07	20.82	4.51	4.50	4.24	5
54.82	54.80	20.59	4.44	4.44	4.18	5
53.56	53.54	20.36	4.38	4.38	4.11	5
52.32	52.31	20.12	4.32	4.31	4.05	5
51.10	51.08	19.89	4.25	4.25	3.99	5
49.88	49.87	19.66	4.19	4.18	3.92	5
48.69	48.68	19.43	4.13	4.12	3.86	5
48.69	48.68	19.43	1.93	1.93	1.91	4
46.69	46.68	18.75	1.92	1.92	1.90	4
44.70	44.69	18.06	1.91	1.91	1.89	4
42.72	42.71	17.38	1.89	1.89	1.87	4
40.75	40.74	16.70	1.88	1.88	1.85	4
38.79	38.78	16.01	1.86	1.86	1.83	4
36.85	36.84	15.33	1.84	1.84	1.81	4
34.91	34.91	14.65	1.82	1.82	1.79	4
33.00	32.99	13.97	1.80	1.80	1.77	4
31.09	31.09	13.28	1.78	1.78	1.75	4
31.09	31.09	13.28	1.47	1.47	1.45	3
29.70	29.70	12.72	1.46	1.46	1.44	3
28.32	28.31	12.16	1.45	1.45	1.43	3
26.94	26.94	11.59	1.44	1.44	1.42	3
25.57	25.57	11.03	1.43	1.43	1.41	3
24.21	24.20	10.47	1.42	1.42	1.40	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.14	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3
18.80	18.79	8.21	1.34	1.34	1.33	2
16.88	16.88	7.39	1.33	1.33	1.32	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.30	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.56	2.46	1.27	1.27	1.26	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.50	228.54	92.29	136.25	121.38	14.86	6
59.96	267.31	76.97	190.34	155.54	34.80	6
59.41	306.30	63.09	243.21	189.91	53.30	6
58.85	345.46	51.82	293.65	224.45	69.20	6
58.30	384.77	43.82	340.95	259.13	81.82	6
57.74	424.16	39.19	384.97	293.91	91.06	6
57.18	463.60	37.58	426.02	328.72	97.29	6
56.62	503.04	38.36	464.68	363.55	101.14	6
56.07	542.46	40.85	501.61	398.34	103.26	6
56.07	542.46	40.85	501.61	398.34	103.26	5
54.80	647.32	65.35	581.96	477.45	104.51	5
53.54	751.28	90.56	660.72	555.67	105.05	5
52.31	854.34	116.11	738.23	632.97	105.25	5
51.08	956.47	141.78	814.70	709.36	105.34	5
49.87	1057.69	167.43	890.26	784.82	105.44	5
48.68	1157.98	193.01	964.97	859.37	105.60	5

48.68	1157.98	193.01	964.97	859.37	105.60	4
46.68	1358.42	267.32	1091.10	983.95	107.15	4
44.69	1558.34	343.56	1214.79	1108.01	106.77	4
42.71	1757.73	426.37	1331.36	1231.54	99.82	4
40.74	1956.52	512.81	1443.71	1354.47	89.24	4
38.78	2154.59	577.02	1577.56	1476.68	100.89	4
36.84	2351.85	647.60	1704.25	1598.08	106.17	4
34.91	2548.24	722.48	1825.76	1718.61	107.15	4
32.99	2743.73	798.34	1945.40	1838.24	107.15	4
31.09	2938.32	874.19	2064.12	1956.97	107.15	4
31.09	2938.32	874.20	2064.12	1956.97	107.15	3
29.70	3086.89	936.05	2150.83	2043.68	107.15	3
28.31	3235.06	997.91	2237.15	2130.00	107.15	3
26.94	3382.86	1061.64	2321.22	2215.94	105.28	3
25.57	3530.31	1124.55	2405.76	2301.52	104.24	3
24.20	3677.40	1186.72	2490.68	2386.76	103.92	3
22.84	3824.14	1248.57	2575.57	2471.65	103.92	3
21.48	3970.54	1310.05	2660.49	2556.18	104.31	3
20.14	4116.59	1371.27	2745.33	2640.38	104.95	3
18.79	4262.30	1432.39	2829.91	2724.23	105.68	3
18.79	4262.30	1432.39	2829.91	2724.23	105.68	2
16.88	4467.97	1517.02	2950.95	2843.80	107.15	2
14.97	4673.11	1603.12	3069.99	2962.84	107.15	2
13.07	4877.72	1689.22	3188.50	3081.35	107.15	2
11.18	5081.79	1775.31	3306.48	3199.33	107.15	2
9.30	5285.35	1861.41	3423.94	3316.78	107.15	2
7.42	5488.36	1947.51	3540.85	3433.70	107.15	2
5.56	5690.88	2033.61	3657.27	3550.12	107.15	2
3.70	5892.98	2124.48	3768.51	3666.13	102.38	2
1.84	6094.70	2231.05	3863.65	3781.74	81.91	2
.00	6295.88	2392.79	3903.09	3896.83	6.27	2

Time = 60. Degree of Consolidation = 9.%

Total Settlement = .080

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 60. = .080

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.00	1.95	1.01
1.50	1.45	.76
1.00	.97	.51
.50	.48	.25
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
1.95	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

1.45	57.53	26.79	30.74	30.74	.00	1
.97	114.65	53.58	61.07	61.07	.00	1
.48	171.63	80.36	91.26	91.26	.00	1
.00	228.54	107.15	121.39	121.38	.00	1

Time = 60. Degree of Consolidation = 100.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 60. = .055

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = .46

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.46	21.42	6.50	6.19	6.18	6
60.02	59.91	21.35	6.49	6.22	6.16	6
59.45	59.36	21.27	6.47	6.26	6.15	6
58.89	58.81	21.20	6.46	6.29	6.13	6
58.33	58.26	21.12	6.44	6.31	6.12	6
57.76	57.71	21.05	6.43	6.33	6.11	6
57.20	57.16	20.97	6.42	6.34	6.09	6
56.64	56.60	20.90	6.40	6.35	6.08	6
56.08	56.04	20.82	6.39	6.35	6.06	6
56.08	56.04	20.82	4.51	4.48	4.24	5
54.82	54.78	20.59	4.44	4.42	4.18	5
53.56	53.53	20.36	4.38	4.36	4.11	5
52.32	52.29	20.12	4.32	4.30	4.05	5
51.10	51.07	19.89	4.25	4.24	3.99	5
49.88	49.86	19.66	4.19	4.18	3.92	5
48.69	48.67	19.43	4.13	4.12	3.86	5
48.69	48.67	19.43	1.93	1.93	1.91	4
46.69	46.67	18.75	1.92	1.92	1.90	4
44.70	44.69	18.06	1.91	1.90	1.89	4
42.72	42.71	17.38	1.89	1.89	1.87	4
40.75	40.74	16.70	1.88	1.87	1.85	4
38.79	38.78	16.01	1.86	1.86	1.83	4
36.85	36.84	15.33	1.84	1.84	1.81	4
34.91	34.90	14.65	1.82	1.82	1.79	4
33.00	32.99	13.97	1.80	1.80	1.77	4
31.09	31.08	13.28	1.78	1.78	1.75	4
31.09	31.08	13.28	1.47	1.47	1.45	3
29.70	29.69	12.72	1.46	1.46	1.44	3
28.32	28.31	12.16	1.45	1.45	1.43	3
26.94	26.93	11.59	1.44	1.44	1.42	3
25.57	25.56	11.03	1.43	1.43	1.41	3
24.21	24.20	10.47	1.42	1.42	1.40	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3

18.80	18.79	8.21	1.34	1.34	1.33	2
16.88	16.87	7.39	1.33	1.33	1.32	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.46	228.52	103.11	125.42	121.37	4.04	6
59.91	267.12	91.30	175.82	155.35	20.47	6
59.36	305.88	80.24	225.64	189.49	36.15	6
58.81	344.79	70.49	274.30	223.78	50.52	6
58.26	383.83	62.45	321.37	258.19	63.18	6
57.71	422.96	56.34	366.63	292.71	73.92	6
57.16	462.17	52.16	410.01	327.30	82.71	6
56.60	501.43	49.79	451.64	361.93	89.70	6
56.04	540.71	48.95	491.76	396.59	95.17	6
56.04	540.71	48.95	491.76	396.59	95.17	5
54.78	645.31	71.46	573.85	475.45	98.40	5
53.53	749.09	95.08	654.00	553.48	100.53	5
52.29	852.00	119.48	732.53	630.64	101.89	5
51.07	954.03	144.40	809.63	706.92	102.71	5
49.86	1055.16	169.66	885.51	782.30	103.21	5
48.67	1155.38	195.13	960.25	856.77	103.48	5
48.67	1155.38	195.13	960.25	856.77	103.48	4
46.67	1355.81	268.47	1087.34	981.34	106.00	4
44.69	1555.72	347.03	1208.69	1105.39	103.30	4
42.71	1755.07	433.75	1321.32	1228.88	92.44	4
40.74	1953.79	518.86	1434.93	1351.74	83.19	4
38.78	2151.79	582.32	1569.47	1473.88	95.59	4
36.84	2349.00	650.36	1698.64	1595.23	103.41	4
34.90	2545.38	722.60	1822.78	1715.75	107.03	4
32.99	2740.87	798.34	1942.53	1835.38	107.15	4
31.08	2935.45	874.19	2061.26	1954.11	107.15	4
31.08	2935.45	874.20	2061.26	1954.11	107.15	3
29.69	3084.02	936.05	2147.97	2040.82	107.15	3
28.31	3232.20	997.91	2234.29	2127.13	107.15	3
26.93	3379.99	1063.05	2316.95	2213.07	103.87	3
25.56	3527.43	1126.33	2401.10	2298.65	102.45	3
24.20	3674.51	1188.66	2485.85	2383.87	101.98	3
22.84	3821.25	1250.42	2570.82	2468.75	102.08	3
21.48	3967.63	1311.78	2655.86	2553.28	102.58	3
20.13	4113.68	1372.88	2740.80	2637.46	103.33	3
18.79	4259.38	1433.66	2825.72	2721.30	104.41	3
18.79	4259.38	1433.66	2825.72	2721.30	104.41	2
16.87	4465.04	1517.55	2947.49	2840.87	106.62	2
14.97	4670.17	1603.12	3067.06	2959.90	107.15	2
13.07	4874.78	1689.22	3185.57	3078.42	107.15	2
11.18	5078.86	1775.31	3303.55	3196.40	107.15	2
9.29	5282.42	1861.41	3421.01	3313.86	107.15	2
7.42	5485.43	1947.51	3537.92	3430.77	107.15	2
5.55	5687.95	2033.61	3654.34	3547.19	107.15	2
3.70	5890.04	2131.81	3758.24	3663.18	95.05	2
1.84	6091.71	2247.68	3844.03	3778.75	65.28	2
.00	6292.84	2394.06	3898.78	3893.78	5.00	2

Time = 120. Degree of Consolidation = 14.%

Total Settlement = .129

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 120. = .129

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.00	1.95	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.95	.00	.00	.00	.00	.00	1
1.45	57.53	26.79	30.74	30.74	.00	1
.97	114.64	53.58	61.06	61.06	.00	1
.48	171.62	80.36	91.25	91.25	.00	1
.00	228.52	107.15	121.37	121.37	.00	1

Time = 120. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 120. = .055

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .42

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.38	21.42	6.50	6.19	6.18	6
60.02	59.84	21.35	6.49	6.21	6.16	6

59.45	59.29	21.27	6.47	6.23	6.15	6
58.89	58.75	21.20	6.46	6.25	6.13	6
58.33	58.20	21.12	6.44	6.26	6.12	6
57.76	57.65	21.05	6.43	6.28	6.11	6
57.20	57.10	20.97	6.42	6.29	6.09	6
56.64	56.55	20.90	6.40	6.30	6.08	6
56.08	56.00	20.82	6.39	6.31	6.06	6
56.08	56.00	20.82	4.51	4.44	4.24	5
54.82	54.74	20.59	4.44	4.39	4.18	5
53.56	53.50	20.36	4.38	4.34	4.11	5
52.32	52.27	20.12	4.32	4.28	4.05	5
51.10	51.05	19.89	4.25	4.22	3.99	5
49.88	49.85	19.66	4.19	4.16	3.92	5
48.69	48.66	19.43	4.13	4.09	3.86	5
48.69	48.66	19.43	1.93	1.93	1.91	4
46.69	46.66	18.75	1.92	1.92	1.90	4
44.70	44.68	18.06	1.91	1.90	1.89	4
42.72	42.70	17.38	1.89	1.89	1.87	4
40.75	40.73	16.70	1.88	1.87	1.85	4
38.79	38.77	16.01	1.86	1.86	1.83	4
36.85	36.83	15.33	1.84	1.84	1.81	4
34.91	34.90	14.65	1.82	1.82	1.79	4
33.00	32.98	13.97	1.80	1.80	1.77	4
31.09	31.08	13.28	1.78	1.78	1.75	4
31.09	31.08	13.28	1.47	1.47	1.45	3
29.70	29.69	12.72	1.46	1.46	1.44	3
28.32	28.31	12.16	1.45	1.45	1.43	3
26.94	26.93	11.59	1.44	1.44	1.42	3
25.57	25.56	11.03	1.43	1.43	1.41	3
24.21	24.19	10.47	1.42	1.42	1.40	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3
18.80	18.79	8.21	1.34	1.34	1.33	2
16.88	16.87	7.39	1.33	1.33	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.38	228.52	104.26	124.26	121.37	2.89	6
59.84	267.07	97.25	169.82	155.29	14.53	6
59.29	305.71	90.47	215.24	189.32	25.92	6
58.75	344.45	84.10	260.35	223.43	36.91	6
58.20	383.27	78.28	304.99	257.64	47.35	6
57.65	422.17	73.17	349.00	291.92	57.08	6
57.10	461.15	68.83	392.31	326.27	66.04	6
56.55	500.17	65.32	434.85	360.68	74.18	6
56.00	539.24	62.67	476.57	395.13	81.45	6
56.00	539.24	62.67	476.57	395.13	81.45	5
54.74	643.37	84.08	559.29	473.51	85.78	5
53.50	746.72	106.44	640.28	551.11	89.18	5
52.27	849.25	129.66	719.59	627.88	91.70	5

51.05	950.93	153.67	797.26	703.82	93.44	5
49.85	1051.74	178.42	873.32	778.87	94.45	5
48.66	1151.64	203.88	947.76	853.03	94.73	5
48.66	1151.64	203.88	947.76	853.03	94.73	4
46.66	1352.01	277.17	1074.84	977.54	97.30	4
44.68	1551.86	356.70	1195.16	1101.53	93.63	4
42.70	1751.14	445.86	1305.28	1224.95	80.33	4
40.73	1949.77	526.65	1423.12	1347.72	75.40	4
38.77	2147.68	589.21	1558.46	1469.77	88.70	4
36.83	2344.82	655.18	1689.64	1591.05	98.59	4
34.90	2541.15	724.78	1816.38	1711.53	104.85	4
32.98	2736.63	798.34	1938.30	1831.15	107.15	4
31.08	2931.22	874.19	2057.03	1949.87	107.15	4
31.08	2931.22	874.20	2057.03	1949.87	107.15	3
29.69	3079.79	936.05	2143.74	2036.58	107.15	3
28.31	3227.97	997.91	2230.05	2122.90	107.15	3
26.93	3375.76	1064.53	2311.23	2208.84	102.39	3
25.56	3523.18	1129.25	2393.94	2294.40	99.54	3
24.19	3670.25	1191.89	2478.36	2379.61	98.75	3
22.83	3816.96	1253.65	2563.31	2464.46	98.85	3
21.48	3963.33	1315.00	2648.33	2548.97	99.35	3
20.13	4109.36	1376.11	2733.25	2633.14	100.11	3
18.79	4255.04	1436.28	2818.76	2716.97	101.79	3
18.79	4255.04	1436.28	2818.76	2716.97	101.79	2
16.87	4460.69	1518.88	2941.80	2836.51	105.29	2
14.96	4665.82	1603.12	3062.70	2955.55	107.15	2
13.06	4870.43	1689.22	3181.21	3074.06	107.15	2
11.17	5074.51	1775.31	3299.19	3192.04	107.15	2
9.29	5278.07	1861.41	3416.66	3309.50	107.15	2
7.42	5481.08	1947.51	3533.57	3426.42	107.15	2
5.55	5683.60	2033.61	3649.99	3542.84	107.15	2
3.69	5885.67	2144.75	3740.92	3658.81	82.11	2
1.84	6087.27	2264.57	3822.70	3774.31	48.38	2
.00	6288.35	2395.35	3893.00	3889.30	3.70	2

Time = 240. Degree of Consolidation = 22.%

Total Settlement = .201

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 240. = .201

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.94	.00	.00	.00	.00	.00	1
1.45	57.53	26.79	30.74	30.74	.00	1
.97	114.64	53.58	61.06	61.06	.00	1
.48	171.61	80.36	91.25	91.25	.00	1
.00	228.52	107.15	121.37	121.37	.00	1

Time = 240. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 240. = .055

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .34

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.32	21.42	6.50	6.18	6.18	6
60.02	59.78	21.35	6.49	6.20	6.16	6
59.45	59.23	21.27	6.47	6.21	6.15	6
58.89	58.69	21.20	6.46	6.23	6.13	6
58.33	58.14	21.12	6.44	6.24	6.12	6
57.76	57.59	21.05	6.43	6.25	6.11	6
57.20	57.05	20.97	6.42	6.26	6.09	6
56.64	56.50	20.90	6.40	6.27	6.08	6
56.08	55.95	20.82	6.39	6.28	6.06	6
56.08	55.95	20.82	4.51	4.42	4.24	5
54.82	54.70	20.59	4.44	4.36	4.18	5
53.56	53.46	20.36	4.38	4.31	4.11	5
52.32	52.24	20.12	4.32	4.25	4.05	5
51.10	51.03	19.89	4.25	4.19	3.99	5
49.88	49.83	19.66	4.19	4.13	3.92	5
48.69	48.65	19.43	4.13	4.07	3.86	5
48.69	48.65	19.43	1.93	1.93	1.91	4
46.69	46.65	18.75	1.92	1.91	1.90	4
44.70	44.67	18.06	1.91	1.90	1.89	4
42.72	42.69	17.38	1.89	1.89	1.87	4
40.75	40.72	16.70	1.88	1.87	1.85	4
38.79	38.77	16.01	1.86	1.85	1.83	4
36.85	36.83	15.33	1.84	1.84	1.81	4
34.91	34.90	14.65	1.82	1.82	1.79	4
33.00	32.98	13.97	1.80	1.80	1.77	4
31.09	31.08	13.28	1.78	1.78	1.75	4
31.09	31.08	13.28	1.47	1.47	1.45	3
29.70	29.69	12.72	1.46	1.46	1.44	3
28.32	28.30	12.16	1.45	1.45	1.43	3
26.94	26.93	11.59	1.44	1.44	1.42	3
25.57	25.56	11.03	1.43	1.43	1.41	3

24.21	24.19	10.47	1.42	1.42	1.40	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3
18.80	18.79	8.21	1.34	1.34	1.33	2
16.88	16.87	7.39	1.33	1.33	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.32	228.52	104.74	123.78	121.37	2.42	6
59.78	267.04	99.72	167.32	155.27	12.05	6
59.23	305.64	94.82	210.82	189.25	21.57	6
58.69	344.30	90.16	254.14	223.29	30.85	6
58.14	383.03	85.84	297.19	257.40	39.79	6
57.59	421.82	81.94	339.88	291.56	48.31	6
57.05	460.66	78.55	382.10	325.78	56.32	6
56.50	499.54	75.73	423.81	360.04	63.76	6
55.95	538.46	73.56	464.90	394.34	70.55	6
55.95	538.46	73.56	464.90	394.34	70.55	5
54.70	642.19	95.23	546.96	472.33	74.63	5
53.46	745.14	117.65	627.49	549.52	77.97	5
52.24	847.26	140.83	706.43	625.90	80.53	5
51.03	948.55	164.77	783.77	701.43	82.34	5
49.83	1048.95	189.44	859.51	776.09	83.42	5
48.65	1148.47	214.82	933.65	849.85	83.79	5
48.65	1148.47	214.82	933.65	849.85	83.79	4
46.65	1348.76	287.37	1061.40	974.29	87.11	4
44.67	1548.54	366.93	1181.61	1098.21	83.40	4
42.69	1747.75	456.36	1291.39	1221.56	69.83	4
40.72	1946.31	532.61	1413.70	1344.26	69.44	4
38.77	2144.15	594.55	1549.60	1466.24	83.36	4
36.83	2341.24	659.13	1682.11	1587.47	94.64	4
34.90	2537.53	726.93	1810.60	1707.91	102.70	4
32.98	2733.00	798.46	1934.54	1827.51	107.02	4
31.08	2927.59	874.25	2053.34	1946.24	107.10	4
31.08	2927.59	874.25	2053.34	1946.24	107.10	3
29.69	3076.16	936.05	2140.11	2032.95	107.15	3
28.30	3224.34	997.91	2226.42	2119.27	107.15	3
26.93	3372.13	1065.66	2306.46	2205.20	101.26	3
25.56	3519.54	1131.48	2388.06	2290.76	97.30	3
24.19	3666.59	1195.20	2471.38	2375.95	95.44	3
22.83	3813.28	1257.01	2556.27	2460.79	95.49	3
21.48	3959.64	1318.37	2641.27	2545.28	95.99	3
20.13	4105.64	1379.47	2726.17	2629.43	96.75	3
18.79	4251.31	1439.17	2812.14	2713.23	98.91	3
18.79	4251.31	1439.17	2812.14	2713.23	98.91	2
16.87	4456.94	1520.79	2936.15	2832.77	103.38	2
14.96	4662.06	1604.02	3058.04	2951.79	106.25	2
13.06	4866.67	1689.22	3177.46	3070.30	107.15	2
11.17	5070.75	1775.31	3295.44	3188.28	107.15	2
9.29	5274.31	1861.41	3412.90	3305.74	107.15	2

7.42	5477.32	1947.51	3529.81	3422.66	107.15	2
5.55	5679.84	2036.02	3643.82	3539.08	104.74	2
3.69	5881.89	2151.75	3730.14	3655.03	75.10	2
1.84	6083.46	2272.43	3811.03	3770.50	40.53	2
.00	6284.52	2395.96	3888.56	3885.46	3.10	2

Time = 365. Degree of Consolidation = 29.%

Total Settlement = .262

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 365. = .262

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.94	.00	.00	.00	.00	.00	1
1.45	57.53	26.79	30.74	30.74	.00	1
.97	114.64	53.58	61.06	61.06	.00	1
.48	171.61	80.36	91.25	91.25	.00	1
.00	228.52	107.15	121.37	121.37	.00	1

Time = 365. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 365. = .055

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .28

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
60.58	60.25	21.42
60.02	59.70	21.35
59.45	59.16	21.27
58.89	58.62	21.20
58.33	58.07	21.12
57.76	57.52	21.05
57.20	56.98	20.97
56.64	56.43	20.90
56.08	55.88	20.82
56.08	55.88	20.82
54.82	54.64	20.59
53.56	53.41	20.36
52.32	52.20	20.12
51.10	50.99	19.89
49.88	49.81	19.66
48.69	48.63	19.43
48.69	48.63	19.43
46.69	46.64	18.75
44.70	44.66	18.06
42.72	42.68	17.38
40.75	40.72	16.70
38.79	38.76	16.01
36.85	36.82	15.33
34.91	34.89	14.65
33.00	32.98	13.97
31.09	31.07	13.28
31.09	31.07	13.28
29.70	29.68	12.72
28.32	28.30	12.16
26.94	26.92	11.59
25.57	25.55	11.03
24.21	24.19	10.47
22.84	22.83	9.90
21.49	21.47	9.34
20.14	20.13	8.78
18.80	18.78	8.21
18.80	18.78	8.21
16.88	16.87	7.39
14.97	14.96	6.57
13.07	13.06	5.75
11.18	11.17	4.93
9.30	9.29	4.11
7.43	7.42	3.29
5.56	5.55	2.46
3.70	3.69	1.64
1.85	1.84	.82
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
6.50	6.18	6.18	6
6.49	6.19	6.16	6
6.47	6.20	6.15	6
6.46	6.21	6.13	6
6.44	6.22	6.12	6
6.43	6.23	6.11	6
6.42	6.23	6.09	6
6.40	6.24	6.08	6
6.39	6.24	6.06	6
4.51	4.39	4.24	5
4.44	4.33	4.18	5
4.38	4.27	4.11	5
4.32	4.22	4.05	5
4.25	4.16	3.99	5
4.19	4.09	3.92	5
4.13	4.03	3.86	5
1.93	1.92	1.91	4
1.92	1.91	1.90	4
1.91	1.90	1.89	4
1.89	1.88	1.87	4
1.88	1.87	1.85	4
1.86	1.85	1.83	4
1.84	1.83	1.81	4
1.82	1.82	1.79	4
1.80	1.80	1.77	4
1.78	1.77	1.75	4
1.47	1.47	1.45	3
1.46	1.46	1.44	3
1.45	1.45	1.43	3
1.44	1.44	1.42	3
1.43	1.43	1.41	3
1.42	1.42	1.40	3
1.41	1.41	1.39	3
1.40	1.40	1.38	3
1.39	1.39	1.37	3
1.38	1.38	1.36	3
1.34	1.34	1.33	2
1.33	1.33	1.32	2
1.32	1.32	1.30	2
1.31	1.31	1.29	2
1.30	1.30	1.28	2
1.29	1.29	1.27	2
1.28	1.28	1.27	2
1.27	1.27	1.26	2
1.26	1.26	1.25	2
1.25	1.25	1.24	2
1.25	1.24	1.24	2

***** Stresses *****

XI	Total	Effective
60.25	228.52	105.17
59.70	267.02	101.93
59.16	305.58	98.79
58.62	344.17	95.83
58.07	382.81	93.13
57.52	421.48	90.75
56.98	460.18	88.75
56.43	498.91	87.23

***** Pore Pressures *****

Total	Static	Excess	Material
123.35	121.37	1.98	6
165.09	155.25	9.84	6
206.78	189.18	17.60	6
248.34	223.16	25.19	6
289.68	257.17	32.50	6
330.73	291.22	39.50	6
371.43	325.31	46.12	6
411.68	359.42	52.27	6

55.88	537.65	86.21	451.44	393.54	57.90	6
55.88	537.65	86.21	451.44	393.54	57.90	5
54.64	640.92	108.55	532.37	471.06	61.31	5
53.41	743.38	131.48	611.90	547.77	64.13	5
52.20	845.01	154.99	690.02	623.64	66.38	5
50.99	945.78	179.11	766.67	698.66	68.01	5
49.81	1045.67	203.86	841.81	772.81	69.01	5
48.63	1144.66	229.21	915.46	846.05	69.41	5
48.63	1144.66	229.21	915.46	846.05	69.41	4
46.64	1344.86	301.64	1043.22	970.39	72.83	4
44.66	1544.55	381.13	1163.42	1094.21	69.20	4
42.68	1743.66	470.77	1272.89	1217.47	55.43	4
40.72	1942.12	540.68	1401.44	1340.07	61.37	4
38.76	2139.87	601.30	1538.56	1461.96	76.61	4
36.82	2336.88	664.51	1672.38	1583.11	89.26	4
34.89	2533.12	731.03	1802.09	1703.50	98.60	4
32.98	2728.55	801.15	1927.40	1823.06	104.33	4
31.07	2923.12	875.41	2047.70	1941.77	105.93	4
31.07	2923.12	875.41	2047.70	1941.77	105.93	3
29.68	3071.68	936.05	2135.63	2028.48	107.15	3
28.30	3219.86	997.91	2221.95	2114.80	107.15	3
26.92	3367.65	1066.88	2300.77	2200.72	100.04	3
25.55	3515.05	1133.89	2381.16	2286.27	94.89	3
24.19	3662.08	1198.77	2463.31	2371.44	91.87	3
22.83	3808.75	1261.72	2547.04	2456.26	90.78	3
21.47	3955.08	1323.07	2632.01	2540.72	91.29	3
20.13	4101.06	1383.64	2717.42	2624.84	92.57	3
18.78	4246.70	1442.78	2803.92	2708.63	95.29	3
18.78	4246.70	1442.78	2803.92	2708.63	95.29	2
16.87	4452.32	1523.24	2929.07	2828.14	100.93	2
14.96	4657.43	1605.27	3052.16	2947.16	105.00	2
13.06	4862.03	1689.22	3172.82	3065.67	107.15	2
11.17	5066.11	1775.31	3290.80	3183.65	107.15	2
9.29	5269.67	1861.41	3408.26	3301.10	107.15	2
7.42	5472.68	1947.51	3525.17	3418.02	107.15	2
5.55	5675.20	2040.18	3635.02	3534.44	100.59	2
3.69	5877.22	2159.95	3717.27	3650.36	66.91	2
1.84	6078.75	2278.61	3800.15	3765.80	34.35	2
.00	6279.80	2396.43	3883.37	3880.75	2.63	2

Time = 540. Degree of Consolidation = 37.%

Total Settlement = .338

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 540. = .338

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1

.50	.48	.25	.98	.91	1
.00	.00	.00	.98	.91	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.94	.00	.00	.00	.00	.00	1
1.45	57.53	26.79	30.74	30.74	.00	1
.97	114.64	53.58	61.06	61.06	.00	1
.48	171.61	80.36	91.25	91.25	.00	1
.00	228.52	107.15	121.37	121.37	.00	1

Time = 540. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 540. = .055

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .21

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.18	21.42	6.50	6.18	6.18	6
60.02	59.63	21.35	6.49	6.19	6.16	6
59.45	59.09	21.27	6.47	6.19	6.15	6
58.89	58.55	21.20	6.46	6.20	6.13	6
58.33	58.00	21.12	6.44	6.20	6.12	6
57.76	57.46	21.05	6.43	6.20	6.11	6
57.20	56.91	20.97	6.42	6.20	6.09	6
56.64	56.37	20.90	6.40	6.20	6.08	6
56.08	55.83	20.82	6.39	6.20	6.06	6
56.08	55.83	20.82	4.51	4.36	4.24	5
54.82	54.59	20.59	4.44	4.30	4.18	5
53.56	53.37	20.36	4.38	4.24	4.11	5
52.32	52.16	20.12	4.32	4.18	4.05	5
51.10	50.97	19.89	4.25	4.12	3.99	5
49.88	49.79	19.66	4.19	4.06	3.92	5
48.69	48.62	19.43	4.13	4.00	3.86	5
48.69	48.62	19.43	1.93	1.92	1.91	4
46.69	46.63	18.75	1.92	1.91	1.90	4
44.70	44.65	18.06	1.91	1.90	1.89	4
42.72	42.67	17.38	1.89	1.88	1.87	4
40.75	40.71	16.70	1.88	1.87	1.85	4
38.79	38.76	16.01	1.86	1.85	1.83	4
36.85	36.82	15.33	1.84	1.83	1.81	4
34.91	34.89	14.65	1.82	1.81	1.79	4
33.00	32.97	13.97	1.80	1.79	1.77	4
31.09	31.07	13.28	1.78	1.77	1.75	4

31.09	31.07	13.28	1.47	1.47	1.45	3
29.70	29.68	12.72	1.46	1.46	1.44	3
28.32	28.30	12.16	1.45	1.45	1.43	3
26.94	26.92	11.59	1.44	1.44	1.42	3
25.57	25.55	11.03	1.43	1.43	1.41	3
24.21	24.19	10.47	1.42	1.42	1.40	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.33	2
16.88	16.87	7.39	1.33	1.33	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.18	228.52	105.56	122.96	121.37	1.59	6
59.63	267.01	103.89	163.12	155.24	7.89	6
59.09	305.52	102.29	203.23	189.13	14.11	6
58.55	344.05	100.85	243.21	223.04	20.16	6
58.00	382.61	99.63	282.98	256.98	26.00	6
57.46	421.18	98.69	322.49	290.92	31.57	6
56.91	459.76	98.06	361.70	324.88	36.82	6
56.37	498.34	97.83	400.51	358.85	41.66	6
55.83	536.93	98.07	438.86	392.82	46.04	6
55.83	536.93	98.07	438.86	392.82	46.04	5
54.59	639.76	121.15	518.61	469.90	48.72	5
53.37	741.75	144.68	597.07	546.14	50.93	5
52.16	842.89	168.69	674.20	621.53	52.67	5
50.97	943.17	193.15	750.02	696.05	53.97	5
49.79	1042.55	218.10	824.45	769.69	54.76	5
48.62	1141.03	243.55	897.48	842.42	55.06	5
48.62	1141.03	243.55	897.48	842.42	55.06	4
46.63	1341.13	316.71	1024.42	966.66	57.76	4
44.65	1540.71	396.46	1144.26	1090.38	53.88	4
42.67	1739.72	486.12	1253.60	1213.53	40.07	4
40.71	1938.07	548.97	1389.10	1336.02	53.08	4
38.76	2135.73	608.40	1527.34	1457.82	69.51	4
36.82	2332.67	670.34	1662.33	1578.90	83.42	4
34.89	2528.85	735.48	1793.37	1699.22	94.15	4
32.97	2724.23	804.07	1920.16	1818.75	101.41	4
31.07	2918.77	876.82	2041.96	1937.43	104.53	4
31.07	2918.77	876.82	2041.96	1937.43	104.53	3
29.68	3067.34	936.05	2131.28	2024.13	107.15	3
28.30	3215.51	997.91	2217.60	2110.45	107.15	3
26.92	3363.30	1067.55	2295.75	2196.38	99.37	3
25.55	3510.70	1135.21	2375.49	2281.92	93.57	3
24.19	3657.72	1200.72	2457.00	2367.08	89.92	3
22.83	3804.38	1264.29	2540.09	2451.88	88.21	3
21.47	3950.69	1326.09	2624.60	2536.33	88.27	3
20.13	4096.65	1386.31	2710.35	2620.44	89.91	3
18.78	4242.28	1445.10	2797.18	2704.21	92.97	3
18.78	4242.28	1445.10	2797.18	2704.21	92.97	2

16.87	4447.88	1524.97	2922.91	2823.71	99.20	2
14.96	4652.99	1606.39	3046.60	2942.72	103.88	2
13.06	4857.59	1689.70	3167.89	3061.22	106.67	2
11.17	5061.67	1775.31	3286.35	3179.20	107.15	2
9.29	5265.22	1861.41	3403.81	3296.66	107.15	2
7.42	5468.24	1947.51	3520.73	3413.57	107.15	2
5.55	5670.75	2040.18	3630.57	3529.99	100.59	2
3.69	5872.77	2159.95	3712.82	3645.91	66.91	2
1.84	6074.31	2278.61	3795.70	3761.35	34.35	2
.00	6275.35	2396.43	3878.92	3876.30	2.63	2

Time = 730. Degree of Consolidation = 45.%

Total Settlement = .409

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 730. = .409

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.94	.00	.00	.00	.00	.00	1
1.45	57.53	26.79	30.74	30.74	.00	1
.97	114.64	53.58	61.06	61.06	.00	1
.48	171.61	80.36	91.25	91.25	.00	1
.00	228.52	107.15	121.37	121.37	.00	1

Time = 730. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 730. = .055

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .14

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.06	21.42	6.50	6.18	6.18	6
60.02	59.52	21.35	6.49	6.18	6.16	6
59.45	58.98	21.27	6.47	6.18	6.15	6
58.89	58.44	21.20	6.46	6.17	6.13	6
58.33	57.90	21.12	6.44	6.17	6.12	6
57.76	57.35	21.05	6.43	6.17	6.11	6
57.20	56.81	20.97	6.42	6.16	6.09	6
56.64	56.27	20.90	6.40	6.16	6.08	6
56.08	55.73	20.82	6.39	6.15	6.06	6
56.08	55.73	20.82	4.51	4.31	4.24	5
54.82	54.51	20.59	4.44	4.25	4.18	5
53.56	53.30	20.36	4.38	4.19	4.11	5
52.32	52.10	20.12	4.32	4.13	4.05	5
51.10	50.92	19.89	4.25	4.07	3.99	5
49.88	49.75	19.66	4.19	4.01	3.92	5
48.69	48.60	19.43	4.13	3.94	3.86	5
48.69	48.60	19.43	1.93	1.92	1.91	4
46.69	46.61	18.75	1.92	1.91	1.90	4
44.70	44.63	18.06	1.91	1.89	1.89	4
42.72	42.66	17.38	1.89	1.88	1.87	4
40.75	40.70	16.70	1.88	1.86	1.85	4
38.79	38.75	16.01	1.86	1.85	1.83	4
36.85	36.81	15.33	1.84	1.83	1.81	4
34.91	34.88	14.65	1.82	1.81	1.79	4
33.00	32.97	13.97	1.80	1.79	1.77	4
31.09	31.07	13.28	1.78	1.77	1.75	4
31.09	31.07	13.28	1.47	1.47	1.45	3
29.70	29.68	12.72	1.46	1.46	1.44	3
28.32	28.30	12.16	1.45	1.45	1.43	3
26.94	26.92	11.59	1.44	1.44	1.42	3
25.57	25.55	11.03	1.43	1.43	1.41	3
24.21	24.19	10.47	1.42	1.42	1.40	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.33	2
16.88	16.87	7.39	1.33	1.33	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.06	228.52	106.14	122.38	121.37	1.01	6
59.52	266.98	106.81	160.17	155.21	4.96	6
58.98	305.44	107.55	197.88	189.05	8.84	6

58.44	343.88	108.42	235.46	222.87	12.59	6
57.90	382.31	109.45	272.86	256.68	16.18	6
57.35	420.72	110.70	310.03	290.47	19.56	6
56.81	459.12	112.21	346.91	324.24	22.67	6
56.27	497.49	114.03	383.46	357.99	25.46	6
55.73	535.83	116.21	419.62	391.71	27.91	6
55.73	535.83	116.21	419.62	391.71	27.91	5
54.51	637.99	140.46	497.53	468.12	29.41	5
53.30	739.27	164.94	574.33	543.66	30.67	5
52.10	839.67	189.69	649.98	618.31	31.67	5
50.92	939.18	214.68	724.50	692.07	32.44	5
49.75	1037.79	239.89	797.90	764.92	32.98	5
48.60	1135.49	265.38	870.11	836.87	33.24	5
48.60	1135.49	265.38	870.11	836.87	33.24	4
46.61	1335.43	339.22	996.22	960.96	35.25	4
44.63	1534.86	420.11	1114.75	1084.53	30.23	4
42.66	1733.70	506.10	1227.60	1207.51	20.09	4
40.70	1931.89	562.30	1369.59	1329.84	39.75	4
38.75	2129.40	620.45	1508.95	1451.49	57.46	4
36.81	2326.20	681.10	1645.10	1572.43	72.67	4
34.88	2522.26	744.32	1777.94	1692.63	85.31	4
32.97	2717.55	810.84	1906.71	1812.06	94.64	4
31.07	2912.02	882.07	2029.95	1930.67	99.28	4
31.07	2912.02	882.07	2029.95	1930.67	99.28	3
29.68	3060.55	939.97	2120.58	2017.35	103.24	3
28.30	3208.71	1001.17	2207.53	2103.65	103.89	3
26.92	3356.47	1070.89	2285.58	2189.55	96.03	3
25.55	3503.85	1138.26	2365.59	2275.07	90.52	3
24.19	3650.86	1203.50	2447.36	2360.22	87.14	3
22.83	3797.51	1266.81	2530.70	2445.01	85.69	3
21.47	3943.80	1328.37	2615.43	2529.44	85.99	3
20.13	4089.75	1388.35	2701.41	2613.54	87.87	3
18.78	4235.37	1446.92	2788.46	2697.30	91.16	3
18.78	4235.37	1446.92	2788.46	2697.30	91.16	2
16.87	4440.96	1526.35	2914.61	2816.79	97.82	2
14.96	4646.06	1607.32	3038.74	2935.79	102.95	2
13.06	4850.66	1690.18	3160.48	3054.29	106.19	2
11.17	5054.73	1775.31	3279.42	3172.27	107.15	2
9.29	5258.29	1861.41	3396.88	3289.72	107.15	2
7.42	5461.30	1947.51	3513.79	3406.64	107.15	2
5.55	5663.82	2040.18	3623.64	3523.06	100.59	2
3.69	5865.84	2159.95	3705.89	3638.98	66.91	2
1.84	6067.37	2278.61	3788.77	3754.42	34.35	2
.00	6268.42	2396.43	3871.99	3869.37	2.63	2

Time = 1080. Degree of Consolidation = 58.%

Total Settlement = .520

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 1080. = .520

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.94	.00	.00	.00	.00	.00	1
1.45	57.53	26.79	30.74	30.74	.00	1
.97	114.64	53.58	61.06	61.06	.00	1
.48	171.61	80.36	91.25	91.25	.00	1
.00	228.52	107.15	121.37	121.37	.00	1

Time = 1080. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 1080. = .055

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .02

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.97	21.42	6.50	6.18	6.18	6
60.02	59.42	21.35	6.49	6.17	6.16	6
59.45	58.88	21.27	6.47	6.16	6.15	6
58.89	58.34	21.20	6.46	6.15	6.13	6
58.33	57.80	21.12	6.44	6.15	6.12	6
57.76	57.26	21.05	6.43	6.14	6.11	6
57.20	56.72	20.97	6.42	6.13	6.09	6
56.64	56.18	20.90	6.40	6.12	6.08	6
56.08	55.65	20.82	6.39	6.10	6.06	6
56.08	55.65	20.82	4.51	4.28	4.24	5
54.82	54.43	20.59	4.44	4.21	4.18	5
53.56	53.23	20.36	4.38	4.15	4.11	5
52.32	52.04	20.12	4.32	4.09	4.05	5
51.10	50.87	19.89	4.25	4.02	3.99	5
49.88	49.71	19.66	4.19	3.96	3.92	5
48.69	48.57	19.43	4.13	3.90	3.86	5
48.69	48.57	19.43	1.93	1.91	1.91	4
46.69	46.58	18.75	1.92	1.90	1.90	4
44.70	44.61	18.06	1.91	1.89	1.89	4
42.72	42.64	17.38	1.89	1.87	1.87	4
40.75	40.68	16.70	1.88	1.86	1.85	4

38.79	38.73	16.01	1.86	1.84	1.83	4
36.85	36.80	15.33	1.84	1.83	1.81	4
34.91	34.87	14.65	1.82	1.81	1.79	4
33.00	32.96	13.97	1.80	1.79	1.77	4
31.09	31.06	13.28	1.78	1.77	1.75	4
31.09	31.06	13.28	1.47	1.47	1.45	3
29.70	29.67	12.72	1.46	1.46	1.44	3
28.32	28.29	12.16	1.45	1.45	1.43	3
26.94	26.92	11.59	1.44	1.44	1.42	3
25.57	25.55	11.03	1.43	1.43	1.41	3
24.21	24.18	10.47	1.42	1.42	1.40	3
22.84	22.82	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.33	2
16.88	16.87	7.39	1.33	1.33	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.97	233.11	106.62	126.49	125.96	.53	6
59.42	271.56	109.22	162.33	159.78	2.55	6
58.88	309.96	111.89	198.08	193.57	4.51	6
58.34	348.33	114.61	233.72	227.32	6.40	6
57.80	386.66	117.46	269.20	261.03	8.18	6
57.26	424.95	120.46	304.49	294.69	9.80	6
56.72	463.19	123.67	339.52	328.31	11.21	6
56.18	501.38	127.13	374.25	361.89	12.36	6
55.65	539.53	130.85	408.68	395.41	13.27	6
55.65	539.53	130.85	408.68	395.41	13.27	5
54.43	641.14	156.03	485.11	471.28	13.83	5
53.23	741.85	181.29	560.56	546.24	14.33	5
52.04	841.66	206.64	635.02	620.29	14.73	5
50.87	940.55	232.11	708.44	693.43	15.00	5
49.71	1038.52	257.69	780.83	765.66	15.17	5
48.57	1135.58	283.37	852.21	836.96	15.25	5
48.57	1135.58	283.37	852.21	836.96	15.25	4
46.58	1335.40	358.68	976.72	960.93	15.79	4
44.61	1534.69	440.60	1094.08	1084.35	9.73	4
42.64	1733.38	518.09	1215.29	1207.19	8.10	4
40.68	1931.43	573.89	1357.54	1329.38	28.16	4
38.73	2128.81	631.67	1497.13	1450.90	46.24	4
36.80	2325.48	691.89	1633.58	1571.71	61.88	4
34.87	2521.41	754.53	1766.89	1691.79	75.10	4
32.96	2716.58	820.51	1896.08	1811.10	84.98	4
31.06	2910.94	891.25	2019.69	1929.59	90.10	4
31.06	2910.94	891.25	2019.69	1929.59	90.10	3
29.67	3059.42	948.57	2110.85	2016.21	94.63	3
28.29	3207.52	1010.68	2196.84	2102.46	94.38	3
26.92	3355.23	1079.72	2275.51	2188.31	87.20	3
25.55	3502.57	1146.46	2356.11	2273.78	82.33	3
24.18	3649.53	1211.09	2438.44	2358.89	79.55	3

22.82	3796.13	1273.83	2522.31	2443.63	78.67	3
21.47	3942.39	1334.84	2607.55	2528.03	79.52	3
20.12	4088.31	1394.31	2694.00	2612.09	81.91	3
18.78	4233.89	1452.38	2781.51	2695.82	85.69	3
18.78	4233.89	1452.38	2781.51	2695.82	85.69	2
16.87	4439.46	1530.51	2908.94	2815.28	93.66	2
14.96	4644.53	1610.15	3034.38	2934.26	100.12	2
13.06	4849.11	1691.62	3157.49	3052.74	104.75	2
11.17	5053.19	1775.31	3277.87	3170.72	107.15	2
9.29	5256.74	1861.41	3395.33	3288.18	107.15	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 1440. Degree of Consolidation = 69.%

Total Settlement = .619

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 1440. = .619

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.00	1.94	1.01
1.50	1.45	.76
1.00	.97	.51
.50	.48	.25
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
1.94	4.59	.00
1.45	62.12	26.79
.97	119.23	53.58
.48	176.21	80.36
.00	233.11	107.15

***** Pore Pressures *****

Total	Static	Excess	Material
4.59	4.59	.00	1
35.33	35.33	.00	1
65.66	65.66	.00	1
95.84	95.84	.00	1
125.96	125.96	.00	1

Time = 1440. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 1440. = .055

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.07

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.88	21.42	6.50	6.18	6.18	6
60.02	59.33	21.35	6.49	6.16	6.16	6
59.45	58.79	21.27	6.47	6.15	6.15	6
58.89	58.25	21.20	6.46	6.13	6.13	6
58.33	57.72	21.12	6.44	6.12	6.12	6
57.76	57.18	21.05	6.43	6.10	6.11	6
57.20	56.64	20.97	6.42	6.09	6.09	6
56.64	56.11	20.90	6.40	6.08	6.08	6
56.08	55.57	20.82	6.39	6.06	6.06	6
56.08	55.57	20.82	4.51	4.24	4.24	5
54.82	54.37	20.59	4.44	4.18	4.18	5
53.56	53.17	20.36	4.38	4.11	4.11	5
52.32	51.99	20.12	4.32	4.05	4.05	5
51.10	50.83	19.89	4.25	3.99	3.99	5
49.88	49.68	19.66	4.19	3.92	3.92	5
48.69	48.55	19.43	4.13	3.86	3.86	5
48.69	48.55	19.43	1.93	1.91	1.91	4
46.69	46.56	18.75	1.92	1.90	1.90	4
44.70	44.59	18.06	1.91	1.89	1.89	4
42.72	42.62	17.38	1.89	1.87	1.87	4
40.75	40.66	16.70	1.88	1.86	1.85	4
38.79	38.72	16.01	1.86	1.84	1.83	4
36.85	36.78	15.33	1.84	1.82	1.81	4
34.91	34.86	14.65	1.82	1.81	1.79	4
33.00	32.95	13.97	1.80	1.79	1.77	4
31.09	31.05	13.28	1.78	1.77	1.75	4
31.09	31.05	13.28	1.47	1.47	1.45	3
29.70	29.67	12.72	1.46	1.46	1.44	3
28.32	28.28	12.16	1.45	1.45	1.43	3
26.94	26.91	11.59	1.44	1.44	1.42	3
25.57	25.54	11.03	1.43	1.43	1.41	3
24.21	24.18	10.47	1.42	1.41	1.40	3
22.84	22.82	9.90	1.41	1.40	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.33	2
16.88	16.87	7.39	1.33	1.33	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.88	238.69	107.15	131.54	131.54	.00	6
59.33	277.10	111.77	165.33	165.33	.00	6
58.79	315.45	116.39	199.06	199.06	.00	6
58.25	353.73	121.01	232.72	232.72	.00	6
57.72	391.95	125.63	266.31	266.31	.00	6
57.18	430.09	130.25	299.84	299.84	.00	6
56.64	468.18	134.87	333.30	333.30	.00	6
56.11	506.19	139.49	366.70	366.70	.00	6
55.57	544.14	144.11	400.03	400.03	.00	6
55.57	544.14	144.11	400.03	400.03	.00	5
54.37	645.27	169.86	475.41	475.41	.00	5
53.17	745.48	195.61	549.86	549.86	.00	5
51.99	844.76	221.36	623.39	623.39	.00	5
50.83	943.11	247.11	696.00	696.00	.00	5
49.68	1040.55	272.86	767.68	767.68	.00	5
48.55	1137.06	298.61	838.44	838.44	.00	5
48.55	1137.06	298.61	838.44	838.44	.00	4
46.56	1336.78	371.83	964.95	962.31	2.64	4
44.59	1536.00	450.33	1085.66	1085.67	.00	4
42.62	1734.61	526.19	1208.42	1208.42	.00	4
40.66	1932.55	583.94	1348.62	1330.50	18.11	4
38.72	2129.80	642.27	1487.54	1451.89	35.64	4
36.78	2326.35	702.16	1624.19	1572.58	51.61	4
34.86	2522.16	764.52	1757.64	1692.53	65.11	4
32.95	2717.22	830.31	1886.91	1811.73	75.18	4
31.05	2911.46	900.99	2010.47	1930.11	80.36	4
31.05	2911.46	900.99	2010.47	1930.11	80.36	3
29.67	3059.87	958.19	2101.68	2016.67	85.02	3
28.28	3207.92	1020.97	2186.94	2102.85	84.09	3
26.91	3355.57	1089.24	2266.33	2188.65	77.68	3
25.54	3502.85	1155.25	2347.60	2274.07	73.53	3
24.18	3649.77	1219.20	2430.57	2359.13	71.44	3
22.82	3796.33	1281.28	2515.04	2443.83	71.21	3
21.47	3942.54	1341.68	2600.87	2528.19	72.68	3
20.12	4088.43	1400.55	2687.87	2612.21	75.66	3
18.78	4233.98	1458.07	2775.91	2695.91	80.01	3
18.78	4233.98	1458.07	2775.91	2695.91	80.01	2
16.87	4439.51	1535.07	2904.44	2815.34	89.11	2
14.96	4644.56	1613.55	3031.01	2934.29	96.72	2
13.06	4849.12	1693.84	3155.28	3052.76	102.53	2
11.17	5053.19	1776.31	3276.88	3170.72	106.16	2
9.29	5256.74	1861.41	3395.33	3288.18	107.15	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 1825. Degree of Consolidation = 79.%

Total Settlement = .708

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 1825. = .707

Settlement caused by Secondary Compression at time 1825. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.94	10.17	.00	10.17	10.17	.00	1
1.45	67.70	26.79	40.91	40.91	.00	1
.97	124.81	53.58	71.23	71.23	.00	1
.48	181.78	80.36	101.42	101.42	.00	1
.00	238.69	107.15	131.54	131.54	.00	1

Time = 1825. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 1825. = .055

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.16

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.85	21.42	6.50	6.18	6.18	6
60.02	59.31	21.35	6.49	6.16	6.16	6
59.45	58.77	21.27	6.47	6.15	6.15	6
58.89	58.23	21.20	6.46	6.13	6.13	6
58.33	57.69	21.12	6.44	6.12	6.12	6
57.76	57.16	21.05	6.43	6.10	6.11	6
57.20	56.62	20.97	6.42	6.09	6.09	6
56.64	56.08	20.90	6.40	6.08	6.08	6
56.08	55.55	20.82	6.39	6.06	6.06	6
56.08	55.55	20.82	4.51	4.24	4.24	5
54.82	54.34	20.59	4.44	4.18	4.18	5
53.56	53.15	20.36	4.38	4.11	4.11	5
52.32	51.97	20.12	4.32	4.05	4.05	5
51.10	50.81	19.89	4.25	3.99	3.99	5
49.88	49.66	19.66	4.19	3.92	3.92	5
48.69	48.52	19.43	4.13	3.86	3.86	5

48.69	48.52	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.90	4
44.70	44.56	18.06	1.91	1.89	1.89	4
42.72	42.59	17.38	1.89	1.87	1.87	4
40.75	40.64	16.70	1.88	1.86	1.85	4
38.79	38.69	16.01	1.86	1.84	1.83	4
36.85	36.76	15.33	1.84	1.82	1.81	4
34.91	34.84	14.65	1.82	1.80	1.79	4
33.00	32.93	13.97	1.80	1.78	1.77	4
31.09	31.04	13.28	1.78	1.76	1.75	4
31.09	31.04	13.28	1.47	1.47	1.45	3
29.70	29.65	12.72	1.46	1.45	1.44	3
28.32	28.27	12.16	1.45	1.44	1.43	3
26.94	26.90	11.59	1.44	1.43	1.42	3
25.57	25.53	11.03	1.43	1.42	1.41	3
24.21	24.17	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.39	1.38	3
20.14	20.12	8.78	1.39	1.38	1.37	3
18.80	18.78	8.21	1.38	1.37	1.36	3
18.80	18.78	8.21	1.34	1.33	1.33	2
16.88	16.86	7.39	1.33	1.32	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.85	240.18	107.15	133.03	133.03	.00	6
59.31	278.59	111.77	166.82	166.82	.00	6
58.77	316.94	116.39	200.55	200.55	.00	6
58.23	355.22	121.01	234.21	234.21	.00	6
57.69	393.44	125.63	267.80	267.80	.00	6
57.16	431.58	130.25	301.33	301.33	.00	6
56.62	469.67	134.87	334.79	334.79	.00	6
56.08	507.68	139.49	368.19	368.19	.00	6
55.55	545.63	144.11	401.52	401.52	.00	6
55.55	545.63	144.11	401.52	401.52	.00	5
54.34	646.76	169.86	476.90	476.90	.00	5
53.15	746.97	195.61	551.35	551.35	.00	5
51.97	846.25	221.36	624.88	624.88	.00	5
50.81	944.60	247.11	697.49	697.49	.00	5
49.66	1042.04	272.86	769.17	769.17	.00	5
48.52	1138.55	298.61	839.93	839.93	.00	5
48.52	1138.55	298.61	839.93	839.93	.00	4
46.54	1338.27	371.83	966.44	963.80	2.64	4
44.56	1537.48	450.33	1087.15	1087.15	.00	4
42.59	1736.10	526.19	1209.91	1209.91	.00	4
40.64	1934.03	586.76	1347.27	1331.98	15.29	4
38.69	2131.22	648.15	1483.08	1453.31	29.76	4
36.76	2327.68	710.82	1616.86	1573.91	42.95	4
34.84	2523.38	775.39	1747.99	1693.75	54.24	4
32.93	2718.29	842.75	1875.54	1812.81	62.73	4
31.04	2912.38	915.03	1997.35	1931.03	66.32	4
31.04	2912.38	915.03	1997.35	1931.03	66.32	3

29.65	3060.70	973.68	2087.02	2017.49	69.53	3
28.27	3208.64	1038.44	2170.20	2103.58	66.62	3
26.90	3356.20	1105.61	2250.59	2189.28	61.31	3
25.53	3503.40	1170.59	2332.81	2274.61	58.19	3
24.17	3650.23	1233.57	2416.66	2359.59	57.07	3
22.81	3796.71	1294.73	2501.98	2444.21	57.76	3
21.46	3942.85	1354.26	2588.59	2528.50	60.09	3
20.12	4088.67	1412.32	2676.35	2612.45	63.90	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	2
16.86	4439.62	1544.02	2895.61	2815.45	80.15	2
14.96	4644.63	1620.43	3024.20	2934.36	89.84	2
13.06	4849.15	1698.58	3150.57	3052.79	97.79	2
11.17	5053.20	1778.84	3274.35	3170.73	103.63	2
9.29	5256.74	1861.64	3395.11	3288.18	106.93	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 2520. Degree of Consolidation = 81.%

Total Settlement = .732

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 2520. = .731

Settlement caused by Secondary Compression at time 2520. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.94	11.66	.00	11.66	11.66	.00	1
1.45	69.19	26.79	42.40	42.40	.00	1
.97	126.30	53.58	72.72	72.72	.00	1
.48	183.27	80.36	102.91	102.91	.00	1
.00	240.18	107.15	133.03	133.03	.00	1

Time = 2520. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 2520. = .055

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.85	21.42	6.50	6.18	6.18	6
60.02	59.31	21.35	6.49	6.16	6.16	6
59.45	58.77	21.27	6.47	6.15	6.15	6
58.89	58.23	21.20	6.46	6.13	6.13	6
58.33	57.69	21.12	6.44	6.12	6.12	6
57.76	57.15	21.05	6.43	6.10	6.11	6
57.20	56.62	20.97	6.42	6.09	6.09	6
56.64	56.08	20.90	6.40	6.08	6.08	6
56.08	55.55	20.82	6.39	6.06	6.06	6
56.08	55.55	20.82	4.51	4.24	4.24	5
54.82	54.34	20.59	4.44	4.18	4.18	5
53.56	53.15	20.36	4.38	4.11	4.11	5
52.32	51.97	20.12	4.32	4.05	4.05	5
51.10	50.80	19.89	4.25	3.99	3.99	5
49.88	49.66	19.66	4.19	3.92	3.92	5
48.69	48.52	19.43	4.13	3.86	3.86	5
48.69	48.52	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.90	4
44.70	44.56	18.06	1.91	1.89	1.89	4
42.72	42.59	17.38	1.89	1.87	1.87	4
40.75	40.64	16.70	1.88	1.86	1.85	4
38.79	38.69	16.01	1.86	1.84	1.83	4
36.85	36.76	15.33	1.84	1.82	1.81	4
34.91	34.84	14.65	1.82	1.80	1.79	4
33.00	32.93	13.97	1.80	1.78	1.77	4
31.09	31.04	13.28	1.78	1.76	1.75	4
31.09	31.04	13.28	1.47	1.46	1.45	3
29.70	29.65	12.72	1.46	1.45	1.44	3
28.32	28.27	12.16	1.45	1.44	1.43	3
26.94	26.90	11.59	1.44	1.43	1.42	3
25.57	25.53	11.03	1.43	1.42	1.41	3
24.21	24.17	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.39	1.38	3
20.14	20.12	8.78	1.39	1.38	1.37	3
18.80	18.78	8.21	1.38	1.37	1.36	3
18.80	18.78	8.21	1.34	1.33	1.33	2
16.88	16.86	7.39	1.33	1.32	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2

1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.85	240.34	107.15	133.19	133.19	.00	6
59.31	278.75	111.77	166.98	166.98	.00	6
58.77	317.10	116.39	200.71	200.71	.00	6
58.23	355.38	121.01	234.37	234.37	.00	6
57.69	393.59	125.63	267.96	267.96	.00	6
57.15	431.74	130.25	301.49	301.49	.00	6
56.62	469.82	134.87	334.95	334.95	.00	6
56.08	507.84	139.49	368.35	368.35	.00	6
55.55	545.79	144.11	401.68	401.68	.00	6
55.55	545.79	144.11	401.68	401.68	.00	5
54.34	646.92	169.86	477.06	477.06	.00	5
53.15	747.13	195.61	551.51	551.51	.00	5
51.97	846.41	221.36	625.04	625.04	.00	5
50.80	944.76	247.11	697.65	697.65	.00	5
49.66	1042.20	272.86	769.33	769.33	.00	5
48.52	1138.71	298.61	840.09	840.09	.00	5
48.52	1138.71	298.61	840.09	840.09	.00	4
46.54	1338.43	371.83	966.60	963.96	2.64	4
44.56	1537.64	450.33	1087.31	1087.31	.00	4
42.59	1736.26	526.19	1210.07	1210.07	.00	4
40.64	1934.18	587.12	1347.06	1332.13	14.93	4
38.69	2131.38	648.91	1482.47	1453.47	29.00	4
36.76	2327.82	712.02	1615.80	1574.05	41.75	4
34.84	2523.50	777.09	1746.41	1693.87	52.54	4
32.93	2718.39	845.05	1873.34	1812.90	60.44	4
31.04	2912.45	917.32	1995.12	1931.10	64.02	4
31.04	2912.45	917.32	1995.12	1931.10	64.02	3
29.65	3060.75	975.87	2084.89	2017.55	67.34	3
28.27	3208.68	1040.67	2168.02	2103.62	64.40	3
26.90	3356.24	1107.49	2248.75	2189.31	59.43	3
25.53	3503.42	1172.13	2331.29	2274.64	56.65	3
24.17	3650.24	1234.78	2415.46	2359.60	55.86	3
22.81	3796.72	1295.63	2501.09	2444.22	56.87	3
21.46	3942.86	1354.85	2588.00	2528.50	59.50	3
20.12	4088.67	1412.61	2676.06	2612.45	63.60	3
18.78	4234.15	1469.06	2765.10	2696.08	69.02	3
18.78	4234.15	1469.06	2765.10	2696.08	69.02	2
16.86	4439.62	1544.02	2895.60	2815.45	80.15	2
14.96	4644.63	1620.43	3024.20	2934.36	89.84	2
13.06	4849.15	1698.59	3150.57	3052.79	97.78	2
11.17	5053.19	1778.84	3274.35	3170.73	103.62	2
9.29	5256.74	1861.64	3395.10	3288.18	106.93	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.44	3867.82	2.63	2

Time = 2880. Degree of Consolidation = 82.%

Total Settlement = .734

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 2880. = .733

Settlement caused by Secondary Compression at time 2880. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.94	11.82	.00	11.82	11.82	.00	1
1.45	69.35	26.79	42.56	42.56	.00	1
.97	126.46	53.58	72.88	72.88	.00	1
.48	183.43	80.36	103.07	103.07	.00	1
.00	240.34	107.15	133.19	133.19	.00	1

Time = 2880. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 2880. = .055

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.85	21.42	6.50	6.18	6.18	6
60.02	59.31	21.35	6.49	6.16	6.16	6
59.45	58.77	21.27	6.47	6.15	6.15	6
58.89	58.23	21.20	6.46	6.13	6.13	6
58.33	57.69	21.12	6.44	6.12	6.12	6
57.76	57.15	21.05	6.43	6.10	6.11	6
57.20	56.62	20.97	6.42	6.09	6.09	6
56.64	56.08	20.90	6.40	6.08	6.08	6
56.08	55.55	20.82	6.39	6.06	6.06	6
56.08	55.55	20.82	4.51	4.24	4.24	5
54.82	54.34	20.59	4.44	4.18	4.18	5

53.56	53.15	20.36	4.38	4.11	4.11	5
52.32	51.97	20.12	4.32	4.05	4.05	5
51.10	50.80	19.89	4.25	3.99	3.99	5
49.88	49.65	19.66	4.19	3.92	3.92	5
48.69	48.52	19.43	4.13	3.86	3.86	5
48.69	48.52	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.90	4
44.70	44.56	18.06	1.91	1.89	1.89	4
42.72	42.59	17.38	1.89	1.87	1.87	4
40.75	40.64	16.70	1.88	1.86	1.85	4
38.79	38.69	16.01	1.86	1.84	1.83	4
36.85	36.76	15.33	1.84	1.82	1.81	4
34.91	34.84	14.65	1.82	1.80	1.79	4
33.00	32.93	13.97	1.80	1.78	1.77	4
31.09	31.04	13.28	1.78	1.76	1.75	4
31.09	31.04	13.28	1.47	1.46	1.45	3
29.70	29.65	12.72	1.46	1.45	1.44	3
28.32	28.27	12.16	1.45	1.44	1.43	3
26.94	26.90	11.59	1.44	1.43	1.42	3
25.57	25.53	11.03	1.43	1.42	1.41	3
24.21	24.17	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.39	1.38	3
20.14	20.12	8.78	1.39	1.38	1.37	3
18.80	18.78	8.21	1.38	1.37	1.36	3
18.80	18.78	8.21	1.34	1.33	1.33	2
16.88	16.86	7.39	1.33	1.32	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.85	240.36	107.15	133.20	133.20	.00	6
59.31	278.77	111.77	167.00	167.00	.00	6
58.77	317.12	116.39	200.73	200.73	.00	6
58.23	355.40	121.01	234.39	234.39	.00	6
57.69	393.61	125.63	267.98	267.98	.00	6
57.15	431.76	130.25	301.51	301.51	.00	6
56.62	469.84	134.87	334.97	334.97	.00	6
56.08	507.86	139.49	368.36	368.36	.00	6
55.55	545.81	144.11	401.69	401.69	.00	6
55.55	545.81	144.11	401.69	401.69	.00	5
54.34	646.94	169.86	477.07	477.07	.00	5
53.15	747.14	195.61	551.53	551.53	.00	5
51.97	846.42	221.36	625.06	625.06	.00	5
50.80	944.78	247.11	697.67	697.67	.00	5
49.65	1042.22	272.86	769.35	769.35	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	4
46.54	1338.45	371.83	966.62	963.97	2.64	4
44.56	1537.66	450.33	1087.33	1087.33	.00	4
42.59	1736.28	526.19	1210.09	1210.09	.00	4
40.64	1934.20	587.16	1347.05	1332.15	14.89	4
38.69	2131.39	648.98	1482.41	1453.48	28.93	4

36.76	2327.84	712.13	1615.71	1574.07	41.64	4
34.84	2523.52	777.25	1746.26	1693.89	52.38	4
32.93	2718.40	845.27	1873.13	1812.92	60.22	4
31.04	2912.45	917.61	1994.84	1931.11	63.73	4
31.04	2912.45	917.61	1994.84	1931.11	63.73	3
29.65	3060.76	976.14	2084.62	2017.56	67.06	3
28.27	3208.69	1040.95	2167.74	2103.63	64.12	3
26.90	3356.24	1107.72	2248.52	2189.32	59.20	3
25.53	3503.42	1172.32	2331.10	2274.64	56.46	3
24.17	3650.24	1234.93	2415.31	2359.60	55.71	3
22.81	3796.72	1295.74	2500.97	2444.22	56.76	3
21.46	3942.86	1354.93	2587.93	2528.50	59.43	3
20.12	4088.67	1412.65	2676.02	2612.45	63.57	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	2
16.86	4439.62	1544.02	2895.60	2815.45	80.15	2
14.96	4644.63	1620.43	3024.20	2934.36	89.84	2
13.06	4849.15	1698.59	3150.57	3052.79	97.78	2
11.17	5053.20	1778.84	3274.35	3170.73	103.62	2
9.29	5256.74	1861.64	3395.10	3288.18	106.93	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 3240. Degree of Consolidation = 82.%

Total Settlement = .735

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 3240. = .733

Settlement caused by Secondary Compression at time 3240. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.94	11.84	.00	11.84	11.84	.00	1
1.45	69.37	26.79	42.58	42.58	.00	1
.97	126.48	53.58	72.90	72.90	.00	1
.48	183.45	80.36	103.09	103.09	.00	1
.00	240.36	107.15	133.20	133.20	.00	1

Time = 3240. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 3240. = .055

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.85	21.42	6.50	6.18	6.18	6
60.02	59.31	21.35	6.49	6.16	6.16	6
59.45	58.77	21.27	6.47	6.15	6.15	6
58.89	58.23	21.20	6.46	6.13	6.13	6
58.33	57.69	21.12	6.44	6.12	6.12	6
57.76	57.15	21.05	6.43	6.10	6.11	6
57.20	56.62	20.97	6.42	6.09	6.09	6
56.64	56.08	20.90	6.40	6.08	6.08	6
56.08	55.55	20.82	6.39	6.06	6.06	6
56.08	55.55	20.82	4.51	4.24	4.24	5
54.82	54.34	20.59	4.44	4.18	4.18	5
53.56	53.15	20.36	4.38	4.11	4.11	5
52.32	51.97	20.12	4.32	4.05	4.05	5
51.10	50.80	19.89	4.25	3.99	3.99	5
49.88	49.65	19.66	4.19	3.92	3.92	5
48.69	48.52	19.43	4.13	3.86	3.86	5
48.69	48.52	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.90	4
44.70	44.56	18.06	1.91	1.89	1.89	4
42.72	42.59	17.38	1.89	1.87	1.87	4
40.75	40.64	16.70	1.88	1.86	1.85	4
38.79	38.69	16.01	1.86	1.84	1.83	4
36.85	36.76	15.33	1.84	1.82	1.81	4
34.91	34.84	14.65	1.82	1.80	1.79	4
33.00	32.93	13.97	1.80	1.78	1.77	4
31.09	31.04	13.28	1.78	1.76	1.75	4
31.09	31.04	13.28	1.47	1.46	1.45	3
29.70	29.65	12.72	1.46	1.45	1.44	3
28.32	28.27	12.16	1.45	1.44	1.43	3
26.94	26.90	11.59	1.44	1.43	1.42	3
25.57	25.53	11.03	1.43	1.42	1.41	3
24.21	24.17	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.39	1.38	3
20.14	20.12	8.78	1.39	1.38	1.37	3
18.80	18.78	8.21	1.38	1.37	1.36	3
18.80	18.78	8.21	1.34	1.33	1.33	2
16.88	16.86	7.39	1.33	1.32	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2

11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.85	240.36	107.15	133.21	133.21	.00	6
59.31	278.77	111.77	167.00	167.00	.00	6
58.77	317.12	116.39	200.73	200.73	.00	6
58.23	355.40	121.01	234.39	234.39	.00	6
57.69	393.61	125.63	267.98	267.98	.00	6
57.15	431.76	130.25	301.51	301.51	.00	6
56.62	469.84	134.87	334.97	334.97	.00	6
56.08	507.86	139.49	368.37	368.37	.00	6
55.55	545.81	144.11	401.70	401.70	.00	6
55.55	545.81	144.11	401.70	401.70	.00	5
54.34	646.94	169.86	477.07	477.07	.00	5
53.15	747.14	195.61	551.53	551.53	.00	5
51.97	846.43	221.36	625.06	625.06	.00	5
50.80	944.78	247.11	697.67	697.67	.00	5
49.65	1042.22	272.86	769.35	769.35	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	4
46.54	1338.45	371.83	966.62	963.97	2.64	4
44.56	1537.66	450.33	1087.33	1087.33	.00	4
42.59	1736.28	526.19	1210.09	1210.09	.00	4
40.64	1934.20	587.16	1347.05	1332.15	14.89	4
38.69	2131.39	648.98	1482.41	1453.48	28.93	4
36.76	2327.84	712.14	1615.70	1574.07	41.63	4
34.84	2523.52	777.26	1746.26	1693.89	52.37	4
32.93	2718.40	845.28	1873.12	1812.92	60.20	4
31.04	2912.45	917.63	1994.83	1931.11	63.72	4
31.04	2912.45	917.63	1994.82	1931.11	63.72	3
29.65	3060.76	976.16	2084.60	2017.56	67.05	3
28.27	3208.69	1040.96	2167.73	2103.63	64.10	3
26.90	3356.24	1107.74	2248.50	2189.32	59.18	3
25.53	3503.42	1172.33	2331.09	2274.64	56.45	3
24.17	3650.24	1234.94	2415.30	2359.60	55.70	3
22.81	3796.72	1295.75	2500.97	2444.22	56.75	3
21.46	3942.86	1354.93	2587.92	2528.50	59.43	3
20.12	4088.67	1412.65	2676.02	2612.45	63.57	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	2
16.86	4439.62	1544.02	2895.60	2815.45	80.15	2
14.96	4644.63	1620.43	3024.20	2934.36	89.84	2
13.06	4849.15	1698.59	3150.57	3052.79	97.78	2
11.17	5053.20	1778.84	3274.35	3170.73	103.62	2
9.29	5256.74	1861.64	3395.10	3288.18	106.93	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 3650. Degree of Consolidation = 82.%

Total Settlement = .735

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 3650. = .733

Settlement caused by Secondary Compression at time 3650. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.94	11.84	.00	11.84	11.84	.00	1
1.45	69.37	26.79	42.58	42.58	.00	1
.97	126.48	53.58	72.90	72.90	.00	1
.48	183.45	80.36	103.09	103.09	.00	1
.00	240.36	107.15	133.21	133.21	.00	1

Time = 3650. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 3650. = .055

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.85	21.42	6.50	6.18	6.18	6
60.02	59.31	21.35	6.49	6.16	6.16	6
59.45	58.77	21.27	6.47	6.15	6.15	6
58.89	58.23	21.20	6.46	6.13	6.13	6
58.33	57.69	21.12	6.44	6.12	6.12	6
57.76	57.15	21.05	6.43	6.10	6.11	6

57.20	56.62	20.97	6.42	6.09	6.09	6
56.64	56.08	20.90	6.40	6.08	6.08	6
56.08	55.55	20.82	6.39	6.06	6.06	6
56.08	55.55	20.82	4.51	4.24	4.24	5
54.82	54.34	20.59	4.44	4.18	4.18	5
53.56	53.15	20.36	4.38	4.11	4.11	5
52.32	51.97	20.12	4.32	4.05	4.05	5
51.10	50.80	19.89	4.25	3.99	3.99	5
49.88	49.65	19.66	4.19	3.92	3.92	5
48.69	48.52	19.43	4.13	3.86	3.86	5
48.69	48.52	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.90	4
44.70	44.56	18.06	1.91	1.89	1.89	4
42.72	42.59	17.38	1.89	1.87	1.87	4
40.75	40.64	16.70	1.88	1.86	1.85	4
38.79	38.69	16.01	1.86	1.84	1.83	4
36.85	36.76	15.33	1.84	1.82	1.81	4
34.91	34.84	14.65	1.82	1.80	1.79	4
33.00	32.93	13.97	1.80	1.78	1.77	4
31.09	31.04	13.28	1.78	1.76	1.75	4
31.09	31.04	13.28	1.47	1.46	1.45	3
29.70	29.65	12.72	1.46	1.45	1.44	3
28.32	28.27	12.16	1.45	1.44	1.43	3
26.94	26.90	11.59	1.44	1.43	1.42	3
25.57	25.53	11.03	1.43	1.42	1.41	3
24.21	24.17	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.39	1.38	3
20.14	20.12	8.78	1.39	1.38	1.37	3
18.80	18.78	8.21	1.38	1.37	1.36	3
18.80	18.78	8.21	1.34	1.33	1.33	2
16.88	16.86	7.39	1.33	1.32	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.85	240.36	107.15	133.21	133.21	.00	6
59.31	278.77	111.77	167.00	167.00	.00	6
58.77	317.12	116.39	200.73	200.73	.00	6
58.23	355.40	121.01	234.39	234.39	.00	6
57.69	393.61	125.63	267.98	267.98	.00	6
57.15	431.76	130.25	301.51	301.51	.00	6
56.62	469.84	134.87	334.97	334.97	.00	6
56.08	507.86	139.49	368.37	368.37	.00	6
55.55	545.81	144.11	401.70	401.70	.00	6
55.55	545.81	144.11	401.70	401.70	.00	5
54.34	646.94	169.86	477.07	477.07	.00	5
53.15	747.14	195.61	551.53	551.53	.00	5
51.97	846.43	221.36	625.06	625.06	.00	5
50.80	944.78	247.11	697.67	697.67	.00	5
49.65	1042.22	272.86	769.35	769.35	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	4

46.54	1338.45	371.83	966.62	963.97	2.64	4
44.56	1537.66	450.33	1087.33	1087.33	.00	4
42.59	1736.28	526.19	1210.09	1210.09	.00	4
40.64	1934.20	587.16	1347.05	1332.15	14.89	4
38.69	2131.39	648.98	1482.41	1453.48	28.93	4
36.76	2327.84	712.14	1615.70	1574.07	41.63	4
34.84	2523.52	777.26	1746.26	1693.89	52.37	4
32.93	2718.40	845.28	1873.12	1812.92	60.20	4
31.04	2912.45	917.63	1994.83	1931.11	63.72	4
31.04	2912.45	917.63	1994.82	1931.11	63.72	3
29.65	3060.76	976.16	2084.60	2017.56	67.05	3
28.27	3208.69	1040.96	2167.73	2103.63	64.10	3
26.90	3356.24	1107.74	2248.50	2189.32	59.18	3
25.53	3503.42	1172.33	2331.09	2274.64	56.45	3
24.17	3650.24	1234.94	2415.30	2359.60	55.70	3
22.81	3796.72	1295.75	2500.97	2444.22	56.75	3
21.46	3942.86	1354.93	2587.92	2528.50	59.43	3
20.12	4088.67	1412.65	2676.02	2612.45	63.57	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	2
16.86	4439.62	1544.02	2895.60	2815.45	80.15	2
14.96	4644.63	1620.43	3024.20	2934.36	89.84	2
13.06	4849.15	1698.59	3150.57	3052.79	97.78	2
11.17	5053.20	1778.84	3274.35	3170.73	103.62	2
9.29	5256.74	1861.64	3395.10	3288.18	106.93	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 4320. Degree of Consolidation = 82.%

Total Settlement = .735

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 4320. = .733

Settlement caused by Secondary Compression at time 4320. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
2.00	1.94	1.01
1.50	1.45	.76
1.00	.97	.51
.50	.48	.25
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.93	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1

***** Stresses *****

XI	Total	Effective
1.94	11.84	.00
1.45	69.37	26.79

***** Pore Pressures *****

Total	Static	Excess	Material
11.84	11.84	.00	1
42.58	42.58	.00	1

.97	126.48	53.58	72.90	72.90	.00	1
.48	183.45	80.36	103.09	103.09	.00	1
.00	240.36	107.15	133.21	133.21	.00	1

Time = 4320. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 4320. = .055

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.85	21.42	6.50	6.18	6.18	6
60.02	59.31	21.35	6.49	6.16	6.16	6
59.45	58.77	21.27	6.47	6.15	6.15	6
58.89	58.23	21.20	6.46	6.13	6.13	6
58.33	57.69	21.12	6.44	6.12	6.12	6
57.76	57.15	21.05	6.43	6.10	6.11	6
57.20	56.62	20.97	6.42	6.09	6.09	6
56.64	56.08	20.90	6.40	6.08	6.08	6
56.08	55.55	20.82	6.39	6.06	6.06	6
56.08	55.55	20.82	4.51	4.24	4.24	5
54.82	54.34	20.59	4.44	4.18	4.18	5
53.56	53.15	20.36	4.38	4.11	4.11	5
52.32	51.97	20.12	4.32	4.05	4.05	5
51.10	50.80	19.89	4.25	3.99	3.99	5
49.88	49.65	19.66	4.19	3.92	3.92	5
48.69	48.52	19.43	4.13	3.86	3.86	5
48.69	48.52	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.90	4
44.70	44.56	18.06	1.91	1.89	1.89	4
42.72	42.59	17.38	1.89	1.87	1.87	4
40.75	40.64	16.70	1.88	1.86	1.85	4
38.79	38.69	16.01	1.86	1.84	1.83	4
36.85	36.76	15.33	1.84	1.82	1.81	4
34.91	34.84	14.65	1.82	1.80	1.79	4
33.00	32.93	13.97	1.80	1.78	1.77	4
31.09	31.04	13.28	1.78	1.76	1.75	4
31.09	31.04	13.28	1.47	1.46	1.45	3
29.70	29.65	12.72	1.46	1.45	1.44	3
28.32	28.27	12.16	1.45	1.44	1.43	3
26.94	26.90	11.59	1.44	1.43	1.42	3
25.57	25.53	11.03	1.43	1.42	1.41	3
24.21	24.17	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.39	1.38	3
20.14	20.12	8.78	1.39	1.38	1.37	3

18.80	18.78	8.21	1.38	1.37	1.36	3
18.80	18.78	8.21	1.34	1.33	1.33	2
16.88	16.86	7.39	1.33	1.32	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.85	240.36	107.15	133.21	133.21	.00	6
59.31	278.77	111.77	167.00	167.00	.00	6
58.77	317.12	116.39	200.73	200.73	.00	6
58.23	355.40	121.01	234.39	234.39	.00	6
57.69	393.61	125.63	267.98	267.98	.00	6
57.15	431.76	130.25	301.51	301.51	.00	6
56.62	469.84	134.87	334.97	334.97	.00	6
56.08	507.86	139.49	368.37	368.37	.00	6
55.55	545.81	144.11	401.70	401.70	.00	6
55.55	545.81	144.11	401.70	401.70	.00	5
54.34	646.94	169.86	477.07	477.07	.00	5
53.15	747.14	195.61	551.53	551.53	.00	5
51.97	846.43	221.36	625.06	625.06	.00	5
50.80	944.78	247.11	697.67	697.67	.00	5
49.65	1042.22	272.86	769.35	769.35	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	4
46.54	1338.45	371.83	966.62	963.97	2.64	4
44.56	1537.66	450.33	1087.33	1087.33	.00	4
42.59	1736.28	526.19	1210.09	1210.09	.00	4
40.64	1934.20	587.16	1347.05	1332.15	14.89	4
38.69	2131.39	648.98	1482.41	1453.48	28.93	4
36.76	2327.84	712.14	1615.70	1574.07	41.63	4
34.84	2523.52	777.26	1746.26	1693.89	52.37	4
32.93	2718.40	845.28	1873.12	1812.92	60.20	4
31.04	2912.45	917.63	1994.83	1931.11	63.72	4
31.04	2912.45	917.63	1994.82	1931.11	63.72	3
29.65	3060.76	976.16	2084.60	2017.56	67.05	3
28.27	3208.69	1040.96	2167.73	2103.63	64.10	3
26.90	3356.24	1107.74	2248.50	2189.32	59.18	3
25.53	3503.42	1172.33	2331.09	2274.64	56.45	3
24.17	3650.24	1234.94	2415.30	2359.60	55.70	3
22.81	3796.72	1295.75	2500.97	2444.22	56.75	3
21.46	3942.86	1354.93	2587.92	2528.50	59.43	3
20.12	4088.67	1412.65	2676.02	2612.45	63.57	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	2
16.86	4439.62	1544.02	2895.60	2815.45	80.15	2
14.96	4644.63	1620.43	3024.20	2934.36	89.84	2
13.06	4849.15	1698.59	3150.57	3052.79	97.78	2
11.17	5053.20	1778.84	3274.35	3170.73	103.62	2
9.29	5256.74	1861.64	3395.10	3288.18	106.93	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2

.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 5040. Degree of Consolidation = 82.%

Total Settlement = .735

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 5040. = .733

Settlement caused by Secondary Compression at time 5040. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.94	11.84	.00	11.84	11.84	.00	1
1.45	69.37	26.79	42.58	42.58	.00	1
.97	126.48	53.58	72.90	72.90	.00	1
.48	183.45	80.36	103.09	103.09	.00	1
.00	240.36	107.15	133.21	133.21	.00	1

Time = 5040. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 5040. = .055

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.85	21.42	6.50	6.18	6.18	6

60.02	59.31	21.35	6.49	6.16	6.16	6
59.45	58.77	21.27	6.47	6.15	6.15	6
58.89	58.23	21.20	6.46	6.13	6.13	6
58.33	57.69	21.12	6.44	6.12	6.12	6
57.76	57.15	21.05	6.43	6.10	6.11	6
57.20	56.62	20.97	6.42	6.09	6.09	6
56.64	56.08	20.90	6.40	6.08	6.08	6
56.08	55.55	20.82	6.39	6.06	6.06	6
56.08	55.55	20.82	4.51	4.24	4.24	5
54.82	54.34	20.59	4.44	4.18	4.18	5
53.56	53.15	20.36	4.38	4.11	4.11	5
52.32	51.97	20.12	4.32	4.05	4.05	5
51.10	50.80	19.89	4.25	3.99	3.99	5
49.88	49.65	19.66	4.19	3.92	3.92	5
48.69	48.52	19.43	4.13	3.86	3.86	5
48.69	48.52	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.90	4
44.70	44.56	18.06	1.91	1.89	1.89	4
42.72	42.59	17.38	1.89	1.87	1.87	4
40.75	40.64	16.70	1.88	1.86	1.85	4
38.79	38.69	16.01	1.86	1.84	1.83	4
36.85	36.76	15.33	1.84	1.82	1.81	4
34.91	34.84	14.65	1.82	1.80	1.79	4
33.00	32.93	13.97	1.80	1.78	1.77	4
31.09	31.04	13.28	1.78	1.76	1.75	4
31.09	31.04	13.28	1.47	1.46	1.45	3
29.70	29.65	12.72	1.46	1.45	1.44	3
28.32	28.27	12.16	1.45	1.44	1.43	3
26.94	26.90	11.59	1.44	1.43	1.42	3
25.57	25.53	11.03	1.43	1.42	1.41	3
24.21	24.17	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.39	1.38	3
20.14	20.12	8.78	1.39	1.38	1.37	3
18.80	18.78	8.21	1.38	1.37	1.36	3
18.80	18.78	8.21	1.34	1.33	1.33	2
16.88	16.86	7.39	1.33	1.32	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.85	240.36	107.15	133.21	133.21	.00	6
59.31	278.77	111.77	167.00	167.00	.00	6
58.77	317.12	116.39	200.73	200.73	.00	6
58.23	355.40	121.01	234.39	234.39	.00	6
57.69	393.61	125.63	267.98	267.98	.00	6
57.15	431.76	130.25	301.51	301.51	.00	6
56.62	469.84	134.87	334.97	334.97	.00	6
56.08	507.86	139.49	368.37	368.37	.00	6
55.55	545.81	144.11	401.70	401.70	.00	6
55.55	545.81	144.11	401.70	401.70	.00	5
54.34	646.94	169.86	477.07	477.07	.00	5
53.15	747.14	195.61	551.53	551.53	.00	5

51.97	846.43	221.36	625.06	625.06	.00	5
50.80	944.78	247.11	697.67	697.67	.00	5
49.65	1042.22	272.86	769.35	769.35	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	4
46.54	1338.45	371.83	966.62	963.97	2.64	4
44.56	1537.66	450.33	1087.33	1087.33	.00	4
42.59	1736.28	526.19	1210.09	1210.09	.00	4
40.64	1934.20	587.16	1347.05	1332.15	14.89	4
38.69	2131.39	648.98	1482.41	1453.48	28.93	4
36.76	2327.84	712.14	1615.70	1574.07	41.63	4
34.84	2523.52	777.26	1746.26	1693.89	52.37	4
32.93	2718.40	845.28	1873.12	1812.92	60.20	4
31.04	2912.45	917.63	1994.83	1931.11	63.72	4
31.04	2912.45	917.63	1994.82	1931.11	63.72	3
29.65	3060.76	976.16	2084.60	2017.56	67.05	3
28.27	3208.69	1040.96	2167.73	2103.63	64.10	3
26.90	3356.24	1107.74	2248.50	2189.32	59.18	3
25.53	3503.42	1172.33	2331.09	2274.64	56.45	3
24.17	3650.24	1234.94	2415.30	2359.60	55.70	3
22.81	3796.72	1295.75	2500.97	2444.22	56.75	3
21.46	3942.86	1354.93	2587.92	2528.50	59.43	3
20.12	4088.67	1412.65	2676.02	2612.45	63.57	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	2
16.86	4439.62	1544.02	2895.60	2815.45	80.15	2
14.96	4644.63	1620.43	3024.20	2934.36	89.84	2
13.06	4849.15	1698.59	3150.57	3052.79	97.78	2
11.17	5053.20	1778.84	3274.35	3170.73	103.62	2
9.29	5256.74	1861.64	3395.10	3288.18	106.93	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 5475. Degree of Consolidation = 82.%

Total Settlement = .735

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 5475. = .733

Settlement caused by Secondary Compression at time 5475. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.94	11.84	.00	11.84	11.84	.00	1
1.45	69.37	26.79	42.58	42.58	.00	1
.97	126.48	53.58	72.90	72.90	.00	1
.48	183.45	80.36	103.09	103.09	.00	1
.00	240.36	107.15	133.21	133.21	.00	1

Time = 5475. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 5475. = .055

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.85	21.42	6.50	6.18	6.18	6
60.02	59.31	21.35	6.49	6.16	6.16	6
59.45	58.77	21.27	6.47	6.15	6.15	6
58.89	58.23	21.20	6.46	6.13	6.13	6
58.33	57.69	21.12	6.44	6.12	6.12	6
57.76	57.15	21.05	6.43	6.10	6.11	6
57.20	56.62	20.97	6.42	6.09	6.09	6
56.64	56.08	20.90	6.40	6.08	6.08	6
56.08	55.55	20.82	6.39	6.06	6.06	6
56.08	55.55	20.82	4.51	4.24	4.24	5
54.82	54.34	20.59	4.44	4.18	4.18	5
53.56	53.15	20.36	4.38	4.11	4.11	5
52.32	51.97	20.12	4.32	4.05	4.05	5
51.10	50.80	19.89	4.25	3.99	3.99	5
49.88	49.65	19.66	4.19	3.92	3.92	5
48.69	48.52	19.43	4.13	3.86	3.86	5
48.69	48.52	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.90	4
44.70	44.56	18.06	1.91	1.89	1.89	4
42.72	42.59	17.38	1.89	1.87	1.87	4
40.75	40.64	16.70	1.88	1.86	1.85	4
38.79	38.69	16.01	1.86	1.84	1.83	4
36.85	36.76	15.33	1.84	1.82	1.81	4
34.91	34.84	14.65	1.82	1.80	1.79	4
33.00	32.93	13.97	1.80	1.78	1.77	4
31.09	31.04	13.28	1.78	1.76	1.75	4
31.09	31.04	13.28	1.47	1.46	1.45	3
29.70	29.65	12.72	1.46	1.45	1.44	3
28.32	28.27	12.16	1.45	1.44	1.43	3
26.94	26.90	11.59	1.44	1.43	1.42	3

25.57	25.53	11.03	1.43	1.42	1.41	3
24.21	24.17	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.39	1.38	3
20.14	20.12	8.78	1.39	1.38	1.37	3
18.80	18.78	8.21	1.38	1.37	1.36	3
18.80	18.78	8.21	1.34	1.33	1.33	2
16.88	16.86	7.39	1.33	1.32	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.85	240.36	107.15	133.21	133.21	.00	6
59.31	278.77	111.77	167.00	167.00	.00	6
58.77	317.12	116.39	200.73	200.73	.00	6
58.23	355.40	121.01	234.39	234.39	.00	6
57.69	393.61	125.63	267.98	267.98	.00	6
57.15	431.76	130.25	301.51	301.51	.00	6
56.62	469.84	134.87	334.97	334.97	.00	6
56.08	507.86	139.49	368.37	368.37	.00	6
55.55	545.81	144.11	401.70	401.70	.00	6
55.55	545.81	144.11	401.70	401.70	.00	5
54.34	646.94	169.86	477.07	477.07	.00	5
53.15	747.14	195.61	551.53	551.53	.00	5
51.97	846.43	221.36	625.06	625.06	.00	5
50.80	944.78	247.11	697.67	697.67	.00	5
49.65	1042.22	272.86	769.35	769.35	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	4
46.54	1338.45	371.83	966.62	963.97	2.64	4
44.56	1537.66	450.33	1087.33	1087.33	.00	4
42.59	1736.28	526.19	1210.09	1210.09	.00	4
40.64	1934.20	587.16	1347.05	1332.15	14.89	4
38.69	2131.39	648.98	1482.41	1453.48	28.93	4
36.76	2327.84	712.14	1615.70	1574.07	41.63	4
34.84	2523.52	777.26	1746.26	1693.89	52.37	4
32.93	2718.40	845.28	1873.12	1812.92	60.20	4
31.04	2912.45	917.63	1994.83	1931.11	63.72	4
31.04	2912.45	917.63	1994.82	1931.11	63.72	3
29.65	3060.76	976.16	2084.60	2017.56	67.05	3
28.27	3208.69	1040.96	2167.73	2103.63	64.10	3
26.90	3356.24	1107.74	2248.50	2189.32	59.18	3
25.53	3503.42	1172.33	2331.09	2274.64	56.45	3
24.17	3650.24	1234.94	2415.30	2359.60	55.70	3
22.81	3796.72	1295.75	2500.97	2444.22	56.75	3
21.46	3942.86	1354.93	2587.92	2528.50	59.43	3
20.12	4088.67	1412.65	2676.02	2612.45	63.57	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	2
16.86	4439.62	1544.02	2895.60	2815.45	80.15	2
14.96	4644.63	1620.43	3024.20	2934.36	89.84	2
13.06	4849.15	1698.59	3150.57	3052.79	97.78	2
11.17	5053.20	1778.84	3274.35	3170.73	103.62	2

9.29	5256.74	1861.64	3395.10	3288.18	106.93	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 6480. Degree of Consolidation = 82.%

Total Settlement = .735

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 6480. = .733

Settlement caused by Secondary Compression at time 6480. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.94	11.84	.00	11.84	11.84	.00	1
1.45	69.37	26.79	42.58	42.58	.00	1
.97	126.48	53.58	72.90	72.90	.00	1
.48	183.45	80.36	103.09	103.09	.00	1
.00	240.36	107.15	133.21	133.21	.00	1

Time = 6480. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 6480. = .055

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
60.58	59.85	21.42
60.02	59.31	21.35
59.45	58.77	21.27
58.89	58.23	21.20
58.33	57.69	21.12
57.76	57.15	21.05
57.20	56.62	20.97
56.64	56.08	20.90
56.08	55.55	20.82
56.08	55.55	20.82
54.82	54.34	20.59
53.56	53.15	20.36
52.32	51.97	20.12
51.10	50.80	19.89
49.88	49.65	19.66
48.69	48.52	19.43
48.69	48.52	19.43
46.69	46.54	18.75
44.70	44.56	18.06
42.72	42.59	17.38
40.75	40.64	16.70
38.79	38.69	16.01
36.85	36.76	15.33
34.91	34.84	14.65
33.00	32.93	13.97
31.09	31.04	13.28
31.09	31.04	13.28
29.70	29.65	12.72
28.32	28.27	12.16
26.94	26.90	11.59
25.57	25.53	11.03
24.21	24.17	10.47
22.84	22.81	9.90
21.49	21.46	9.34
20.14	20.12	8.78
18.80	18.78	8.21
18.80	18.78	8.21
16.88	16.86	7.39
14.97	14.96	6.57
13.07	13.06	5.75
11.18	11.17	4.93
9.30	9.29	4.11
7.43	7.42	3.29
5.56	5.55	2.46
3.70	3.69	1.64
1.85	1.84	.82
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
6.50	6.18	6.18	6
6.49	6.16	6.16	6
6.47	6.15	6.15	6
6.46	6.13	6.13	6
6.44	6.12	6.12	6
6.43	6.10	6.11	6
6.42	6.09	6.09	6
6.40	6.08	6.08	6
6.39	6.06	6.06	6
4.51	4.24	4.24	5
4.44	4.18	4.18	5
4.38	4.11	4.11	5
4.32	4.05	4.05	5
4.25	3.99	3.99	5
4.19	3.92	3.92	5
4.13	3.86	3.86	5
1.93	1.91	1.91	4
1.92	1.90	1.90	4
1.91	1.89	1.89	4
1.89	1.87	1.87	4
1.88	1.86	1.85	4
1.86	1.84	1.83	4
1.84	1.82	1.81	4
1.82	1.80	1.79	4
1.80	1.78	1.77	4
1.78	1.76	1.75	4
1.47	1.46	1.45	3
1.46	1.45	1.44	3
1.45	1.44	1.43	3
1.44	1.43	1.42	3
1.43	1.42	1.41	3
1.42	1.41	1.40	3
1.41	1.40	1.39	3
1.40	1.39	1.38	3
1.39	1.38	1.37	3
1.38	1.37	1.36	3
1.34	1.33	1.33	2
1.33	1.32	1.32	2
1.32	1.32	1.30	2
1.31	1.31	1.29	2
1.30	1.30	1.28	2
1.29	1.29	1.27	2
1.28	1.28	1.27	2
1.27	1.27	1.26	2
1.26	1.26	1.25	2
1.25	1.25	1.24	2
1.25	1.24	1.24	2

***** Stresses *****

XI	Total	Effective
59.85	240.36	107.15
59.31	278.77	111.77
58.77	317.12	116.39
58.23	355.40	121.01
57.69	393.61	125.63
57.15	431.76	130.25
56.62	469.84	134.87

***** Pore Pressures *****

Total	Static	Excess	Material
133.21	133.21	.00	6
167.00	167.00	.00	6
200.73	200.73	.00	6
234.39	234.39	.00	6
267.98	267.98	.00	6
301.51	301.51	.00	6
334.97	334.97	.00	6

56.08	507.86	139.49	368.37	368.37	.00	6
55.55	545.81	144.11	401.70	401.70	.00	6
55.55	545.81	144.11	401.70	401.70	.00	5
54.34	646.94	169.86	477.07	477.07	.00	5
53.15	747.14	195.61	551.53	551.53	.00	5
51.97	846.43	221.36	625.06	625.06	.00	5
50.80	944.78	247.11	697.67	697.67	.00	5
49.65	1042.22	272.86	769.35	769.35	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	4
46.54	1338.45	371.83	966.62	963.97	2.64	4
44.56	1537.66	450.33	1087.33	1087.33	.00	4
42.59	1736.28	526.19	1210.09	1210.09	.00	4
40.64	1934.20	587.16	1347.05	1332.15	14.89	4
38.69	2131.39	648.98	1482.41	1453.48	28.93	4
36.76	2327.84	712.14	1615.70	1574.07	41.63	4
34.84	2523.52	777.26	1746.26	1693.89	52.37	4
32.93	2718.40	845.28	1873.12	1812.92	60.20	4
31.04	2912.45	917.63	1994.83	1931.11	63.72	4
31.04	2912.45	917.63	1994.82	1931.11	63.72	3
29.65	3060.76	976.16	2084.60	2017.56	67.05	3
28.27	3208.69	1040.96	2167.73	2103.63	64.10	3
26.90	3356.24	1107.74	2248.50	2189.32	59.18	3
25.53	3503.42	1172.33	2331.09	2274.64	56.45	3
24.17	3650.24	1234.94	2415.30	2359.60	55.70	3
22.81	3796.72	1295.75	2500.97	2444.22	56.75	3
21.46	3942.86	1354.93	2587.92	2528.50	59.43	3
20.12	4088.67	1412.65	2676.02	2612.45	63.57	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	2
16.86	4439.62	1544.02	2895.60	2815.45	80.15	2
14.96	4644.63	1620.43	3024.20	2934.36	89.84	2
13.06	4849.15	1698.59	3150.57	3052.79	97.78	2
11.17	5053.20	1778.84	3274.35	3170.73	103.62	2
9.29	5256.74	1861.64	3395.10	3288.18	106.93	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 7300. Degree of Consolidation = 82.%

Total Settlement = .735

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 7300. = .733

Settlement caused by Secondary Compression at time 7300. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1

1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
1.94	11.84	.00	11.84	11.84	.00	1
1.45	69.37	26.79	42.58	42.58	.00	1
.97	126.48	53.58	72.90	72.90	.00	1
.48	183.45	80.36	103.09	103.09	.00	1
.00	240.36	107.15	133.21	133.21	.00	1

Time = 7300. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 7300. = .055

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.85	21.42	6.50	6.18	6.18	6
60.02	59.31	21.35	6.49	6.16	6.16	6
59.45	58.77	21.27	6.47	6.15	6.15	6
58.89	58.23	21.20	6.46	6.13	6.13	6
58.33	57.69	21.12	6.44	6.12	6.12	6
57.76	57.15	21.05	6.43	6.10	6.11	6
57.20	56.62	20.97	6.42	6.09	6.09	6
56.64	56.08	20.90	6.40	6.08	6.08	6
56.08	55.55	20.82	6.39	6.06	6.06	6
56.08	55.55	20.82	4.51	4.24	4.24	5
54.82	54.34	20.59	4.44	4.18	4.18	5
53.56	53.15	20.36	4.38	4.11	4.11	5
52.32	51.97	20.12	4.32	4.05	4.05	5
51.10	50.80	19.89	4.25	3.99	3.99	5
49.88	49.65	19.66	4.19	3.92	3.92	5
48.69	48.52	19.43	4.13	3.86	3.86	5
48.69	48.52	19.43	1.93	1.91	1.91	4
46.69	46.54	18.75	1.92	1.90	1.90	4
44.70	44.56	18.06	1.91	1.89	1.89	4
42.72	42.59	17.38	1.89	1.87	1.87	4
40.75	40.64	16.70	1.88	1.86	1.85	4
38.79	38.69	16.01	1.86	1.84	1.83	4
36.85	36.76	15.33	1.84	1.82	1.81	4
34.91	34.84	14.65	1.82	1.80	1.79	4
33.00	32.93	13.97	1.80	1.78	1.77	4

31.09	31.04	13.28	1.78	1.76	1.75	4
31.09	31.04	13.28	1.47	1.46	1.45	3
29.70	29.65	12.72	1.46	1.45	1.44	3
28.32	28.27	12.16	1.45	1.44	1.43	3
26.94	26.90	11.59	1.44	1.43	1.42	3
25.57	25.53	11.03	1.43	1.42	1.41	3
24.21	24.17	10.47	1.42	1.41	1.40	3
22.84	22.81	9.90	1.41	1.40	1.39	3
21.49	21.46	9.34	1.40	1.39	1.38	3
20.14	20.12	8.78	1.39	1.38	1.37	3
18.80	18.78	8.21	1.38	1.37	1.36	3
18.80	18.78	8.21	1.34	1.33	1.33	2
16.88	16.86	7.39	1.33	1.32	1.32	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.27	2
5.56	5.55	2.46	1.27	1.27	1.26	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.24	1.24	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.85	240.36	107.15	133.21	133.21	.00	6
59.31	278.77	111.77	167.00	167.00	.00	6
58.77	317.12	116.39	200.73	200.73	.00	6
58.23	355.40	121.01	234.39	234.39	.00	6
57.69	393.61	125.63	267.98	267.98	.00	6
57.15	431.76	130.25	301.51	301.51	.00	6
56.62	469.84	134.87	334.97	334.97	.00	6
56.08	507.86	139.49	368.37	368.37	.00	6
55.55	545.81	144.11	401.70	401.70	.00	6
55.55	545.81	144.11	401.70	401.70	.00	5
54.34	646.94	169.86	477.07	477.07	.00	5
53.15	747.14	195.61	551.53	551.53	.00	5
51.97	846.43	221.36	625.06	625.06	.00	5
50.80	944.78	247.11	697.67	697.67	.00	5
49.65	1042.22	272.86	769.35	769.35	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	5
48.52	1138.73	298.61	840.11	840.11	.00	4
46.54	1338.45	371.83	966.62	963.97	2.64	4
44.56	1537.66	450.33	1087.33	1087.33	.00	4
42.59	1736.28	526.19	1210.09	1210.09	.00	4
40.64	1934.20	587.16	1347.05	1332.15	14.89	4
38.69	2131.39	648.98	1482.41	1453.48	28.93	4
36.76	2327.84	712.14	1615.70	1574.07	41.63	4
34.84	2523.52	777.26	1746.26	1693.89	52.37	4
32.93	2718.40	845.28	1873.12	1812.92	60.20	4
31.04	2912.45	917.63	1994.83	1931.11	63.72	4
31.04	2912.45	917.63	1994.82	1931.11	63.72	3
29.65	3060.76	976.16	2084.60	2017.56	67.05	3
28.27	3208.69	1040.96	2167.73	2103.63	64.10	3
26.90	3356.24	1107.74	2248.50	2189.32	59.18	3
25.53	3503.42	1172.33	2331.09	2274.64	56.45	3
24.17	3650.24	1234.94	2415.30	2359.60	55.70	3
22.81	3796.72	1295.75	2500.97	2444.22	56.75	3
21.46	3942.86	1354.93	2587.92	2528.50	59.43	3
20.12	4088.67	1412.65	2676.02	2612.45	63.57	3
18.78	4234.16	1469.06	2765.10	2696.08	69.02	3

18.78	4234.16	1469.06	2765.10	2696.08	69.02	2
16.86	4439.62	1544.02	2895.60	2815.45	80.15	2
14.96	4644.63	1620.43	3024.20	2934.36	89.84	2
13.06	4849.15	1698.59	3150.57	3052.79	97.78	2
11.17	5053.20	1778.84	3274.35	3170.73	103.62	2
9.29	5256.74	1861.64	3395.10	3288.18	106.93	2
7.42	5459.76	1947.51	3512.25	3405.09	107.15	2
5.55	5662.27	2040.18	3622.09	3521.51	100.59	2
3.69	5864.29	2159.95	3704.34	3637.43	66.91	2
1.84	6065.83	2278.61	3787.22	3752.87	34.35	2
.00	6266.87	2396.43	3870.45	3867.82	2.63	2

Time = 9125. Degree of Consolidation = 82.%

Total Settlement = .735

Settlement at End of Primary Consolidation = .901

Settlement caused by Primary Consolidation at time 9125. = .733

Settlement caused by Secondary Compression at time 9125. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
2.00	1.94	1.01	.98	.98	.98	1
1.50	1.45	.76	.98	.93	.93	1
1.00	.97	.51	.98	.92	.92	1
.50	.48	.25	.98	.91	.91	1
.00	.00	.00	.98	.91	.91	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
1.94	11.84	.00	11.84	11.84	.00	1
1.45	69.37	26.79	42.58	42.58	.00	1
.97	126.48	53.58	72.90	72.90	.00	1
.48	183.45	80.36	103.09	103.09	.00	1
.00	240.36	107.15	133.21	133.21	.00	1

Time = 9125. Degree of Consolidation = 101.%

Total Settlement = .055

Settlement at End of Primary Consolidation = .055

Settlement caused by Primary Consolidation at time 9125. = .055

Settlement caused by Secondary Compression at time 9125. = .000

Settlement Due to Desiccation = .000

Surface Elevation = -.19

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou Dupont - 3ft Fill Height

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	3.0	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.623E-01	1.106	.30000E-04	z = .05

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	6.01	6
60.02	60.02	21.35	6.49	6.49	6.00	6
59.45	59.45	21.27	6.47	6.47	5.99	6
58.89	58.89	21.20	6.46	6.46	5.97	6

58.33	58.33	21.12	6.44	6.44	5.96	6
57.76	57.76	21.05	6.43	6.43	5.94	6
57.20	57.20	20.97	6.42	6.42	5.93	6
56.64	56.64	20.90	6.40	6.40	5.92	6
56.08	56.08	20.82	6.39	6.39	5.90	6
56.08	56.08	20.82	4.51	4.51	4.11	5
54.82	54.82	20.59	4.44	4.44	4.05	5
53.56	53.56	20.36	4.38	4.38	3.98	5
52.32	52.32	20.12	4.32	4.32	3.92	5
51.10	51.10	19.89	4.25	4.25	3.85	5
49.88	49.88	19.66	4.19	4.19	3.79	5
48.69	48.69	19.43	4.13	4.13	3.73	5
48.69	48.69	19.43	1.93	1.93	1.90	4
46.69	46.69	18.75	1.92	1.92	1.89	4
44.70	44.70	18.06	1.91	1.91	1.88	4
42.72	42.72	17.38	1.89	1.89	1.86	4
40.75	40.75	16.70	1.88	1.88	1.84	4
38.79	38.79	16.01	1.86	1.86	1.82	4
36.85	36.85	15.33	1.84	1.84	1.79	4
34.91	34.91	14.65	1.82	1.82	1.77	4
33.00	33.00	13.97	1.80	1.80	1.75	4
31.09	31.09	13.28	1.78	1.78	1.73	4
31.09	31.09	13.28	1.47	1.47	1.44	3
29.70	29.70	12.72	1.46	1.46	1.43	3
28.32	28.32	12.16	1.45	1.45	1.42	3
26.94	26.94	11.59	1.44	1.44	1.41	3
25.57	25.57	11.03	1.43	1.43	1.40	3
24.21	24.21	10.47	1.42	1.42	1.39	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.49	9.34	1.40	1.40	1.38	3
20.14	20.14	8.78	1.39	1.39	1.37	3
18.80	18.80	8.21	1.38	1.38	1.36	3
18.80	18.80	8.21	1.34	1.34	1.32	2
16.88	16.88	7.39	1.33	1.33	1.31	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.30	4.11	1.29	1.29	1.27	2
7.43	7.43	3.29	1.28	1.28	1.26	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.85	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.25	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	347.93	.00	347.93	187.20	160.73	6
60.02	387.87	4.62	383.25	222.53	160.73	6
59.45	427.76	9.24	418.52	257.79	160.73	6
58.89	467.57	13.86	453.71	292.98	160.73	6
58.33	507.32	18.48	488.84	328.11	160.73	6
57.76	547.01	23.10	523.90	363.18	160.73	6
57.20	586.62	27.72	558.90	398.18	160.73	6
56.64	626.18	32.34	593.84	433.11	160.73	6
56.08	665.66	36.96	628.70	467.97	160.73	6
56.08	665.66	36.96	628.70	467.97	160.73	5
54.82	770.64	62.71	707.93	547.20	160.73	5
53.56	874.69	88.46	786.22	625.50	160.73	5
52.32	977.81	114.21	863.60	702.87	160.73	5
51.10	1080.01	139.96	940.05	779.32	160.73	5
49.88	1181.29	165.71	1015.58	854.85	160.73	5

48.69	1281.65	191.46	1090.18	929.46	160.73	5
48.69	1281.65	191.46	1090.18	929.46	160.73	4
46.69	1482.09	267.32	1214.77	1054.04	160.73	4
44.70	1682.03	343.18	1338.85	1178.12	160.73	4
42.72	1881.42	419.04	1462.38	1301.66	160.73	4
40.75	2080.37	494.90	1585.47	1424.74	160.73	4
38.79	2278.57	570.76	1707.81	1547.08	160.73	4
36.85	2475.87	646.62	1829.25	1668.52	160.73	4
34.91	2672.26	722.48	1949.79	1789.06	160.73	4
33.00	2867.75	798.34	2069.42	1908.69	160.73	4
31.09	3062.34	874.19	2188.14	2027.42	160.73	4
31.09	3062.34	874.19	2188.14	2027.42	160.73	3
29.70	3210.91	936.05	2274.85	2114.13	160.73	3
28.32	3359.08	997.91	2361.17	2200.44	160.73	3
26.94	3506.89	1059.77	2447.12	2286.39	160.73	3
25.57	3654.34	1121.63	2532.72	2371.99	160.73	3
24.21	3801.46	1183.49	2617.97	2457.24	160.73	3
22.84	3948.22	1245.35	2702.87	2542.14	160.73	3
21.49	4094.63	1307.21	2787.43	2626.70	160.73	3
20.14	4240.70	1369.06	2871.64	2710.91	160.73	3
18.80	4386.42	1430.92	2955.50	2794.77	160.73	3
18.80	4386.42	1430.92	2955.50	2794.77	160.73	2
16.88	4592.09	1517.02	3075.07	2914.34	160.73	2
14.97	4797.23	1603.12	3194.11	3033.38	160.73	2
13.07	5001.84	1689.22	3312.62	3151.89	160.73	2
11.18	5205.92	1775.31	3430.60	3269.87	160.73	2
9.30	5409.47	1861.41	3548.06	3387.33	160.73	2
7.43	5612.49	1947.51	3664.98	3504.25	160.73	2
5.56	5814.99	2033.61	3781.38	3620.66	160.73	2
3.70	6017.11	2119.71	3897.40	3736.68	160.73	2
1.85	6218.88	2205.80	4013.07	3852.34	160.73	2
.00	6420.29	2291.90	4128.39	3967.66	160.73	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	3.00	1.52	.98	.98	.98	1
2.25	2.25	1.14	.98	.98	.92	1
1.50	1.50	.76	.98	.98	.91	1
.75	.75	.38	.98	.98	.91	1
.00	.00	.00	.98	.98	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

3.00	.00	.00	.00	.00	.00	1
2.25	86.98	.00	86.98	46.80	40.18	1
1.50	173.96	.00	173.96	93.60	80.36	1
.75	260.95	.00	260.95	140.40	120.55	1
.00	347.93	.00	347.93	187.20	160.73	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.52	21.42	6.50	6.14	6.01	6
60.02	59.97	21.35	6.49	6.24	6.00	6
59.45	59.42	21.27	6.47	6.32	5.99	6
58.89	58.87	21.20	6.46	6.37	5.97	6
58.33	58.31	21.12	6.44	6.40	5.96	6
57.76	57.75	21.05	6.43	6.41	5.94	6
57.20	57.19	20.97	6.42	6.41	5.93	6
56.64	56.63	20.90	6.40	6.40	5.92	6
56.08	56.07	20.82	6.39	6.39	5.90	6
56.08	56.07	20.82	4.51	4.51	4.11	5
54.82	54.80	20.59	4.44	4.44	4.05	5
53.56	53.55	20.36	4.38	4.38	3.98	5
52.32	52.31	20.12	4.32	4.31	3.92	5
51.10	51.08	19.89	4.25	4.25	3.85	5
49.88	49.88	19.66	4.19	4.19	3.79	5
48.69	48.68	19.43	4.13	4.12	3.73	5
48.69	48.68	19.43	1.93	1.93	1.90	4
46.69	46.68	18.75	1.92	1.92	1.89	4
44.70	44.70	18.06	1.91	1.91	1.88	4
42.72	42.72	17.38	1.89	1.89	1.86	4
40.75	40.74	16.70	1.88	1.88	1.84	4
38.79	38.79	16.01	1.86	1.86	1.82	4
36.85	36.84	15.33	1.84	1.84	1.79	4
34.91	34.91	14.65	1.82	1.82	1.77	4
33.00	32.99	13.97	1.80	1.80	1.75	4
31.09	31.09	13.28	1.78	1.78	1.73	4
31.09	31.09	13.28	1.47	1.47	1.44	3
29.70	29.70	12.72	1.46	1.46	1.43	3
28.32	28.31	12.16	1.45	1.45	1.42	3
26.94	26.94	11.59	1.44	1.44	1.41	3
25.57	25.57	11.03	1.43	1.43	1.40	3
24.21	24.20	10.47	1.42	1.42	1.39	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.14	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3
18.80	18.79	8.21	1.34	1.34	1.32	2

16.88	16.88	7.39	1.33	1.33	1.31	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.30	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.52	342.59	119.10	223.49	181.86	41.63	6
59.97	381.11	85.94	295.17	215.77	79.40	6
59.42	420.07	59.35	360.72	250.10	110.62	6
58.87	459.34	41.60	417.74	284.76	132.99	6
58.31	498.81	32.31	466.50	319.60	146.90	6
57.75	538.35	29.37	508.98	354.53	154.45	6
57.19	577.91	30.42	547.49	389.46	158.03	6
56.63	617.44	33.64	583.80	424.37	159.43	6
56.07	656.91	37.98	618.93	459.22	159.71	6
56.07	656.91	37.98	618.93	459.22	159.71	5
54.80	761.85	63.56	698.28	538.41	159.88	5
53.55	865.87	89.33	776.54	616.68	159.86	5
52.31	968.96	115.12	853.85	694.02	159.82	5
51.08	1071.13	140.88	930.25	770.44	159.80	5
49.88	1172.38	166.61	1005.76	845.94	159.83	5
48.68	1272.70	192.27	1080.43	920.51	159.92	5
48.68	1272.70	192.27	1080.43	920.51	159.92	4
46.68	1473.14	267.32	1205.82	1045.09	160.73	4
44.70	1673.06	343.18	1329.88	1169.16	160.73	4
42.72	1872.47	421.73	1450.74	1292.70	158.04	4
40.74	2071.30	507.72	1563.58	1415.68	147.90	4
38.79	2269.42	573.60	1695.83	1537.94	157.89	4
36.84	2466.71	646.64	1820.07	1659.37	160.70	4
34.91	2663.11	722.48	1940.63	1779.90	160.73	4
32.99	2858.60	798.34	2060.26	1899.54	160.73	4
31.09	3053.18	874.20	2178.99	2018.26	160.73	4
31.09	3053.18	874.20	2178.99	2018.26	160.73	3
29.70	3201.75	936.05	2265.70	2104.97	160.73	3
28.31	3349.93	997.91	2352.01	2191.29	160.73	3
26.94	3497.73	1060.96	2436.77	2277.23	159.54	3
25.57	3645.18	1123.09	2522.09	2362.82	159.26	3
24.20	3792.28	1184.92	2607.36	2448.07	159.29	3
22.84	3939.04	1246.78	2692.26	2532.96	159.29	3
21.48	4085.44	1308.57	2776.87	2617.51	159.36	3
20.14	4231.50	1370.17	2861.34	2701.71	159.62	3
18.79	4377.22	1431.72	2945.50	2785.57	159.93	3
18.79	4377.22	1431.72	2945.50	2785.57	159.93	2
16.88	4582.88	1517.18	3065.70	2905.14	160.56	2
14.97	4788.02	1603.12	3184.90	3024.18	160.73	2
13.07	4992.63	1689.22	3303.42	3142.69	160.73	2
11.18	5196.71	1775.31	3421.40	3260.67	160.73	2
9.30	5400.27	1861.41	3538.85	3378.13	160.73	2
7.42	5603.28	1947.51	3655.77	3495.04	160.73	2
5.56	5805.80	2033.61	3772.19	3611.47	160.73	2
3.70	6007.90	2121.70	3886.21	3727.47	158.74	2
1.84	6209.65	2224.81	3984.83	3843.12	141.72	2
.00	6410.77	2440.01	3970.76	3958.14	12.62	2

Time = 30. Degree of Consolidation = 5.%

Total Settlement = .067

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 30. = .067

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.18	1.14	.98	.93	.92	1
1.50	1.45	.76	.98	.92	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.91	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.18	86.24	32.43	53.81	46.05	7.75	1
1.45	171.85	64.99	106.87	91.49	15.38	1
.72	257.27	93.46	163.81	136.72	27.08	1
.00	342.59	119.10	223.49	181.86	41.63	1

Time = 30. Degree of Consolidation = 95.%

Total Settlement = .086

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 30. = .086

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 1.45

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.48	21.42	6.50	6.12	6.01	6
60.02	59.94	21.35	6.49	6.19	6.00	6
59.45	59.39	21.27	6.47	6.26	5.99	6
58.89	58.84	21.20	6.46	6.31	5.97	6
58.33	58.29	21.12	6.44	6.34	5.96	6

57.76	57.73	21.05	6.43	6.37	5.94	6
57.20	57.18	20.97	6.42	6.38	5.93	6
56.64	56.62	20.90	6.40	6.38	5.92	6
56.08	56.06	20.82	6.39	6.37	5.90	6
56.08	56.06	20.82	4.51	4.50	4.11	5
54.82	54.80	20.59	4.44	4.44	4.05	5
53.56	53.54	20.36	4.38	4.38	3.98	5
52.32	52.30	20.12	4.32	4.31	3.92	5
51.10	51.08	19.89	4.25	4.25	3.85	5
49.88	49.87	19.66	4.19	4.18	3.79	5
48.69	48.67	19.43	4.13	4.12	3.73	5
48.69	48.67	19.43	1.93	1.93	1.90	4
46.69	46.68	18.75	1.92	1.92	1.89	4
44.70	44.69	18.06	1.91	1.91	1.88	4
42.72	42.71	17.38	1.89	1.89	1.86	4
40.75	40.74	16.70	1.88	1.88	1.84	4
38.79	38.78	16.01	1.86	1.86	1.82	4
36.85	36.84	15.33	1.84	1.84	1.79	4
34.91	34.91	14.65	1.82	1.82	1.77	4
33.00	32.99	13.97	1.80	1.80	1.75	4
31.09	31.09	13.28	1.78	1.78	1.73	4
31.09	31.09	13.28	1.47	1.47	1.44	3
29.70	29.70	12.72	1.46	1.46	1.43	3
28.32	28.31	12.16	1.45	1.45	1.42	3
26.94	26.94	11.59	1.44	1.44	1.41	3
25.57	25.56	11.03	1.43	1.43	1.40	3
24.21	24.20	10.47	1.42	1.42	1.39	3
22.84	22.84	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3
18.80	18.79	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.97	6.57	1.32	1.32	1.30	2
13.07	13.07	5.75	1.31	1.31	1.29	2
11.18	11.18	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.48	342.56	124.71	217.85	181.84	36.02	6
59.94	380.94	101.22	279.72	215.59	64.13	6
59.39	419.63	80.37	339.26	249.66	89.60	6
58.84	458.59	63.52	395.07	284.00	111.07	6
58.29	497.76	51.33	446.42	318.55	127.87	6
57.73	537.07	43.76	493.30	353.24	140.06	6
57.18	576.45	40.21	536.24	388.00	148.23	6
56.62	615.87	39.80	576.07	422.80	153.27	6
56.06	655.27	41.58	613.69	457.58	156.11	6
56.06	655.27	41.58	613.69	457.58	156.11	5
54.80	760.11	65.67	694.44	536.67	157.77	5
53.54	864.07	90.70	773.37	614.88	158.49	5
52.30	967.12	116.17	850.95	692.18	158.77	5
51.08	1069.25	141.80	927.45	768.56	158.89	5
49.87	1170.47	167.45	1003.02	844.03	158.99	5
48.67	1270.76	193.02	1077.74	918.57	159.17	5

48.67	1270.76	193.02	1077.74	918.57	159.17	4
46.68	1471.20	267.32	1203.88	1043.15	160.73	4
44.69	1671.13	343.57	1327.56	1167.22	160.34	4
42.71	1870.51	426.39	1444.12	1290.75	153.37	4
40.74	2069.30	512.81	1556.49	1413.67	142.82	4
38.78	2267.37	577.04	1690.32	1535.88	154.44	4
36.84	2464.63	647.56	1817.07	1657.29	159.78	4
34.91	2661.02	722.48	1938.55	1777.82	160.73	4
32.99	2856.51	798.34	2058.18	1897.45	160.73	4
31.09	3051.10	874.20	2176.90	2016.17	160.73	4
31.09	3051.10	874.20	2176.90	2016.17	160.73	3
29.70	3199.67	936.05	2263.61	2102.89	160.73	3
28.31	3347.84	997.91	2349.93	2189.20	160.73	3
26.94	3495.64	1061.73	2433.91	2275.14	158.76	3
25.56	3643.09	1124.37	2518.71	2360.73	157.98	3
24.20	3790.18	1186.36	2603.82	2445.97	157.86	3
22.84	3936.93	1248.22	2688.71	2530.85	157.86	3
21.48	4083.33	1309.82	2773.51	2615.39	158.11	3
20.13	4229.38	1371.24	2858.14	2699.59	158.55	3
18.79	4375.09	1432.58	2942.51	2783.44	159.07	3
18.79	4375.09	1432.58	2942.51	2783.44	159.07	2
16.87	4580.75	1517.62	3063.13	2903.00	160.13	2
14.97	4785.89	1603.12	3182.77	3022.04	160.73	2
13.07	4990.50	1689.22	3301.28	3140.55	160.73	2
11.18	5194.58	1775.31	3419.26	3258.53	160.73	2
9.29	5398.13	1861.41	3536.72	3375.99	160.73	2
7.42	5601.15	1947.51	3653.64	3492.91	160.73	2
5.55	5803.66	2033.61	3770.05	3609.32	160.73	2
3.69	6005.76	2126.17	3879.59	3725.33	154.27	2
1.84	6207.46	2243.16	3964.29	3840.92	123.37	2
.00	6408.52	2442.86	3965.66	3955.89	9.77	2

Time = 60. Degree of Consolidation = 8.%

Total Settlement = .103

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 60. = .103

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.00	2.91	1.52
2.25	2.18	1.14
1.50	1.45	.76
.75	.72	.38
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.92	1
.98	.92	.91	1
.98	.91	.91	1
.98	.91	.90	1

***** Stresses *****

XI	Total	Effective
2.91	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

2.18	86.24	32.63	53.61	46.05	7.55	1
1.45	171.85	66.39	105.46	91.48	13.97	1
.72	257.26	95.69	161.57	136.71	24.86	1
.00	342.56	124.71	217.85	181.84	36.02	1

Time = 60. Degree of Consolidation = 95.%

Total Settlement = .086

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 60. = .086

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 1.41

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.43	21.42	6.50	6.11	6.01	6
60.02	59.89	21.35	6.49	6.16	6.00	6
59.45	59.34	21.27	6.47	6.20	5.99	6
58.89	58.80	21.20	6.46	6.24	5.97	6
58.33	58.25	21.12	6.44	6.28	5.96	6
57.76	57.70	21.05	6.43	6.30	5.94	6
57.20	57.15	20.97	6.42	6.32	5.93	6
56.64	56.59	20.90	6.40	6.34	5.92	6
56.08	56.04	20.82	6.39	6.34	5.90	6
56.08	56.04	20.82	4.51	4.47	4.11	5
54.82	54.78	20.59	4.44	4.42	4.05	5
53.56	53.53	20.36	4.38	4.36	3.98	5
52.32	52.29	20.12	4.32	4.30	3.92	5
51.10	51.07	19.89	4.25	4.24	3.85	5
49.88	49.86	19.66	4.19	4.18	3.79	5
48.69	48.67	19.43	4.13	4.12	3.73	5
48.69	48.67	19.43	1.93	1.93	1.90	4
46.69	46.67	18.75	1.92	1.92	1.89	4
44.70	44.68	18.06	1.91	1.90	1.88	4
42.72	42.70	17.38	1.89	1.89	1.86	4
40.75	40.73	16.70	1.88	1.87	1.84	4
38.79	38.78	16.01	1.86	1.86	1.82	4
36.85	36.83	15.33	1.84	1.84	1.79	4
34.91	34.90	14.65	1.82	1.82	1.77	4
33.00	32.98	13.97	1.80	1.80	1.75	4
31.09	31.08	13.28	1.78	1.78	1.73	4
31.09	31.08	13.28	1.47	1.47	1.44	3
29.70	29.69	12.72	1.46	1.46	1.43	3
28.32	28.31	12.16	1.45	1.45	1.42	3
26.94	26.93	11.59	1.44	1.44	1.41	3
25.57	25.56	11.03	1.43	1.43	1.40	3
24.21	24.19	10.47	1.42	1.42	1.39	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.48	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.79	8.21	1.38	1.38	1.36	3

18.80	18.79	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.43	342.54	129.34	213.20	181.81	31.38	6
59.89	380.79	113.48	267.31	215.45	51.87	6
59.34	419.27	98.63	320.63	249.30	71.33	6
58.80	457.94	85.39	372.55	283.35	89.20	6
58.25	496.79	74.19	422.60	317.58	105.02	6
57.70	535.77	65.28	470.50	351.95	118.55	6
57.15	574.88	58.68	516.19	386.43	129.76	6
56.59	614.05	54.25	559.80	420.98	138.81	6
56.04	653.28	51.67	601.61	455.59	146.02	6
56.04	653.28	51.67	601.61	455.59	146.02	5
54.78	757.81	73.16	684.65	534.37	150.28	5
53.53	861.54	96.09	765.45	612.35	153.10	5
52.29	964.42	120.05	844.37	689.49	154.89	5
51.07	1066.44	144.73	921.71	765.75	155.96	5
49.86	1167.56	169.87	997.69	841.12	156.57	5
48.67	1267.77	195.32	1072.45	915.58	156.87	5
48.67	1267.77	195.32	1072.45	915.58	156.87	4
46.67	1468.20	268.51	1199.69	1040.15	159.54	4
44.68	1668.11	347.12	1320.99	1164.20	156.79	4
42.70	1867.46	433.96	1433.50	1287.69	145.81	4
40.73	2066.18	518.96	1547.22	1410.55	136.67	4
38.78	2264.17	582.38	1681.79	1532.69	149.11	4
36.83	2461.39	650.40	1810.98	1654.04	156.94	4
34.90	2657.76	722.59	1935.17	1774.56	160.61	4
32.98	2853.25	798.34	2054.92	1894.19	160.73	4
31.08	3047.84	874.20	2173.64	2012.91	160.73	4
31.08	3047.84	874.20	2173.64	2012.91	160.73	3
29.69	3196.41	936.05	2260.35	2099.63	160.73	3
28.31	3344.58	997.91	2346.67	2185.94	160.73	3
26.93	3492.38	1063.04	2429.34	2271.88	157.46	3
25.56	3639.81	1126.53	2513.29	2357.46	155.83	3
24.19	3786.90	1188.83	2598.07	2442.68	155.39	3
22.83	3933.63	1250.63	2683.00	2527.55	155.44	3
21.48	4080.01	1312.10	2767.91	2612.08	155.83	3
20.13	4226.06	1373.39	2852.66	2696.26	156.40	3
18.79	4371.75	1434.33	2937.42	2780.10	157.32	3
18.79	4371.75	1434.33	2937.42	2780.10	157.32	2
16.87	4577.41	1518.56	3058.84	2899.66	159.18	2
14.96	4782.54	1603.54	3179.00	3018.69	160.31	2
13.06	4987.15	1689.22	3297.93	3137.20	160.73	2
11.17	5191.23	1775.31	3415.91	3255.18	160.73	2
9.29	5394.78	1861.41	3533.37	3372.64	160.73	2
7.42	5597.80	1947.51	3650.29	3489.56	160.73	2
5.55	5800.31	2033.61	3766.70	3605.97	160.73	2
3.69	6002.40	2137.52	3864.88	3721.96	142.91	2
1.84	6204.01	2267.77	3936.24	3837.48	98.76	2
.00	6405.00	2444.85	3960.15	3952.37	7.78	2

Time = 120. Degree of Consolidation = 12.%

Total Settlement = .159

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 120. = .159

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.18	1.14	.98	.93	.92	1
1.50	1.45	.76	.98	.92	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.91	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.18	86.24	32.79	53.45	46.05	7.39	1
1.45	171.84	67.52	104.32	91.48	12.84	1
.72	257.24	97.51	159.74	136.70	23.04	1
.00	342.54	129.34	213.20	181.81	31.38	1

Time = 120. Degree of Consolidation = 95.%

Total Settlement = .086

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 120. = .086

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.36

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.34	21.42	6.50	6.10	6.01	6
60.02	59.80	21.35	6.49	6.13	6.00	6

59.45	59.26	21.27	6.47	6.16	5.99	6
58.89	58.72	21.20	6.46	6.19	5.97	6
58.33	58.17	21.12	6.44	6.22	5.96	6
57.76	57.63	21.05	6.43	6.24	5.94	6
57.20	57.08	20.97	6.42	6.26	5.93	6
56.64	56.53	20.90	6.40	6.28	5.92	6
56.08	55.98	20.82	6.39	6.29	5.90	6
56.08	55.98	20.82	4.51	4.43	4.11	5
54.82	54.73	20.59	4.44	4.38	4.05	5
53.56	53.49	20.36	4.38	4.33	3.98	5
52.32	52.26	20.12	4.32	4.27	3.92	5
51.10	51.04	19.89	4.25	4.21	3.85	5
49.88	49.84	19.66	4.19	4.15	3.79	5
48.69	48.65	19.43	4.13	4.09	3.73	5
48.69	48.65	19.43	1.93	1.93	1.90	4
46.69	46.66	18.75	1.92	1.92	1.89	4
44.70	44.67	18.06	1.91	1.90	1.88	4
42.72	42.69	17.38	1.89	1.89	1.86	4
40.75	40.73	16.70	1.88	1.87	1.84	4
38.79	38.77	16.01	1.86	1.85	1.82	4
36.85	36.83	15.33	1.84	1.84	1.79	4
34.91	34.89	14.65	1.82	1.82	1.77	4
33.00	32.98	13.97	1.80	1.80	1.75	4
31.09	31.08	13.28	1.78	1.78	1.73	4
31.09	31.08	13.28	1.47	1.47	1.44	3
29.70	29.69	12.72	1.46	1.46	1.43	3
28.32	28.30	12.16	1.45	1.45	1.42	3
26.94	26.93	11.59	1.44	1.44	1.41	3
25.57	25.55	11.03	1.43	1.43	1.40	3
24.21	24.19	10.47	1.42	1.42	1.39	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.13	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.87	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.29	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.34	342.53	132.79	209.73	181.80	27.93	6
59.80	380.69	122.41	258.28	215.34	42.94	6
59.26	419.00	112.36	306.64	249.03	57.61	6
58.72	457.45	102.85	354.60	282.86	71.74	6
58.17	496.03	94.06	401.97	316.82	85.15	6
57.63	534.73	86.14	448.58	350.90	97.69	6
57.08	573.53	79.19	494.34	385.08	109.26	6
56.53	612.43	73.26	539.17	419.36	119.81	6
55.98	651.40	68.37	583.03	453.71	129.32	6
55.98	651.40	68.37	583.03	453.71	129.32	5
54.73	755.35	88.43	666.93	531.91	135.01	5
53.49	858.56	109.71	748.85	609.37	139.48	5
52.26	960.99	132.14	828.85	686.05	142.80	5

51.04	1062.59	155.63	906.97	761.90	145.06	5
49.84	1163.33	180.08	983.26	836.89	146.36	5
48.65	1263.18	205.46	1057.72	910.99	146.73	5
48.65	1263.18	205.46	1057.72	910.99	146.73	4
46.66	1463.54	278.00	1185.54	1035.49	150.05	4
44.67	1663.39	357.37	1306.02	1159.48	146.54	4
42.69	1862.66	446.17	1416.49	1282.90	133.59	4
40.73	2061.29	526.77	1534.52	1405.66	128.86	4
38.77	2259.20	589.43	1669.77	1527.71	142.06	4
36.83	2456.34	655.39	1800.95	1648.99	151.96	4
34.89	2652.67	724.92	1927.75	1769.47	158.28	4
32.98	2848.15	798.34	2049.81	1889.09	160.73	4
31.08	3042.74	874.20	2168.54	2007.81	160.73	4
31.08	3042.74	874.20	2168.54	2007.81	160.73	3
29.69	3191.31	936.05	2255.25	2094.52	160.73	3
28.30	3339.48	997.91	2341.57	2180.84	160.73	3
26.93	3487.27	1064.53	2422.75	2266.78	155.97	3
25.55	3634.70	1129.46	2505.24	2352.34	152.90	3
24.19	3781.76	1192.75	2589.01	2437.54	151.47	3
22.83	3928.47	1254.94	2673.53	2522.39	151.14	3
21.47	4074.83	1316.41	2758.42	2606.90	151.53	3
20.13	4220.85	1377.30	2843.54	2691.06	152.49	3
18.78	4366.52	1437.59	2928.93	2774.88	154.06	3
18.78	4366.52	1437.59	2928.93	2774.88	154.06	2
16.87	4572.16	1520.48	3051.69	2894.41	157.27	2
14.96	4777.29	1604.65	3172.63	3013.44	159.19	2
13.06	4981.89	1689.50	3292.39	3131.95	160.44	2
11.17	5185.97	1775.31	3410.65	3249.93	160.73	2
9.29	5389.53	1861.41	3528.11	3367.39	160.73	2
7.41	5592.54	1947.51	3645.03	3484.30	160.73	2
5.55	5795.06	2036.65	3758.40	3600.72	157.68	2
3.69	5997.10	2156.78	3840.32	3716.66	123.66	2
1.84	6198.61	2293.17	3905.44	3832.08	73.36	2
.00	6399.54	2446.96	3952.58	3946.91	5.67	2

Time = 240. Degree of Consolidation = 18.%

Total Settlement = .246

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 240. = .246

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.18	1.14	.98	.93	.92	1
1.50	1.45	.76	.98	.92	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.91	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.18	86.23	32.91	53.33	46.05	7.27	1
1.45	171.84	68.36	103.48	91.48	12.01	1
.72	257.24	98.85	158.38	136.69	21.69	1
.00	342.53	132.79	209.73	181.80	27.93	1

Time = 240. Degree of Consolidation = 96.%

Total Settlement = .087

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 240. = .087

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.27

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.26	21.42	6.50	6.09	6.01	6
60.02	59.73	21.35	6.49	6.12	6.00	6
59.45	59.19	21.27	6.47	6.14	5.99	6
58.89	58.65	21.20	6.46	6.16	5.97	6
58.33	58.10	21.12	6.44	6.19	5.96	6
57.76	57.56	21.05	6.43	6.21	5.94	6
57.20	57.02	20.97	6.42	6.22	5.93	6
56.64	56.47	20.90	6.40	6.24	5.92	6
56.08	55.92	20.82	6.39	6.25	5.90	6
56.08	55.92	20.82	4.51	4.40	4.11	5
54.82	54.68	20.59	4.44	4.35	4.05	5
53.56	53.44	20.36	4.38	4.29	3.98	5
52.32	52.22	20.12	4.32	4.24	3.92	5
51.10	51.01	19.89	4.25	4.18	3.85	5
49.88	49.82	19.66	4.19	4.12	3.79	5
48.69	48.64	19.43	4.13	4.06	3.73	5
48.69	48.64	19.43	1.93	1.93	1.90	4
46.69	46.65	18.75	1.92	1.91	1.89	4
44.70	44.66	18.06	1.91	1.90	1.88	4
42.72	42.68	17.38	1.89	1.89	1.86	4
40.75	40.72	16.70	1.88	1.87	1.84	4
38.79	38.76	16.01	1.86	1.85	1.82	4
36.85	36.82	15.33	1.84	1.84	1.79	4
34.91	34.89	14.65	1.82	1.82	1.77	4
33.00	32.97	13.97	1.80	1.80	1.75	4
31.09	31.07	13.28	1.78	1.78	1.73	4
31.09	31.07	13.28	1.47	1.47	1.44	3
29.70	29.68	12.72	1.46	1.46	1.43	3
28.32	28.30	12.16	1.45	1.45	1.42	3
26.94	26.92	11.59	1.44	1.44	1.41	3
25.57	25.55	11.03	1.43	1.43	1.40	3

24.21	24.18	10.47	1.42	1.42	1.39	3
22.84	22.83	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.96	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.26	342.52	134.32	208.19	181.79	26.40	6
59.73	380.64	126.31	254.33	215.30	39.03	6
59.19	418.88	118.49	300.39	248.91	51.47	6
58.65	457.23	110.98	346.25	282.64	63.61	6
58.10	495.68	103.90	391.78	316.47	75.31	6
57.56	534.23	97.34	436.89	350.40	86.49	6
57.02	572.87	91.41	481.46	384.42	97.04	6
56.47	611.58	86.19	525.39	418.51	106.88	6
55.92	650.37	81.76	568.61	452.68	115.93	6
55.92	650.37	81.76	568.61	452.68	115.93	5
54.68	753.84	102.04	651.79	530.40	121.40	5
53.44	856.56	123.34	733.21	607.37	125.85	5
52.22	958.50	145.65	812.85	683.56	129.29	5
51.01	1059.62	168.98	890.64	758.93	131.71	5
49.82	1159.88	193.30	966.58	833.44	133.14	5
48.64	1259.26	218.60	1040.66	907.07	133.59	5
48.64	1259.26	218.60	1040.66	907.07	133.59	4
46.65	1459.53	290.36	1169.17	1031.48	137.69	4
44.66	1659.29	369.31	1289.98	1155.39	134.59	4
42.68	1858.49	458.27	1400.22	1278.72	121.50	4
40.72	2057.03	533.47	1523.56	1401.41	122.16	4
38.76	2254.87	595.11	1659.75	1523.38	136.37	4
36.82	2451.95	659.69	1792.26	1644.60	147.66	4
34.89	2648.24	727.47	1920.77	1765.03	155.74	4
32.97	2843.70	798.72	2044.98	1884.64	160.35	4
31.07	3038.29	874.37	2163.92	2003.36	160.56	4
31.07	3038.29	874.37	2163.92	2003.36	160.56	3
29.68	3186.85	936.05	2250.80	2090.07	160.73	3
28.30	3335.03	997.91	2337.12	2176.39	160.73	3
26.92	3482.82	1066.03	2416.79	2262.32	154.47	3
25.55	3630.23	1131.93	2498.30	2347.88	150.43	3
24.18	3777.28	1195.94	2581.33	2433.06	148.27	3
22.83	3923.97	1258.34	2665.63	2517.89	147.74	3
21.47	4070.31	1319.80	2750.51	2602.38	148.13	3
20.12	4216.31	1380.50	2835.81	2686.52	149.29	3
18.78	4361.97	1440.39	2921.58	2770.32	151.26	3
18.78	4361.97	1440.39	2921.58	2770.32	151.26	2
16.86	4567.59	1522.47	3045.13	2889.85	155.28	2
14.96	4772.71	1606.01	3166.70	3008.86	157.84	2
13.06	4977.30	1690.19	3287.11	3127.36	159.75	2
11.17	5181.38	1775.31	3406.07	3245.34	160.73	2
9.28	5384.94	1861.41	3523.52	3362.80	160.73	2

7.41	5587.95	1947.51	3640.44	3479.71	160.73	2
5.55	5790.46	2042.63	3747.83	3596.12	151.71	2
3.69	5992.46	2170.11	3822.35	3712.02	110.32	2
1.84	6193.92	2305.72	3888.20	3827.39	60.82	2
.00	6394.81	2447.93	3946.88	3942.18	4.70	2

Time = 365. Degree of Consolidation = 24.%

Total Settlement = .322

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 365. = .322

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.00	2.91	1.52
2.25	2.18	1.14
1.50	1.45	.76
.75	.72	.38
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.93	.92	1
.98	.92	.91	1
.98	.91	.91	1
.98	.91	.90	1

***** Stresses *****

XI	Total	Effective
2.91	.00	.00
2.18	86.23	32.96
1.45	171.84	68.72
.72	257.23	99.45
.00	342.52	134.32

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
53.28	46.05	7.22	1
103.12	91.48	11.64	1
157.79	136.69	21.10	1
208.19	181.79	26.40	1

Time = 365. Degree of Consolidation = 96.%

Total Settlement = .087

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 365. = .087

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.19

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.17	21.42	6.50	6.09	6.01	6
60.02	59.63	21.35	6.49	6.11	6.00	6
59.45	59.10	21.27	6.47	6.13	5.99	6
58.89	58.56	21.20	6.46	6.14	5.97	6
58.33	58.02	21.12	6.44	6.16	5.96	6
57.76	57.47	21.05	6.43	6.17	5.94	6
57.20	56.93	20.97	6.42	6.19	5.93	6
56.64	56.39	20.90	6.40	6.20	5.92	6
56.08	55.85	20.82	6.39	6.21	5.90	6
56.08	55.85	20.82	4.51	4.36	4.11	5
54.82	54.61	20.59	4.44	4.31	4.05	5
53.56	53.39	20.36	4.38	4.25	3.98	5
52.32	52.17	20.12	4.32	4.20	3.92	5
51.10	50.98	19.89	4.25	4.14	3.85	5
49.88	49.79	19.66	4.19	4.08	3.79	5
48.69	48.62	19.43	4.13	4.01	3.73	5
48.69	48.62	19.43	1.93	1.92	1.90	4
46.69	46.63	18.75	1.92	1.91	1.89	4
44.70	44.65	18.06	1.91	1.90	1.88	4
42.72	42.67	17.38	1.89	1.88	1.86	4
40.75	40.71	16.70	1.88	1.87	1.84	4
38.79	38.75	16.01	1.86	1.85	1.82	4
36.85	36.81	15.33	1.84	1.83	1.79	4
34.91	34.88	14.65	1.82	1.82	1.77	4
33.00	32.97	13.97	1.80	1.80	1.75	4
31.09	31.07	13.28	1.78	1.77	1.73	4
31.09	31.07	13.28	1.47	1.47	1.44	3
29.70	29.68	12.72	1.46	1.46	1.43	3
28.32	28.29	12.16	1.45	1.45	1.42	3
26.94	26.92	11.59	1.44	1.44	1.41	3
25.57	25.55	11.03	1.43	1.43	1.40	3
24.21	24.18	10.47	1.42	1.42	1.39	3
22.84	22.82	9.90	1.41	1.41	1.39	3
21.49	21.47	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.78	8.21	1.38	1.38	1.36	3
18.80	18.78	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.95	6.57	1.32	1.32	1.30	2
13.07	13.06	5.75	1.31	1.31	1.29	2
11.18	11.17	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.17	342.51	135.72	206.79	181.79	25.01	6
59.63	380.60	129.82	250.78	215.26	35.52	6
59.10	418.78	124.07	294.71	248.81	45.90	6
58.56	457.03	118.55	338.48	282.44	56.04	6
58.02	495.36	113.36	382.00	316.15	65.85	6
57.47	533.76	108.59	425.17	349.93	75.24	6
56.93	572.23	104.30	467.93	383.78	84.15	6
56.39	610.75	100.57	510.17	417.68	92.50	6

55.85	649.32	97.50	551.82	451.63	100.19	6
55.85	649.32	97.50	551.82	451.63	100.19	5
54.61	752.21	118.56	633.65	528.77	104.88	5
53.39	854.32	140.42	713.91	605.13	108.77	5
52.17	955.64	163.12	792.52	680.70	111.82	5
50.98	1056.13	186.67	869.46	755.44	114.02	5
49.79	1155.76	211.07	944.69	829.32	115.37	5
48.62	1254.50	236.31	1018.19	902.31	115.88	5
48.62	1254.50	236.31	1018.19	902.31	115.88	4
46.63	1454.66	307.55	1147.11	1026.61	120.50	4
44.65	1654.30	386.13	1268.17	1150.40	117.78	4
42.67	1853.38	474.96	1378.42	1273.61	104.81	4
40.71	2051.82	542.30	1509.51	1396.19	113.32	4
38.75	2249.55	602.50	1647.05	1518.07	128.98	4
36.81	2446.55	665.57	1780.98	1639.21	141.77	4
34.88	2642.78	731.65	1911.13	1759.58	151.55	4
32.97	2838.21	801.33	2036.87	1879.14	157.73	4
31.07	3032.77	875.66	2157.10	1997.85	159.26	4
31.07	3032.77	875.66	2157.10	1997.85	159.26	3
29.68	3181.33	936.05	2245.28	2084.55	160.73	3
28.29	3329.51	997.91	2331.60	2170.87	160.73	3
26.92	3477.30	1067.18	2410.11	2256.80	153.31	3
25.55	3624.70	1134.13	2490.57	2342.34	148.22	3
24.18	3771.73	1199.07	2572.66	2427.52	145.14	3
22.82	3918.40	1262.30	2656.10	2512.33	143.78	3
21.47	4064.72	1323.99	2740.73	2596.79	143.95	3
20.12	4210.70	1384.64	2826.06	2680.91	145.15	3
18.78	4356.33	1444.09	2912.25	2764.68	147.56	3
18.78	4356.33	1444.09	2912.25	2764.68	147.56	2
16.86	4561.94	1525.26	3036.68	2884.19	152.49	2
14.95	4767.04	1608.07	3158.97	3003.19	155.78	2
13.06	4971.62	1691.49	3280.13	3121.68	158.45	2
11.17	5175.69	1775.83	3399.87	3239.65	160.22	2
9.28	5379.24	1861.41	3517.83	3357.10	160.73	2
7.41	5582.26	1947.51	3634.75	3474.03	160.73	2
5.54	5784.76	2050.11	3734.64	3590.42	144.22	2
3.69	5986.72	2181.06	3805.66	3706.28	99.38	2
1.84	6188.13	2314.80	3873.34	3821.60	51.74	2
.00	6389.00	2448.63	3940.37	3936.37	4.00	2

Time = 540. Degree of Consolidation = 31.%

Total Settlement = .415

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 540. = .415

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.18	1.14	.98	.93	.92	1
1.50	1.45	.76	.98	.92	.91	1

.75	.72	.38	.98	.91	1
.00	.00	.00	.98	.91	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.18	86.23	33.01	53.23	46.05	7.18	1
1.45	171.84	69.05	102.79	91.47	11.31	1
.72	257.23	99.99	157.24	136.68	20.56	1
.00	342.51	135.72	206.79	181.79	25.01	1

Time = 540. Degree of Consolidation = 96.%

Total Settlement = .087

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 540. = .087

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.10

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.08	21.42	6.50	6.08	6.01	6
60.02	59.54	21.35	6.49	6.10	6.00	6
59.45	59.01	21.27	6.47	6.11	5.99	6
58.89	58.47	21.20	6.46	6.12	5.97	6
58.33	57.93	21.12	6.44	6.13	5.96	6
57.76	57.39	21.05	6.43	6.14	5.94	6
57.20	56.85	20.97	6.42	6.15	5.93	6
56.64	56.31	20.90	6.40	6.16	5.92	6
56.08	55.77	20.82	6.39	6.16	5.90	6
56.08	55.77	20.82	4.51	4.32	4.11	5
54.82	54.54	20.59	4.44	4.27	4.05	5
53.56	53.33	20.36	4.38	4.21	3.98	5
52.32	52.13	20.12	4.32	4.15	3.92	5
51.10	50.94	19.89	4.25	4.09	3.85	5
49.88	49.77	19.66	4.19	4.03	3.79	5
48.69	48.61	19.43	4.13	3.97	3.73	5
48.69	48.61	19.43	1.93	1.92	1.90	4
46.69	46.62	18.75	1.92	1.91	1.89	4
44.70	44.63	18.06	1.91	1.90	1.88	4
42.72	42.66	17.38	1.89	1.88	1.86	4
40.75	40.70	16.70	1.88	1.87	1.84	4
38.79	38.75	16.01	1.86	1.85	1.82	4
36.85	36.81	15.33	1.84	1.83	1.79	4
34.91	34.88	14.65	1.82	1.81	1.77	4
33.00	32.96	13.97	1.80	1.79	1.75	4
31.09	31.06	13.28	1.78	1.77	1.73	4

31.09	31.06	13.28	1.47	1.47	1.44	3
29.70	29.67	12.72	1.46	1.46	1.43	3
28.32	28.29	12.16	1.45	1.45	1.42	3
26.94	26.91	11.59	1.44	1.44	1.41	3
25.57	25.54	11.03	1.43	1.43	1.40	3
24.21	24.18	10.47	1.42	1.42	1.39	3
22.84	22.82	9.90	1.41	1.41	1.39	3
21.49	21.46	9.34	1.40	1.40	1.38	3
20.14	20.12	8.78	1.39	1.39	1.37	3
18.80	18.77	8.21	1.38	1.38	1.36	3
18.80	18.77	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.95	6.57	1.32	1.32	1.30	2
13.07	13.05	5.75	1.31	1.31	1.29	2
11.18	11.16	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.08	342.50	138.16	204.34	181.77	22.56	6
59.54	380.55	133.84	246.71	215.20	31.51	6
59.01	418.65	129.70	288.95	248.68	40.27	6
58.47	456.81	125.80	331.01	282.22	48.79	6
57.93	495.03	122.21	372.82	315.82	57.00	6
57.39	533.29	119.00	414.29	349.46	64.83	6
56.85	571.60	116.24	455.36	383.15	72.21	6
56.31	609.94	113.98	495.95	416.87	79.09	6
55.77	648.31	112.30	536.01	450.62	85.39	6
55.77	648.31	112.30	536.01	450.62	85.39	5
54.54	750.65	134.17	616.48	527.21	89.27	5
53.33	852.20	156.70	695.50	603.01	92.49	5
52.13	952.92	179.91	773.01	677.98	95.03	5
50.94	1052.80	203.80	849.01	752.11	96.89	5
49.77	1151.81	228.37	923.44	825.37	98.07	5
48.61	1249.93	253.61	996.32	897.74	98.58	5
48.61	1249.93	253.61	996.32	897.74	98.58	4
46.62	1449.97	324.88	1125.09	1021.92	103.17	4
44.63	1649.50	403.34	1246.16	1145.59	100.57	4
42.66	1848.46	492.04	1356.42	1268.69	87.73	4
40.70	2046.78	551.58	1495.20	1391.15	104.05	4
38.75	2244.41	610.41	1634.00	1512.93	121.07	4
36.81	2441.33	672.06	1769.26	1633.98	135.28	4
34.88	2637.49	736.71	1900.78	1754.28	146.49	4
32.96	2832.86	804.84	2028.02	1873.79	154.22	4
31.06	3027.39	877.47	2149.91	1992.47	157.45	4
31.06	3027.39	877.47	2149.91	1992.47	157.45	3
29.67	3175.95	936.33	2239.62	2079.17	160.45	3
28.29	3324.13	998.20	2325.93	2165.49	160.44	3
26.91	3471.91	1068.43	2403.48	2251.41	152.07	3
25.54	3619.30	1136.27	2483.03	2336.94	146.09	3
24.18	3766.32	1201.60	2564.71	2422.10	142.61	3
22.82	3912.97	1265.14	2647.84	2506.90	140.94	3
21.46	4059.28	1327.13	2732.14	2591.34	140.80	3
20.12	4205.23	1387.77	2817.47	2675.44	142.02	3
18.77	4350.85	1447.21	2903.65	2759.20	144.44	3
18.77	4350.85	1447.21	2903.65	2759.20	144.44	2

16.86	4556.44	1528.29	3028.15	2878.69	149.46	2
14.95	4761.52	1610.55	3150.97	2997.67	153.29	2
13.05	4966.09	1693.42	3272.67	3116.15	156.52	2
11.16	5170.15	1777.18	3392.97	3234.11	158.86	2
9.28	5373.70	1862.17	3511.53	3351.56	159.97	2
7.41	5576.71	1948.79	3627.92	3468.47	159.45	2
5.54	5779.19	2054.68	3724.51	3584.85	139.66	2
3.69	5981.13	2187.09	3794.04	3700.69	93.34	2
1.84	6182.52	2319.37	3863.16	3815.99	47.17	2
.00	6383.38	2448.98	3934.40	3930.75	3.65	2

Time = 730. Degree of Consolidation = 37.%

Total Settlement = .505

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 730. = .505

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.18	1.14	.98	.93	.92	1
1.50	1.45	.76	.98	.92	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.91	.90	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.18	86.23	33.09	53.14	46.05	7.09	1
1.45	171.84	69.67	102.17	91.47	10.70	1
.72	257.22	101.82	155.40	136.68	18.73	1
.00	342.50	138.16	204.34	181.77	22.56	1

Time = 730. Degree of Consolidation = 96.%

Total Settlement = .087

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 730. = .087

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.01

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.93	21.42	6.50	6.07	6.01	6
60.02	59.40	21.35	6.49	6.08	6.00	6
59.45	58.86	21.27	6.47	6.08	5.99	6
58.89	58.33	21.20	6.46	6.08	5.97	6
58.33	57.79	21.12	6.44	6.09	5.96	6
57.76	57.26	21.05	6.43	6.09	5.94	6
57.20	56.72	20.97	6.42	6.09	5.93	6
56.64	56.19	20.90	6.40	6.09	5.92	6
56.08	55.65	20.82	6.39	6.09	5.90	6
56.08	55.65	20.82	4.51	4.26	4.11	5
54.82	54.44	20.59	4.44	4.21	4.05	5
53.56	53.24	20.36	4.38	4.15	3.98	5
52.32	52.05	20.12	4.32	4.09	3.92	5
51.10	50.88	19.89	4.25	4.03	3.85	5
49.88	49.72	19.66	4.19	3.97	3.79	5
48.69	48.57	19.43	4.13	3.90	3.73	5
48.69	48.57	19.43	1.93	1.92	1.90	4
46.69	46.59	18.75	1.92	1.90	1.89	4
44.70	44.61	18.06	1.91	1.89	1.88	4
42.72	42.64	17.38	1.89	1.88	1.86	4
40.75	40.68	16.70	1.88	1.86	1.84	4
38.79	38.73	16.01	1.86	1.85	1.82	4
36.85	36.79	15.33	1.84	1.83	1.79	4
34.91	34.87	14.65	1.82	1.81	1.77	4
33.00	32.95	13.97	1.80	1.79	1.75	4
31.09	31.05	13.28	1.78	1.77	1.73	4
31.09	31.05	13.28	1.47	1.47	1.44	3
29.70	29.66	12.72	1.46	1.46	1.43	3
28.32	28.28	12.16	1.45	1.45	1.42	3
26.94	26.90	11.59	1.44	1.44	1.41	3
25.57	25.53	11.03	1.43	1.43	1.40	3
24.21	24.17	10.47	1.42	1.42	1.39	3
22.84	22.81	9.90	1.41	1.41	1.39	3
21.49	21.46	9.34	1.40	1.40	1.38	3
20.14	20.11	8.78	1.39	1.39	1.37	3
18.80	18.77	8.21	1.38	1.38	1.36	3
18.80	18.77	8.21	1.34	1.34	1.32	2
16.88	16.86	7.39	1.33	1.33	1.31	2
14.97	14.95	6.57	1.32	1.32	1.30	2
13.07	13.05	5.75	1.31	1.31	1.29	2
11.18	11.16	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.93	342.48	142.34	200.15	181.76	18.39	6
59.40	380.45	140.57	239.88	215.10	24.78	6
58.86	418.44	138.95	279.49	248.47	31.02	6

58.33	456.45	137.54	318.91	281.86	37.05	6
57.79	494.48	136.39	358.09	315.27	42.82	6
57.26	532.53	135.56	396.97	348.70	48.27	6
56.72	570.58	135.08	435.50	382.13	53.37	6
56.19	608.64	135.02	473.62	415.57	58.05	6
55.65	646.69	135.41	511.28	449.00	62.28	6
55.65	646.69	135.41	511.28	449.00	62.28	5
54.44	748.18	158.53	589.66	524.74	64.91	5
53.24	848.84	182.07	666.76	599.65	67.12	5
52.05	948.64	206.07	742.57	673.70	68.87	5
50.88	1047.57	230.52	817.05	746.88	70.17	5
49.72	1145.61	255.42	890.20	819.17	71.02	5
48.57	1242.76	280.75	962.01	890.57	71.44	5
48.57	1242.76	280.75	962.01	890.57	71.44	4
46.59	1442.61	352.89	1089.72	1014.56	75.16	4
44.61	1641.94	432.36	1209.58	1138.04	71.54	4
42.64	1840.71	512.17	1328.54	1260.94	67.60	4
40.68	2038.83	567.20	1471.63	1383.20	88.43	4
38.73	2236.29	624.40	1611.89	1504.80	107.08	4
36.79	2433.05	684.02	1749.03	1625.70	123.33	4
34.87	2629.08	746.74	1882.33	1745.87	136.46	4
32.95	2824.34	813.25	2011.09	1865.28	145.81	4
31.05	3018.78	884.62	2134.16	1983.86	150.30	4
31.05	3018.78	884.62	2134.16	1983.86	150.30	3
29.66	3167.30	942.26	2225.03	2070.52	154.52	3
28.28	3315.44	1003.52	2311.93	2156.80	155.12	3
26.90	3463.19	1073.04	2390.15	2242.69	147.45	3
25.53	3610.56	1140.45	2470.11	2328.20	141.90	3
24.17	3757.55	1205.94	2551.62	2413.34	138.28	3
22.81	3904.18	1269.70	2634.48	2498.11	136.37	3
21.46	4050.46	1331.94	2718.52	2582.53	135.99	3
20.11	4196.39	1392.82	2803.57	2666.60	136.97	3
18.77	4341.98	1452.51	2889.47	2750.33	139.14	3
18.77	4341.98	1452.51	2889.47	2750.33	139.14	2
16.86	4547.53	1533.86	3013.67	2869.78	143.88	2
14.95	4752.58	1616.10	3136.48	2988.73	147.75	2
13.05	4957.12	1698.95	3258.17	3107.18	151.00	2
11.16	5161.15	1782.70	3378.44	3225.10	153.34	2
9.28	5364.66	1867.70	3496.95	3342.52	154.44	2
7.41	5567.64	1954.37	3613.27	3459.40	153.87	2
5.54	5770.08	2063.04	3707.04	3575.75	131.29	2
3.69	5971.98	2195.46	3776.53	3691.55	84.98	2
1.84	6173.35	2324.24	3849.11	3806.82	42.30	2
.00	6374.20	2449.35	3924.85	3921.57	3.28	2

Time = 1080. Degree of Consolidation = 48.%

Total Settlement = .651

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 1080. = .651

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.17	1.14	.98	.93	.92	1
1.50	1.45	.76	.98	.92	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.91	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.17	86.23	33.24	53.00	46.05	6.94	1
1.45	171.83	70.71	101.12	91.47	9.66	1
.72	257.21	104.96	152.25	136.67	15.59	1
.00	342.48	142.34	200.15	181.76	18.39	1

Time = 1080. Degree of Consolidation = 96.%

Total Settlement = .087

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 1080. = .087

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .86

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.80	21.42	6.50	6.06	6.01	6
60.02	59.27	21.35	6.49	6.06	6.00	6
59.45	58.74	21.27	6.47	6.06	5.99	6
58.89	58.20	21.20	6.46	6.05	5.97	6
58.33	57.67	21.12	6.44	6.05	5.96	6
57.76	57.14	21.05	6.43	6.05	5.94	6
57.20	56.60	20.97	6.42	6.04	5.93	6
56.64	56.07	20.90	6.40	6.04	5.92	6
56.08	55.54	20.82	6.39	6.03	5.90	6
56.08	55.54	20.82	4.51	4.22	4.11	5
54.82	54.34	20.59	4.44	4.16	4.05	5
53.56	53.15	20.36	4.38	4.10	3.98	5
52.32	51.98	20.12	4.32	4.03	3.92	5
51.10	50.82	19.89	4.25	3.97	3.85	5
49.88	49.67	19.66	4.19	3.91	3.79	5
48.69	48.54	19.43	4.13	3.85	3.73	5
48.69	48.54	19.43	1.93	1.91	1.90	4
46.69	46.56	18.75	1.92	1.90	1.89	4
44.70	44.58	18.06	1.91	1.89	1.88	4
42.72	42.61	17.38	1.89	1.87	1.86	4
40.75	40.66	16.70	1.88	1.86	1.84	4

38.79	38.71	16.01	1.86	1.84	1.82	4
36.85	36.78	15.33	1.84	1.83	1.79	4
34.91	34.85	14.65	1.82	1.81	1.77	4
33.00	32.94	13.97	1.80	1.79	1.75	4
31.09	31.04	13.28	1.78	1.77	1.73	4
31.09	31.04	13.28	1.47	1.47	1.44	3
29.70	29.65	12.72	1.46	1.46	1.43	3
28.32	28.27	12.16	1.45	1.45	1.42	3
26.94	26.90	11.59	1.44	1.44	1.41	3
25.57	25.53	11.03	1.43	1.43	1.40	3
24.21	24.16	10.47	1.42	1.42	1.39	3
22.84	22.81	9.90	1.41	1.41	1.39	3
21.49	21.45	9.34	1.40	1.40	1.38	3
20.14	20.11	8.78	1.39	1.39	1.37	3
18.80	18.76	8.21	1.38	1.38	1.36	3
18.80	18.76	8.21	1.34	1.33	1.32	2
16.88	16.85	7.39	1.33	1.33	1.31	2
14.97	14.95	6.57	1.32	1.32	1.30	2
13.07	13.05	5.75	1.31	1.31	1.29	2
11.18	11.16	4.93	1.30	1.30	1.28	2
9.30	9.28	4.11	1.29	1.29	1.27	2
7.43	7.41	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.80	342.47	145.92	196.55	181.74	14.81	6
59.27	380.37	146.30	234.06	215.02	19.04	6
58.74	418.26	146.80	271.46	248.29	23.17	6
58.20	456.15	147.46	308.69	281.56	27.13	6
57.67	494.02	148.34	345.68	314.81	30.87	6
57.14	531.88	149.48	382.40	348.05	34.34	6
56.60	569.72	150.93	418.79	381.27	37.52	6
56.07	607.54	152.70	454.84	414.47	40.37	6
55.54	645.33	154.84	490.49	447.64	42.85	6
55.54	645.33	154.84	490.49	447.64	42.85	5
54.34	746.11	179.02	567.09	522.67	44.42	5
53.15	846.01	203.44	642.56	596.82	45.75	5
51.98	945.03	228.13	716.90	670.09	46.81	5
50.82	1043.16	253.10	790.06	742.47	47.59	5
49.67	1140.39	278.33	862.05	813.95	48.11	5
48.54	1236.71	303.82	932.89	884.52	48.37	5
48.54	1236.71	303.82	932.89	884.52	48.37	4
46.56	1436.40	377.31	1059.09	1008.35	50.74	4
44.58	1635.56	458.36	1177.20	1131.65	45.55	4
42.61	1834.14	527.27	1306.87	1254.37	52.50	4
40.66	2032.09	581.54	1450.54	1376.46	74.08	4
38.71	2229.38	637.71	1591.67	1497.90	93.78	4
36.78	2425.99	696.30	1729.69	1618.64	111.04	4
34.85	2621.88	757.88	1864.00	1738.68	125.32	4
32.94	2817.01	823.23	1993.79	1857.95	135.84	4
31.04	3011.34	893.86	2117.48	1976.42	141.06	4
31.04	3011.34	893.86	2117.48	1976.42	141.06	3
29.65	3159.80	950.84	2208.96	2063.02	145.94	3
28.27	3307.89	1012.40	2295.49	2149.25	146.24	3
26.90	3455.60	1081.25	2374.34	2235.10	139.24	3
25.53	3602.92	1148.26	2454.66	2320.56	134.10	3
24.16	3749.87	1213.38	2536.49	2405.66	130.84	3

22.81	3896.46	1276.81	2619.65	2490.39	129.26	3
21.45	4042.70	1338.74	2703.96	2574.76	129.19	3
20.11	4188.59	1399.33	2789.26	2658.80	130.46	3
18.76	4334.15	1458.76	2875.39	2742.50	132.89	3
18.76	4334.15	1458.76	2875.39	2742.50	132.89	2
16.85	4539.66	1539.60	3000.06	2861.91	138.15	2
14.95	4744.67	1621.79	3122.88	2980.83	142.05	2
13.05	4949.18	1704.62	3244.55	3099.23	145.32	2
11.16	5153.17	1788.37	3364.79	3217.13	147.67	2
9.28	5356.64	1873.39	3483.25	3334.50	148.75	2
7.41	5559.59	1960.10	3599.49	3451.35	148.14	2
5.54	5762.00	2071.64	3690.35	3567.66	122.69	2
3.69	5963.87	2201.44	3762.43	3683.43	78.99	2
1.84	6165.22	2327.28	3837.94	3798.68	39.25	2
.00	6366.06	2449.58	3916.47	3913.42	3.05	2

Time = 1440. Degree of Consolidation = 58.%

Total Settlement = .782

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 1440. = .782

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.17	1.14	.98	.93	.92	1
1.50	1.45	.76	.98	.92	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.91	.90	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.17	86.23	33.36	52.87	46.05	6.82	1
1.45	171.83	71.59	100.24	91.46	8.77	1
.72	257.20	107.64	149.57	136.66	12.91	1
.00	342.47	145.92	196.55	181.74	14.81	1

Time = 1440. Degree of Consolidation = 97.%

Total Settlement = .088

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 1440. = .088

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .73

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.68	21.42	6.50	6.05	6.01	6
60.02	59.15	21.35	6.49	6.04	6.00	6
59.45	58.62	21.27	6.47	6.04	5.99	6
58.89	58.09	21.20	6.46	6.03	5.97	6
58.33	57.56	21.12	6.44	6.02	5.96	6
57.76	57.03	21.05	6.43	6.01	5.94	6
57.20	56.50	20.97	6.42	6.00	5.93	6
56.64	55.97	20.90	6.40	5.99	5.92	6
56.08	55.44	20.82	6.39	5.98	5.90	6
56.08	55.44	20.82	4.51	4.17	4.11	5
54.82	54.25	20.59	4.44	4.11	4.05	5
53.56	53.07	20.36	4.38	4.05	3.98	5
52.32	51.91	20.12	4.32	3.99	3.92	5
51.10	50.76	19.89	4.25	3.92	3.85	5
49.88	49.63	19.66	4.19	3.86	3.79	5
48.69	48.51	19.43	4.13	3.80	3.73	5
48.69	48.51	19.43	1.93	1.91	1.90	4
46.69	46.52	18.75	1.92	1.90	1.89	4
44.70	44.55	18.06	1.91	1.88	1.88	4
42.72	42.59	17.38	1.89	1.87	1.86	4
40.75	40.63	16.70	1.88	1.85	1.84	4
38.79	38.69	16.01	1.86	1.84	1.82	4
36.85	36.76	15.33	1.84	1.82	1.79	4
34.91	34.84	14.65	1.82	1.80	1.77	4
33.00	32.93	13.97	1.80	1.79	1.75	4
31.09	31.03	13.28	1.78	1.77	1.73	4
31.09	31.03	13.28	1.47	1.47	1.44	3
29.70	29.64	12.72	1.46	1.46	1.43	3
28.32	28.26	12.16	1.45	1.45	1.42	3
26.94	26.89	11.59	1.44	1.44	1.41	3
25.57	25.52	11.03	1.43	1.42	1.40	3
24.21	24.16	10.47	1.42	1.41	1.39	3
22.84	22.80	9.90	1.41	1.40	1.39	3
21.49	21.45	9.34	1.40	1.39	1.38	3
20.14	20.10	8.78	1.39	1.38	1.37	3
18.80	18.76	8.21	1.38	1.38	1.36	3
18.80	18.76	8.21	1.34	1.33	1.32	2
16.88	16.85	7.39	1.33	1.32	1.31	2
14.97	14.94	6.57	1.32	1.31	1.30	2
13.07	13.05	5.75	1.31	1.30	1.29	2
11.18	11.16	4.93	1.30	1.29	1.28	2
9.30	9.28	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.68	342.45	149.13	193.32	181.73	11.60	6
59.15	380.29	151.40	228.89	214.95	13.95	6
58.62	418.10	153.76	264.34	248.13	16.21	6
58.09	455.87	156.25	299.62	281.29	18.33	6
57.56	493.61	158.92	334.69	314.40	20.29	6
57.03	531.31	161.78	369.53	347.48	22.05	6
56.50	568.96	164.87	404.09	380.51	23.58	6
55.97	606.57	168.24	438.34	413.50	24.83	6
55.44	644.13	171.89	472.24	446.44	25.80	6
55.44	644.13	171.89	472.24	446.44	25.80	5
54.25	744.28	197.03	547.25	520.84	26.41	5
53.07	843.52	222.26	621.26	594.33	26.93	5
51.91	941.85	247.60	694.25	666.91	27.34	5
50.76	1039.27	273.06	766.21	738.58	27.63	5
49.63	1135.78	298.63	837.15	809.34	27.81	5
48.51	1231.37	324.29	907.08	879.18	27.90	5
48.51	1231.37	324.29	907.08	879.18	27.90	4
46.52	1430.91	399.42	1031.49	1002.86	28.63	4
44.55	1629.92	482.38	1147.54	1126.01	21.53	4
42.59	1828.33	541.56	1286.77	1248.56	38.21	4
40.63	2026.11	595.38	1430.74	1370.48	60.25	4
38.69	2223.24	651.14	1572.10	1491.75	80.35	4
36.76	2419.69	709.30	1710.39	1612.34	98.04	4
34.84	2615.43	770.30	1845.13	1732.22	112.90	4
32.93	2810.42	835.15	1975.27	1851.35	123.92	4
31.03	3004.60	905.40	2099.20	1969.68	129.52	4
31.03	3004.60	905.40	2099.20	1969.68	129.52	3
29.64	3152.99	962.00	2190.99	2056.21	134.78	3
28.26	3301.02	1024.04	2276.98	2142.38	134.60	3
26.89	3448.66	1091.37	2357.29	2228.16	129.13	3
25.52	3595.93	1157.26	2438.66	2313.57	125.09	3
24.16	3742.83	1221.91	2520.92	2398.61	122.31	3
22.80	3889.37	1284.89	2604.48	2483.30	121.18	3
21.45	4035.57	1346.40	2689.17	2567.63	121.54	3
20.10	4181.42	1406.59	2774.82	2651.63	123.20	3
18.76	4326.93	1465.65	2861.28	2735.28	126.00	3
18.76	4326.93	1465.65	2861.28	2735.28	126.00	2
16.85	4532.41	1545.73	2986.68	2854.66	132.02	2
14.94	4737.38	1627.60	3109.78	2973.54	136.25	2
13.05	4941.85	1710.10	3231.75	3091.91	139.84	2
11.16	5145.81	1793.53	3352.28	3209.77	142.51	2
9.28	5349.25	1878.23	3471.03	3327.11	143.91	2
7.40	5552.17	1964.61	3587.56	3443.93	143.62	2
5.54	5754.55	2077.42	3677.14	3560.22	116.92	2
3.69	5956.41	2205.25	3751.15	3675.97	75.18	2
1.84	6157.74	2329.22	3828.52	3791.21	37.31	2
.00	6358.58	2449.74	3908.84	3905.95	2.90	2

Time = 1825. Degree of Consolidation = 67.%

Total Settlement = .901

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 1825. = .901

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.17	1.14	.98	.93	.92	1
1.50	1.45	.76	.98	.92	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.91	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.17	86.23	33.47	52.76	46.05	6.71	1
1.45	171.83	72.37	99.45	91.46	7.99	1
.72	257.20	110.02	147.18	136.65	10.53	1
.00	342.45	149.13	193.32	181.73	11.60	1

Time = 1825. Degree of Consolidation = 97.%

Total Settlement = .088

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 1825. = .088

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .61

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.50	21.42	6.50	6.01	6.01	6
60.02	58.97	21.35	6.49	6.00	6.00	6
59.45	58.44	21.27	6.47	5.99	5.99	6
58.89	57.91	21.20	6.46	5.97	5.97	6
58.33	57.39	21.12	6.44	5.96	5.96	6
57.76	56.86	21.05	6.43	5.94	5.94	6
57.20	56.34	20.97	6.42	5.93	5.93	6
56.64	55.82	20.90	6.40	5.92	5.92	6
56.08	55.29	20.82	6.39	5.90	5.90	6
56.08	55.29	20.82	4.51	4.11	4.11	5
54.82	54.12	20.59	4.44	4.05	4.05	5
53.56	52.95	20.36	4.38	3.98	3.98	5
52.32	51.81	20.12	4.32	3.92	3.92	5
51.10	50.67	19.89	4.25	3.85	3.85	5
49.88	49.56	19.66	4.19	3.79	3.79	5
48.69	48.45	19.43	4.13	3.73	3.73	5

48.69	48.45	19.43	1.93	1.90	1.90	4
46.69	46.47	18.75	1.92	1.89	1.89	4
44.70	44.50	18.06	1.91	1.88	1.88	4
42.72	42.54	17.38	1.89	1.86	1.86	4
40.75	40.59	16.70	1.88	1.85	1.84	4
38.79	38.65	16.01	1.86	1.83	1.82	4
36.85	36.72	15.33	1.84	1.82	1.79	4
34.91	34.81	14.65	1.82	1.80	1.77	4
33.00	32.90	13.97	1.80	1.78	1.75	4
31.09	31.01	13.28	1.78	1.76	1.73	4
31.09	31.01	13.28	1.47	1.46	1.44	3
29.70	29.62	12.72	1.46	1.45	1.43	3
28.32	28.24	12.16	1.45	1.44	1.42	3
26.94	26.87	11.59	1.44	1.43	1.41	3
25.57	25.51	11.03	1.43	1.42	1.40	3
24.21	24.14	10.47	1.42	1.41	1.39	3
22.84	22.79	9.90	1.41	1.40	1.39	3
21.49	21.44	9.34	1.40	1.39	1.38	3
20.14	20.09	8.78	1.39	1.38	1.37	3
18.80	18.75	8.21	1.38	1.37	1.36	3
18.80	18.75	8.21	1.34	1.33	1.32	2
16.88	16.84	7.39	1.33	1.32	1.31	2
14.97	14.94	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.69	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.50	342.28	160.73	181.55	181.55	.00	6
58.97	379.94	165.35	214.59	214.59	.00	6
58.44	417.53	169.97	247.56	247.56	.00	6
57.91	455.05	174.59	280.46	280.46	.00	6
57.39	492.51	179.21	313.30	313.30	.00	6
56.86	529.90	183.83	346.07	346.07	.00	6
56.34	567.23	188.45	378.78	378.78	.00	6
55.82	604.49	193.07	411.42	411.42	.00	6
55.29	641.68	197.69	443.99	443.99	.00	6
55.29	641.68	197.69	443.99	443.99	.00	5
54.12	740.89	223.44	517.45	517.45	.00	5
52.95	839.17	249.19	589.98	589.98	.00	5
51.81	936.53	274.94	661.59	661.59	.00	5
50.67	1032.97	300.69	732.28	732.28	.00	5
49.56	1128.48	326.44	802.04	802.04	.00	5
48.45	1223.07	352.19	870.88	870.88	.00	5
48.45	1223.07	352.19	870.88	870.88	.00	4
46.47	1422.42	426.67	995.75	994.37	1.38	4
44.50	1621.26	503.91	1117.35	1117.35	.00	4
42.54	1819.48	559.27	1260.21	1239.71	20.50	4
40.59	2017.04	615.01	1402.03	1361.41	40.62	4
38.65	2213.93	671.78	1542.15	1482.44	59.70	4
36.72	2410.13	730.12	1680.01	1602.79	77.23	4
34.81	2605.62	791.07	1814.55	1722.42	92.13	4
32.90	2800.36	855.73	1944.63	1841.30	103.33	4
31.01	2994.30	926.14	2068.16	1959.38	108.78	4
31.01	2994.30	926.14	2068.16	1959.38	108.78	3

29.62	3142.56	982.76	2159.81	2045.78	114.03	3
28.24	3290.45	1046.54	2243.91	2131.81	112.10	3
26.87	3437.98	1111.93	2326.05	2217.48	108.57	3
25.51	3585.13	1175.97	2409.16	2302.78	106.38	3
24.14	3731.94	1238.87	2493.07	2387.72	105.35	3
22.79	3878.39	1300.77	2577.61	2472.31	105.30	3
21.44	4024.49	1361.40	2663.10	2556.56	106.54	3
20.09	4170.26	1420.76	2749.50	2640.47	109.03	3
18.75	4315.70	1479.04	2836.66	2724.05	112.61	3
18.75	4315.70	1479.04	2836.66	2724.05	112.61	2
16.84	4521.10	1557.28	2963.82	2843.35	120.47	2
14.94	4726.01	1637.90	3088.10	2962.16	125.94	2
13.04	4930.42	1719.31	3211.11	3080.47	130.63	2
11.15	5134.32	1801.62	3332.71	3198.28	134.42	2
9.27	5337.72	1885.16	3452.56	3315.58	136.98	2
7.40	5540.60	1970.35	3570.25	3432.36	137.89	2
5.54	5742.95	2083.97	3658.98	3548.61	110.37	2
3.69	5944.78	2209.57	3735.21	3664.34	70.86	2
1.84	6146.10	2331.42	3814.69	3779.57	35.12	2
.00	6346.93	2449.90	3897.03	3894.30	2.73	2

Time = 2520. Degree of Consolidation = 80.%

Total Settlement = 1.085

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 2520. = 1.085

Settlement caused by Secondary Compression at time 2520. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.00	2.91	1.52
2.25	2.17	1.14
1.50	1.45	.76
.75	.72	.38
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
2.91	.00	.00
2.17	86.17	40.18
1.45	171.71	80.36
.72	257.05	120.55
.00	342.28	160.73

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
45.99	45.99	.00	1
91.34	91.34	.00	1
136.50	136.50	.00	1
181.55	181.55	.00	1

Time = 2520. Degree of Consolidation = 100.%

Total Settlement = .091

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 2520. = .091

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .42

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.48	21.42	6.50	6.01	6.01	6
60.02	58.95	21.35	6.49	6.00	6.00	6
59.45	58.42	21.27	6.47	5.98	5.99	6
58.89	57.89	21.20	6.46	5.97	5.97	6
58.33	57.37	21.12	6.44	5.96	5.96	6
57.76	56.84	21.05	6.43	5.94	5.94	6
57.20	56.32	20.97	6.42	5.93	5.93	6
56.64	55.80	20.90	6.40	5.91	5.92	6
56.08	55.28	20.82	6.39	5.90	5.90	6
56.08	55.28	20.82	4.51	4.11	4.11	5
54.82	54.10	20.59	4.44	4.05	4.05	5
53.56	52.94	20.36	4.38	3.98	3.98	5
52.32	51.79	20.12	4.32	3.92	3.92	5
51.10	50.66	19.89	4.25	3.85	3.85	5
49.88	49.54	19.66	4.19	3.79	3.79	5
48.69	48.43	19.43	4.13	3.73	3.73	5
48.69	48.43	19.43	1.93	1.90	1.90	4
46.69	46.46	18.75	1.92	1.89	1.89	4
44.70	44.48	18.06	1.91	1.88	1.88	4
42.72	42.52	17.38	1.89	1.86	1.86	4
40.75	40.57	16.70	1.88	1.85	1.84	4
38.79	38.64	16.01	1.86	1.83	1.82	4
36.85	36.71	15.33	1.84	1.81	1.79	4
34.91	34.79	14.65	1.82	1.80	1.77	4
33.00	32.89	13.97	1.80	1.78	1.75	4
31.09	31.00	13.28	1.78	1.76	1.73	4
31.09	31.00	13.28	1.47	1.46	1.44	3
29.70	29.61	12.72	1.46	1.45	1.43	3
28.32	28.24	12.16	1.45	1.44	1.42	3
26.94	26.86	11.59	1.44	1.43	1.41	3
25.57	25.50	11.03	1.43	1.42	1.40	3
24.21	24.14	10.47	1.42	1.41	1.39	3
22.84	22.78	9.90	1.41	1.40	1.39	3
21.49	21.43	9.34	1.40	1.39	1.38	3
20.14	20.09	8.78	1.39	1.38	1.37	3
18.80	18.75	8.21	1.38	1.37	1.36	3
18.80	18.75	8.21	1.34	1.33	1.32	2
16.88	16.84	7.39	1.33	1.32	1.31	2
14.97	14.94	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.69	1.64	1.26	1.25	1.25	2

1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.48	342.28	160.73	181.55	181.55	.00	6
58.95	379.93	165.35	214.58	214.58	.00	6
58.42	417.50	169.97	247.54	247.54	.00	6
57.89	455.01	174.59	280.43	280.43	.00	6
57.37	492.46	179.21	313.25	313.25	.00	6
56.84	529.84	183.83	346.01	346.01	.00	6
56.32	567.15	188.45	378.70	378.70	.00	6
55.80	604.40	193.07	411.33	411.33	.00	6
55.28	641.58	197.69	443.89	443.89	.00	6
55.28	641.58	197.69	443.89	443.89	.00	5
54.10	740.79	223.44	517.35	517.35	.00	5
52.94	839.07	249.19	589.88	589.88	.00	5
51.79	936.43	274.94	661.49	661.49	.00	5
50.66	1032.87	300.69	732.18	732.18	.00	5
49.54	1128.38	326.44	801.94	801.94	.00	5
48.43	1222.97	352.19	870.78	870.78	.00	5
48.43	1222.97	352.19	870.78	870.78	.00	4
46.46	1422.32	426.67	995.65	994.27	1.38	4
44.48	1621.16	503.91	1117.26	1117.26	.00	4
42.52	1819.37	561.18	1258.20	1239.61	18.59	4
40.57	2016.90	618.66	1398.24	1361.27	36.97	4
38.64	2213.73	677.02	1536.72	1482.25	54.47	4
36.71	2409.86	736.70	1673.16	1602.52	70.64	4
34.79	2605.27	798.75	1806.52	1722.07	84.45	4
32.89	2799.92	864.17	1935.75	1840.85	94.89	4
31.00	2993.75	934.92	2058.83	1958.83	100.00	4
31.00	2993.75	934.92	2058.83	1958.83	100.00	3
29.61	3141.95	991.84	2150.11	2045.17	104.94	3
28.24	3289.79	1056.75	2233.04	2131.15	101.89	3
26.86	3437.25	1121.63	2315.62	2216.76	98.87	3
25.50	3584.36	1185.22	2399.14	2302.00	97.14	3
24.14	3731.11	1247.68	2483.43	2386.90	96.53	3
22.78	3877.51	1309.16	2568.36	2471.44	96.92	3
21.43	4023.57	1369.24	2654.33	2555.64	98.69	3
20.09	4169.30	1428.10	2741.20	2639.51	101.69	3
18.75	4314.70	1485.90	2828.80	2723.05	105.75	3
18.75	4314.70	1485.90	2828.80	2723.05	105.75	2
16.84	4520.06	1563.55	2956.51	2842.31	114.20	2
14.94	4724.93	1643.59	3081.34	2961.08	120.26	2
13.04	4929.30	1724.39	3204.92	3079.36	125.56	2
11.15	5133.18	1806.07	3327.11	3197.14	129.97	2
9.27	5336.55	1888.98	3447.57	3314.41	133.16	2
7.40	5539.41	1973.51	3565.90	3431.17	134.73	2
5.54	5741.74	2087.57	3654.18	3547.41	106.77	2
3.69	5943.56	2211.95	3731.62	3663.13	68.49	2
1.84	6144.88	2332.62	3812.25	3778.34	33.91	2
.00	6345.70	2450.00	3895.71	3893.07	2.64	2

Time = 2880. Degree of Consolidation = 82.%

Total Settlement = 1.105

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 2880. = 1.103

Settlement caused by Secondary Compression at time 2880. = .002

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.17	1.14	.98	.92	.92	1
1.50	1.45	.76	.98	.91	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.90	.90	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.17	86.17	40.18	45.99	45.99	.00	1
1.45	171.71	80.36	91.34	91.34	.00	1
.72	257.05	120.55	136.50	136.50	.00	1
.00	342.28	160.73	181.55	181.55	.00	1

Time = 2880. Degree of Consolidation = 100.%

Total Settlement = .091

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 2880. = .091

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .40

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.46	21.42	6.50	6.01	6.01	6
60.02	58.93	21.35	6.49	5.99	6.00	6
59.45	58.41	21.27	6.47	5.98	5.99	6
58.89	57.88	21.20	6.46	5.97	5.97	6
58.33	57.35	21.12	6.44	5.95	5.96	6
57.76	56.83	21.05	6.43	5.94	5.94	6
57.20	56.30	20.97	6.42	5.92	5.93	6
56.64	55.78	20.90	6.40	5.91	5.92	6
56.08	55.26	20.82	6.39	5.90	5.90	6
56.08	55.26	20.82	4.51	4.11	4.11	5
54.82	54.08	20.59	4.44	4.05	4.05	5

53.56	52.92	20.36	4.38	3.98	3.98	5
52.32	51.77	20.12	4.32	3.92	3.92	5
51.10	50.64	19.89	4.25	3.85	3.85	5
49.88	49.52	19.66	4.19	3.79	3.79	5
48.69	48.42	19.43	4.13	3.73	3.73	5
48.69	48.42	19.43	1.93	1.90	1.90	4
46.69	46.44	18.75	1.92	1.89	1.89	4
44.70	44.47	18.06	1.91	1.88	1.88	4
42.72	42.51	17.38	1.89	1.86	1.86	4
40.75	40.56	16.70	1.88	1.85	1.84	4
38.79	38.62	16.01	1.86	1.83	1.82	4
36.85	36.69	15.33	1.84	1.81	1.79	4
34.91	34.78	14.65	1.82	1.79	1.77	4
33.00	32.88	13.97	1.80	1.78	1.75	4
31.09	30.99	13.28	1.78	1.76	1.73	4
31.09	30.99	13.28	1.47	1.46	1.44	3
29.70	29.60	12.72	1.46	1.45	1.43	3
28.32	28.23	12.16	1.45	1.44	1.42	3
26.94	26.86	11.59	1.44	1.43	1.41	3
25.57	25.49	11.03	1.43	1.42	1.40	3
24.21	24.13	10.47	1.42	1.41	1.39	3
22.84	22.78	9.90	1.41	1.40	1.39	3
21.49	21.43	9.34	1.40	1.39	1.38	3
20.14	20.08	8.78	1.39	1.38	1.37	3
18.80	18.75	8.21	1.38	1.37	1.36	3
18.80	18.75	8.21	1.34	1.33	1.32	2
16.88	16.84	7.39	1.33	1.32	1.31	2
14.97	14.93	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.46	342.28	160.73	181.55	181.55	.00	6
58.93	379.92	165.35	214.57	214.57	.00	6
58.41	417.48	169.97	247.51	247.51	.00	6
57.88	454.98	174.59	280.39	280.39	.00	6
57.35	492.41	179.21	313.20	313.20	.00	6
56.83	529.78	183.83	345.95	345.95	.00	6
56.30	567.08	188.45	378.63	378.63	.00	6
55.78	604.31	193.07	411.24	411.24	.00	6
55.26	641.48	197.69	443.79	443.79	.00	6
55.26	641.48	197.69	443.79	443.79	.00	5
54.08	740.69	223.44	517.25	517.25	.00	5
52.92	838.97	249.19	589.78	589.78	.00	5
51.77	936.33	274.94	661.39	661.39	.00	5
50.64	1032.77	300.69	732.08	732.08	.00	5
49.52	1128.28	326.44	801.84	801.84	.00	5
48.42	1222.87	352.19	870.68	870.68	.00	5
48.42	1222.87	352.19	870.68	870.68	.00	4
46.44	1422.22	426.67	995.55	994.17	1.38	4
44.47	1621.07	503.91	1117.16	1117.16	.00	4
42.51	1819.27	562.33	1256.94	1239.50	17.44	4
40.56	2016.77	621.05	1395.72	1361.15	34.57	4
38.62	2213.57	680.41	1533.16	1482.09	51.08	4

36.69	2409.66	741.22	1668.44	1602.31	66.12	4
34.78	2605.00	804.15	1800.86	1721.80	79.06	4
32.88	2799.58	870.47	1929.11	1840.52	88.60	4
30.99	2993.33	942.00	2051.34	1958.41	92.93	4
30.99	2993.33	942.00	2051.34	1958.41	92.93	3
29.60	3141.49	999.66	2141.83	2044.71	97.12	3
28.23	3289.27	1065.79	2223.49	2130.63	92.85	3
26.86	3436.69	1130.51	2306.18	2216.19	89.99	3
25.49	3583.74	1193.95	2389.79	2301.39	88.40	3
24.13	3730.45	1256.30	2474.15	2386.23	87.92	3
22.78	3876.80	1317.35	2559.45	2470.73	88.72	3
21.43	4022.82	1377.05	2645.77	2554.89	90.88	3
20.08	4168.50	1435.55	2732.95	2638.71	94.24	3
18.75	4313.86	1493.00	2820.86	2722.21	98.65	3
18.75	4313.86	1493.00	2820.86	2722.21	98.65	2
16.84	4519.17	1569.98	2949.20	2841.43	107.77	2
14.93	4724.01	1649.33	3074.68	2960.16	114.51	2
13.04	4928.35	1729.51	3198.84	3078.41	120.43	2
11.15	5132.20	1810.57	3321.63	3196.16	125.47	2
9.27	5335.55	1892.83	3442.71	3313.40	129.31	2
7.40	5538.38	1976.69	3561.69	3430.14	131.55	2
5.54	5740.70	2091.19	3649.50	3546.36	103.14	2
3.68	5942.50	2214.34	3728.16	3662.07	66.10	2
1.84	6143.81	2333.84	3809.97	3777.28	32.69	2
.00	6344.64	2450.09	3894.54	3892.00	2.54	2

Time = 3240. Degree of Consolidation = 83.%

Total Settlement = 1.122

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 3240. = 1.118

Settlement caused by Secondary Compression at time 3240. = .004

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.17	1.14	.98	.92	.92	1
1.50	1.45	.76	.98	.91	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.90	.90	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.17	86.17	40.18	45.99	45.99	.00	1
1.45	171.71	80.36	91.34	91.34	.00	1
.72	257.05	120.55	136.50	136.50	.00	1
.00	342.28	160.73	181.55	181.55	.00	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .091

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 3240. = .091

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .39

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.44	21.42	6.50	6.01	6.01	6
60.02	58.91	21.35	6.49	5.99	6.00	6
59.45	58.39	21.27	6.47	5.98	5.99	6
58.89	57.86	21.20	6.46	5.96	5.97	6
58.33	57.34	21.12	6.44	5.95	5.96	6
57.76	56.81	21.05	6.43	5.94	5.94	6
57.20	56.29	20.97	6.42	5.92	5.93	6
56.64	55.76	20.90	6.40	5.91	5.92	6
56.08	55.24	20.82	6.39	5.89	5.90	6
56.08	55.24	20.82	4.51	4.11	4.11	5
54.82	54.07	20.59	4.44	4.05	4.05	5
53.56	52.90	20.36	4.38	3.98	3.98	5
52.32	51.76	20.12	4.32	3.92	3.92	5
51.10	50.62	19.89	4.25	3.85	3.85	5
49.88	49.51	19.66	4.19	3.79	3.79	5
48.69	48.40	19.43	4.13	3.73	3.73	5
48.69	48.40	19.43	1.93	1.90	1.90	4
46.69	46.42	18.75	1.92	1.89	1.89	4
44.70	44.45	18.06	1.91	1.88	1.88	4
42.72	42.49	17.38	1.89	1.86	1.86	4
40.75	40.54	16.70	1.88	1.85	1.84	4
38.79	38.60	16.01	1.86	1.83	1.82	4
36.85	36.68	15.33	1.84	1.81	1.79	4
34.91	34.76	14.65	1.82	1.79	1.77	4
33.00	32.86	13.97	1.80	1.77	1.75	4
31.09	30.98	13.28	1.78	1.75	1.73	4
31.09	30.98	13.28	1.47	1.46	1.44	3
29.70	29.59	12.72	1.46	1.45	1.43	3
28.32	28.22	12.16	1.45	1.44	1.42	3
26.94	26.85	11.59	1.44	1.43	1.41	3
25.57	25.48	11.03	1.43	1.42	1.40	3
24.21	24.12	10.47	1.42	1.41	1.39	3
22.84	22.77	9.90	1.41	1.40	1.39	3
21.49	21.42	9.34	1.40	1.39	1.38	3
20.14	20.08	8.78	1.39	1.38	1.37	3
18.80	18.74	8.21	1.38	1.37	1.36	3
18.80	18.74	8.21	1.34	1.33	1.32	2
16.88	16.83	7.39	1.33	1.32	1.31	2
14.97	14.93	6.57	1.32	1.31	1.30	2
13.07	13.04	5.75	1.31	1.30	1.29	2

11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.44	342.28	160.73	181.55	181.55	.00	6
58.91	379.91	165.35	214.56	214.56	.00	6
58.39	417.46	169.97	247.49	247.49	.00	6
57.86	454.94	174.59	280.35	280.35	.00	6
57.34	492.36	179.21	313.15	313.15	.00	6
56.81	529.71	183.83	345.88	345.88	.00	6
56.29	566.99	188.45	378.55	378.55	.00	6
55.76	604.21	193.07	411.14	411.14	.00	6
55.24	641.37	197.69	443.68	443.68	.00	6
55.24	641.37	197.69	443.68	443.68	.00	5
54.07	740.58	223.44	517.14	517.14	.00	5
52.90	838.86	249.19	589.67	589.67	.00	5
51.76	936.22	274.94	661.28	661.28	.00	5
50.62	1032.65	300.69	731.96	731.96	.00	5
49.51	1128.17	326.44	801.73	801.73	.00	5
48.40	1222.75	352.19	870.56	870.56	.00	5
48.40	1222.75	352.19	870.56	870.56	.00	4
46.42	1422.10	426.67	995.44	994.05	1.38	4
44.45	1620.95	503.91	1117.05	1117.05	.00	4
42.49	1819.15	563.22	1255.93	1239.38	16.55	4
40.54	2016.64	622.91	1393.73	1361.01	32.71	4
38.60	2213.41	683.32	1530.09	1481.92	48.16	4
36.68	2409.45	745.26	1664.19	1602.11	62.08	4
34.76	2604.74	809.49	1795.25	1721.54	73.71	4
32.86	2799.25	877.06	1922.19	1840.18	82.00	4
30.98	2992.92	950.23	2042.69	1957.99	84.70	4
30.98	2992.92	950.23	2042.69	1957.99	84.70	3
29.59	3141.02	1009.43	2131.58	2044.24	87.35	3
28.22	3288.75	1075.61	2213.13	2130.11	83.03	3
26.85	3436.11	1140.33	2295.78	2215.61	80.17	3
25.48	3583.11	1203.77	2379.34	2300.75	78.59	3
24.12	3729.75	1265.89	2463.87	2385.54	78.33	3
22.77	3876.06	1326.51	2549.55	2469.98	79.56	3
21.42	4022.02	1385.80	2636.22	2554.09	82.13	3
20.08	4167.66	1443.92	2723.73	2637.87	85.87	3
18.74	4312.97	1501.03	2811.94	2721.32	90.62	3
18.74	4312.97	1501.03	2811.94	2721.32	90.62	2
16.83	4518.24	1577.26	2940.98	2840.49	100.49	2
14.93	4723.03	1655.87	3067.16	2959.18	107.97	2
13.04	4927.33	1735.35	3191.98	3077.39	114.59	2
11.15	5131.15	1815.69	3315.45	3195.11	120.35	2
9.27	5334.46	1897.22	3437.25	3312.32	124.92	2
7.40	5537.27	1980.31	3556.96	3429.04	127.93	2
5.54	5739.57	2095.32	3644.25	3545.24	99.02	2
3.68	5941.36	2217.06	3724.30	3660.93	63.37	2
1.84	6142.66	2335.23	3807.44	3776.13	31.31	2
.00	6343.48	2450.20	3893.29	3890.85	2.43	2

Time = 3650. Degree of Consolidation = 84.%

Total Settlement = 1.140

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 3650. = 1.135

Settlement caused by Secondary Compression at time 3650. = .005

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.17	1.14	.98	.92	.92	1
1.50	1.45	.76	.98	.91	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.90	.90	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.17	86.17	40.18	45.99	45.99	.00	1
1.45	171.71	80.36	91.34	91.34	.00	1
.72	257.05	120.55	136.50	136.50	.00	1
.00	342.28	160.73	181.55	181.55	.00	1

Time = 3650. Degree of Consolidation = 100.%

Total Settlement = .091

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 3650. = .091

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .37

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.42	21.42	6.50	6.01	6.01	6
60.02	58.89	21.35	6.49	5.99	6.00	6
59.45	58.36	21.27	6.47	5.98	5.99	6
58.89	57.83	21.20	6.46	5.96	5.97	6
58.33	57.31	21.12	6.44	5.95	5.96	6
57.76	56.78	21.05	6.43	5.93	5.94	6

57.20	56.26	20.97	6.42	5.92	5.93	6
56.64	55.74	20.90	6.40	5.91	5.92	6
56.08	55.22	20.82	6.39	5.89	5.90	6
56.08	55.22	20.82	4.51	4.11	4.11	5
54.82	54.04	20.59	4.44	4.05	4.05	5
53.56	52.88	20.36	4.38	3.98	3.98	5
52.32	51.73	20.12	4.32	3.92	3.92	5
51.10	50.60	19.89	4.25	3.85	3.85	5
49.88	49.48	19.66	4.19	3.79	3.79	5
48.69	48.38	19.43	4.13	3.73	3.73	5
48.69	48.38	19.43	1.93	1.90	1.90	4
46.69	46.40	18.75	1.92	1.89	1.89	4
44.70	44.43	18.06	1.91	1.88	1.88	4
42.72	42.47	17.38	1.89	1.86	1.86	4
40.75	40.52	16.70	1.88	1.84	1.84	4
38.79	38.58	16.01	1.86	1.83	1.82	4
36.85	36.65	15.33	1.84	1.81	1.79	4
34.91	34.74	14.65	1.82	1.79	1.77	4
33.00	32.84	13.97	1.80	1.77	1.75	4
31.09	30.96	13.28	1.78	1.75	1.73	4
31.09	30.96	13.28	1.47	1.46	1.44	3
29.70	29.58	12.72	1.46	1.45	1.43	3
28.32	28.20	12.16	1.45	1.44	1.42	3
26.94	26.83	11.59	1.44	1.42	1.41	3
25.57	25.47	11.03	1.43	1.41	1.40	3
24.21	24.11	10.47	1.42	1.41	1.39	3
22.84	22.76	9.90	1.41	1.40	1.39	3
21.49	21.41	9.34	1.40	1.39	1.38	3
20.14	20.07	8.78	1.39	1.38	1.37	3
18.80	18.74	8.21	1.38	1.37	1.36	3
18.80	18.74	8.21	1.34	1.33	1.32	2
16.88	16.83	7.39	1.33	1.32	1.31	2
14.97	14.93	6.57	1.32	1.31	1.30	2
13.07	13.03	5.75	1.31	1.30	1.29	2
11.18	11.15	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.42	342.28	160.73	181.55	181.55	.00	6
58.89	379.91	165.35	214.56	214.56	.00	6
58.36	417.45	169.97	247.48	247.48	.00	6
57.83	454.93	174.59	280.34	280.34	.00	6
57.31	492.34	179.21	313.13	313.13	.00	6
56.78	529.69	183.83	345.86	345.86	.00	6
56.26	566.97	188.45	378.52	378.52	.00	6
55.74	604.18	193.07	411.11	411.11	.00	6
55.22	641.33	197.69	443.64	443.64	.00	6
55.22	641.33	197.69	443.64	443.64	.00	5
54.04	740.53	223.44	517.09	517.09	.00	5
52.88	838.82	249.19	589.63	589.63	.00	5
51.73	936.18	274.94	661.24	661.24	.00	5
50.60	1032.61	300.69	731.92	731.92	.00	5
49.48	1128.12	326.44	801.68	801.68	.00	5
48.38	1222.71	352.19	870.52	870.52	.00	5
48.38	1222.71	352.19	870.52	870.52	.00	4

46.40	1422.06	426.67	995.39	994.01	1.38	4
44.43	1620.91	503.91	1117.01	1117.01	.00	4
42.47	1819.10	564.62	1254.48	1239.34	15.15	4
40.52	2016.57	625.82	1390.74	1360.94	29.81	4
38.58	2213.29	687.90	1525.39	1481.81	43.59	4
36.65	2409.27	751.36	1657.91	1601.93	55.98	4
34.74	2604.48	817.38	1787.10	1721.27	65.82	4
32.84	2798.88	887.14	1911.74	1839.81	71.92	4
30.96	2992.41	963.18	2029.22	1957.49	71.74	4
30.96	2992.41	963.18	2029.23	1957.49	71.74	3
29.58	3140.42	1025.15	2115.27	2043.64	71.63	3
28.20	3288.06	1091.63	2196.43	2129.42	67.01	3
26.83	3435.33	1156.35	2278.99	2214.83	64.15	3
25.47	3582.24	1219.46	2362.78	2299.89	62.89	3
24.11	3728.80	1280.95	2447.85	2384.59	63.26	3
22.76	3875.02	1341.00	2534.03	2468.95	65.08	3
21.41	4020.91	1399.75	2621.16	2552.98	68.18	3
20.07	4166.47	1457.38	2709.08	2636.68	72.41	3
18.74	4311.70	1514.03	2797.67	2720.05	77.62	3
18.74	4311.70	1514.03	2797.67	2720.05	77.62	2
16.83	4516.90	1589.10	2927.80	2839.15	88.65	2
14.93	4721.62	1666.55	3055.07	2957.77	97.30	2
13.03	4925.86	1744.88	3180.99	3075.92	105.07	2
11.15	5129.62	1824.04	3305.58	3193.58	112.00	2
9.27	5332.89	1904.36	3428.53	3310.75	117.78	2
7.40	5535.66	1986.20	3549.46	3427.42	122.04	2
5.54	5737.93	2102.02	3635.91	3543.59	92.32	2
3.68	5939.69	2221.48	3718.21	3659.26	58.95	2
1.84	6140.98	2337.47	3803.51	3774.45	29.06	2
.00	6341.80	2450.37	3891.43	3889.17	2.26	2

Time = 4320. Degree of Consolidation = 86.%

Total Settlement = 1.167

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 4320. = 1.161

Settlement caused by Secondary Compression at time 4320. = .006

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.00	2.91	1.52
2.25	2.17	1.14
1.50	1.45	.76
.75	.72	.38
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
2.91	.00	.00
2.17	86.17	40.18

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
45.99	45.99	.00	1

1.45	171.71	80.36	91.34	91.34	.00	1
.72	257.05	120.55	136.50	136.50	.00	1
.00	342.28	160.73	181.55	181.55	.00	1

Time = 4320. Degree of Consolidation = 100.%

Total Settlement = .091

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 4320. = .091

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .34

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.39	21.42	6.50	6.01	6.01	6
60.02	58.86	21.35	6.49	5.99	6.00	6
59.45	58.34	21.27	6.47	5.98	5.99	6
58.89	57.81	21.20	6.46	5.96	5.97	6
58.33	57.28	21.12	6.44	5.95	5.96	6
57.76	56.76	21.05	6.43	5.93	5.94	6
57.20	56.24	20.97	6.42	5.92	5.93	6
56.64	55.71	20.90	6.40	5.91	5.92	6
56.08	55.19	20.82	6.39	5.89	5.90	6
56.08	55.19	20.82	4.51	4.11	4.11	5
54.82	54.02	20.59	4.44	4.05	4.05	5
53.56	52.85	20.36	4.38	3.98	3.98	5
52.32	51.71	20.12	4.32	3.92	3.92	5
51.10	50.57	19.89	4.25	3.85	3.85	5
49.88	49.46	19.66	4.19	3.79	3.79	5
48.69	48.35	19.43	4.13	3.73	3.73	5
48.69	48.35	19.43	1.93	1.90	1.90	4
46.69	46.37	18.75	1.92	1.89	1.89	4
44.70	44.40	18.06	1.91	1.88	1.88	4
42.72	42.44	17.38	1.89	1.86	1.86	4
40.75	40.49	16.70	1.88	1.84	1.84	4
38.79	38.56	16.01	1.86	1.83	1.82	4
36.85	36.63	15.33	1.84	1.81	1.79	4
34.91	34.72	14.65	1.82	1.79	1.77	4
33.00	32.82	13.97	1.80	1.77	1.75	4
31.09	30.94	13.28	1.78	1.75	1.73	4
31.09	30.94	13.28	1.47	1.45	1.44	3
29.70	29.56	12.72	1.46	1.44	1.43	3
28.32	28.19	12.16	1.45	1.43	1.42	3
26.94	26.82	11.59	1.44	1.42	1.41	3
25.57	25.46	11.03	1.43	1.41	1.40	3
24.21	24.10	10.47	1.42	1.40	1.39	3
22.84	22.75	9.90	1.41	1.39	1.39	3
21.49	21.40	9.34	1.40	1.38	1.38	3
20.14	20.06	8.78	1.39	1.37	1.37	3

18.80	18.73	8.21	1.38	1.37	1.36	3
18.80	18.73	8.21	1.34	1.33	1.32	2
16.88	16.82	7.39	1.33	1.32	1.31	2
14.97	14.92	6.57	1.32	1.31	1.30	2
13.07	13.03	5.75	1.31	1.30	1.29	2
11.18	11.14	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.39	342.28	160.73	181.55	181.55	.00	6
58.86	379.91	165.35	214.56	214.56	.00	6
58.34	417.45	169.97	247.48	247.48	.00	6
57.81	454.93	174.59	280.34	280.34	.00	6
57.28	492.34	179.21	313.13	313.13	.00	6
56.76	529.69	183.83	345.86	345.86	.00	6
56.24	566.97	188.45	378.52	378.52	.00	6
55.71	604.18	193.07	411.11	411.11	.00	6
55.19	641.33	197.69	443.64	443.64	.00	6
55.19	641.33	197.69	443.64	443.64	.00	5
54.02	740.53	223.44	517.09	517.09	.00	5
52.85	838.82	249.19	589.63	589.63	.00	5
51.71	936.18	274.94	661.24	661.24	.00	5
50.57	1032.61	300.69	731.92	731.92	.00	5
49.46	1128.12	326.44	801.68	801.68	.00	5
48.35	1222.71	352.19	870.52	870.52	.00	5
48.35	1222.71	352.19	870.52	870.52	.00	4
46.37	1422.06	426.67	995.39	994.01	1.38	4
44.40	1620.92	503.91	1117.01	1117.01	.00	4
42.44	1819.10	565.76	1253.33	1239.33	14.00	4
40.49	2016.54	628.21	1388.33	1360.91	27.41	4
38.56	2213.23	691.67	1521.56	1481.74	39.82	4
36.63	2409.15	756.69	1652.46	1601.81	50.65	4
34.72	2604.29	824.34	1779.95	1721.08	58.87	4
32.82	2798.59	896.11	1902.48	1839.53	62.96	4
30.94	2992.00	974.23	2017.77	1957.08	60.69	4
30.94	2992.00	974.23	2017.77	1957.08	60.69	3
29.56	3139.95	1038.28	2101.67	2043.17	58.50	3
28.19	3287.51	1104.86	2182.65	2128.87	53.78	3
26.82	3434.71	1169.47	2265.24	2214.21	51.03	3
25.46	3581.55	1232.31	2349.23	2299.19	50.04	3
24.10	3728.04	1293.57	2434.47	2383.82	50.65	3
22.75	3874.18	1353.40	2520.78	2468.11	52.67	3
21.40	4020.00	1411.99	2608.01	2552.07	55.95	3
20.06	4165.49	1469.47	2696.02	2635.70	60.32	3
18.73	4310.66	1526.00	2784.65	2719.01	65.64	3
18.73	4310.66	1526.00	2784.66	2719.01	65.65	2
16.82	4515.78	1600.54	2915.24	2838.03	77.20	2
14.92	4720.43	1677.15	3043.28	2956.59	86.69	2
13.03	4924.62	1754.33	3170.29	3074.67	95.62	2
11.14	5128.32	1832.32	3296.00	3192.28	103.72	2
9.27	5331.54	1911.43	3420.11	3309.40	110.71	2
7.40	5534.27	1992.03	3542.24	3426.03	116.21	2
5.54	5736.51	2108.65	3627.86	3542.17	85.69	2
3.68	5938.25	2225.85	3712.40	3657.82	54.58	2
1.84	6139.52	2339.70	3799.82	3772.99	26.83	2

.00	6340.34	2450.54	3889.79	3887.71	2.09	2

Time = 5040. Degree of Consolidation = 88.%

Total Settlement = 1.191

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 5040. = 1.185

Settlement caused by Secondary Compression at time 5040. = .006

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.00	2.91	1.52
2.25	2.17	1.14
1.50	1.45	.76
.75	.72	.38
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
2.91	.00	.00
2.17	86.17	40.18
1.45	171.71	80.36
.72	257.05	120.55
.00	342.28	160.73

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
45.99	45.99	.00	1
91.34	91.34	.00	1
136.50	136.50	.00	1
181.55	181.55	.00	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .091

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 5040. = .091

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .32

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
60.58	59.38	21.42

***** Void Ratios *****

Einitial	E	Eeop	Material
6.50	6.01	6.01	6

60.02	58.85	21.35	6.49	5.99	6.00	6
59.45	58.33	21.27	6.47	5.98	5.99	6
58.89	57.80	21.20	6.46	5.96	5.97	6
58.33	57.27	21.12	6.44	5.95	5.96	6
57.76	56.75	21.05	6.43	5.93	5.94	6
57.20	56.23	20.97	6.42	5.92	5.93	6
56.64	55.70	20.90	6.40	5.91	5.92	6
56.08	55.18	20.82	6.39	5.89	5.90	6
56.08	55.18	20.82	4.51	4.11	4.11	5
54.82	54.00	20.59	4.44	4.05	4.05	5
53.56	52.84	20.36	4.38	3.98	3.98	5
52.32	51.69	20.12	4.32	3.92	3.92	5
51.10	50.56	19.89	4.25	3.85	3.85	5
49.88	49.44	19.66	4.19	3.79	3.79	5
48.69	48.34	19.43	4.13	3.73	3.73	5
48.69	48.34	19.43	1.93	1.90	1.90	4
46.69	46.36	18.75	1.92	1.89	1.89	4
44.70	44.39	18.06	1.91	1.88	1.88	4
42.72	42.43	17.38	1.89	1.86	1.86	4
40.75	40.48	16.70	1.88	1.84	1.84	4
38.79	38.55	16.01	1.86	1.83	1.82	4
36.85	36.62	15.33	1.84	1.81	1.79	4
34.91	34.71	14.65	1.82	1.79	1.77	4
33.00	32.81	13.97	1.80	1.77	1.75	4
31.09	30.93	13.28	1.78	1.75	1.73	4
31.09	30.93	13.28	1.47	1.45	1.44	3
29.70	29.55	12.72	1.46	1.44	1.43	3
28.32	28.18	12.16	1.45	1.43	1.42	3
26.94	26.81	11.59	1.44	1.42	1.41	3
25.57	25.45	11.03	1.43	1.41	1.40	3
24.21	24.09	10.47	1.42	1.40	1.39	3
22.84	22.74	9.90	1.41	1.39	1.39	3
21.49	21.40	9.34	1.40	1.38	1.38	3
20.14	20.06	8.78	1.39	1.37	1.37	3
18.80	18.73	8.21	1.38	1.36	1.36	3
18.80	18.73	8.21	1.34	1.33	1.32	2
16.88	16.82	7.39	1.33	1.32	1.31	2
14.97	14.92	6.57	1.32	1.31	1.30	2
13.07	13.03	5.75	1.31	1.30	1.29	2
11.18	11.14	4.93	1.30	1.29	1.28	2
9.30	9.27	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.38	342.28	160.73	181.55	181.55	.00	6
58.85	379.91	165.35	214.56	214.56	.00	6
58.33	417.45	169.97	247.48	247.48	.00	6
57.80	454.93	174.59	280.34	280.34	.00	6
57.27	492.34	179.21	313.13	313.13	.00	6
56.75	529.69	183.83	345.86	345.86	.00	6
56.23	566.97	188.45	378.52	378.52	.00	6
55.70	604.18	193.07	411.11	411.11	.00	6
55.18	641.33	197.69	443.64	443.64	.00	6
55.18	641.33	197.69	443.64	443.64	.00	5
54.00	740.53	223.44	517.09	517.09	.00	5
52.84	838.82	249.19	589.63	589.63	.00	5

51.69	936.18	274.94	661.24	661.24	.00	5
50.56	1032.61	300.69	731.92	731.92	.00	5
49.44	1128.12	326.44	801.68	801.68	.00	5
48.34	1222.71	352.19	870.52	870.52	.00	5
48.34	1222.71	352.19	870.52	870.52	.00	4
46.36	1422.06	426.67	995.39	994.01	1.38	4
44.39	1620.92	503.91	1117.01	1117.01	.00	4
42.43	1819.10	566.31	1252.78	1239.33	13.45	4
40.48	2016.53	629.36	1387.17	1360.90	26.27	4
38.55	2213.20	693.48	1519.72	1481.71	38.01	4
36.62	2409.10	759.26	1649.84	1601.75	48.08	4
34.71	2604.20	827.54	1776.66	1720.99	55.67	4
32.81	2798.46	900.05	1898.41	1839.39	59.02	4
30.93	2991.82	979.19	2012.63	1956.90	55.73	4
30.93	2991.82	979.19	2012.63	1956.90	55.73	3
29.55	3139.73	1044.15	2095.58	2042.95	52.63	3
28.18	3287.26	1110.76	2176.50	2128.62	47.88	3
26.81	3434.42	1175.41	2259.02	2213.92	45.09	3
25.45	3581.23	1238.30	2342.93	2298.87	44.06	3
24.09	3727.68	1299.61	2428.07	2383.47	44.60	3
22.74	3873.80	1359.52	2514.28	2467.72	46.55	3
21.40	4019.58	1418.19	2601.39	2551.65	49.75	3
20.06	4165.03	1475.76	2689.27	2635.24	54.03	3
18.73	4310.17	1532.41	2777.76	2718.52	59.24	3
18.73	4310.17	1532.41	2777.76	2718.52	59.24	2
16.82	4515.25	1607.46	2907.79	2837.50	70.29	2
14.92	4719.86	1683.40	3036.46	2956.01	80.45	2
13.03	4924.00	1759.89	3164.11	3074.06	90.05	2
11.14	5127.68	1837.19	3290.49	3191.63	98.85	2
9.27	5330.87	1915.59	3415.28	3308.73	106.55	2
7.40	5533.58	1995.45	3538.13	3425.34	112.79	2
5.54	5735.79	2112.53	3623.26	3541.46	81.80	2
3.68	5937.53	2228.42	3709.11	3657.09	52.02	2
1.84	6138.79	2341.00	3797.79	3772.26	25.53	2
.00	6339.60	2450.64	3888.96	3886.97	1.99	2

Time = 5475. Degree of Consolidation = 89.%

Total Settlement = 1.203

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 5475. = 1.196

Settlement caused by Secondary Compression at time 5475. = .006

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.17	1.14	.98	.92	.92	1
1.50	1.45	.76	.98	.91	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.90	.90	1

XI	Total Stresses	Effective Stresses	Total Pore Pressures	Static Pore Pressures	Excess Pore Pressures	Material
2.91	.00	.00	.00	.00	.00	1
2.17	86.17	40.18	45.99	45.99	.00	1
1.45	171.71	80.36	91.34	91.34	.00	1
.72	257.05	120.55	136.50	136.50	.00	1
.00	342.28	160.73	181.55	181.55	.00	1

Time = 5475. Degree of Consolidation = 100.%

Total Settlement = .091

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 5475. = .091

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .31

**********Current Conditions in Compressible Foundation**********

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.36	21.42	6.50	6.01	6.01	6
60.02	58.83	21.35	6.49	5.99	6.00	6
59.45	58.30	21.27	6.47	5.98	5.99	6
58.89	57.78	21.20	6.46	5.96	5.97	6
58.33	57.25	21.12	6.44	5.95	5.96	6
57.76	56.73	21.05	6.43	5.93	5.94	6
57.20	56.20	20.97	6.42	5.92	5.93	6
56.64	55.68	20.90	6.40	5.91	5.92	6
56.08	55.16	20.82	6.39	5.89	5.90	6
56.08	55.16	20.82	4.51	4.11	4.11	5
54.82	53.98	20.59	4.44	4.05	4.05	5
53.56	52.82	20.36	4.38	3.98	3.98	5
52.32	51.67	20.12	4.32	3.92	3.92	5
51.10	50.54	19.89	4.25	3.85	3.85	5
49.88	49.42	19.66	4.19	3.79	3.79	5
48.69	48.32	19.43	4.13	3.73	3.73	5
48.69	48.32	19.43	1.93	1.90	1.90	4
46.69	46.34	18.75	1.92	1.89	1.89	4
44.70	44.37	18.06	1.91	1.88	1.88	4
42.72	42.41	17.38	1.89	1.86	1.86	4
40.75	40.46	16.70	1.88	1.84	1.84	4
38.79	38.52	16.01	1.86	1.82	1.82	4
36.85	36.60	15.33	1.84	1.81	1.79	4
34.91	34.69	14.65	1.82	1.79	1.77	4
33.00	32.80	13.97	1.80	1.77	1.75	4
31.09	30.91	13.28	1.78	1.74	1.73	4
31.09	30.91	13.28	1.47	1.45	1.44	3
29.70	29.54	12.72	1.46	1.44	1.43	3
28.32	28.16	12.16	1.45	1.43	1.42	3
26.94	26.80	11.59	1.44	1.42	1.41	3

25.57	25.44	11.03	1.43	1.41	1.40	3
24.21	24.08	10.47	1.42	1.40	1.39	3
22.84	22.73	9.90	1.41	1.39	1.39	3
21.49	21.39	9.34	1.40	1.38	1.38	3
20.14	20.05	8.78	1.39	1.37	1.37	3
18.80	18.72	8.21	1.38	1.36	1.36	3
18.80	18.72	8.21	1.34	1.32	1.32	2
16.88	16.81	7.39	1.33	1.32	1.31	2
14.97	14.91	6.57	1.32	1.31	1.30	2
13.07	13.02	5.75	1.31	1.30	1.29	2
11.18	11.14	4.93	1.30	1.29	1.28	2
9.30	9.26	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.36	342.28	160.73	181.55	181.55	.00	6
58.83	379.91	165.35	214.56	214.56	.00	6
58.30	417.45	169.97	247.48	247.48	.00	6
57.78	454.93	174.59	280.34	280.34	.00	6
57.25	492.34	179.21	313.13	313.13	.00	6
56.73	529.69	183.83	345.86	345.86	.00	6
56.20	566.97	188.45	378.52	378.52	.00	6
55.68	604.18	193.07	411.11	411.11	.00	6
55.16	641.33	197.69	443.64	443.64	.00	6
55.16	641.33	197.69	443.64	443.64	.00	5
53.98	740.53	223.44	517.09	517.09	.00	5
52.82	838.82	249.19	589.63	589.63	.00	5
51.67	936.18	274.94	661.24	661.24	.00	5
50.54	1032.61	300.69	731.92	731.92	.00	5
49.42	1128.12	326.44	801.68	801.68	.00	5
48.32	1222.71	352.19	870.52	870.52	.00	5
48.32	1222.71	352.19	870.52	870.52	.00	4
46.34	1422.06	426.67	995.39	994.01	1.38	4
44.37	1620.92	503.91	1117.01	1117.01	.00	4
42.41	1819.09	567.31	1251.78	1239.32	12.46	4
40.46	2016.50	631.44	1385.06	1360.88	24.18	4
38.52	2213.14	696.78	1516.37	1481.66	34.71	4
36.60	2409.00	763.94	1645.05	1601.65	43.40	4
34.69	2604.03	833.86	1770.17	1720.82	49.34	4
32.80	2798.21	907.94	1890.26	1839.14	51.12	4
30.91	2991.46	989.26	2002.20	1956.54	45.66	4
30.91	2991.46	989.26	2002.20	1956.54	45.66	3
29.54	3139.30	1056.14	2083.17	2042.52	40.65	3
28.16	3286.77	1122.74	2164.03	2128.13	35.90	3
26.80	3433.86	1187.39	2246.48	2213.37	33.11	3
25.44	3580.60	1250.28	2330.32	2298.24	32.08	3
24.08	3726.99	1311.59	2415.40	2382.77	32.62	3
22.73	3873.04	1371.50	2501.54	2466.96	34.57	3
21.39	4018.75	1430.17	2588.58	2550.82	37.77	3
20.05	4164.14	1487.75	2676.39	2634.35	42.05	3
18.72	4309.20	1544.36	2764.84	2717.55	47.29	3
18.72	4309.20	1544.36	2764.84	2717.55	47.29	2
16.81	4514.21	1618.86	2895.35	2836.46	58.88	2
14.91	4718.76	1693.70	3025.06	2954.91	70.15	2
13.02	4922.84	1769.07	3153.77	3072.90	80.87	2
11.14	5126.46	1845.23	3281.23	3190.42	90.81	2

9.26	5329.61	1922.46	3407.15	3307.47	99.68	2
7.40	5532.28	2001.62	3530.66	3424.04	106.62	2
5.54	5734.46	2118.90	3615.56	3540.13	75.44	2
3.68	5936.17	2232.61	3703.56	3655.74	47.82	2
1.84	6137.43	2343.14	3794.29	3770.89	23.39	2
.00	6338.23	2450.81	3887.42	3885.60	1.82	2

Time = 6480. Degree of Consolidation = 91.%

Total Settlement = 1.225

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 6480. = 1.218

Settlement caused by Secondary Compression at time 6480. = .006

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.17	1.14	.98	.92	.92	1
1.50	1.45	.76	.98	.91	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.17	86.17	40.18	45.99	45.99	.00	1
1.45	171.71	80.36	91.34	91.34	.00	1
.72	257.05	120.55	136.50	136.50	.00	1
.00	342.28	160.73	181.55	181.55	.00	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .091

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 6480. = .091

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .28

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.34	21.42	6.50	6.01	6.01	6
60.02	58.81	21.35	6.49	5.99	6.00	6
59.45	58.29	21.27	6.47	5.98	5.99	6
58.89	57.76	21.20	6.46	5.96	5.97	6
58.33	57.23	21.12	6.44	5.95	5.96	6
57.76	56.71	21.05	6.43	5.93	5.94	6
57.20	56.19	20.97	6.42	5.92	5.93	6
56.64	55.66	20.90	6.40	5.91	5.92	6
56.08	55.14	20.82	6.39	5.89	5.90	6
56.08	55.14	20.82	4.51	4.11	4.11	5
54.82	53.97	20.59	4.44	4.05	4.05	5
53.56	52.80	20.36	4.38	3.98	3.98	5
52.32	51.66	20.12	4.32	3.92	3.92	5
51.10	50.52	19.89	4.25	3.85	3.85	5
49.88	49.41	19.66	4.19	3.79	3.79	5
48.69	48.30	19.43	4.13	3.73	3.73	5
48.69	48.30	19.43	1.93	1.90	1.90	4
46.69	46.32	18.75	1.92	1.89	1.89	4
44.70	44.35	18.06	1.91	1.88	1.88	4
42.72	42.39	17.38	1.89	1.86	1.86	4
40.75	40.44	16.70	1.88	1.84	1.84	4
38.79	38.51	16.01	1.86	1.82	1.82	4
36.85	36.59	15.33	1.84	1.81	1.79	4
34.91	34.68	14.65	1.82	1.79	1.77	4
33.00	32.78	13.97	1.80	1.76	1.75	4
31.09	30.90	13.28	1.78	1.74	1.73	4
31.09	30.90	13.28	1.47	1.45	1.44	3
29.70	29.52	12.72	1.46	1.44	1.43	3
28.32	28.15	12.16	1.45	1.43	1.42	3
26.94	26.79	11.59	1.44	1.42	1.41	3
25.57	25.43	11.03	1.43	1.41	1.40	3
24.21	24.08	10.47	1.42	1.40	1.39	3
22.84	22.73	9.90	1.41	1.39	1.39	3
21.49	21.38	9.34	1.40	1.38	1.38	3
20.14	20.05	8.78	1.39	1.37	1.37	3
18.80	18.71	8.21	1.38	1.36	1.36	3
18.80	18.71	8.21	1.34	1.32	1.32	2
16.88	16.81	7.39	1.33	1.31	1.31	2
14.97	14.91	6.57	1.32	1.31	1.30	2
13.07	13.02	5.75	1.31	1.30	1.29	2
11.18	11.14	4.93	1.30	1.29	1.28	2
9.30	9.26	4.11	1.29	1.28	1.27	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.34	342.28	160.73	181.55	181.55	.00	6
58.81	379.91	165.35	214.56	214.56	.00	6
58.29	417.45	169.97	247.48	247.48	.00	6
57.76	454.93	174.59	280.34	280.34	.00	6
57.23	492.34	179.21	313.13	313.13	.00	6
56.71	529.69	183.83	345.86	345.86	.00	6
56.19	566.97	188.45	378.52	378.52	.00	6

55.66	604.18	193.07	411.11	411.11	.00	6
55.14	641.33	197.69	443.64	443.64	.00	6
55.14	641.33	197.69	443.64	443.64	.00	5
53.97	740.53	223.44	517.09	517.09	.00	5
52.80	838.82	249.19	589.63	589.63	.00	5
51.66	936.18	274.94	661.24	661.24	.00	5
50.52	1032.61	300.69	731.92	731.92	.00	5
49.41	1128.12	326.44	801.68	801.68	.00	5
48.30	1222.71	352.19	870.52	870.52	.00	5
48.30	1222.71	352.19	870.52	870.52	.00	4
46.32	1422.06	426.67	995.39	994.01	1.38	4
44.35	1620.92	503.91	1117.01	1117.01	.00	4
42.39	1819.09	567.97	1251.12	1239.32	11.80	4
40.44	2016.49	632.82	1383.67	1360.86	22.81	4
38.51	2213.11	698.95	1514.15	1481.62	32.53	4
36.59	2408.93	767.04	1641.89	1601.58	40.30	4
34.68	2603.92	838.06	1765.86	1720.71	45.14	4
32.78	2798.04	913.53	1884.51	1838.97	45.53	4
30.90	2991.21	996.71	1994.50	1956.29	38.21	4
30.90	2991.21	996.71	1994.50	1956.29	38.21	3
29.52	3139.01	1065.66	2073.34	2042.23	31.12	3
28.15	3286.42	1132.51	2153.90	2127.78	26.13	3
26.79	3433.46	1197.16	2236.29	2212.96	23.33	3
25.43	3580.14	1260.05	2320.08	2297.78	22.30	3
24.08	3726.47	1321.37	2405.10	2382.26	22.85	3
22.73	3872.47	1381.28	2491.19	2466.39	24.80	3
21.38	4018.12	1439.94	2578.18	2550.19	27.99	3
20.05	4163.46	1497.52	2665.94	2633.67	32.27	3
18.71	4308.47	1553.63	2754.84	2716.82	38.02	3
18.71	4308.47	1553.63	2754.84	2716.82	38.02	2
16.81	4513.42	1627.33	2886.09	2835.67	50.42	2
14.91	4717.92	1701.35	3016.57	2954.07	62.49	2
13.02	4921.96	1775.91	3146.05	3072.01	74.03	2
11.14	5125.54	1851.24	3274.30	3189.50	84.80	2
9.26	5328.65	1927.62	3401.03	3306.51	94.52	2
7.40	5531.29	2007.87	3523.42	3423.05	100.37	2
5.54	5733.45	2123.50	3609.96	3539.12	70.84	2
3.68	5935.15	2235.65	3699.50	3654.72	44.79	2
1.84	6136.39	2344.68	3791.71	3769.86	21.85	2
.00	6337.19	2450.92	3886.27	3884.56	1.71	2

Time = 7300. Degree of Consolidation = 92.%

Total Settlement = 1.241

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 7300. = 1.235

Settlement caused by Secondary Compression at time 7300. = .006

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
3.00	2.91	1.52	.98	.98	.98	1
2.25	2.17	1.14	.98	.92	.92	1

1.50	1.45	.76	.98	.91	.91	1
.75	.72	.38	.98	.91	.91	1
.00	.00	.00	.98	.90	.90	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
2.91	.00	.00	.00	.00	.00	1
2.17	86.17	40.18	45.99	45.99	.00	1
1.45	171.71	80.36	91.34	91.34	.00	1
.72	257.05	120.55	136.50	136.50	.00	1
.00	342.28	160.73	181.55	181.55	.00	1

Time = 7300. Degree of Consolidation = 100.%

Total Settlement = .091

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 7300. = .091

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .27

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.31	21.42	6.50	6.01	6.01	6
60.02	58.78	21.35	6.49	5.99	6.00	6
59.45	58.25	21.27	6.47	5.98	5.99	6
58.89	57.72	21.20	6.46	5.96	5.97	6
58.33	57.20	21.12	6.44	5.95	5.96	6
57.76	56.67	21.05	6.43	5.93	5.94	6
57.20	56.15	20.97	6.42	5.92	5.93	6
56.64	55.63	20.90	6.40	5.91	5.92	6
56.08	55.11	20.82	6.39	5.89	5.90	6
56.08	55.11	20.82	4.51	4.11	4.11	5
54.82	53.93	20.59	4.44	4.05	4.05	5
53.56	52.77	20.36	4.38	3.98	3.98	5
52.32	51.62	20.12	4.32	3.92	3.92	5
51.10	50.49	19.89	4.25	3.85	3.85	5
49.88	49.37	19.66	4.19	3.79	3.79	5
48.69	48.27	19.43	4.13	3.73	3.73	5
48.69	48.27	19.43	1.93	1.90	1.90	4
46.69	46.29	18.75	1.92	1.89	1.89	4
44.70	44.32	18.06	1.91	1.88	1.88	4
42.72	42.36	17.38	1.89	1.86	1.86	4
40.75	40.41	16.70	1.88	1.84	1.84	4
38.79	38.47	16.01	1.86	1.82	1.82	4
36.85	36.55	15.33	1.84	1.80	1.79	4
34.91	34.64	14.65	1.82	1.78	1.77	4
33.00	32.75	13.97	1.80	1.76	1.75	4

31.09	30.87	13.28	1.78	1.74	1.73	4
31.09	30.87	13.28	1.47	1.45	1.44	3
29.70	29.50	12.72	1.46	1.44	1.43	3
28.32	28.13	12.16	1.45	1.43	1.42	3
26.94	26.77	11.59	1.44	1.42	1.41	3
25.57	25.41	11.03	1.43	1.40	1.40	3
24.21	24.06	10.47	1.42	1.40	1.39	3
22.84	22.71	9.90	1.41	1.39	1.39	3
21.49	21.37	9.34	1.40	1.38	1.38	3
20.14	20.03	8.78	1.39	1.37	1.37	3
18.80	18.70	8.21	1.38	1.36	1.36	3
18.80	18.70	8.21	1.34	1.32	1.32	2
16.88	16.80	7.39	1.33	1.31	1.31	2
14.97	14.90	6.57	1.32	1.30	1.30	2
13.07	13.02	5.75	1.31	1.30	1.29	2
11.18	11.13	4.93	1.30	1.29	1.28	2
9.30	9.26	4.11	1.29	1.28	1.27	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.25	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.31	342.28	160.73	181.55	181.55	.00	6
58.78	379.91	165.35	214.56	214.56	.00	6
58.25	417.45	169.97	247.48	247.48	.00	6
57.72	454.93	174.59	280.34	280.34	.00	6
57.20	492.34	179.21	313.13	313.13	.00	6
56.67	529.69	183.83	345.86	345.86	.00	6
56.15	566.97	188.45	378.52	378.52	.00	6
55.63	604.18	193.07	411.11	411.11	.00	6
55.11	641.33	197.69	443.64	443.64	.00	6
55.11	641.33	197.69	443.64	443.64	.00	5
53.93	740.53	223.44	517.09	517.09	.00	5
52.77	838.82	249.19	589.63	589.63	.00	5
51.62	936.18	274.94	661.24	661.24	.00	5
50.49	1032.61	300.69	731.92	731.92	.00	5
49.37	1128.12	326.44	801.68	801.68	.00	5
48.27	1222.71	352.19	870.52	870.52	.00	5
48.27	1222.71	352.19	870.52	870.52	.00	4
46.29	1422.06	426.67	995.39	994.01	1.38	4
44.32	1620.92	503.91	1117.01	1117.01	.00	4
42.36	1819.08	569.41	1249.67	1239.31	10.36	4
40.41	2016.46	635.84	1380.62	1360.83	19.79	4
38.47	2213.03	703.74	1509.29	1481.54	27.74	4
36.55	2408.78	773.87	1634.91	1601.43	33.47	4
34.64	2603.67	847.35	1756.32	1720.47	35.85	4
32.75	2797.66	925.96	1871.70	1838.60	33.10	4
30.87	2990.67	1012.14	1978.53	1955.75	22.78	4
30.87	2990.67	1012.14	1978.53	1955.75	22.78	3
29.50	3138.37	1083.35	2055.02	2041.59	13.43	3
28.13	3285.68	1151.84	2133.84	2127.04	6.80	3
26.77	3432.60	1217.83	2214.78	2212.11	2.67	3
25.41	3579.17	1281.53	2297.64	2296.81	.83	3
24.06	3725.38	1343.12	2382.25	2381.16	1.09	3
22.71	3871.25	1403.03	2468.22	2465.18	3.04	3
21.37	4016.79	1461.70	2555.09	2548.85	6.23	3
20.03	4162.00	1518.87	2643.13	2632.21	10.93	3
18.70	4306.89	1574.57	2732.32	2715.24	17.08	3

18.70	4306.89	1574.57	2732.32	2715.24	17.08	2
16.80	4511.72	1646.44	2865.28	2833.97	31.31	2
14.90	4716.10	1718.63	2997.47	2952.26	45.21	2
13.02	4920.04	1791.33	3128.71	3070.10	58.61	2
11.13	5123.54	1864.77	3258.76	3187.49	71.27	2
9.26	5326.57	1939.22	3387.35	3304.43	82.92	2
7.39	5529.15	2021.92	3507.22	3420.91	86.31	2
5.53	5731.26	2133.84	3597.42	3536.92	60.49	2
3.68	5932.92	2242.47	3690.45	3652.48	37.96	2
1.84	6134.14	2348.15	3785.99	3767.61	18.38	2
.00	6334.93	2451.19	3883.74	3882.30	1.44	2

Time = 9125. Degree of Consolidation = 94.%

Total Settlement = 1.277

Settlement at End of Primary Consolidation = 1.353

Settlement caused by Primary Consolidation at time 9125. = 1.271

Settlement caused by Secondary Compression at time 9125. = .006

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
3.00	2.91	1.52
2.25	2.17	1.14
1.50	1.45	.76
.75	.72	.38
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.91	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
2.91	.00	.00
2.17	86.17	40.18
1.45	171.71	80.36
.72	257.05	120.55
.00	342.28	160.73

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
45.99	45.99	.00	1
91.34	91.34	.00	1
136.50	136.50	.00	1
181.55	181.55	.00	1

Time = 9125. Degree of Consolidation = 100.%

Total Settlement = .091

Settlement at End of Primary Consolidation = .091

Settlement caused by Primary Consolidation at time 9125. = .091

Settlement caused by Secondary Compression at time 9125. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .23

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou Dupont - 4ft Fill Height

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	4.0	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.111	1.106	.30000E-04	z = .05

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	5.85	6
60.02	60.02	21.35	6.49	6.49	5.84	6
59.45	59.45	21.27	6.47	6.47	5.82	6
58.89	58.89	21.20	6.46	6.46	5.81	6

58.33	58.33	21.12	6.44	6.44	5.80	6
57.76	57.76	21.05	6.43	6.43	5.78	6
57.20	57.20	20.97	6.42	6.42	5.77	6
56.64	56.64	20.90	6.40	6.40	5.76	6
56.08	56.08	20.82	6.39	6.39	5.74	6
56.08	56.08	20.82	4.51	4.51	3.98	5
54.82	54.82	20.59	4.44	4.44	3.91	5
53.56	53.56	20.36	4.38	4.38	3.85	5
52.32	52.32	20.12	4.32	4.32	3.79	5
51.10	51.10	19.89	4.25	4.25	3.72	5
49.88	49.88	19.66	4.19	4.19	3.66	5
48.69	48.69	19.43	4.13	4.13	3.59	5
48.69	48.69	19.43	1.93	1.93	1.90	4
46.69	46.69	18.75	1.92	1.92	1.88	4
44.70	44.70	18.06	1.91	1.91	1.86	4
42.72	42.72	17.38	1.89	1.89	1.84	4
40.75	40.75	16.70	1.88	1.88	1.82	4
38.79	38.79	16.01	1.86	1.86	1.80	4
36.85	36.85	15.33	1.84	1.84	1.78	4
34.91	34.91	14.65	1.82	1.82	1.76	4
33.00	33.00	13.97	1.80	1.80	1.74	4
31.09	31.09	13.28	1.78	1.78	1.71	4
31.09	31.09	13.28	1.47	1.47	1.44	3
29.70	29.70	12.72	1.46	1.46	1.43	3
28.32	28.32	12.16	1.45	1.45	1.42	3
26.94	26.94	11.59	1.44	1.44	1.41	3
25.57	25.57	11.03	1.43	1.43	1.40	3
24.21	24.21	10.47	1.42	1.42	1.39	3
22.84	22.84	9.90	1.41	1.41	1.38	3
21.49	21.49	9.34	1.40	1.40	1.37	3
20.14	20.14	8.78	1.39	1.39	1.36	3
18.80	18.80	8.21	1.38	1.38	1.35	3
18.80	18.80	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.43	3.29	1.28	1.28	1.26	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.25	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	463.90	.00	463.90	249.60	214.30	6
60.02	503.85	4.62	499.23	284.93	214.30	6
59.45	543.73	9.24	534.49	320.19	214.30	6
58.89	583.55	13.86	569.69	355.38	214.30	6
58.33	623.30	18.48	604.82	390.51	214.30	6
57.76	662.98	23.10	639.88	425.58	214.30	6
57.20	702.60	27.72	674.88	460.58	214.30	6
56.64	742.15	32.34	709.81	495.51	214.30	6
56.08	781.64	36.96	744.68	530.37	214.30	6
56.08	781.64	36.96	744.68	530.37	214.30	5
54.82	886.61	62.71	823.90	609.60	214.30	5
53.56	990.66	88.46	902.20	687.90	214.30	5
52.32	1093.79	114.21	979.58	765.27	214.30	5
51.10	1195.99	139.96	1056.03	841.72	214.30	5
49.88	1297.27	165.71	1131.56	917.25	214.30	5

48.69	1397.62	191.46	1206.16	991.86	214.30	5
48.69	1397.62	191.46	1206.16	991.86	214.30	4
46.69	1598.07	267.32	1330.74	1116.44	214.30	4
44.70	1798.01	343.18	1454.83	1240.52	214.30	4
42.72	1997.40	419.04	1578.36	1364.06	214.30	4
40.75	2196.35	494.90	1701.45	1487.14	214.30	4
38.79	2394.54	570.76	1823.78	1609.48	214.30	4
36.85	2591.84	646.62	1945.23	1730.92	214.30	4
34.91	2788.24	722.48	2065.76	1851.46	214.30	4
33.00	2983.73	798.34	2185.39	1971.09	214.30	4
31.09	3178.31	874.19	2304.12	2089.82	214.30	4
31.09	3178.31	874.19	2304.12	2089.82	214.30	3
29.70	3326.88	936.05	2390.83	2176.53	214.30	3
28.32	3475.05	997.91	2477.14	2262.84	214.30	3
26.94	3622.86	1059.77	2563.09	2348.79	214.30	3
25.57	3770.32	1121.63	2648.69	2434.39	214.30	3
24.21	3917.43	1183.49	2733.94	2519.64	214.30	3
22.84	4064.19	1245.35	2818.85	2604.54	214.30	3
21.49	4210.61	1307.21	2903.40	2689.10	214.30	3
20.14	4356.68	1369.06	2987.61	2773.31	214.30	3
18.80	4502.40	1430.92	3071.47	2857.17	214.30	3
18.80	4502.40	1430.92	3071.47	2857.17	214.30	2
16.88	4708.06	1517.02	3191.04	2976.74	214.30	2
14.97	4913.20	1603.12	3310.08	3095.78	214.30	2
13.07	5117.81	1689.22	3428.59	3214.29	214.30	2
11.18	5321.89	1775.31	3546.58	3332.27	214.30	2
9.30	5525.44	1861.41	3664.03	3449.73	214.30	2
7.43	5728.46	1947.51	3780.95	3566.65	214.30	2
5.56	5930.97	2033.61	3897.36	3683.06	214.30	2
3.70	6133.09	2119.71	4013.38	3799.08	214.30	2
1.85	6334.85	2205.80	4129.05	3914.74	214.30	2
.00	6536.27	2291.90	4244.36	4030.06	214.30	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	4.00	2.02	.98	.98	.98	1
3.00	3.00	1.52	.98	.98	.92	1
2.00	2.00	1.01	.98	.98	.91	1
1.00	1.00	.51	.98	.98	.90	1
.00	.00	.00	.98	.98	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

4.00	.00	.00	.00	.00	.00	1
3.00	115.98	.00	115.98	62.40	53.58	1
2.00	231.95	.00	231.95	124.80	107.15	1
1.00	347.93	.00	347.93	187.20	160.73	1
.00	463.90	.00	463.90	249.60	214.30	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.50	21.42	6.50	6.05	5.85	6
60.02	59.97	21.35	6.49	6.19	5.84	6
59.45	59.42	21.27	6.47	6.29	5.82	6
58.89	58.87	21.20	6.46	6.36	5.81	6
58.33	58.31	21.12	6.44	6.40	5.80	6
57.76	57.75	21.05	6.43	6.41	5.78	6
57.20	57.19	20.97	6.42	6.41	5.77	6
56.64	56.63	20.90	6.40	6.40	5.76	6
56.08	56.07	20.82	6.39	6.39	5.74	6
56.08	56.07	20.82	4.51	4.51	3.98	5
54.82	54.80	20.59	4.44	4.44	3.91	5
53.56	53.55	20.36	4.38	4.38	3.85	5
52.32	52.31	20.12	4.32	4.31	3.79	5
51.10	51.08	19.89	4.25	4.25	3.72	5
49.88	49.87	19.66	4.19	4.19	3.66	5
48.69	48.68	19.43	4.13	4.12	3.59	5
48.69	48.68	19.43	1.93	1.93	1.90	4
46.69	46.68	18.75	1.92	1.92	1.88	4
44.70	44.69	18.06	1.91	1.91	1.86	4
42.72	42.71	17.38	1.89	1.89	1.84	4
40.75	40.74	16.70	1.88	1.88	1.82	4
38.79	38.78	16.01	1.86	1.86	1.80	4
36.85	36.84	15.33	1.84	1.84	1.78	4
34.91	34.91	14.65	1.82	1.82	1.76	4
33.00	32.99	13.97	1.80	1.80	1.74	4
31.09	31.09	13.28	1.78	1.78	1.71	4
31.09	31.09	13.28	1.47	1.47	1.44	3
29.70	29.70	12.72	1.46	1.46	1.43	3
28.32	28.31	12.16	1.45	1.45	1.42	3
26.94	26.94	11.59	1.44	1.44	1.41	3
25.57	25.56	11.03	1.43	1.43	1.40	3
24.21	24.20	10.47	1.42	1.42	1.39	3
22.84	22.84	9.90	1.41	1.41	1.38	3
21.49	21.48	9.34	1.40	1.40	1.37	3
20.14	20.13	8.78	1.39	1.39	1.36	3
18.80	18.79	8.21	1.38	1.38	1.35	3
18.80	18.79	8.21	1.34	1.34	1.31	2

16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.50	456.28	148.49	307.80	241.98	65.82	6
59.97	494.48	103.43	391.05	275.56	115.49	6
59.42	533.25	68.76	464.49	309.71	154.79	6
58.87	572.43	46.15	526.27	344.26	182.01	6
58.31	611.85	34.29	577.56	379.06	198.50	6
57.75	651.37	30.15	621.22	413.97	207.26	6
57.19	690.93	30.69	660.23	448.90	211.33	6
56.63	730.45	33.73	696.72	483.80	212.91	6
56.07	769.92	38.01	731.91	518.65	213.25	6
56.07	769.92	38.01	731.91	518.65	213.25	5
54.80	874.86	63.57	811.28	597.84	213.44	5
53.55	978.88	89.33	889.55	676.11	213.44	5
52.31	1081.97	115.11	966.86	753.46	213.40	5
51.08	1184.14	140.88	1043.26	829.88	213.38	5
49.87	1285.39	166.62	1118.77	905.37	213.40	5
48.68	1385.71	192.28	1193.43	979.94	213.49	5
48.68	1385.71	192.28	1193.43	979.94	213.49	4
46.68	1586.15	267.32	1318.83	1104.52	214.30	4
44.69	1786.07	343.18	1442.89	1228.59	214.30	4
42.71	1985.48	421.72	1563.76	1352.13	211.62	4
40.74	2184.31	507.72	1676.59	1475.11	201.48	4
38.78	2382.43	573.59	1808.84	1597.37	211.47	4
36.84	2579.72	646.64	1933.08	1718.80	214.28	4
34.91	2776.12	722.48	2053.64	1839.34	214.30	4
32.99	2971.61	798.34	2173.27	1958.97	214.30	4
31.09	3166.19	874.19	2292.00	2077.70	214.30	4
31.09	3166.19	874.20	2292.00	2077.70	214.30	3
29.70	3314.76	936.05	2378.71	2164.41	214.30	3
28.31	3462.94	997.91	2465.02	2250.72	214.30	3
26.94	3610.74	1060.97	2549.77	2336.67	213.10	3
25.56	3758.19	1123.17	2635.02	2422.26	212.76	3
24.20	3905.29	1185.00	2720.29	2507.50	212.79	3
22.84	4052.05	1246.76	2805.29	2592.40	212.89	3
21.48	4198.45	1308.56	2889.89	2676.95	212.94	3
20.13	4344.51	1370.28	2974.24	2761.15	213.09	3
18.79	4490.23	1431.81	3058.42	2845.00	213.42	3
18.79	4490.23	1431.81	3058.42	2845.00	213.42	2
16.87	4695.89	1517.27	3178.62	2964.57	214.05	2
14.97	4901.03	1603.12	3297.91	3083.61	214.30	2
13.07	5105.64	1689.22	3416.42	3202.12	214.30	2
11.18	5309.72	1775.31	3534.40	3320.10	214.30	2
9.29	5513.27	1861.41	3651.86	3437.56	214.30	2
7.42	5716.29	1947.51	3768.78	3554.47	214.30	2
5.55	5918.81	2033.61	3885.20	3670.90	214.30	2
3.70	6120.91	2122.13	3998.78	3786.90	211.88	2
1.84	6322.65	2230.91	4091.74	3902.54	189.19	2
.00	6523.68	2489.21	4034.47	4017.47	17.00	2

Time = 30. Degree of Consolidation = 4.%

Total Settlement = .080

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 30. = .080

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.88	2.02	.98	.98	.98	1
3.00	2.90	1.52	.98	.92	.92	1
2.00	1.93	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.91	.90	1
.00	.00	.00	.98	.91	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.88	.00	.00	.00	.00	.00	1
2.90	114.88	42.51	72.36	61.30	11.07	1
1.93	228.88	88.02	140.86	121.73	19.13	1
.96	342.63	125.29	217.34	181.91	35.44	1
.00	456.28	148.49	307.80	241.98	65.82	1

Time = 30. Degree of Consolidation = 94.%

Total Settlement = .122

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 30. = .122

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 2.40

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.46	21.42	6.50	6.00	5.85	6
60.02	59.92	21.35	6.49	6.11	5.84	6
59.45	59.38	21.27	6.47	6.20	5.82	6
58.89	58.84	21.20	6.46	6.27	5.81	6
58.33	58.29	21.12	6.44	6.32	5.80	6

57.76	57.73	21.05	6.43	6.35	5.78	6
57.20	57.17	20.97	6.42	6.37	5.77	6
56.64	56.62	20.90	6.40	6.38	5.76	6
56.08	56.06	20.82	6.39	6.37	5.74	6
56.08	56.06	20.82	4.51	4.50	3.98	5
54.82	54.79	20.59	4.44	4.44	3.91	5
53.56	53.54	20.36	4.38	4.37	3.85	5
52.32	52.30	20.12	4.32	4.31	3.79	5
51.10	51.08	19.89	4.25	4.25	3.72	5
49.88	49.87	19.66	4.19	4.18	3.66	5
48.69	48.67	19.43	4.13	4.12	3.59	5
48.69	48.67	19.43	1.93	1.93	1.90	4
46.69	46.68	18.75	1.92	1.92	1.88	4
44.70	44.69	18.06	1.91	1.91	1.86	4
42.72	42.71	17.38	1.89	1.89	1.84	4
40.75	40.74	16.70	1.88	1.88	1.82	4
38.79	38.78	16.01	1.86	1.86	1.80	4
36.85	36.83	15.33	1.84	1.84	1.78	4
34.91	34.90	14.65	1.82	1.82	1.76	4
33.00	32.99	13.97	1.80	1.80	1.74	4
31.09	31.08	13.28	1.78	1.78	1.71	4
31.09	31.08	13.28	1.47	1.47	1.44	3
29.70	29.69	12.72	1.46	1.46	1.43	3
28.32	28.31	12.16	1.45	1.45	1.42	3
26.94	26.93	11.59	1.44	1.44	1.41	3
25.57	25.56	11.03	1.43	1.43	1.40	3
24.21	24.20	10.47	1.42	1.42	1.39	3
22.84	22.83	9.90	1.41	1.41	1.38	3
21.49	21.48	9.34	1.40	1.40	1.37	3
20.14	20.13	8.78	1.39	1.39	1.36	3
18.80	18.79	8.21	1.38	1.38	1.35	3
18.80	18.79	8.21	1.34	1.34	1.31	2
16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.46	456.19	164.37	291.82	241.88	49.93	6
59.92	494.08	129.71	364.37	275.15	89.22	6
59.38	532.43	99.81	432.63	308.89	123.74	6
58.84	571.17	76.06	495.10	343.00	152.10	6
58.29	610.19	58.98	551.21	377.41	173.80	6
57.73	649.42	48.17	601.25	412.01	189.24	6
57.17	688.76	42.61	646.15	446.73	199.41	6
56.62	728.15	41.04	687.11	481.50	205.61	6
56.06	767.54	42.19	725.35	516.27	209.07	6
56.06	767.54	42.19	725.35	516.27	209.07	5
54.79	872.36	65.92	806.45	595.35	211.10	5
53.54	976.32	90.79	885.53	673.55	211.98	5
52.30	1079.37	116.20	963.17	750.85	212.32	5
51.08	1181.50	141.81	1039.69	827.23	212.46	5
49.87	1282.71	167.45	1115.26	902.70	212.56	5
48.67	1383.01	193.03	1189.98	977.24	212.74	5

48.67	1383.01	193.03	1189.98	977.24	212.74	4
46.68	1583.44	267.32	1316.12	1101.82	214.30	4
44.69	1783.37	343.57	1439.80	1225.89	213.91	4
42.71	1982.76	426.41	1556.35	1349.41	206.94	4
40.74	2181.54	512.81	1668.73	1472.34	196.39	4
38.78	2379.61	577.04	1802.57	1594.55	208.02	4
36.83	2576.87	647.56	1929.31	1715.95	213.36	4
34.90	2773.27	722.48	2050.79	1836.49	214.30	4
32.99	2968.76	798.34	2170.42	1956.12	214.30	4
31.08	3163.34	874.19	2289.15	2074.84	214.30	4
31.08	3163.34	874.20	2289.15	2074.84	214.30	3
29.69	3311.91	936.05	2375.86	2161.55	214.30	3
28.31	3460.08	997.91	2462.17	2247.87	214.30	3
26.93	3607.88	1061.83	2546.06	2333.81	212.25	3
25.56	3755.33	1124.46	2630.87	2419.40	211.47	3
24.20	3902.42	1186.41	2716.01	2504.63	211.38	3
22.83	4049.17	1248.17	2801.00	2589.52	211.48	3
21.48	4195.57	1309.82	2885.75	2674.06	211.69	3
20.13	4341.62	1371.38	2970.24	2758.26	211.99	3
18.79	4487.33	1432.63	3054.70	2842.10	212.59	3
18.79	4487.33	1432.63	3054.70	2842.10	212.59	2
16.87	4692.99	1517.54	3175.45	2961.67	213.78	2
14.96	4898.13	1603.25	3294.88	3080.71	214.17	2
13.06	5102.74	1689.22	3413.52	3199.22	214.30	2
11.17	5306.82	1775.31	3531.50	3317.20	214.30	2
9.29	5510.37	1861.41	3648.96	3434.66	214.30	2
7.42	5713.39	1947.51	3765.88	3551.57	214.30	2
5.55	5915.90	2033.61	3882.29	3667.99	214.30	2
3.69	6118.00	2127.91	3990.09	3783.99	206.10	2
1.84	6319.67	2255.21	4064.47	3899.57	164.90	2
.00	6520.62	2493.00	4027.63	4014.42	13.21	2

Time = 60. Degree of Consolidation = 7.%

Total Settlement = .127

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 60. = .127

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.00	3.88	2.02
3.00	2.89	1.52
2.00	1.93	1.01
1.00	.96	.51
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.91	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.88	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

2.89	114.87	43.09	71.79	61.30	10.49	1
1.93	228.86	92.08	136.78	121.71	15.07	1
.96	342.58	137.57	205.01	181.85	23.16	1
.00	456.19	164.37	291.82	241.88	49.93	1

Time = 60. Degree of Consolidation = 95.%

Total Settlement = .124

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 60. = .124

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 2.35

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.38	21.42	6.50	5.96	5.85	6
60.02	59.85	21.35	6.49	6.04	5.84	6
59.45	59.32	21.27	6.47	6.11	5.82	6
58.89	58.78	21.20	6.46	6.17	5.81	6
58.33	58.23	21.12	6.44	6.22	5.80	6
57.76	57.69	21.05	6.43	6.26	5.78	6
57.20	57.14	20.97	6.42	6.30	5.77	6
56.64	56.59	20.90	6.40	6.32	5.76	6
56.08	56.03	20.82	6.39	6.33	5.74	6
56.08	56.03	20.82	4.51	4.46	3.98	5
54.82	54.77	20.59	4.44	4.41	3.91	5
53.56	53.52	20.36	4.38	4.36	3.85	5
52.32	52.29	20.12	4.32	4.30	3.79	5
51.10	51.06	19.89	4.25	4.24	3.72	5
49.88	49.86	19.66	4.19	4.18	3.66	5
48.69	48.66	19.43	4.13	4.12	3.59	5
48.69	48.66	19.43	1.93	1.93	1.90	4
46.69	46.67	18.75	1.92	1.92	1.88	4
44.70	44.68	18.06	1.91	1.90	1.86	4
42.72	42.70	17.38	1.89	1.89	1.84	4
40.75	40.73	16.70	1.88	1.87	1.82	4
38.79	38.77	16.01	1.86	1.86	1.80	4
36.85	36.83	15.33	1.84	1.84	1.78	4
34.91	34.90	14.65	1.82	1.82	1.76	4
33.00	32.98	13.97	1.80	1.80	1.74	4
31.09	31.08	13.28	1.78	1.78	1.71	4
31.09	31.08	13.28	1.47	1.47	1.44	3
29.70	29.69	12.72	1.46	1.46	1.43	3
28.32	28.31	12.16	1.45	1.45	1.42	3
26.94	26.93	11.59	1.44	1.44	1.41	3
25.57	25.56	11.03	1.43	1.43	1.40	3
24.21	24.19	10.47	1.42	1.42	1.39	3
22.84	22.83	9.90	1.41	1.41	1.38	3
21.49	21.48	9.34	1.40	1.40	1.37	3
20.14	20.13	8.78	1.39	1.39	1.36	3
18.80	18.78	8.21	1.38	1.38	1.35	3

18.80	18.78	8.21	1.34	1.34	1.31	2
16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.38	456.10	179.19	276.91	241.80	35.12	6
59.85	493.71	153.73	339.98	274.79	65.19	6
59.32	531.67	130.31	401.36	308.13	93.23	6
58.78	569.95	109.64	460.31	341.78	118.53	6
58.23	608.50	92.20	516.29	375.71	140.58	6
57.69	647.27	78.22	569.04	409.86	159.18	6
57.14	686.21	67.63	618.58	444.19	174.40	6
56.59	725.29	60.10	665.19	478.64	186.55	6
56.03	764.45	55.11	709.34	513.18	196.15	6
56.03	764.45	55.11	709.34	513.18	196.15	5
54.77	868.88	75.18	793.70	591.87	201.84	5
53.52	972.55	97.22	875.34	669.79	205.55	5
52.29	1075.41	120.67	954.75	746.90	207.85	5
51.06	1177.41	145.06	1032.35	823.14	209.21	5
49.86	1278.52	170.07	1108.45	898.50	209.95	5
48.66	1378.72	195.51	1183.22	972.96	210.26	5
48.66	1378.72	195.51	1183.22	972.96	210.26	4
46.67	1579.15	268.56	1310.59	1097.52	213.07	4
44.68	1779.06	347.09	1431.97	1221.58	210.40	4
42.70	1978.41	433.97	1544.44	1345.07	199.38	4
40.73	2177.13	518.96	1658.17	1467.93	190.24	4
38.77	2375.13	582.38	1792.75	1590.07	202.69	4
36.83	2572.34	650.36	1921.98	1711.42	210.56	4
34.90	2768.72	722.58	2046.14	1831.94	214.20	4
32.98	2964.21	798.34	2165.87	1951.57	214.30	4
31.08	3158.79	874.19	2284.60	2070.29	214.30	4
31.08	3158.79	874.20	2284.60	2070.29	214.30	3
29.69	3307.36	936.05	2371.31	2157.00	214.30	3
28.31	3455.54	997.91	2457.62	2243.32	214.30	3
26.93	3603.33	1063.07	2540.26	2329.26	211.00	3
25.56	3750.77	1126.60	2624.17	2414.83	209.33	3
24.19	3897.85	1188.99	2708.86	2500.06	208.80	3
22.83	4044.58	1250.73	2793.85	2584.93	208.92	3
21.48	4190.97	1312.24	2878.73	2669.46	209.27	3
20.13	4337.01	1373.39	2963.61	2753.64	209.97	3
18.78	4482.70	1434.24	3048.46	2837.48	210.98	3
18.78	4482.70	1434.24	3048.46	2837.48	210.98	2
16.87	4688.36	1518.37	3169.99	2957.04	212.96	2
14.96	4893.49	1603.66	3289.83	3076.07	213.76	2
13.06	5098.10	1689.23	3408.87	3194.58	214.29	2
11.17	5302.18	1775.31	3526.86	3312.56	214.30	2
9.29	5505.74	1861.41	3644.33	3430.02	214.30	2
7.41	5708.75	1947.51	3761.24	3546.94	214.30	2
5.55	5911.27	2033.61	3877.66	3663.35	214.30	2
3.69	6113.34	2142.72	3970.63	3779.33	191.29	2
1.84	6314.91	2287.66	4027.25	3894.80	132.45	2
.00	6515.77	2495.68	4020.08	4009.56	10.53	2

Time = 120. Degree of Consolidation = 11.%

Total Settlement = .203

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 120. = .203

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.91	.90	1
.00	.00	.00	.98	.90	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.87	43.58	71.29	61.29	10.00	1
1.92	228.84	95.60	133.24	121.69	11.55	1
.96	342.53	148.57	193.96	181.81	12.15	1
.00	456.10	179.19	276.91	241.80	35.12	1

Time = 120. Degree of Consolidation = 97.%

Total Settlement = .125

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 120. = .125

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.27

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.26	21.42	6.50	5.94	5.85	6
60.02	59.74	21.35	6.49	5.99	5.84	6

59.45	59.21	21.27	6.47	6.04	5.82	6
58.89	58.67	21.20	6.46	6.08	5.81	6
58.33	58.14	21.12	6.44	6.13	5.80	6
57.76	57.60	21.05	6.43	6.17	5.78	6
57.20	57.05	20.97	6.42	6.20	5.77	6
56.64	56.51	20.90	6.40	6.24	5.76	6
56.08	55.96	20.82	6.39	6.26	5.74	6
56.08	55.96	20.82	4.51	4.41	3.98	5
54.82	54.71	20.59	4.44	4.36	3.91	5
53.56	53.47	20.36	4.38	4.31	3.85	5
52.32	52.25	20.12	4.32	4.26	3.79	5
51.10	51.03	19.89	4.25	4.21	3.72	5
49.88	49.83	19.66	4.19	4.15	3.66	5
48.69	48.65	19.43	4.13	4.08	3.59	5
48.69	48.65	19.43	1.93	1.93	1.90	4
46.69	46.65	18.75	1.92	1.92	1.88	4
44.70	44.67	18.06	1.91	1.90	1.86	4
42.72	42.69	17.38	1.89	1.89	1.84	4
40.75	40.72	16.70	1.88	1.87	1.82	4
38.79	38.76	16.01	1.86	1.85	1.80	4
36.85	36.82	15.33	1.84	1.84	1.78	4
34.91	34.89	14.65	1.82	1.82	1.76	4
33.00	32.97	13.97	1.80	1.80	1.74	4
31.09	31.07	13.28	1.78	1.78	1.71	4
31.09	31.07	13.28	1.47	1.47	1.44	3
29.70	29.68	12.72	1.46	1.46	1.43	3
28.32	28.30	12.16	1.45	1.45	1.42	3
26.94	26.92	11.59	1.44	1.44	1.41	3
25.57	25.55	11.03	1.43	1.43	1.40	3
24.21	24.18	10.47	1.42	1.42	1.39	3
22.84	22.82	9.90	1.41	1.41	1.38	3
21.49	21.47	9.34	1.40	1.40	1.37	3
20.14	20.12	8.78	1.39	1.39	1.36	3
18.80	18.78	8.21	1.38	1.38	1.35	3
18.80	18.78	8.21	1.34	1.34	1.31	2
16.88	16.86	7.39	1.33	1.33	1.30	2
14.97	14.95	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.28	4.11	1.29	1.29	1.26	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.26	455.81	186.08	269.74	241.51	28.23	6
59.74	493.26	169.67	323.59	274.34	49.26	6
59.21	530.94	153.54	377.40	307.40	70.01	6
58.67	568.85	138.04	430.81	340.68	90.13	6
58.14	606.97	123.47	483.49	374.18	109.31	6
57.60	645.28	110.09	535.19	407.88	127.31	6
57.05	683.78	98.07	585.71	441.76	143.96	6
56.51	722.45	87.49	634.96	475.80	159.16	6
55.96	761.25	78.36	682.89	509.98	172.91	6
55.96	761.25	78.36	682.89	509.98	172.91	5
54.71	864.89	95.84	769.05	587.87	181.18	5
53.47	967.87	115.13	852.74	665.11	187.63	5
52.25	1070.13	136.12	934.01	741.61	192.39	5

51.03	1171.61	158.65	1012.96	817.34	195.62	5
49.83	1272.25	182.58	1089.67	892.24	197.44	5
48.65	1372.01	207.83	1164.19	966.25	197.94	5
48.65	1372.01	207.83	1164.19	966.25	197.94	4
46.65	1572.36	279.21	1293.15	1090.74	202.41	4
44.67	1772.20	357.91	1414.29	1214.72	199.57	4
42.69	1971.47	446.49	1524.98	1338.13	186.85	4
40.72	2170.10	526.85	1643.25	1460.90	182.35	4
38.76	2368.01	589.47	1778.54	1582.95	195.59	4
36.82	2565.15	655.40	1909.75	1704.23	205.52	4
34.89	2761.48	724.95	2036.53	1824.70	211.83	4
32.97	2956.96	798.34	2158.62	1944.32	214.30	4
31.07	3151.54	874.19	2277.35	2063.05	214.30	4
31.07	3151.54	874.20	2277.35	2063.05	214.30	3
29.68	3300.11	936.05	2364.06	2149.76	214.30	3
28.30	3448.29	997.91	2450.38	2236.08	214.30	3
26.92	3596.08	1064.78	2531.30	2322.01	209.30	3
25.55	3743.50	1129.63	2613.87	2407.57	206.30	3
24.18	3890.57	1192.89	2697.67	2492.77	204.90	3
22.82	4037.27	1255.07	2782.20	2577.62	204.58	3
21.47	4183.64	1316.46	2867.18	2662.13	205.05	3
20.12	4329.65	1377.30	2952.35	2746.29	206.07	3
18.78	4475.33	1437.55	3037.78	2830.10	207.67	3
18.78	4475.33	1437.55	3037.78	2830.10	207.67	2
16.86	4680.97	1520.52	3160.45	2949.64	210.81	2
14.95	4886.09	1604.74	3281.35	3068.67	212.68	2
13.06	5090.69	1689.78	3400.91	3187.17	213.74	2
11.17	5294.77	1775.31	3519.46	3305.15	214.30	2
9.28	5498.33	1861.41	3636.92	3422.61	214.30	2
7.41	5701.34	1947.51	3753.83	3539.53	214.30	2
5.54	5903.85	2040.10	3863.75	3655.94	207.81	2
3.69	6105.87	2168.58	3937.29	3771.85	165.44	2
1.84	6307.30	2321.27	3986.04	3887.19	98.84	2
.00	6508.06	2498.37	4009.70	4001.86	7.84	2

Time = 240. Degree of Consolidation = 18.%

Total Settlement = .322

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 240. = .322

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.51	241.51	.00	1

Time = 240. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 240. = .130

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.15

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.16	21.42	6.50	5.91	5.85	6
60.02	59.63	21.35	6.49	5.95	5.84	6
59.45	59.11	21.27	6.47	6.00	5.82	6
58.89	58.57	21.20	6.46	6.04	5.81	6
58.33	58.04	21.12	6.44	6.08	5.80	6
57.76	57.51	21.05	6.43	6.11	5.78	6
57.20	56.97	20.97	6.42	6.15	5.77	6
56.64	56.43	20.90	6.40	6.18	5.76	6
56.08	55.88	20.82	6.39	6.21	5.74	6
56.08	55.88	20.82	4.51	4.36	3.98	5
54.82	54.64	20.59	4.44	4.32	3.91	5
53.56	53.42	20.36	4.38	4.27	3.85	5
52.32	52.20	20.12	4.32	4.22	3.79	5
51.10	51.00	19.89	4.25	4.16	3.72	5
49.88	49.81	19.66	4.19	4.10	3.66	5
48.69	48.63	19.43	4.13	4.04	3.59	5
48.69	48.63	19.43	1.93	1.92	1.90	4
46.69	46.64	18.75	1.92	1.91	1.88	4
44.70	44.65	18.06	1.91	1.90	1.86	4
42.72	42.68	17.38	1.89	1.89	1.84	4
40.75	40.71	16.70	1.88	1.87	1.82	4
38.79	38.76	16.01	1.86	1.85	1.80	4
36.85	36.81	15.33	1.84	1.84	1.78	4
34.91	34.88	14.65	1.82	1.82	1.76	4
33.00	32.97	13.97	1.80	1.80	1.74	4
31.09	31.07	13.28	1.78	1.78	1.71	4
31.09	31.07	13.28	1.47	1.47	1.44	3
29.70	29.68	12.72	1.46	1.46	1.43	3
28.32	28.29	12.16	1.45	1.45	1.42	3
26.94	26.92	11.59	1.44	1.44	1.41	3
25.57	25.54	11.03	1.43	1.43	1.40	3

24.21	24.18	10.47	1.42	1.42	1.39	3
22.84	22.82	9.90	1.41	1.41	1.38	3
21.49	21.47	9.34	1.40	1.40	1.37	3
20.14	20.12	8.78	1.39	1.39	1.36	3
18.80	18.77	8.21	1.38	1.38	1.35	3
18.80	18.77	8.21	1.34	1.34	1.31	2
16.88	16.86	7.39	1.33	1.33	1.30	2
14.97	14.95	6.57	1.32	1.32	1.29	2
13.07	13.05	5.75	1.31	1.31	1.28	2
11.18	11.16	4.93	1.30	1.30	1.27	2
9.30	9.28	4.11	1.29	1.29	1.26	2
7.43	7.41	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.68	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.16	455.81	194.88	260.93	241.51	19.42	6
59.63	493.12	180.52	312.60	274.20	38.40	6
59.11	530.63	166.46	364.17	307.09	57.08	6
58.57	568.34	152.88	415.45	340.17	75.28	6
58.04	606.23	139.95	466.28	373.45	92.83	6
57.51	644.31	127.81	516.50	406.90	109.59	6
56.97	682.55	116.59	565.96	440.52	125.43	6
56.43	720.94	106.40	614.54	474.30	140.24	6
55.88	759.48	97.32	662.15	508.21	153.94	6
55.88	759.48	97.32	662.15	508.21	153.94	5
54.64	862.44	114.73	747.71	585.42	162.29	5
53.42	964.75	133.71	831.04	661.98	169.06	5
52.20	1066.35	154.27	912.08	737.83	174.25	5
51.00	1167.18	176.36	990.82	812.92	177.90	5
49.81	1267.20	199.96	1067.24	887.18	180.05	5
48.63	1366.34	225.02	1141.32	960.57	180.75	5
48.63	1366.34	225.02	1141.32	960.57	180.75	4
46.64	1566.58	294.65	1271.93	1084.95	186.97	4
44.65	1766.32	372.13	1394.19	1208.83	185.36	4
42.68	1965.49	460.04	1505.45	1332.15	173.30	4
40.71	2164.03	534.04	1629.99	1454.83	175.16	4
38.76	2361.86	595.37	1766.48	1576.80	189.69	4
36.81	2558.94	659.81	1899.13	1698.02	201.11	4
34.88	2755.23	727.45	2027.77	1818.45	209.33	4
32.97	2950.69	798.71	2151.98	1938.05	213.93	4
31.07	3145.28	874.37	2270.90	2056.78	214.13	4
31.07	3145.28	874.37	2270.90	2056.78	214.13	3
29.68	3293.84	936.05	2357.79	2143.49	214.30	3
28.29	3442.02	997.91	2444.11	2229.81	214.30	3
26.92	3589.81	1065.99	2523.82	2315.74	208.09	3
25.54	3737.22	1131.97	2605.25	2401.29	203.97	3
24.18	3884.27	1196.00	2688.27	2486.48	201.79	3
22.82	4030.96	1258.61	2772.34	2571.31	201.04	3
21.47	4177.30	1320.06	2857.24	2655.79	201.45	3
20.12	4323.30	1380.76	2942.53	2739.93	202.60	3
18.77	4468.95	1440.59	3028.36	2823.73	204.64	3
18.77	4468.95	1440.59	3028.36	2823.73	204.64	2
16.86	4674.58	1522.72	3151.85	2943.25	208.60	2
14.95	4879.69	1605.94	3273.75	3062.27	211.48	2
13.05	5084.28	1690.53	3393.76	3180.76	212.99	2
11.16	5288.36	1775.58	3512.78	3298.74	214.03	2
9.28	5491.91	1861.41	3630.50	3416.19	214.30	2

7.41	5694.93	1947.51	3747.42	3533.12	214.30	2
5.54	5897.42	2050.07	3847.35	3649.51	197.84	2
3.68	6099.37	2187.24	3912.13	3765.36	146.77	2
1.84	6300.73	2338.42	3962.31	3880.62	81.69	2
.00	6501.45	2499.78	4001.67	3995.24	6.43	2

Time = 365. Degree of Consolidation = 24.%

Total Settlement = .428

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 365. = .428

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.51	241.51	.00	1

Time = 365. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 365. = .130

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.04

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
60.58	60.03	21.42
60.02	59.51	21.35
59.45	58.98	21.27
58.89	58.45	21.20
58.33	57.92	21.12
57.76	57.39	21.05
57.20	56.86	20.97
56.64	56.32	20.90
56.08	55.78	20.82
56.08	55.78	20.82
54.82	54.56	20.59
53.56	53.34	20.36
52.32	52.14	20.12
51.10	50.95	19.89
49.88	49.77	19.66
48.69	48.61	19.43
48.69	48.61	19.43
46.69	46.62	18.75
44.70	44.64	18.06
42.72	42.66	17.38
40.75	40.70	16.70
38.79	38.75	16.01
36.85	36.81	15.33
34.91	34.88	14.65
33.00	32.96	13.97
31.09	31.06	13.28
31.09	31.06	13.28
29.70	29.67	12.72
28.32	28.29	12.16
26.94	26.91	11.59
25.57	25.54	11.03
24.21	24.17	10.47
22.84	22.81	9.90
21.49	21.46	9.34
20.14	20.11	8.78
18.80	18.77	8.21
18.80	18.77	8.21
16.88	16.86	7.39
14.97	14.95	6.57
13.07	13.05	5.75
11.18	11.16	4.93
9.30	9.28	4.11
7.43	7.40	3.29
5.56	5.54	2.46
3.70	3.68	1.64
1.85	1.84	.82
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
6.50	5.90	5.85	6
6.49	5.94	5.84	6
6.47	5.97	5.82	6
6.46	6.00	5.81	6
6.44	6.03	5.80	6
6.43	6.06	5.78	6
6.42	6.09	5.77	6
6.40	6.12	5.76	6
6.39	6.14	5.74	6
4.51	4.30	3.98	5
4.44	4.26	3.91	5
4.38	4.21	3.85	5
4.32	4.16	3.79	5
4.25	4.10	3.72	5
4.19	4.04	3.66	5
4.13	3.98	3.59	5
1.93	1.92	1.90	4
1.92	1.91	1.88	4
1.91	1.90	1.86	4
1.89	1.88	1.84	4
1.88	1.87	1.82	4
1.86	1.85	1.80	4
1.84	1.83	1.78	4
1.82	1.82	1.76	4
1.80	1.80	1.74	4
1.78	1.77	1.71	4
1.47	1.47	1.44	3
1.46	1.46	1.43	3
1.45	1.45	1.42	3
1.44	1.44	1.41	3
1.43	1.43	1.40	3
1.42	1.42	1.39	3
1.41	1.41	1.38	3
1.40	1.40	1.37	3
1.39	1.39	1.36	3
1.38	1.38	1.35	3
1.34	1.34	1.31	2
1.33	1.33	1.30	2
1.32	1.32	1.29	2
1.31	1.31	1.28	2
1.30	1.30	1.27	2
1.29	1.29	1.26	2
1.28	1.28	1.26	2
1.27	1.27	1.25	2
1.26	1.25	1.24	2
1.25	1.24	1.24	2
1.25	1.23	1.23	2

***** Stresses *****

XI	Total	Effective
60.03	455.81	197.82
59.51	493.05	186.50
58.98	530.46	175.38
58.45	568.02	164.58
57.92	605.73	154.23
57.39	643.59	144.43
56.86	681.58	135.31
56.32	719.69	126.96

***** Pore Pressures *****

Total	Static	Excess	Material
257.99	241.51	16.48	6
306.56	274.13	32.43	6
355.08	306.92	48.17	6
403.44	339.86	63.58	6
451.50	372.95	78.56	6
499.15	406.18	92.97	6
546.27	439.55	106.72	6
592.73	473.04	119.68	6

55.78	757.92	119.50	638.42	506.65	131.77	6
55.78	757.92	119.50	638.42	506.65	131.77	5
54.56	860.07	137.78	722.29	583.05	139.24	5
53.34	961.54	157.35	804.19	658.77	145.42	5
52.14	1062.28	178.24	884.04	733.77	150.27	5
50.95	1162.25	200.48	961.77	807.99	153.78	5
49.77	1261.40	224.05	1037.35	881.39	155.96	5
48.61	1359.68	248.95	1110.73	953.92	156.81	5
48.61	1359.68	248.95	1110.73	953.92	156.81	4
46.62	1559.77	317.15	1242.61	1078.14	164.47	4
44.64	1759.35	393.25	1366.11	1201.87	164.24	4
42.66	1958.39	479.97	1478.42	1325.05	153.38	4
40.70	2156.80	544.27	1612.52	1447.60	164.93	4
38.75	2354.52	603.72	1750.80	1569.45	181.34	4
36.81	2551.51	666.17	1885.33	1690.59	194.75	4
34.88	2747.73	731.88	2015.85	1810.95	204.90	4
32.96	2943.15	801.47	2141.68	1930.51	211.17	4
31.06	3137.71	875.72	2261.99	2049.22	212.78	4
31.06	3137.71	875.72	2261.99	2049.22	212.78	3
29.67	3286.28	936.05	2350.22	2135.92	214.30	3
28.29	3434.46	997.91	2436.55	2222.24	214.30	3
26.91	3582.24	1067.19	2515.05	2308.17	206.89	3
25.54	3729.64	1134.34	2595.31	2393.71	201.60	3
24.17	3876.67	1199.27	2677.40	2478.88	198.52	3
22.81	4023.34	1262.44	2760.91	2563.69	197.21	3
21.46	4169.66	1324.09	2845.57	2648.15	197.42	3
20.11	4315.64	1384.66	2930.98	2732.27	198.71	3
18.77	4461.27	1444.16	3017.11	2816.05	201.06	3
18.77	4461.27	1444.16	3017.11	2816.05	201.06	2
16.86	4666.88	1525.67	3141.21	2935.55	205.66	2
14.95	4871.97	1608.21	3263.76	3054.55	209.21	2
13.05	5076.56	1692.10	3384.46	3173.04	211.42	2
11.16	5280.62	1776.84	3503.79	3291.01	212.78	2
9.28	5484.17	1862.34	3621.83	3408.45	213.38	2
7.40	5687.18	1949.90	3737.28	3525.36	211.92	2
5.54	5889.64	2061.27	3828.37	3641.73	186.64	2
3.68	6091.53	2203.43	3888.10	3757.52	130.58	2
1.84	6292.83	2350.93	3941.90	3872.72	69.17	2
.00	6493.52	2500.75	3992.77	3987.31	5.46	2

Time = 540. Degree of Consolidation = 31.%

Total Settlement = .555

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 540. = .555

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1

1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.51	241.51	.00	1

Time = 540. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 540. = .130

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.91

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.91	21.42	6.50	5.90	5.85	6
60.02	59.39	21.35	6.49	5.92	5.84	6
59.45	58.86	21.27	6.47	5.95	5.82	6
58.89	58.34	21.20	6.46	5.97	5.81	6
58.33	57.81	21.12	6.44	6.00	5.80	6
57.76	57.28	21.05	6.43	6.02	5.78	6
57.20	56.75	20.97	6.42	6.04	5.77	6
56.64	56.21	20.90	6.40	6.06	5.76	6
56.08	55.68	20.82	6.39	6.08	5.74	6
56.08	55.68	20.82	4.51	4.25	3.98	5
54.82	54.47	20.59	4.44	4.20	3.91	5
53.56	53.27	20.36	4.38	4.15	3.85	5
52.32	52.08	20.12	4.32	4.10	3.79	5
51.10	50.90	19.89	4.25	4.04	3.72	5
49.88	49.74	19.66	4.19	3.99	3.66	5
48.69	48.59	19.43	4.13	3.92	3.59	5
48.69	48.59	19.43	1.93	1.92	1.90	4
46.69	46.60	18.75	1.92	1.91	1.88	4
44.70	44.62	18.06	1.91	1.89	1.86	4
42.72	42.65	17.38	1.89	1.88	1.84	4
40.75	40.69	16.70	1.88	1.86	1.82	4
38.79	38.74	16.01	1.86	1.85	1.80	4
36.85	36.80	15.33	1.84	1.83	1.78	4
34.91	34.87	14.65	1.82	1.81	1.76	4
33.00	32.96	13.97	1.80	1.79	1.74	4
31.09	31.05	13.28	1.78	1.77	1.71	4

31.09	31.05	13.28	1.47	1.47	1.44	3
29.70	29.66	12.72	1.46	1.46	1.43	3
28.32	28.28	12.16	1.45	1.45	1.42	3
26.94	26.90	11.59	1.44	1.44	1.41	3
25.57	25.53	11.03	1.43	1.43	1.40	3
24.21	24.17	10.47	1.42	1.42	1.39	3
22.84	22.81	9.90	1.41	1.41	1.38	3
21.49	21.46	9.34	1.40	1.40	1.37	3
20.14	20.11	8.78	1.39	1.39	1.36	3
18.80	18.77	8.21	1.38	1.38	1.35	3
18.80	18.77	8.21	1.34	1.34	1.31	2
16.88	16.85	7.39	1.33	1.33	1.30	2
14.97	14.94	6.57	1.32	1.32	1.29	2
13.07	13.05	5.75	1.31	1.31	1.28	2
11.18	11.16	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.26	2
5.56	5.54	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.91	455.81	200.25	255.56	241.51	14.06	6
59.39	493.00	191.40	301.60	274.08	27.53	6
58.86	530.32	182.73	347.59	306.77	40.82	6
58.34	567.76	174.33	393.42	339.59	53.83	6
57.81	605.31	166.32	438.99	372.53	66.47	6
57.28	642.98	158.78	484.20	405.57	78.62	6
56.75	680.75	151.81	528.94	438.72	90.21	6
56.21	718.61	145.51	573.11	471.97	101.14	6
55.68	756.56	139.95	616.61	505.30	111.31	6
55.68	756.56	139.95	616.61	505.30	111.31	5
54.47	857.96	159.33	698.63	580.94	117.68	5
53.27	958.64	179.76	778.88	655.87	123.00	5
52.08	1058.57	201.28	857.29	730.05	127.24	5
50.90	1157.71	223.90	933.81	803.44	130.37	5
49.74	1256.01	247.63	1008.39	876.00	132.39	5
48.59	1353.45	272.45	1081.00	947.68	133.32	5
48.59	1353.45	272.45	1081.00	947.68	133.32	4
46.60	1553.37	340.00	1213.37	1071.75	141.63	4
44.62	1752.81	415.36	1337.45	1195.32	142.12	4
42.65	1951.70	500.85	1450.85	1318.35	132.49	4
40.69	2149.96	555.58	1594.38	1440.76	153.62	4
38.74	2347.55	613.16	1734.39	1562.49	171.90	4
36.80	2544.44	673.71	1870.73	1683.52	187.21	4
34.87	2740.59	737.58	2003.01	1803.81	199.20	4
32.96	2935.95	805.33	2130.62	1923.31	207.31	4
31.05	3130.48	877.83	2252.64	2041.98	210.66	4
31.05	3130.48	877.83	2252.64	2041.98	210.66	3
29.66	3279.04	936.55	2342.48	2128.68	213.80	3
28.28	3427.21	998.31	2428.91	2215.00	213.91	3
26.90	3574.99	1068.47	2506.53	2300.92	205.61	3
25.53	3722.38	1136.35	2586.03	2386.45	199.58	3
24.17	3869.40	1201.92	2667.48	2471.61	195.87	3
22.81	4016.05	1265.51	2750.55	2556.41	194.14	3
21.46	4162.36	1327.50	2834.86	2640.85	194.01	3
20.11	4308.31	1388.07	2920.24	2724.94	195.30	3
18.77	4453.93	1447.35	3006.58	2808.71	197.87	3
18.77	4453.93	1447.35	3006.58	2808.71	197.87	2

16.85	4659.51	1528.37	3131.14	2928.19	202.95	2
14.94	4864.60	1610.42	3254.18	3047.17	207.00	2
13.05	5069.17	1693.80	3375.37	3165.65	209.72	2
11.16	5273.22	1778.54	3494.68	3283.61	211.08	2
9.27	5476.75	1865.37	3611.38	3401.04	210.34	2
7.40	5679.74	1954.85	3724.89	3517.93	206.96	2
5.54	5882.17	2071.49	3810.68	3634.26	176.42	2
3.68	6084.02	2214.14	3869.88	3750.01	119.87	2
1.84	6285.28	2358.12	3927.15	3865.17	61.99	2
.00	6485.95	2501.30	3984.64	3979.74	4.90	2

Time = 730. Degree of Consolidation = 37.%

Total Settlement = .677

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 730. = .677

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses *****

***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.51	241.51	.00	1

Time = 730. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 730. = .130

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.79

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.72	21.42	6.50	5.88	5.85	6
60.02	59.19	21.35	6.49	5.90	5.84	6
59.45	58.67	21.27	6.47	5.92	5.82	6
58.89	58.15	21.20	6.46	5.93	5.81	6
58.33	57.63	21.12	6.44	5.94	5.80	6
57.76	57.10	21.05	6.43	5.96	5.78	6
57.20	56.57	20.97	6.42	5.97	5.77	6
56.64	56.05	20.90	6.40	5.98	5.76	6
56.08	55.52	20.82	6.39	5.98	5.74	6
56.08	55.52	20.82	4.51	4.18	3.98	5
54.82	54.33	20.59	4.44	4.12	3.91	5
53.56	53.15	20.36	4.38	4.07	3.85	5
52.32	51.98	20.12	4.32	4.01	3.79	5
51.10	50.82	19.89	4.25	3.96	3.72	5
49.88	49.68	19.66	4.19	3.90	3.66	5
48.69	48.55	19.43	4.13	3.83	3.59	5
48.69	48.55	19.43	1.93	1.91	1.90	4
46.69	46.57	18.75	1.92	1.90	1.88	4
44.70	44.59	18.06	1.91	1.89	1.86	4
42.72	42.62	17.38	1.89	1.87	1.84	4
40.75	40.67	16.70	1.88	1.86	1.82	4
38.79	38.72	16.01	1.86	1.84	1.80	4
36.85	36.78	15.33	1.84	1.83	1.78	4
34.91	34.86	14.65	1.82	1.81	1.76	4
33.00	32.94	13.97	1.80	1.79	1.74	4
31.09	31.04	13.28	1.78	1.77	1.71	4
31.09	31.04	13.28	1.47	1.47	1.44	3
29.70	29.65	12.72	1.46	1.46	1.43	3
28.32	28.27	12.16	1.45	1.45	1.42	3
26.94	26.90	11.59	1.44	1.44	1.41	3
25.57	25.53	11.03	1.43	1.43	1.40	3
24.21	24.16	10.47	1.42	1.42	1.39	3
22.84	22.80	9.90	1.41	1.41	1.38	3
21.49	21.45	9.34	1.40	1.40	1.37	3
20.14	20.10	8.78	1.39	1.39	1.36	3
18.80	18.76	8.21	1.38	1.38	1.35	3
18.80	18.76	8.21	1.34	1.34	1.31	2
16.88	16.85	7.39	1.33	1.33	1.30	2
14.97	14.94	6.57	1.32	1.32	1.29	2
13.07	13.04	5.75	1.31	1.31	1.28	2
11.18	11.15	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.72	455.81	203.89	251.92	241.50	10.41	6
59.19	492.92	198.71	294.21	274.00	20.21	6
58.67	530.11	193.69	336.42	306.56	29.86	6

58.15	567.37	188.89	378.47	339.20	39.27	6
57.63	604.69	184.40	420.29	371.90	48.39	6
57.10	642.07	180.29	461.79	404.67	57.12	6
56.57	679.51	176.63	502.88	437.49	65.40	6
56.05	717.00	173.49	543.51	470.36	73.15	6
55.52	754.53	170.95	583.58	503.26	80.32	6
55.52	754.53	170.95	583.58	503.26	80.32	5
54.33	854.78	192.11	662.67	577.76	84.90	5
53.15	954.26	213.99	740.27	651.49	88.77	5
51.98	1052.94	236.61	816.33	724.42	91.90	5
50.82	1150.80	259.99	890.80	796.53	94.27	5
49.68	1247.80	284.14	963.66	867.78	95.88	5
48.55	1343.92	309.04	1034.88	938.16	96.73	5
48.55	1343.92	309.04	1034.88	938.16	96.73	4
46.57	1543.59	377.28	1166.31	1061.97	104.34	4
44.59	1742.77	453.32	1289.45	1185.29	104.16	4
42.62	1941.40	522.09	1419.31	1308.06	111.26	4
40.67	2139.42	574.88	1564.55	1430.22	134.33	4
38.72	2336.80	630.17	1706.64	1551.74	154.90	4
36.78	2533.50	688.34	1845.16	1672.58	172.58	4
34.86	2729.49	749.82	1979.67	1792.71	186.96	4
32.94	2924.72	815.33	2109.38	1912.08	197.31	4
31.04	3119.14	886.18	2232.95	2030.64	202.32	4
31.04	3119.14	886.18	2232.95	2030.64	202.32	3
29.65	3267.65	943.37	2324.28	2117.29	206.99	3
28.27	3415.78	1004.48	2411.30	2203.57	207.73	3
26.90	3563.53	1073.94	2489.59	2289.46	200.14	3
25.53	3710.89	1141.26	2569.63	2374.96	194.67	3
24.16	3857.88	1206.63	2651.25	2460.09	191.16	3
22.80	4004.51	1270.21	2734.30	2544.86	189.44	3
21.45	4150.78	1332.21	2818.57	2629.28	189.30	3
20.10	4296.71	1392.80	2903.91	2713.35	190.57	3
18.76	4442.31	1452.15	2990.16	2797.08	193.08	3
18.76	4442.31	1452.15	2990.16	2797.08	193.08	2
16.85	4647.86	1533.27	3114.58	2916.53	198.05	2
14.94	4852.91	1615.45	3237.46	3035.49	201.97	2
13.04	5057.45	1698.98	3358.47	3153.93	204.54	2
11.15	5261.47	1784.23	3477.25	3271.86	205.39	2
9.27	5464.97	1871.64	3593.33	3389.25	204.08	2
7.40	5667.91	1962.33	3705.58	3506.10	199.48	2
5.53	5870.29	2084.29	3786.00	3622.38	163.62	2
3.68	6072.09	2225.81	3846.27	3738.08	108.20	2
1.84	6273.31	2365.15	3908.15	3853.20	54.95	2
.00	6473.96	2501.85	3972.12	3967.75	4.36	2

Time = 1080. Degree of Consolidation = 48.%

Total Settlement = .869

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 1080. = .869

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.50	241.50	.00	1

Time = 1080. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 1080. = .130

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.60

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.55	21.42	6.50	5.87	5.85	6
60.02	59.03	21.35	6.49	5.88	5.84	6
59.45	58.51	21.27	6.47	5.89	5.82	6
58.89	57.99	21.20	6.46	5.89	5.81	6
58.33	57.47	21.12	6.44	5.90	5.80	6
57.76	56.95	21.05	6.43	5.90	5.78	6
57.20	56.42	20.97	6.42	5.91	5.77	6
56.64	55.90	20.90	6.40	5.91	5.76	6
56.08	55.38	20.82	6.39	5.91	5.74	6
56.08	55.38	20.82	4.51	4.11	3.98	5
54.82	54.20	20.59	4.44	4.06	3.91	5
53.56	53.04	20.36	4.38	4.00	3.85	5
52.32	51.88	20.12	4.32	3.94	3.79	5
51.10	50.75	19.89	4.25	3.88	3.72	5
49.88	49.62	19.66	4.19	3.82	3.66	5
48.69	48.51	19.43	4.13	3.76	3.59	5
48.69	48.51	19.43	1.93	1.91	1.90	4
46.69	46.53	18.75	1.92	1.89	1.88	4
44.70	44.56	18.06	1.91	1.88	1.86	4
42.72	42.59	17.38	1.89	1.87	1.84	4
40.75	40.64	16.70	1.88	1.85	1.82	4

38.79	38.70	16.01	1.86	1.84	1.80	4
36.85	36.76	15.33	1.84	1.82	1.78	4
34.91	34.84	14.65	1.82	1.81	1.76	4
33.00	32.93	13.97	1.80	1.79	1.74	4
31.09	31.03	13.28	1.78	1.77	1.71	4
31.09	31.03	13.28	1.47	1.47	1.44	3
29.70	29.64	12.72	1.46	1.46	1.43	3
28.32	28.26	12.16	1.45	1.45	1.42	3
26.94	26.89	11.59	1.44	1.44	1.41	3
25.57	25.52	11.03	1.43	1.43	1.40	3
24.21	24.15	10.47	1.42	1.42	1.39	3
22.84	22.80	9.90	1.41	1.41	1.38	3
21.49	21.44	9.34	1.40	1.40	1.37	3
20.14	20.10	8.78	1.39	1.39	1.36	3
18.80	18.76	8.21	1.38	1.38	1.35	3
18.80	18.76	8.21	1.34	1.33	1.31	2
16.88	16.84	7.39	1.33	1.33	1.30	2
14.97	14.94	6.57	1.32	1.32	1.29	2
13.07	13.04	5.75	1.31	1.31	1.28	2
11.18	11.15	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.28	1.26	2
7.43	7.40	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.55	455.81	207.01	248.80	241.50	7.29	6
59.03	492.85	204.80	288.05	273.93	14.12	6
58.51	529.93	202.72	327.21	306.39	20.82	6
57.99	567.04	200.83	366.21	338.88	27.33	6
57.47	604.17	199.19	404.98	371.39	33.59	6
56.95	641.33	197.86	443.47	403.92	39.54	6
56.42	678.50	196.89	481.61	436.47	45.13	6
55.90	715.68	196.33	519.35	469.03	50.31	6
55.38	752.87	196.24	556.62	501.60	55.02	6
55.38	752.87	196.24	556.62	501.60	55.02	5
54.20	852.18	218.94	633.24	575.17	58.08	5
53.04	950.67	242.08	708.59	647.91	60.69	5
51.88	1048.33	265.70	782.63	719.81	62.82	5
50.75	1145.13	289.79	855.33	790.86	64.47	5
49.62	1241.05	314.38	926.67	861.04	65.63	5
48.51	1336.09	339.45	996.64	930.32	66.31	5
48.51	1336.09	339.45	996.64	930.32	66.32	4
46.53	1535.54	409.22	1126.32	1053.92	72.40	4
44.56	1734.50	487.11	1247.39	1177.02	70.37	4
42.59	1932.90	541.58	1391.32	1299.56	91.77	4
40.64	2130.69	593.06	1537.63	1421.49	116.14	4
38.70	2327.86	646.88	1680.99	1542.80	138.19	4
36.76	2524.37	703.55	1820.82	1663.45	157.37	4
34.84	2720.19	763.63	1956.55	1783.41	173.15	4
32.93	2915.26	827.81	2087.45	1902.62	184.83	4
31.03	3109.54	897.59	2211.94	2021.04	190.91	4
31.03	3109.54	897.59	2211.94	2021.04	190.91	3
29.64	3257.98	953.77	2304.21	2107.62	196.59	3
28.26	3406.05	1014.91	2391.15	2193.84	197.31	3
26.89	3553.74	1082.83	2470.92	2279.67	191.25	3
25.52	3701.06	1149.13	2551.93	2365.13	186.80	3
24.15	3848.01	1213.84	2634.17	2450.22	183.95	3

22.80	3994.60	1277.15	2717.44	2534.95	182.50	3
21.44	4140.83	1338.98	2801.85	2619.32	182.52	3
20.10	4286.72	1399.43	2887.29	2703.36	183.94	3
18.76	4432.28	1458.65	2973.63	2787.05	186.58	3
18.76	4432.28	1458.65	2973.63	2787.05	186.58	2
16.84	4637.79	1539.69	3098.11	2906.47	191.64	2
14.94	4842.80	1621.84	3220.97	3025.38	195.59	2
13.04	5047.31	1705.36	3341.94	3143.79	198.16	2
11.15	5251.29	1790.63	3460.66	3261.67	198.99	2
9.27	5454.74	1878.09	3576.65	3379.03	197.63	2
7.40	5657.65	1968.89	3688.76	3495.83	192.92	2
5.53	5859.98	2094.03	3765.96	3612.07	153.89	2
3.68	6061.74	2233.49	3828.25	3727.73	100.52	2
1.84	6262.94	2370.01	3892.93	3842.83	50.10	2
.00	6463.58	2502.22	3961.36	3957.38	3.99	2

Time = 1440. Degree of Consolidation = 57.%

Total Settlement = 1.035

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 1440. = 1.035

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.00	3.87	2.02
3.00	2.89	1.52
2.00	1.92	1.01
1.00	.96	.51
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.87	.00	.00
2.89	114.77	53.58
1.92	228.65	107.15
.96	342.31	160.73
.00	455.81	214.30

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
61.19	61.19	.00	1
121.50	121.50	.00	1
181.58	181.58	.00	1
241.50	241.50	.00	1

Time = 1440. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 1440. = .130

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.44

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.40	21.42	6.50	5.87	5.85	6
60.02	58.88	21.35	6.49	5.87	5.84	6
59.45	58.36	21.27	6.47	5.86	5.82	6
58.89	57.84	21.20	6.46	5.86	5.81	6
58.33	57.32	21.12	6.44	5.86	5.80	6
57.76	56.81	21.05	6.43	5.86	5.78	6
57.20	56.29	20.97	6.42	5.85	5.77	6
56.64	55.77	20.90	6.40	5.85	5.76	6
56.08	55.25	20.82	6.39	5.84	5.74	6
56.08	55.25	20.82	4.51	4.06	3.98	5
54.82	54.09	20.59	4.44	4.00	3.91	5
53.56	52.94	20.36	4.38	3.94	3.85	5
52.32	51.80	20.12	4.32	3.88	3.79	5
51.10	50.67	19.89	4.25	3.82	3.72	5
49.88	49.56	19.66	4.19	3.76	3.66	5
48.69	48.47	19.43	4.13	3.69	3.59	5
48.69	48.47	19.43	1.93	1.90	1.90	4
46.69	46.49	18.75	1.92	1.89	1.88	4
44.70	44.52	18.06	1.91	1.88	1.86	4
42.72	42.56	17.38	1.89	1.86	1.84	4
40.75	40.61	16.70	1.88	1.85	1.82	4
38.79	38.67	16.01	1.86	1.83	1.80	4
36.85	36.74	15.33	1.84	1.82	1.78	4
34.91	34.82	14.65	1.82	1.80	1.76	4
33.00	32.91	13.97	1.80	1.78	1.74	4
31.09	31.02	13.28	1.78	1.76	1.71	4
31.09	31.02	13.28	1.47	1.47	1.44	3
29.70	29.63	12.72	1.46	1.46	1.43	3
28.32	28.25	12.16	1.45	1.45	1.42	3
26.94	26.88	11.59	1.44	1.43	1.41	3
25.57	25.51	11.03	1.43	1.42	1.40	3
24.21	24.14	10.47	1.42	1.41	1.39	3
22.84	22.79	9.90	1.41	1.40	1.38	3
21.49	21.44	9.34	1.40	1.39	1.37	3
20.14	20.09	8.78	1.39	1.38	1.36	3
18.80	18.75	8.21	1.38	1.38	1.35	3
18.80	18.75	8.21	1.34	1.33	1.31	2
16.88	16.84	7.39	1.33	1.32	1.30	2
14.97	14.93	6.57	1.32	1.31	1.29	2
13.07	13.03	5.75	1.31	1.30	1.28	2
11.18	11.15	4.93	1.30	1.29	1.27	2
9.30	9.27	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.40	455.81	209.75	246.06	241.50	4.56	6
58.88	492.80	210.10	282.70	273.87	8.83	6
58.36	529.78	210.55	319.24	306.24	13.00	6
57.84	566.76	211.14	355.62	338.60	17.03	6
57.32	603.73	211.93	391.80	370.95	20.85	6
56.81	640.69	212.97	427.72	403.28	24.44	6
56.29	677.63	214.29	463.34	435.60	27.74	6
55.77	714.54	215.93	498.61	467.90	30.71	6
55.25	751.43	217.95	533.49	500.17	33.32	6
55.25	751.43	217.94	533.49	500.17	33.32	5
54.09	849.95	241.98	607.97	572.93	35.04	5
52.94	947.59	266.25	681.34	644.83	36.51	5
51.80	1044.36	290.79	753.57	715.85	37.73	5
50.67	1140.25	315.59	824.65	785.98	38.67	5
49.56	1235.24	340.67	894.56	855.22	39.34	5
48.47	1329.32	366.02	963.30	923.56	39.75	5
48.47	1329.32	366.02	963.30	923.56	39.75	4
46.49	1528.59	438.32	1090.27	1046.97	43.30	4
44.52	1727.34	510.49	1216.86	1169.86	47.00	4
42.56	1925.52	559.67	1365.85	1292.18	73.67	4
40.61	2123.11	610.64	1512.47	1413.90	98.56	4
38.67	2320.07	663.81	1656.25	1535.01	121.25	4
36.74	2516.38	719.59	1796.79	1655.46	141.33	4
34.82	2712.01	778.66	1933.35	1775.23	158.12	4
32.91	2906.91	842.11	2064.80	1894.27	170.53	4
31.02	3101.02	911.29	2189.72	2012.52	177.20	4
31.02	3101.02	911.29	2189.72	2012.52	177.20	3
29.63	3249.37	966.83	2282.54	2099.02	183.52	3
28.25	3397.37	1028.32	2369.04	2185.15	183.89	3
26.88	3544.99	1094.59	2450.40	2270.92	179.49	3
25.51	3692.24	1159.49	2532.75	2356.31	176.44	3
24.14	3839.14	1223.20	2615.94	2441.34	174.59	3
22.79	3985.67	1285.57	2700.10	2526.02	174.08	3
21.44	4131.86	1346.77	2785.10	2610.36	174.74	3
20.09	4277.71	1406.95	2870.76	2694.35	176.42	3
18.75	4423.23	1465.96	2957.27	2778.00	179.27	3
18.75	4423.23	1465.96	2957.27	2778.00	179.27	2
16.84	4628.70	1546.59	3082.11	2897.37	184.74	2
14.93	4833.67	1628.70	3204.97	3016.24	188.72	2
13.03	5038.13	1712.21	3325.92	3134.61	191.31	2
11.15	5242.07	1797.49	3444.58	3252.45	192.13	2
9.27	5445.48	1884.99	3560.49	3369.76	190.73	2
7.39	5648.34	1975.82	3672.53	3486.53	186.00	2
5.53	5850.64	2102.52	3748.12	3602.73	145.39	2
3.68	6052.37	2239.27	3813.10	3718.36	94.75	2
1.84	6253.55	2373.19	3880.36	3833.44	46.92	2
.00	6454.18	2502.47	3951.72	3947.98	3.74	2

Time = 1825. Degree of Consolidation = 66.%

Total Settlement = 1.186

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 1825. = 1.186

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.50	241.50	.00	1

Time = 1825. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 1825. = .130

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.28

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.16	21.42	6.50	5.85	5.85	6
60.02	58.64	21.35	6.49	5.84	5.84	6
59.45	58.13	21.27	6.47	5.82	5.82	6
58.89	57.61	21.20	6.46	5.81	5.81	6
58.33	57.10	21.12	6.44	5.80	5.80	6
57.76	56.58	21.05	6.43	5.78	5.78	6
57.20	56.07	20.97	6.42	5.77	5.77	6
56.64	55.56	20.90	6.40	5.75	5.76	6
56.08	55.05	20.82	6.39	5.74	5.74	6
56.08	55.05	20.82	4.51	3.98	3.98	5
54.82	53.91	20.59	4.44	3.91	3.91	5
53.56	52.77	20.36	4.38	3.85	3.85	5
52.32	51.66	20.12	4.32	3.78	3.79	5
51.10	50.56	19.89	4.25	3.72	3.72	5
49.88	49.47	19.66	4.19	3.66	3.66	5
48.69	48.40	19.43	4.13	3.59	3.59	5

48.69	48.40	19.43	1.93	1.90	1.90	4
46.69	46.42	18.75	1.92	1.88	1.88	4
44.70	44.46	18.06	1.91	1.87	1.86	4
42.72	42.50	17.38	1.89	1.86	1.84	4
40.75	40.56	16.70	1.88	1.84	1.82	4
38.79	38.62	16.01	1.86	1.83	1.80	4
36.85	36.70	15.33	1.84	1.81	1.78	4
34.91	34.78	14.65	1.82	1.79	1.76	4
33.00	32.88	13.97	1.80	1.78	1.74	4
31.09	30.99	13.28	1.78	1.76	1.71	4
31.09	30.99	13.28	1.47	1.46	1.44	3
29.70	29.61	12.72	1.46	1.45	1.43	3
28.32	28.23	12.16	1.45	1.44	1.42	3
26.94	26.86	11.59	1.44	1.43	1.41	3
25.57	25.49	11.03	1.43	1.42	1.40	3
24.21	24.13	10.47	1.42	1.41	1.39	3
22.84	22.77	9.90	1.41	1.40	1.38	3
21.49	21.42	9.34	1.40	1.39	1.37	3
20.14	20.08	8.78	1.39	1.38	1.36	3
18.80	18.74	8.21	1.38	1.37	1.35	3
18.80	18.74	8.21	1.34	1.33	1.31	2
16.88	16.83	7.39	1.33	1.32	1.30	2
14.97	14.92	6.57	1.32	1.31	1.29	2
13.07	13.03	5.75	1.31	1.30	1.28	2
11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.16	455.81	214.30	241.50	241.50	.00	6
58.64	492.70	218.92	273.78	273.78	.00	6
58.13	529.53	223.54	305.98	305.98	.00	6
57.61	566.29	228.16	338.12	338.12	.00	6
57.10	602.98	232.78	370.20	370.20	.00	6
56.58	639.61	237.40	402.21	402.21	.00	6
56.07	676.17	242.03	434.15	434.15	.00	6
55.56	712.67	246.65	466.03	466.03	.00	6
55.05	749.10	251.27	497.84	497.84	.00	6
55.05	749.10	251.27	497.84	497.84	.00	5
53.91	846.38	277.02	569.37	569.37	.00	5
52.77	942.74	302.77	639.97	639.97	.00	5
51.66	1038.17	328.52	709.66	709.66	.00	5
50.56	1132.68	354.27	778.42	778.42	.00	5
49.47	1226.27	380.02	846.25	846.25	.00	5
48.40	1318.93	405.77	913.16	913.16	.00	5
48.40	1318.93	405.77	913.16	913.16	.00	4
46.42	1517.92	481.63	1036.29	1036.29	.00	4
44.46	1716.35	537.93	1178.42	1158.87	19.56	4
42.50	1914.20	587.35	1326.85	1280.86	45.99	4
40.56	2111.46	638.08	1473.38	1402.25	71.12	4
38.62	2308.09	690.77	1617.32	1523.03	94.29	4
36.70	2504.09	746.01	1758.08	1643.17	114.91	4
34.78	2699.40	804.51	1894.89	1762.62	132.27	4
32.88	2894.00	867.39	2026.61	1881.36	145.25	4
30.99	3087.81	936.39	2151.42	1999.31	152.11	4
30.99	3087.81	936.39	2151.42	1999.31	152.11	3

29.61	3236.00	991.65	2244.35	2085.65	158.70	3
28.23	3383.84	1054.89	2328.95	2171.63	157.32	3
26.86	3531.33	1118.53	2412.79	2257.25	155.54	3
25.49	3678.45	1181.24	2497.21	2342.52	154.69	3
24.13	3825.23	1242.86	2582.37	2427.44	154.93	3
22.77	3971.66	1303.56	2668.10	2512.01	156.09	3
21.42	4117.75	1363.48	2754.27	2596.24	158.02	3
20.08	4263.51	1422.47	2841.04	2680.14	160.90	3
18.74	4408.94	1480.65	2928.28	2763.71	164.57	3
18.74	4408.94	1480.65	2928.28	2763.71	164.57	2
16.83	4614.32	1559.71	3054.62	2883.00	171.62	2
14.92	4819.21	1640.98	3178.24	3001.79	176.44	2
13.03	5023.60	1723.97	3299.63	3120.08	179.55	2
11.14	5227.47	1808.74	3418.73	3237.85	180.87	2
9.26	5430.82	1895.76	3535.05	3355.10	179.95	2
7.39	5633.61	1985.60	3648.01	3471.80	176.21	2
5.53	5835.86	2114.70	3721.15	3587.94	133.21	2
3.68	6037.54	2248.62	3788.93	3703.53	85.40	2
1.84	6238.69	2377.95	3860.74	3818.58	42.16	2
.00	6439.32	2502.83	3936.48	3933.11	3.37	2

Time = 2520. Degree of Consolidation = 79.%

Total Settlement = 1.424

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 2520. = 1.423

Settlement caused by Secondary Compression at time 2520. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.00	3.87	2.02
3.00	2.89	1.52
2.00	1.92	1.01
1.00	.96	.51
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.87	.00	.00
2.89	114.77	53.58
1.92	228.65	107.15
.96	342.31	160.73
.00	455.81	214.30

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
61.19	61.19	.00	1
121.50	121.50	.00	1
181.58	181.58	.00	1
241.50	241.50	.00	1

Time = 2520. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 2520. = .130

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.05

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.13	21.42	6.50	5.85	5.85	6
60.02	58.61	21.35	6.49	5.84	5.84	6
59.45	58.10	21.27	6.47	5.82	5.82	6
58.89	57.58	21.20	6.46	5.81	5.81	6
58.33	57.07	21.12	6.44	5.79	5.80	6
57.76	56.56	21.05	6.43	5.78	5.78	6
57.20	56.04	20.97	6.42	5.77	5.77	6
56.64	55.53	20.90	6.40	5.75	5.76	6
56.08	55.02	20.82	6.39	5.74	5.74	6
56.08	55.02	20.82	4.51	3.98	3.98	5
54.82	53.88	20.59	4.44	3.91	3.91	5
53.56	52.75	20.36	4.38	3.85	3.85	5
52.32	51.63	20.12	4.32	3.78	3.79	5
51.10	50.53	19.89	4.25	3.72	3.72	5
49.88	49.44	19.66	4.19	3.66	3.66	5
48.69	48.37	19.43	4.13	3.59	3.59	5
48.69	48.37	19.43	1.93	1.90	1.90	4
46.69	46.40	18.75	1.92	1.88	1.88	4
44.70	44.43	18.06	1.91	1.87	1.86	4
42.72	42.48	17.38	1.89	1.85	1.84	4
40.75	40.53	16.70	1.88	1.84	1.82	4
38.79	38.60	16.01	1.86	1.82	1.80	4
36.85	36.68	15.33	1.84	1.81	1.78	4
34.91	34.76	14.65	1.82	1.79	1.76	4
33.00	32.86	13.97	1.80	1.77	1.74	4
31.09	30.98	13.28	1.78	1.75	1.71	4
31.09	30.98	13.28	1.47	1.46	1.44	3
29.70	29.59	12.72	1.46	1.45	1.43	3
28.32	28.22	12.16	1.45	1.44	1.42	3
26.94	26.85	11.59	1.44	1.43	1.41	3
25.57	25.48	11.03	1.43	1.42	1.40	3
24.21	24.12	10.47	1.42	1.41	1.39	3
22.84	22.77	9.90	1.41	1.40	1.38	3
21.49	21.42	9.34	1.40	1.39	1.37	3
20.14	20.07	8.78	1.39	1.38	1.36	3
18.80	18.74	8.21	1.38	1.37	1.35	3
18.80	18.74	8.21	1.34	1.33	1.31	2
16.88	16.82	7.39	1.33	1.32	1.30	2
14.97	14.92	6.57	1.32	1.31	1.29	2
13.07	13.03	5.75	1.31	1.30	1.28	2
11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2

1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.13	455.81	214.30	241.50	241.50	.00	6
58.61	492.70	218.92	273.77	273.77	.00	6
58.10	529.51	223.54	305.97	305.97	.00	6
57.58	566.27	228.16	338.10	338.10	.00	6
57.07	602.96	232.78	370.17	370.17	.00	6
56.56	639.58	237.40	402.17	402.17	.00	6
56.04	676.13	242.03	434.11	434.11	.00	6
55.53	712.62	246.65	465.98	465.98	.00	6
55.02	749.05	251.27	497.78	497.78	.00	6
55.02	749.05	251.27	497.78	497.78	.00	5
53.88	846.32	277.02	569.30	569.30	.00	5
52.75	942.66	302.77	639.90	639.90	.00	5
51.63	1038.08	328.52	709.57	709.57	.00	5
50.53	1132.58	354.27	778.31	778.31	.00	5
49.44	1226.15	380.02	846.14	846.14	.00	5
48.37	1318.80	405.77	913.04	913.04	.00	5
48.37	1318.80	405.77	913.04	913.04	.00	4
46.40	1517.80	481.63	1036.17	1036.17	.00	4
44.43	1716.21	541.38	1174.83	1158.73	16.10	4
42.48	1914.00	593.90	1320.10	1280.66	39.44	4
40.53	2111.16	647.00	1464.16	1401.96	62.20	4
38.60	2307.68	701.20	1606.49	1522.62	83.86	4
36.68	2503.55	757.38	1746.17	1642.63	103.54	4
34.76	2698.73	816.47	1882.25	1761.95	120.31	4
32.86	2893.17	879.82	2013.36	1880.53	132.82	4
30.98	3086.83	949.30	2137.53	1998.33	139.19	4
30.98	3086.83	949.30	2137.53	1998.33	139.19	3
29.59	3234.95	1005.04	2229.90	2084.59	145.31	3
28.22	3382.71	1068.78	2313.93	2170.49	143.44	3
26.85	3530.11	1131.47	2398.64	2256.04	142.60	3
25.48	3677.17	1193.29	2483.88	2341.24	142.65	3
24.12	3823.88	1254.07	2569.81	2426.09	143.72	3
22.77	3970.25	1313.97	2656.27	2510.60	145.67	3
21.42	4116.29	1373.16	2743.12	2594.78	148.34	3
20.07	4261.99	1431.64	2830.35	2678.62	151.73	3
18.74	4407.37	1489.35	2918.02	2762.14	155.87	3
18.74	4407.37	1489.35	2918.02	2762.14	155.87	2
16.82	4612.71	1567.29	3045.42	2881.38	164.04	2
14.92	4817.55	1647.43	3170.12	3000.13	169.99	2
13.03	5021.90	1729.85	3292.05	3118.38	173.67	2
11.14	5225.74	1814.05	3411.68	3236.12	175.56	2
9.26	5429.05	1900.49	3528.56	3353.33	175.23	2
7.39	5631.82	1989.73	3642.09	3470.01	172.09	2
5.53	5834.04	2119.81	3714.23	3586.13	128.10	2
3.68	6035.71	2252.22	3783.49	3701.70	81.79	2
1.84	6236.85	2379.78	3857.06	3816.74	40.32	2
.00	6437.47	2502.98	3934.49	3931.26	3.23	2

Time = 2880. Degree of Consolidation = 80.%

Total Settlement = 1.454

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 2880. = 1.451

Settlement caused by Secondary Compression at time 2880. = .003

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.50	241.50	.00	1

Time = 2880. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 2880. = .130

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.02

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.10	21.42	6.50	5.85	5.85	6
60.02	58.59	21.35	6.49	5.83	5.84	6
59.45	58.07	21.27	6.47	5.82	5.82	6
58.89	57.56	21.20	6.46	5.81	5.81	6
58.33	57.04	21.12	6.44	5.79	5.80	6
57.76	56.53	21.05	6.43	5.78	5.78	6
57.20	56.02	20.97	6.42	5.77	5.77	6
56.64	55.51	20.90	6.40	5.75	5.76	6
56.08	55.00	20.82	6.39	5.74	5.74	6
56.08	55.00	20.82	4.51	3.97	3.98	5
54.82	53.85	20.59	4.44	3.91	3.91	5

53.56	52.72	20.36	4.38	3.85	3.85	5
52.32	51.60	20.12	4.32	3.78	3.79	5
51.10	50.50	19.89	4.25	3.72	3.72	5
49.88	49.42	19.66	4.19	3.66	3.66	5
48.69	48.34	19.43	4.13	3.59	3.59	5
48.69	48.34	19.43	1.93	1.90	1.90	4
46.69	46.37	18.75	1.92	1.88	1.88	4
44.70	44.41	18.06	1.91	1.87	1.86	4
42.72	42.45	17.38	1.89	1.85	1.84	4
40.75	40.51	16.70	1.88	1.84	1.82	4
38.79	38.58	16.01	1.86	1.82	1.80	4
36.85	36.66	15.33	1.84	1.81	1.78	4
34.91	34.75	14.65	1.82	1.79	1.76	4
33.00	32.85	13.97	1.80	1.77	1.74	4
31.09	30.96	13.28	1.78	1.75	1.71	4
31.09	30.96	13.28	1.47	1.46	1.44	3
29.70	29.58	12.72	1.46	1.45	1.43	3
28.32	28.21	12.16	1.45	1.44	1.42	3
26.94	26.84	11.59	1.44	1.43	1.41	3
25.57	25.47	11.03	1.43	1.42	1.40	3
24.21	24.11	10.47	1.42	1.41	1.39	3
22.84	22.76	9.90	1.41	1.40	1.38	3
21.49	21.41	9.34	1.40	1.39	1.37	3
20.14	20.07	8.78	1.39	1.38	1.36	3
18.80	18.73	8.21	1.38	1.37	1.35	3
18.80	18.73	8.21	1.34	1.33	1.31	2
16.88	16.82	7.39	1.33	1.32	1.30	2
14.97	14.92	6.57	1.32	1.31	1.29	2
13.07	13.02	5.75	1.31	1.30	1.28	2
11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.10	455.81	214.30	241.50	241.50	.00	6
58.59	492.69	218.92	273.77	273.77	.00	6
58.07	529.50	223.54	305.96	305.96	.00	6
57.56	566.25	228.16	338.08	338.08	.00	6
57.04	602.93	232.78	370.14	370.14	.00	6
56.53	639.54	237.40	402.14	402.14	.00	6
56.02	676.09	242.03	434.07	434.07	.00	6
55.51	712.58	246.65	465.93	465.93	.00	6
55.00	748.99	251.27	497.73	497.73	.00	6
55.00	748.99	251.27	497.73	497.73	.00	5
53.85	846.25	277.02	569.23	569.23	.00	5
52.72	942.58	302.77	639.82	639.82	.00	5
51.60	1037.99	328.52	709.48	709.48	.00	5
50.50	1132.48	354.27	778.21	778.21	.00	5
49.42	1226.04	380.02	846.03	846.03	.00	5
48.34	1318.68	405.77	912.91	912.91	.00	5
48.34	1318.68	405.77	912.91	912.91	.00	4
46.37	1517.68	481.63	1036.05	1036.05	.00	4
44.41	1716.08	543.12	1172.96	1158.60	14.37	4
42.45	1913.84	597.51	1316.33	1280.50	35.83	4
40.51	2110.95	652.42	1458.53	1401.74	56.79	4
38.58	2307.39	708.38	1599.02	1522.33	76.68	4

36.66	2503.16	766.10	1737.06	1642.24	94.82	4
34.75	2698.23	826.54	1871.68	1761.45	110.24	4
32.85	2892.55	891.14	2001.41	1879.91	121.50	4
30.96	3086.06	962.26	2123.80	1997.56	126.24	4
30.96	3086.06	962.26	2123.80	1997.56	126.24	3
29.58	3234.09	1019.49	2214.60	2083.74	130.87	3
28.21	3381.78	1082.30	2299.47	2169.56	129.91	3
26.84	3529.11	1144.13	2384.98	2255.03	129.95	3
25.47	3676.09	1205.13	2470.96	2340.16	130.80	3
24.11	3822.74	1265.15	2557.59	2424.95	132.65	3
22.76	3969.05	1324.33	2644.72	2509.40	135.32	3
21.41	4115.03	1382.84	2732.19	2593.52	138.66	3
20.07	4260.68	1440.81	2819.88	2677.32	142.56	3
18.73	4406.01	1498.04	2907.98	2760.79	147.19	3
18.73	4406.01	1498.04	2907.98	2760.79	147.19	2
16.82	4611.30	1575.00	3036.30	2879.97	156.33	2
14.92	4816.10	1654.16	3161.94	2998.68	163.26	2
13.02	5020.41	1735.91	3284.50	3116.89	167.61	2
11.14	5224.21	1819.46	3404.75	3234.59	170.16	2
9.26	5427.49	1905.22	3522.27	3351.78	170.49	2
7.39	5630.24	1993.77	3636.47	3468.42	168.05	2
5.53	5832.43	2124.65	3707.78	3584.52	123.26	2
3.68	6034.08	2255.41	3778.67	3700.07	78.60	2
1.84	6235.21	2381.41	3853.80	3815.10	38.70	2
.00	6435.83	2503.10	3932.73	3929.62	3.10	2

Time = 3240. Degree of Consolidation = 82.%

Total Settlement = 1.480

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 3240. = 1.475

Settlement caused by Secondary Compression at time 3240. = .005

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.00	3.87	2.02
3.00	2.89	1.52
2.00	1.92	1.01
1.00	.96	.51
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.87	.00	.00
2.89	114.77	53.58
1.92	228.65	107.15
.96	342.31	160.73
.00	455.81	214.30

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
61.19	61.19	.00	1
121.50	121.50	.00	1
181.58	181.58	.00	1
241.50	241.50	.00	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 3240. = .130

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .99

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.08	21.42	6.50	5.85	5.85	6
60.02	58.56	21.35	6.49	5.83	5.84	6
59.45	58.04	21.27	6.47	5.82	5.82	6
58.89	57.53	21.20	6.46	5.81	5.81	6
58.33	57.02	21.12	6.44	5.79	5.80	6
57.76	56.50	21.05	6.43	5.78	5.78	6
57.20	55.99	20.97	6.42	5.76	5.77	6
56.64	55.48	20.90	6.40	5.75	5.76	6
56.08	54.97	20.82	6.39	5.74	5.74	6
56.08	54.97	20.82	4.51	3.97	3.98	5
54.82	53.83	20.59	4.44	3.91	3.91	5
53.56	52.70	20.36	4.38	3.85	3.85	5
52.32	51.58	20.12	4.32	3.78	3.79	5
51.10	50.48	19.89	4.25	3.72	3.72	5
49.88	49.39	19.66	4.19	3.65	3.66	5
48.69	48.32	19.43	4.13	3.59	3.59	5
48.69	48.32	19.43	1.93	1.90	1.90	4
46.69	46.35	18.75	1.92	1.88	1.88	4
44.70	44.38	18.06	1.91	1.87	1.86	4
42.72	42.43	17.38	1.89	1.85	1.84	4
40.75	40.49	16.70	1.88	1.84	1.82	4
38.79	38.56	16.01	1.86	1.82	1.80	4
36.85	36.64	15.33	1.84	1.80	1.78	4
34.91	34.73	14.65	1.82	1.79	1.76	4
33.00	32.83	13.97	1.80	1.77	1.74	4
31.09	30.95	13.28	1.78	1.75	1.71	4
31.09	30.95	13.28	1.47	1.45	1.44	3
29.70	29.57	12.72	1.46	1.44	1.43	3
28.32	28.19	12.16	1.45	1.43	1.42	3
26.94	26.82	11.59	1.44	1.42	1.41	3
25.57	25.46	11.03	1.43	1.42	1.40	3
24.21	24.10	10.47	1.42	1.41	1.39	3
22.84	22.75	9.90	1.41	1.40	1.38	3
21.49	21.40	9.34	1.40	1.39	1.37	3
20.14	20.06	8.78	1.39	1.38	1.36	3
18.80	18.73	8.21	1.38	1.37	1.35	3
18.80	18.73	8.21	1.34	1.33	1.31	2
16.88	16.82	7.39	1.33	1.32	1.30	2
14.97	14.92	6.57	1.32	1.31	1.29	2
13.07	13.02	5.75	1.31	1.30	1.28	2

11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.08	455.81	214.30	241.50	241.50	.00	6
58.56	492.68	218.92	273.76	273.76	.00	6
58.04	529.49	223.54	305.94	305.94	.00	6
57.53	566.23	228.16	338.06	338.06	.00	6
57.02	602.90	232.78	370.11	370.11	.00	6
56.50	639.50	237.40	402.10	402.10	.00	6
55.99	676.04	242.03	434.02	434.02	.00	6
55.48	712.52	246.65	465.87	465.87	.00	6
54.97	748.93	251.27	497.66	497.66	.00	6
54.97	748.93	251.27	497.66	497.66	.00	5
53.83	846.18	277.02	569.16	569.16	.00	5
52.70	942.51	302.77	639.74	639.74	.00	5
51.58	1037.91	328.52	709.39	709.39	.00	5
50.48	1132.38	354.27	778.12	778.12	.00	5
49.39	1225.94	380.02	845.92	845.92	.00	5
48.32	1318.56	405.77	912.80	912.80	.00	5
48.32	1318.56	405.77	912.80	912.80	.00	4
46.35	1517.56	481.63	1035.94	1035.94	.00	4
44.38	1715.96	544.69	1171.26	1158.47	12.79	4
42.43	1913.69	600.66	1313.02	1280.34	32.68	4
40.49	2110.75	657.14	1453.60	1401.54	52.06	4
38.56	2307.13	714.69	1592.44	1522.06	70.37	4
36.64	2502.81	774.03	1728.78	1641.89	86.89	4
34.73	2697.77	836.12	1861.65	1760.99	100.66	4
32.83	2891.97	902.42	1989.55	1879.33	110.22	4
30.95	3085.33	975.41	2109.92	1996.84	113.08	4
30.95	3085.33	975.41	2109.92	1996.84	113.08	3
29.57	3233.28	1034.39	2198.89	2082.93	115.96	3
28.19	3380.88	1096.65	2284.24	2168.67	115.57	3
26.82	3528.14	1157.97	2370.17	2254.06	116.11	3
25.46	3675.05	1218.26	2456.79	2339.11	117.67	3
24.10	3821.62	1277.61	2544.01	2423.83	120.18	3
22.75	3967.86	1336.18	2631.68	2508.21	123.47	3
21.40	4113.78	1394.11	2719.67	2592.27	127.40	3
20.06	4259.37	1451.56	2807.81	2676.00	131.81	3
18.73	4404.64	1508.31	2896.33	2759.41	136.91	3
18.73	4404.64	1508.31	2896.33	2759.41	136.91	2
16.82	4609.86	1584.30	3025.56	2878.54	147.03	2
14.92	4814.61	1662.49	3152.13	2997.19	154.94	2
13.02	5018.87	1743.26	3275.61	3115.35	160.26	2
11.14	5222.63	1825.96	3396.68	3233.01	163.66	2
9.26	5425.88	1910.85	3515.03	3350.16	164.87	2
7.39	5628.59	1998.49	3630.10	3466.77	163.33	2
5.53	5830.76	2130.16	3700.59	3582.85	117.75	2
3.68	6032.39	2259.05	3773.34	3698.38	74.96	2
1.84	6233.51	2383.26	3850.25	3813.40	36.85	2
.00	6434.12	2503.25	3930.88	3927.91	2.96	2

Time = 3650. Degree of Consolidation = 83.%

Total Settlement = 1.507

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 3650. = 1.500

Settlement caused by Secondary Compression at time 3650. = .007

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.50	241.50	.00	1

Time = 3650. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 3650. = .130

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .96

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.04	21.42	6.50	5.85	5.85	6
60.02	58.52	21.35	6.49	5.83	5.84	6
59.45	58.01	21.27	6.47	5.82	5.82	6
58.89	57.49	21.20	6.46	5.80	5.81	6
58.33	56.98	21.12	6.44	5.79	5.80	6
57.76	56.47	21.05	6.43	5.77	5.78	6

57.20	55.95	20.97	6.42	5.76	5.77	6
56.64	55.44	20.90	6.40	5.75	5.76	6
56.08	54.93	20.82	6.39	5.73	5.74	6
56.08	54.93	20.82	4.51	3.97	3.98	5
54.82	53.79	20.59	4.44	3.91	3.91	5
53.56	52.66	20.36	4.38	3.85	3.85	5
52.32	51.54	20.12	4.32	3.78	3.79	5
51.10	50.44	19.89	4.25	3.72	3.72	5
49.88	49.35	19.66	4.19	3.65	3.66	5
48.69	48.28	19.43	4.13	3.59	3.59	5
48.69	48.28	19.43	1.93	1.90	1.90	4
46.69	46.31	18.75	1.92	1.88	1.88	4
44.70	44.34	18.06	1.91	1.87	1.86	4
42.72	42.39	17.38	1.89	1.85	1.84	4
40.75	40.45	16.70	1.88	1.83	1.82	4
38.79	38.52	16.01	1.86	1.82	1.80	4
36.85	36.60	15.33	1.84	1.80	1.78	4
34.91	34.70	14.65	1.82	1.78	1.76	4
33.00	32.80	13.97	1.80	1.76	1.74	4
31.09	30.92	13.28	1.78	1.74	1.71	4
31.09	30.92	13.28	1.47	1.45	1.44	3
29.70	29.54	12.72	1.46	1.44	1.43	3
28.32	28.17	12.16	1.45	1.43	1.42	3
26.94	26.81	11.59	1.44	1.42	1.41	3
25.57	25.44	11.03	1.43	1.41	1.40	3
24.21	24.09	10.47	1.42	1.40	1.39	3
22.84	22.74	9.90	1.41	1.39	1.38	3
21.49	21.39	9.34	1.40	1.38	1.37	3
20.14	20.05	8.78	1.39	1.37	1.36	3
18.80	18.72	8.21	1.38	1.37	1.35	3
18.80	18.72	8.21	1.34	1.33	1.31	2
16.88	16.81	7.39	1.33	1.32	1.30	2
14.97	14.91	6.57	1.32	1.31	1.29	2
13.07	13.02	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.84	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.04	455.81	214.30	241.50	241.50	.00	6
58.52	492.68	218.92	273.75	273.75	.00	6
58.01	529.47	223.54	305.92	305.92	.00	6
57.49	566.19	228.16	338.03	338.03	.00	6
56.98	602.85	232.78	370.06	370.06	.00	6
56.47	639.44	237.40	402.04	402.04	.00	6
55.95	675.97	242.03	433.94	433.94	.00	6
55.44	712.43	246.65	465.78	465.78	.00	6
54.93	748.82	251.27	497.56	497.56	.00	6
54.93	748.82	251.27	497.56	497.56	.00	5
53.79	846.08	277.02	569.06	569.06	.00	5
52.66	942.40	302.77	639.64	639.64	.00	5
51.54	1037.80	328.52	709.29	709.29	.00	5
50.44	1132.28	354.27	778.01	778.01	.00	5
49.35	1225.83	380.02	845.82	845.82	.00	5
48.28	1318.46	405.77	912.69	912.69	.00	5
48.28	1318.46	405.77	912.69	912.69	.00	4

46.31	1517.46	481.63	1035.83	1035.83	.00	4
44.34	1715.84	546.56	1169.28	1158.36	10.93	4
42.39	1913.54	604.48	1309.06	1280.20	28.86	4
40.45	2110.54	663.01	1447.53	1401.34	46.20	4
38.52	2306.84	722.75	1584.09	1521.78	62.31	4
36.60	2502.41	784.33	1718.08	1641.49	76.59	4
34.70	2697.24	848.79	1848.45	1760.46	87.99	4
32.80	2891.27	917.75	1973.52	1878.63	94.89	4
30.92	3084.43	993.88	2090.55	1995.94	94.62	4
30.92	3084.43	993.88	2090.55	1995.94	94.62	3
29.54	3232.26	1056.01	2176.25	2081.91	94.34	3
28.17	3379.74	1117.86	2261.88	2167.53	94.35	3
26.81	3526.88	1178.51	2348.37	2252.80	95.57	3
25.44	3673.67	1238.11	2435.56	2337.74	97.82	3
24.09	3820.14	1296.84	2523.30	2422.35	100.95	3
22.74	3966.27	1354.84	2611.44	2506.62	104.81	3
21.39	4112.09	1412.24	2699.85	2590.58	109.27	3
20.05	4257.58	1468.85	2788.72	2674.21	114.51	3
18.72	4402.75	1524.83	2877.92	2757.53	120.39	3
18.72	4402.75	1524.83	2877.92	2757.53	120.39	2
16.81	4607.88	1599.32	3008.56	2876.55	132.01	2
14.91	4812.54	1676.00	3136.54	2995.12	141.42	2
13.02	5016.72	1755.27	3261.45	3113.20	148.25	2
11.13	5220.41	1836.66	3383.75	3230.79	152.96	2
9.26	5423.59	1920.22	3503.38	3347.88	155.50	2
7.39	5626.25	2009.44	3616.81	3464.44	152.37	2
5.53	5828.38	2139.17	3689.21	3580.47	108.74	2
3.68	6029.98	2264.99	3764.99	3695.97	69.02	2
1.84	6231.08	2386.29	3844.79	3810.97	33.82	2
.00	6431.69	2503.48	3928.21	3925.48	2.73	2

Time = 4320. Degree of Consolidation = 86.%

Total Settlement = 1.546

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 4320. = 1.538

Settlement caused by Secondary Compression at time 4320. = .008

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.00	3.87	2.02
3.00	2.89	1.52
2.00	1.92	1.01
1.00	.96	.51
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.87	.00	.00
2.89	114.77	53.58

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
61.19	61.19	.00	1

1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.50	241.50	.00	1

Time = 4320. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 4320. = .130

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .92

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.00	21.42	6.50	5.85	5.85	6
60.02	58.48	21.35	6.49	5.83	5.84	6
59.45	57.97	21.27	6.47	5.81	5.82	6
58.89	57.46	21.20	6.46	5.80	5.81	6
58.33	56.94	21.12	6.44	5.79	5.80	6
57.76	56.43	21.05	6.43	5.77	5.78	6
57.20	55.92	20.97	6.42	5.76	5.77	6
56.64	55.41	20.90	6.40	5.74	5.76	6
56.08	54.90	20.82	6.39	5.73	5.74	6
56.08	54.90	20.82	4.51	3.97	3.98	5
54.82	53.75	20.59	4.44	3.91	3.91	5
53.56	52.62	20.36	4.38	3.85	3.85	5
52.32	51.51	20.12	4.32	3.78	3.79	5
51.10	50.41	19.89	4.25	3.72	3.72	5
49.88	49.32	19.66	4.19	3.65	3.66	5
48.69	48.25	19.43	4.13	3.59	3.59	5
48.69	48.25	19.43	1.93	1.90	1.90	4
46.69	46.27	18.75	1.92	1.88	1.88	4
44.70	44.31	18.06	1.91	1.87	1.86	4
42.72	42.36	17.38	1.89	1.85	1.84	4
40.75	40.42	16.70	1.88	1.83	1.82	4
38.79	38.49	16.01	1.86	1.82	1.80	4
36.85	36.57	15.33	1.84	1.80	1.78	4
34.91	34.67	14.65	1.82	1.78	1.76	4
33.00	32.78	13.97	1.80	1.76	1.74	4
31.09	30.90	13.28	1.78	1.74	1.71	4
31.09	30.90	13.28	1.47	1.45	1.44	3
29.70	29.52	12.72	1.46	1.44	1.43	3
28.32	28.15	12.16	1.45	1.43	1.42	3
26.94	26.79	11.59	1.44	1.42	1.41	3
25.57	25.43	11.03	1.43	1.41	1.40	3
24.21	24.07	10.47	1.42	1.40	1.39	3
22.84	22.72	9.90	1.41	1.39	1.38	3
21.49	21.38	9.34	1.40	1.38	1.37	3
20.14	20.04	8.78	1.39	1.37	1.36	3

18.80	18.71	8.21	1.38	1.36	1.35	3
18.80	18.71	8.21	1.34	1.33	1.31	2
16.88	16.80	7.39	1.33	1.32	1.30	2
14.97	14.90	6.57	1.32	1.31	1.29	2
13.07	13.01	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.00	455.81	214.30	241.50	241.50	.00	6
58.48	492.67	218.92	273.74	273.74	.00	6
57.97	529.44	223.54	305.90	305.90	.00	6
57.46	566.15	228.16	337.99	337.99	.00	6
56.94	602.79	232.78	370.01	370.01	.00	6
56.43	639.37	237.40	401.97	401.97	.00	6
55.92	675.89	242.03	433.86	433.86	.00	6
55.41	712.33	246.65	465.69	465.69	.00	6
54.90	748.71	251.27	497.45	497.45	.00	6
54.90	748.71	251.27	497.45	497.45	.00	5
53.75	845.96	277.02	568.95	568.95	.00	5
52.62	942.29	302.77	639.52	639.52	.00	5
51.51	1037.69	328.52	709.18	709.18	.00	5
50.41	1132.17	354.27	777.90	777.90	.00	5
49.32	1225.72	380.02	845.70	845.70	.00	5
48.25	1318.35	405.77	912.58	912.58	.00	5
48.25	1318.35	405.77	912.58	912.58	.00	4
46.27	1517.35	481.63	1035.72	1035.72	.00	4
44.31	1715.72	548.06	1167.66	1158.24	9.42	4
42.36	1913.39	607.63	1305.77	1280.05	25.72	4
40.42	2110.35	667.94	1442.40	1401.15	41.26	4
38.49	2306.58	729.46	1577.12	1521.51	55.60	4
36.57	2502.06	793.02	1709.04	1641.14	67.90	4
34.67	2696.76	859.76	1837.00	1759.98	77.02	4
32.78	2890.65	931.30	1959.35	1878.01	81.34	4
30.90	3083.64	1009.69	2073.94	1995.14	78.80	4
30.90	3083.64	1009.69	2073.94	1995.14	78.80	3
29.52	3231.37	1074.00	2157.37	2081.01	76.36	3
28.15	3378.75	1136.58	2242.16	2166.53	75.63	3
26.79	3525.77	1197.66	2328.12	2251.70	76.42	3
25.43	3672.46	1257.39	2415.07	2336.53	78.54	3
24.07	3818.82	1315.95	2502.86	2421.03	81.84	3
22.72	3964.85	1373.49	2591.36	2505.20	86.16	3
21.38	4110.56	1430.16	2680.40	2589.05	91.35	3
20.04	4255.95	1486.10	2769.85	2672.58	97.26	3
18.71	4401.03	1541.45	2859.58	2755.80	103.77	3
18.71	4401.03	1541.45	2859.58	2755.80	103.78	2
16.80	4606.06	1614.68	2991.37	2874.73	116.64	2
14.90	4810.63	1690.14	3120.49	2993.21	127.29	2
13.01	5014.73	1768.18	3246.55	3111.21	135.34	2
11.13	5218.34	1848.18	3370.17	3228.72	141.44	2
9.25	5421.46	1930.32	3491.14	3345.74	145.40	2
7.39	5624.06	2022.04	3602.02	3462.25	139.77	2
5.53	5826.14	2148.85	3677.29	3578.23	99.06	2
3.68	6027.71	2271.38	3756.33	3693.70	62.63	2
1.83	6228.79	2389.54	3839.25	3808.68	30.57	2

.00	6429.39	2503.73	3925.66	3923.18	2.48	2

Time = 5040. Degree of Consolidation = 88.%

Total Settlement = 1.583

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 5040. = 1.573

Settlement caused by Secondary Compression at time 5040. = .010

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.50	241.50	.00	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 5040. = .130

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .89

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.98	21.42	6.50	5.85	5.85	6

60.02	58.47	21.35	6.49	5.83	5.84	6
59.45	57.95	21.27	6.47	5.81	5.82	6
58.89	57.44	21.20	6.46	5.80	5.81	6
58.33	56.92	21.12	6.44	5.78	5.80	6
57.76	56.41	21.05	6.43	5.77	5.78	6
57.20	55.90	20.97	6.42	5.76	5.77	6
56.64	55.39	20.90	6.40	5.74	5.76	6
56.08	54.88	20.82	6.39	5.73	5.74	6
56.08	54.88	20.82	4.51	3.97	3.98	5
54.82	53.74	20.59	4.44	3.91	3.91	5
53.56	52.60	20.36	4.38	3.85	3.85	5
52.32	51.49	20.12	4.32	3.78	3.79	5
51.10	50.39	19.89	4.25	3.72	3.72	5
49.88	49.30	19.66	4.19	3.65	3.66	5
48.69	48.23	19.43	4.13	3.59	3.59	5
48.69	48.23	19.43	1.93	1.90	1.90	4
46.69	46.26	18.75	1.92	1.88	1.88	4
44.70	44.29	18.06	1.91	1.87	1.86	4
42.72	42.34	17.38	1.89	1.85	1.84	4
40.75	40.40	16.70	1.88	1.83	1.82	4
38.79	38.47	16.01	1.86	1.81	1.80	4
36.85	36.56	15.33	1.84	1.80	1.78	4
34.91	34.65	14.65	1.82	1.78	1.76	4
33.00	32.76	13.97	1.80	1.76	1.74	4
31.09	30.89	13.28	1.78	1.74	1.71	4
31.09	30.89	13.28	1.47	1.45	1.44	3
29.70	29.51	12.72	1.46	1.44	1.43	3
28.32	28.14	12.16	1.45	1.43	1.42	3
26.94	26.78	11.59	1.44	1.42	1.41	3
25.57	25.42	11.03	1.43	1.41	1.40	3
24.21	24.06	10.47	1.42	1.40	1.39	3
22.84	22.72	9.90	1.41	1.39	1.38	3
21.49	21.37	9.34	1.40	1.38	1.37	3
20.14	20.04	8.78	1.39	1.37	1.36	3
18.80	18.70	8.21	1.38	1.36	1.35	3
18.80	18.70	8.21	1.34	1.32	1.31	2
16.88	16.80	7.39	1.33	1.32	1.30	2
14.97	14.90	6.57	1.32	1.31	1.29	2
13.07	13.01	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.98	455.81	214.30	241.50	241.50	.00	6
58.47	492.66	218.92	273.74	273.74	.00	6
57.95	529.43	223.54	305.88	305.88	.00	6
57.44	566.13	228.16	337.96	337.96	.00	6
56.92	602.76	232.78	369.98	369.98	.00	6
56.41	639.33	237.40	401.93	401.93	.00	6
55.90	675.84	242.03	433.81	433.81	.00	6
55.39	712.27	246.65	465.63	465.63	.00	6
54.88	748.64	251.27	497.38	497.38	.00	6
54.88	748.64	251.27	497.38	497.38	.00	5
53.74	845.90	277.02	568.88	568.88	.00	5
52.60	942.22	302.77	639.46	639.46	.00	5

51.49	1037.62	328.52	709.11	709.11	.00	5
50.39	1132.10	354.27	777.83	777.83	.00	5
49.30	1225.65	380.02	845.64	845.64	.00	5
48.23	1318.28	405.77	912.51	912.51	.00	5
48.23	1318.28	405.77	912.51	912.51	.00	4
46.26	1517.28	481.63	1035.66	1035.66	.00	4
44.29	1715.65	548.86	1166.79	1158.17	8.62	4
42.34	1913.31	609.31	1304.00	1279.96	24.04	4
40.40	2110.24	670.46	1439.77	1401.03	38.74	4
38.47	2306.43	732.92	1573.51	1521.37	52.14	4
36.56	2501.86	797.48	1704.39	1640.94	63.44	4
34.65	2696.51	865.22	1831.29	1759.73	71.55	4
32.76	2890.32	938.07	1952.25	1877.68	74.57	4
30.89	3083.22	1017.16	2066.06	1994.73	71.34	4
30.89	3083.22	1017.16	2066.06	1994.73	71.34	3
29.51	3230.91	1082.23	2148.68	2080.56	68.12	3
28.14	3378.24	1145.28	2232.96	2166.03	66.93	3
26.78	3525.22	1206.50	2318.72	2251.15	67.57	3
25.42	3671.86	1266.28	2405.58	2335.93	69.65	3
24.06	3818.16	1324.88	2493.29	2420.37	72.91	3
22.72	3964.14	1382.46	2581.68	2504.49	77.19	3
21.37	4109.80	1439.17	2670.63	2588.29	82.34	3
20.04	4255.14	1495.16	2759.98	2671.78	88.21	3
18.70	4400.17	1550.35	2849.82	2754.95	94.87	3
18.70	4400.17	1550.35	2849.82	2754.95	94.87	2
16.80	4605.15	1623.15	2981.99	2873.82	108.17	2
14.90	4809.67	1698.19	3111.47	2992.25	119.23	2
13.01	5013.72	1775.70	3238.02	3110.20	127.82	2
11.13	5217.29	1854.92	3362.37	3227.67	134.70	2
9.25	5420.36	1936.26	3484.10	3344.65	139.45	2
7.39	5622.93	2029.53	3593.40	3461.12	132.28	2
5.53	5824.99	2154.70	3670.29	3577.08	93.21	2
3.68	6026.54	2275.24	3751.30	3692.53	58.77	2
1.83	6227.60	2391.50	3836.10	3807.49	28.61	2
.00	6428.20	2503.88	3924.32	3921.99	2.33	2

Time = 5475. Degree of Consolidation = 89.%

Total Settlement = 1.602

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 5475. = 1.591

Settlement caused by Secondary Compression at time 5475. = .011

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

XI	Total Stress	Effective Stress	Total Pore Pressure	Static Pore Pressure	Excess Pore Pressure	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.50	241.50	.00	1

Time = 5475. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 5475. = .130

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .87

**********Current Conditions in Compressible Foundation**********

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.94	21.42	6.50	5.85	5.85	6
60.02	58.43	21.35	6.49	5.82	5.84	6
59.45	57.91	21.27	6.47	5.81	5.82	6
58.89	57.40	21.20	6.46	5.79	5.81	6
58.33	56.89	21.12	6.44	5.78	5.80	6
57.76	56.37	21.05	6.43	5.77	5.78	6
57.20	55.86	20.97	6.42	5.75	5.77	6
56.64	55.35	20.90	6.40	5.74	5.76	6
56.08	54.85	20.82	6.39	5.72	5.74	6
56.08	54.85	20.82	4.51	3.97	3.98	5
54.82	53.70	20.59	4.44	3.91	3.91	5
53.56	52.57	20.36	4.38	3.85	3.85	5
52.32	51.45	20.12	4.32	3.78	3.79	5
51.10	50.35	19.89	4.25	3.72	3.72	5
49.88	49.26	19.66	4.19	3.65	3.66	5
48.69	48.19	19.43	4.13	3.59	3.59	5
48.69	48.19	19.43	1.93	1.90	1.90	4
46.69	46.22	18.75	1.92	1.88	1.88	4
44.70	44.26	18.06	1.91	1.87	1.86	4
42.72	42.31	17.38	1.89	1.85	1.84	4
40.75	40.37	16.70	1.88	1.83	1.82	4
38.79	38.44	16.01	1.86	1.81	1.80	4
36.85	36.52	15.33	1.84	1.79	1.78	4
34.91	34.62	14.65	1.82	1.77	1.76	4
33.00	32.73	13.97	1.80	1.75	1.74	4
31.09	30.86	13.28	1.78	1.73	1.71	4
31.09	30.86	13.28	1.47	1.45	1.44	3
29.70	29.49	12.72	1.46	1.43	1.43	3
28.32	28.12	12.16	1.45	1.42	1.42	3
26.94	26.76	11.59	1.44	1.41	1.41	3

25.57	25.40	11.03	1.43	1.40	1.40	3
24.21	24.05	10.47	1.42	1.39	1.39	3
22.84	22.70	9.90	1.41	1.39	1.38	3
21.49	21.36	9.34	1.40	1.38	1.37	3
20.14	20.02	8.78	1.39	1.37	1.36	3
18.80	18.69	8.21	1.38	1.36	1.35	3
18.80	18.69	8.21	1.34	1.32	1.31	2
16.88	16.79	7.39	1.33	1.31	1.30	2
14.97	14.89	6.57	1.32	1.30	1.29	2
13.07	13.00	5.75	1.31	1.30	1.28	2
11.18	11.12	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.26	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.94	455.81	214.30	241.50	241.50	.00	6
58.43	492.65	218.92	273.72	273.72	.00	6
57.91	529.39	223.54	305.85	305.85	.00	6
57.40	566.07	228.16	337.91	337.91	.00	6
56.89	602.69	232.78	369.90	369.90	.00	6
56.37	639.24	237.40	401.83	401.83	.00	6
55.86	675.72	242.03	433.69	433.69	.00	6
55.35	712.14	246.65	465.49	465.49	.00	6
54.85	748.49	251.27	497.22	497.22	.00	6
54.85	748.49	251.27	497.22	497.22	.00	5
53.70	845.74	277.02	568.72	568.72	.00	5
52.57	942.07	302.77	639.30	639.30	.00	5
51.45	1037.47	328.52	708.95	708.95	.00	5
50.35	1131.94	354.27	777.68	777.68	.00	5
49.26	1225.50	380.02	845.48	845.48	.00	5
48.19	1318.12	405.77	912.36	912.36	.00	5
48.19	1318.12	405.77	912.36	912.36	.00	4
46.22	1517.13	481.63	1035.50	1035.50	.00	4
44.26	1715.49	550.26	1165.23	1158.01	7.23	4
42.31	1913.12	612.23	1300.89	1279.78	21.12	4
40.37	2110.00	674.98	1435.03	1400.80	34.23	4
38.44	2306.13	739.17	1566.97	1521.07	45.90	4
36.52	2501.48	805.58	1695.90	1640.56	55.34	4
34.62	2696.02	875.31	1820.71	1759.24	61.47	4
32.73	2889.70	950.42	1939.28	1877.06	62.22	4
30.86	3082.44	1030.80	2051.64	1993.94	57.70	4
30.86	3082.44	1030.80	2051.64	1993.94	57.70	3
29.49	3230.05	1097.25	2132.80	2079.69	53.11	3
28.12	3377.29	1161.48	2215.81	2165.07	50.73	3
26.76	3524.17	1223.88	2300.29	2250.10	50.19	3
25.40	3670.71	1284.63	2386.08	2334.78	51.30	3
24.05	3816.91	1343.90	2473.01	2419.12	53.89	3
22.70	3962.78	1401.85	2560.93	2503.13	57.80	3
21.36	4108.33	1458.64	2649.70	2586.82	62.87	3
20.02	4253.56	1514.40	2739.16	2670.20	68.96	3
18.69	4398.49	1569.29	2829.19	2753.26	75.93	3
18.69	4398.49	1569.29	2829.19	2753.26	75.93	2
16.79	4603.35	1641.74	2961.61	2872.02	89.59	2
14.89	4807.75	1716.00	3091.75	2990.33	101.42	2
13.00	5011.70	1791.63	3220.07	3108.18	111.89	2
11.12	5215.18	1868.96	3346.22	3225.56	120.66	2

9.25	5418.18	1948.37	3469.81	3342.46	127.35	2
7.38	5620.68	2044.28	3576.39	3458.86	117.53	2
5.53	5822.68	2165.63	3657.05	3574.77	82.28	2
3.68	6024.19	2282.46	3741.73	3690.18	51.55	2
1.83	6225.23	2395.18	3830.06	3805.12	24.93	2
.00	6425.82	2504.17	3921.66	3919.61	2.04	2

Time = 6480. Degree of Consolidation = 91.%

Total Settlement = 1.640

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 6480. = 1.626

Settlement caused by Secondary Compression at time 6480. = .014

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1
2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.50	241.50	.00	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 6480. = .130

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .83

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
60.58	58.92	21.42
60.02	58.40	21.35
59.45	57.89	21.27
58.89	57.38	21.20
58.33	56.86	21.12
57.76	56.35	21.05
57.20	55.84	20.97
56.64	55.33	20.90
56.08	54.82	20.82
56.08	54.82	20.82
54.82	53.68	20.59
53.56	52.55	20.36
52.32	51.43	20.12
51.10	50.33	19.89
49.88	49.24	19.66
48.69	48.17	19.43
48.69	48.17	19.43
46.69	46.20	18.75
44.70	44.23	18.06
42.72	42.28	17.38
40.75	40.34	16.70
38.79	38.42	16.01
36.85	36.50	15.33
34.91	34.60	14.65
33.00	32.71	13.97
31.09	30.84	13.28
31.09	30.84	13.28
29.70	29.47	12.72
28.32	28.10	12.16
26.94	26.74	11.59
25.57	25.39	11.03
24.21	24.03	10.47
22.84	22.69	9.90
21.49	21.35	9.34
20.14	20.01	8.78
18.80	18.68	8.21
18.80	18.68	8.21
16.88	16.78	7.39
14.97	14.89	6.57
13.07	13.00	5.75
11.18	11.12	4.93
9.30	9.25	4.11
7.43	7.38	3.29
5.56	5.53	2.46
3.70	3.68	1.64
1.85	1.83	.82
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
6.50	5.85	5.85	6
6.49	5.82	5.84	6
6.47	5.81	5.82	6
6.46	5.79	5.81	6
6.44	5.78	5.80	6
6.43	5.76	5.78	6
6.42	5.75	5.77	6
6.40	5.74	5.76	6
6.39	5.72	5.74	6
4.51	3.97	3.98	5
4.44	3.91	3.91	5
4.38	3.85	3.85	5
4.32	3.78	3.79	5
4.25	3.72	3.72	5
4.19	3.65	3.66	5
4.13	3.59	3.59	5
1.93	1.90	1.90	4
1.92	1.88	1.88	4
1.91	1.87	1.86	4
1.89	1.85	1.84	4
1.88	1.83	1.82	4
1.86	1.81	1.80	4
1.84	1.79	1.78	4
1.82	1.77	1.76	4
1.80	1.75	1.74	4
1.78	1.73	1.71	4
1.47	1.44	1.44	3
1.46	1.43	1.43	3
1.45	1.42	1.42	3
1.44	1.41	1.41	3
1.43	1.40	1.40	3
1.42	1.39	1.39	3
1.41	1.38	1.38	3
1.40	1.37	1.37	3
1.39	1.37	1.36	3
1.38	1.36	1.35	3
1.34	1.32	1.31	2
1.33	1.31	1.30	2
1.32	1.30	1.29	2
1.31	1.29	1.28	2
1.30	1.28	1.27	2
1.29	1.28	1.26	2
1.28	1.27	1.26	2
1.27	1.26	1.25	2
1.26	1.25	1.24	2
1.25	1.24	1.24	2
1.25	1.23	1.23	2

***** Stresses *****

XI	Total	Effective
58.92	455.81	214.30
58.40	492.64	218.92
57.89	529.38	223.54
57.38	566.05	228.16
56.86	602.65	232.78
56.35	639.19	237.40
55.84	675.67	242.03

***** Pore Pressures *****

Total	Static	Excess	Material
241.50	241.50	.00	6
273.72	273.72	.00	6
305.83	305.83	.00	6
337.89	337.89	.00	6
369.87	369.87	.00	6
401.79	401.79	.00	6
433.64	433.64	.00	6

55.33	712.07	246.65	465.43	465.43	.00	6
54.82	748.41	251.27	497.15	497.15	.00	6
54.82	748.41	251.27	497.15	497.15	.00	5
53.68	845.67	277.02	568.65	568.65	.00	5
52.55	941.99	302.77	639.23	639.23	.00	5
51.43	1037.39	328.52	708.88	708.88	.00	5
50.33	1131.87	354.27	777.60	777.61	.00	5
49.24	1225.42	380.02	845.41	845.41	.00	5
48.17	1318.05	405.77	912.28	912.28	.00	5
48.17	1318.05	405.77	912.28	912.28	.00	4
46.20	1517.06	481.63	1035.43	1035.43	.00	4
44.23	1715.41	551.10	1164.31	1157.93	6.38	4
42.28	1913.03	614.00	1299.02	1279.68	19.34	4
40.34	2109.88	677.78	1432.10	1400.68	31.42	4
38.42	2305.97	742.97	1563.00	1520.91	42.09	4
36.50	2501.27	810.56	1690.71	1640.35	50.36	4
34.60	2695.74	881.72	1814.02	1758.96	55.06	4
32.71	2889.33	958.38	1930.95	1876.69	54.26	4
30.84	3081.97	1039.93	2042.04	1993.47	48.57	4
30.84	3081.97	1039.93	2042.04	1993.47	48.57	3
29.47	3229.53	1107.31	2122.21	2079.17	43.04	3
28.10	3376.71	1172.34	2204.37	2164.49	39.88	3
26.74	3523.53	1235.20	2288.33	2249.45	38.87	3
25.39	3670.00	1296.13	2373.87	2334.07	39.80	3
24.03	3816.14	1355.59	2460.55	2418.35	42.21	3
22.69	3961.94	1413.73	2548.21	2502.29	45.92	3
21.35	4107.42	1470.72	2636.71	2585.92	50.79	3
20.01	4252.59	1526.70	2725.89	2669.22	56.67	3
18.68	4397.44	1581.69	2815.75	2752.21	63.54	3
18.68	4397.44	1581.68	2815.76	2752.21	63.54	2
16.78	4602.22	1653.93	2948.29	2870.90	77.39	2
14.89	4806.56	1727.28	3079.29	2989.14	90.15	2
13.00	5010.44	1801.99	3208.45	3106.92	101.53	2
11.12	5213.86	1878.39	3335.47	3224.24	111.23	2
9.25	5416.80	1956.87	3459.93	3341.08	118.85	2
7.38	5619.25	2055.31	3563.94	3457.44	106.51	2
5.53	5821.21	2173.75	3647.46	3573.30	74.16	2
3.68	6022.70	2287.82	3734.88	3688.69	46.19	2
1.83	6223.72	2397.91	3825.82	3803.62	22.20	2
.00	6424.31	2504.38	3919.93	3918.10	1.83	2

Time = 7300. Degree of Consolidation = 92.%

Total Settlement = 1.664

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 7300. = 1.649

Settlement caused by Secondary Compression at time 7300. = .015

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
4.00	3.87	2.02	.98	.98	.98	1
3.00	2.89	1.52	.98	.92	.92	1

2.00	1.92	1.01	.98	.91	.91	1
1.00	.96	.51	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
3.87	.00	.00	.00	.00	.00	1
2.89	114.77	53.58	61.19	61.19	.00	1
1.92	228.65	107.15	121.50	121.50	.00	1
.96	342.31	160.73	181.58	181.58	.00	1
.00	455.81	214.30	241.50	241.50	.00	1

Time = 7300. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 7300. = .130

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .81

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.88	21.42	6.50	5.85	5.85	6
60.02	58.36	21.35	6.49	5.82	5.84	6
59.45	57.85	21.27	6.47	5.81	5.82	6
58.89	57.34	21.20	6.46	5.79	5.81	6
58.33	56.82	21.12	6.44	5.78	5.80	6
57.76	56.31	21.05	6.43	5.76	5.78	6
57.20	55.80	20.97	6.42	5.75	5.77	6
56.64	55.29	20.90	6.40	5.74	5.76	6
56.08	54.78	20.82	6.39	5.72	5.74	6
56.08	54.78	20.82	4.51	3.97	3.98	5
54.82	53.64	20.59	4.44	3.91	3.91	5
53.56	52.51	20.36	4.38	3.85	3.85	5
52.32	51.39	20.12	4.32	3.78	3.79	5
51.10	50.29	19.89	4.25	3.72	3.72	5
49.88	49.20	19.66	4.19	3.65	3.66	5
48.69	48.13	19.43	4.13	3.59	3.59	5
48.69	48.13	19.43	1.93	1.90	1.90	4
46.69	46.16	18.75	1.92	1.88	1.88	4
44.70	44.19	18.06	1.91	1.87	1.86	4
42.72	42.24	17.38	1.89	1.85	1.84	4
40.75	40.30	16.70	1.88	1.83	1.82	4
38.79	38.38	16.01	1.86	1.81	1.80	4
36.85	36.47	15.33	1.84	1.79	1.78	4
34.91	34.57	14.65	1.82	1.77	1.76	4
33.00	32.68	13.97	1.80	1.75	1.74	4

31.09	30.81	13.28	1.78	1.72	1.71	4
31.09	30.81	13.28	1.47	1.44	1.44	3
29.70	29.44	12.72	1.46	1.43	1.43	3
28.32	28.08	12.16	1.45	1.42	1.42	3
26.94	26.72	11.59	1.44	1.41	1.41	3
25.57	25.36	11.03	1.43	1.40	1.40	3
24.21	24.01	10.47	1.42	1.39	1.39	3
22.84	22.67	9.90	1.41	1.38	1.38	3
21.49	21.33	9.34	1.40	1.37	1.37	3
20.14	20.00	8.78	1.39	1.36	1.36	3
18.80	18.67	8.21	1.38	1.35	1.35	3
18.80	18.67	8.21	1.34	1.32	1.31	2
16.88	16.77	7.39	1.33	1.31	1.30	2
14.97	14.88	6.57	1.32	1.30	1.29	2
13.07	12.99	5.75	1.31	1.29	1.28	2
11.18	11.11	4.93	1.30	1.28	1.27	2
9.30	9.24	4.11	1.29	1.27	1.26	2
7.43	7.38	3.29	1.28	1.26	1.26	2
5.56	5.52	2.46	1.27	1.25	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.24	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.88	455.81	214.30	241.50	241.50	.00	6
58.36	492.64	218.92	273.72	273.72	.00	6
57.85	529.38	223.54	305.83	305.83	.00	6
57.34	566.05	228.16	337.89	337.89	.00	6
56.82	602.65	232.78	369.87	369.87	.00	6
56.31	639.19	237.40	401.79	401.79	.00	6
55.80	675.67	242.03	433.64	433.64	.00	6
55.29	712.07	246.65	465.43	465.43	.00	6
54.78	748.41	251.27	497.15	497.15	.00	6
54.78	748.41	251.27	497.15	497.15	.00	5
53.64	845.67	277.02	568.65	568.65	.00	5
52.51	941.99	302.77	639.23	639.23	.00	5
51.39	1037.39	328.52	708.88	708.88	.00	5
50.29	1131.87	354.27	777.60	777.61	.00	5
49.20	1225.42	380.02	845.41	845.41	.00	5
48.13	1318.05	405.77	912.28	912.28	.00	5
48.13	1318.05	405.77	912.28	912.28	.00	4
46.16	1517.06	481.63	1035.43	1035.43	.00	4
44.19	1715.41	552.39	1163.01	1157.92	5.09	4
42.24	1913.00	616.71	1296.28	1279.65	16.63	4
40.30	2109.81	682.07	1427.74	1400.61	27.13	4
38.38	2305.84	749.05	1556.79	1520.78	36.01	4
36.47	2501.05	818.49	1682.56	1640.13	42.43	4
34.57	2695.42	891.65	1803.77	1758.64	45.13	4
32.68	2888.88	971.00	1917.88	1876.24	41.64	4
30.81	3081.35	1054.26	2027.09	1992.85	34.24	4
30.81	3081.35	1054.26	2027.09	1992.85	34.24	3
29.44	3228.82	1123.05	2105.76	2078.46	27.30	3
28.08	3375.91	1189.41	2186.50	2163.69	22.81	3
26.72	3522.63	1253.60	2269.03	2248.56	20.47	3
25.36	3669.00	1315.83	2353.17	2333.06	20.10	3
24.01	3815.02	1376.27	2438.75	2417.23	21.52	3
22.67	3960.71	1435.09	2525.62	2501.06	24.56	3
21.33	4106.07	1492.44	2613.62	2584.56	29.07	3
20.00	4251.11	1548.49	2702.62	2667.74	34.88	3
18.67	4395.84	1603.36	2792.47	2750.61	41.86	3

18.67	4395.84	1603.36	2792.47	2750.61	41.86	2
16.77	4600.49	1674.64	2925.85	2869.17	56.69	2
14.88	4804.70	1747.03	3057.67	2987.28	70.39	2
12.99	5008.46	1820.83	3187.64	3104.94	82.69	2
11.11	5211.77	1896.32	3315.45	3222.15	93.30	2
9.24	5414.60	1973.90	3440.70	3338.88	101.81	2
7.38	5616.96	2077.00	3539.96	3455.14	84.82	2
5.52	5818.84	2189.73	3629.11	3570.93	58.19	2
3.68	6020.27	2298.36	3721.91	3686.26	35.65	2
1.83	6221.26	2403.27	3817.99	3801.16	16.84	2
.00	6421.83	2504.79	3917.04	3915.63	1.42	2

Time = 9125. Degree of Consolidation = 94.%

Total Settlement = 1.704

Settlement at End of Primary Consolidation = 1.807

Settlement caused by Primary Consolidation at time 9125. = 1.689

Settlement caused by Secondary Compression at time 9125. = .015

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
4.00	3.87	2.02
3.00	2.89	1.52
2.00	1.92	1.01
1.00	.96	.51
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
3.87	.00	.00
2.89	114.77	53.58
1.92	228.65	107.15
.96	342.31	160.73
.00	455.81	214.30

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
61.19	61.19	.00	1
121.50	121.50	.00	1
181.58	181.58	.00	1
241.50	241.50	.00	1

Time = 9125. Degree of Consolidation = 100.%

Total Settlement = .130

Settlement at End of Primary Consolidation = .130

Settlement caused by Primary Consolidation at time 9125. = .130

Settlement caused by Secondary Compression at time 9125. = .000

Settlement Due to Desiccation = .000

Surface Elevation = .77

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou Dupont - 5ft Fill Height

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	5.0	4	.98	120.	4	1
30.					120.	4	1
60.					120.	4	1
120.					120.	4	1
240.					120.	4	1
365.					120.	4	1
540.					120.	4	1
730.					120.	4	1
1080.					120.	4	1
1440.					120.	4	1
1825.					120.	4	1
2520.					120.	4	1
2880.					120.	4	1
3240.					120.	4	1
3650.					120.	4	1
4320.					120.	4	1
5040.					120.	4	1
5475.					120.	4	1
6480.					120.	4	1
7300.					120.	4	1
9125.					120.	4	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.173	1.106	.30000E-04	z = .05

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	5.69	6
60.02	60.02	21.35	6.49	6.49	5.68	6
59.45	59.45	21.27	6.47	6.47	5.66	6
58.89	58.89	21.20	6.46	6.46	5.65	6

58.33	58.33	21.12	6.44	6.44	5.64	6
57.76	57.76	21.05	6.43	6.43	5.62	6
57.20	57.20	20.97	6.42	6.42	5.61	6
56.64	56.64	20.90	6.40	6.40	5.59	6
56.08	56.08	20.82	6.39	6.39	5.58	6
56.08	56.08	20.82	4.51	4.51	3.84	5
54.82	54.82	20.59	4.44	4.44	3.78	5
53.56	53.56	20.36	4.38	4.38	3.72	5
52.32	52.32	20.12	4.32	4.32	3.65	5
51.10	51.10	19.89	4.25	4.25	3.59	5
49.88	49.88	19.66	4.19	4.19	3.52	5
48.69	48.69	19.43	4.13	4.13	3.46	5
48.69	48.69	19.43	1.93	1.93	1.89	4
46.69	46.69	18.75	1.92	1.92	1.87	4
44.70	44.70	18.06	1.91	1.91	1.85	4
42.72	42.72	17.38	1.89	1.89	1.83	4
40.75	40.75	16.70	1.88	1.88	1.81	4
38.79	38.79	16.01	1.86	1.86	1.79	4
36.85	36.85	15.33	1.84	1.84	1.76	4
34.91	34.91	14.65	1.82	1.82	1.74	4
33.00	33.00	13.97	1.80	1.80	1.72	4
31.09	31.09	13.28	1.78	1.78	1.70	4
31.09	31.09	13.28	1.47	1.47	1.43	3
29.70	29.70	12.72	1.46	1.46	1.42	3
28.32	28.32	12.16	1.45	1.45	1.41	3
26.94	26.94	11.59	1.44	1.44	1.40	3
25.57	25.57	11.03	1.43	1.43	1.39	3
24.21	24.21	10.47	1.42	1.42	1.38	3
22.84	22.84	9.90	1.41	1.41	1.37	3
21.49	21.49	9.34	1.40	1.40	1.36	3
20.14	20.14	8.78	1.39	1.39	1.35	3
18.80	18.80	8.21	1.38	1.38	1.34	3
18.80	18.80	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.43	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.25	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	579.88	.00	579.88	312.00	267.88	6
60.02	619.83	4.62	615.21	347.33	267.88	6
59.45	659.71	9.24	650.47	382.59	267.88	6
58.89	699.52	13.86	685.66	417.78	267.88	6
58.33	739.27	18.48	720.79	452.91	267.88	6
57.76	778.96	23.10	755.86	487.98	267.88	6
57.20	818.58	27.72	790.85	522.98	267.88	6
56.64	858.13	32.34	825.79	557.91	267.88	6
56.08	897.62	36.96	860.65	592.77	267.88	6
56.08	897.62	36.96	860.65	592.77	267.88	5
54.82	1002.59	62.71	939.88	672.00	267.88	5
53.56	1106.64	88.46	1018.18	750.30	267.88	5
52.32	1209.76	114.21	1095.55	827.67	267.88	5
51.10	1311.97	139.96	1172.00	904.12	267.88	5
49.88	1413.24	165.71	1247.53	979.65	267.88	5

48.69	1513.60	191.46	1322.14	1054.26	267.88	5
48.69	1513.60	191.46	1322.14	1054.26	267.88	4
46.69	1714.04	267.32	1446.72	1178.84	267.88	4
44.70	1913.98	343.18	1570.80	1302.92	267.88	4
42.72	2113.37	419.04	1694.33	1426.46	267.88	4
40.75	2312.32	494.90	1817.42	1549.54	267.88	4
38.79	2510.52	570.76	1939.76	1671.88	267.88	4
36.85	2707.82	646.62	2061.20	1793.32	267.88	4
34.91	2904.21	722.48	2181.74	1913.86	267.88	4
33.00	3099.70	798.34	2301.37	2033.49	267.88	4
31.09	3294.29	874.19	2420.09	2152.22	267.88	4
31.09	3294.29	874.19	2420.09	2152.22	267.88	3
29.70	3442.86	936.05	2506.81	2238.93	267.88	3
28.32	3591.03	997.91	2593.12	2325.24	267.88	3
26.94	3738.84	1059.77	2679.07	2411.19	267.88	3
25.57	3886.30	1121.63	2764.67	2496.79	267.88	3
24.21	4033.41	1183.49	2849.92	2582.04	267.88	3
22.84	4180.17	1245.35	2934.82	2666.94	267.88	3
21.49	4326.58	1307.21	3019.38	2751.50	267.88	3
20.14	4472.65	1369.06	3103.59	2835.71	267.88	3
18.80	4618.37	1430.92	3187.45	2919.57	267.88	3
18.80	4618.37	1430.92	3187.45	2919.57	267.88	2
16.88	4824.04	1517.02	3307.02	3039.14	267.88	2
14.97	5029.18	1603.12	3426.06	3158.18	267.88	2
13.07	5233.79	1689.22	3544.57	3276.69	267.88	2
11.18	5437.87	1775.31	3662.55	3394.67	267.88	2
9.30	5641.42	1861.41	3780.01	3512.13	267.88	2
7.43	5844.44	1947.51	3896.93	3629.05	267.88	2
5.56	6046.94	2033.61	4013.34	3745.46	267.88	2
3.70	6249.06	2119.71	4129.36	3861.48	267.88	2
1.85	6450.83	2205.80	4245.02	3977.14	267.88	2
.00	6652.24	2291.90	4360.34	4092.46	267.88	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	5.00	2.53	.98	.98	.98	1
3.75	3.75	1.89	.98	.98	.92	1
2.50	2.50	1.26	.98	.98	.91	1
1.25	1.25	.63	.98	.98	.90	1
.00	.00	.00	.98	.98	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

5.00	.00	.00	.00	.00	.00	1
3.75	144.97	.00	144.97	78.00	66.97	1
2.50	289.94	.00	289.94	156.00	133.94	1
1.25	434.91	.00	434.91	234.00	200.91	1
.00	579.88	.00	579.88	312.00	267.88	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.49	21.42	6.50	5.99	5.69	6
60.02	59.96	21.35	6.49	6.15	5.68	6
59.45	59.42	21.27	6.47	6.27	5.66	6
58.89	58.86	21.20	6.46	6.35	5.65	6
58.33	58.31	21.12	6.44	6.39	5.64	6
57.76	57.75	21.05	6.43	6.41	5.62	6
57.20	57.19	20.97	6.42	6.41	5.61	6
56.64	56.63	20.90	6.40	6.40	5.59	6
56.08	56.07	20.82	6.39	6.39	5.58	6
56.08	56.07	20.82	4.51	4.51	3.84	5
54.82	54.80	20.59	4.44	4.44	3.78	5
53.56	53.55	20.36	4.38	4.38	3.72	5
52.32	52.31	20.12	4.32	4.31	3.65	5
51.10	51.08	19.89	4.25	4.25	3.59	5
49.88	49.87	19.66	4.19	4.19	3.52	5
48.69	48.68	19.43	4.13	4.12	3.46	5
48.69	48.68	19.43	1.93	1.93	1.89	4
46.69	46.68	18.75	1.92	1.92	1.87	4
44.70	44.69	18.06	1.91	1.91	1.85	4
42.72	42.71	17.38	1.89	1.89	1.83	4
40.75	40.74	16.70	1.88	1.88	1.81	4
38.79	38.78	16.01	1.86	1.86	1.79	4
36.85	36.84	15.33	1.84	1.84	1.76	4
34.91	34.90	14.65	1.82	1.82	1.74	4
33.00	32.99	13.97	1.80	1.80	1.72	4
31.09	31.08	13.28	1.78	1.78	1.70	4
31.09	31.08	13.28	1.47	1.47	1.43	3
29.70	29.69	12.72	1.46	1.46	1.42	3
28.32	28.31	12.16	1.45	1.45	1.41	3
26.94	26.93	11.59	1.44	1.44	1.40	3
25.57	25.56	11.03	1.43	1.43	1.39	3
24.21	24.20	10.47	1.42	1.42	1.38	3
22.84	22.84	9.90	1.41	1.41	1.37	3
21.49	21.48	9.34	1.40	1.40	1.36	3
20.14	20.13	8.78	1.39	1.39	1.35	3
18.80	18.79	8.21	1.38	1.38	1.34	3
18.80	18.79	8.21	1.34	1.34	1.31	2

16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.49	569.86	168.28	401.57	301.98	99.60	6
59.96	607.82	116.28	491.54	335.32	156.22	6
59.42	646.45	76.21	570.23	369.33	200.91	6
58.86	685.55	49.98	635.56	403.81	231.76	6
58.31	724.93	36.03	688.90	438.57	250.33	6
57.75	764.44	30.85	733.59	473.46	260.13	6
57.19	803.98	30.95	773.04	508.38	264.65	6
56.63	843.50	33.81	809.69	543.28	266.41	6
56.07	882.97	38.05	844.93	578.13	266.79	6
56.07	882.97	38.05	844.93	578.13	266.79	5
54.80	987.91	63.58	924.33	657.32	267.01	5
53.55	1091.93	89.33	1002.60	735.59	267.01	5
52.31	1195.03	115.12	1079.91	812.94	266.97	5
51.08	1297.20	140.89	1156.30	889.35	266.95	5
49.87	1398.44	166.62	1231.82	964.85	266.97	5
48.68	1498.76	192.28	1306.48	1039.42	267.06	5
48.68	1498.76	192.28	1306.48	1039.42	267.06	4
46.68	1699.20	267.32	1431.88	1164.00	267.88	4
44.69	1899.13	343.18	1555.95	1288.07	267.88	4
42.71	2098.53	421.74	1676.79	1411.61	265.18	4
40.74	2297.37	507.75	1789.62	1534.59	255.03	4
38.78	2495.49	573.59	1921.90	1656.85	265.04	4
36.84	2692.78	646.64	2046.13	1778.28	267.85	4
34.90	2889.17	722.48	2166.70	1898.82	267.88	4
32.99	3084.66	798.34	2286.33	2018.45	267.88	4
31.08	3279.25	874.20	2405.05	2137.17	267.88	4
31.08	3279.25	874.20	2405.05	2137.17	267.88	3
29.69	3427.82	936.05	2491.76	2223.88	267.88	3
28.31	3575.99	997.91	2578.08	2310.20	267.88	3
26.93	3723.79	1060.98	2662.81	2396.14	266.66	3
25.56	3871.24	1123.18	2748.07	2481.73	266.33	3
24.20	4018.34	1185.03	2833.31	2566.98	266.33	3
22.84	4165.10	1246.77	2918.33	2651.87	266.45	3
21.48	4311.51	1308.53	3002.97	2736.42	266.55	3
20.13	4457.57	1370.27	3087.30	2820.62	266.67	3
18.79	4603.28	1431.77	3171.51	2904.48	267.03	3
18.79	4603.28	1431.77	3171.51	2904.48	267.03	2
16.87	4808.95	1517.20	3291.75	3024.05	267.70	2
14.96	5014.08	1603.18	3410.91	3143.09	267.82	2
13.06	5218.69	1689.22	3529.48	3261.60	267.88	2
11.17	5422.77	1775.31	3647.46	3379.58	267.88	2
9.29	5626.33	1861.41	3764.91	3497.03	267.88	2
7.42	5829.34	1947.51	3881.83	3613.95	267.88	2
5.55	6031.87	2033.61	3998.26	3730.38	267.88	2
3.69	6233.96	2122.57	4111.39	3846.38	265.02	2
1.84	6435.70	2237.08	4198.62	3962.01	236.61	2
.00	6636.63	2538.47	4098.16	4076.85	21.31	2

Time = 30. Degree of Consolidation = 4.%

Total Settlement = .090

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 30. = .090

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.84	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.41	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.84	.00	.00	.00	.00	.00	1
3.61	143.46	54.95	88.51	76.49	12.02	1
2.41	285.80	110.72	175.08	151.86	23.22	1
1.20	427.88	150.98	276.90	226.97	49.93	1
.00	569.86	168.28	401.57	301.98	99.60	1

Time = 30. Degree of Consolidation = 95.%

Total Settlement = .161

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 30. = .161

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 3.35

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.44	21.42	6.50	5.94	5.69	6
60.02	59.91	21.35	6.49	6.06	5.68	6
59.45	59.38	21.27	6.47	6.16	5.66	6
58.89	58.83	21.20	6.46	6.25	5.65	6
58.33	58.28	21.12	6.44	6.31	5.64	6

57.76	57.73	21.05	6.43	6.35	5.62	6
57.20	57.17	20.97	6.42	6.37	5.61	6
56.64	56.61	20.90	6.40	6.37	5.59	6
56.08	56.06	20.82	6.39	6.37	5.58	6
56.08	56.06	20.82	4.51	4.49	3.84	5
54.82	54.79	20.59	4.44	4.44	3.78	5
53.56	53.54	20.36	4.38	4.37	3.72	5
52.32	52.30	20.12	4.32	4.31	3.65	5
51.10	51.07	19.89	4.25	4.25	3.59	5
49.88	49.87	19.66	4.19	4.18	3.52	5
48.69	48.67	19.43	4.13	4.12	3.46	5
48.69	48.67	19.43	1.93	1.93	1.89	4
46.69	46.67	18.75	1.92	1.92	1.87	4
44.70	44.69	18.06	1.91	1.91	1.85	4
42.72	42.71	17.38	1.89	1.89	1.83	4
40.75	40.74	16.70	1.88	1.88	1.81	4
38.79	38.78	16.01	1.86	1.86	1.79	4
36.85	36.83	15.33	1.84	1.84	1.76	4
34.91	34.90	14.65	1.82	1.82	1.74	4
33.00	32.98	13.97	1.80	1.80	1.72	4
31.09	31.08	13.28	1.78	1.78	1.70	4
31.09	31.08	13.28	1.47	1.47	1.43	3
29.70	29.69	12.72	1.46	1.46	1.42	3
28.32	28.31	12.16	1.45	1.45	1.41	3
26.94	26.93	11.59	1.44	1.44	1.40	3
25.57	25.56	11.03	1.43	1.43	1.39	3
24.21	24.19	10.47	1.42	1.42	1.38	3
22.84	22.83	9.90	1.41	1.41	1.37	3
21.49	21.48	9.34	1.40	1.40	1.36	3
20.14	20.13	8.78	1.39	1.39	1.35	3
18.80	18.78	8.21	1.38	1.38	1.34	3
18.80	18.78	8.21	1.34	1.34	1.31	2
16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.44	569.70	186.67	383.03	301.82	81.21	6
59.91	607.31	146.63	460.68	334.81	125.87	6
59.38	645.46	111.98	533.48	368.34	165.14	6
58.83	684.05	84.31	599.74	402.31	197.43	6
58.28	722.98	64.23	658.75	436.62	222.13	6
57.73	762.15	51.30	710.84	471.17	239.68	6
57.17	801.45	44.37	757.08	505.85	251.23	6
56.61	840.82	41.96	798.86	540.60	258.26	6
56.06	880.20	42.64	837.56	575.36	262.20	6
56.06	880.20	42.64	837.56	575.36	262.20	5
54.79	985.02	66.10	918.92	654.43	264.49	5
53.54	1088.97	90.86	998.11	732.63	265.48	5
52.30	1192.01	116.22	1075.79	809.92	265.87	5
51.07	1294.15	141.82	1152.33	886.31	266.02	5
49.87	1395.36	167.46	1227.90	961.77	266.13	5
48.67	1495.66	193.04	1302.62	1036.31	266.31	5

48.67	1495.66	193.04	1302.62	1036.31	266.31	4
46.67	1696.09	267.32	1428.77	1160.89	267.88	4
44.69	1896.02	343.57	1552.45	1284.96	267.49	4
42.71	2095.41	426.42	1668.99	1408.49	260.50	4
40.74	2294.19	512.82	1781.37	1531.41	249.96	4
38.78	2492.26	577.04	1915.21	1653.62	261.59	4
36.83	2689.52	647.56	2041.96	1775.03	266.93	4
34.90	2885.91	722.48	2163.44	1895.56	267.88	4
32.98	3081.40	798.34	2283.07	2015.19	267.88	4
31.08	3275.99	874.20	2401.79	2133.91	267.88	4
31.08	3275.99	874.20	2401.79	2133.91	267.88	3
29.69	3424.56	936.05	2488.50	2220.63	267.88	3
28.31	3572.73	997.91	2574.82	2306.94	267.88	3
26.93	3720.53	1061.83	2658.70	2392.88	265.82	3
25.56	3867.98	1124.49	2743.48	2478.47	265.01	3
24.19	4015.07	1186.45	2828.62	2563.70	264.92	3
22.83	4161.82	1248.19	2913.63	2648.59	265.04	3
21.48	4308.22	1309.82	2998.40	2733.13	265.26	3
20.13	4454.27	1371.37	3082.90	2817.33	265.57	3
18.78	4599.98	1432.62	3167.35	2901.18	266.18	3
18.78	4599.98	1432.62	3167.35	2901.18	266.18	2
16.87	4805.64	1517.54	3288.10	3020.74	267.36	2
14.96	5010.78	1603.35	3407.43	3139.78	267.65	2
13.06	5215.38	1689.22	3526.17	3258.29	267.88	2
11.17	5419.46	1775.31	3644.15	3376.27	267.88	2
9.29	5623.02	1861.41	3761.61	3493.73	267.88	2
7.42	5826.03	1947.51	3878.52	3610.64	267.88	2
5.55	6028.55	2033.61	3994.94	3727.06	267.88	2
3.69	6230.65	2129.63	4101.02	3843.06	257.96	2
1.84	6432.30	2267.20	4165.10	3958.61	206.49	2
.00	6633.13	2543.08	4090.05	4073.35	16.70	2

Time = 60. Degree of Consolidation = 6.%

Total Settlement = .143

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 60. = .143

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
5.00	4.84	2.53
3.75	3.61	1.89
2.50	2.40	1.26
1.25	1.20	.63
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.84	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

3.61	143.44	58.19	85.26	76.48	8.78	1
2.40	285.76	120.50	165.26	151.82	13.44	1
1.20	427.79	165.10	262.68	226.88	35.81	1
.00	569.70	186.67	383.03	301.82	81.21	1

Time = 60. Degree of Consolidation = 96.%

Total Settlement = .163

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 60. = .163

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 3.29

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.35	21.42	6.50	5.89	5.69	6
60.02	59.83	21.35	6.49	5.97	5.68	6
59.45	59.30	21.27	6.47	6.06	5.66	6
58.89	58.77	21.20	6.46	6.13	5.65	6
58.33	58.22	21.12	6.44	6.19	5.64	6
57.76	57.68	21.05	6.43	6.24	5.62	6
57.20	57.13	20.97	6.42	6.28	5.61	6
56.64	56.58	20.90	6.40	6.31	5.59	6
56.08	56.03	20.82	6.39	6.33	5.58	6
56.08	56.03	20.82	4.51	4.46	3.84	5
54.82	54.77	20.59	4.44	4.41	3.78	5
53.56	53.52	20.36	4.38	4.36	3.72	5
52.32	52.28	20.12	4.32	4.30	3.65	5
51.10	51.06	19.89	4.25	4.24	3.59	5
49.88	49.85	19.66	4.19	4.18	3.52	5
48.69	48.66	19.43	4.13	4.11	3.46	5
48.69	48.66	19.43	1.93	1.93	1.89	4
46.69	46.66	18.75	1.92	1.92	1.87	4
44.70	44.68	18.06	1.91	1.90	1.85	4
42.72	42.70	17.38	1.89	1.89	1.83	4
40.75	40.73	16.70	1.88	1.87	1.81	4
38.79	38.77	16.01	1.86	1.86	1.79	4
36.85	36.83	15.33	1.84	1.84	1.76	4
34.91	34.89	14.65	1.82	1.82	1.74	4
33.00	32.98	13.97	1.80	1.80	1.72	4
31.09	31.07	13.28	1.78	1.78	1.70	4
31.09	31.07	13.28	1.47	1.47	1.43	3
29.70	29.69	12.72	1.46	1.46	1.42	3
28.32	28.30	12.16	1.45	1.45	1.41	3
26.94	26.92	11.59	1.44	1.44	1.40	3
25.57	25.55	11.03	1.43	1.43	1.39	3
24.21	24.19	10.47	1.42	1.42	1.38	3
22.84	22.83	9.90	1.41	1.41	1.37	3
21.49	21.47	9.34	1.40	1.40	1.36	3
20.14	20.12	8.78	1.39	1.39	1.35	3
18.80	18.78	8.21	1.38	1.38	1.34	3

18.80	18.78	8.21	1.34	1.34	1.31	2
16.88	16.86	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.06	5.75	1.31	1.31	1.28	2
11.18	11.17	4.93	1.30	1.30	1.27	2
9.30	9.28	4.11	1.29	1.29	1.26	2
7.43	7.41	3.29	1.28	1.28	1.25	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.35	569.57	203.47	366.10	301.69	64.41	6
59.83	606.87	174.13	432.74	334.37	98.37	6
59.30	644.56	146.97	497.59	367.44	130.14	6
58.77	682.63	122.85	559.77	400.89	158.89	6
58.22	721.01	102.36	618.65	434.65	184.00	6
57.68	759.65	85.75	673.90	468.67	205.23	6
57.13	798.51	72.98	725.53	502.91	222.62	6
56.58	837.52	63.68	773.84	537.30	236.54	6
56.03	876.64	57.26	819.38	571.80	247.58	6
56.03	876.64	57.26	819.38	571.80	247.58	5
54.77	981.01	76.48	904.53	650.42	254.11	5
53.52	1084.65	97.97	986.68	728.31	258.37	5
52.28	1187.49	121.09	1066.39	805.39	261.00	5
51.06	1289.47	145.30	1144.17	881.63	262.54	5
49.85	1390.57	170.22	1220.35	956.98	263.37	5
48.66	1490.77	195.64	1295.13	1031.43	263.70	5
48.66	1490.77	195.64	1295.13	1031.43	263.70	4
46.66	1691.20	268.60	1422.60	1156.00	266.60	4
44.68	1891.11	347.11	1544.00	1280.05	263.95	4
42.70	2090.46	433.99	1656.47	1403.54	252.93	4
40.73	2289.18	518.98	1770.20	1526.40	243.80	4
38.77	2487.18	582.40	1904.78	1648.54	256.24	4
36.83	2684.39	650.38	2034.01	1769.89	264.12	4
34.89	2880.77	722.58	2158.18	1890.41	267.77	4
32.98	3076.26	798.34	2277.92	2010.04	267.88	4
31.07	3270.84	874.20	2396.65	2128.77	267.88	4
31.07	3270.84	874.20	2396.65	2128.77	267.88	3
29.69	3419.41	936.05	2483.36	2215.48	267.88	3
28.30	3567.59	997.91	2569.67	2301.79	267.88	3
26.92	3715.38	1063.07	2652.31	2387.73	264.58	3
25.55	3862.82	1126.63	2736.19	2473.31	262.88	3
24.19	4009.90	1189.02	2820.88	2558.53	262.35	3
22.83	4156.63	1250.83	2905.80	2643.40	262.40	3
21.47	4303.01	1312.26	2990.76	2727.93	262.83	3
20.12	4449.06	1373.45	3075.60	2812.11	263.49	3
18.78	4594.75	1434.29	3160.47	2895.95	264.52	3
18.78	4594.75	1434.29	3160.47	2895.95	264.52	2
16.86	4800.41	1518.37	3282.04	3015.51	266.53	2
14.96	5005.54	1603.69	3401.85	3134.54	267.30	2
13.06	5210.15	1689.36	3520.79	3253.05	267.74	2
11.17	5414.23	1775.31	3638.91	3371.03	267.88	2
9.28	5617.78	1861.41	3756.37	3488.49	267.88	2
7.41	5820.80	1947.51	3873.29	3605.41	267.88	2
5.55	6023.31	2033.87	3989.45	3721.82	267.62	2
3.69	6225.38	2147.89	4077.50	3837.80	239.70	2
1.84	6426.90	2307.57	4119.33	3953.22	166.11	2
.00	6627.62	2546.41	4081.21	4067.84	13.37	2

Time = 120. Degree of Consolidation = 10.%

Total Settlement = .229

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 120. = .229

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.43	60.63	82.81	76.46	6.34	1
2.40	285.72	128.00	157.72	151.78	5.94	1
1.20	427.71	176.33	251.38	226.80	24.58	1
.00	569.57	203.47	366.10	301.69	64.41	1

Time = 120. Degree of Consolidation = 97.%

Total Settlement = .165

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 120. = .165

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.21

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.22	21.42	6.50	5.85	5.69	6
60.02	59.70	21.35	6.49	5.91	5.68	6

59.45	59.18	21.27	6.47	5.97	5.66	6
58.89	58.65	21.20	6.46	6.03	5.65	6
58.33	58.11	21.12	6.44	6.08	5.64	6
57.76	57.58	21.05	6.43	6.13	5.62	6
57.20	57.04	20.97	6.42	6.17	5.61	6
56.64	56.49	20.90	6.40	6.21	5.59	6
56.08	55.95	20.82	6.39	6.25	5.58	6
56.08	55.95	20.82	4.51	4.39	3.84	5
54.82	54.70	20.59	4.44	4.35	3.78	5
53.56	53.46	20.36	4.38	4.31	3.72	5
52.32	52.24	20.12	4.32	4.26	3.65	5
51.10	51.03	19.89	4.25	4.20	3.59	5
49.88	49.83	19.66	4.19	4.14	3.52	5
48.69	48.64	19.43	4.13	4.08	3.46	5
48.69	48.64	19.43	1.93	1.93	1.89	4
46.69	46.65	18.75	1.92	1.92	1.87	4
44.70	44.66	18.06	1.91	1.90	1.85	4
42.72	42.68	17.38	1.89	1.89	1.83	4
40.75	40.72	16.70	1.88	1.87	1.81	4
38.79	38.76	16.01	1.86	1.85	1.79	4
36.85	36.82	15.33	1.84	1.84	1.76	4
34.91	34.89	14.65	1.82	1.82	1.74	4
33.00	32.97	13.97	1.80	1.80	1.72	4
31.09	31.07	13.28	1.78	1.78	1.70	4
31.09	31.07	13.28	1.47	1.47	1.43	3
29.70	29.68	12.72	1.46	1.46	1.42	3
28.32	28.29	12.16	1.45	1.45	1.41	3
26.94	26.92	11.59	1.44	1.44	1.40	3
25.57	25.54	11.03	1.43	1.43	1.39	3
24.21	24.18	10.47	1.42	1.42	1.38	3
22.84	22.82	9.90	1.41	1.41	1.37	3
21.49	21.47	9.34	1.40	1.40	1.36	3
20.14	20.12	8.78	1.39	1.39	1.35	3
18.80	18.77	8.21	1.38	1.38	1.34	3
18.80	18.77	8.21	1.34	1.34	1.31	2
16.88	16.86	7.39	1.33	1.33	1.30	2
14.97	14.95	6.57	1.32	1.32	1.29	2
13.07	13.05	5.75	1.31	1.31	1.28	2
11.18	11.16	4.93	1.30	1.30	1.27	2
9.30	9.28	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.25	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.68	1.64	1.26	1.26	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.22	569.51	216.51	353.01	301.63	51.37	6
59.70	606.56	195.60	410.96	334.06	76.90	6
59.18	643.90	175.45	468.45	366.78	101.67	6
58.65	681.52	156.35	525.17	399.78	125.39	6
58.11	719.40	138.57	580.83	433.04	147.79	6
57.58	757.52	122.32	635.21	466.54	168.67	6
57.04	795.87	107.71	688.16	500.27	187.89	6
56.49	834.41	94.80	739.61	534.19	205.43	6
55.95	873.12	83.56	789.56	568.28	221.28	6
55.95	873.12	83.56	789.56	568.28	221.28	5
54.70	976.60	99.75	876.85	646.01	230.84	5
53.46	1079.46	118.06	961.40	723.12	238.28	5
52.24	1181.63	138.32	1043.31	799.54	243.77	5

51.03	1283.04	160.36	1122.68	875.20	247.49	5
49.83	1383.63	184.02	1199.61	950.04	249.58	5
48.64	1483.34	209.19	1274.15	1024.00	250.16	5
48.64	1483.34	209.19	1274.15	1024.00	250.16	4
46.65	1683.68	279.97	1403.72	1148.48	255.23	4
44.66	1883.52	358.34	1525.18	1272.46	252.72	4
42.68	2082.79	446.75	1636.03	1395.87	240.17	4
40.72	2281.41	526.93	1754.48	1518.63	235.85	4
38.76	2479.32	589.52	1889.80	1640.68	249.12	4
36.82	2676.46	655.44	2021.02	1761.96	259.06	4
34.89	2872.79	724.98	2147.81	1882.43	265.38	4
32.97	3068.27	798.34	2269.93	2002.05	267.88	4
31.07	3262.85	874.20	2388.66	2120.78	267.88	4
31.07	3262.85	874.20	2388.66	2120.78	267.88	3
29.68	3411.42	936.05	2475.37	2207.49	267.88	3
28.29	3559.60	997.91	2561.69	2293.81	267.88	3
26.92	3707.39	1064.80	2642.60	2379.74	262.85	3
25.54	3854.81	1129.71	2725.11	2465.30	259.80	3
24.18	4001.87	1193.03	2808.84	2550.51	258.33	3
22.82	4148.58	1255.22	2893.36	2635.36	258.01	3
21.47	4294.94	1316.60	2978.34	2719.86	258.48	3
20.12	4440.96	1377.34	3063.62	2804.02	259.60	3
18.77	4586.64	1437.56	3149.07	2887.84	261.24	3
18.77	4586.64	1437.56	3149.07	2887.84	261.24	2
16.86	4792.27	1520.43	3271.84	3007.38	264.47	2
14.95	4997.40	1604.78	3392.62	3126.40	266.22	2
13.05	5202.00	1689.91	3512.09	3244.90	267.19	2
11.16	5406.08	1775.38	3630.69	3362.88	267.81	2
9.28	5609.63	1861.41	3748.22	3480.34	267.88	2
7.40	5812.65	1947.51	3865.14	3597.26	267.88	2
5.54	6015.15	2043.72	3971.43	3713.66	257.76	2
3.68	6217.14	2180.51	4036.63	3829.55	207.08	2
1.83	6418.49	2349.35	4069.14	3944.81	124.33	2
.00	6619.09	2549.81	4069.29	4059.31	9.98	2

Time = 240. Degree of Consolidation = 16.%

Total Settlement = .365

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 240. = .365

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.43	61.76	81.66	76.46	5.21	1
2.40	285.70	131.55	154.16	151.76	2.39	1
1.20	427.68	181.79	245.89	226.77	19.12	1
.00	569.51	216.51	353.01	301.63	51.37	1

Time = 240. Degree of Consolidation = 98.%

Total Settlement = .166

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 240. = .166

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.07

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.10	21.42	6.50	5.83	5.69	6
60.02	59.58	21.35	6.49	5.88	5.68	6
59.45	59.06	21.27	6.47	5.93	5.66	6
58.89	58.54	21.20	6.46	5.98	5.65	6
58.33	58.01	21.12	6.44	6.03	5.64	6
57.76	57.48	21.05	6.43	6.07	5.62	6
57.20	56.94	20.97	6.42	6.11	5.61	6
56.64	56.40	20.90	6.40	6.15	5.59	6
56.08	55.86	20.82	6.39	6.18	5.58	6
56.08	55.86	20.82	4.51	4.34	3.84	5
54.82	54.63	20.59	4.44	4.30	3.78	5
53.56	53.40	20.36	4.38	4.26	3.72	5
52.32	52.19	20.12	4.32	4.21	3.65	5
51.10	50.99	19.89	4.25	4.15	3.59	5
49.88	49.80	19.66	4.19	4.10	3.52	5
48.69	48.63	19.43	4.13	4.03	3.46	5
48.69	48.63	19.43	1.93	1.92	1.89	4
46.69	46.63	18.75	1.92	1.91	1.87	4
44.70	44.65	18.06	1.91	1.90	1.85	4
42.72	42.67	17.38	1.89	1.89	1.83	4
40.75	40.71	16.70	1.88	1.87	1.81	4
38.79	38.75	16.01	1.86	1.85	1.79	4
36.85	36.81	15.33	1.84	1.84	1.76	4
34.91	34.88	14.65	1.82	1.82	1.74	4
33.00	32.96	13.97	1.80	1.80	1.72	4
31.09	31.06	13.28	1.78	1.78	1.70	4
31.09	31.06	13.28	1.47	1.47	1.43	3
29.70	29.67	12.72	1.46	1.46	1.42	3
28.32	28.29	12.16	1.45	1.45	1.41	3
26.94	26.91	11.59	1.44	1.44	1.40	3
25.57	25.54	11.03	1.43	1.43	1.39	3

24.21	24.17	10.47	1.42	1.42	1.38	3
22.84	22.81	9.90	1.41	1.41	1.37	3
21.49	21.46	9.34	1.40	1.40	1.36	3
20.14	20.11	8.78	1.39	1.39	1.35	3
18.80	18.77	8.21	1.38	1.38	1.34	3
18.80	18.77	8.21	1.34	1.34	1.31	2
16.88	16.85	7.39	1.33	1.33	1.30	2
14.97	14.95	6.57	1.32	1.32	1.29	2
13.07	13.05	5.75	1.31	1.31	1.28	2
11.18	11.16	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.25	2
5.56	5.54	2.46	1.27	1.27	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.10	569.48	222.60	346.88	301.60	45.28	6
59.58	606.42	205.40	401.02	333.92	67.10	6
59.06	643.59	188.60	454.99	366.47	88.52	6
58.54	681.00	172.37	508.63	399.26	109.37	6
58.01	718.64	156.88	561.76	432.28	129.48	6
57.48	756.49	142.27	614.22	465.51	148.71	6
56.94	794.55	128.69	665.86	498.94	166.91	6
56.40	832.78	116.24	716.54	532.56	183.98	6
55.86	871.19	105.02	766.17	566.35	199.82	6
55.86	871.19	105.02	766.17	566.35	199.82	5
54.63	973.90	121.08	852.82	643.31	209.51	5
53.40	1076.00	138.96	937.04	719.66	217.38	5
52.19	1177.43	158.66	1018.77	795.34	223.43	5
50.99	1278.12	180.15	1097.97	870.28	227.69	5
49.80	1378.01	203.38	1174.62	944.42	230.21	5
48.63	1477.03	228.30	1248.73	1017.69	231.04	5
48.63	1477.03	228.30	1248.73	1017.69	231.04	4
46.63	1677.25	296.82	1380.43	1142.05	238.38	4
44.65	1876.98	373.50	1503.48	1265.92	237.56	4
42.67	2076.15	460.86	1615.29	1389.23	226.06	4
40.71	2274.68	534.30	1740.38	1511.90	228.48	4
38.75	2472.50	595.53	1876.97	1633.87	243.10	4
36.81	2669.58	659.86	2009.72	1755.08	254.64	4
34.88	2865.87	727.49	2138.38	1875.51	262.87	4
32.96	3061.33	798.72	2262.61	1995.12	267.50	4
31.06	3255.92	874.38	2381.54	2113.84	267.69	4
31.06	3255.92	874.38	2381.54	2113.84	267.69	3
29.67	3404.49	936.05	2468.43	2200.55	267.88	3
28.29	3552.66	997.91	2554.75	2286.87	267.88	3
26.91	3700.45	1066.02	2634.44	2372.80	261.63	3
25.54	3847.86	1132.06	2715.81	2458.36	257.45	3
24.17	3994.91	1196.11	2798.80	2543.54	255.26	3
22.81	4141.60	1258.75	2882.85	2628.37	254.48	3
21.46	4287.94	1320.20	2967.74	2712.85	254.89	3
20.11	4433.94	1380.79	3053.15	2796.99	256.15	3
18.77	4579.59	1440.58	3139.02	2880.79	258.23	3
18.77	4579.59	1440.58	3139.02	2880.79	258.22	2
16.85	4785.22	1522.58	3262.63	3000.32	262.32	2
14.95	4990.33	1606.21	3384.12	3119.33	264.78	2
13.05	5194.93	1690.62	3504.30	3237.83	266.47	2
11.16	5399.00	1775.79	3623.21	3355.81	267.40	2
9.27	5602.55	1861.50	3741.05	3473.26	267.80	2

7.40	5805.57	1948.24	3857.33	3590.18	267.15	2
5.54	6008.04	2056.93	3951.11	3706.55	244.56	2
3.68	6209.95	2204.33	4005.62	3822.36	183.26	2
1.83	6411.21	2370.88	4040.33	3937.52	102.81	2
.00	6611.75	2551.53	4060.22	4051.97	8.25	2

Time = 365. Degree of Consolidation = 21.%

Total Settlement = .482

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 365. = .482

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.43	62.27	81.16	76.46	4.70	1
2.40	285.70	133.12	152.57	151.76	.81	1
1.20	427.66	184.25	243.42	226.76	16.66	1
.00	569.48	222.60	346.88	301.60	45.28	1

Time = 365. Degree of Consolidation = 98.%

Total Settlement = .167

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 365. = .167

Settlement caused by Secondary Compression at time 365. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.95

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.96	21.42	6.50	5.81	5.69	6
60.02	59.44	21.35	6.49	5.85	5.68	6
59.45	58.92	21.27	6.47	5.90	5.66	6
58.89	58.40	21.20	6.46	5.94	5.65	6
58.33	57.87	21.12	6.44	5.98	5.64	6
57.76	57.35	21.05	6.43	6.01	5.62	6
57.20	56.81	20.97	6.42	6.05	5.61	6
56.64	56.28	20.90	6.40	6.08	5.59	6
56.08	55.74	20.82	6.39	6.11	5.58	6
56.08	55.74	20.82	4.51	4.28	3.84	5
54.82	54.53	20.59	4.44	4.24	3.78	5
53.56	53.32	20.36	4.38	4.19	3.72	5
52.32	52.12	20.12	4.32	4.14	3.65	5
51.10	50.93	19.89	4.25	4.09	3.59	5
49.88	49.76	19.66	4.19	4.03	3.52	5
48.69	48.60	19.43	4.13	3.97	3.46	5
48.69	48.60	19.43	1.93	1.92	1.89	4
46.69	46.61	18.75	1.92	1.91	1.87	4
44.70	44.63	18.06	1.91	1.90	1.85	4
42.72	42.66	17.38	1.89	1.88	1.83	4
40.75	40.69	16.70	1.88	1.87	1.81	4
38.79	38.74	16.01	1.86	1.85	1.79	4
36.85	36.80	15.33	1.84	1.83	1.76	4
34.91	34.87	14.65	1.82	1.82	1.74	4
33.00	32.95	13.97	1.80	1.80	1.72	4
31.09	31.05	13.28	1.78	1.77	1.70	4
31.09	31.05	13.28	1.47	1.47	1.43	3
29.70	29.66	12.72	1.46	1.46	1.42	3
28.32	28.28	12.16	1.45	1.45	1.41	3
26.94	26.90	11.59	1.44	1.44	1.40	3
25.57	25.53	11.03	1.43	1.43	1.39	3
24.21	24.17	10.47	1.42	1.42	1.38	3
22.84	22.81	9.90	1.41	1.41	1.37	3
21.49	21.45	9.34	1.40	1.40	1.36	3
20.14	20.11	8.78	1.39	1.39	1.35	3
18.80	18.76	8.21	1.38	1.38	1.34	3
18.80	18.76	8.21	1.34	1.34	1.31	2
16.88	16.85	7.39	1.33	1.33	1.30	2
14.97	14.94	6.57	1.32	1.32	1.29	2
13.07	13.04	5.75	1.31	1.31	1.28	2
11.18	11.15	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.25	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.96	569.46	227.81	341.65	301.59	40.06	6
59.44	606.30	213.78	392.52	333.80	58.72	6
58.92	643.34	200.02	443.32	366.22	77.10	6
58.40	680.56	186.66	493.90	398.82	95.08	6
57.87	717.98	173.83	544.15	431.62	112.53	6
57.35	755.57	161.64	593.93	464.59	129.34	6
56.81	793.33	150.23	643.10	497.73	145.37	6
56.28	831.25	139.71	691.54	531.03	160.52	6

55.74	869.31	130.17	739.14	564.47	174.67	6
55.74	869.31	130.17	739.14	564.47	174.67	5
54.53	971.10	147.12	823.98	640.51	183.47	5
53.32	1072.26	165.60	906.66	715.92	190.75	5
52.12	1172.72	185.63	987.10	790.63	196.47	5
50.93	1272.44	207.23	1065.22	864.60	200.62	5
49.76	1371.36	230.40	1140.96	937.77	203.20	5
48.60	1469.42	255.11	1214.31	1010.07	204.23	5
48.60	1469.42	255.11	1214.31	1010.07	204.24	4
46.61	1669.46	321.72	1347.74	1134.26	213.48	4
44.63	1869.02	396.51	1472.52	1257.96	214.55	4
42.66	2068.04	482.28	1585.76	1381.12	204.64	4
40.69	2266.43	545.16	1721.28	1503.66	217.62	4
38.74	2464.14	604.22	1859.92	1625.51	234.41	4
36.80	2661.13	666.43	1994.70	1746.63	248.07	4
34.87	2857.35	732.04	2125.31	1867.00	258.31	4
32.95	3052.77	801.51	2251.26	1986.56	264.71	4
31.05	3247.33	875.72	2371.61	2105.26	266.35	4
31.05	3247.33	875.72	2371.61	2105.26	266.35	3
29.66	3395.90	936.05	2459.84	2191.97	267.88	3
28.28	3544.08	997.91	2546.16	2278.29	267.88	3
26.90	3691.86	1067.35	2624.51	2364.21	260.30	3
25.53	3839.26	1134.48	2704.78	2449.75	255.02	3
24.17	3986.29	1199.40	2786.89	2534.92	251.97	3
22.81	4132.96	1262.56	2870.40	2619.73	250.66	3
21.45	4279.28	1324.27	2955.01	2704.19	250.82	3
20.11	4425.25	1384.78	3040.47	2788.31	252.16	3
18.76	4570.89	1444.24	3126.65	2872.09	254.56	3
18.76	4570.89	1444.24	3126.65	2872.09	254.56	2
16.85	4776.49	1525.60	3250.89	2991.59	259.30	2
14.94	4981.59	1608.22	3373.36	3110.59	262.78	2
13.04	5186.17	1692.12	3494.05	3229.08	264.97	2
11.15	5390.24	1777.05	3613.19	3347.04	266.15	2
9.27	5593.78	1863.61	3730.17	3464.48	265.68	2
7.40	5796.77	1953.51	3843.27	3581.38	261.88	2
5.53	5999.20	2073.11	3926.09	3697.71	228.38	2
3.68	6201.03	2225.57	3975.46	3813.44	162.01	2
1.83	6402.21	2387.03	4015.18	3928.52	86.66	2
.00	6602.71	2552.84	4049.87	4042.93	6.94	2

Time = 540. Degree of Consolidation = 28.%

Total Settlement = .627

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 540. = .627

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1

1.25	1.20	.63	.98	.90	1
.00	.00	.00	.98	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.42	62.53	80.90	76.45	4.44	1
2.40	285.69	133.94	151.75	151.75	.00	1
1.20	427.66	186.13	241.52	226.75	14.77	1
.00	569.46	227.81	341.65	301.59	40.07	1

Time = 540. Degree of Consolidation = 99.%

Total Settlement = .167

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 540. = .167

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.81

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.82	21.42	6.50	5.80	5.69	6
60.02	59.30	21.35	6.49	5.83	5.68	6
59.45	58.79	21.27	6.47	5.87	5.66	6
58.89	58.27	21.20	6.46	5.90	5.65	6
58.33	57.74	21.12	6.44	5.93	5.64	6
57.76	57.22	21.05	6.43	5.96	5.62	6
57.20	56.69	20.97	6.42	5.99	5.61	6
56.64	56.16	20.90	6.40	6.01	5.59	6
56.08	55.63	20.82	6.39	6.04	5.58	6
56.08	55.63	20.82	4.51	4.22	3.84	5
54.82	54.43	20.59	4.44	4.17	3.78	5
53.56	53.23	20.36	4.38	4.13	3.72	5
52.32	52.05	20.12	4.32	4.08	3.65	5
51.10	50.88	19.89	4.25	4.02	3.59	5
49.88	49.72	19.66	4.19	3.96	3.52	5
48.69	48.58	19.43	4.13	3.90	3.46	5
48.69	48.58	19.43	1.93	1.91	1.89	4
46.69	46.59	18.75	1.92	1.90	1.87	4
44.70	44.61	18.06	1.91	1.89	1.85	4
42.72	42.64	17.38	1.89	1.88	1.83	4
40.75	40.68	16.70	1.88	1.86	1.81	4
38.79	38.73	16.01	1.86	1.85	1.79	4
36.85	36.79	15.33	1.84	1.83	1.76	4
34.91	34.86	14.65	1.82	1.81	1.74	4
33.00	32.95	13.97	1.80	1.79	1.72	4
31.09	31.05	13.28	1.78	1.77	1.70	4

31.09	31.05	13.28	1.47	1.47	1.43	3
29.70	29.66	12.72	1.46	1.46	1.42	3
28.32	28.27	12.16	1.45	1.45	1.41	3
26.94	26.90	11.59	1.44	1.44	1.40	3
25.57	25.53	11.03	1.43	1.43	1.39	3
24.21	24.16	10.47	1.42	1.42	1.38	3
22.84	22.80	9.90	1.41	1.41	1.37	3
21.49	21.45	9.34	1.40	1.40	1.36	3
20.14	20.10	8.78	1.39	1.39	1.35	3
18.80	18.76	8.21	1.38	1.38	1.34	3
18.80	18.76	8.21	1.34	1.34	1.31	2
16.88	16.84	7.39	1.33	1.33	1.30	2
14.97	14.94	6.57	1.32	1.32	1.29	2
13.07	13.04	5.75	1.31	1.31	1.28	2
11.18	11.15	4.93	1.30	1.30	1.27	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.39	3.29	1.28	1.27	1.25	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.82	569.45	232.06	337.39	301.57	35.82	6
59.30	606.21	220.67	385.54	333.71	51.83	6
58.79	643.13	209.52	433.61	366.01	67.60	6
58.27	680.20	198.72	481.48	398.46	83.02	6
57.74	717.43	188.38	529.05	431.07	97.98	6
57.22	754.80	178.59	576.21	463.82	112.39	6
56.69	792.30	169.46	622.84	496.70	126.14	6
56.16	829.93	161.10	668.83	529.71	139.13	6
55.63	867.67	153.59	714.08	562.83	151.26	6
55.63	867.67	153.59	714.08	562.83	151.26	5
54.43	968.60	171.68	796.92	638.01	158.91	5
53.23	1068.86	191.03	877.83	712.52	165.31	5
52.05	1168.40	211.69	956.71	786.31	170.40	5
50.88	1267.18	233.67	1033.51	859.33	174.18	5
49.72	1365.14	256.97	1108.17	931.55	176.62	5
48.58	1462.25	281.58	1180.67	1002.90	177.77	5
48.58	1462.25	281.58	1180.67	1002.90	177.76	4
46.59	1662.11	347.26	1314.85	1126.91	187.94	4
44.61	1861.51	421.08	1440.43	1250.45	189.98	4
42.64	2060.36	503.31	1557.05	1373.44	183.61	4
40.68	2258.60	557.29	1701.30	1495.82	205.48	4
38.73	2456.17	614.27	1841.91	1617.54	224.37	4
36.79	2653.05	674.40	1978.66	1738.56	240.10	4
34.86	2849.19	737.98	2111.22	1858.84	252.38	4
32.95	3044.55	805.52	2239.03	1978.34	260.69	4
31.05	3239.08	877.92	2361.15	2097.00	264.15	4
31.05	3239.08	877.92	2361.15	2097.00	264.15	3
29.66	3387.64	936.58	2451.06	2183.70	267.35	3
28.27	3535.81	998.33	2537.48	2270.02	267.46	3
26.90	3683.59	1068.54	2615.05	2355.94	259.11	3
25.53	3830.98	1136.43	2694.56	2441.47	253.08	3
24.16	3978.00	1202.03	2775.96	2526.63	249.33	3
22.80	4124.65	1265.72	2858.93	2611.43	247.50	3
21.45	4270.95	1327.73	2943.22	2695.87	247.36	3
20.10	4416.91	1388.25	3028.66	2779.96	248.70	3
18.76	4562.52	1447.54	3114.98	2863.72	251.26	3
18.76	4562.52	1447.54	3114.98	2863.72	251.26	2

16.84	4768.11	1528.58	3239.52	2983.21	256.32	2
14.94	4973.19	1610.77	3362.42	3102.19	260.23	2
13.04	5177.76	1694.41	3483.34	3220.66	262.68	2
11.15	5381.81	1779.89	3601.91	3338.61	263.30	2
9.27	5585.32	1867.77	3717.55	3456.03	261.52	2
7.39	5788.29	1960.11	3828.18	3572.90	255.28	2
5.53	5990.67	2087.23	3903.44	3689.18	214.26	2
3.68	6192.43	2240.20	3952.24	3804.85	147.39	2
1.83	6393.56	2396.86	3996.70	3919.88	76.82	2
.00	6594.04	2553.60	4040.44	4034.26	6.18	2

Time = 730. Degree of Consolidation = 34.%

Total Settlement = .766

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 730. = .766

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.42	62.53	80.90	76.45	4.44	1
2.40	285.69	133.94	151.75	151.75	.00	1
1.20	427.65	187.41	240.24	226.74	13.50	1
.00	569.45	232.06	337.39	301.57	35.82	1

Time = 730. Degree of Consolidation = 99.%

Total Settlement = .167

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 730. = .167

Settlement caused by Secondary Compression at time 730. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.67

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.60	21.42	6.50	5.78	5.69	6
60.02	59.08	21.35	6.49	5.80	5.68	6
59.45	58.57	21.27	6.47	5.82	5.66	6
58.89	58.05	21.20	6.46	5.84	5.65	6
58.33	57.53	21.12	6.44	5.86	5.64	6
57.76	57.02	21.05	6.43	5.88	5.62	6
57.20	56.49	20.97	6.42	5.90	5.61	6
56.64	55.97	20.90	6.40	5.91	5.59	6
56.08	55.45	20.82	6.39	5.93	5.58	6
56.08	55.45	20.82	4.51	4.13	3.84	5
54.82	54.27	20.59	4.44	4.08	3.78	5
53.56	53.09	20.36	4.38	4.03	3.72	5
52.32	51.93	20.12	4.32	3.97	3.65	5
51.10	50.79	19.89	4.25	3.92	3.59	5
49.88	49.65	19.66	4.19	3.86	3.52	5
48.69	48.53	19.43	4.13	3.80	3.46	5
48.69	48.53	19.43	1.93	1.91	1.89	4
46.69	46.55	18.75	1.92	1.90	1.87	4
44.70	44.58	18.06	1.91	1.89	1.85	4
42.72	42.61	17.38	1.89	1.87	1.83	4
40.75	40.65	16.70	1.88	1.86	1.81	4
38.79	38.71	16.01	1.86	1.84	1.79	4
36.85	36.77	15.33	1.84	1.83	1.76	4
34.91	34.85	14.65	1.82	1.81	1.74	4
33.00	32.93	13.97	1.80	1.79	1.72	4
31.09	31.03	13.28	1.78	1.77	1.70	4
31.09	31.03	13.28	1.47	1.47	1.43	3
29.70	29.64	12.72	1.46	1.46	1.42	3
28.32	28.26	12.16	1.45	1.45	1.41	3
26.94	26.89	11.59	1.44	1.44	1.40	3
25.57	25.52	11.03	1.43	1.43	1.39	3
24.21	24.15	10.47	1.42	1.42	1.38	3
22.84	22.79	9.90	1.41	1.41	1.37	3
21.49	21.44	9.34	1.40	1.40	1.36	3
20.14	20.09	8.78	1.39	1.39	1.35	3
18.80	18.75	8.21	1.38	1.38	1.34	3
18.80	18.75	8.21	1.34	1.34	1.31	2
16.88	16.84	7.39	1.33	1.33	1.30	2
14.97	14.93	6.57	1.32	1.32	1.29	2
13.07	13.03	5.75	1.31	1.31	1.28	2
11.18	11.14	4.93	1.30	1.30	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.25	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.68	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.60	569.44	238.69	330.75	301.56	29.19	6
59.08	606.07	231.22	374.85	333.57	41.28	6
58.57	642.81	223.97	418.84	365.69	53.15	6

58.05	679.65	217.02	462.64	397.91	64.72	6
57.53	716.59	210.44	506.15	430.23	75.92	6
57.02	753.62	204.32	549.30	462.64	86.66	6
56.49	790.73	198.73	592.00	495.13	96.87	6
55.97	827.92	193.75	634.16	527.70	106.47	6
55.45	865.17	189.46	675.71	560.33	115.38	6
55.45	865.17	189.46	675.71	560.33	115.38	5
54.27	964.78	209.44	755.34	634.19	121.15	5
53.09	1063.65	230.33	833.33	707.31	126.02	5
51.93	1161.76	252.14	909.63	779.67	129.96	5
50.79	1259.07	274.89	984.18	851.23	132.95	5
49.65	1355.55	298.60	1056.95	921.96	134.99	5
48.53	1451.16	323.25	1127.91	991.82	136.09	5
48.53	1451.16	323.25	1127.91	991.82	136.09	4
46.55	1650.74	389.34	1261.40	1115.54	145.86	4
44.58	1849.85	463.56	1386.28	1238.79	147.50	4
42.61	2048.41	526.84	1521.58	1361.49	160.08	4
40.65	2246.39	578.37	1668.01	1483.61	184.40	4
38.71	2443.73	632.70	1811.03	1605.09	205.94	4
36.77	2640.40	690.13	1950.27	1725.90	224.37	4
34.85	2836.37	751.04	2085.33	1846.01	239.31	4
32.93	3031.59	816.22	2215.36	1965.37	249.99	4
31.03	3226.00	886.86	2339.13	2083.92	255.21	4
31.03	3226.00	886.86	2339.13	2083.92	255.21	3
29.64	3374.50	943.86	2430.65	2170.57	260.08	3
28.26	3522.64	1004.86	2517.78	2256.85	260.93	3
26.89	3670.38	1074.25	2596.14	2342.73	253.40	3
25.52	3817.74	1141.68	2676.06	2428.24	247.82	3
24.15	3964.73	1207.28	2757.45	2513.36	244.09	3
22.79	4111.35	1271.11	2840.24	2598.13	242.11	3
21.44	4257.62	1333.27	2924.35	2682.54	241.82	3
20.09	4403.54	1393.93	3009.62	2766.60	243.02	3
18.75	4549.13	1453.26	3095.87	2850.33	245.54	3
18.75	4549.13	1453.26	3095.87	2850.33	245.54	2
16.84	4754.68	1534.37	3220.31	2969.78	250.53	2
14.93	4959.72	1616.65	3343.07	3088.72	254.34	2
13.03	5164.26	1700.52	3463.74	3207.16	256.58	2
11.14	5368.27	1787.06	3581.20	3325.07	256.13	2
9.26	5571.73	1876.86	3694.87	3442.44	252.43	2
7.39	5774.64	1971.57	3803.06	3559.25	243.82	2
5.53	5976.94	2106.02	3870.92	3675.45	195.47	2
3.68	6178.63	2256.72	3921.91	3791.04	130.87	2
1.83	6379.70	2406.94	3972.76	3906.02	66.75	2
.00	6580.16	2554.39	4025.77	4020.38	5.40	2

Time = 1080. Degree of Consolidation = 44.%

Total Settlement = .988

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 1080. = .988

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.42	62.53	80.90	76.45	4.44	1
2.40	285.69	133.94	151.75	151.75	.00	1
1.20	427.65	189.35	238.30	226.74	11.56	1
.00	569.44	238.69	330.75	301.56	29.19	1

Time = 1080. Degree of Consolidation = 99.%

Total Settlement = .167

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 1080. = .167

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.44

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.40	21.42	6.50	5.76	5.69	6
60.02	58.89	21.35	6.49	5.77	5.68	6
59.45	58.38	21.27	6.47	5.79	5.66	6
58.89	57.87	21.20	6.46	5.80	5.65	6
58.33	57.35	21.12	6.44	5.81	5.64	6
57.76	56.84	21.05	6.43	5.82	5.62	6
57.20	56.32	20.97	6.42	5.83	5.61	6
56.64	55.81	20.90	6.40	5.83	5.59	6
56.08	55.29	20.82	6.39	5.84	5.58	6
56.08	55.29	20.82	4.51	4.06	3.84	5
54.82	54.12	20.59	4.44	4.00	3.78	5
53.56	52.97	20.36	4.38	3.95	3.72	5
52.32	51.83	20.12	4.32	3.89	3.65	5
51.10	50.70	19.89	4.25	3.83	3.59	5
49.88	49.59	19.66	4.19	3.77	3.52	5
48.69	48.49	19.43	4.13	3.71	3.46	5
48.69	48.49	19.43	1.93	1.90	1.89	4
46.69	46.51	18.75	1.92	1.89	1.87	4
44.70	44.54	18.06	1.91	1.88	1.85	4
42.72	42.58	17.38	1.89	1.87	1.83	4
40.75	40.62	16.70	1.88	1.85	1.81	4

38.79	38.68	16.01	1.86	1.84	1.79	4
36.85	36.75	15.33	1.84	1.82	1.76	4
34.91	34.83	14.65	1.82	1.81	1.74	4
33.00	32.92	13.97	1.80	1.79	1.72	4
31.09	31.02	13.28	1.78	1.77	1.70	4
31.09	31.02	13.28	1.47	1.47	1.43	3
29.70	29.63	12.72	1.46	1.46	1.42	3
28.32	28.25	12.16	1.45	1.45	1.41	3
26.94	26.87	11.59	1.44	1.44	1.40	3
25.57	25.51	11.03	1.43	1.43	1.39	3
24.21	24.14	10.47	1.42	1.42	1.38	3
22.84	22.78	9.90	1.41	1.41	1.37	3
21.49	21.43	9.34	1.40	1.40	1.36	3
20.14	20.09	8.78	1.39	1.39	1.35	3
18.80	18.74	8.21	1.38	1.38	1.34	3
18.80	18.74	8.21	1.34	1.33	1.31	2
16.88	16.83	7.39	1.33	1.33	1.30	2
14.97	14.92	6.57	1.32	1.32	1.29	2
13.07	13.03	5.75	1.31	1.31	1.28	2
11.18	11.14	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.25	2
5.56	5.53	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.40	569.31	244.20	325.10	301.43	23.68	6
58.89	605.84	240.08	365.76	333.34	32.42	6
58.38	642.43	236.08	406.35	365.31	41.04	6
57.87	679.08	232.28	446.79	397.34	49.46	6
57.35	715.77	228.78	486.99	429.41	57.58	6
56.84	752.52	225.65	526.87	461.54	65.33	6
56.32	789.31	222.95	566.35	493.71	72.65	6
55.81	826.13	220.75	605.38	525.91	79.47	6
55.29	862.98	219.10	643.88	558.14	85.74	6
55.29	862.98	219.10	643.88	558.14	85.74	5
54.12	961.49	240.71	720.78	630.90	89.88	5
52.97	1059.22	262.93	796.29	702.88	93.41	5
51.83	1156.14	285.79	870.35	774.05	96.30	5
50.70	1252.23	309.30	942.93	844.39	98.54	5
49.59	1347.46	333.47	1014.00	913.87	100.12	5
48.49	1441.82	358.28	1083.54	982.48	101.06	5
48.49	1441.82	358.28	1083.54	982.48	101.06	4
46.51	1641.16	425.85	1215.31	1105.96	109.36	4
44.54	1840.01	501.03	1338.98	1228.95	110.03	4
42.58	2038.31	548.72	1489.58	1351.39	138.19	4
40.62	2236.03	598.71	1637.32	1473.25	164.07	4
38.68	2433.14	651.34	1781.80	1594.50	187.30	4
36.75	2629.60	706.96	1922.64	1715.10	207.54	4
34.83	2825.38	766.21	2059.17	1835.02	224.15	4
32.92	3020.43	829.87	2190.56	1954.21	236.35	4
31.02	3214.68	899.35	2315.33	2072.60	242.72	4
31.02	3214.68	899.35	2315.33	2072.60	242.72	3
29.63	3363.11	955.22	2407.88	2159.18	248.71	3
28.25	3511.18	1016.11	2495.07	2245.39	249.68	3
26.87	3658.86	1083.81	2575.05	2331.21	243.84	3
25.51	3806.17	1149.95	2656.22	2416.67	239.55	3
24.14	3953.12	1214.56	2738.55	2501.75	236.80	3

22.78	4099.70	1277.78	2821.92	2586.48	235.44	3
21.43	4245.93	1339.57	2906.36	2670.85	235.51	3
20.09	4391.82	1400.11	2991.71	2754.88	236.83	3
18.74	4537.37	1459.44	3077.93	2838.57	239.36	3
18.74	4537.37	1459.44	3077.93	2838.57	239.36	2
16.83	4742.88	1540.55	3202.33	2957.98	244.35	2
14.92	4947.89	1622.89	3325.00	3076.89	248.11	2
13.03	5152.38	1707.50	3444.88	3195.28	249.59	2
11.14	5356.34	1794.88	3561.47	3313.15	248.32	2
9.26	5559.76	1885.60	3674.16	3430.47	243.69	2
7.39	5762.61	1981.04	3781.57	3547.22	234.35	2
5.53	5964.85	2119.74	3845.12	3663.37	181.75	2
3.67	6166.49	2267.27	3899.22	3778.91	120.32	2
1.83	6367.53	2413.07	3954.46	3893.85	60.61	2
.00	6567.98	2554.86	4013.12	4008.19	4.92	2

Time = 1440. Degree of Consolidation = 52.%

Total Settlement = 1.181

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 1440. = 1.181

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
5.00	4.83	2.53
3.75	3.61	1.89
2.50	2.40	1.26
1.25	1.20	.63
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.83	.00	.00
3.61	143.38	66.97
2.40	285.65	133.94
1.20	427.58	200.91
.00	569.31	267.88

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
76.41	76.41	.00	1
151.71	151.71	.00	1
226.67	226.67	.00	1
301.43	301.43	.00	1

Time = 1440. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 1440. = .169

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.25

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.22	21.42	6.50	5.73	5.69	6
60.02	58.71	21.35	6.49	5.73	5.68	6
59.45	58.20	21.27	6.47	5.74	5.66	6
58.89	57.69	21.20	6.46	5.75	5.65	6
58.33	57.18	21.12	6.44	5.75	5.64	6
57.76	56.67	21.05	6.43	5.75	5.62	6
57.20	56.16	20.97	6.42	5.75	5.61	6
56.64	55.65	20.90	6.40	5.76	5.59	6
56.08	55.14	20.82	6.39	5.75	5.58	6
56.08	55.14	20.82	4.51	3.99	3.84	5
54.82	53.99	20.59	4.44	3.93	3.78	5
53.56	52.85	20.36	4.38	3.87	3.72	5
52.32	51.73	20.12	4.32	3.82	3.65	5
51.10	50.62	19.89	4.25	3.76	3.59	5
49.88	49.52	19.66	4.19	3.69	3.52	5
48.69	48.44	19.43	4.13	3.63	3.46	5
48.69	48.44	19.43	1.93	1.90	1.89	4
46.69	46.47	18.75	1.92	1.89	1.87	4
44.70	44.50	18.06	1.91	1.87	1.85	4
42.72	42.54	17.38	1.89	1.86	1.83	4
40.75	40.59	16.70	1.88	1.85	1.81	4
38.79	38.65	16.01	1.86	1.83	1.79	4
36.85	36.72	15.33	1.84	1.82	1.76	4
34.91	34.80	14.65	1.82	1.80	1.74	4
33.00	32.90	13.97	1.80	1.78	1.72	4
31.09	31.00	13.28	1.78	1.76	1.70	4
31.09	31.00	13.28	1.47	1.47	1.43	3
29.70	29.62	12.72	1.46	1.46	1.42	3
28.32	28.24	12.16	1.45	1.45	1.41	3
26.94	26.86	11.59	1.44	1.43	1.40	3
25.57	25.49	11.03	1.43	1.42	1.39	3
24.21	24.13	10.47	1.42	1.41	1.38	3
22.84	22.78	9.90	1.41	1.40	1.37	3
21.49	21.42	9.34	1.40	1.39	1.36	3
20.14	20.08	8.78	1.39	1.38	1.35	3
18.80	18.74	8.21	1.38	1.38	1.34	3
18.80	18.74	8.21	1.34	1.33	1.31	2
16.88	16.82	7.39	1.33	1.32	1.30	2
14.97	14.92	6.57	1.32	1.31	1.29	2
13.07	13.02	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.26	4.11	1.29	1.28	1.26	2
7.43	7.39	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.22	569.30	255.44	313.86	301.42	12.44	6
58.71	605.66	253.40	352.26	333.16	19.10	6
58.20	642.05	251.53	390.51	364.93	25.59	6
57.69	678.46	249.88	428.58	396.72	31.86	6
57.18	714.89	248.50	466.39	428.53	37.86	6
56.67	751.34	247.45	503.89	460.36	43.53	6
56.16	787.80	246.77	541.03	492.20	48.83	6
55.65	824.27	246.52	577.75	524.05	53.70	6
55.14	860.74	246.75	613.99	555.90	58.10	6
55.14	860.74	246.75	613.99	555.90	58.09	5
53.99	958.24	269.53	688.71	627.65	61.06	5
52.85	1054.92	292.75	762.16	698.58	63.59	5
51.73	1150.75	316.44	834.32	768.66	65.65	5
50.62	1245.73	340.59	905.14	837.89	67.25	5
49.52	1339.83	365.22	974.62	906.24	68.38	5
48.44	1433.04	390.31	1042.73	973.70	69.03	5
48.44	1433.04	390.31	1042.73	973.70	69.03	4
46.47	1632.15	460.43	1171.73	1096.95	74.77	4
44.50	1830.76	521.67	1309.09	1219.70	89.39	4
42.54	2028.82	568.94	1459.88	1341.90	117.98	4
40.59	2226.30	618.29	1608.02	1463.52	144.49	4
38.65	2423.18	670.00	1753.18	1584.54	168.64	4
36.72	2619.43	724.62	1894.81	1704.93	189.88	4
34.80	2815.00	782.80	2032.20	1824.65	207.55	4
32.90	3009.86	845.48	2164.37	1943.64	220.73	4
31.00	3203.93	914.17	2289.76	2061.85	227.91	4
31.00	3203.93	914.17	2289.76	2061.85	227.91	3
29.62	3352.27	969.23	2383.04	2148.33	234.70	3
28.24	3500.25	1030.52	2469.73	2234.46	235.27	3
26.86	3647.86	1096.34	2551.52	2320.21	231.31	3
25.49	3795.10	1160.92	2634.19	2405.60	228.59	3
24.13	3941.99	1224.32	2717.67	2490.62	227.05	3
22.78	4088.52	1286.60	2801.92	2575.30	226.62	3
21.42	4234.71	1347.72	2886.99	2659.62	227.37	3
20.08	4380.55	1407.83	2972.72	2743.61	229.12	3
18.74	4526.06	1466.97	3059.08	2827.26	231.83	3
18.74	4526.06	1466.97	3059.08	2827.26	231.83	2
16.82	4731.52	1547.67	3183.85	2946.62	237.23	2
14.92	4936.48	1630.31	3306.18	3065.49	240.69	2
13.02	5140.93	1715.27	3425.66	3183.83	241.82	2
11.13	5344.85	1803.05	3541.80	3301.65	240.14	2
9.26	5548.21	1894.24	3653.97	3418.92	235.05	2
7.39	5751.00	1989.63	3761.38	3535.61	225.76	2
5.52	5953.20	2130.75	3822.45	3651.71	170.74	2
3.67	6154.80	2275.42	3879.38	3767.21	112.17	2
1.83	6355.81	2417.23	3938.58	3882.13	56.46	2
.00	6556.25	2555.19	4001.06	3996.47	4.60	2

Time = 1825. Degree of Consolidation = 60.%

Total Settlement = 1.369

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 1825. = 1.369

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.65	133.94	151.71	151.71	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 1825. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 1825. = .169

Settlement caused by Secondary Compression at time 1825. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.06

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.94	21.42	6.50	5.71	5.69	6
60.02	58.44	21.35	6.49	5.70	5.68	6
59.45	57.93	21.27	6.47	5.69	5.66	6
58.89	57.43	21.20	6.46	5.69	5.65	6
58.33	56.92	21.12	6.44	5.68	5.64	6
57.76	56.42	21.05	6.43	5.67	5.62	6
57.20	55.91	20.97	6.42	5.66	5.61	6
56.64	55.41	20.90	6.40	5.65	5.59	6
56.08	54.91	20.82	6.39	5.64	5.58	6
56.08	54.91	20.82	4.51	3.89	3.84	5
54.82	53.78	20.59	4.44	3.83	3.78	5
53.56	52.67	20.36	4.38	3.77	3.72	5
52.32	51.57	20.12	4.32	3.71	3.65	5
51.10	50.49	19.89	4.25	3.65	3.59	5
49.88	49.42	19.66	4.19	3.58	3.52	5
48.69	48.36	19.43	4.13	3.52	3.46	5

48.69	48.36	19.43	1.93	1.89	1.89	4
46.69	46.39	18.75	1.92	1.88	1.87	4
44.70	44.43	18.06	1.91	1.87	1.85	4
42.72	42.48	17.38	1.89	1.85	1.83	4
40.75	40.53	16.70	1.88	1.84	1.81	4
38.79	38.60	16.01	1.86	1.82	1.79	4
36.85	36.68	15.33	1.84	1.81	1.76	4
34.91	34.76	14.65	1.82	1.79	1.74	4
33.00	32.86	13.97	1.80	1.78	1.72	4
31.09	30.97	13.28	1.78	1.76	1.70	4
31.09	30.97	13.28	1.47	1.46	1.43	3
29.70	29.59	12.72	1.46	1.45	1.42	3
28.32	28.21	12.16	1.45	1.44	1.41	3
26.94	26.84	11.59	1.44	1.43	1.40	3
25.57	25.47	11.03	1.43	1.42	1.39	3
24.21	24.11	10.47	1.42	1.41	1.38	3
22.84	22.76	9.90	1.41	1.40	1.37	3
21.49	21.41	9.34	1.40	1.39	1.36	3
20.14	20.07	8.78	1.39	1.38	1.35	3
18.80	18.73	8.21	1.38	1.37	1.34	3
18.80	18.73	8.21	1.34	1.33	1.31	2
16.88	16.81	7.39	1.33	1.32	1.30	2
14.97	14.91	6.57	1.32	1.31	1.29	2
13.07	13.02	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.94	569.30	263.07	306.24	301.42	4.81	6
58.44	605.52	265.13	340.39	333.02	7.37	6
57.93	641.71	267.30	374.41	364.59	9.82	6
57.43	677.87	269.61	408.26	396.13	12.13	6
56.92	713.99	272.10	441.89	427.63	14.26	6
56.42	750.08	274.80	475.28	459.10	16.18	6
55.91	786.13	277.75	508.38	490.53	17.85	6
55.41	822.13	280.97	541.16	521.91	19.25	6
54.91	858.09	284.49	573.60	553.25	20.35	6
54.91	858.09	284.49	573.60	553.25	20.35	5
53.78	954.19	309.48	644.71	623.60	21.11	5
52.67	1049.40	334.54	714.86	693.06	21.80	5
51.57	1143.71	359.66	784.05	761.62	22.43	5
50.49	1237.12	384.84	852.28	829.28	23.00	5
49.42	1329.62	410.05	919.57	896.03	23.54	5
48.36	1421.22	435.26	985.96	961.88	24.08	5
48.36	1421.22	435.26	985.96	961.88	24.08	4
46.39	1620.00	506.42	1113.59	1084.80	28.78	4
44.43	1818.25	552.66	1265.59	1207.19	58.40	4
42.48	2015.93	600.08	1415.85	1329.02	86.84	4
40.53	2213.05	649.13	1563.92	1450.27	113.65	4
38.60	2409.56	700.30	1709.26	1570.93	138.33	4
36.68	2605.45	754.17	1851.28	1690.96	160.32	4
34.76	2800.68	811.50	1989.18	1810.32	178.86	4
32.86	2995.19	873.40	2121.79	1928.98	192.81	4
30.97	3188.94	941.67	2247.27	2046.86	200.41	4
30.97	3188.94	941.67	2247.27	2046.86	200.41	3

29.59	3337.10	996.22	2340.88	2133.17	207.71	3
28.21	3484.92	1059.37	2425.55	2219.13	206.42	3
26.84	3632.37	1122.31	2510.06	2304.72	205.34	3
25.47	3779.48	1184.44	2595.04	2389.97	205.07	3
24.11	3926.24	1245.81	2680.43	2474.87	205.56	3
22.76	4072.65	1306.37	2766.28	2559.43	206.86	3
21.41	4218.73	1366.22	2852.51	2643.65	208.86	3
20.07	4364.47	1425.36	2939.11	2727.53	211.58	3
18.73	4509.89	1483.94	3025.94	2811.08	214.86	3
18.73	4509.89	1483.94	3025.94	2811.08	214.86	2
16.81	4715.25	1563.43	3151.82	2930.35	221.47	2
14.91	4920.12	1645.30	3274.82	3049.12	225.70	2
13.02	5124.47	1729.53	3394.94	3167.38	227.57	2
11.13	5328.30	1816.60	3511.71	3285.11	226.60	2
9.25	5531.59	1907.11	3624.48	3402.30	222.18	2
7.38	5734.30	2002.69	3731.61	3518.91	212.70	2
5.52	5936.43	2146.32	3790.11	3634.94	155.17	2
3.67	6137.97	2286.85	3851.13	3750.39	100.74	2
1.83	6338.95	2423.29	3915.66	3865.26	50.39	2
.00	6539.37	2555.66	3983.72	3979.59	4.13	2

Time = 2520. Degree of Consolidation = 72.%

Total Settlement = 1.639

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 2520. = 1.639

Settlement caused by Secondary Compression at time 2520. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
5.00	4.83	2.53
3.75	3.61	1.89
2.50	2.40	1.26
1.25	1.20	.63
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.83	.00	.00
3.61	143.38	66.97
2.40	285.65	133.94
1.20	427.58	200.91
.00	569.30	267.88

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
76.41	76.41	.00	1
151.71	151.71	.00	1
226.67	226.67	.00	1
301.42	301.42	.00	1

Time = 2520. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 2520. = .169

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.79

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.80	21.42	6.50	5.69	5.69	6
60.02	58.30	21.35	6.49	5.68	5.68	6
59.45	57.79	21.27	6.47	5.66	5.66	6
58.89	57.29	21.20	6.46	5.65	5.65	6
58.33	56.79	21.12	6.44	5.63	5.64	6
57.76	56.29	21.05	6.43	5.62	5.62	6
57.20	55.79	20.97	6.42	5.61	5.61	6
56.64	55.29	20.90	6.40	5.59	5.59	6
56.08	54.79	20.82	6.39	5.58	5.58	6
56.08	54.79	20.82	4.51	3.84	3.84	5
54.82	53.68	20.59	4.44	3.78	3.78	5
53.56	52.58	20.36	4.38	3.72	3.72	5
52.32	51.49	20.12	4.32	3.65	3.65	5
51.10	50.42	19.89	4.25	3.59	3.59	5
49.88	49.36	19.66	4.19	3.52	3.52	5
48.69	48.32	19.43	4.13	3.46	3.46	5
48.69	48.32	19.43	1.93	1.89	1.89	4
46.69	46.35	18.75	1.92	1.87	1.87	4
44.70	44.40	18.06	1.91	1.86	1.85	4
42.72	42.45	17.38	1.89	1.85	1.83	4
40.75	40.50	16.70	1.88	1.83	1.81	4
38.79	38.57	16.01	1.86	1.82	1.79	4
36.85	36.65	15.33	1.84	1.80	1.76	4
34.91	34.74	14.65	1.82	1.79	1.74	4
33.00	32.84	13.97	1.80	1.77	1.72	4
31.09	30.96	13.28	1.78	1.75	1.70	4
31.09	30.96	13.28	1.47	1.46	1.43	3
29.70	29.58	12.72	1.46	1.45	1.42	3
28.32	28.20	12.16	1.45	1.44	1.41	3
26.94	26.83	11.59	1.44	1.43	1.40	3
25.57	25.46	11.03	1.43	1.42	1.39	3
24.21	24.10	10.47	1.42	1.41	1.38	3
22.84	22.75	9.90	1.41	1.40	1.37	3
21.49	21.40	9.34	1.40	1.39	1.36	3
20.14	20.06	8.78	1.39	1.38	1.35	3
18.80	18.72	8.21	1.38	1.37	1.34	3
18.80	18.72	8.21	1.34	1.33	1.31	2
16.88	16.81	7.39	1.33	1.32	1.30	2
14.97	14.91	6.57	1.32	1.31	1.29	2
13.07	13.01	5.75	1.31	1.30	1.28	2
11.18	11.13	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2

1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.80	569.30	267.88	301.42	301.42	.00	6
58.30	605.43	272.50	332.93	332.94	.00	6
57.79	641.50	277.12	364.38	364.38	.00	6
57.29	677.50	281.74	395.76	395.76	.00	6
56.79	713.43	286.36	427.07	427.07	.00	6
56.29	749.30	290.98	458.32	458.32	.00	6
55.79	785.10	295.60	489.50	489.50	.00	6
55.29	820.84	300.22	520.62	520.62	.00	6
54.79	856.51	304.84	551.67	551.67	.00	6
54.79	856.51	304.84	551.67	551.67	.00	5
53.68	951.87	330.59	621.28	621.28	.00	5
52.58	1046.31	356.34	689.97	689.97	.00	5
51.49	1139.82	382.09	757.73	757.73	.00	5
50.42	1232.41	407.84	824.57	824.57	.00	5
49.36	1324.08	433.59	890.49	890.49	.00	5
48.32	1414.82	459.34	955.48	955.48	.00	5
48.32	1414.82	459.34	955.48	955.48	.00	4
46.35	1613.45	519.41	1094.04	1078.24	15.79	4
44.40	1811.54	564.92	1246.62	1200.48	46.14	4
42.45	2009.08	612.57	1396.51	1322.16	74.35	4
40.50	2206.04	662.15	1543.89	1443.26	100.63	4
38.57	2402.40	713.77	1688.63	1563.76	124.86	4
36.65	2598.13	767.95	1830.18	1683.63	146.55	4
34.74	2793.19	825.61	1967.58	1802.83	164.75	4
32.84	2987.53	887.95	2099.58	1921.32	178.27	4
30.96	3181.09	957.09	2224.00	2039.02	184.98	4
30.96	3181.09	957.09	2224.00	2039.02	184.98	3
29.58	3329.17	1012.45	2316.71	2125.23	191.48	3
28.20	3476.89	1074.80	2402.09	2211.10	190.99	3
26.83	3624.26	1136.55	2487.72	2296.61	191.10	3
25.46	3771.29	1197.65	2573.64	2381.78	191.86	3
24.10	3917.98	1258.06	2659.92	2466.61	193.31	3
22.75	4064.33	1317.79	2746.54	2551.10	195.44	3
21.40	4210.34	1376.92	2833.42	2635.26	198.16	3
20.06	4356.03	1435.51	2920.51	2719.08	201.43	3
18.72	4501.38	1493.58	3007.80	2802.58	205.22	3
18.72	4501.38	1493.58	3007.80	2802.58	205.22	2
16.81	4706.69	1572.12	3134.57	2921.79	212.78	2
14.91	4911.51	1653.35	3258.16	3040.51	217.65	2
13.01	5115.81	1737.02	3378.79	3158.72	220.07	2
11.13	5319.60	1823.54	3496.06	3276.41	219.66	2
9.25	5522.84	1913.50	3609.35	3393.55	215.79	2
7.38	5725.52	2011.07	3714.45	3510.13	204.32	2
5.52	5927.62	2152.85	3774.77	3626.13	148.64	2
3.67	6129.14	2291.51	3837.63	3741.55	96.07	2
1.83	6330.10	2426.18	3903.92	3856.41	47.50	2
.00	6530.52	2555.88	3974.64	3970.73	3.90	2

Time = 2880. Degree of Consolidation = 79.%

Total Settlement = 1.781

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 2880. = 1.781

Settlement caused by Secondary Compression at time 2880. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.65	133.94	151.71	151.71	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 2880. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 2880. = .169

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.65

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.77	21.42	6.50	5.69	5.69	6
60.02	58.26	21.35	6.49	5.67	5.68	6
59.45	57.76	21.27	6.47	5.66	5.66	6
58.89	57.25	21.20	6.46	5.65	5.65	6
58.33	56.75	21.12	6.44	5.63	5.64	6
57.76	56.25	21.05	6.43	5.62	5.62	6
57.20	55.75	20.97	6.42	5.60	5.61	6
56.64	55.25	20.90	6.40	5.59	5.59	6
56.08	54.76	20.82	6.39	5.58	5.58	6
56.08	54.76	20.82	4.51	3.84	3.84	5
54.82	53.64	20.59	4.44	3.78	3.78	5

53.56	52.54	20.36	4.38	3.72	3.72	5
52.32	51.45	20.12	4.32	3.65	3.65	5
51.10	50.38	19.89	4.25	3.59	3.59	5
49.88	49.33	19.66	4.19	3.52	3.52	5
48.69	48.29	19.43	4.13	3.46	3.46	5
48.69	48.29	19.43	1.93	1.89	1.89	4
46.69	46.32	18.75	1.92	1.87	1.87	4
44.70	44.36	18.06	1.91	1.86	1.85	4
42.72	42.41	17.38	1.89	1.85	1.83	4
40.75	40.47	16.70	1.88	1.83	1.81	4
38.79	38.55	16.01	1.86	1.82	1.79	4
36.85	36.63	15.33	1.84	1.80	1.76	4
34.91	34.72	14.65	1.82	1.78	1.74	4
33.00	32.82	13.97	1.80	1.77	1.72	4
31.09	30.94	13.28	1.78	1.75	1.70	4
31.09	30.94	13.28	1.47	1.45	1.43	3
29.70	29.56	12.72	1.46	1.45	1.42	3
28.32	28.19	12.16	1.45	1.44	1.41	3
26.94	26.82	11.59	1.44	1.43	1.40	3
25.57	25.45	11.03	1.43	1.42	1.39	3
24.21	24.09	10.47	1.42	1.41	1.38	3
22.84	22.74	9.90	1.41	1.40	1.37	3
21.49	21.39	9.34	1.40	1.39	1.36	3
20.14	20.05	8.78	1.39	1.38	1.35	3
18.80	18.71	8.21	1.38	1.37	1.34	3
18.80	18.71	8.21	1.34	1.33	1.31	2
16.88	16.81	7.39	1.33	1.32	1.30	2
14.97	14.90	6.57	1.32	1.31	1.29	2
13.07	13.01	5.75	1.31	1.30	1.28	2
11.18	11.12	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.77	569.30	267.88	301.42	301.42	.00	6
58.26	605.43	272.50	332.93	332.93	.00	6
57.76	641.48	277.12	364.36	364.36	.00	6
57.25	677.47	281.74	395.73	395.73	.00	6
56.75	713.40	286.36	427.04	427.04	.00	6
56.25	749.26	290.98	458.28	458.28	.00	6
55.75	785.05	295.60	489.45	489.45	.00	6
55.25	820.77	300.22	520.55	520.55	.00	6
54.76	856.44	304.84	551.59	551.59	.00	6
54.76	856.44	304.84	551.59	551.59	.00	5
53.64	951.79	330.59	621.20	621.20	.00	5
52.54	1046.22	356.34	689.88	689.88	.00	5
51.45	1139.73	382.09	757.64	757.64	.00	5
50.38	1232.31	407.84	824.47	824.47	.00	5
49.33	1323.97	433.59	890.38	890.38	.00	5
48.29	1414.71	459.34	955.37	955.37	.00	5
48.29	1414.71	459.34	955.36	955.37	.00	4
46.32	1613.30	524.77	1088.53	1078.10	10.43	4
44.36	1811.31	574.01	1237.29	1200.25	37.05	4
42.41	2008.72	623.66	1385.06	1321.81	63.26	4
40.47	2205.55	674.26	1531.28	1442.77	88.51	4
38.55	2401.75	726.57	1675.18	1563.12	112.07	4

36.63	2597.32	781.33	1816.00	1682.83	133.17	4
34.72	2792.22	839.61	1952.61	1801.86	150.75	4
32.82	2986.39	902.87	2083.53	1920.18	163.35	4
30.94	3179.77	973.46	2206.31	2037.70	168.61	4
30.94	3179.77	973.46	2206.31	2037.70	168.61	3
29.56	3327.74	1030.18	2297.56	2123.81	173.75	3
28.19	3475.37	1091.13	2384.24	2209.58	174.66	3
26.82	3622.65	1151.56	2471.09	2295.00	176.09	3
25.45	3769.60	1211.43	2558.17	2380.09	178.08	3
24.09	3916.21	1270.86	2645.36	2464.85	180.51	3
22.74	4062.49	1329.80	2732.69	2549.27	183.42	3
21.39	4208.44	1388.19	2820.25	2633.36	186.89	3
20.05	4354.06	1446.17	2907.89	2717.12	190.77	3
18.71	4499.36	1503.75	2995.61	2800.56	195.05	3
18.71	4499.36	1503.75	2995.61	2800.56	195.05	2
16.81	4704.61	1581.33	3123.28	2919.71	203.57	2
14.90	4909.37	1661.61	3247.76	3038.37	209.38	2
13.01	5113.63	1744.60	3369.03	3156.54	212.50	2
11.12	5317.37	1830.43	3486.94	3274.18	212.76	2
9.25	5520.58	1919.70	3600.88	3391.29	209.59	2
7.38	5723.22	2018.95	3704.27	3507.83	196.44	2
5.52	5925.29	2159.05	3766.24	3623.80	142.44	2
3.67	6126.79	2295.60	3831.18	3739.20	91.98	2
1.83	6327.73	2428.27	3899.47	3854.05	45.42	2
.00	6528.15	2556.04	3972.11	3968.36	3.74	2

Time = 3240. Degree of Consolidation = 80.%

Total Settlement = 1.819

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 3240. = 1.817

Settlement caused by Secondary Compression at time 3240. = .002

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
5.00	4.83	2.53
3.75	3.61	1.89
2.50	2.40	1.26
1.25	1.20	.63
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.83	.00	.00
3.61	143.38	66.97
2.40	285.65	133.94
1.20	427.58	200.91
.00	569.30	267.88

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
76.41	76.41	.00	1
151.71	151.71	.00	1
226.67	226.67	.00	1
301.42	301.42	.00	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 3240. = .169

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.61

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.73	21.42	6.50	5.69	5.69	6
60.02	58.22	21.35	6.49	5.67	5.68	6
59.45	57.72	21.27	6.47	5.66	5.66	6
58.89	57.22	21.20	6.46	5.64	5.65	6
58.33	56.71	21.12	6.44	5.63	5.64	6
57.76	56.21	21.05	6.43	5.62	5.62	6
57.20	55.71	20.97	6.42	5.60	5.61	6
56.64	55.22	20.90	6.40	5.59	5.59	6
56.08	54.72	20.82	6.39	5.57	5.58	6
56.08	54.72	20.82	4.51	3.84	3.84	5
54.82	53.60	20.59	4.44	3.78	3.78	5
53.56	52.50	20.36	4.38	3.72	3.72	5
52.32	51.42	20.12	4.32	3.65	3.65	5
51.10	50.35	19.89	4.25	3.59	3.59	5
49.88	49.29	19.66	4.19	3.52	3.52	5
48.69	48.25	19.43	4.13	3.46	3.46	5
48.69	48.25	19.43	1.93	1.89	1.89	4
46.69	46.28	18.75	1.92	1.87	1.87	4
44.70	44.33	18.06	1.91	1.86	1.85	4
42.72	42.38	17.38	1.89	1.84	1.83	4
40.75	40.44	16.70	1.88	1.83	1.81	4
38.79	38.52	16.01	1.86	1.81	1.79	4
36.85	36.60	15.33	1.84	1.80	1.76	4
34.91	34.69	14.65	1.82	1.78	1.74	4
33.00	32.80	13.97	1.80	1.76	1.72	4
31.09	30.92	13.28	1.78	1.74	1.70	4
31.09	30.92	13.28	1.47	1.45	1.43	3
29.70	29.54	12.72	1.46	1.44	1.42	3
28.32	28.17	12.16	1.45	1.43	1.41	3
26.94	26.80	11.59	1.44	1.42	1.40	3
25.57	25.44	11.03	1.43	1.41	1.39	3
24.21	24.08	10.47	1.42	1.40	1.38	3
22.84	22.73	9.90	1.41	1.39	1.37	3
21.49	21.39	9.34	1.40	1.39	1.36	3
20.14	20.04	8.78	1.39	1.38	1.35	3
18.80	18.71	8.21	1.38	1.37	1.34	3
18.80	18.71	8.21	1.34	1.33	1.31	2
16.88	16.80	7.39	1.33	1.32	1.30	2
14.97	14.90	6.57	1.32	1.31	1.29	2
13.07	13.01	5.75	1.31	1.30	1.28	2

11.18	11.12	4.93	1.30	1.29	1.27	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.73	569.30	267.88	301.42	301.42	.00	6
58.22	605.42	272.50	332.92	332.92	.00	6
57.72	641.47	277.12	364.35	364.35	.00	6
57.22	677.44	281.74	395.71	395.71	.00	6
56.71	713.36	286.36	427.00	427.00	.00	6
56.21	749.21	290.98	458.23	458.23	.00	6
55.71	784.99	295.60	489.39	489.39	.00	6
55.22	820.70	300.22	520.48	520.48	.00	6
54.72	856.35	304.84	551.51	551.51	.00	6
54.72	856.35	304.84	551.51	551.51	.00	5
53.60	951.70	330.59	621.11	621.11	.00	5
52.50	1046.12	356.34	689.78	689.78	.00	5
51.42	1139.62	382.09	757.53	757.53	.00	5
50.35	1232.20	407.84	824.36	824.36	.00	5
49.29	1323.85	433.59	890.26	890.26	.00	5
48.25	1414.58	459.34	955.23	955.23	.00	5
48.25	1414.58	459.34	955.23	955.23	.00	4
46.28	1613.15	527.13	1086.02	1077.95	8.07	4
44.33	1811.12	578.79	1232.33	1200.06	32.27	4
42.38	2008.47	630.73	1377.73	1321.55	56.18	4
40.44	2205.19	683.48	1521.71	1442.41	79.29	4
38.52	2401.28	737.68	1663.59	1562.64	100.95	4
36.60	2596.70	794.10	1802.61	1682.21	120.40	4
34.69	2791.44	853.88	1937.56	1801.08	136.48	4
32.80	2985.43	918.71	2066.73	1919.22	147.51	4
30.92	3178.61	991.27	2187.34	2036.54	150.80	4
30.92	3178.61	991.27	2187.34	2036.54	150.80	3
29.54	3326.47	1049.88	2276.58	2122.53	154.05	3
28.17	3473.99	1109.56	2364.43	2208.19	156.23	3
26.80	3621.17	1168.80	2452.37	2293.52	158.85	3
25.44	3768.03	1227.55	2540.48	2378.52	161.96	3
24.08	3914.55	1285.94	2628.61	2463.18	165.43	3
22.73	4060.75	1343.91	2716.84	2547.52	169.31	3
21.39	4206.62	1401.45	2805.17	2631.54	173.63	3
20.04	4352.17	1458.64	2893.53	2715.23	178.30	3
18.71	4497.40	1515.61	2981.79	2798.60	183.19	3
18.71	4497.40	1515.61	2981.79	2798.60	183.19	2
16.80	4702.58	1591.98	3110.60	2917.68	192.92	2
14.90	4907.28	1671.04	3236.24	3036.28	199.96	2
13.01	5111.48	1753.24	3358.24	3154.39	203.86	2
11.12	5315.17	1838.28	3476.89	3271.98	204.91	2
9.25	5518.33	1926.76	3591.57	3389.04	202.53	2
7.38	5720.93	2027.92	3693.01	3505.54	187.47	2
5.52	5922.97	2166.11	3756.86	3621.48	135.38	2
3.67	6124.44	2300.27	3824.18	3736.86	87.32	2
1.83	6325.38	2430.64	3894.74	3851.69	43.04	2
.00	6525.78	2556.22	3969.56	3966.00	3.56	2

Time = 3650. Degree of Consolidation = 82.%

Total Settlement = 1.857

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 3650. = 1.853

Settlement caused by Secondary Compression at time 3650. = .004

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.65	133.94	151.71	151.71	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 3650. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 3650. = .169

Settlement caused by Secondary Compression at time 3650. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.57

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.67	21.42	6.50	5.69	5.69	6
60.02	58.17	21.35	6.49	5.67	5.68	6
59.45	57.67	21.27	6.47	5.66	5.66	6
58.89	57.16	21.20	6.46	5.64	5.65	6
58.33	56.66	21.12	6.44	5.63	5.64	6
57.76	56.16	21.05	6.43	5.61	5.62	6

57.20	55.66	20.97	6.42	5.60	5.61	6
56.64	55.16	20.90	6.40	5.59	5.59	6
56.08	54.67	20.82	6.39	5.57	5.58	6
56.08	54.67	20.82	4.51	3.84	3.84	5
54.82	53.55	20.59	4.44	3.78	3.78	5
53.56	52.45	20.36	4.38	3.71	3.72	5
52.32	51.37	20.12	4.32	3.65	3.65	5
51.10	50.30	19.89	4.25	3.59	3.59	5
49.88	49.24	19.66	4.19	3.52	3.52	5
48.69	48.20	19.43	4.13	3.46	3.46	5
48.69	48.20	19.43	1.93	1.89	1.89	4
46.69	46.23	18.75	1.92	1.87	1.87	4
44.70	44.28	18.06	1.91	1.86	1.85	4
42.72	42.33	17.38	1.89	1.84	1.83	4
40.75	40.39	16.70	1.88	1.83	1.81	4
38.79	38.47	16.01	1.86	1.81	1.79	4
36.85	36.56	15.33	1.84	1.79	1.76	4
34.91	34.66	14.65	1.82	1.78	1.74	4
33.00	32.77	13.97	1.80	1.76	1.72	4
31.09	30.89	13.28	1.78	1.74	1.70	4
31.09	30.89	13.28	1.47	1.45	1.43	3
29.70	29.51	12.72	1.46	1.44	1.42	3
28.32	28.14	12.16	1.45	1.43	1.41	3
26.94	26.78	11.59	1.44	1.42	1.40	3
25.57	25.42	11.03	1.43	1.41	1.39	3
24.21	24.07	10.47	1.42	1.40	1.38	3
22.84	22.72	9.90	1.41	1.39	1.37	3
21.49	21.37	9.34	1.40	1.38	1.36	3
20.14	20.03	8.78	1.39	1.37	1.35	3
18.80	18.70	8.21	1.38	1.36	1.34	3
18.80	18.70	8.21	1.34	1.33	1.31	2
16.88	16.79	7.39	1.33	1.32	1.30	2
14.97	14.89	6.57	1.32	1.31	1.29	2
13.07	13.00	5.75	1.31	1.30	1.28	2
11.18	11.12	4.93	1.30	1.29	1.27	2
9.30	9.24	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.25	2
3.70	3.67	1.64	1.26	1.25	1.24	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.67	569.30	267.88	301.42	301.42	.00	6
58.17	605.41	272.50	332.92	332.92	.00	6
57.67	641.45	277.12	364.33	364.33	.00	6
57.16	677.42	281.74	395.68	395.68	.00	6
56.66	713.32	286.36	426.96	426.96	.00	6
56.16	749.16	290.98	458.18	458.18	.00	6
55.66	784.93	295.60	489.33	489.33	.00	6
55.16	820.64	300.22	520.42	520.42	.00	6
54.67	856.28	304.84	551.44	551.44	.00	6
54.67	856.28	304.84	551.44	551.44	.00	5
53.55	951.61	330.59	621.02	621.02	.00	5
52.45	1046.02	356.34	689.68	689.68	.00	5
51.37	1139.51	382.09	757.42	757.42	.00	5
50.30	1232.07	407.84	824.23	824.23	.00	5
49.24	1323.71	433.59	890.12	890.12	.00	5
48.20	1414.42	459.34	955.08	955.08	.00	5
48.20	1414.42	459.34	955.08	955.08	.00	4

46.23	1612.98	529.73	1083.25	1077.78	5.47	4
44.28	1810.90	584.15	1226.75	1199.84	26.91	4
42.33	2008.17	638.84	1369.33	1321.25	48.08	4
40.39	2204.78	694.35	1510.43	1442.00	68.42	4
38.47	2400.72	751.25	1649.47	1562.08	87.39	4
36.56	2595.97	810.44	1785.53	1681.47	104.05	4
34.66	2790.49	873.04	1917.45	1800.14	117.32	4
32.77	2984.24	940.92	2043.32	1918.02	125.29	4
30.89	3177.13	1015.61	2161.53	2035.06	126.47	4
30.89	3177.13	1015.61	2161.53	2035.06	126.47	3
29.51	3324.84	1076.32	2248.52	2120.91	127.61	3
28.14	3472.22	1135.88	2336.33	2206.42	129.91	3
26.78	3619.26	1194.49	2424.76	2291.61	133.16	3
25.42	3765.97	1252.46	2513.51	2376.46	137.05	3
24.07	3912.35	1309.91	2602.44	2460.99	141.45	3
22.72	4058.42	1366.85	2691.57	2545.19	146.37	3
21.37	4204.17	1423.37	2780.79	2629.08	151.71	3
20.03	4349.60	1479.61	2869.99	2712.65	157.34	3
18.70	4494.71	1535.69	2959.02	2795.91	163.11	3
18.70	4494.71	1535.69	2959.02	2795.91	163.11	2
16.79	4699.77	1610.35	3089.42	2914.87	174.55	2
14.89	4904.36	1687.72	3216.64	3033.36	183.28	2
13.00	5108.47	1768.23	3340.24	3151.37	188.87	2
11.12	5312.07	1851.56	3460.51	3268.88	191.64	2
9.24	5515.15	1938.29	3576.87	3385.86	191.00	2
7.38	5717.69	2042.10	3675.59	3502.30	173.29	2
5.52	5919.67	2176.72	3742.96	3618.19	124.77	2
3.67	6121.11	2307.27	3813.84	3733.53	80.31	2
1.83	6322.03	2434.21	3887.82	3848.34	39.47	2
.00	6522.43	2556.50	3965.92	3962.64	3.28	2

Time = 4320. Degree of Consolidation = 84.%

Total Settlement = 1.911

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 4320. = 1.904

Settlement caused by Secondary Compression at time 4320. = .007

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
5.00	4.83	2.53
3.75	3.61	1.89
2.50	2.40	1.26
1.25	1.20	.63
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.83	.00	.00
3.61	143.38	66.97

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
76.41	76.41	.00	1

2.40	285.65	133.94	151.71	151.71	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 4320. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 4320. = .169

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.52

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.63	21.42	6.50	5.69	5.69	6
60.02	58.12	21.35	6.49	5.67	5.68	6
59.45	57.62	21.27	6.47	5.65	5.66	6
58.89	57.12	21.20	6.46	5.64	5.65	6
58.33	56.61	21.12	6.44	5.63	5.64	6
57.76	56.11	21.05	6.43	5.61	5.62	6
57.20	55.61	20.97	6.42	5.60	5.61	6
56.64	55.12	20.90	6.40	5.58	5.59	6
56.08	54.62	20.82	6.39	5.57	5.58	6
56.08	54.62	20.82	4.51	3.84	3.84	5
54.82	53.50	20.59	4.44	3.78	3.78	5
53.56	52.40	20.36	4.38	3.71	3.72	5
52.32	51.32	20.12	4.32	3.65	3.65	5
51.10	50.25	19.89	4.25	3.59	3.59	5
49.88	49.19	19.66	4.19	3.52	3.52	5
48.69	48.15	19.43	4.13	3.46	3.46	5
48.69	48.15	19.43	1.93	1.89	1.89	4
46.69	46.19	18.75	1.92	1.87	1.87	4
44.70	44.23	18.06	1.91	1.86	1.85	4
42.72	42.29	17.38	1.89	1.84	1.83	4
40.75	40.35	16.70	1.88	1.82	1.81	4
38.79	38.43	16.01	1.86	1.81	1.79	4
36.85	36.52	15.33	1.84	1.79	1.76	4
34.91	34.62	14.65	1.82	1.77	1.74	4
33.00	32.73	13.97	1.80	1.75	1.72	4
31.09	30.86	13.28	1.78	1.73	1.70	4
31.09	30.86	13.28	1.47	1.44	1.43	3
29.70	29.49	12.72	1.46	1.43	1.42	3
28.32	28.12	12.16	1.45	1.42	1.41	3
26.94	26.76	11.59	1.44	1.42	1.40	3
25.57	25.40	11.03	1.43	1.41	1.39	3
24.21	24.05	10.47	1.42	1.40	1.38	3
22.84	22.70	9.90	1.41	1.39	1.37	3
21.49	21.36	9.34	1.40	1.38	1.36	3
20.14	20.02	8.78	1.39	1.37	1.35	3

18.80	18.69	8.21	1.38	1.36	1.34	3
18.80	18.69	8.21	1.34	1.32	1.31	2
16.88	16.78	7.39	1.33	1.31	1.30	2
14.97	14.88	6.57	1.32	1.31	1.29	2
13.07	13.00	5.75	1.31	1.30	1.28	2
11.18	11.11	4.93	1.30	1.29	1.27	2
9.30	9.24	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.25	1.25	2
3.70	3.67	1.64	1.26	1.24	1.24	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.63	569.30	267.88	301.42	301.42	.00	6
58.12	605.41	272.50	332.91	332.91	.00	6
57.62	641.43	277.12	364.32	364.32	.00	6
57.12	677.39	281.74	395.66	395.66	.00	6
56.61	713.29	286.36	426.93	426.93	.00	6
56.11	749.12	290.98	458.14	458.14	.00	6
55.61	784.88	295.60	489.28	489.28	.00	6
55.12	820.58	300.22	520.36	520.36	.00	6
54.62	856.21	304.84	551.37	551.37	.00	6
54.62	856.21	304.84	551.37	551.37	.00	5
53.50	951.53	330.59	620.94	620.94	.00	5
52.40	1045.92	356.34	689.58	689.58	.00	5
51.32	1139.39	382.09	757.30	757.30	.00	5
50.25	1231.94	407.84	824.10	824.10	.00	5
49.19	1323.56	433.59	889.97	889.97	.00	5
48.15	1414.26	459.34	954.92	954.92	.00	5
48.15	1414.26	459.34	954.92	954.92	.00	4
46.19	1612.81	531.66	1081.15	1077.61	3.54	4
44.23	1810.70	588.14	1222.56	1199.64	22.92	4
42.29	2007.90	645.02	1362.89	1320.98	41.90	4
40.35	2204.43	702.77	1501.66	1441.65	60.01	4
38.43	2400.25	762.02	1638.23	1561.62	76.62	4
36.52	2595.36	823.61	1771.75	1680.86	90.89	4
34.62	2789.71	888.74	1900.97	1799.36	101.62	4
32.73	2983.25	959.31	2023.95	1917.04	106.91	4
30.86	3175.92	1035.15	2140.77	2033.84	106.93	4
30.86	3175.92	1035.15	2140.77	2033.84	106.93	3
29.49	3323.52	1096.98	2226.54	2119.58	106.95	3
28.12	3470.77	1157.41	2313.36	2204.98	108.38	3
26.76	3617.68	1216.65	2401.03	2290.03	111.00	3
25.40	3764.27	1274.86	2489.41	2374.76	114.64	3
24.05	3910.53	1332.20	2578.33	2459.16	119.16	3
22.70	4056.47	1388.91	2667.56	2543.25	124.32	3
21.36	4202.10	1445.03	2757.07	2627.01	130.06	3
20.02	4347.41	1500.69	2846.71	2710.46	136.25	3
18.69	4492.40	1556.05	2936.35	2793.60	142.75	3
18.69	4492.40	1556.05	2936.35	2793.60	142.75	2
16.78	4697.34	1629.11	3068.23	2912.44	155.79	2
14.88	4901.83	1704.90	3196.93	3030.83	166.10	2
13.00	5105.83	1783.82	3322.01	3148.74	173.28	2
11.11	5309.34	1865.55	3443.79	3266.15	177.64	2
9.24	5512.34	1950.67	3561.68	3383.05	178.63	2
7.38	5714.81	2057.15	3657.66	3499.42	158.24	2
5.52	5916.74	2187.80	3728.94	3615.25	113.69	2
3.67	6118.14	2314.59	3803.55	3730.56	73.00	2
1.83	6319.03	2437.94	3881.10	3845.35	35.75	2

.00	6519.42	2556.79	3962.63	3959.64	2.99	2

Time = 5040. Degree of Consolidation = 87.%

Total Settlement = 1.959

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 5040. = 1.950

Settlement caused by Secondary Compression at time 5040. = .009

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.65	133.94	151.71	151.71	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 5040. = .169

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.47

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.60	21.42	6.50	5.69	5.69	6

60.02	58.10	21.35	6.49	5.67	5.68	6
59.45	57.59	21.27	6.47	5.65	5.66	6
58.89	57.09	21.20	6.46	5.64	5.65	6
58.33	56.59	21.12	6.44	5.63	5.64	6
57.76	56.09	21.05	6.43	5.61	5.62	6
57.20	55.59	20.97	6.42	5.60	5.61	6
56.64	55.09	20.90	6.40	5.58	5.59	6
56.08	54.59	20.82	6.39	5.57	5.58	6
56.08	54.59	20.82	4.51	3.84	3.84	5
54.82	53.48	20.59	4.44	3.78	3.78	5
53.56	52.38	20.36	4.38	3.71	3.72	5
52.32	51.30	20.12	4.32	3.65	3.65	5
51.10	50.22	19.89	4.25	3.58	3.59	5
49.88	49.17	19.66	4.19	3.52	3.52	5
48.69	48.13	19.43	4.13	3.46	3.46	5
48.69	48.13	19.43	1.93	1.89	1.89	4
46.69	46.16	18.75	1.92	1.87	1.87	4
44.70	44.21	18.06	1.91	1.85	1.85	4
42.72	42.26	17.38	1.89	1.84	1.83	4
40.75	40.33	16.70	1.88	1.82	1.81	4
38.79	38.41	16.01	1.86	1.81	1.79	4
36.85	36.50	15.33	1.84	1.79	1.76	4
34.91	34.60	14.65	1.82	1.77	1.74	4
33.00	32.72	13.97	1.80	1.75	1.72	4
31.09	30.85	13.28	1.78	1.73	1.70	4
31.09	30.85	13.28	1.47	1.44	1.43	3
29.70	29.47	12.72	1.46	1.43	1.42	3
28.32	28.11	12.16	1.45	1.42	1.41	3
26.94	26.74	11.59	1.44	1.41	1.40	3
25.57	25.39	11.03	1.43	1.40	1.39	3
24.21	24.04	10.47	1.42	1.40	1.38	3
22.84	22.69	9.90	1.41	1.39	1.37	3
21.49	21.35	9.34	1.40	1.38	1.36	3
20.14	20.01	8.78	1.39	1.37	1.35	3
18.80	18.68	8.21	1.38	1.36	1.34	3
18.80	18.68	8.21	1.34	1.32	1.31	2
16.88	16.78	7.39	1.33	1.31	1.30	2
14.97	14.88	6.57	1.32	1.30	1.29	2
13.07	12.99	5.75	1.31	1.29	1.28	2
11.18	11.11	4.93	1.30	1.29	1.27	2
9.30	9.24	4.11	1.29	1.28	1.26	2
7.43	7.37	3.29	1.28	1.26	1.25	2
5.56	5.52	2.46	1.27	1.25	1.25	2
3.70	3.67	1.64	1.26	1.24	1.24	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.60	569.30	267.88	301.42	301.42	.00	6
58.10	605.40	272.50	332.91	332.91	.00	6
57.59	641.43	277.12	364.31	364.31	.00	6
57.09	677.38	281.74	395.64	395.64	.00	6
56.59	713.27	286.36	426.91	426.91	.00	6
56.09	749.09	290.98	458.11	458.11	.00	6
55.59	784.85	295.60	489.25	489.25	.00	6
55.09	820.54	300.22	520.32	520.32	.00	6
54.59	856.16	304.84	551.32	551.32	.00	6
54.59	856.16	304.84	551.32	551.32	.00	5
53.48	951.48	330.59	620.88	620.88	.00	5
52.38	1045.86	356.34	689.52	689.52	.00	5

51.30	1139.32	382.09	757.23	757.23	.00	5
50.22	1231.86	407.84	824.02	824.02	.00	5
49.17	1323.48	433.59	889.89	889.89	.00	5
48.13	1414.17	459.34	954.83	954.83	.00	5
48.13	1414.17	459.34	954.83	954.83	.00	4
46.16	1612.71	532.70	1080.01	1077.51	2.50	4
44.21	1810.58	590.26	1220.31	1199.52	20.80	4
42.26	2007.75	648.21	1359.54	1320.83	38.71	4
40.33	2204.23	707.03	1497.20	1441.45	55.75	4
38.41	2400.00	767.35	1632.65	1561.36	71.28	4
36.50	2595.04	830.03	1765.00	1680.54	84.47	4
34.60	2789.30	896.33	1892.97	1798.95	94.02	4
32.72	2982.75	968.32	2014.43	1916.53	97.90	4
30.85	3175.30	1044.87	2130.43	2033.22	97.21	4
30.85	3175.30	1044.87	2130.43	2033.22	97.21	3
29.47	3322.84	1107.39	2215.45	2118.91	96.54	3
28.11	3470.03	1168.35	2301.68	2204.24	97.44	3
26.74	3616.88	1227.92	2388.96	2289.23	99.73	3
25.39	3763.41	1286.27	2477.14	2373.90	103.24	3
24.04	3909.60	1343.67	2565.93	2458.24	107.70	3
22.69	4055.48	1400.35	2655.13	2542.25	112.88	3
21.35	4201.04	1456.44	2744.60	2625.96	118.64	3
20.01	4346.28	1512.09	2834.20	2709.34	124.86	3
18.68	4491.22	1567.23	2923.99	2792.42	131.57	3
18.68	4491.22	1567.23	2923.99	2792.42	131.57	2
16.78	4696.09	1639.70	3056.39	2911.19	145.20	2
14.88	4900.51	1714.92	3185.59	3029.51	156.08	2
12.99	5104.46	1792.98	3311.48	3147.36	164.12	2
11.11	5307.92	1873.85	3434.06	3264.72	169.34	2
9.24	5510.87	1958.09	3552.77	3381.58	171.20	2
7.37	5713.29	2066.17	3647.12	3497.90	149.22	2
5.52	5915.19	2194.45	3720.74	3613.70	107.04	2
3.67	6116.57	2318.98	3797.59	3728.98	68.61	2
1.83	6317.45	2440.17	3877.27	3843.76	33.51	2
.00	6517.83	2556.97	3960.87	3958.05	2.82	2

Time = 5475. Degree of Consolidation = 88.%

Total Settlement = 1.984

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 5475. = 1.974

Settlement caused by Secondary Compression at time 5475. = .011

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

XI	Total Stresses	Effective Stresses	Total Pore Pressures	Static Pore Pressures	Excess Pore Pressures	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.65	133.94	151.71	151.71	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 5475. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 5475. = .169

Settlement caused by Secondary Compression at time 5475. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.45

**********Current Conditions in Compressible Foundation**********

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.55	21.42	6.50	5.69	5.69	6
60.02	58.05	21.35	6.49	5.66	5.68	6
59.45	57.54	21.27	6.47	5.65	5.66	6
58.89	57.04	21.20	6.46	5.64	5.65	6
58.33	56.54	21.12	6.44	5.62	5.64	6
57.76	56.04	21.05	6.43	5.61	5.62	6
57.20	55.54	20.97	6.42	5.59	5.61	6
56.64	55.04	20.90	6.40	5.58	5.59	6
56.08	54.55	20.82	6.39	5.57	5.58	6
56.08	54.55	20.82	4.51	3.84	3.84	5
54.82	53.43	20.59	4.44	3.78	3.78	5
53.56	52.33	20.36	4.38	3.71	3.72	5
52.32	51.25	20.12	4.32	3.65	3.65	5
51.10	50.18	19.89	4.25	3.58	3.59	5
49.88	49.12	19.66	4.19	3.52	3.52	5
48.69	48.08	19.43	4.13	3.46	3.46	5
48.69	48.08	19.43	1.93	1.89	1.89	4
46.69	46.12	18.75	1.92	1.87	1.87	4
44.70	44.16	18.06	1.91	1.85	1.85	4
42.72	42.22	17.38	1.89	1.84	1.83	4
40.75	40.29	16.70	1.88	1.82	1.81	4
38.79	38.37	16.01	1.86	1.80	1.79	4
36.85	36.46	15.33	1.84	1.78	1.76	4
34.91	34.56	14.65	1.82	1.77	1.74	4
33.00	32.68	13.97	1.80	1.74	1.72	4
31.09	30.81	13.28	1.78	1.72	1.70	4
31.09	30.81	13.28	1.47	1.44	1.43	3
29.70	29.44	12.72	1.46	1.43	1.42	3
28.32	28.08	12.16	1.45	1.42	1.41	3
26.94	26.72	11.59	1.44	1.41	1.40	3

25.57	25.36	11.03	1.43	1.40	1.39	3
24.21	24.01	10.47	1.42	1.39	1.38	3
22.84	22.67	9.90	1.41	1.38	1.37	3
21.49	21.33	9.34	1.40	1.37	1.36	3
20.14	20.00	8.78	1.39	1.36	1.35	3
18.80	18.67	8.21	1.38	1.36	1.34	3
18.80	18.67	8.21	1.34	1.32	1.31	2
16.88	16.77	7.39	1.33	1.31	1.30	2
14.97	14.87	6.57	1.32	1.30	1.29	2
13.07	12.98	5.75	1.31	1.29	1.28	2
11.18	11.11	4.93	1.30	1.28	1.27	2
9.30	9.23	4.11	1.29	1.27	1.26	2
7.43	7.37	3.29	1.28	1.26	1.25	2
5.56	5.52	2.46	1.27	1.25	1.25	2
3.70	3.67	1.64	1.26	1.24	1.24	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.55	569.30	267.88	301.42	301.42	.00	6
58.05	605.40	272.50	332.90	332.90	.00	6
57.54	641.40	277.12	364.28	364.28	.00	6
57.04	677.35	281.74	395.61	395.61	.00	6
56.54	713.22	286.36	426.86	426.86	.00	6
56.04	749.03	290.98	458.05	458.05	.00	6
55.54	784.77	295.60	489.17	489.17	.00	6
55.04	820.45	300.22	520.23	520.23	.00	6
54.55	856.07	304.84	551.22	551.22	.00	6
54.55	856.07	304.84	551.22	551.22	.00	5
53.43	951.38	330.59	620.78	620.78	.00	5
52.33	1045.76	356.34	689.42	689.42	.00	5
51.25	1139.22	382.09	757.13	757.13	.00	5
50.18	1231.75	407.84	823.91	823.91	.00	5
49.12	1323.36	433.59	889.77	889.77	.00	5
48.08	1414.05	459.34	954.71	954.71	.00	5
48.08	1414.05	459.34	954.71	954.71	.00	4
46.12	1612.58	534.27	1078.32	1077.38	.93	4
44.16	1810.42	593.55	1216.87	1199.36	17.51	4
42.22	2007.54	653.38	1354.16	1320.62	33.54	4
40.29	2203.95	714.14	1489.81	1441.17	48.64	4
38.37	2399.62	776.51	1623.11	1560.98	62.13	4
36.46	2594.53	841.43	1753.10	1680.04	73.07	4
34.56	2788.65	910.30	1878.35	1798.30	80.06	4
32.68	2981.91	985.23	1996.68	1915.70	80.99	4
30.81	3174.24	1063.26	2110.98	2032.17	78.81	4
30.81	3174.24	1063.26	2110.98	2032.17	78.81	3
29.44	3321.68	1127.20	2194.48	2117.74	76.73	3
28.08	3468.75	1189.36	2279.39	2202.96	76.43	3
26.72	3615.49	1249.93	2365.56	2287.84	77.72	3
25.36	3761.88	1309.08	2452.80	2372.38	80.43	3
24.01	3907.95	1366.97	2540.98	2456.58	84.40	3
22.67	4053.70	1423.84	2629.86	2540.47	89.39	3
21.33	4199.12	1479.95	2719.17	2624.04	95.13	3
20.00	4344.24	1535.46	2808.78	2707.29	101.48	3
18.67	4489.04	1590.37	2898.67	2790.24	108.43	3
18.67	4489.04	1590.37	2898.67	2790.24	108.43	2
16.77	4693.77	1662.21	3031.56	2908.87	122.69	2
14.87	4898.05	1736.08	3161.98	3027.06	134.92	2
12.98	5101.88	1812.33	3289.55	3144.78	144.77	2
11.11	5305.22	1891.39	3413.84	3262.03	151.81	2

9.23	5508.07	1973.16	3534.91	3378.78	156.13	2
7.37	5710.42	2084.44	3625.98	3495.03	130.95	2
5.52	5912.25	2207.91	3704.34	3610.76	93.58	2
3.67	6113.58	2327.86	3785.72	3726.00	59.72	2
1.83	6314.43	2444.70	3869.73	3840.75	28.99	2
.00	6514.81	2557.32	3957.49	3955.02	2.47	2

Time = 6480. Degree of Consolidation = 90.%

Total Settlement = 2.033

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 6480. = 2.020

Settlement caused by Secondary Compression at time 6480. = .013

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.65	133.94	151.71	151.71	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 6480. = .169

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.40

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.52	21.42	6.50	5.69	5.69	6
60.02	58.01	21.35	6.49	5.66	5.68	6
59.45	57.51	21.27	6.47	5.65	5.66	6
58.89	57.01	21.20	6.46	5.63	5.65	6
58.33	56.51	21.12	6.44	5.62	5.64	6
57.76	56.01	21.05	6.43	5.61	5.62	6
57.20	55.51	20.97	6.42	5.59	5.61	6
56.64	55.01	20.90	6.40	5.58	5.59	6
56.08	54.52	20.82	6.39	5.56	5.58	6
56.08	54.52	20.82	4.51	3.84	3.84	5
54.82	53.40	20.59	4.44	3.78	3.78	5
53.56	52.30	20.36	4.38	3.71	3.72	5
52.32	51.22	20.12	4.32	3.65	3.65	5
51.10	50.15	19.89	4.25	3.58	3.59	5
49.88	49.09	19.66	4.19	3.52	3.52	5
48.69	48.05	19.43	4.13	3.46	3.46	5
48.69	48.05	19.43	1.93	1.89	1.89	4
46.69	46.08	18.75	1.92	1.87	1.87	4
44.70	44.13	18.06	1.91	1.85	1.85	4
42.72	42.19	17.38	1.89	1.84	1.83	4
40.75	40.26	16.70	1.88	1.82	1.81	4
38.79	38.34	16.01	1.86	1.80	1.79	4
36.85	36.43	15.33	1.84	1.78	1.76	4
34.91	34.54	14.65	1.82	1.76	1.74	4
33.00	32.66	13.97	1.80	1.74	1.72	4
31.09	30.79	13.28	1.78	1.72	1.70	4
31.09	30.79	13.28	1.47	1.44	1.43	3
29.70	29.42	12.72	1.46	1.43	1.42	3
28.32	28.06	12.16	1.45	1.42	1.41	3
26.94	26.70	11.59	1.44	1.41	1.40	3
25.57	25.35	11.03	1.43	1.40	1.39	3
24.21	24.00	10.47	1.42	1.39	1.38	3
22.84	22.66	9.90	1.41	1.38	1.37	3
21.49	21.32	9.34	1.40	1.37	1.36	3
20.14	19.98	8.78	1.39	1.36	1.35	3
18.80	18.66	8.21	1.38	1.35	1.34	3
18.80	18.66	8.21	1.34	1.32	1.31	2
16.88	16.76	7.39	1.33	1.31	1.30	2
14.97	14.86	6.57	1.32	1.30	1.29	2
13.07	12.98	5.75	1.31	1.29	1.28	2
11.18	11.10	4.93	1.30	1.28	1.27	2
9.30	9.23	4.11	1.29	1.27	1.26	2
7.43	7.37	3.29	1.28	1.26	1.25	2
5.56	5.52	2.46	1.27	1.25	1.25	2
3.70	3.67	1.64	1.26	1.24	1.24	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.52	569.30	267.88	301.42	301.42	.00	6
58.01	605.39	272.50	332.89	332.89	.00	6
57.51	641.39	277.12	364.27	364.27	.00	6
57.01	677.32	281.74	395.58	395.58	.00	6
56.51	713.18	286.36	426.82	426.82	.00	6
56.01	748.98	290.98	458.00	458.00	.00	6
55.51	784.71	295.60	489.11	489.11	.00	6

55.01	820.38	300.22	520.16	520.16	.00	6
54.52	855.98	304.84	551.14	551.14	.00	6
54.52	855.98	304.84	551.14	551.14	.00	5
53.40	951.29	330.59	620.70	620.70	.00	5
52.30	1045.68	356.34	689.34	689.34	.00	5
51.22	1139.14	382.09	757.05	757.05	.00	5
50.15	1231.67	407.84	823.83	823.83	.00	5
49.09	1323.28	433.59	889.69	889.69	.00	5
48.05	1413.97	459.34	954.62	954.62	.00	5
48.05	1413.97	459.34	954.62	954.62	.00	4
46.08	1612.49	535.20	1077.29	1077.29	.00	4
44.13	1810.31	595.61	1214.71	1199.25	15.45	4
42.19	2007.41	656.53	1350.88	1320.49	30.39	4
40.26	2203.77	718.51	1485.26	1440.99	44.27	4
38.34	2399.38	782.22	1617.16	1560.74	56.42	4
36.43	2594.21	848.56	1745.65	1679.72	65.93	4
34.54	2788.24	919.05	1869.19	1797.88	71.31	4
32.66	2981.38	996.09	1985.29	1915.17	70.12	4
30.79	3173.58	1075.27	2098.30	2031.50	66.80	4
30.79	3173.58	1075.27	2098.30	2031.50	66.80	3
29.42	3320.94	1140.28	2180.66	2117.00	63.65	3
28.06	3467.94	1203.30	2264.64	2202.15	62.49	3
26.70	3614.59	1264.53	2350.06	2286.94	63.12	3
25.35	3760.90	1324.13	2436.77	2371.40	65.37	3
24.00	3906.89	1382.36	2524.53	2455.52	69.01	3
22.66	4052.54	1439.49	2613.06	2539.32	73.74	3
21.32	4197.88	1495.66	2702.22	2622.80	79.42	3
19.98	4342.91	1551.03	2791.87	2705.96	85.91	3
18.66	4487.62	1605.74	2881.89	2788.82	93.07	3
18.66	4487.62	1605.74	2881.89	2788.82	93.06	2
16.76	4692.26	1677.19	3015.07	2907.36	107.71	2
14.86	4896.46	1750.68	3145.77	3025.46	120.32	2
12.98	5100.19	1826.50	3273.69	3143.09	130.59	2
11.10	5303.45	1904.29	3399.16	3260.26	138.90	2
9.23	5506.23	1984.50	3521.72	3376.94	144.79	2
7.37	5708.50	2098.65	3609.85	3493.11	116.74	2
5.52	5910.29	2218.45	3691.83	3608.80	83.03	2
3.67	6111.58	2334.93	3776.65	3724.00	52.66	2
1.83	6312.41	2448.30	3864.11	3838.73	25.39	2
.00	6512.78	2557.60	3955.18	3953.00	2.19	2

Time = 7300. Degree of Consolidation = 91.%

Total Settlement = 2.065

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 7300. = 2.051

Settlement caused by Secondary Compression at time 7300. = .014

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1

2.50	2.40	1.26	.98	.91	1
1.25	1.20	.63	.98	.90	1
.00	.00	.00	.98	.90	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.65	133.94	151.71	151.71	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 7300. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 7300. = .169

Settlement caused by Secondary Compression at time 7300. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.37

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.46	21.42	6.50	5.69	5.69	6
60.02	57.96	21.35	6.49	5.66	5.68	6
59.45	57.46	21.27	6.47	5.64	5.66	6
58.89	56.95	21.20	6.46	5.63	5.65	6
58.33	56.45	21.12	6.44	5.62	5.64	6
57.76	55.96	21.05	6.43	5.60	5.62	6
57.20	55.46	20.97	6.42	5.59	5.61	6
56.64	54.96	20.90	6.40	5.57	5.59	6
56.08	54.46	20.82	6.39	5.56	5.58	6
56.08	54.46	20.82	4.51	3.84	3.84	5
54.82	53.35	20.59	4.44	3.78	3.78	5
53.56	52.25	20.36	4.38	3.71	3.72	5
52.32	51.16	20.12	4.32	3.65	3.65	5
51.10	50.09	19.89	4.25	3.58	3.59	5
49.88	49.04	19.66	4.19	3.52	3.52	5
48.69	48.00	19.43	4.13	3.46	3.46	5
48.69	48.00	19.43	1.93	1.89	1.89	4
46.69	46.03	18.75	1.92	1.87	1.87	4
44.70	44.08	18.06	1.91	1.85	1.85	4
42.72	42.14	17.38	1.89	1.84	1.83	4
40.75	40.20	16.70	1.88	1.82	1.81	4
38.79	38.29	16.01	1.86	1.80	1.79	4
36.85	36.38	15.33	1.84	1.78	1.76	4
34.91	34.49	14.65	1.82	1.76	1.74	4
33.00	32.62	13.97	1.80	1.74	1.72	4

31.09	30.75	13.28	1.78	1.71	1.70	4
31.09	30.75	13.28	1.47	1.43	1.43	3
29.70	29.39	12.72	1.46	1.42	1.42	3
28.32	28.02	12.16	1.45	1.41	1.41	3
26.94	26.67	11.59	1.44	1.40	1.40	3
25.57	25.32	11.03	1.43	1.39	1.39	3
24.21	23.97	10.47	1.42	1.38	1.38	3
22.84	22.63	9.90	1.41	1.38	1.37	3
21.49	21.29	9.34	1.40	1.37	1.36	3
20.14	19.96	8.78	1.39	1.36	1.35	3
18.80	18.64	8.21	1.38	1.35	1.34	3
18.80	18.64	8.21	1.34	1.31	1.31	2
16.88	16.74	7.39	1.33	1.31	1.30	2
14.97	14.85	6.57	1.32	1.30	1.29	2
13.07	12.97	5.75	1.31	1.29	1.28	2
11.18	11.09	4.93	1.30	1.28	1.27	2
9.30	9.23	4.11	1.29	1.27	1.26	2
7.43	7.37	3.29	1.28	1.26	1.25	2
5.56	5.51	2.46	1.27	1.25	1.25	2
3.70	3.67	1.64	1.26	1.24	1.24	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.23	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.46	569.30	267.88	301.42	301.42	.00	6
57.96	605.37	272.50	332.87	332.87	.00	6
57.46	641.35	277.12	364.23	364.23	.00	6
56.95	677.25	281.74	395.51	395.51	.00	6
56.45	713.09	286.36	426.73	426.74	.00	6
55.96	748.87	290.98	457.89	457.89	.00	6
55.46	784.58	295.60	488.98	488.98	.00	6
54.96	820.22	300.22	520.00	520.00	.00	6
54.46	855.80	304.84	550.96	550.96	.00	6
54.46	855.80	304.84	550.96	550.96	.00	5
53.35	951.11	330.59	620.52	620.52	.00	5
52.25	1045.50	356.34	689.15	689.15	.00	5
51.16	1138.96	382.09	756.86	756.86	.00	5
50.09	1231.49	407.84	823.65	823.65	.00	5
49.04	1323.10	433.59	889.51	889.51	.00	5
48.00	1413.78	459.34	954.44	954.44	.00	5
48.00	1413.78	459.34	954.44	954.44	.00	4
46.03	1612.32	535.20	1077.11	1077.12	.00	4
44.08	1810.12	597.57	1212.55	1199.06	13.49	4
42.14	2007.18	660.63	1346.55	1320.26	26.29	4
40.20	2203.48	724.85	1478.63	1440.70	37.93	4
38.29	2399.00	791.04	1607.96	1560.36	47.60	4
36.38	2593.71	860.16	1733.56	1679.22	54.34	4
34.49	2787.58	933.95	1853.63	1797.23	56.40	4
32.62	2980.53	1013.77	1966.76	1914.31	52.45	4
30.75	3172.49	1094.97	2077.52	2030.41	47.10	4
30.75	3172.49	1094.97	2077.52	2030.41	47.10	3
29.39	3319.73	1161.79	2157.94	2115.80	42.14	3
28.02	3466.61	1226.42	2240.19	2200.82	39.37	3
26.67	3613.13	1289.04	2324.09	2285.48	38.61	3
25.32	3759.30	1349.84	2409.46	2369.79	39.67	3
23.97	3905.13	1408.99	2496.14	2453.77	42.37	3
22.63	4050.64	1466.69	2583.95	2537.41	46.53	3
21.29	4195.82	1523.26	2672.57	2620.74	51.82	3
19.96	4340.69	1578.84	2761.86	2703.75	58.11	3
18.64	4485.25	1633.37	2851.89	2786.45	65.43	3

18.64	4485.25	1633.37	2851.89	2786.45	65.43	2
16.74	4689.72	1704.65	2985.08	2904.82	80.25	2
14.85	4893.75	1777.27	3116.48	3022.75	93.72	2
12.97	5097.32	1851.54	3245.78	3140.23	105.56	2
11.09	5300.44	1927.81	3372.63	3257.24	115.39	2
9.23	5503.07	2009.12	3493.95	3373.78	120.17	2
7.37	5705.23	2125.84	3579.39	3489.84	89.55	2
5.51	5906.91	2239.20	3667.71	3605.43	62.28	2
3.67	6108.14	2349.52	3758.62	3720.55	38.06	2
1.83	6308.92	2455.73	3853.19	3835.23	17.96	2
.00	6509.27	2558.17	3951.10	3949.49	1.61	2

Time = 9125. Degree of Consolidation = 94.%

Total Settlement = 2.122

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 9125. = 2.105

Settlement caused by Secondary Compression at time 9125. = .017

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
5.00	4.83	2.53
3.75	3.61	1.89
2.50	2.40	1.26
1.25	1.20	.63
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.92	.92	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1

***** Stresses *****

XI	Total	Effective
4.83	.00	.00
3.61	143.38	66.97
2.40	285.65	133.94
1.20	427.58	200.91
.00	569.30	267.88

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
76.41	76.41	.00	1
151.71	151.71	.00	1
226.67	226.67	.00	1
301.42	301.42	.00	1

Time = 9125. Degree of Consolidation = 100.%

Total Settlement = .169

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 9125. = .169

Settlement caused by Secondary Compression at time 9125. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.31

****
Consolidation and desiccation of soft layers---dredged fill
****

Problem Bayou Dupont - 6ft Fill Height

**********Soil data for compressible foundation**********

Material Type	Layer Thickness	Numbers of Sub-layers	Ca/Cc	Cr/Cc
2	18.80	10	.015	.114
3	12.30	9	.021	.135
4	17.60	9	.014	.140
5	7.40	6	.012	.097
6	4.50	8	.040	.215

Material type : 2 Specific Gravity of Solids: 2.68

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.510	.000E+00	.100E-02	.398E-03	.650E-02	-.100E+05	-.398E+01
2	1.460	.500E+03	.180E-03	.732E-04	.287E-02	-.833E+04	-.610E+00
3	1.390	.100E+04	.130E-03	.544E-04	.263E-03	-.789E+04	-.429E+00
4	1.270	.200E+04	.526E-04	.232E-04	.150E-03	-.107E+05	-.248E+00
5	1.110	.400E+04	.263E-04	.125E-04	.530E-04	-.194E+05	-.241E+00
6	.960	.800E+04	.132E-04	.673E-05	.294E-04	-.400E+05	-.269E+00
7	.810	.160E+05	.658E-05	.364E-05	.171E-04	-.857E+05	-.312E+00
8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00

8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01
4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit

1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02
5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	6.0	4	.98	10000.	6	1
30.					10000.	6	1
60.					10000.	6	1
120.					10000.	6	1
240.					10000.	6	1
365.					10000.	6	1
540.					10000.	6	1
730.					10000.	6	1
1080.					10000.	6	1
1440.					10000.	6	1
1825.					10000.	6	1
2520.					10000.	6	1
2880.					10000.	6	1
3240.					10000.	6	1
3650.					10000.	6	1
4320.					10000.	6	1
5040.					10000.	6	1
5475.					10000.	6	1
6480.					10000.	6	1
7300.					10000.	6	1
9125.					10000.	6	1

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250
3	.400	.380

4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.249	1.106	.30000E-04	z = .05

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	10000.00
month of initial desiccation	6
elevation of fixed water table	.00
elevation of top of incompres. found.	-62.00

**********Initial Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	21.42	6.50	6.50	5.53	6
60.02	60.02	21.35	6.49	6.49	5.52	6
59.45	59.45	21.27	6.47	6.47	5.50	6
58.89	58.89	21.20	6.46	6.46	5.49	6

58.33	58.33	21.12	6.44	6.44	5.47	6
57.76	57.76	21.05	6.43	6.43	5.46	6
57.20	57.20	20.97	6.42	6.42	5.45	6
56.64	56.64	20.90	6.40	6.40	5.43	6
56.08	56.08	20.82	6.39	6.39	5.42	6
56.08	56.08	20.82	4.51	4.51	3.71	5
54.82	54.82	20.59	4.44	4.44	3.65	5
53.56	53.56	20.36	4.38	4.38	3.58	5
52.32	52.32	20.12	4.32	4.32	3.52	5
51.10	51.10	19.89	4.25	4.25	3.46	5
49.88	49.88	19.66	4.19	4.19	3.39	5
48.69	48.69	19.43	4.13	4.13	3.35	5
48.69	48.69	19.43	1.93	1.93	1.88	4
46.69	46.69	18.75	1.92	1.92	1.86	4
44.70	44.70	18.06	1.91	1.91	1.83	4
42.72	42.72	17.38	1.89	1.89	1.81	4
40.75	40.75	16.70	1.88	1.88	1.79	4
38.79	38.79	16.01	1.86	1.86	1.77	4
36.85	36.85	15.33	1.84	1.84	1.75	4
34.91	34.91	14.65	1.82	1.82	1.73	4
33.00	33.00	13.97	1.80	1.80	1.71	4
31.09	31.09	13.28	1.78	1.78	1.68	4
31.09	31.09	13.28	1.47	1.47	1.42	3
29.70	29.70	12.72	1.46	1.46	1.41	3
28.32	28.32	12.16	1.45	1.45	1.40	3
26.94	26.94	11.59	1.44	1.44	1.39	3
25.57	25.57	11.03	1.43	1.43	1.38	3
24.21	24.21	10.47	1.42	1.42	1.37	3
22.84	22.84	9.90	1.41	1.41	1.36	3
21.49	21.49	9.34	1.40	1.40	1.35	3
20.14	20.14	8.78	1.39	1.39	1.34	3
18.80	18.80	8.21	1.38	1.38	1.33	3
18.80	18.80	8.21	1.34	1.34	1.30	2
16.88	16.88	7.39	1.33	1.33	1.29	2
14.97	14.97	6.57	1.32	1.32	1.28	2
13.07	13.07	5.75	1.31	1.31	1.27	2
11.18	11.18	4.93	1.30	1.30	1.26	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.43	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.24	2
3.70	3.70	1.64	1.26	1.26	1.23	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.25	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	695.85	.00	695.85	374.40	321.45	6
60.02	735.80	4.62	731.18	409.73	321.46	6
59.45	775.68	9.24	766.44	444.99	321.45	6
58.89	815.50	13.86	801.64	480.18	321.46	6
58.33	855.25	18.48	836.77	515.31	321.46	6
57.76	894.93	23.10	871.83	550.38	321.45	6
57.20	934.55	27.72	906.83	585.38	321.46	6
56.64	974.10	32.34	941.76	620.31	321.45	6
56.08	1013.59	36.96	976.63	655.17	321.45	6
56.08	1013.59	36.96	976.63	655.17	321.45	5
54.82	1118.56	62.71	1055.85	734.40	321.45	5
53.56	1222.61	88.46	1134.15	812.70	321.45	5
52.32	1325.74	114.21	1211.53	890.07	321.45	5
51.10	1427.94	139.96	1287.98	966.52	321.45	5
49.88	1529.22	165.71	1363.51	1042.05	321.45	5

48.69	1629.57	191.46	1438.11	1116.66	321.45	5
48.69	1629.57	191.46	1438.11	1116.66	321.45	4
46.69	1830.02	267.32	1562.70	1241.24	321.45	4
44.70	2029.96	343.18	1686.78	1365.32	321.46	4
42.72	2229.35	419.04	1810.31	1488.86	321.45	4
40.75	2428.30	494.90	1933.40	1611.94	321.46	4
38.79	2626.49	570.76	2055.74	1734.28	321.45	4
36.85	2823.79	646.62	2177.18	1855.72	321.45	4
34.91	3020.19	722.48	2297.71	1976.26	321.45	4
33.00	3215.68	798.34	2417.34	2095.89	321.45	4
31.09	3410.26	874.19	2536.07	2214.62	321.45	4
31.09	3410.26	874.19	2536.07	2214.62	321.45	3
29.70	3558.84	936.05	2622.78	2301.33	321.45	3
28.32	3707.01	997.91	2709.09	2387.64	321.45	3
26.94	3854.81	1059.77	2795.04	2473.59	321.46	3
25.57	4002.27	1121.63	2880.64	2559.19	321.45	3
24.21	4149.38	1183.49	2965.90	2644.44	321.45	3
22.84	4296.15	1245.35	3050.80	2729.34	321.46	3
21.49	4442.56	1307.21	3135.36	2813.90	321.45	3
20.14	4588.63	1369.06	3219.56	2898.11	321.45	3
18.80	4734.35	1430.92	3303.43	2981.97	321.46	3
18.80	4734.35	1430.92	3303.42	2981.97	321.45	2
16.88	4940.02	1517.02	3422.99	3101.54	321.45	2
14.97	5145.15	1603.12	3542.04	3220.58	321.45	2
13.07	5349.76	1689.22	3660.55	3339.09	321.46	2
11.18	5553.84	1775.31	3778.53	3457.07	321.46	2
9.30	5757.40	1861.41	3895.98	3574.53	321.46	2
7.43	5960.41	1947.51	4012.90	3691.45	321.46	2
5.56	6162.92	2033.61	4129.31	3807.86	321.46	2
3.70	6365.04	2119.71	4245.33	3923.88	321.45	2
1.85	6566.80	2205.80	4361.00	4039.54	321.46	2
.00	6768.22	2291.90	4476.31	4154.86	321.46	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	6.00	3.03	.98	.98	.98	1
4.50	4.50	2.27	.98	.98	.91	1
3.00	3.00	1.52	.98	.98	.90	1
1.50	1.50	.76	.98	.98	.90	1
.00	.00	.00	.98	.98	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

6.00	.00	.00	.00	.00	.00	1
4.50	173.96	.00	173.96	93.60	80.36	1
3.00	347.93	.00	347.93	187.20	160.73	1
1.50	521.89	.00	521.89	280.80	241.09	1
.00	695.85	.00	695.85	374.40	321.45	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.49	21.42	6.50	5.96	5.53	6
60.02	59.96	21.35	6.49	6.13	5.52	6
59.45	59.41	21.27	6.47	6.26	5.50	6
58.89	58.86	21.20	6.46	6.34	5.49	6
58.33	58.30	21.12	6.44	6.39	5.47	6
57.76	57.74	21.05	6.43	6.41	5.46	6
57.20	57.19	20.97	6.42	6.41	5.45	6
56.64	56.63	20.90	6.40	6.40	5.43	6
56.08	56.07	20.82	6.39	6.39	5.42	6
56.08	56.07	20.82	4.51	4.51	3.71	5
54.82	54.80	20.59	4.44	4.44	3.65	5
53.56	53.54	20.36	4.38	4.38	3.58	5
52.32	52.30	20.12	4.32	4.31	3.52	5
51.10	51.08	19.89	4.25	4.25	3.46	5
49.88	49.87	19.66	4.19	4.19	3.39	5
48.69	48.68	19.43	4.13	4.12	3.35	5
48.69	48.68	19.43	1.93	1.93	1.88	4
46.69	46.68	18.75	1.92	1.92	1.86	4
44.70	44.69	18.06	1.91	1.91	1.83	4
42.72	42.71	17.38	1.89	1.89	1.81	4
40.75	40.74	16.70	1.88	1.88	1.79	4
38.79	38.78	16.01	1.86	1.86	1.77	4
36.85	36.83	15.33	1.84	1.84	1.75	4
34.91	34.90	14.65	1.82	1.82	1.73	4
33.00	32.99	13.97	1.80	1.80	1.71	4
31.09	31.08	13.28	1.78	1.78	1.68	4
31.09	31.08	13.28	1.47	1.47	1.42	3
29.70	29.69	12.72	1.46	1.46	1.41	3
28.32	28.31	12.16	1.45	1.45	1.40	3
26.94	26.93	11.59	1.44	1.44	1.39	3
25.57	25.56	11.03	1.43	1.43	1.38	3
24.21	24.19	10.47	1.42	1.42	1.37	3
22.84	22.83	9.90	1.41	1.41	1.36	3
21.49	21.48	9.34	1.40	1.40	1.35	3
20.14	20.13	8.78	1.39	1.39	1.34	3
18.80	18.79	8.21	1.38	1.38	1.33	3
18.80	18.79	8.21	1.34	1.34	1.30	2

16.88	16.87	7.39	1.33	1.33	1.29	2
14.97	14.96	6.57	1.32	1.32	1.28	2
13.07	13.06	5.75	1.31	1.31	1.27	2
11.18	11.17	4.93	1.30	1.30	1.26	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.55	2.46	1.27	1.27	1.24	2
3.70	3.69	1.64	1.26	1.26	1.23	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.49	683.29	178.97	504.32	361.84	142.48	6
59.96	721.13	123.37	597.76	395.06	202.70	6
59.41	759.68	80.44	679.24	428.99	250.25	6
58.86	798.73	52.21	746.52	463.42	283.10	6
58.30	838.09	37.06	801.03	498.16	302.87	6
57.74	877.59	31.27	846.32	533.04	313.28	6
57.19	917.14	31.10	886.04	567.96	318.08	6
56.63	956.66	33.86	922.79	602.86	319.94	6
56.07	996.12	38.06	958.06	637.71	320.36	6
56.07	996.12	38.06	958.06	637.71	320.36	5
54.80	1101.06	63.59	1037.48	716.90	320.58	5
53.54	1205.08	89.33	1115.75	795.17	320.58	5
52.30	1308.18	115.12	1193.06	872.51	320.55	5
51.08	1410.34	140.89	1269.45	948.93	320.53	5
49.87	1511.59	166.62	1344.97	1024.42	320.54	5
48.68	1611.91	192.28	1419.64	1099.00	320.64	5
48.68	1611.91	192.28	1419.64	1099.00	320.64	4
46.68	1812.35	267.32	1545.03	1223.58	321.45	4
44.69	2012.28	343.18	1669.10	1347.64	321.45	4
42.71	2211.68	421.74	1789.94	1471.19	318.75	4
40.74	2410.52	507.76	1902.75	1594.16	308.59	4
38.78	2608.64	573.60	2035.04	1716.42	318.61	4
36.83	2805.93	646.64	2159.28	1837.85	321.43	4
34.90	3002.32	722.48	2279.84	1958.39	321.45	4
32.99	3197.81	798.34	2399.48	2078.02	321.45	4
31.08	3392.40	874.19	2518.20	2196.75	321.45	4
31.08	3392.40	874.19	2518.20	2196.75	321.45	3
29.69	3540.97	936.05	2604.91	2283.46	321.45	3
28.31	3689.14	997.91	2691.23	2369.77	321.45	3
26.93	3836.94	1060.98	2775.96	2455.72	320.24	3
25.56	3984.39	1123.18	2861.21	2541.31	319.91	3
24.19	4131.49	1185.02	2946.47	2626.55	319.92	3
22.83	4278.25	1246.79	3031.46	2711.45	320.01	3
21.48	4424.66	1308.56	3116.10	2796.00	320.10	3
20.13	4570.72	1370.27	3200.45	2880.20	320.25	3
18.79	4716.43	1431.78	3284.65	2964.05	320.59	3
18.79	4716.43	1431.78	3284.65	2964.05	320.59	2
16.87	4922.09	1517.22	3404.87	3083.62	321.25	2
14.96	5127.23	1603.24	3523.99	3202.66	321.33	2
13.06	5331.84	1689.22	3642.62	3321.17	321.46	2
11.17	5535.92	1775.31	3760.61	3439.15	321.46	2
9.29	5739.48	1861.41	3878.06	3556.61	321.46	2
7.42	5942.49	1947.51	3994.98	3673.53	321.46	2
5.55	6145.02	2033.61	4111.42	3789.96	321.46	2
3.69	6347.11	2123.00	4224.12	3905.95	318.16	2
1.84	6548.84	2243.23	4305.61	4021.58	284.03	2
.00	6749.68	2587.78	4161.90	4136.32	25.58	2

Time = 30. Degree of Consolidation = 4.%

Total Settlement = .096

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 30. = .096

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.80	3.03	.98	.98	.98	1
4.50	4.33	2.27	.98	.91	.91	1
3.00	2.88	1.52	.98	.91	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.90	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.80	.00	.00	.00	.00	.00	1
4.33	171.97	80.36	91.61	91.61	.00	1
2.88	342.60	139.76	202.84	181.87	20.97	1
1.44	512.98	167.48	345.51	271.89	73.61	1
.00	683.29	178.97	504.32	361.84	142.48	1

Time = 30. Degree of Consolidation = 95.%

Total Settlement = .201

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 30. = .201

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 4.30

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.43	21.42	6.50	5.90	5.53	6
60.02	59.91	21.35	6.49	6.03	5.52	6
59.45	59.37	21.27	6.47	6.14	5.50	6
58.89	58.83	21.20	6.46	6.23	5.49	6
58.33	58.28	21.12	6.44	6.30	5.47	6

57.76	57.72	21.05	6.43	6.34	5.46	6
57.20	57.17	20.97	6.42	6.36	5.45	6
56.64	56.61	20.90	6.40	6.37	5.43	6
56.08	56.06	20.82	6.39	6.37	5.42	6
56.08	56.06	20.82	4.51	4.49	3.71	5
54.82	54.79	20.59	4.44	4.44	3.65	5
53.56	53.54	20.36	4.38	4.37	3.58	5
52.32	52.30	20.12	4.32	4.31	3.52	5
51.10	51.07	19.89	4.25	4.25	3.46	5
49.88	49.86	19.66	4.19	4.18	3.39	5
48.69	48.67	19.43	4.13	4.12	3.35	5
48.69	48.67	19.43	1.93	1.93	1.88	4
46.69	46.67	18.75	1.92	1.92	1.86	4
44.70	44.68	18.06	1.91	1.91	1.83	4
42.72	42.70	17.38	1.89	1.89	1.81	4
40.75	40.73	16.70	1.88	1.88	1.79	4
38.79	38.78	16.01	1.86	1.86	1.77	4
36.85	36.83	15.33	1.84	1.84	1.75	4
34.91	34.90	14.65	1.82	1.82	1.73	4
33.00	32.98	13.97	1.80	1.80	1.71	4
31.09	31.08	13.28	1.78	1.78	1.68	4
31.09	31.08	13.28	1.47	1.47	1.42	3
29.70	29.69	12.72	1.46	1.46	1.41	3
28.32	28.31	12.16	1.45	1.45	1.40	3
26.94	26.93	11.59	1.44	1.44	1.39	3
25.57	25.56	11.03	1.43	1.43	1.38	3
24.21	24.19	10.47	1.42	1.42	1.37	3
22.84	22.83	9.90	1.41	1.41	1.36	3
21.49	21.48	9.34	1.40	1.40	1.35	3
20.14	20.13	8.78	1.39	1.39	1.34	3
18.80	18.78	8.21	1.38	1.38	1.33	3
18.80	18.78	8.21	1.34	1.34	1.30	2
16.88	16.87	7.39	1.33	1.33	1.29	2
14.97	14.96	6.57	1.32	1.32	1.28	2
13.07	13.06	5.75	1.31	1.31	1.27	2
11.18	11.17	4.93	1.30	1.30	1.26	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.41	3.29	1.28	1.28	1.25	2
5.56	5.55	2.46	1.27	1.27	1.24	2
3.70	3.69	1.64	1.26	1.26	1.23	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.43	683.15	198.21	484.94	361.69	123.25	6
59.91	720.61	155.53	565.08	394.54	170.54	6
59.37	758.65	118.49	640.16	427.96	212.21	6
58.83	797.16	88.79	708.37	461.85	246.52	6
58.28	836.04	67.12	768.92	496.11	272.81	6
57.72	875.18	53.05	822.13	530.62	291.50	6
57.17	914.46	45.36	869.10	565.29	303.82	6
56.61	953.82	42.48	911.34	600.03	311.31	6
56.06	993.20	42.88	950.32	634.78	315.53	6
56.06	993.20	42.88	950.32	634.78	315.53	5
54.79	1098.01	66.20	1031.81	713.84	317.97	5
53.54	1201.95	90.89	1111.06	792.04	319.03	5
52.30	1305.00	116.23	1188.77	869.33	319.44	5
51.07	1407.13	141.82	1265.32	945.72	319.60	5
49.86	1508.35	167.45	1340.90	1021.18	319.72	5
48.67	1608.64	193.02	1415.62	1095.73	319.89	5

48.67	1608.64	193.02	1415.62	1095.73	319.89	4
46.67	1809.08	267.32	1541.76	1220.30	321.45	4
44.68	2009.01	343.57	1665.43	1344.37	321.06	4
42.70	2208.39	426.42	1781.97	1467.90	314.07	4
40.73	2407.18	512.82	1894.35	1590.82	303.53	4
38.78	2605.25	577.05	2028.20	1713.03	315.16	4
36.83	2802.51	647.56	2154.95	1834.44	320.51	4
34.90	2998.90	722.48	2276.42	1954.97	321.46	4
32.98	3194.39	798.34	2396.06	2074.60	321.45	4
31.08	3388.98	874.19	2514.78	2193.33	321.45	4
31.08	3388.98	874.19	2514.78	2193.33	321.45	3
29.69	3537.55	936.05	2601.49	2280.04	321.45	3
28.31	3685.72	997.91	2687.81	2366.35	321.45	3
26.93	3833.52	1061.84	2771.68	2452.29	319.39	3
25.56	3980.96	1124.50	2856.46	2537.88	318.58	3
24.19	4128.06	1186.47	2941.59	2623.12	318.47	3
22.83	4274.80	1248.22	3026.59	2708.00	318.58	3
21.48	4421.20	1309.86	3111.34	2792.54	318.80	3
20.13	4567.26	1371.39	3195.87	2876.74	319.13	3
18.78	4712.97	1432.64	3280.33	2960.59	319.74	3
18.78	4712.97	1432.64	3280.33	2960.59	319.74	2
16.87	4918.63	1517.55	3401.08	3080.15	320.93	2
14.96	5123.76	1603.36	3520.41	3199.19	321.22	2
13.06	5328.37	1689.25	3639.12	3317.70	321.42	2
11.17	5532.45	1775.31	3757.14	3435.68	321.45	2
9.29	5736.01	1861.41	3874.59	3553.14	321.46	2
7.41	5939.02	1947.51	3991.51	3670.06	321.46	2
5.55	6141.54	2033.61	4107.93	3786.48	321.46	2
3.69	6343.63	2131.34	4212.29	3902.47	309.82	2
1.84	6545.26	2279.19	4266.07	4018.00	248.07	2
.00	6745.98	2593.16	4152.82	4132.62	20.20	2

Time = 60. Degree of Consolidation = 6.%

Total Settlement = .153

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 60. = .153

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
6.00	5.80	3.03
4.50	4.33	2.27
3.00	2.88	1.52
1.50	1.44	.76
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.91	.90	1
.98	.90	.90	1
.98	.90	.89	1

***** Stresses *****

XI	Total	Effective
5.80	.00	.00

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1

4.33	171.98	80.36	91.61	91.61	.00	1
2.88	342.58	148.11	194.47	181.86	12.61	1
1.44	512.92	181.99	330.92	271.83	59.10	1
.00	683.15	198.21	484.94	361.69	123.25	1

Time = 60. Degree of Consolidation = 97.%

Total Settlement = .204

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 60. = .204

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 4.24

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.34	21.42	6.50	5.85	5.53	6
60.02	59.82	21.35	6.49	5.94	5.52	6
59.45	59.29	21.27	6.47	6.03	5.50	6
58.89	58.76	21.20	6.46	6.11	5.49	6
58.33	58.22	21.12	6.44	6.17	5.47	6
57.76	57.67	21.05	6.43	6.23	5.46	6
57.20	57.13	20.97	6.42	6.27	5.45	6
56.64	56.57	20.90	6.40	6.30	5.43	6
56.08	56.02	20.82	6.39	6.32	5.42	6
56.08	56.02	20.82	4.51	4.46	3.71	5
54.82	54.76	20.59	4.44	4.41	3.65	5
53.56	53.51	20.36	4.38	4.36	3.58	5
52.32	52.28	20.12	4.32	4.30	3.52	5
51.10	51.06	19.89	4.25	4.24	3.46	5
49.88	49.85	19.66	4.19	4.18	3.39	5
48.69	48.66	19.43	4.13	4.11	3.35	5
48.69	48.66	19.43	1.93	1.93	1.88	4
46.69	46.66	18.75	1.92	1.92	1.86	4
44.70	44.67	18.06	1.91	1.90	1.83	4
42.72	42.69	17.38	1.89	1.89	1.81	4
40.75	40.72	16.70	1.88	1.87	1.79	4
38.79	38.77	16.01	1.86	1.86	1.77	4
36.85	36.82	15.33	1.84	1.84	1.75	4
34.91	34.89	14.65	1.82	1.82	1.73	4
33.00	32.97	13.97	1.80	1.80	1.71	4
31.09	31.07	13.28	1.78	1.78	1.68	4
31.09	31.07	13.28	1.47	1.47	1.42	3
29.70	29.68	12.72	1.46	1.46	1.41	3
28.32	28.30	12.16	1.45	1.45	1.40	3
26.94	26.92	11.59	1.44	1.44	1.39	3
25.57	25.55	11.03	1.43	1.43	1.38	3
24.21	24.18	10.47	1.42	1.42	1.37	3
22.84	22.82	9.90	1.41	1.41	1.36	3
21.49	21.47	9.34	1.40	1.40	1.35	3
20.14	20.12	8.78	1.39	1.39	1.34	3
18.80	18.78	8.21	1.38	1.38	1.33	3

18.80	18.78	8.21	1.34	1.34	1.30	2
16.88	16.86	7.39	1.33	1.33	1.29	2
14.97	14.95	6.57	1.32	1.32	1.28	2
13.07	13.05	5.75	1.31	1.31	1.27	2
11.18	11.16	4.93	1.30	1.30	1.26	2
9.30	9.28	4.11	1.29	1.29	1.26	2
7.43	7.41	3.29	1.28	1.28	1.25	2
5.56	5.54	2.46	1.27	1.27	1.24	2
3.70	3.68	1.64	1.26	1.26	1.23	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.34	683.06	216.12	466.94	361.60	105.33	6
59.82	720.19	184.67	535.52	394.11	141.40	6
59.29	757.75	155.59	602.16	427.05	175.11	6
58.76	795.70	129.71	666.00	460.39	205.61	6
58.22	834.00	107.65	726.35	494.06	232.29	6
57.67	872.58	89.70	782.88	528.02	254.86	6
57.13	911.39	75.79	835.60	562.21	273.39	6
56.57	950.36	65.55	884.81	596.57	288.24	6
56.02	989.46	58.37	931.09	631.05	300.04	6
56.02	989.46	58.37	931.09	631.05	300.04	5
54.76	1093.80	77.15	1016.65	709.64	307.02	5
53.51	1197.42	98.36	1099.06	787.50	311.56	5
52.28	1300.25	121.30	1178.94	864.58	314.36	5
51.06	1402.23	145.41	1256.81	940.81	316.00	5
49.85	1503.33	170.29	1333.04	1016.16	316.88	5
48.66	1603.52	195.70	1407.83	1090.61	317.22	5
48.66	1603.52	195.70	1407.83	1090.61	317.22	4
46.66	1803.95	268.62	1535.33	1215.17	320.16	4
44.67	2003.86	347.12	1656.74	1339.22	317.52	4
42.69	2203.21	434.00	1769.21	1462.72	306.49	4
40.72	2401.93	518.99	1882.94	1585.58	297.37	4
38.77	2599.93	582.40	2017.53	1707.71	309.81	4
36.82	2797.14	650.38	2146.76	1829.07	317.69	4
34.89	2993.52	722.58	2270.93	1949.58	321.35	4
32.97	3189.01	798.34	2390.67	2069.22	321.46	4
31.07	3383.59	874.19	2509.40	2187.94	321.46	4
31.07	3383.59	874.19	2509.40	2187.94	321.46	3
29.68	3532.16	936.05	2596.11	2274.65	321.46	3
28.30	3680.34	997.91	2682.42	2360.97	321.46	3
26.92	3828.13	1063.10	2765.04	2446.91	318.13	3
25.55	3975.57	1126.66	2848.91	2532.48	316.42	3
24.18	4122.65	1189.05	2933.59	2617.70	315.89	3
22.82	4269.38	1250.86	3018.52	2702.58	315.95	3
21.47	4415.76	1312.33	3103.44	2787.10	316.33	3
20.12	4561.80	1373.53	3188.28	2871.28	316.99	3
18.78	4707.50	1434.33	3273.17	2955.12	318.05	3
18.78	4707.50	1434.33	3273.17	2955.12	318.05	2
16.86	4913.15	1518.36	3394.79	3074.68	320.12	2
14.95	5118.29	1603.63	3514.66	3193.71	320.94	2
13.05	5322.90	1689.39	3633.51	3312.22	321.29	2
11.16	5526.97	1775.31	3751.66	3430.20	321.46	2
9.28	5730.53	1861.41	3869.12	3547.67	321.46	2
7.41	5933.54	1947.51	3986.03	3664.58	321.46	2
5.54	6136.06	2034.42	4101.64	3781.00	320.65	2
3.68	6338.12	2153.10	4185.02	3896.96	288.06	2
1.83	6539.59	2327.44	4212.16	4012.33	199.82	2
.00	6740.17	2597.17	4143.00	4126.81	16.19	2

Time = 120. Degree of Consolidation = 9.%

Total Settlement = .244

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 120. = .244

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.33	2.27	.98	.91	.91	1
3.00	2.88	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.90	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.33	171.98	80.36	91.62	91.62	.00	1
2.88	342.58	152.67	189.91	181.85	8.06	1
1.44	512.88	190.34	322.54	271.79	50.75	1
.00	683.06	216.12	466.94	361.60	105.33	1

Time = 120. Degree of Consolidation = 97.%

Total Settlement = .205

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 120. = .205

Settlement caused by Secondary Compression at time 120. = .000

Surface Elevation = 4.15

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.20	21.42	6.50	5.80	5.53	6
60.02	59.68	21.35	6.49	5.87	5.52	6
59.45	59.16	21.27	6.47	5.94	5.50	6
58.89	58.63	21.20	6.46	6.00	5.49	6

58.33	58.10	21.12	6.44	6.06	5.47	6
57.76	57.56	21.05	6.43	6.11	5.46	6
57.20	57.03	20.97	6.42	6.16	5.45	6
56.64	56.48	20.90	6.40	6.20	5.43	6
56.08	55.94	20.82	6.39	6.24	5.42	6
56.08	55.94	20.82	4.51	4.39	3.71	5
54.82	54.69	20.59	4.44	4.35	3.65	5
53.56	53.46	20.36	4.38	4.30	3.58	5
52.32	52.23	20.12	4.32	4.25	3.52	5
51.10	51.02	19.89	4.25	4.20	3.46	5
49.88	49.82	19.66	4.19	4.14	3.39	5
48.69	48.64	19.43	4.13	4.08	3.35	5
48.69	48.64	19.43	1.93	1.93	1.88	4
46.69	46.64	18.75	1.92	1.92	1.86	4
44.70	44.66	18.06	1.91	1.90	1.83	4
42.72	42.68	17.38	1.89	1.89	1.81	4
40.75	40.71	16.70	1.88	1.87	1.79	4
38.79	38.76	16.01	1.86	1.85	1.77	4
36.85	36.81	15.33	1.84	1.84	1.75	4
34.91	34.88	14.65	1.82	1.82	1.73	4
33.00	32.96	13.97	1.80	1.80	1.71	4
31.09	31.06	13.28	1.78	1.78	1.68	4
31.09	31.06	13.28	1.47	1.47	1.42	3
29.70	29.67	12.72	1.46	1.46	1.41	3
28.32	28.29	12.16	1.45	1.45	1.40	3
26.94	26.91	11.59	1.44	1.44	1.39	3
25.57	25.54	11.03	1.43	1.43	1.38	3
24.21	24.18	10.47	1.42	1.42	1.37	3
22.84	22.82	9.90	1.41	1.41	1.36	3
21.49	21.46	9.34	1.40	1.40	1.35	3
20.14	20.11	8.78	1.39	1.39	1.34	3
18.80	18.77	8.21	1.38	1.38	1.33	3
18.80	18.77	8.21	1.34	1.34	1.30	2
16.88	16.85	7.39	1.33	1.33	1.29	2
14.97	14.95	6.57	1.32	1.32	1.28	2
13.07	13.05	5.75	1.31	1.31	1.27	2
11.18	11.16	4.93	1.30	1.30	1.26	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.25	2
5.56	5.53	2.46	1.27	1.27	1.24	2
3.70	3.68	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.20	682.99	231.26	451.73	361.54	90.19	6
59.68	719.84	208.50	511.34	393.77	117.57	6
59.16	757.01	186.58	570.43	426.32	144.11	6
58.63	794.49	165.81	628.67	459.17	169.50	6
58.10	832.25	146.47	685.78	492.31	193.47	6
57.56	870.27	128.75	741.52	525.71	215.80	6
57.03	908.53	112.80	795.73	559.35	236.38	6
56.48	947.01	98.65	848.35	593.21	255.14	6
55.94	985.67	86.29	899.38	627.26	272.12	6
55.94	985.67	86.29	899.38	627.26	272.12	5
54.69	1089.07	101.80	987.27	704.90	282.37	5
53.46	1191.86	119.57	1072.29	781.95	290.34	5
52.23	1293.99	139.45	1154.54	858.32	296.22	5
51.02	1395.36	161.22	1234.14	933.94	300.20	5
49.82	1495.92	184.73	1311.19	1008.75	302.44	5

48.64	1595.61	209.86	1385.75	1082.69	303.06	5
48.64	1595.61	209.86	1385.75	1082.69	303.06	4
46.64	1795.95	280.33	1515.62	1207.17	308.45	4
44.66	1995.78	358.52	1637.26	1331.14	306.12	4
42.68	2195.05	446.82	1748.23	1454.55	293.68	4
40.71	2393.67	526.96	1866.71	1577.32	289.39	4
38.76	2591.58	589.53	2002.05	1699.37	302.68	4
36.81	2788.72	655.44	2133.27	1820.65	312.63	4
34.88	2985.05	724.97	2260.08	1941.12	318.96	4
32.96	3180.53	798.34	2382.19	2060.74	321.46	4
31.06	3375.11	874.19	2500.92	2179.47	321.45	4
31.06	3375.11	874.19	2500.92	2179.47	321.45	3
29.67	3523.68	936.05	2587.63	2266.18	321.45	3
28.29	3671.86	997.91	2673.95	2352.49	321.45	3
26.91	3819.65	1064.82	2754.84	2438.43	316.41	3
25.54	3967.07	1129.78	2837.30	2523.99	313.31	3
24.18	4114.13	1193.09	2921.05	2609.19	311.85	3
22.82	4260.84	1255.25	3005.59	2694.04	311.55	3
21.46	4407.20	1316.62	3090.58	2778.54	312.04	3
20.11	4553.22	1377.36	3175.86	2862.70	313.16	3
18.77	4698.90	1437.51	3261.39	2946.52	314.87	3
18.77	4698.90	1437.51	3261.39	2946.52	314.87	2
16.85	4904.53	1520.27	3384.26	3066.06	318.20	2
14.95	5109.66	1604.60	3505.06	3185.09	319.98	2
13.05	5314.26	1689.86	3624.40	3303.59	320.81	2
11.16	5518.34	1775.43	3742.91	3421.57	321.34	2
9.27	5721.89	1861.41	3860.48	3539.03	321.46	2
7.40	5924.91	1947.51	3977.40	3655.94	321.46	2
5.53	6127.40	2047.51	4079.89	3772.34	307.55	2
3.68	6329.36	2192.51	4136.85	3888.20	248.65	2
1.83	6530.64	2377.43	4153.21	4003.38	149.83	2
.00	6731.08	2601.23	4129.85	4117.72	12.13	2

Time = 240. Degree of Consolidation = 14.%

Total Settlement = .389

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 240. = .389

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.33	2.27	.98	.91	.91	1
3.00	2.88	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.90	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material

5.79	.00	.00	.00	.00	.00	1
4.33	171.99	80.36	91.62	91.62	.00	1
2.88	342.57	155.88	186.69	181.84	4.85	1
1.44	512.85	196.46	316.39	271.76	44.63	1
.00	682.99	231.26	451.73	361.54	90.19	1

Time = 240. Degree of Consolidation = 98.%

Total Settlement = .206

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 240. = .206

Settlement caused by Secondary Compression at time 240. = .000

Surface Elevation = 4.00

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	60.07	21.42	6.50	5.78	5.53	6
60.02	59.56	21.35	6.49	5.84	5.52	6
59.45	59.04	21.27	6.47	5.89	5.50	6
58.89	58.51	21.20	6.46	5.95	5.49	6
58.33	57.99	21.12	6.44	6.00	5.47	6
57.76	57.46	21.05	6.43	6.05	5.46	6
57.20	56.92	20.97	6.42	6.09	5.45	6
56.64	56.39	20.90	6.40	6.13	5.43	6
56.08	55.84	20.82	6.39	6.17	5.42	6
56.08	55.84	20.82	4.51	4.33	3.71	5
54.82	54.61	20.59	4.44	4.29	3.65	5
53.56	53.39	20.36	4.38	4.25	3.58	5
52.32	52.18	20.12	4.32	4.20	3.52	5
51.10	50.98	19.89	4.25	4.15	3.46	5
49.88	49.79	19.66	4.19	4.09	3.39	5
48.69	48.62	19.43	4.13	4.03	3.35	5
48.69	48.62	19.43	1.93	1.92	1.88	4
46.69	46.63	18.75	1.92	1.91	1.86	4
44.70	44.64	18.06	1.91	1.90	1.83	4
42.72	42.67	17.38	1.89	1.89	1.81	4
40.75	40.70	16.70	1.88	1.87	1.79	4
38.79	38.75	16.01	1.86	1.85	1.77	4
36.85	36.80	15.33	1.84	1.84	1.75	4
34.91	34.87	14.65	1.82	1.82	1.73	4
33.00	32.96	13.97	1.80	1.80	1.71	4
31.09	31.05	13.28	1.78	1.78	1.68	4
31.09	31.05	13.28	1.47	1.47	1.42	3
29.70	29.66	12.72	1.46	1.46	1.41	3
28.32	28.28	12.16	1.45	1.45	1.40	3
26.94	26.90	11.59	1.44	1.44	1.39	3
25.57	25.53	11.03	1.43	1.43	1.38	3
24.21	24.17	10.47	1.42	1.42	1.37	3
22.84	22.81	9.90	1.41	1.41	1.36	3
21.49	21.45	9.34	1.40	1.40	1.35	3
20.14	20.11	8.78	1.39	1.39	1.34	3

18.80	18.76	8.21	1.38	1.38	1.33	3
18.80	18.76	8.21	1.34	1.34	1.30	2
16.88	16.85	7.39	1.33	1.33	1.29	2
14.97	14.94	6.57	1.32	1.32	1.28	2
13.07	13.04	5.75	1.31	1.31	1.27	2
11.18	11.15	4.93	1.30	1.30	1.26	2
9.30	9.27	4.11	1.29	1.29	1.26	2
7.43	7.40	3.29	1.28	1.28	1.25	2
5.56	5.53	2.46	1.27	1.26	1.24	2
3.70	3.68	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.07	682.96	238.53	444.43	361.51	82.92	6
59.56	719.68	219.66	500.03	393.61	106.42	6
59.04	756.67	201.23	555.44	425.97	129.47	6
58.51	793.91	183.42	610.49	458.59	151.89	6
57.99	831.40	166.42	664.98	491.47	173.52	6
57.46	869.13	150.37	718.76	524.57	194.19	6
56.92	907.07	135.41	771.67	557.90	213.77	6
56.39	945.23	121.66	823.57	591.43	232.14	6
55.84	983.56	109.22	874.35	625.15	249.20	6
55.84	983.56	109.22	874.35	625.15	249.20	5
54.61	1086.14	124.51	961.63	701.97	259.66	5
53.39	1188.13	141.78	1046.35	778.21	268.14	5
52.18	1289.47	161.00	1128.46	853.80	274.67	5
50.98	1390.08	182.15	1207.93	928.66	279.27	5
49.79	1489.90	205.18	1284.72	1002.73	281.99	5
48.62	1588.86	230.02	1358.84	1075.94	282.90	5
48.62	1588.86	230.02	1358.84	1075.94	282.90	4
46.63	1789.07	297.94	1491.13	1200.29	290.84	4
44.64	1988.79	374.18	1614.60	1324.15	290.45	4
42.67	2187.95	461.29	1726.66	1447.46	279.21	4
40.70	2386.48	534.45	1852.03	1570.13	281.90	4
38.75	2584.31	595.63	1988.68	1692.09	296.58	4
36.80	2781.38	659.93	2121.45	1813.31	308.14	4
34.87	2977.67	727.52	2250.15	1933.74	316.41	4
32.96	3173.13	798.74	2374.40	2053.34	321.05	4
31.05	3367.72	874.39	2493.33	2172.07	321.26	4
31.05	3367.72	874.39	2493.33	2172.07	321.26	3
29.66	3516.29	936.05	2580.24	2258.78	321.45	3
28.28	3664.47	997.91	2666.55	2345.10	321.46	3
26.90	3812.25	1066.08	2746.18	2431.03	315.15	3
25.53	3959.67	1132.13	2827.53	2516.58	310.95	3
24.17	4106.71	1196.22	2910.49	2601.77	308.72	3
22.81	4253.40	1258.81	2994.59	2686.60	307.99	3
21.45	4399.74	1320.24	3079.50	2771.08	308.42	3
20.11	4545.74	1380.80	3164.93	2855.22	309.72	3
18.76	4691.39	1440.54	3250.86	2939.02	311.84	3
18.76	4691.39	1440.54	3250.86	2939.02	311.84	2
16.85	4897.02	1522.46	3374.56	3058.54	316.02	2
14.94	5102.13	1606.00	3496.13	3177.56	318.57	2
13.04	5306.73	1690.55	3616.17	3296.06	320.12	2
11.15	5510.80	1775.80	3735.00	3414.03	320.97	2
9.27	5714.35	1861.77	3852.58	3531.48	321.10	2
7.40	5917.36	1949.64	3967.72	3648.40	319.32	2
5.53	6119.82	2064.19	4055.64	3764.76	290.88	2
3.68	6321.68	2221.51	4100.17	3880.52	219.65	2
1.83	6522.84	2403.38	4119.46	3995.58	123.88	2

.00	6723.21	2603.31	4119.90	4109.85	10.05	2

Time = 365. Degree of Consolidation = 19.%

Total Settlement = .515

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 365. = .515

Settlement caused by Secondary Compression at time 365. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.33	2.27	.98	.91	.91	1
3.00	2.88	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.90	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.33	171.99	80.36	91.62	91.62	.00	1
2.88	342.57	157.30	185.27	181.84	3.42	1
1.44	512.84	199.24	313.60	271.75	41.85	1
.00	682.96	238.53	444.43	361.51	82.92	1

Time = 365. Degree of Consolidation = 98.%

Total Settlement = .207

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 365. = .207

Settlement caused by Secondary Compression at time 365. = .000

Surface Elevation = 3.88

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.91	21.42	6.50	5.76	5.53	6
60.02	59.40	21.35	6.49	5.80	5.52	6
59.45	58.89	21.27	6.47	5.85	5.50	6

58.89	58.37	21.20	6.46	5.90	5.49	6
58.33	57.84	21.12	6.44	5.94	5.47	6
57.76	57.32	21.05	6.43	5.98	5.46	6
57.20	56.79	20.97	6.42	6.02	5.45	6
56.64	56.26	20.90	6.40	6.06	5.43	6
56.08	55.72	20.82	6.39	6.09	5.42	6
56.08	55.72	20.82	4.51	4.26	3.71	5
54.82	54.51	20.59	4.44	4.22	3.65	5
53.56	53.30	20.36	4.38	4.18	3.58	5
52.32	52.11	20.12	4.32	4.13	3.52	5
51.10	50.92	19.89	4.25	4.08	3.46	5
49.88	49.75	19.66	4.19	4.02	3.39	5
48.69	48.60	19.43	4.13	3.96	3.35	5
48.69	48.60	19.43	1.93	1.92	1.88	4
46.69	46.61	18.75	1.92	1.91	1.86	4
44.70	44.62	18.06	1.91	1.90	1.83	4
42.72	42.65	17.38	1.89	1.88	1.81	4
40.75	40.69	16.70	1.88	1.87	1.79	4
38.79	38.73	16.01	1.86	1.85	1.77	4
36.85	36.79	15.33	1.84	1.83	1.75	4
34.91	34.86	14.65	1.82	1.82	1.73	4
33.00	32.95	13.97	1.80	1.80	1.71	4
31.09	31.05	13.28	1.78	1.77	1.68	4
31.09	31.05	13.28	1.47	1.47	1.42	3
29.70	29.66	12.72	1.46	1.46	1.41	3
28.32	28.27	12.16	1.45	1.45	1.40	3
26.94	26.90	11.59	1.44	1.44	1.39	3
25.57	25.52	11.03	1.43	1.43	1.38	3
24.21	24.16	10.47	1.42	1.42	1.37	3
22.84	22.80	9.90	1.41	1.41	1.36	3
21.49	21.45	9.34	1.40	1.40	1.35	3
20.14	20.10	8.78	1.39	1.39	1.34	3
18.80	18.76	8.21	1.38	1.38	1.33	3
18.80	18.76	8.21	1.34	1.34	1.30	2
16.88	16.84	7.39	1.33	1.33	1.29	2
14.97	14.93	6.57	1.32	1.32	1.28	2
13.07	13.04	5.75	1.31	1.31	1.27	2
11.18	11.15	4.93	1.30	1.30	1.26	2
9.30	9.26	4.11	1.29	1.29	1.26	2
7.43	7.39	3.29	1.28	1.28	1.25	2
5.56	5.53	2.46	1.27	1.26	1.24	2
3.70	3.67	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.91	682.93	246.31	436.62	361.48	75.15	6
59.40	719.52	230.34	489.18	393.44	95.74	6
58.89	756.33	214.77	541.56	425.63	115.92	6
58.37	793.36	199.72	593.64	458.04	135.60	6
57.84	830.60	185.30	645.30	490.66	154.64	6
57.32	868.04	171.62	696.42	523.48	172.94	6
56.79	905.67	158.80	746.86	556.49	190.37	6
56.26	943.47	146.96	796.52	589.68	206.84	6
55.72	981.44	136.19	845.25	623.02	222.23	6
55.72	981.44	136.19	845.25	623.02	222.23	5
54.51	1083.03	152.34	930.69	698.86	231.83	5
53.30	1184.01	170.16	1013.85	774.09	239.76	5
52.11	1284.32	189.68	1094.65	848.66	245.99	5
50.92	1383.90	210.91	1173.00	922.49	250.51	5

49.75	1482.69	233.83	1248.86	995.53	253.33	5
48.60	1580.63	258.43	1322.20	1067.71	254.49	5
48.60	1580.63	258.43	1322.20	1067.71	254.49	4
46.61	1780.65	324.13	1456.52	1191.88	264.64	4
44.62	1980.20	398.20	1582.00	1315.57	266.44	4
42.65	2179.21	483.44	1695.77	1438.72	257.06	4
40.69	2377.60	545.59	1832.01	1561.24	270.77	4
38.73	2575.30	604.48	1970.82	1683.09	287.73	4
36.79	2772.29	666.58	2105.70	1804.21	301.49	4
34.86	2968.51	732.11	2236.40	1924.58	311.82	4
32.95	3163.93	801.54	2362.38	2044.14	318.25	4
31.05	3358.49	875.74	2482.75	2162.84	319.91	4
31.05	3358.49	875.74	2482.75	2162.84	319.91	3
29.66	3507.05	936.05	2571.00	2249.54	321.45	3
28.27	3655.23	997.91	2657.32	2335.86	321.45	3
26.90	3803.02	1067.33	2735.69	2421.79	313.90	3
25.52	3950.42	1134.49	2815.93	2507.33	308.60	3
24.16	4097.45	1199.43	2898.02	2592.50	305.52	3
22.80	4244.11	1262.57	2981.54	2677.31	304.23	3
21.45	4390.43	1324.27	3066.17	2761.77	304.39	3
20.10	4536.41	1384.74	3151.66	2845.89	305.78	3
18.76	4682.04	1444.13	3237.92	2929.67	308.25	3
18.76	4682.04	1444.13	3237.92	2929.67	308.25	2
16.84	4887.65	1525.33	3362.32	3049.17	313.15	2
14.93	5092.75	1608.09	3484.65	3168.17	316.48	2
13.04	5297.33	1692.14	3605.19	3286.66	318.53	2
11.15	5501.40	1777.44	3723.95	3404.63	319.33	2
9.26	5704.93	1864.99	3839.94	3522.06	317.88	2
7.39	5907.91	1957.21	3950.70	3638.95	311.76	2
5.53	6110.31	2085.19	4025.12	3755.24	269.88	2
3.67	6312.06	2247.86	4064.20	3870.90	193.30	2
1.83	6513.12	2423.11	4090.01	3985.86	104.15	2
.00	6713.45	2604.89	4108.56	4100.09	8.47	2

Time = 540. Degree of Consolidation = 25.%

Total Settlement = .671

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 540. = .671

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.88	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.90	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.99	80.36	91.62	91.62	.00	1
2.88	342.57	158.83	183.73	181.84	1.89	1
1.44	512.83	203.98	308.84	271.74	37.11	1
.00	682.93	246.30	436.63	361.48	75.15	1

Time = 540. Degree of Consolidation = 98.%

Total Settlement = .207

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 540. = .207

Settlement caused by Secondary Compression at time 540. = .000

Surface Elevation = 3.72

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.76	21.42	6.50	5.73	5.53	6
60.02	59.25	21.35	6.49	5.77	5.52	6
59.45	58.74	21.27	6.47	5.81	5.50	6
58.89	58.22	21.20	6.46	5.85	5.49	6
58.33	57.70	21.12	6.44	5.89	5.47	6
57.76	57.18	21.05	6.43	5.92	5.46	6
57.20	56.66	20.97	6.42	5.95	5.45	6
56.64	56.13	20.90	6.40	5.98	5.43	6
56.08	55.60	20.82	6.39	6.01	5.42	6
56.08	55.60	20.82	4.51	4.20	3.71	5
54.82	54.40	20.59	4.44	4.16	3.65	5
53.56	53.21	20.36	4.38	4.11	3.58	5
52.32	52.03	20.12	4.32	4.06	3.52	5
51.10	50.86	19.89	4.25	4.01	3.46	5
49.88	49.71	19.66	4.19	3.95	3.39	5
48.69	48.57	19.43	4.13	3.89	3.35	5
48.69	48.57	19.43	1.93	1.91	1.88	4
46.69	46.58	18.75	1.92	1.90	1.86	4
44.70	44.60	18.06	1.91	1.89	1.83	4
42.72	42.63	17.38	1.89	1.88	1.81	4
40.75	40.67	16.70	1.88	1.86	1.79	4
38.79	38.72	16.01	1.86	1.85	1.77	4
36.85	36.78	15.33	1.84	1.83	1.75	4
34.91	34.85	14.65	1.82	1.81	1.73	4
33.00	32.94	13.97	1.80	1.79	1.71	4
31.09	31.04	13.28	1.78	1.77	1.68	4
31.09	31.04	13.28	1.47	1.47	1.42	3
29.70	29.65	12.72	1.46	1.46	1.41	3
28.32	28.27	12.16	1.45	1.45	1.40	3
26.94	26.89	11.59	1.44	1.44	1.39	3
25.57	25.52	11.03	1.43	1.43	1.38	3
24.21	24.15	10.47	1.42	1.42	1.37	3
22.84	22.79	9.90	1.41	1.41	1.36	3
21.49	21.44	9.34	1.40	1.40	1.35	3

20.14	20.09	8.78	1.39	1.39	1.34	3
18.80	18.75	8.21	1.38	1.38	1.33	3
18.80	18.75	8.21	1.34	1.34	1.30	2
16.88	16.84	7.39	1.33	1.33	1.29	2
14.97	14.93	6.57	1.32	1.32	1.28	2
13.07	13.03	5.75	1.31	1.31	1.27	2
11.18	11.14	4.93	1.30	1.30	1.26	2
9.30	9.26	4.11	1.29	1.29	1.26	2
7.43	7.39	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.24	2
3.70	3.67	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.24	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.76	682.89	254.15	428.74	361.44	67.30	6
59.25	719.35	240.62	478.73	393.28	85.45	6
58.74	756.00	227.47	528.53	425.31	103.22	6
58.22	792.83	214.78	578.05	457.52	120.53	6
57.70	829.84	202.66	627.18	489.91	137.27	6
57.18	867.02	191.21	675.81	522.46	153.35	6
56.66	904.35	180.52	723.84	555.18	168.66	6
56.13	941.84	170.69	771.15	588.04	183.11	6
55.60	979.45	161.81	817.64	621.03	196.61	6
55.60	979.45	161.81	817.64	621.03	196.61	5
54.40	1080.10	178.99	901.11	695.93	205.17	5
53.21	1180.11	197.61	982.50	770.19	212.31	5
52.03	1279.43	217.68	1061.74	843.76	217.98	5
50.86	1378.00	239.23	1138.76	916.58	222.18	5
49.71	1475.77	262.26	1213.51	988.60	224.91	5
48.57	1572.69	286.73	1285.96	1059.77	226.19	5
48.57	1572.69	286.73	1285.96	1059.77	226.19	4
46.58	1772.52	351.29	1421.23	1183.74	237.48	4
44.60	1971.89	424.17	1547.72	1307.25	240.47	4
42.63	2170.72	504.61	1666.12	1430.23	235.89	4
40.67	2368.95	558.17	1810.78	1552.60	258.19	4
38.72	2566.52	614.82	1951.69	1674.31	277.39	4
36.78	2763.39	674.76	2088.63	1795.32	293.31	4
34.85	2959.53	738.21	2221.32	1915.60	305.72	4
32.94	3154.89	805.64	2349.24	2035.10	314.15	4
31.04	3349.41	878.00	2471.41	2153.76	317.65	4
31.04	3349.41	878.00	2471.41	2153.76	317.65	3
29.65	3497.97	936.61	2561.36	2240.46	320.90	3
28.27	3646.14	998.34	2647.80	2326.78	321.02	3
26.89	3793.92	1068.54	2725.38	2412.70	312.68	3
25.52	3941.32	1136.43	2804.88	2498.23	306.65	3
24.15	4088.33	1202.03	2886.31	2583.39	302.92	3
22.79	4234.98	1265.67	2969.31	2668.18	301.13	3
21.44	4381.28	1327.63	3053.65	2752.62	301.03	3
20.09	4527.24	1388.16	3139.08	2836.72	302.36	3
18.75	4672.86	1447.41	3225.45	2920.48	304.96	3
18.75	4672.86	1447.41	3225.45	2920.48	304.96	2
16.84	4878.44	1528.36	3350.08	3039.97	310.12	2
14.93	5083.52	1610.87	3472.65	3158.95	313.70	2
13.03	5288.09	1694.81	3593.28	3277.42	315.86	2
11.14	5492.14	1781.02	3711.12	3395.37	315.75	2
9.26	5695.64	1870.70	3824.94	3512.77	312.17	2
7.39	5898.58	1966.29	3932.29	3629.61	302.67	2
5.52	6100.91	2103.49	3997.42	3745.84	251.58	2
3.67	6302.59	2266.39	4036.20	3861.42	174.78	2

1.83	6503.58	2435.42	4068.17	3976.32	91.85	2
.00	6703.88	2605.88	4098.00	4090.52	7.48	2

Time = 730. Degree of Consolidation = 30.%

Total Settlement = .823

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 730. = .823

Settlement caused by Secondary Compression at time 730. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.88	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.90	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.99	80.36	91.62	91.62	.00	1
2.88	342.56	160.35	182.22	181.84	.38	1
1.44	512.81	209.38	303.43	271.72	31.71	1
.00	682.89	254.15	428.74	361.44	67.30	1

Time = 730. Degree of Consolidation = 98.%

Total Settlement = .208

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 730. = .208

Settlement caused by Secondary Compression at time 730. = .000

Surface Elevation = 3.57

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.51	21.42	6.50	5.70	5.53	6
60.02	59.01	21.35	6.49	5.73	5.52	6

59.45	58.50	21.27	6.47	5.75	5.50	6
58.89	57.98	21.20	6.46	5.78	5.49	6
58.33	57.47	21.12	6.44	5.81	5.47	6
57.76	56.96	21.05	6.43	5.83	5.46	6
57.20	56.44	20.97	6.42	5.85	5.45	6
56.64	55.92	20.90	6.40	5.87	5.43	6
56.08	55.40	20.82	6.39	5.89	5.42	6
56.08	55.40	20.82	4.51	4.10	3.71	5
54.82	54.22	20.59	4.44	4.05	3.65	5
53.56	53.06	20.36	4.38	4.00	3.58	5
52.32	51.90	20.12	4.32	3.95	3.52	5
51.10	50.76	19.89	4.25	3.89	3.46	5
49.88	49.64	19.66	4.19	3.84	3.39	5
48.69	48.52	19.43	4.13	3.78	3.35	5
48.69	48.52	19.43	1.93	1.91	1.88	4
46.69	46.54	18.75	1.92	1.90	1.86	4
44.70	44.57	18.06	1.91	1.88	1.83	4
42.72	42.60	17.38	1.89	1.87	1.81	4
40.75	40.64	16.70	1.88	1.86	1.79	4
38.79	38.70	16.01	1.86	1.84	1.77	4
36.85	36.76	15.33	1.84	1.83	1.75	4
34.91	34.84	14.65	1.82	1.81	1.73	4
33.00	32.92	13.97	1.80	1.79	1.71	4
31.09	31.02	13.28	1.78	1.77	1.68	4
31.09	31.02	13.28	1.47	1.47	1.42	3
29.70	29.63	12.72	1.46	1.46	1.41	3
28.32	28.25	12.16	1.45	1.45	1.40	3
26.94	26.88	11.59	1.44	1.44	1.39	3
25.57	25.51	11.03	1.43	1.43	1.38	3
24.21	24.14	10.47	1.42	1.42	1.37	3
22.84	22.78	9.90	1.41	1.41	1.36	3
21.49	21.43	9.34	1.40	1.40	1.35	3
20.14	20.08	8.78	1.39	1.39	1.34	3
18.80	18.74	8.21	1.38	1.38	1.33	3
18.80	18.74	8.21	1.34	1.34	1.30	2
16.88	16.83	7.39	1.33	1.33	1.29	2
14.97	14.92	6.57	1.32	1.32	1.28	2
13.07	13.02	5.75	1.31	1.31	1.27	2
11.18	11.13	4.93	1.30	1.30	1.26	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.24	2
3.70	3.67	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.51	682.85	265.72	417.13	361.40	55.74	6
59.01	719.12	256.12	462.99	393.04	69.95	6
58.50	755.52	246.84	508.68	424.82	83.86	6
57.98	792.05	237.94	554.11	456.73	97.38	6
57.47	828.70	229.50	599.20	488.77	110.43	6
56.96	865.47	221.61	643.86	520.91	122.94	6
56.44	902.35	214.35	688.00	553.17	134.83	6
55.92	939.32	207.79	731.54	585.53	146.01	6
55.40	976.39	202.00	774.39	617.97	156.42	6
55.40	976.39	202.00	774.39	617.97	156.42	5
54.22	1075.57	220.96	854.60	691.40	163.20	5
53.06	1174.04	241.00	933.04	764.13	168.92	5
51.90	1271.78	262.13	1009.65	836.12	173.53	5

50.76	1368.74	284.38	1084.36	907.33	177.03	5
49.64	1464.89	307.75	1157.14	977.72	179.42	5
48.52	1560.17	332.22	1227.96	1047.25	180.70	5
48.52	1560.17	332.22	1227.96	1047.25	180.70	4
46.54	1759.70	396.76	1362.94	1170.92	192.02	4
44.57	1958.76	469.71	1489.04	1294.12	194.92	4
42.60	2157.28	529.66	1627.62	1416.79	210.83	4
40.64	2355.23	580.46	1774.77	1538.87	235.90	4
38.70	2552.55	634.21	1918.34	1660.33	258.01	4
36.76	2749.21	691.17	2058.04	1781.14	276.90	4
34.84	2945.17	751.78	2193.38	1901.23	292.15	4
32.92	3140.38	816.73	2323.64	2020.59	303.06	4
31.02	3334.78	887.26	2447.52	2139.13	308.39	4
31.02	3334.78	887.26	2447.52	2139.13	308.39	3
29.63	3483.28	944.13	2539.15	2225.78	313.38	3
28.25	3631.42	1005.06	2626.36	2312.05	314.31	3
26.88	3779.16	1074.31	2704.85	2397.94	306.92	3
25.51	3926.52	1141.67	2784.86	2483.44	301.42	3
24.14	4073.51	1207.14	2866.37	2568.57	297.80	3
22.78	4220.13	1270.83	2949.30	2653.33	295.97	3
21.43	4366.40	1332.92	3033.49	2737.74	295.74	3
20.08	4512.33	1393.57	3118.76	2821.81	296.95	3
18.74	4657.92	1452.97	3204.95	2905.54	299.41	3
18.74	4657.92	1452.97	3204.95	2905.54	299.41	2
16.83	4863.46	1534.17	3329.29	3024.99	304.31	2
14.92	5068.51	1617.01	3451.50	3143.94	307.57	2
13.02	5273.04	1701.99	3571.05	3262.37	308.68	2
11.13	5477.03	1789.99	3687.05	3380.26	306.78	2
9.25	5680.48	1882.30	3798.17	3497.61	300.56	2
7.38	5883.33	1981.06	3902.27	3614.37	287.90	2
5.52	6085.56	2127.90	3957.67	3730.50	227.17	2
3.67	6287.15	2287.62	3999.52	3845.98	153.54	2
1.83	6488.07	2448.33	4039.74	3960.81	78.93	2
.00	6688.34	2606.89	4081.45	4074.98	6.47	2

Time = 1080. Degree of Consolidation = 39.%

Total Settlement = 1.072

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 1080. = 1.072

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.88	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.90	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.99	80.36	91.62	91.62	.00	1
2.88	342.56	160.73	181.84	181.84	.00	1
1.44	512.80	216.01	296.79	271.71	25.08	1
.00	682.85	265.72	417.13	361.40	55.74	1

Time = 1080. Degree of Consolidation = 99.%

Total Settlement = .208

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 1080. = .208

Settlement caused by Secondary Compression at time 1080. = .000

Surface Elevation = 3.32

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.29	21.42	6.50	5.67	5.53	6
60.02	58.79	21.35	6.49	5.69	5.52	6
59.45	58.28	21.27	6.47	5.70	5.50	6
58.89	57.77	21.20	6.46	5.72	5.49	6
58.33	57.27	21.12	6.44	5.74	5.47	6
57.76	56.76	21.05	6.43	5.75	5.46	6
57.20	56.25	20.97	6.42	5.77	5.45	6
56.64	55.73	20.90	6.40	5.78	5.43	6
56.08	55.22	20.82	6.39	5.79	5.42	6
56.08	55.22	20.82	4.51	4.01	3.71	5
54.82	54.06	20.59	4.44	3.96	3.65	5
53.56	52.92	20.36	4.38	3.91	3.58	5
52.32	51.79	20.12	4.32	3.86	3.52	5
51.10	50.67	19.89	4.25	3.80	3.46	5
49.88	49.56	19.66	4.19	3.74	3.39	5
48.69	48.47	19.43	4.13	3.68	3.35	5
48.69	48.47	19.43	1.93	1.90	1.88	4
46.69	46.49	18.75	1.92	1.89	1.86	4
44.70	44.52	18.06	1.91	1.88	1.83	4
42.72	42.56	17.38	1.89	1.87	1.81	4
40.75	40.61	16.70	1.88	1.85	1.79	4
38.79	38.67	16.01	1.86	1.84	1.77	4
36.85	36.74	15.33	1.84	1.82	1.75	4
34.91	34.81	14.65	1.82	1.81	1.73	4
33.00	32.90	13.97	1.80	1.79	1.71	4
31.09	31.01	13.28	1.78	1.77	1.68	4
31.09	31.01	13.28	1.47	1.47	1.42	3
29.70	29.62	12.72	1.46	1.46	1.41	3
28.32	28.24	12.16	1.45	1.45	1.40	3
26.94	26.86	11.59	1.44	1.44	1.39	3
25.57	25.49	11.03	1.43	1.43	1.38	3
24.21	24.13	10.47	1.42	1.42	1.37	3
22.84	22.77	9.90	1.41	1.41	1.36	3

21.49	21.42	9.34	1.40	1.40	1.35	3
20.14	20.07	8.78	1.39	1.39	1.34	3
18.80	18.73	8.21	1.38	1.38	1.33	3
18.80	18.73	8.21	1.34	1.33	1.30	2
16.88	16.82	7.39	1.33	1.33	1.29	2
14.97	14.91	6.57	1.32	1.32	1.28	2
13.07	13.02	5.75	1.31	1.30	1.27	2
11.18	11.13	4.93	1.30	1.29	1.26	2
9.30	9.25	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.24	2
3.70	3.67	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.29	682.82	275.79	407.03	361.37	45.67	6
58.79	718.92	269.40	449.51	392.84	56.67	6
58.28	755.11	263.30	491.81	424.41	67.39	6
57.77	791.38	257.54	533.84	456.06	77.78	6
57.27	827.73	252.17	575.56	487.80	87.76	6
56.76	864.16	247.28	616.88	519.60	97.28	6
56.25	900.65	242.90	657.74	551.47	106.27	6
55.73	937.20	239.12	698.08	583.40	114.68	6
55.22	973.80	235.97	737.83	615.38	122.45	6
55.22	973.80	235.97	737.83	615.38	122.45	5
54.06	1071.73	256.54	815.19	687.56	127.63	5
52.92	1168.90	277.89	891.02	758.99	132.03	5
51.79	1265.30	300.04	965.26	829.63	135.63	5
50.67	1360.89	323.02	1037.87	899.47	138.40	5
49.56	1455.63	346.82	1108.82	968.47	140.35	5
48.47	1549.51	371.43	1178.08	1036.60	141.49	5
48.47	1549.51	371.43	1178.08	1036.60	141.49	4
46.49	1748.77	437.31	1311.46	1159.99	151.46	4
44.52	1947.55	506.61	1440.94	1282.91	158.03	4
42.56	2145.79	553.18	1592.61	1405.30	187.31	4
40.61	2343.46	602.20	1741.26	1527.11	214.15	4
38.67	2540.53	654.03	1886.50	1648.32	238.18	4
36.74	2736.97	709.02	2027.95	1768.90	259.05	4
34.81	2932.73	767.76	2164.97	1888.80	276.17	4
32.90	3127.76	831.02	2296.73	2007.97	288.77	4
31.01	3322.00	900.22	2421.78	2126.35	295.43	4
31.01	3322.00	900.22	2421.78	2126.35	295.43	3
29.62	3470.42	955.82	2514.60	2212.92	301.69	3
28.24	3618.49	1016.59	2601.89	2299.12	302.77	3
26.86	3766.17	1084.01	2682.16	2384.95	297.22	3
25.49	3913.48	1150.04	2763.45	2470.40	293.05	3
24.13	4060.42	1214.59	2845.83	2555.48	290.35	3
22.77	4207.01	1277.72	2929.29	2640.21	289.08	3
21.42	4353.24	1339.57	3013.67	2724.58	289.09	3
20.07	4499.13	1400.19	3098.94	2808.61	290.33	3
18.73	4644.68	1459.71	3184.97	2892.30	292.66	3
18.73	4644.68	1459.71	3184.97	2892.30	292.66	2
16.82	4850.19	1541.20	3308.98	3011.71	297.27	2
14.91	5055.18	1624.59	3430.60	3130.61	299.98	2
13.02	5259.66	1710.57	3549.10	3248.99	300.11	2
11.13	5463.60	1799.88	3663.72	3366.83	296.89	2
9.25	5666.98	1893.58	3773.40	3484.11	289.29	2
7.38	5869.77	1993.28	3876.49	3600.80	275.69	2
5.52	6071.92	2145.49	3926.43	3716.86	209.58	2

3.67	6273.44	2301.47	3971.97	3832.28	139.70	2
1.83	6474.32	2456.05	4018.27	3947.06	71.21	2
.00	6674.57	2607.49	4067.08	4061.21	5.87	2

Time = 1440. Degree of Consolidation = 47.%

Total Settlement = 1.292

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 1440. = 1.292

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.88	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.98	80.36	91.62	91.62	.00	1
2.88	342.56	160.73	181.84	181.84	.00	1
1.44	512.79	221.41	291.38	271.70	19.68	1
.00	682.82	275.79	407.03	361.37	45.67	1

Time = 1440. Degree of Consolidation = 99.%

Total Settlement = .209

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 1440. = .209

Settlement caused by Secondary Compression at time 1440. = .000

Surface Elevation = 3.10

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.09	21.42	6.50	5.64	5.53	6

60.02	58.58	21.35	6.49	5.65	5.52	6
59.45	58.08	21.27	6.47	5.66	5.50	6
58.89	57.58	21.20	6.46	5.67	5.49	6
58.33	57.07	21.12	6.44	5.68	5.47	6
57.76	56.57	21.05	6.43	5.68	5.46	6
57.20	56.06	20.97	6.42	5.69	5.45	6
56.64	55.56	20.90	6.40	5.69	5.43	6
56.08	55.05	20.82	6.39	5.70	5.42	6
56.08	55.05	20.82	4.51	3.94	3.71	5
54.82	53.91	20.59	4.44	3.88	3.65	5
53.56	52.79	20.36	4.38	3.83	3.58	5
52.32	51.68	20.12	4.32	3.77	3.52	5
51.10	50.58	19.89	4.25	3.71	3.46	5
49.88	49.49	19.66	4.19	3.65	3.39	5
48.69	48.42	19.43	4.13	3.59	3.35	5
48.69	48.42	19.43	1.93	1.89	1.88	4
46.69	46.45	18.75	1.92	1.88	1.86	4
44.70	44.48	18.06	1.91	1.87	1.83	4
42.72	42.52	17.38	1.89	1.86	1.81	4
40.75	40.58	16.70	1.88	1.85	1.79	4
38.79	38.64	16.01	1.86	1.83	1.77	4
36.85	36.71	15.33	1.84	1.82	1.75	4
34.91	34.79	14.65	1.82	1.80	1.73	4
33.00	32.88	13.97	1.80	1.78	1.71	4
31.09	30.99	13.28	1.78	1.76	1.68	4
31.09	30.99	13.28	1.47	1.47	1.42	3
29.70	29.60	12.72	1.46	1.46	1.41	3
28.32	28.22	12.16	1.45	1.44	1.40	3
26.94	26.85	11.59	1.44	1.43	1.39	3
25.57	25.48	11.03	1.43	1.42	1.38	3
24.21	24.12	10.47	1.42	1.41	1.37	3
22.84	22.76	9.90	1.41	1.40	1.36	3
21.49	21.41	9.34	1.40	1.39	1.35	3
20.14	20.06	8.78	1.39	1.38	1.34	3
18.80	18.72	8.21	1.38	1.38	1.33	3
18.80	18.72	8.21	1.34	1.33	1.30	2
16.88	16.81	7.39	1.33	1.32	1.29	2
14.97	14.91	6.57	1.32	1.31	1.28	2
13.07	13.01	5.75	1.31	1.30	1.27	2
11.18	11.12	4.93	1.30	1.29	1.26	2
9.30	9.24	4.11	1.29	1.28	1.26	2
7.43	7.38	3.29	1.28	1.27	1.25	2
5.56	5.52	2.46	1.27	1.26	1.24	2
3.70	3.67	1.64	1.26	1.25	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.09	682.79	285.45	397.34	361.33	36.00	6
58.58	718.73	281.86	436.87	392.66	44.21	6
58.08	754.72	278.52	476.20	424.03	52.17	6
57.58	790.76	275.48	515.28	455.44	59.84	6
57.07	826.84	272.78	554.05	486.90	67.15	6
56.57	862.95	270.48	592.46	518.39	74.07	6
56.06	899.09	268.63	630.46	549.92	80.54	6
55.56	935.26	267.28	667.98	581.46	86.52	6
55.05	971.44	266.45	704.98	613.02	91.96	6
55.05	971.44	266.45	704.98	613.02	91.96	5
53.91	1068.25	288.49	779.76	684.08	95.68	5
52.79	1164.25	311.08	853.18	754.34	98.84	5

51.68	1259.44	334.24	925.20	823.77	101.43	5
50.58	1353.79	357.98	995.80	892.37	103.43	5
49.49	1447.27	382.31	1064.96	960.10	104.85	5
48.42	1539.87	407.22	1132.65	1026.95	105.70	5
48.42	1539.87	407.22	1132.65	1026.95	105.70	4
46.45	1738.87	475.75	1263.12	1150.10	113.02	4
44.48	1937.38	529.33	1408.06	1272.75	135.31	4
42.52	2135.36	575.23	1560.13	1394.86	165.27	4
40.58	2332.77	623.39	1709.39	1516.42	192.97	4
38.64	2529.60	674.14	1855.45	1637.38	218.07	4
36.71	2725.80	727.94	1997.85	1757.73	240.13	4
34.79	2921.34	785.45	2135.88	1877.41	258.48	4
32.88	3116.16	847.57	2268.59	1996.37	272.22	4
30.99	3310.21	915.87	2394.34	2114.56	279.78	4
30.99	3310.21	915.87	2394.34	2114.56	279.78	3
29.60	3458.54	970.58	2487.96	2201.03	286.93	3
28.22	3606.52	1031.73	2574.78	2287.15	287.63	3
26.85	3754.12	1097.17	2656.95	2372.90	284.05	3
25.48	3901.36	1161.59	2739.77	2458.28	281.49	3
24.12	4048.24	1224.93	2823.31	2543.30	280.01	3
22.76	4194.77	1287.17	2907.60	2627.97	279.63	3
21.41	4340.95	1348.42	2992.54	2712.29	280.24	3
20.06	4486.79	1408.75	3078.04	2796.27	281.77	3
18.72	4632.29	1468.27	3164.03	2879.92	284.11	3
18.72	4632.29	1468.27	3164.03	2879.92	284.11	2
16.81	4837.75	1549.74	3288.00	2999.27	288.73	2
14.91	5042.69	1633.44	3409.26	3118.12	291.14	2
13.01	5247.12	1719.77	3527.35	3236.45	290.90	2
11.12	5451.00	1809.74	3641.26	3354.23	287.03	2
9.24	5654.31	1904.20	3750.12	3471.45	278.67	2
7.38	5857.03	2006.02	3851.02	3588.07	262.95	2
5.52	6059.12	2159.84	3899.29	3704.06	195.23	2
3.67	6260.59	2312.02	3948.57	3819.43	129.14	2
1.83	6461.44	2461.84	3999.60	3934.18	65.42	2
.00	6661.67	2607.94	4053.73	4048.32	5.42	2

Time = 1825. Degree of Consolidation = 55.%

Total Settlement = 1.498

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 1825. = 1.498

Settlement caused by Secondary Compression at time 1825. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.88	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.89	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.98	80.36	91.62	91.62	.00	1
2.88	342.56	160.73	181.84	181.84	.00	1
1.44	512.79	226.45	286.33	271.69	14.64	1
.00	682.79	285.45	397.34	361.33	36.00	1

Time = 1825. Degree of Consolidation = 99.%

Total Settlement = .209

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 1825. = .209

Settlement caused by Secondary Compression at time 1825. = .000

Surface Elevation = 2.89

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.79	21.42	6.50	5.61	5.53	6
60.02	58.29	21.35	6.49	5.60	5.52	6
59.45	57.79	21.27	6.47	5.60	5.50	6
58.89	57.30	21.20	6.46	5.60	5.49	6
58.33	56.80	21.12	6.44	5.59	5.47	6
57.76	56.30	21.05	6.43	5.59	5.46	6
57.20	55.80	20.97	6.42	5.58	5.45	6
56.64	55.30	20.90	6.40	5.58	5.43	6
56.08	54.81	20.82	6.39	5.57	5.42	6
56.08	54.81	20.82	4.51	3.84	3.71	5
54.82	53.69	20.59	4.44	3.78	3.65	5
53.56	52.59	20.36	4.38	3.72	3.58	5
52.32	51.51	20.12	4.32	3.66	3.52	5
51.10	50.43	19.89	4.25	3.60	3.46	5
49.88	49.38	19.66	4.19	3.54	3.39	5
48.69	48.33	19.43	4.13	3.48	3.35	5
48.69	48.33	19.43	1.93	1.89	1.88	4
46.69	46.36	18.75	1.92	1.88	1.86	4
44.70	44.40	18.06	1.91	1.86	1.83	4
42.72	42.45	17.38	1.89	1.85	1.81	4
40.75	40.51	16.70	1.88	1.84	1.79	4
38.79	38.58	16.01	1.86	1.82	1.77	4
36.85	36.66	15.33	1.84	1.81	1.75	4
34.91	34.75	14.65	1.82	1.79	1.73	4
33.00	32.84	13.97	1.80	1.77	1.71	4
31.09	30.96	13.28	1.78	1.76	1.68	4
31.09	30.96	13.28	1.47	1.46	1.42	3
29.70	29.57	12.72	1.46	1.45	1.41	3
28.32	28.20	12.16	1.45	1.44	1.40	3
26.94	26.82	11.59	1.44	1.43	1.39	3
25.57	25.46	11.03	1.43	1.42	1.38	3
24.21	24.10	10.47	1.42	1.41	1.37	3

22.84	22.74	9.90	1.41	1.40	1.36	3
21.49	21.39	9.34	1.40	1.39	1.35	3
20.14	20.05	8.78	1.39	1.38	1.34	3
18.80	18.71	8.21	1.38	1.37	1.33	3
18.80	18.71	8.21	1.34	1.33	1.30	2
16.88	16.80	7.39	1.33	1.32	1.29	2
14.97	14.90	6.57	1.32	1.31	1.28	2
13.07	13.00	5.75	1.31	1.30	1.27	2
11.18	11.12	4.93	1.30	1.29	1.26	2
9.30	9.24	4.11	1.29	1.28	1.26	2
7.43	7.37	3.29	1.28	1.27	1.25	2
5.56	5.51	2.46	1.27	1.26	1.24	2
3.70	3.67	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.79	682.68	295.63	387.05	361.22	25.83	6
58.29	718.44	296.56	421.88	392.37	29.52	6
57.79	754.19	297.61	456.58	423.50	33.08	6
57.30	789.93	298.82	491.11	454.61	36.50	6
56.80	825.64	300.20	525.45	485.71	39.74	6
56.30	861.34	301.78	559.56	516.78	42.78	6
55.80	897.01	303.60	593.41	547.83	45.58	6
55.30	932.65	305.68	626.97	578.85	48.12	6
54.81	968.26	308.04	660.22	609.85	50.37	6
54.81	968.26	308.04	660.22	609.85	50.37	5
53.69	1063.54	332.21	731.33	679.37	51.96	5
52.59	1157.95	356.41	801.53	748.03	53.50	5
51.51	1251.49	380.65	870.83	815.82	55.01	5
50.43	1344.16	404.93	939.23	882.74	56.49	5
49.38	1435.96	429.22	1006.73	948.79	57.94	5
48.33	1526.88	453.51	1073.37	1013.96	59.41	5
48.33	1526.88	453.51	1073.37	1013.96	59.41	4
46.36	1725.54	516.48	1209.06	1136.77	72.29	4
44.40	1923.67	561.73	1361.94	1259.04	102.90	4
42.45	2121.26	608.21	1513.05	1380.76	132.29	4
40.51	2318.28	656.31	1661.97	1501.93	160.04	4
38.58	2514.71	706.57	1808.14	1622.50	185.64	4
36.66	2710.53	759.60	1950.93	1742.46	208.47	4
34.75	2905.70	816.19	2089.51	1861.77	227.74	4
32.84	3100.16	877.51	2222.65	1980.37	242.28	4
30.96	3293.86	945.33	2348.53	2098.21	250.32	4
30.96	3293.86	945.33	2348.53	2098.21	250.32	3
29.57	3442.00	999.48	2442.52	2184.50	258.02	3
28.20	3589.80	1062.48	2527.32	2270.43	256.89	3
26.82	3737.24	1124.98	2612.26	2356.01	256.25	3
25.46	3884.33	1186.85	2697.48	2441.25	256.23	3
24.10	4031.08	1248.03	2783.05	2526.13	256.92	3
22.74	4177.48	1308.52	2868.96	2610.68	258.28	3
21.39	4323.55	1368.48	2955.07	2694.89	260.18	3
20.05	4469.27	1427.90	3041.38	2778.76	262.62	3
18.71	4614.67	1486.85	3127.82	2862.29	265.53	3
18.71	4614.67	1486.85	3127.82	2862.29	265.53	2
16.80	4820.01	1567.12	3252.90	2981.54	271.36	2
14.90	5024.86	1650.13	3374.72	3100.28	274.44	2
13.00	5229.18	1736.39	3492.79	3218.51	274.28	2
11.12	5432.96	1826.38	3606.58	3336.19	270.39	2
9.24	5636.17	1920.57	3715.60	3453.30	262.29	2
7.37	5838.79	2028.58	3810.21	3569.82	240.38	2

5.51	6040.80	2178.44	3862.36	3685.73	176.62	2
3.67	6242.20	2325.83	3916.37	3801.03	115.34	2
1.83	6443.00	2469.40	3973.59	3915.74	57.86	2
.00	6643.22	2608.53	4034.69	4029.86	4.83	2

Time = 2520. Degree of Consolidation = 66.%

Total Settlement = 1.792

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 2520. = 1.792

Settlement caused by Secondary Compression at time 2520. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.87	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.98	80.36	91.61	91.61	.00	1
2.87	342.56	160.73	181.83	181.83	.00	1
1.44	512.76	241.09	271.67	271.66	.00	1
.00	682.68	321.45	361.22	361.22	.00	1

Time = 2520. Degree of Consolidation = 100.%

Total Settlement = .211

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 2520. = .211

Settlement caused by Secondary Compression at time 2520. = .000

Surface Elevation = 2.60

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material

60.58	58.68	21.42	6.50	5.57	5.53	6
60.02	58.18	21.35	6.49	5.57	5.52	6
59.45	57.68	21.27	6.47	5.56	5.50	6
58.89	57.19	21.20	6.46	5.56	5.49	6
58.33	56.69	21.12	6.44	5.55	5.47	6
57.76	56.20	21.05	6.43	5.55	5.46	6
57.20	55.70	20.97	6.42	5.54	5.45	6
56.64	55.21	20.90	6.40	5.53	5.43	6
56.08	54.72	20.82	6.39	5.53	5.42	6
56.08	54.72	20.82	4.51	3.80	3.71	5
54.82	53.61	20.59	4.44	3.74	3.65	5
53.56	52.52	20.36	4.38	3.68	3.58	5
52.32	51.44	20.12	4.32	3.62	3.52	5
51.10	50.38	19.89	4.25	3.56	3.46	5
49.88	49.33	19.66	4.19	3.50	3.39	5
48.69	48.29	19.43	4.13	3.44	3.35	5
48.69	48.29	19.43	1.93	1.89	1.88	4
46.69	46.32	18.75	1.92	1.87	1.86	4
44.70	44.37	18.06	1.91	1.86	1.83	4
42.72	42.42	17.38	1.89	1.85	1.81	4
40.75	40.48	16.70	1.88	1.83	1.79	4
38.79	38.55	16.01	1.86	1.82	1.77	4
36.85	36.63	15.33	1.84	1.80	1.75	4
34.91	34.72	14.65	1.82	1.79	1.73	4
33.00	32.82	13.97	1.80	1.77	1.71	4
31.09	30.94	13.28	1.78	1.75	1.68	4
31.09	30.94	13.28	1.47	1.46	1.42	3
29.70	29.56	12.72	1.46	1.45	1.41	3
28.32	28.18	12.16	1.45	1.44	1.40	3
26.94	26.81	11.59	1.44	1.43	1.39	3
25.57	25.45	11.03	1.43	1.42	1.38	3
24.21	24.09	10.47	1.42	1.41	1.37	3
22.84	22.73	9.90	1.41	1.40	1.36	3
21.49	21.38	9.34	1.40	1.39	1.35	3
20.14	20.04	8.78	1.39	1.38	1.34	3
18.80	18.70	8.21	1.38	1.37	1.33	3
18.80	18.70	8.21	1.34	1.33	1.30	2
16.88	16.79	7.39	1.33	1.32	1.29	2
14.97	14.89	6.57	1.32	1.31	1.28	2
13.07	13.00	5.75	1.31	1.30	1.27	2
11.18	11.11	4.93	1.30	1.29	1.26	2
9.30	9.24	4.11	1.29	1.28	1.26	2
7.43	7.37	3.29	1.28	1.27	1.25	2
5.56	5.51	2.46	1.27	1.26	1.24	2
3.70	3.67	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.68	682.67	307.12	375.56	361.22	14.34	6
58.18	718.27	308.45	409.82	392.19	17.62	6
57.68	753.85	309.92	443.92	423.15	20.77	6
57.19	789.40	311.56	477.85	454.09	23.76	6
56.69	824.93	313.37	511.57	485.00	26.57	6
56.20	860.44	315.38	545.06	515.88	29.18	6
55.70	895.91	317.61	578.30	546.74	31.57	6
55.21	931.35	320.08	611.28	577.56	33.72	6
54.72	966.76	322.79	643.97	608.34	35.63	6
54.72	966.76	322.79	643.97	608.34	35.63	5
53.61	1061.50	347.18	714.32	677.33	36.98	5

52.52	1155.37	371.49	783.88	745.45	38.43	5
51.44	1248.37	395.70	852.67	812.70	39.96	5
50.38	1340.50	419.81	920.69	879.08	41.61	5
49.33	1431.77	443.79	987.98	944.60	43.38	5
48.29	1522.18	467.61	1054.57	1009.27	45.31	5
48.29	1522.18	467.61	1054.57	1009.27	45.31	4
46.32	1720.73	526.51	1194.23	1131.96	62.27	4
44.37	1918.74	573.11	1345.62	1254.10	91.52	4
42.42	2116.18	620.68	1495.50	1375.69	119.81	4
40.48	2313.05	669.64	1643.40	1496.69	146.71	4
38.55	2509.32	720.56	1788.76	1617.11	171.66	4
36.63	2704.97	774.09	1930.88	1736.90	193.98	4
34.72	2899.96	831.14	2068.82	1856.03	212.79	4
32.82	3094.24	893.14	2201.10	1974.45	226.65	4
30.94	3287.74	962.26	2325.48	2092.09	233.39	4
30.94	3287.74	962.26	2325.48	2092.09	233.39	3
29.56	3435.78	1017.59	2418.19	2178.27	239.91	3
28.18	3583.48	1079.23	2504.25	2264.11	240.14	3
26.81	3730.83	1140.41	2590.42	2349.60	240.81	3
25.45	3877.84	1201.09	2676.74	2434.75	241.99	3
24.09	4024.51	1261.29	2763.22	2519.56	243.66	3
22.73	4170.84	1320.99	2849.85	2604.04	245.81	3
21.38	4316.83	1380.23	2936.61	2688.17	248.43	3
20.04	4462.50	1439.13	3023.37	2771.98	251.39	3
18.70	4607.83	1497.69	3110.14	2855.46	254.68	3
18.70	4607.83	1497.69	3110.14	2855.46	254.68	2
16.79	4813.11	1577.11	3236.01	2974.64	261.37	2
14.89	5017.89	1659.61	3358.29	3093.32	264.97	2
13.00	5222.16	1745.36	3476.80	3211.49	265.31	2
11.11	5425.88	1834.96	3590.92	3329.11	261.81	2
9.24	5629.05	1928.57	3700.48	3446.18	254.30	2
7.37	5831.62	2039.34	3792.28	3562.65	229.62	2
5.51	6033.59	2187.05	3846.54	3678.52	168.02	2
3.67	6234.96	2331.61	3903.35	3793.79	109.56	2
1.83	6435.74	2472.35	3963.39	3908.48	54.91	2
.00	6635.96	2608.76	4027.20	4022.60	4.60	2

Time = 2880. Degree of Consolidation = 70.%

Total Settlement = 1.908

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 2880. = 1.908

Settlement caused by Secondary Compression at time 2880. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.87	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.89	.89	1

XI	Total Stress	Effective Stress	Total Pore Pressure	Static Pore Pressure	Excess Pore Pressure	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.97	80.36	91.61	91.61	.00	1
2.87	342.56	160.73	181.83	181.83	.00	1
1.44	512.75	241.09	271.66	271.66	.00	1
.00	682.67	321.45	361.22	361.22	.00	1

Time = 2880. Degree of Consolidation = 100.%

Total Settlement = .211

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 2880. = .211

Settlement caused by Secondary Compression at time 2880. = .000

Surface Elevation = 2.48

**********Current Conditions in Compressible Foundation**********

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.58	21.42	6.50	5.56	5.53	6
60.02	58.09	21.35	6.49	5.55	5.52	6
59.45	57.59	21.27	6.47	5.54	5.50	6
58.89	57.10	21.20	6.46	5.54	5.49	6
58.33	56.61	21.12	6.44	5.53	5.47	6
57.76	56.11	21.05	6.43	5.52	5.46	6
57.20	55.62	20.97	6.42	5.51	5.45	6
56.64	55.13	20.90	6.40	5.50	5.43	6
56.08	54.64	20.82	6.39	5.49	5.42	6
56.08	54.64	20.82	4.51	3.77	3.71	5
54.82	53.54	20.59	4.44	3.71	3.65	5
53.56	52.45	20.36	4.38	3.65	3.58	5
52.32	51.38	20.12	4.32	3.59	3.52	5
51.10	50.33	19.89	4.25	3.53	3.46	5
49.88	49.28	19.66	4.19	3.47	3.39	5
48.69	48.25	19.43	4.13	3.41	3.35	5
48.69	48.25	19.43	1.93	1.88	1.88	4
46.69	46.29	18.75	1.92	1.87	1.86	4
44.70	44.33	18.06	1.91	1.86	1.83	4
42.72	42.38	17.38	1.89	1.84	1.81	4
40.75	40.45	16.70	1.88	1.83	1.79	4
38.79	38.52	16.01	1.86	1.81	1.77	4
36.85	36.60	15.33	1.84	1.80	1.75	4
34.91	34.70	14.65	1.82	1.78	1.73	4
33.00	32.80	13.97	1.80	1.77	1.71	4
31.09	30.92	13.28	1.78	1.75	1.68	4
31.09	30.92	13.28	1.47	1.45	1.42	3
29.70	29.54	12.72	1.46	1.44	1.41	3
28.32	28.17	12.16	1.45	1.43	1.40	3
26.94	26.80	11.59	1.44	1.42	1.39	3
25.57	25.43	11.03	1.43	1.42	1.38	3

24.21	24.08	10.47	1.42	1.41	1.37	3
22.84	22.72	9.90	1.41	1.40	1.36	3
21.49	21.38	9.34	1.40	1.39	1.35	3
20.14	20.03	8.78	1.39	1.38	1.34	3
18.80	18.70	8.21	1.38	1.37	1.33	3
18.80	18.70	8.21	1.34	1.33	1.30	2
16.88	16.79	7.39	1.33	1.32	1.29	2
14.97	14.89	6.57	1.32	1.31	1.28	2
13.07	13.00	5.75	1.31	1.30	1.27	2
11.18	11.11	4.93	1.30	1.29	1.26	2
9.30	9.24	4.11	1.29	1.28	1.26	2
7.43	7.37	3.29	1.28	1.27	1.25	2
5.56	5.51	2.46	1.27	1.25	1.24	2
3.70	3.67	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.58	682.67	311.47	371.21	361.22	9.99	6
58.09	718.20	313.80	404.40	392.12	12.27	6
57.59	753.69	316.23	437.46	423.00	14.46	6
57.10	789.15	318.77	470.38	453.84	16.54	6
56.61	824.58	321.43	503.15	484.64	18.51	6
56.11	859.96	324.22	535.74	515.40	20.33	6
55.62	895.30	327.17	568.13	546.13	22.00	6
55.13	930.60	330.28	600.32	576.81	23.52	6
54.64	965.86	333.56	632.30	607.44	24.86	6
54.64	965.86	333.56	632.30	607.44	24.86	5
53.54	1060.21	358.35	701.86	676.04	25.82	5
52.45	1153.67	382.90	770.77	743.75	27.02	5
51.38	1246.26	407.21	839.05	810.59	28.46	5
50.33	1337.98	431.26	906.72	876.56	30.15	5
49.28	1428.84	455.05	973.80	941.67	32.12	5
48.25	1518.85	478.54	1040.32	1005.94	34.38	5
48.25	1518.85	478.54	1040.32	1005.94	34.38	4
46.29	1717.32	534.55	1182.77	1128.54	54.23	4
44.33	1915.22	582.45	1332.77	1250.58	82.18	4
42.38	2112.54	631.18	1481.36	1372.05	109.32	4
40.45	2309.28	681.19	1628.09	1492.93	135.17	4
38.52	2505.41	733.02	1772.39	1613.19	159.19	4
36.60	2700.90	787.45	1913.46	1732.83	180.63	4
34.70	2895.73	845.50	2050.23	1851.80	198.43	4
32.80	3089.83	908.63	2181.20	1970.04	211.16	4
30.92	3283.14	979.43	2303.71	2087.49	216.22	4
30.92	3283.14	979.43	2303.71	2087.49	216.22	3
29.54	3431.07	1036.32	2394.75	2173.56	221.19	3
28.17	3578.67	1096.56	2482.11	2259.30	222.81	3
26.80	3725.92	1156.52	2569.41	2344.70	224.71	3
25.43	3872.84	1216.09	2656.76	2429.76	227.00	3
24.08	4019.43	1275.23	2744.20	2514.49	229.71	3
22.72	4165.69	1334.07	2831.62	2598.89	232.73	3
21.38	4311.61	1392.62	2918.99	2682.95	236.04	3
20.03	4457.21	1450.88	3006.33	2766.69	239.64	3
18.70	4602.48	1508.94	3093.54	2850.10	243.44	3
18.70	4602.48	1508.94	3093.54	2850.10	243.44	2
16.79	4807.69	1587.39	3220.30	2969.22	251.08	2
14.89	5012.41	1669.14	3343.27	3087.84	255.43	2
13.00	5216.62	1754.15	3462.47	3205.95	256.52	2
11.11	5420.29	1843.02	3577.28	3323.53	253.75	2
9.24	5623.41	1935.89	3687.52	3440.54	246.98	2

7.37	5825.94	2048.51	3777.43	3556.98	220.46	2
5.51	6027.88	2193.93	3833.95	3672.81	161.14	2
3.67	6229.22	2336.17	3893.05	3788.06	104.99	2
1.83	6429.99	2474.68	3955.31	3902.73	52.58	2
.00	6630.20	2608.94	4021.26	4016.84	4.42	2

Time = 3240. Degree of Consolidation = 73.%

Total Settlement = 2.001

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 3240. = 2.001

Settlement caused by Secondary Compression at time 3240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.87	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.97	80.36	91.61	91.61	.00	1
2.87	342.56	160.73	181.83	181.83	.00	1
1.44	512.75	241.09	271.66	271.66	.00	1
.00	682.67	321.45	361.22	361.22	.00	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .211

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 3240. = .211

Settlement caused by Secondary Compression at time 3240. = .000

Surface Elevation = 2.39

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.50	21.42	6.50	5.55	5.53	6
60.02	58.00	21.35	6.49	5.54	5.52	6
59.45	57.51	21.27	6.47	5.53	5.50	6
58.89	57.02	21.20	6.46	5.52	5.49	6
58.33	56.52	21.12	6.44	5.51	5.47	6
57.76	56.03	21.05	6.43	5.50	5.46	6
57.20	55.54	20.97	6.42	5.49	5.45	6
56.64	55.05	20.90	6.40	5.48	5.43	6
56.08	54.56	20.82	6.39	5.47	5.42	6
56.08	54.56	20.82	4.51	3.75	3.71	5
54.82	53.47	20.59	4.44	3.69	3.65	5
53.56	52.39	20.36	4.38	3.63	3.58	5
52.32	51.32	20.12	4.32	3.57	3.52	5
51.10	50.27	19.89	4.25	3.51	3.46	5
49.88	49.23	19.66	4.19	3.45	3.39	5
48.69	48.21	19.43	4.13	3.39	3.35	5
48.69	48.21	19.43	1.93	1.88	1.88	4
46.69	46.25	18.75	1.92	1.87	1.86	4
44.70	44.29	18.06	1.91	1.85	1.83	4
42.72	42.35	17.38	1.89	1.84	1.81	4
40.75	40.41	16.70	1.88	1.83	1.79	4
38.79	38.49	16.01	1.86	1.81	1.77	4
36.85	36.57	15.33	1.84	1.80	1.75	4
34.91	34.67	14.65	1.82	1.78	1.73	4
33.00	32.78	13.97	1.80	1.76	1.71	4
31.09	30.90	13.28	1.78	1.74	1.68	4
31.09	30.90	13.28	1.47	1.45	1.42	3
29.70	29.52	12.72	1.46	1.44	1.41	3
28.32	28.15	12.16	1.45	1.43	1.40	3
26.94	26.78	11.59	1.44	1.42	1.39	3
25.57	25.42	11.03	1.43	1.41	1.38	3
24.21	24.06	10.47	1.42	1.40	1.37	3
22.84	22.71	9.90	1.41	1.39	1.36	3
21.49	21.37	9.34	1.40	1.38	1.35	3
20.14	20.03	8.78	1.39	1.38	1.34	3
18.80	18.69	8.21	1.38	1.37	1.33	3
18.80	18.69	8.21	1.34	1.33	1.30	2
16.88	16.78	7.39	1.33	1.32	1.29	2
14.97	14.88	6.57	1.32	1.31	1.28	2
13.07	12.99	5.75	1.31	1.30	1.27	2
11.18	11.11	4.93	1.30	1.29	1.26	2
9.30	9.23	4.11	1.29	1.28	1.26	2
7.43	7.37	3.29	1.28	1.27	1.25	2
5.56	5.51	2.46	1.27	1.25	1.24	2
3.70	3.67	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.50	682.67	315.07	367.60	361.22	6.39	6
58.00	718.14	318.21	399.93	392.07	7.86	6
57.51	753.57	321.42	432.15	422.87	9.28	6
57.02	788.95	324.69	464.26	453.63	10.62	6
56.52	824.28	328.05	496.24	484.35	11.89	6
56.03	859.57	331.49	528.08	515.01	13.06	6
55.54	894.80	335.04	559.76	545.63	14.14	6
55.05	929.99	338.69	591.29	576.19	15.10	6
54.56	965.12	342.47	622.65	606.70	15.95	6
54.56	965.12	342.47	622.65	606.70	15.95	5

53.47	1059.14	367.60	691.54	674.97	16.57	5
52.39	1152.27	392.38	759.89	742.35	17.54	5
51.32	1244.51	416.80	827.71	808.85	18.87	5
50.27	1335.89	440.85	895.04	874.47	20.57	5
49.23	1426.41	464.51	961.90	939.24	22.66	5
48.21	1516.09	487.76	1028.32	1003.17	25.15	5
48.21	1516.09	487.76	1028.32	1003.17	25.15	4
46.25	1714.48	541.74	1172.74	1125.70	47.04	4
44.29	1912.28	591.18	1321.10	1247.65	73.45	4
42.35	2109.49	641.32	1468.17	1369.00	99.17	4
40.41	2306.10	692.64	1613.46	1489.75	123.72	4
38.49	2502.08	745.74	1756.35	1609.87	146.48	4
36.57	2697.42	801.42	1896.01	1729.35	166.66	4
34.67	2892.07	860.77	2031.30	1848.14	183.16	4
32.78	3085.98	925.46	2160.53	1966.19	194.33	4
30.90	3279.08	998.34	2280.74	2083.43	197.31	4
30.90	3279.08	998.34	2280.74	2083.43	197.31	3
29.52	3426.89	1057.25	2369.64	2169.39	200.25	3
28.15	3574.37	1116.20	2458.17	2255.01	203.17	3
26.78	3721.52	1174.90	2546.62	2340.30	206.33	3
25.42	3868.34	1233.30	2635.05	2425.26	209.79	3
24.06	4014.84	1291.49	2723.35	2509.90	213.45	3
22.71	4161.00	1349.46	2811.54	2594.20	217.34	3
21.37	4306.85	1407.21	2899.63	2678.19	221.45	3
20.03	4452.36	1464.81	2987.55	2761.84	225.71	3
18.69	4597.55	1522.31	3075.24	2845.18	230.06	3
18.69	4597.55	1522.31	3075.24	2845.18	230.06	2
16.78	4802.69	1599.72	3202.97	2964.21	238.76	2
14.88	5007.34	1680.43	3326.91	3082.76	244.15	2
12.99	5211.48	1764.41	3447.07	3200.81	246.27	2
11.11	5415.09	1852.24	3562.85	3318.32	244.53	2
9.23	5618.15	1944.06	3674.10	3435.29	238.81	2
7.37	5820.64	2058.49	3762.15	3551.67	210.47	2
5.51	6022.54	2201.30	3821.24	3667.48	153.76	2
3.67	6223.86	2341.07	3882.79	3782.70	100.09	2
1.83	6424.61	2477.18	3947.44	3897.35	50.08	2
.00	6624.82	2609.14	4015.68	4011.46	4.22	2

Time = 3650. Degree of Consolidation = 77.%

Total Settlement = 2.087

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 3650. = 2.087

Settlement caused by Secondary Compression at time 3650. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.87	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.89	.89	1

XI	Stresses ***** Total	Stresses ***** Effective	Pore Pressures ***** Total	Pore Pressures ***** Static	Pore Pressures ***** Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.97	80.36	91.61	91.61	.00	1
2.87	342.56	160.73	181.83	181.83	.00	1
1.44	512.75	241.09	271.66	271.66	.00	1
.00	682.67	321.45	361.22	361.22	.00	1

Time = 3650. Degree of Consolidation = 100.%

Total Settlement = .211

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 3650. = .211

Settlement caused by Secondary Compression at time 3650. = .000

Surface Elevation = 2.30

**********Current Conditions in Compressible Foundation**********

A	Coordinates ***** XI	Coordinates ***** Z	Void Ratios ***** Einitial	Void Ratios ***** E	Void Ratios ***** Eeop	Material
60.58	58.34	21.42	6.50	5.53	5.53	6
60.02	57.85	21.35	6.49	5.51	5.52	6
59.45	57.36	21.27	6.47	5.50	5.50	6
58.89	56.87	21.20	6.46	5.49	5.49	6
58.33	56.38	21.12	6.44	5.47	5.47	6
57.76	55.89	21.05	6.43	5.46	5.46	6
57.20	55.40	20.97	6.42	5.44	5.45	6
56.64	54.92	20.90	6.40	5.43	5.43	6
56.08	54.43	20.82	6.39	5.42	5.42	6
56.08	54.43	20.82	4.51	3.71	3.71	5
54.82	53.35	20.59	4.44	3.65	3.65	5
53.56	52.28	20.36	4.38	3.58	3.58	5
52.32	51.22	20.12	4.32	3.52	3.52	5
51.10	50.18	19.89	4.25	3.46	3.46	5
49.88	49.15	19.66	4.19	3.39	3.39	5
48.69	48.14	19.43	4.13	3.35	3.35	5
48.69	48.14	19.43	1.93	1.88	1.88	4
46.69	46.18	18.75	1.92	1.86	1.86	4
44.70	44.23	18.06	1.91	1.85	1.83	4
42.72	42.29	17.38	1.89	1.84	1.81	4
40.75	40.36	16.70	1.88	1.82	1.79	4
38.79	38.44	16.01	1.86	1.81	1.77	4
36.85	36.53	15.33	1.84	1.79	1.75	4
34.91	34.63	14.65	1.82	1.77	1.73	4
33.00	32.74	13.97	1.80	1.75	1.71	4
31.09	30.87	13.28	1.78	1.73	1.68	4
31.09	30.87	13.28	1.47	1.45	1.42	3
29.70	29.49	12.72	1.46	1.44	1.41	3
28.32	28.12	12.16	1.45	1.43	1.40	3
26.94	26.76	11.59	1.44	1.42	1.39	3

25.57	25.40	11.03	1.43	1.41	1.38	3
24.21	24.04	10.47	1.42	1.40	1.37	3
22.84	22.69	9.90	1.41	1.39	1.36	3
21.49	21.35	9.34	1.40	1.38	1.35	3
20.14	20.01	8.78	1.39	1.37	1.34	3
18.80	18.68	8.21	1.38	1.36	1.33	3
18.80	18.68	8.21	1.34	1.32	1.30	2
16.88	16.77	7.39	1.33	1.32	1.29	2
14.97	14.87	6.57	1.32	1.31	1.28	2
13.07	12.98	5.75	1.31	1.30	1.27	2
11.18	11.10	4.93	1.30	1.29	1.26	2
9.30	9.23	4.11	1.29	1.28	1.26	2
7.43	7.37	3.29	1.28	1.26	1.25	2
5.56	5.51	2.46	1.27	1.25	1.24	2
3.70	3.67	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.34	682.67	321.45	361.22	361.22	.00	6
57.85	718.04	326.07	391.96	391.96	.00	6
57.36	753.34	330.70	422.64	422.64	.00	6
56.87	788.57	335.32	453.25	453.25	.00	6
56.38	823.74	339.94	483.80	483.80	.00	6
55.89	858.84	344.56	514.28	514.28	.00	6
55.40	893.87	349.18	544.70	544.70	.00	6
54.92	928.84	353.80	575.04	575.04	.00	6
54.43	963.75	358.42	605.33	605.33	.00	6
54.43	963.75	358.42	605.33	605.33	.00	5
53.35	1057.18	384.17	673.02	673.02	.00	5
52.28	1149.70	409.92	739.78	739.78	.00	5
51.22	1241.28	435.67	805.61	805.61	.00	5
50.18	1331.96	461.42	870.54	870.54	.00	5
49.15	1421.69	487.17	934.52	934.52	.00	5
48.14	1510.60	512.92	997.69	997.69	.00	5
48.14	1510.60	512.92	997.69	997.69	.00	4
46.18	1708.76	560.69	1148.08	1119.98	28.09	4
44.23	1906.35	608.90	1297.45	1241.71	55.73	4
42.29	2103.35	658.51	1444.85	1362.86	81.99	4
40.36	2299.75	710.17	1589.58	1483.40	106.18	4
38.44	2495.52	764.44	1731.08	1603.31	127.78	4
36.53	2690.62	821.84	1868.78	1722.55	146.23	4
34.63	2885.02	883.37	2001.65	1841.09	160.56	4
32.74	3078.65	950.75	2127.90	1958.85	169.04	4
30.87	3271.43	1024.70	2246.73	2075.78	170.95	4
30.87	3271.43	1024.70	2246.73	2075.78	170.95	3
29.49	3419.09	1084.67	2334.41	2161.58	172.83	3
28.12	3566.41	1143.76	2422.65	2247.05	175.61	3
26.76	3713.41	1202.12	2511.28	2332.18	179.10	3
25.40	3860.08	1259.91	2600.17	2416.99	183.17	3
24.04	4006.42	1317.26	2689.16	2501.48	187.68	3
22.69	4152.45	1374.33	2778.12	2585.65	192.47	3
21.35	4298.15	1431.13	2867.03	2669.49	197.53	3
20.01	4443.54	1487.76	2955.78	2753.02	202.76	3
18.68	4588.60	1544.37	3044.23	2836.22	208.01	3
18.68	4588.60	1544.37	3044.23	2836.22	208.01	2
16.77	4793.61	1619.98	3173.62	2955.13	218.49	2
14.87	4998.14	1698.93	3299.21	3073.56	225.64	2
12.98	5202.17	1781.15	3421.02	3191.50	229.53	2
11.10	5405.69	1867.21	3538.47	3308.92	229.56	2

9.23	5608.66	1957.23	3651.43	3425.79	225.64	2
7.37	5811.07	2074.68	3736.39	3542.11	194.28	2
5.51	6012.91	2213.34	3799.58	3657.85	141.73	2
3.67	6214.19	2349.08	3865.11	3773.03	92.08	2
1.83	6414.92	2481.26	3933.67	3887.66	46.00	2
.00	6615.12	2609.45	4005.66	4001.76	3.91	2

Time = 4320. Degree of Consolidation = 82.%

Total Settlement = 2.242

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 4320. = 2.241

Settlement caused by Secondary Compression at time 4320. = .001

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.87	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.89	.89	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.97	80.36	91.61	91.61	.00	1
2.87	342.56	160.73	181.83	181.83	.00	1
1.44	512.75	241.09	271.66	271.66	.00	1
.00	682.67	321.45	361.22	361.22	.00	1

Time = 4320. Degree of Consolidation = 100.%

Total Settlement = .211

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 4320. = .211

Settlement caused by Secondary Compression at time 4320. = .000

Surface Elevation = 2.15

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.28	21.42	6.50	5.53	5.53	6
60.02	57.79	21.35	6.49	5.51	5.52	6
59.45	57.29	21.27	6.47	5.50	5.50	6
58.89	56.80	21.20	6.46	5.48	5.49	6
58.33	56.32	21.12	6.44	5.47	5.47	6
57.76	55.83	21.05	6.43	5.46	5.46	6
57.20	55.34	20.97	6.42	5.44	5.45	6
56.64	54.85	20.90	6.40	5.43	5.43	6
56.08	54.37	20.82	6.39	5.41	5.42	6
56.08	54.37	20.82	4.51	3.71	3.71	5
54.82	53.28	20.59	4.44	3.65	3.65	5
53.56	52.21	20.36	4.38	3.58	3.58	5
52.32	51.16	20.12	4.32	3.52	3.52	5
51.10	50.12	19.89	4.25	3.45	3.46	5
49.88	49.09	19.66	4.19	3.39	3.39	5
48.69	48.08	19.43	4.13	3.34	3.35	5
48.69	48.08	19.43	1.93	1.88	1.88	4
46.69	46.12	18.75	1.92	1.86	1.86	4
44.70	44.17	18.06	1.91	1.85	1.83	4
42.72	42.23	17.38	1.89	1.83	1.81	4
40.75	40.31	16.70	1.88	1.82	1.79	4
38.79	38.39	16.01	1.86	1.80	1.77	4
36.85	36.48	15.33	1.84	1.78	1.75	4
34.91	34.58	14.65	1.82	1.77	1.73	4
33.00	32.70	13.97	1.80	1.75	1.71	4
31.09	30.83	13.28	1.78	1.73	1.68	4
31.09	30.83	13.28	1.47	1.44	1.42	3
29.70	29.46	12.72	1.46	1.43	1.41	3
28.32	28.09	12.16	1.45	1.42	1.40	3
26.94	26.73	11.59	1.44	1.41	1.39	3
25.57	25.37	11.03	1.43	1.40	1.38	3
24.21	24.02	10.47	1.42	1.40	1.37	3
22.84	22.68	9.90	1.41	1.39	1.36	3
21.49	21.33	9.34	1.40	1.38	1.35	3
20.14	20.00	8.78	1.39	1.37	1.34	3
18.80	18.67	8.21	1.38	1.36	1.33	3
18.80	18.67	8.21	1.34	1.32	1.30	2
16.88	16.76	7.39	1.33	1.31	1.29	2
14.97	14.87	6.57	1.32	1.30	1.28	2
13.07	12.98	5.75	1.31	1.29	1.27	2
11.18	11.10	4.93	1.30	1.28	1.26	2
9.30	9.23	4.11	1.29	1.27	1.26	2
7.43	7.36	3.29	1.28	1.26	1.25	2
5.56	5.51	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.28	682.67	321.45	361.22	361.22	.00	6
57.79	718.03	326.07	391.95	391.95	.00	6
57.29	753.31	330.70	422.62	422.62	.00	6
56.80	788.53	335.32	453.22	453.22	.00	6
56.32	823.69	339.94	483.75	483.75	.00	6
55.83	858.78	344.56	514.22	514.22	.00	6
55.34	893.80	349.18	544.62	544.62	.00	6
54.85	928.76	353.80	574.96	574.96	.00	6
54.37	963.65	358.42	605.23	605.23	.00	6

54.37	963.65	358.42	605.23	605.23	.00	5
53.28	1057.07	384.17	672.91	672.91	.00	5
52.21	1149.58	409.92	739.66	739.66	.00	5
51.16	1241.15	435.67	805.48	805.48	.00	5
50.12	1331.82	461.42	870.40	870.40	.00	5
49.09	1421.54	487.17	934.37	934.37	.00	5
48.08	1510.44	512.92	997.53	997.53	.00	5
48.08	1510.44	512.92	997.53	997.53	.00	4
46.12	1708.57	566.03	1142.54	1119.79	22.75	4
44.17	1906.06	619.15	1286.91	1241.43	45.48	4
42.23	2102.92	672.76	1430.16	1362.42	67.74	4
40.31	2299.13	727.40	1571.73	1482.78	88.95	4
38.39	2494.68	783.78	1710.90	1602.47	108.43	4
36.48	2689.54	842.89	1846.65	1721.47	125.18	4
34.58	2883.68	906.06	1977.61	1839.74	137.87	4
32.70	3077.02	975.45	2101.57	1957.23	144.34	4
30.83	3269.50	1049.57	2219.93	2073.85	146.08	4
30.83	3269.50	1049.57	2219.93	2073.85	146.08	3
29.46	3417.02	1109.75	2307.27	2159.51	147.76	3
28.09	3564.20	1168.88	2395.32	2244.84	150.49	3
26.73	3711.06	1227.19	2483.87	2329.83	154.04	3
25.37	3857.59	1284.82	2572.77	2414.50	158.27	3
24.02	4003.79	1341.92	2661.88	2498.85	163.03	3
22.68	4149.68	1398.57	2751.11	2582.88	168.23	3
21.33	4295.25	1454.83	2840.42	2666.59	173.83	3
20.00	4440.50	1510.84	2929.66	2749.98	179.68	3
18.67	4585.44	1566.74	3018.70	2833.06	185.64	3
18.67	4585.44	1566.74	3018.70	2833.06	185.64	2
16.76	4790.31	1640.66	3149.65	2951.84	197.82	2
14.87	4994.72	1717.92	3276.80	3070.15	206.65	2
12.98	5198.64	1798.47	3400.17	3187.97	212.20	2
11.10	5402.06	1882.73	3519.32	3305.29	214.03	2
9.23	5604.94	1970.93	3634.01	3422.07	211.94	2
7.36	5807.27	2091.89	3715.39	3538.31	177.08	2
5.51	6009.05	2226.24	3782.82	3653.99	128.83	2
3.66	6210.29	2357.68	3852.61	3769.13	83.48	2
1.83	6410.99	2485.64	3925.35	3883.73	41.62	2
.00	6611.18	2609.79	4001.39	3997.82	3.57	2

Time = 5040. Degree of Consolidation = 85.%

Total Settlement = 2.305

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 5040. = 2.302

Settlement caused by Secondary Compression at time 5040. = .004

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.87	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1

.00	.00	.00	.98	.89	.89	1

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.97	80.36	91.61	91.61	.00	1
2.87	342.56	160.73	181.83	181.83	.00	1
1.44	512.75	241.09	271.66	271.66	.00	1
.00	682.67	321.45	361.22	361.22	.00	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .211

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 5040. = .211

Settlement caused by Secondary Compression at time 5040. = .000

Surface Elevation = 2.08

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.25	21.42	6.50	5.53	5.53	6
60.02	57.75	21.35	6.49	5.51	5.52	6
59.45	57.26	21.27	6.47	5.50	5.50	6
58.89	56.77	21.20	6.46	5.48	5.49	6
58.33	56.28	21.12	6.44	5.47	5.47	6
57.76	55.80	21.05	6.43	5.45	5.46	6
57.20	55.31	20.97	6.42	5.44	5.45	6
56.64	54.82	20.90	6.40	5.43	5.43	6
56.08	54.34	20.82	6.39	5.41	5.42	6
56.08	54.34	20.82	4.51	3.71	3.71	5
54.82	53.25	20.59	4.44	3.65	3.65	5
53.56	52.18	20.36	4.38	3.58	3.58	5
52.32	51.13	20.12	4.32	3.52	3.52	5
51.10	50.09	19.89	4.25	3.45	3.46	5
49.88	49.06	19.66	4.19	3.39	3.39	5
48.69	48.05	19.43	4.13	3.34	3.35	5
48.69	48.05	19.43	1.93	1.88	1.88	4
46.69	46.09	18.75	1.92	1.86	1.86	4
44.70	44.14	18.06	1.91	1.85	1.83	4
42.72	42.20	17.38	1.89	1.83	1.81	4
40.75	40.28	16.70	1.88	1.81	1.79	4
38.79	38.36	16.01	1.86	1.80	1.77	4
36.85	36.46	15.33	1.84	1.78	1.75	4
34.91	34.56	14.65	1.82	1.76	1.73	4
33.00	32.68	13.97	1.80	1.74	1.71	4
31.09	30.81	13.28	1.78	1.72	1.68	4
31.09	30.81	13.28	1.47	1.44	1.42	3
29.70	29.44	12.72	1.46	1.43	1.41	3
28.32	28.08	12.16	1.45	1.42	1.40	3

26.94	26.72	11.59	1.44	1.41	1.39	3
25.57	25.36	11.03	1.43	1.40	1.38	3
24.21	24.01	10.47	1.42	1.39	1.37	3
22.84	22.66	9.90	1.41	1.38	1.36	3
21.49	21.32	9.34	1.40	1.38	1.35	3
20.14	19.99	8.78	1.39	1.37	1.34	3
18.80	18.66	8.21	1.38	1.36	1.33	3
18.80	18.66	8.21	1.34	1.32	1.30	2
16.88	16.76	7.39	1.33	1.31	1.29	2
14.97	14.86	6.57	1.32	1.30	1.28	2
13.07	12.97	5.75	1.31	1.29	1.27	2
11.18	11.10	4.93	1.30	1.28	1.26	2
9.30	9.22	4.11	1.29	1.27	1.26	2
7.43	7.36	3.29	1.28	1.26	1.25	2
5.56	5.51	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.25	682.67	321.45	361.22	361.22	.00	6
57.75	718.02	326.07	391.95	391.95	.00	6
57.26	753.30	330.70	422.61	422.61	.00	6
56.77	788.51	335.32	453.20	453.20	.00	6
56.28	823.66	339.94	483.72	483.72	.00	6
55.80	858.74	344.56	514.18	514.18	.00	6
55.31	893.75	349.18	544.58	544.58	.00	6
54.82	928.70	353.80	574.91	574.91	.00	6
54.34	963.59	358.42	605.17	605.17	.00	6
54.34	963.59	358.42	605.17	605.17	.00	5
53.25	1057.01	384.17	672.84	672.84	.00	5
52.18	1149.51	409.92	739.59	739.59	.00	5
51.13	1241.07	435.67	805.40	805.40	.00	5
50.09	1331.73	461.42	870.32	870.32	.00	5
49.06	1421.45	487.17	934.28	934.28	.00	5
48.05	1510.35	512.92	997.43	997.43	.00	5
48.05	1510.35	512.92	997.43	997.43	.00	4
46.09	1708.46	567.58	1140.89	1119.69	21.20	4
44.14	1905.93	622.30	1283.63	1241.29	42.34	4
42.20	2102.74	677.51	1425.23	1362.24	62.98	4
40.28	2298.88	733.74	1565.14	1482.53	82.61	4
38.36	2494.35	791.68	1702.67	1602.14	100.53	4
36.46	2689.11	852.28	1836.83	1721.03	115.79	4
34.56	2883.12	916.96	1966.16	1839.19	126.97	4
32.68	3076.32	988.01	2088.32	1956.53	131.79	4
30.81	3268.65	1062.56	2206.08	2073.00	133.08	4
30.81	3268.65	1062.56	2206.08	2073.00	133.08	3
29.44	3416.09	1123.19	2292.90	2158.58	134.31	3
28.08	3563.20	1182.58	2380.62	2243.83	136.79	3
26.72	3709.98	1240.96	2469.02	2328.75	140.27	3
25.36	3856.43	1298.55	2557.88	2413.34	144.54	3
24.01	4002.56	1355.49	2647.07	2497.61	149.45	3
22.66	4148.37	1411.92	2736.45	2581.57	154.88	3
21.32	4293.86	1467.99	2825.87	2665.20	160.67	3
19.99	4439.04	1523.83	2915.21	2748.52	166.69	3
18.66	4583.91	1579.46	3004.44	2831.53	172.91	3
18.66	4583.91	1579.46	3004.44	2831.53	172.91	2
16.76	4788.70	1652.78	3135.93	2950.23	185.70	2
14.86	4993.04	1729.17	3263.87	3068.47	195.41	2
12.97	5196.89	1808.86	3388.04	3186.22	201.81	2

11.10	5400.25	1892.06	3508.19	3303.48	204.71	2
9.22	5603.08	1979.17	3623.91	3420.21	203.70	2
7.36	5805.37	2102.27	3703.09	3536.40	166.69	2
5.51	6007.11	2234.03	3773.08	3652.05	121.04	2
3.66	6208.32	2362.88	3845.44	3767.16	78.29	2
1.83	6409.00	2488.29	3920.72	3881.74	38.97	2
.00	6609.18	2610.00	3999.18	3995.83	3.36	2

Time = 5475. Degree of Consolidation = 86.%

Total Settlement = 2.337

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 5475. = 2.332

Settlement caused by Secondary Compression at time 5475. = .005

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
6.00	5.79	3.03
4.50	4.32	2.27
3.00	2.87	1.52
1.50	1.44	.76
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
5.79	.00	.00
4.32	171.97	80.36
2.87	342.56	160.73
1.44	512.75	241.09
.00	682.67	321.45

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
91.61	91.61	.00	1
181.83	181.83	.00	1
271.66	271.66	.00	1
361.22	361.22	.00	1

Time = 5475. Degree of Consolidation = 100.%

Total Settlement = .211

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 5475. = .211

Settlement caused by Secondary Compression at time 5475. = .000

Surface Elevation = 2.05

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****

A	XI	Z
60.58	58.19	21.42
60.02	57.69	21.35
59.45	57.20	21.27
58.89	56.71	21.20
58.33	56.22	21.12
57.76	55.73	21.05
57.20	55.25	20.97
56.64	54.76	20.90
56.08	54.28	20.82
56.08	54.28	20.82
54.82	53.19	20.59
53.56	52.12	20.36
52.32	51.07	20.12
51.10	50.03	19.89
49.88	49.00	19.66
48.69	47.99	19.43
48.69	47.99	19.43
46.69	46.03	18.75
44.70	44.08	18.06
42.72	42.15	17.38
40.75	40.22	16.70
38.79	38.31	16.01
36.85	36.40	15.33
34.91	34.51	14.65
33.00	32.64	13.97
31.09	30.78	13.28
31.09	30.78	13.28
29.70	29.41	12.72
28.32	28.04	12.16
26.94	26.68	11.59
25.57	25.33	11.03
24.21	23.98	10.47
22.84	22.64	9.90
21.49	21.30	9.34
20.14	19.97	8.78
18.80	18.64	8.21
18.80	18.64	8.21
16.88	16.74	7.39
14.97	14.85	6.57
13.07	12.97	5.75
11.18	11.09	4.93
9.30	9.22	4.11
7.43	7.36	3.29
5.56	5.51	2.46
3.70	3.66	1.64
1.85	1.83	.82
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
6.50	5.53	5.53	6
6.49	5.51	5.52	6
6.47	5.49	5.50	6
6.46	5.48	5.49	6
6.44	5.47	5.47	6
6.43	5.45	5.46	6
6.42	5.44	5.45	6
6.40	5.42	5.43	6
6.39	5.41	5.42	6
4.51	3.71	3.71	5
4.44	3.65	3.65	5
4.38	3.58	3.58	5
4.32	3.52	3.52	5
4.25	3.45	3.46	5
4.19	3.39	3.39	5
4.13	3.34	3.35	5
1.93	1.88	1.88	4
1.92	1.86	1.86	4
1.91	1.84	1.83	4
1.89	1.83	1.81	4
1.88	1.81	1.79	4
1.86	1.79	1.77	4
1.84	1.78	1.75	4
1.82	1.76	1.73	4
1.80	1.74	1.71	4
1.78	1.71	1.68	4
1.47	1.44	1.42	3
1.46	1.43	1.41	3
1.45	1.42	1.40	3
1.44	1.41	1.39	3
1.43	1.40	1.38	3
1.42	1.39	1.37	3
1.41	1.38	1.36	3
1.40	1.37	1.35	3
1.39	1.36	1.34	3
1.38	1.35	1.33	3
1.34	1.32	1.30	2
1.33	1.31	1.29	2
1.32	1.30	1.28	2
1.31	1.29	1.27	2
1.30	1.28	1.26	2
1.29	1.27	1.26	2
1.28	1.26	1.25	2
1.27	1.25	1.24	2
1.26	1.24	1.23	2
1.25	1.23	1.23	2
1.25	1.22	1.22	2

***** Stresses *****

XI	Total	Effective
58.19	682.67	321.45
57.69	718.02	326.07
57.20	753.29	330.70
56.71	788.49	335.32
56.22	823.63	339.94
55.73	858.70	344.56
55.25	893.70	349.18
54.76	928.64	353.80

***** Pore Pressures *****

Total	Static	Excess	Material
361.22	361.22	.00	6
391.94	391.94	.00	6
422.59	422.59	.00	6
453.17	453.17	.00	6
483.69	483.69	.00	6
514.14	514.14	.00	6
544.52	544.52	.00	6
574.84	574.84	.00	6

54.28	963.51	358.42	605.10	605.10	.00	6
54.28	963.51	358.42	605.10	605.10	.00	5
53.19	1056.92	384.17	672.76	672.76	.00	5
52.12	1149.41	409.92	739.49	739.49	.00	5
51.07	1240.96	435.67	805.29	805.29	.00	5
50.03	1331.61	461.42	870.19	870.19	.00	5
49.00	1421.31	487.17	934.14	934.14	.00	5
47.99	1510.19	512.92	997.27	997.28	.00	5
47.99	1510.19	512.92	997.27	997.28	.00	4
46.03	1708.30	569.99	1138.31	1119.52	18.79	4
44.08	1905.72	627.25	1278.46	1241.08	37.38	4
42.15	2102.45	685.11	1417.34	1361.96	55.39	4
40.22	2298.49	744.05	1554.44	1482.14	72.30	4
38.31	2493.81	804.81	1689.00	1601.60	87.40	4
36.40	2688.40	868.39	1820.00	1720.32	99.68	4
34.51	2882.20	936.40	1945.80	1838.27	107.53	4
32.64	3075.15	1010.49	2064.66	1955.36	109.30	4
30.78	3267.19	1086.56	2180.62	2071.54	109.08	4
30.78	3267.19	1086.56	2180.62	2071.54	109.08	3
29.41	3414.49	1148.58	2265.91	2156.98	108.93	3
28.04	3561.45	1209.08	2352.38	2242.09	110.29	3
26.68	3708.08	1268.25	2439.83	2326.85	112.97	3
25.33	3854.38	1326.39	2527.99	2411.29	116.70	3
23.98	4000.35	1383.63	2616.72	2495.41	121.31	3
22.64	4146.00	1440.12	2705.88	2579.20	126.68	3
21.30	4291.34	1496.01	2795.32	2662.68	132.65	3
19.97	4436.36	1551.44	2884.92	2745.84	139.08	3
18.64	4581.07	1606.53	2974.54	2828.70	145.84	3
18.64	4581.07	1606.53	2974.54	2828.70	145.84	2
16.74	4785.71	1678.67	3107.03	2947.23	159.80	2
14.85	4989.88	1753.69	3236.19	3065.31	170.88	2
12.97	5193.59	1831.48	3362.11	3182.92	179.19	2
11.09	5396.82	1912.54	3484.28	3300.05	184.23	2
9.22	5599.53	1997.19	3602.34	3416.66	185.67	2
7.36	5801.71	2124.87	3676.85	3532.75	144.10	2
5.51	6003.38	2251.47	3751.91	3648.31	103.60	2
3.66	6204.52	2374.85	3829.67	3763.36	66.31	2
1.83	6405.17	2494.40	3910.77	3877.91	32.86	2
.00	6605.34	2610.48	3994.86	3991.98	2.88	2

Time = 6480. Degree of Consolidation = 88.%

Total Settlement = 2.399

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 6480. = 2.391

Settlement caused by Secondary Compression at time 6480. = .008

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1
3.00	2.87	1.52	.98	.90	.90	1

1.50	1.44	.76	.98	.90	1
.00	.00	.00	.98	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.97	80.36	91.61	91.61	.00	1
2.87	342.56	160.73	181.83	181.83	.00	1
1.44	512.75	241.09	271.66	271.66	.00	1
.00	682.67	321.45	361.22	361.22	.00	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .211

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 6480. = .211

Settlement caused by Secondary Compression at time 6480. = .000

Surface Elevation = 1.99

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.14	21.42	6.50	5.53	5.53	6
60.02	57.65	21.35	6.49	5.51	5.52	6
59.45	57.16	21.27	6.47	5.49	5.50	6
58.89	56.67	21.20	6.46	5.48	5.49	6
58.33	56.18	21.12	6.44	5.46	5.47	6
57.76	55.69	21.05	6.43	5.45	5.46	6
57.20	55.21	20.97	6.42	5.44	5.45	6
56.64	54.72	20.90	6.40	5.42	5.43	6
56.08	54.24	20.82	6.39	5.41	5.42	6
56.08	54.24	20.82	4.51	3.71	3.71	5
54.82	53.15	20.59	4.44	3.64	3.65	5
53.56	52.08	20.36	4.38	3.58	3.58	5
52.32	51.03	20.12	4.32	3.52	3.52	5
51.10	49.99	19.89	4.25	3.45	3.46	5
49.88	48.96	19.66	4.19	3.39	3.39	5
48.69	47.95	19.43	4.13	3.34	3.35	5
48.69	47.95	19.43	1.93	1.88	1.88	4
46.69	45.99	18.75	1.92	1.86	1.86	4
44.70	44.05	18.06	1.91	1.84	1.83	4
42.72	42.11	17.38	1.89	1.83	1.81	4
40.75	40.18	16.70	1.88	1.81	1.79	4
38.79	38.27	16.01	1.86	1.79	1.77	4
36.85	36.37	15.33	1.84	1.77	1.75	4
34.91	34.48	14.65	1.82	1.75	1.73	4
33.00	32.61	13.97	1.80	1.73	1.71	4
31.09	30.75	13.28	1.78	1.71	1.68	4
31.09	30.75	13.28	1.47	1.43	1.42	3
29.70	29.38	12.72	1.46	1.42	1.41	3

28.32	28.02	12.16	1.45	1.41	1.40	3
26.94	26.66	11.59	1.44	1.40	1.39	3
25.57	25.31	11.03	1.43	1.39	1.38	3
24.21	23.97	10.47	1.42	1.39	1.37	3
22.84	22.62	9.90	1.41	1.38	1.36	3
21.49	21.29	9.34	1.40	1.37	1.35	3
20.14	19.96	8.78	1.39	1.36	1.34	3
18.80	18.63	8.21	1.38	1.35	1.33	3
18.80	18.63	8.21	1.34	1.31	1.30	2
16.88	16.73	7.39	1.33	1.31	1.29	2
14.97	14.84	6.57	1.32	1.30	1.28	2
13.07	12.96	5.75	1.31	1.29	1.27	2
11.18	11.08	4.93	1.30	1.28	1.26	2
9.30	9.22	4.11	1.29	1.27	1.26	2
7.43	7.36	3.29	1.28	1.26	1.25	2
5.56	5.51	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.14	682.67	321.45	361.22	361.22	.00	6
57.65	718.01	326.07	391.94	391.94	.00	6
57.16	753.27	330.70	422.58	422.58	.00	6
56.67	788.47	335.32	453.15	453.15	.00	6
56.18	823.60	339.94	483.66	483.66	.00	6
55.69	858.66	344.56	514.11	514.11	.00	6
55.21	893.66	349.18	544.48	544.48	.00	6
54.72	928.59	353.80	574.79	574.79	.00	6
54.24	963.46	358.42	605.04	605.04	.00	6
54.24	963.46	358.42	605.04	605.04	.00	5
53.15	1056.85	384.17	672.69	672.69	.00	5
52.08	1149.33	409.92	739.41	739.41	.00	5
51.03	1240.87	435.67	805.20	805.20	.00	5
49.99	1331.50	461.42	870.09	870.09	.00	5
48.96	1421.20	487.17	934.03	934.03	.00	5
47.95	1510.07	512.92	997.15	997.15	.00	5
47.95	1510.07	512.92	997.15	997.15	.00	4
45.99	1708.16	571.41	1136.75	1119.39	17.36	4
44.05	1905.56	630.16	1275.40	1240.92	34.47	4
42.11	2102.25	689.58	1412.67	1361.75	50.91	4
40.18	2298.22	750.26	1547.96	1481.87	66.09	4
38.27	2493.46	812.95	1680.51	1601.25	79.26	4
36.37	2687.93	878.72	1809.21	1719.86	89.35	4
34.48	2881.60	949.23	1932.37	1837.67	94.70	4
32.61	3074.38	1024.94	2049.45	1954.59	94.85	4
30.75	3266.23	1102.06	2164.17	2070.58	93.59	4
30.75	3266.23	1102.06	2164.17	2070.58	93.59	3
29.38	3413.45	1165.11	2248.34	2155.94	92.40	3
28.02	3560.32	1226.49	2333.82	2240.95	92.87	3
26.66	3706.84	1286.39	2420.45	2325.62	94.84	3
25.31	3853.03	1344.96	2508.07	2409.95	98.12	3
23.97	3998.90	1402.48	2596.42	2493.96	102.46	3
22.62	4144.45	1459.12	2685.32	2577.65	107.68	3
21.29	4289.68	1515.04	2774.63	2661.02	113.62	3
19.96	4434.59	1570.37	2864.22	2744.07	120.15	3
18.63	4579.20	1625.20	2954.00	2826.82	127.18	3
18.63	4579.20	1625.20	2954.00	2826.82	127.18	2
16.73	4783.72	1696.98	3086.74	2945.24	141.50	2
14.84	4987.79	1771.17	3216.62	3063.21	153.41	2

12.96	5191.39	1848.16	3343.23	3180.72	162.51	2
11.08	5394.52	1927.89	3466.63	3297.75	168.88	2
9.22	5597.14	2015.84	3581.29	3414.27	167.02	2
7.36	5799.25	2140.89	3658.36	3530.28	128.07	2
5.51	6000.85	2263.56	3737.29	3645.79	91.50	2
3.66	6201.96	2383.20	3818.76	3760.80	57.97	2
1.83	6402.58	2499.17	3903.41	3875.32	28.09	2
.00	6602.74	2610.85	3991.89	3989.38	2.51	2

Time = 7300. Degree of Consolidation = 90.%

Total Settlement = 2.441

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 7300. = 2.431

Settlement caused by Secondary Compression at time 7300. = .010

**********Current Conditions in Dredged Fill**********

***** Coordinates *****

A	XI	Z
6.00	5.79	3.03
4.50	4.32	2.27
3.00	2.87	1.52
1.50	1.44	.76
.00	.00	.00

***** Void Ratios *****

Einitial	E	Eeop	Material
.98	.98	.98	1
.98	.91	.91	1
.98	.90	.90	1
.98	.90	.90	1
.98	.89	.89	1

***** Stresses *****

XI	Total	Effective
5.79	.00	.00
4.32	171.97	80.36
2.87	342.56	160.73
1.44	512.75	241.09
.00	682.67	321.45

***** Pore Pressures *****

Total	Static	Excess	Material
.00	.00	.00	1
91.61	91.61	.00	1
181.83	181.83	.00	1
271.66	271.66	.00	1
361.22	361.22	.00	1

Time = 7300. Degree of Consolidation = 100.%

Total Settlement = .211

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 7300. = .211

Settlement caused by Secondary Compression at time 7300. = .000

Surface Elevation = 1.95

**********Current Conditions in Compressible Foundation**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	58.07	21.42	6.50	5.53	5.53	6
60.02	57.58	21.35	6.49	5.50	5.52	6
59.45	57.09	21.27	6.47	5.49	5.50	6
58.89	56.60	21.20	6.46	5.47	5.49	6
58.33	56.11	21.12	6.44	5.46	5.47	6
57.76	55.62	21.05	6.43	5.45	5.46	6
57.20	55.13	20.97	6.42	5.43	5.45	6
56.64	54.65	20.90	6.40	5.42	5.43	6
56.08	54.16	20.82	6.39	5.40	5.42	6
56.08	54.16	20.82	4.51	3.71	3.71	5
54.82	53.08	20.59	4.44	3.64	3.65	5
53.56	52.01	20.36	4.38	3.58	3.58	5
52.32	50.96	20.12	4.32	3.52	3.52	5
51.10	49.92	19.89	4.25	3.45	3.46	5
49.88	48.89	19.66	4.19	3.39	3.39	5
48.69	47.88	19.43	4.13	3.34	3.35	5
48.69	47.88	19.43	1.93	1.88	1.88	4
46.69	45.92	18.75	1.92	1.86	1.86	4
44.70	43.98	18.06	1.91	1.84	1.83	4
42.72	42.04	17.38	1.89	1.82	1.81	4
40.75	40.12	16.70	1.88	1.81	1.79	4
38.79	38.21	16.01	1.86	1.79	1.77	4
36.85	36.31	15.33	1.84	1.77	1.75	4
34.91	34.43	14.65	1.82	1.75	1.73	4
33.00	32.56	13.97	1.80	1.73	1.71	4
31.09	30.70	13.28	1.78	1.70	1.68	4
31.09	30.70	13.28	1.47	1.43	1.42	3
29.70	29.34	12.72	1.46	1.42	1.41	3
28.32	27.98	12.16	1.45	1.41	1.40	3
26.94	26.62	11.59	1.44	1.40	1.39	3
25.57	25.27	11.03	1.43	1.39	1.38	3
24.21	23.93	10.47	1.42	1.38	1.37	3
22.84	22.59	9.90	1.41	1.37	1.36	3
21.49	21.26	9.34	1.40	1.36	1.35	3
20.14	19.93	8.78	1.39	1.35	1.34	3
18.80	18.61	8.21	1.38	1.34	1.33	3
18.80	18.61	8.21	1.34	1.31	1.30	2
16.88	16.71	7.39	1.33	1.30	1.29	2
14.97	14.83	6.57	1.32	1.29	1.28	2
13.07	12.95	5.75	1.31	1.28	1.27	2
11.18	11.07	4.93	1.30	1.28	1.26	2
9.30	9.21	4.11	1.29	1.27	1.26	2
7.43	7.35	3.29	1.28	1.26	1.25	2
5.56	5.50	2.46	1.27	1.25	1.24	2
3.70	3.66	1.64	1.26	1.24	1.23	2
1.85	1.83	.82	1.25	1.23	1.23	2
.00	.00	.00	1.25	1.22	1.22	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.07	682.67	321.45	361.22	361.22	.00	6
57.58	718.00	326.07	391.93	391.93	.00	6
57.09	753.25	330.70	422.55	422.55	.00	6
56.60	788.43	335.32	453.11	453.11	.00	6
56.11	823.54	339.94	483.60	483.60	.00	6
55.62	858.59	344.56	514.03	514.03	.00	6
55.13	893.57	349.18	544.39	544.39	.00	6

54.65	928.48	353.80	574.68	574.68	.00	6
54.16	963.33	358.42	604.91	604.91	.00	6
54.16	963.33	358.42	604.91	604.91	.00	5
53.08	1056.72	384.17	672.55	672.55	.00	5
52.01	1149.18	409.92	739.26	739.26	.00	5
50.96	1240.70	435.67	805.04	805.04	.00	5
49.92	1331.33	461.42	869.91	869.91	.00	5
48.89	1421.00	487.17	933.83	933.83	.00	5
47.88	1509.85	512.92	996.94	996.94	.00	5
47.88	1509.85	512.92	996.94	996.94	.00	4
45.92	1707.93	573.74	1134.20	1119.16	15.04	4
43.98	1905.29	634.98	1270.31	1240.65	29.66	4
42.04	2101.90	697.10	1404.81	1361.41	43.40	4
40.12	2297.77	760.73	1537.04	1481.42	55.63	4
38.21	2492.87	826.62	1666.25	1600.66	65.59	4
36.31	2687.16	896.04	1791.12	1719.09	72.03	4
34.43	2880.59	971.02	1909.57	1836.66	72.91	4
32.56	3073.09	1049.76	2023.33	1953.30	70.03	4
30.70	3264.62	1128.97	2135.65	2068.97	66.68	4
30.70	3264.62	1128.97	2135.65	2068.97	66.68	3
29.34	3411.68	1193.79	2217.88	2154.17	63.71	3
27.98	3558.38	1256.68	2301.70	2239.01	62.69	3
26.62	3704.73	1317.80	2386.93	2323.50	63.43	3
25.27	3850.74	1377.34	2473.40	2407.66	65.75	3
23.93	3996.43	1435.61	2560.82	2491.48	69.33	3
22.59	4141.78	1492.76	2649.02	2574.98	74.04	3
21.26	4286.82	1548.94	2737.88	2658.16	79.72	3
19.93	4431.55	1604.29	2827.25	2741.03	86.22	3
18.61	4575.96	1658.96	2917.01	2823.59	93.42	3
18.61	4575.96	1658.96	2917.01	2823.59	93.42	2
16.71	4780.28	1730.35	3049.92	2941.80	108.12	2
14.83	4984.14	1803.61	3180.53	3059.57	120.96	2
12.95	5187.55	1879.01	3308.54	3176.88	131.66	2
11.07	5390.49	1956.52	3433.97	3293.72	140.25	2
9.21	5592.95	2053.44	3539.51	3410.08	129.43	2
7.35	5794.92	2171.58	3623.34	3525.96	97.38	2
5.50	5996.41	2286.72	3709.69	3641.35	68.34	2
3.66	6197.44	2398.50	3798.94	3756.28	42.66	2
1.83	6398.02	2506.97	3891.05	3870.76	20.29	2
.00	6598.15	2611.45	3986.70	3984.80	1.90	2

Time = 9125. Degree of Consolidation = 92.%

Total Settlement = 2.514

Settlement at End of Primary Consolidation = 2.722

Settlement caused by Primary Consolidation at time 9125. = 2.501

Settlement caused by Secondary Compression at time 9125. = .013

**********Current Conditions in Dredged Fill**********

***** Coordinates *****			***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
6.00	5.79	3.03	.98	.98	.98	1
4.50	4.32	2.27	.98	.91	.91	1

3.00	2.87	1.52	.98	.90	.90	1
1.50	1.44	.76	.98	.90	.90	1
.00	.00	.00	.98	.89	.89	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
5.79	.00	.00	.00	.00	.00	1
4.32	171.97	80.36	91.61	91.61	.00	1
2.87	342.56	160.73	181.83	181.83	.00	1
1.44	512.75	241.09	271.66	271.66	.00	1
.00	682.67	321.45	361.22	361.22	.00	1

Time = 9125. Degree of Consolidation = 100.%

Total Settlement = .211

Settlement at End of Primary Consolidation = .211

Settlement caused by Primary Consolidation at time 9125. = .211

Settlement caused by Secondary Compression at time 9125. = .000

Surface Elevation = 1.87

APPENDIX E

PSDDF Settlement Analysis for Bayou Dupont Marsh Creation (BA-48)

FINAL REPORT

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SUMMARY

This report summarizes the results of settlement analysis for Bayou Dupont marsh creation due to the placement of dredged sediments as hydraulic fill on marsh soil in Bayou Dupont. The settlement analysis was performed to estimate the long-term settlement of the dredged fill and the existing marsh foundation soils using the US Army Corps of Engineers computer program Primary Consolidation, Secondary Compression, and Desiccation of Dredged Fill (PSDDF). The settlement analysis considered five fill heights over the project life of >20 years. Two sample calculations and the corresponding output files for two different cases of marsh soil stratification and classification were provided.

TABLE OF CONTENTS

1. INTRODUCTION

This report presents the results of a settlement analysis for the proposed Bayou Dupont March Creation Project (BA-46) that involves placing dredged sediments on existing marsh soil in Bayou Dupont. The US Army Corps of Engineers (USACE) computer program Primary Consolidation, Secondary Compression, and Desiccation of Dredged Fill (PSDDF) was used to determine the long-term settlement of the dredged fill and existing marsh foundation soil. The long-term total settlement consists of primary consolidation, secondary compression, and desiccation induced settlement.

2. INPUT DATA

Marsh Soil as the Foundation for the Dredged Fill

Information on the soil profile and stratification of the marsh soil was obtained from the results of geotechnical site investigation provided by URS Corporation. Totally 9 boring logs, 13 1-D consolidation test results, and other index testing results were provided by URS Corporation. These geotechnical investigation results were analyzed, compiled, and evaluated to obtain the marsh soil profile stratification and related consolidation properties of each soil stratum. Based on the boring logs, the average existing surface elevation of the marsh is estimated to be 0-1.4 feet (the current water table or the sea level elevation is taken as 0.0 ft). The underlying soil is subdivided into five (5) layers. The thickness of each layer can be found in the PSDDF output data (see Appendix II or III). The three deepest borings terminated at elevation around -60 to -63 ft. Therefore, no information is available for soils beneath this elevation, and it was assumed the soils beneath this elevation contribute little estimated settlement of the subsurface foundation soils.

The engineering properties of the five layer compressible foundation soils were obtained from the results of geotechnical laboratory testing provided by URS Corporation. The required properties include: the relationship or plot of void ratio – effective stress – permeability, the ratios of C_α/C_c and C_r/C_c, initial void ratio, and specific gravity. Again, details of these data on engineering properties can be found in the PSDDF output data (see Appendices II and III).

Dredged Fill

Required input data for the proposed dredged fill material include the self-weight consolidation properties and basic index properties. These data were obtained from a previous Bayou Dupont Marsh Creation project (BA-39). Again, details of these data can be found in the PSDDF output data (see Appendices II and III).

Climatic Data

Consideration of the desiccation-induced settlement requires the monthly evaporation and precipitation (E&P) data at the construction site. The available climatic data from the nearest weather station – Houma Station, Louisiana, were obtained from the National Climatic Data Center (http://www.ncdc.noaa.gov/). For this specific station, E&P data were available from 1931 to 2006, totally 76 years (see Appendix I). The monthly evaporation and precipitation values were averaged over 76 years and subsequently used as input to the PSDDF program.

3. SETTLEMENT CALCULATION

Settlement calculation considered five target fill heights, including 2.0, 3.0, 3.5, 4.0, and 5.0 ft above the existing marsh surface elevation. The time duration considered for primary consolidation, secondary compression, and desiccation is 20 years. An example calculation is provided in Appendix II.

The PSDDF analysis provides zero or negligible desiccation-induced settlement, this is due to two reasons: (1) the tested dredged fill material is primarily a sand river deposit, and shrinkage will cause a negligible volume change or settlement; and (2) the average monthly precipitation is mostly greater than the evaporation for the selected weather station used for the construction site. Therefore, for this special case, the desiccation-induced settlement is very small or negligible.

Upon request of URS Corporation, two cases of the foundation soil profile were considered for the settlement analysis. In particular, the two cases considered two different interpretations for the 5^{th} layer (7.40 ft thick) of the marsh soil: (A) this layer is a silty clay or clayey silt material; and (B) this layer is a highly organic soil or peat material, similar to the surface layer (the 6^{th} layer). These two different interpretations were mainly caused by the variation in both horizontal and vertical stratification in the marsh soil. As a result, Case A gives much smaller settlement than Case B.

4. RESULTS

The results of final settlement analysis consist of three sets of plots:

Case A:

This set of plots treats the 5^{th} layer as a silty clay or clayey silt;
Figure 1 plots the predicted surface elevation of the dredged fill versus time (30 years);
Figure 2 plots the marsh foundation total settlement versus time;
Figure 3 plots the dredged fill settlement versus time.

Case B:

This set of plots treats the 5^{th} layer as an organic soil or peat;
Figure 4 plots the predicted surface elevation of the dredged fill versus time (30 years);
Figure 5 plots the marsh foundation total settlement versus time;
Figure 6 plots the dredged fill settlement versus time.

Case C:

This set of plots is the average results of Case A and Case B;
Figure 7 plots the predicted surface elevation of the dredged fill versus time (30 years);
Figure 8 plots the marsh foundation total settlement versus time;
Figure 9 plots the dredged fill settlement versus time.

Appendix III shows an example PSDDF output file for Case A 5 ft initial fill elevation.
Appendix IV shows an example PSDDF output file for Case B 5 ft initial fill elevation.

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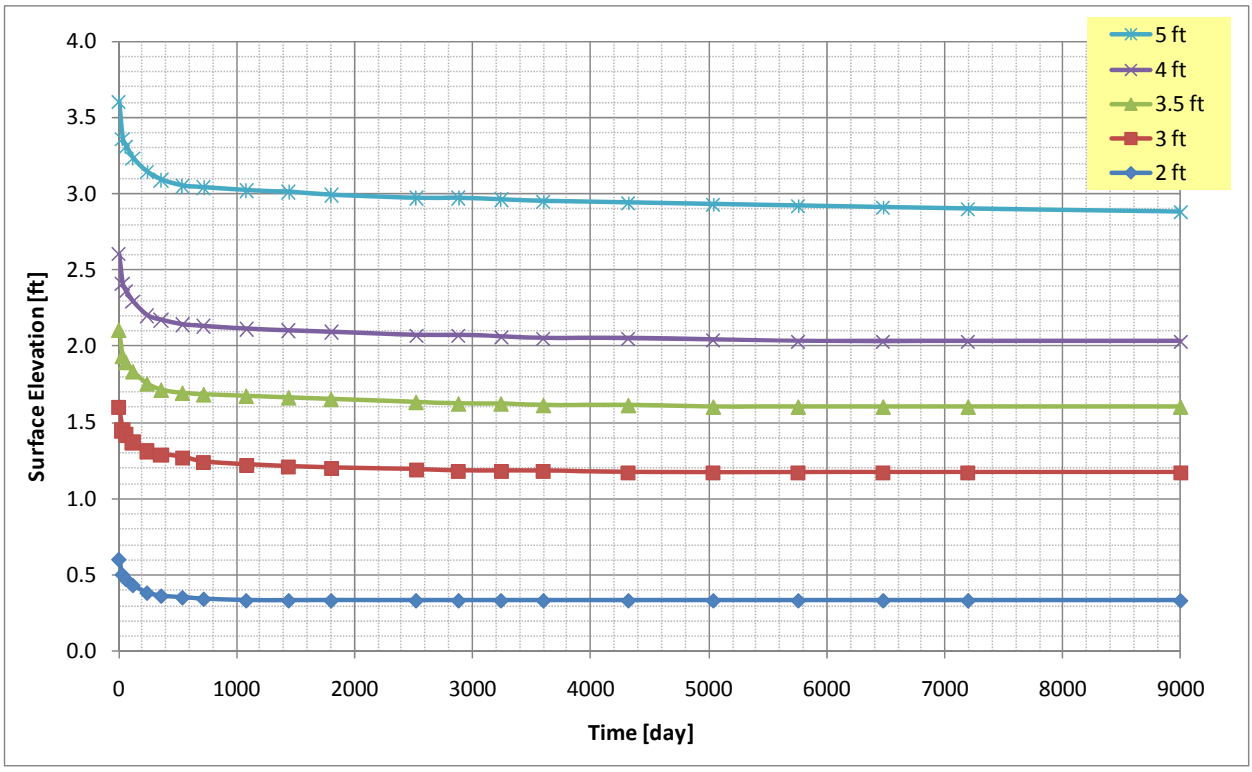

Figure 1. Case A: surface elevation vs. time curves for five initial fill heights (2, 3, 3.5, 4, and 5 ft above the marsh surface).

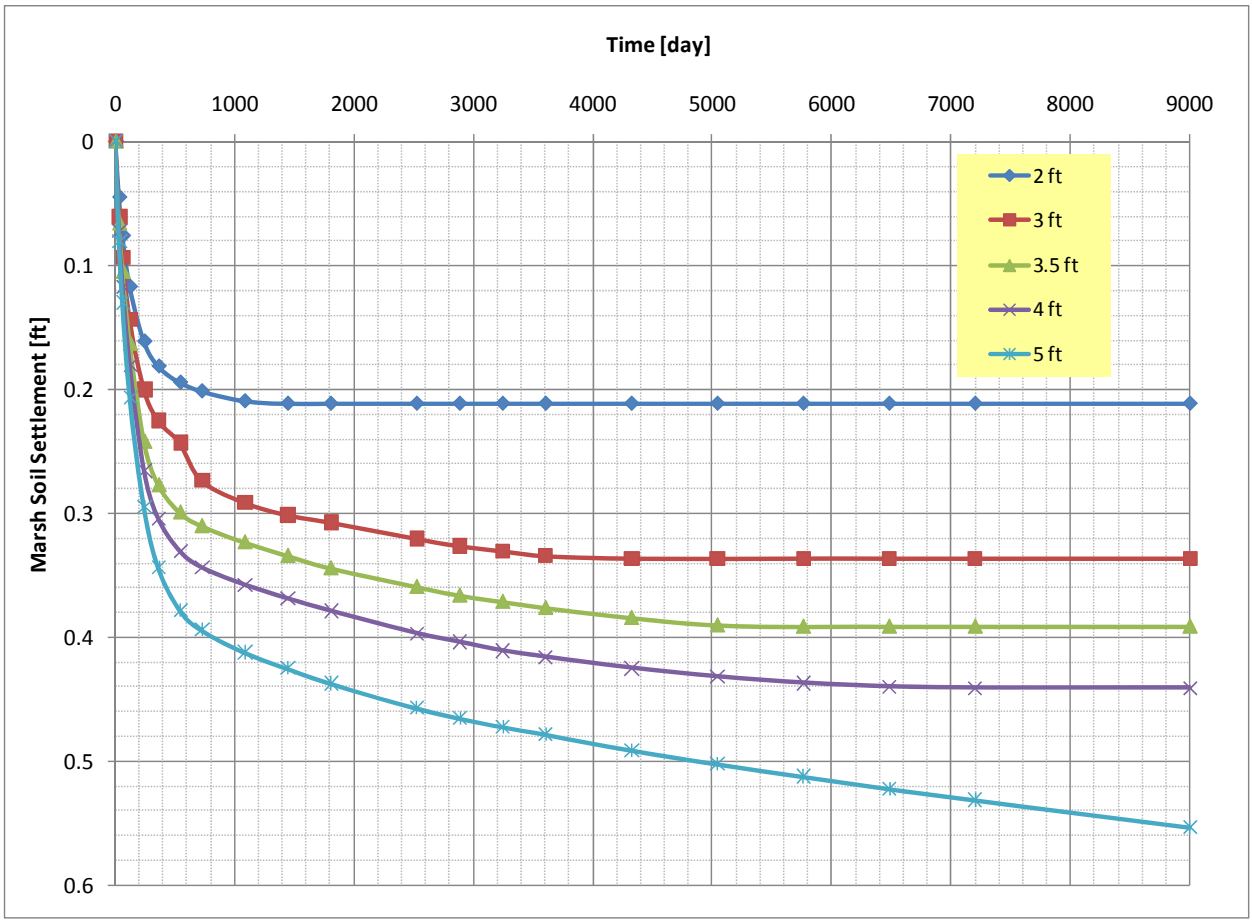

Figure 2. Case A: marsh soil settlement vs. time curves for five fill heights (2, 3, 3.5, 4, and 5 ft above the marsh soil).

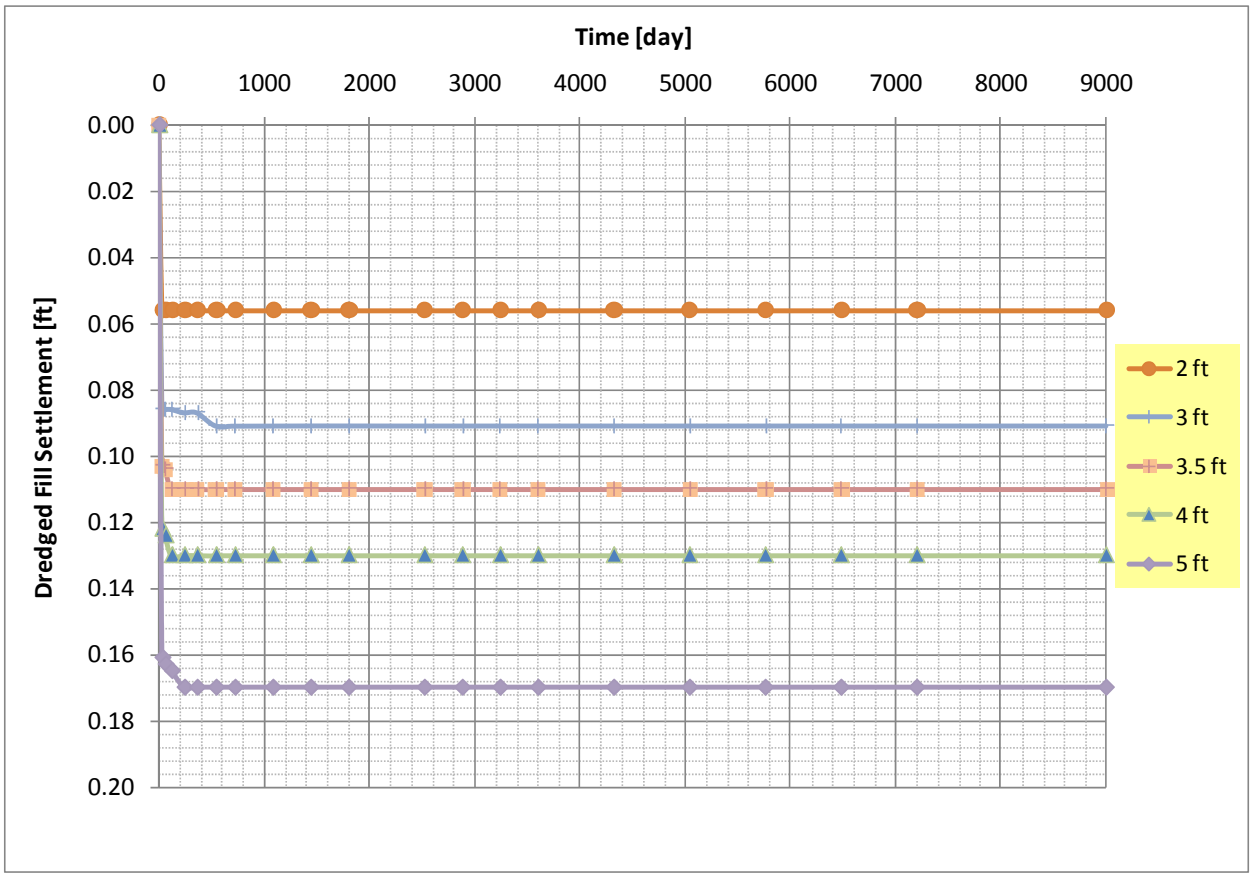

Figure 3. Case A: fill settlement vs. time curves for five fill heights (2, 3, 3.5, 4, and 5 ft above the marsh soil).

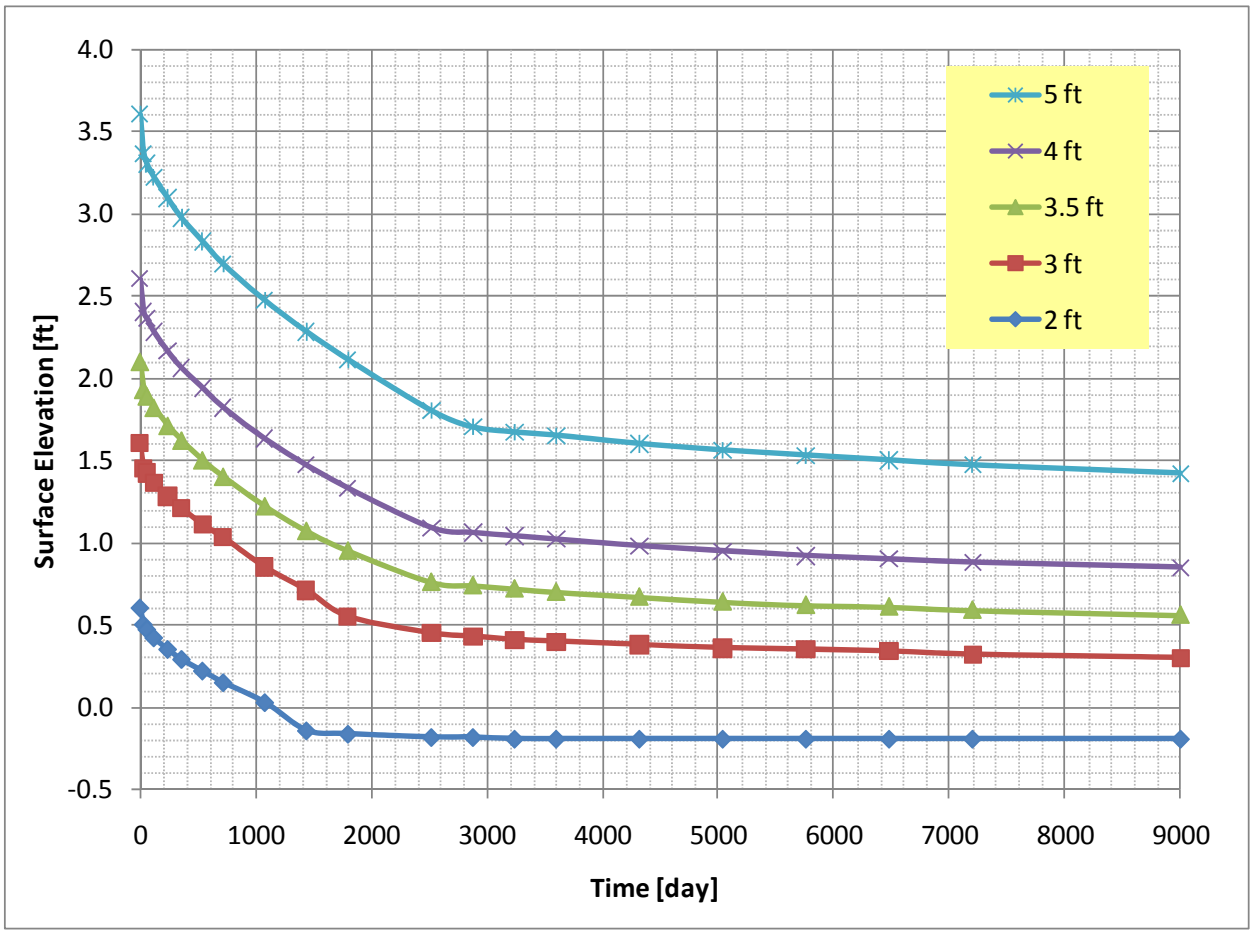

Figure 4. Case B: surface elevation vs. time curves for five initial fill heights (2, 3, 3.5, 4, and 5 ft above the marsh surface).

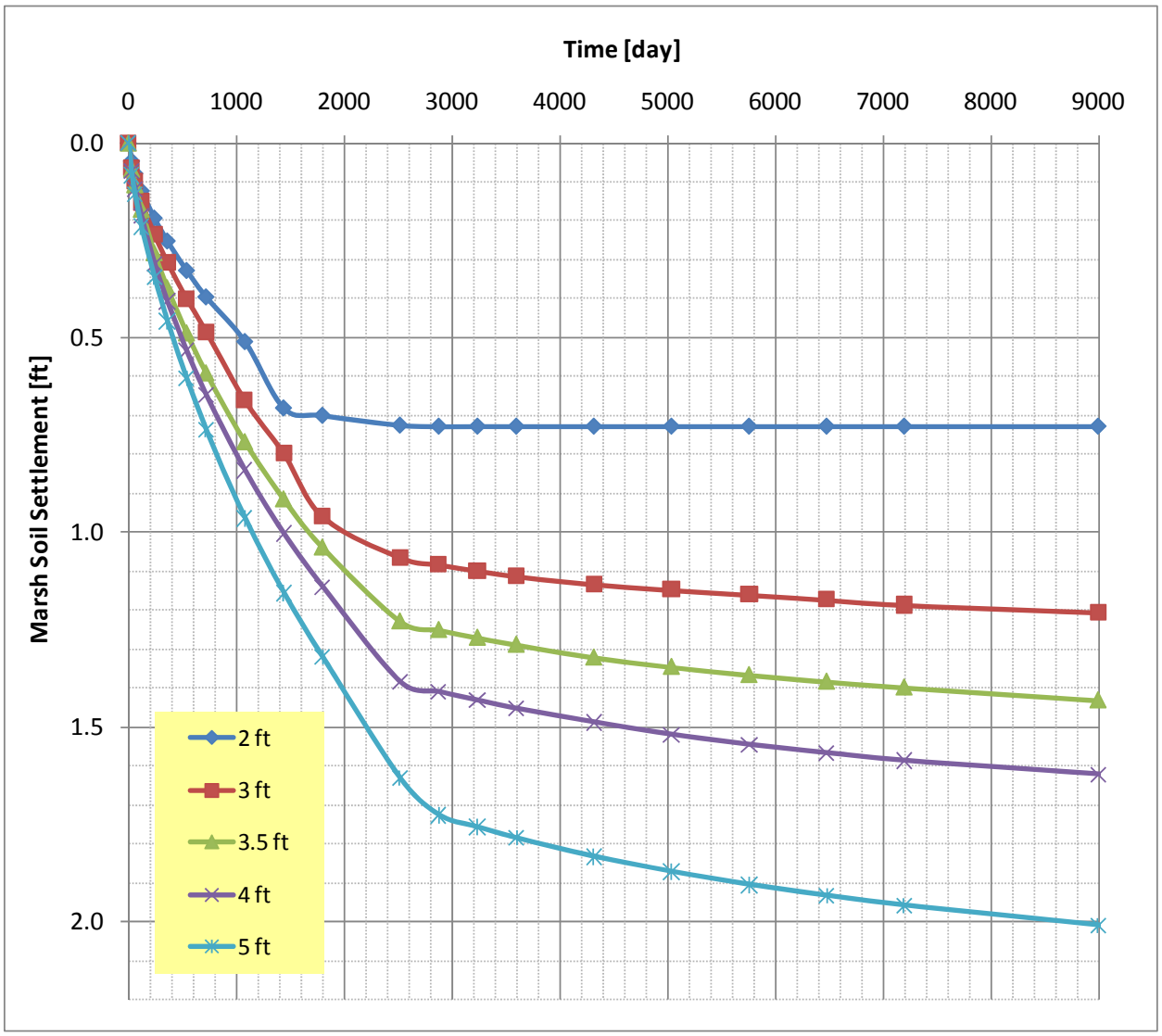

Figure 5. Case B: marsh soil settlement vs. time curves for five fill heights (2, 3, 3.5, 4, and 5 ft above the marsh soil).

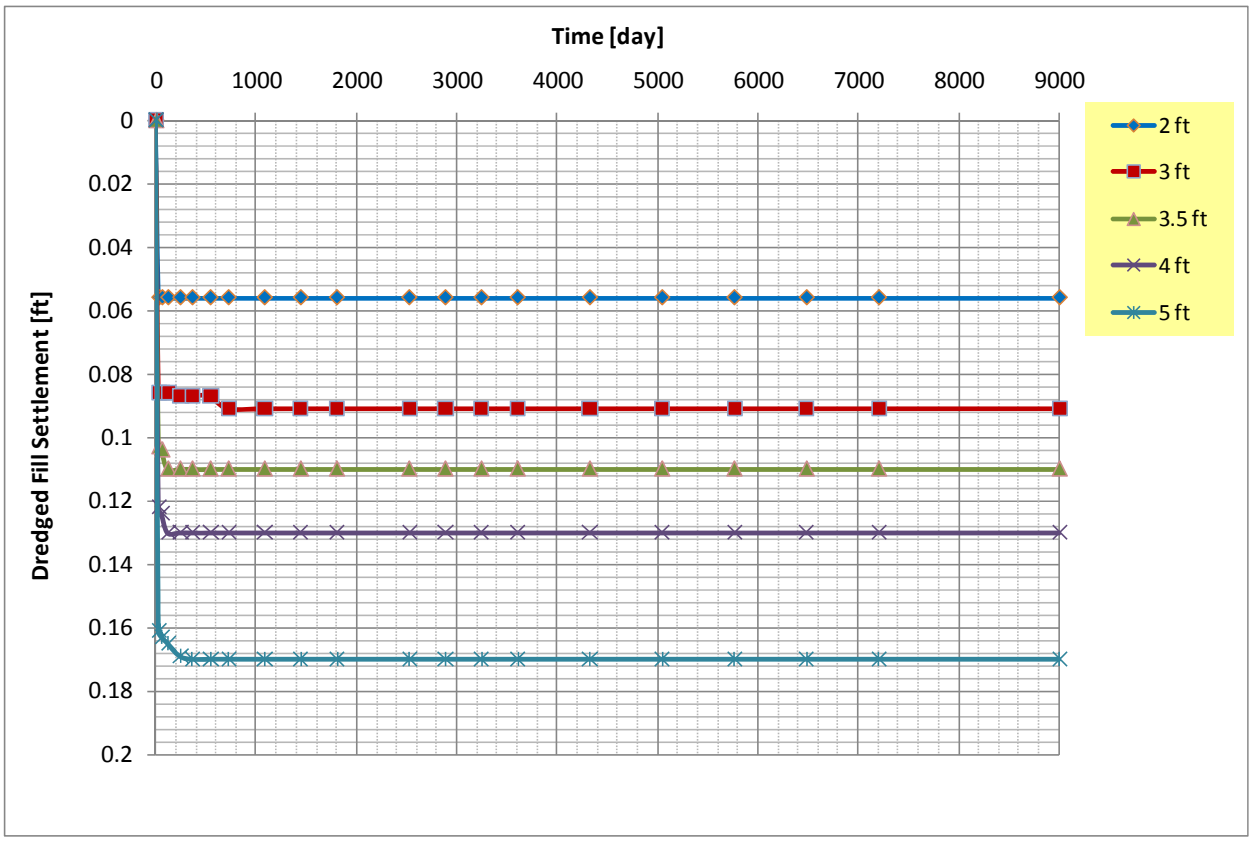

Figure 6. Case B: fill settlement vs. time curves for five fill heights (2, 3, 3.5, 4, and 5 ft above the marsh soil).

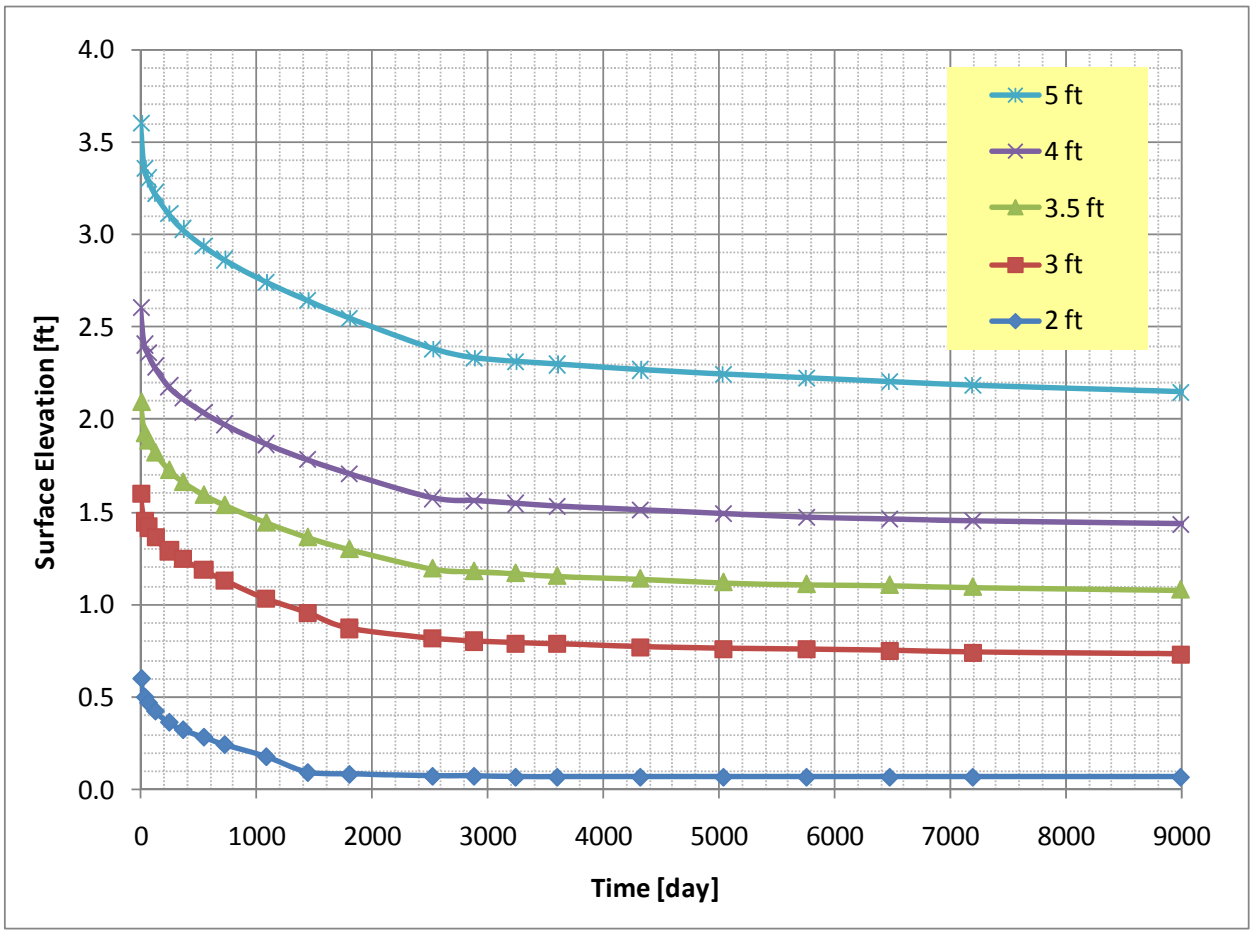

Figure 7. Case C: surface elevation vs. time curves for five initial fill heights (2, 3, 3.5, 4, and 5 ft above the marsh surface).

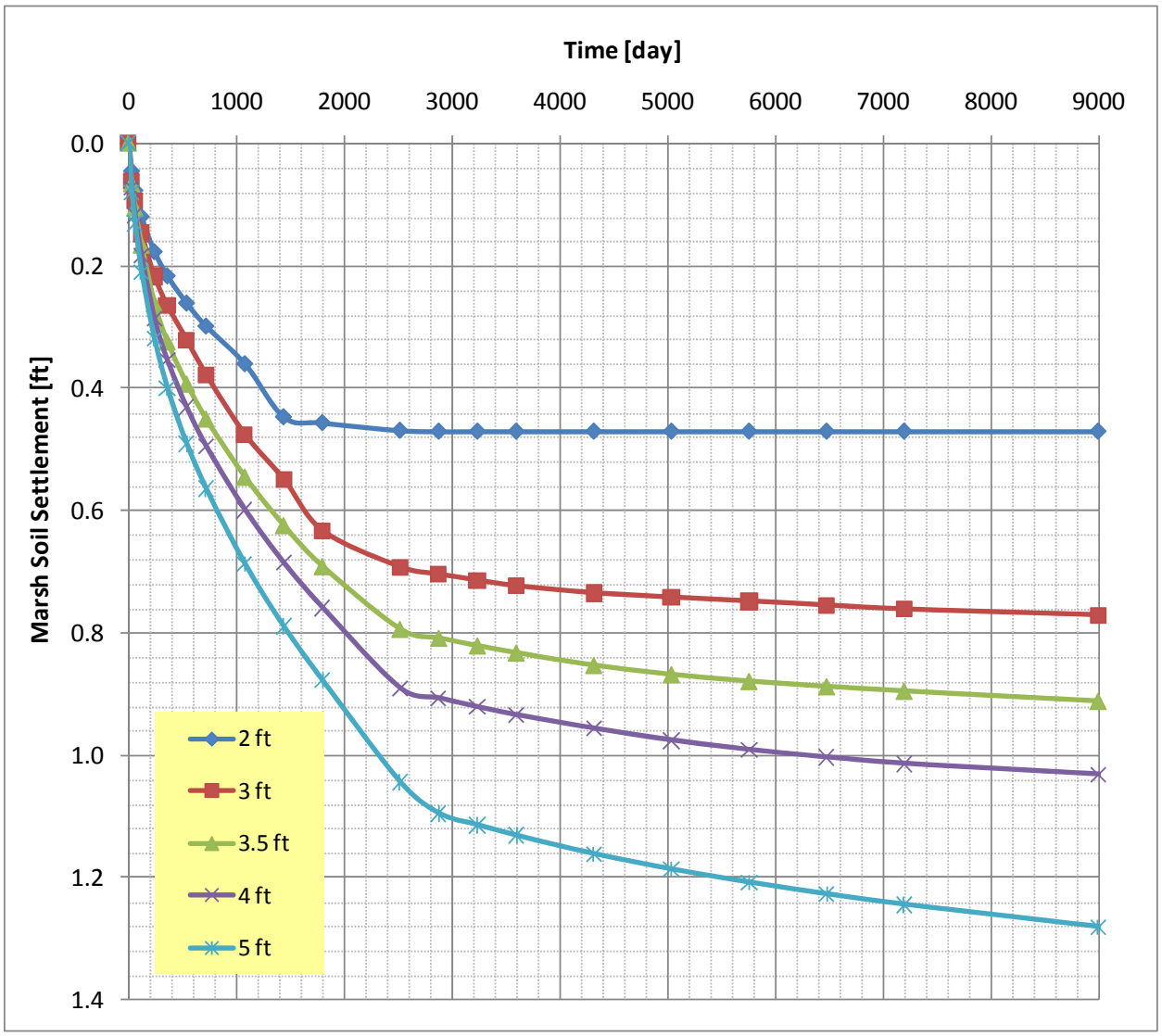

Figure 8. Case C: marsh soil settlement vs. time curves for five fill heights (2, 3, 3.5, 4, and 5 ft above the marsh soil).

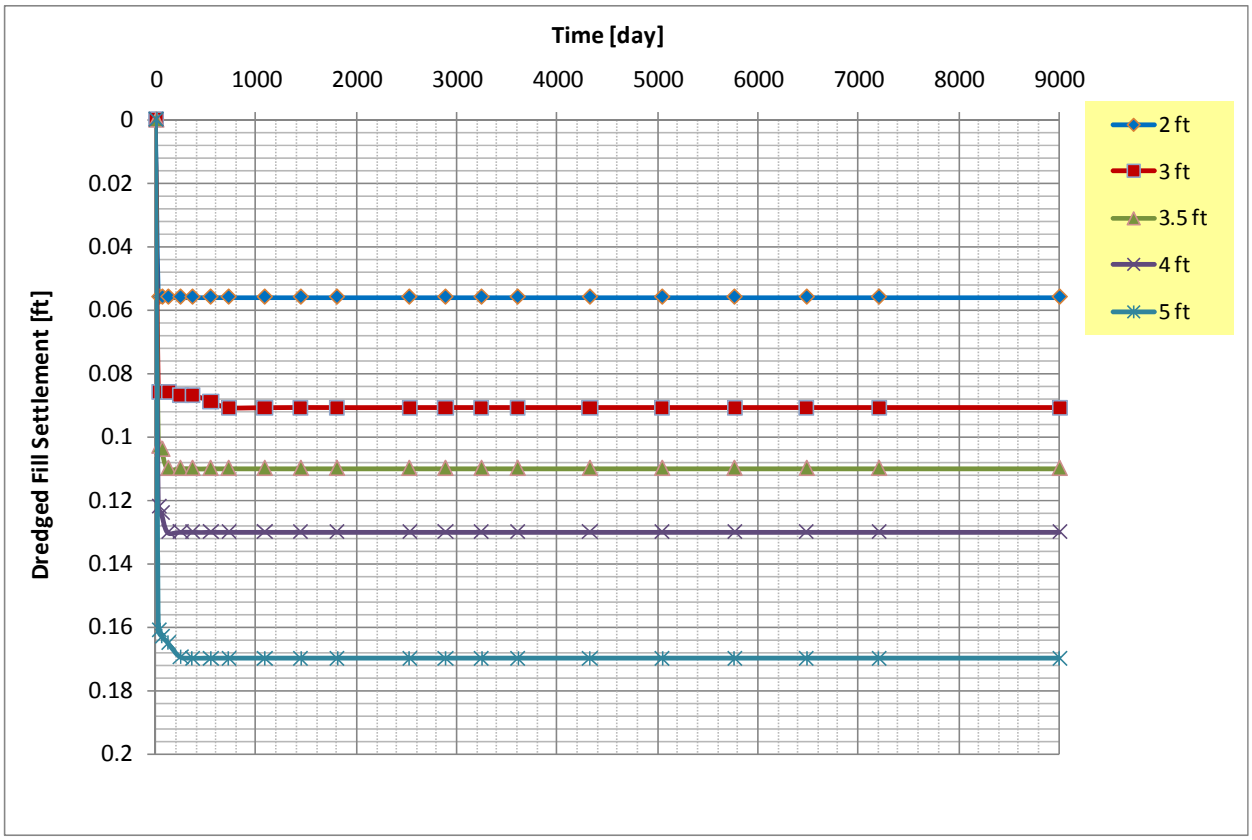

Figure 9. Case C: fill settlement vs. time curves for five fill heights (2, 3, 3.5, 4, and 5 ft above the marsh soil).

APPENDIX I

Climatic Data for Houma Weather Station

COOPID,WBNID,CD,ELEM,UN,YEAR,A,S,MO,DA, JAN ,F,F,MO,DA, FEB ,F,F,MO,DA, MAR ,F,F,MO,DA, APR ,F,F,MO,DA, MAY ,F,F,MO,DA, JUN ,F,F,MO,DA, JUL ,F,F,MO,DA, AUG ,F,F,MO,DA, SEP ,F,F,MO,DA, OCT ,F,F,MO,DA, NOV ,F,F,MO,DA, DEC ,F,F,MO,DA,ANNUAL,F,F

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164407,99999,09,TEVP,HI,2005,9,9,01,99,-99999,M, ,02,00, 00246,B, ,03,00, 00461,B, ,04,00, 00570,B, ,05,99,-99999,M, ,06,99,-99999,M, ,07,00, 00666,B, ,08,00, 00571,B, ,09,00, 00654,B, ,10,00, 00561,B, ,11,00, 00325, , ,12,00, 00272,B, ,13,99,-99999,M,
164407,99999,09,TPCP,HI,2005,9,9,01,00, 00355, , ,02,00, 01272, , ,03,00, 00745, , ,04,00, 00177, , ,05,00, 00149, , ,06,00, 00860, , ,07,00, 00586, , ,08,00, 00903, , ,09,00, 00611, , ,10,00, 00030, , ,11,00, 00290, , ,12,00, 00311, , ,13,00, 06289, ,
164407,99999,09,TEVP,HI,2006,9,9,01,00, 00266, , ,02,00, 00351,B, ,03,00, 00503,B, ,04,00, 00689,B, ,05,00, 00693,B, ,06,99,-99999,M, ,07,00, 00676,B, ,08,00, 00667,B, ,09,00, 00707, , ,10,00, 00482,B, ,11,00, 00330,B, ,12,00, 00226,B, ,13,99,-99999,M,
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APPENDIX II

PSDDF sample calculation and output file for CASE A 5.0 ft thick fill in Bayou Dupont Marsh

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**********************************************************
Consolidation and desiccation of soft layers---dredged fill
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 Problem    Bayou Dupont Marsh Creation BA-48 5.0 ft Fill



**********Soil data for compressible foundation**********

 Material   Layer      Numbers of     Ca/Cc    Cr/Cc
 Type       Thickness  Sub-layers

  2         18.80      10             .015     .113

  3         12.30      9              .021     .135

  4         17.60      9              .014     .140

  5          7.40      6              .019     .147

  6          4.50      8              .040     .215

 Material type :   2              Specific Gravity of Solids:   2.68


     Void  Effective   Perm-    k/1+e
  I Ratio   Stress  eability   PK      Beta      Dsde     Alpha
  1 1.510  .000E+00 .100E-02  .398E-03  .650E-02 -.100E+05 -.398E+01
  2 1.460  .500E+03 .180E-03  .732E-04  .287E-02 -.833E+04 -.610E+00
  3 1.390  .100E+04 .130E-03  .544E-04  .263E-03 -.789E+04 -.429E+00
  4 1.270  .200E+04 .526E-04  .232E-04  .150E-03 -.107E+05 -.248E+00
  5 1.110  .400E+04 .263E-04  .125E-04  .530E-04 -.194E+05 -.241E+00
  6  .960  .800E+04 .132E-04  .673E-05  .294E-04 -.400E+05 -.269E+00
  7  .810  .160E+05 .658E-05  .364E-05  .171E-04 -.857E+05 -.312E+00
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8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00
8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.890	.000E+00	.600E-02	.317E-02	.388E-01	-.125E+05	-.397E+02
2	.850	.500E+03	.300E-02	.162E-02	.319E-01	-.143E+05	-.232E+02
3	.820	.100E+04	.171E-02	.940E-03	.167E-01	-.300E+05	-.282E+02

4	.800	.200E+04	.142E-02	.789E-03	.764E-02	-.500E+05	-.394E+02
5	.760	.400E+04	.847E-03	.481E-03	.695E-02	-.750E+05	-.361E+02
6	.720	.800E+04	.400E-03	.233E-03	.428E-02	-.133E+06	-.310E+02
7	.670	.160E+05	.161E-03	.964E-04	.184E-02	-.240E+06	-.231E+02
8	.620	.320E+05	.787E-04	.486E-04	.957E-03	-.320E+06	-.155E+02

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit
1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02

5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	5.0	4	.98	120.	4	1
30.				120.	4	1	
60.				120.	4	1	
120.				120.	4	1	
240.				120.	4	1	
360.				120.	4	1	
540.				120.	4	1	
720.				120.	4	1	
1080.				120.	4	1	
1440.				120.	4	1	
1800.				120.	4	1	
2520.				120.	4	1	
2880.				120.	4	1	
3240.				120.	4	1	
3600.				120.	4	1	
4320.				120.	4	1	
5040.				120.	4	1	
5760.				120.	4	1	
6480.				120.	4	1	
7200.				120.	4	1	
9000.				120.	4	1	

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250

3	.400	.380
4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.173	1.106	.30000E-04	z = 14.25

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4

elevation of fixed water table .00
elevation of top of incompres. found. -62.00
==========

**********Initial Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.58	24.38	6.50	6.50	5.69	6
60.02	60.02	24.30	6.49	6.49	5.68	6
59.45	59.45	24.22	6.47	6.47	5.66	6
58.89	58.89	24.15	6.46	6.46	5.65	6
58.33	58.33	24.07	6.44	6.44	5.64	6
57.76	57.76	24.00	6.43	6.43	5.62	6
57.20	57.20	23.92	6.42	6.42	5.61	6
56.64	56.64	23.85	6.40	6.40	5.59	6
56.09	56.09	23.77	6.39	6.39	5.58	6
56.09	56.09	23.77	.89	.89	.87	5
54.84	54.84	23.11	.88	.88	.86	5
53.60	53.60	22.45	.88	.88	.85	5
52.37	52.37	21.79	.87	.87	.85	5
51.14	51.14	21.13	.86	.86	.84	5
49.91	49.91	20.47	.86	.86	.84	5
48.69	48.69	19.81	.85	.85	.84	5
48.69	48.69	19.81	1.88	1.88	1.81	4
46.67	46.67	19.11	1.86	1.86	1.79	4
44.67	44.67	18.41	1.84	1.84	1.77	4
42.68	42.68	17.71	1.82	1.82	1.75	4
40.71	40.71	17.01	1.80	1.80	1.72	4
38.76	38.76	16.31	1.78	1.78	1.70	4
36.82	36.82	15.61	1.76	1.76	1.68	4
34.90	34.90	14.91	1.73	1.73	1.66	4
32.99	32.99	14.21	1.71	1.71	1.63	4
31.09	31.09	13.50	1.69	1.69	1.61	4
31.09	31.09	13.50	1.42	1.42	1.38	3
29.70	29.70	12.93	1.41	1.41	1.37	3
28.32	28.32	12.35	1.40	1.40	1.36	3
26.94	26.94	11.78	1.39	1.39	1.35	3
25.57	25.57	11.20	1.38	1.38	1.34	3
24.20	24.20	10.63	1.37	1.37	1.33	3
22.84	22.84	10.05	1.36	1.36	1.32	3

21.49	21.49	9.48	1.35	1.35	1.31	3
20.14	20.14	8.90	1.34	1.34	1.30	3
18.80	18.80	8.33	1.33	1.33	1.29	3
18.80	18.80	8.33	1.30	1.30	1.27	2
16.88	16.88	7.50	1.29	1.29	1.26	2
14.98	14.98	6.66	1.28	1.28	1.25	2
13.09	13.09	5.83	1.27	1.27	1.25	2
11.20	11.20	5.00	1.26	1.26	1.24	2
9.32	9.32	4.16	1.26	1.26	1.23	2
7.44	7.44	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.71	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.23	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	579.88	.00	579.88	312.00	267.88	6
60.02	619.83	4.62	615.20	347.33	267.88	6
59.45	659.71	9.24	650.47	382.59	267.88	6
58.89	699.52	13.86	685.66	417.78	267.88	6
58.33	739.27	18.48	720.79	452.91	267.88	6
57.76	778.96	23.10	755.85	487.98	267.88	6
57.20	818.58	27.72	790.85	522.98	267.88	6
56.64	858.13	32.34	825.79	557.91	267.88	6
56.09	897.62	36.96	860.65	592.77	267.88	6
56.09	897.62	36.96	860.65	592.77	267.88	5
54.84	1048.43	110.23	938.20	670.33	267.88	5
53.60	1199.01	183.50	1015.51	747.64	267.88	5
52.37	1349.34	256.76	1092.58	824.70	267.88	5
51.14	1499.43	330.03	1169.41	901.53	267.88	5
49.91	1649.29	403.29	1245.99	978.12	267.88	5
48.69	1798.90	476.56	1322.34	1054.46	267.88	5
48.69	1798.90	476.56	1322.34	1054.46	267.88	4
46.67	2002.53	554.43	1448.10	1180.22	267.88	4
44.67	2205.26	632.30	1572.95	1305.08	267.88	4
42.68	2407.03	710.18	1696.85	1428.97	267.88	4
40.71	2607.85	788.05	1819.80	1551.92	267.88	4
38.76	2807.71	865.92	1941.79	1673.91	267.88	4
36.82	3006.62	943.80	2062.82	1794.95	267.88	4
34.90	3204.57	1021.67	2182.90	1915.03	267.88	4
32.99	3401.55	1099.54	2302.01	2034.13	267.88	4
31.09	3597.54	1177.41	2420.12	2152.25	267.88	4
31.09	3597.54	1177.41	2420.12	2152.25	267.88	3
29.70	3747.40	1240.57	2506.84	2238.96	267.88	3

28.32	3896.90	1303.72	2593.18	2325.31	267.88	3
26.94	4046.04	1366.87	2679.17	2411.29	267.88	3
25.57	4194.82	1430.03	2764.80	2496.92	267.88	3
24.20	4343.24	1493.18	2850.06	2582.18	267.88	3
22.84	4491.29	1556.33	2934.96	2667.08	267.88	3
21.49	4638.98	1619.49	3019.49	2751.62	267.88	3
20.14	4786.31	1682.64	3103.67	2835.79	267.88	3
18.80	4933.27	1745.79	3187.48	2919.60	267.88	3
18.80	4933.27	1745.79	3187.48	2919.60	267.88	2
16.88	5139.86	1833.10	3306.76	3038.88	267.88	2
14.98	5345.92	1920.41	3425.51	3157.63	267.88	2
13.09	5551.41	2007.72	3543.68	3275.81	267.88	2
11.20	5756.47	2095.03	3661.44	3393.56	267.88	2
9.32	5961.18	2182.34	3778.84	3510.96	267.88	2
7.44	6165.52	2269.65	3895.87	3627.99	267.88	2
5.57	6369.50	2356.96	4012.54	3744.66	267.88	2
3.71	6573.12	2444.27	4128.85	3860.97	267.88	2
1.85	6776.37	2531.58	4244.79	3976.91	267.88	2
.00	6979.26	2618.89	4360.37	4092.49	267.88	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	5.00	2.53	.98	.98	.98	1
3.75	3.75	1.89	.98	.98	.92	1
2.50	2.50	1.26	.98	.98	.91	1
1.25	1.25	.63	.98	.98	.90	1
.00	.00	.00	.98	.98	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.00	.00	.00	.00	.00	.00	1
3.75	144.97	.00	144.97	78.00	66.97	1
2.50	289.94	.00	289.94	156.00	133.94	1
1.25	434.91	.00	434.91	234.00	200.91	1
.00	579.88	.00	579.88	312.00	267.88	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.50	24.38	6.50	5.99	5.69	6
60.02	59.97	24.30	6.49	6.15	5.68	6
59.45	59.42	24.22	6.47	6.27	5.66	6
58.89	58.87	24.15	6.46	6.35	5.65	6
58.33	58.32	24.07	6.44	6.39	5.64	6
57.76	57.76	24.00	6.43	6.40	5.62	6
57.20	57.20	23.92	6.42	6.40	5.61	6
56.64	56.64	23.85	6.40	6.39	5.59	6
56.09	56.08	23.77	6.39	6.37	5.58	6
56.09	56.08	23.77	.89	.89	.87	5
54.84	54.84	23.11	.88	.88	.86	5
53.60	53.60	22.45	.88	.87	.85	5
52.37	52.36	21.79	.87	.87	.85	5
51.14	51.13	21.13	.86	.86	.84	5
49.91	49.91	20.47	.86	.86	.84	5
48.69	48.68	19.81	.85	.85	.84	5
48.69	48.68	19.81	1.88	1.88	1.81	4
46.67	46.67	19.11	1.86	1.86	1.79	4

44.67	44.67	18.41	1.84	1.84	1.77	4
42.68	42.68	17.71	1.82	1.82	1.75	4
40.71	40.71	17.01	1.80	1.80	1.72	4
38.76	38.76	16.31	1.78	1.78	1.70	4
36.82	36.82	15.61	1.76	1.76	1.68	4
34.90	34.89	14.91	1.73	1.73	1.66	4
32.99	32.99	14.21	1.71	1.71	1.63	4
31.09	31.09	13.50	1.69	1.69	1.61	4
31.09	31.09	13.50	1.42	1.42	1.38	3
29.70	29.70	12.93	1.41	1.41	1.37	3
28.32	28.32	12.35	1.40	1.40	1.36	3
26.94	26.94	11.78	1.39	1.39	1.35	3
25.57	25.57	11.20	1.38	1.38	1.34	3
24.20	24.20	10.63	1.37	1.37	1.33	3
22.84	22.84	10.05	1.36	1.36	1.32	3
21.49	21.49	9.48	1.35	1.35	1.31	3
20.14	20.14	8.90	1.34	1.34	1.30	3
18.80	18.80	8.33	1.33	1.33	1.29	3
18.80	18.80	8.33	1.30	1.30	1.27	2
16.88	16.88	7.50	1.29	1.29	1.26	2
14.98	14.98	6.66	1.28	1.28	1.25	2
13.09	13.09	5.83	1.27	1.27	1.25	2
11.20	11.20	5.00	1.26	1.26	1.24	2
9.32	9.32	4.16	1.26	1.26	1.23	2
7.44	7.44	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.71	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.23	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.50	569.86	168.29	401.56	301.98	99.58	6
59.97	607.82	116.30	491.52	335.32	156.20	6
59.42	646.45	76.26	570.19	369.33	200.86	6
58.87	685.54	50.11	635.43	403.80	231.63	6
58.32	724.92	36.36	688.56	438.56	250.00	6
57.76	764.43	31.61	732.82	473.45	259.37	6
57.20	803.95	32.54	771.42	508.35	263.06	6
56.64	843.44	36.88	806.56	543.22	263.34	6
56.08	882.85	43.49	839.37	578.01	261.35	6
56.08	882.85	43.49	839.37	578.01	261.35	5
54.84	1033.65	117.45	916.20	655.54	260.65	5
53.60	1184.20	190.97	993.23	732.83	260.40	5
52.36	1334.51	264.15	1070.36	809.87	260.49	5

51.13	1484.58	337.11	1147.47	886.67	260.80	5
49.91	1634.41	409.99	1224.42	963.24	261.18	5
48.68	1784.00	483.00	1301.00	1039.56	261.44	5
48.68	1784.00	483.00	1301.00	1039.56	261.44	4
46.67	1987.58	557.97	1429.61	1165.27	264.34	4
44.67	2190.29	632.44	1557.85	1290.11	267.74	4
42.68	2392.06	710.18	1681.88	1414.01	267.88	4
40.71	2592.88	788.05	1804.83	1536.95	267.88	4
38.76	2792.74	865.92	1926.82	1658.94	267.88	4
36.82	2991.65	943.80	2047.85	1779.98	267.88	4
34.89	3189.60	1021.76	2167.85	1900.06	267.79	4
32.99	3386.58	1100.05	2286.53	2019.16	267.37	4
31.09	3582.55	1178.35	2404.20	2137.26	266.94	4
31.09	3582.55	1178.35	2404.20	2137.26	266.94	3
29.70	3732.41	1241.92	2490.49	2223.97	266.53	3
28.32	3881.91	1305.06	2576.85	2310.31	266.54	3
26.94	4031.04	1368.17	2662.87	2396.29	266.58	3
25.57	4179.81	1431.19	2748.62	2481.91	266.71	3
24.20	4328.22	1494.26	2833.96	2567.16	266.79	3
22.84	4476.27	1557.35	2918.91	2652.06	266.86	3
21.49	4623.95	1620.39	3003.56	2736.59	266.97	3
20.14	4771.27	1683.42	3087.86	2820.76	267.10	3
18.80	4918.23	1746.31	3171.92	2904.56	267.36	3
18.80	4918.23	1746.31	3171.92	2904.56	267.36	2
16.88	5124.82	1833.10	3291.72	3023.84	267.88	2
14.98	5330.88	1920.41	3410.47	3142.59	267.88	2
13.09	5536.37	2007.72	3528.65	3260.77	267.88	2
11.20	5741.43	2095.75	3645.68	3378.52	267.16	2
9.32	5946.14	2183.12	3763.02	3495.92	267.10	2
7.44	6150.48	2270.43	3880.05	3612.95	267.10	2
5.57	6354.45	2357.74	3996.71	3729.61	267.10	2
3.71	6558.07	2445.05	4113.02	3845.92	267.10	2
1.85	6761.32	2532.35	4228.97	3961.86	267.11	2
.00	6964.20	2620.88	4343.32	4077.43	265.89	2

Time = 30. Degree of Consolidation = 6.%

Total Settlement = .081

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 30. = .081

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.84	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.41	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.84	.00	.00	.00	.00	.00	1
3.61	143.46	54.95	88.51	76.49	12.02	1
2.41	285.80	110.73	175.08	151.86	23.21	1
1.20	427.88	150.99	276.89	226.97	49.92	1
.00	569.86	168.29	401.56	301.98	99.58	1

Time = 30. Degree of Consolidation = 95.%

Total Settlement = .161

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 30. = .161

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 3.36

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.45	24.38	6.50	5.94	5.69	6

60.02	59.93	24.30	6.49	6.06	5.68	6
59.45	59.39	24.22	6.47	6.16	5.66	6
58.89	58.84	24.15	6.46	6.24	5.65	6
58.33	58.29	24.07	6.44	6.30	5.64	6
57.76	57.74	24.00	6.43	6.34	5.62	6
57.20	57.19	23.92	6.42	6.35	5.61	6
56.64	56.63	23.85	6.40	6.35	5.59	6
56.09	56.08	23.77	6.39	6.34	5.58	6
56.09	56.08	23.77	.89	.89	.87	5
54.84	54.83	23.11	.88	.88	.86	5
53.60	53.60	22.45	.88	.87	.85	5
52.37	52.36	21.79	.87	.87	.85	5
51.14	51.13	21.13	.86	.86	.84	5
49.91	49.90	20.47	.86	.86	.84	5
48.69	48.68	19.81	.85	.85	.84	5
48.69	48.68	19.81	1.88	1.88	1.81	4
46.67	46.67	19.11	1.86	1.86	1.79	4
44.67	44.67	18.41	1.84	1.84	1.77	4
42.68	42.68	17.71	1.82	1.82	1.75	4
40.71	40.71	17.01	1.80	1.80	1.72	4
38.76	38.76	16.31	1.78	1.78	1.70	4
36.82	36.82	15.61	1.76	1.76	1.68	4
34.90	34.89	14.91	1.73	1.73	1.66	4
32.99	32.98	14.21	1.71	1.71	1.63	4
31.09	31.09	13.50	1.69	1.69	1.61	4
31.09	31.09	13.50	1.42	1.42	1.38	3
29.70	29.70	12.93	1.41	1.41	1.37	3
28.32	28.32	12.35	1.40	1.40	1.36	3
26.94	26.94	11.78	1.39	1.39	1.35	3
25.57	25.57	11.20	1.38	1.38	1.34	3
24.20	24.20	10.63	1.37	1.37	1.33	3
22.84	22.84	10.05	1.36	1.36	1.32	3
21.49	21.49	9.48	1.35	1.35	1.31	3
20.14	20.14	8.90	1.34	1.34	1.30	3
18.80	18.80	8.33	1.33	1.33	1.29	3
18.80	18.80	8.33	1.30	1.30	1.27	2
16.88	16.88	7.50	1.29	1.29	1.26	2
14.98	14.98	6.66	1.28	1.28	1.25	2
13.09	13.09	5.83	1.27	1.27	1.25	2
11.20	11.20	5.00	1.26	1.26	1.24	2
9.32	9.32	4.16	1.26	1.26	1.23	2
7.44	7.44	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.71	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.23	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.45	569.70	186.80	382.89	301.82	81.08	6
59.93	607.31	146.86	460.45	334.81	125.64	6
59.39	645.45	112.40	533.05	368.33	164.72	6
58.84	684.03	85.09	598.94	402.29	196.65	6
58.29	722.95	65.64	657.31	436.59	220.72	6
57.74	762.09	53.75	708.34	471.11	237.23	6
57.19	801.35	48.44	752.91	505.75	247.16	6
56.63	840.64	48.51	792.13	540.42	251.71	6
56.08	879.91	52.84	827.07	575.06	252.00	6
56.08	879.91	52.84	827.07	575.06	252.00	5
54.83	1030.67	126.03	904.64	652.56	252.07	5
53.60	1181.19	198.89	982.31	729.82	252.49	5
52.36	1331.48	271.48	1059.99	806.84	253.15	5
51.13	1481.53	343.95	1137.57	883.62	253.95	5
49.90	1631.33	416.44	1214.89	960.16	254.73	5
48.68	1780.90	489.14	1291.76	1036.46	255.29	5
48.68	1780.90	489.14	1291.76	1036.46	255.29	4
46.67	1984.44	560.54	1423.91	1162.14	261.77	4
44.67	2187.13	633.32	1553.81	1286.95	266.86	4
42.68	2388.90	710.18	1678.72	1410.85	267.88	4
40.71	2589.72	788.05	1801.67	1533.79	267.88	4
38.76	2789.58	865.92	1923.66	1655.78	267.88	4
36.82	2988.49	943.80	2044.70	1776.82	267.88	4
34.89	3186.44	1021.90	2164.55	1896.90	267.65	4
32.98	3383.41	1100.55	2282.87	2015.99	266.87	4
31.09	3579.38	1179.20	2400.18	2134.09	266.09	4
31.09	3579.38	1179.20	2400.18	2134.09	266.09	3
29.70	3729.24	1243.08	2486.15	2220.79	265.36	3
28.32	3878.72	1306.35	2572.37	2307.12	265.25	3
26.94	4027.85	1369.40	2658.45	2393.10	265.36	3
25.57	4176.61	1432.35	2744.26	2478.71	265.55	3
24.20	4325.01	1495.33	2829.68	2563.96	265.72	3
22.84	4473.05	1558.34	2914.72	2648.84	265.87	3
21.49	4620.73	1621.30	2999.44	2733.37	266.07	3
20.14	4768.05	1684.16	3083.89	2817.53	266.35	3
18.80	4915.01	1746.85	3168.16	2901.34	266.82	3
18.80	4915.01	1746.85	3168.16	2901.34	266.82	2
16.88	5121.60	1833.19	3288.40	3020.62	267.79	2
14.98	5327.65	1920.41	3407.24	3139.36	267.88	2
13.09	5533.14	2007.72	3525.42	3257.54	267.88	2
11.20	5738.21	2096.27	3641.94	3375.30	266.64	2
9.32	5942.91	2183.89	3759.01	3492.69	266.33	2
7.44	6147.24	2271.20	3876.04	3609.71	266.33	2

5.57	6351.22	2358.51	3992.70	3726.38	266.33	2
3.71	6554.83	2445.82	4109.00	3842.68	266.33	2
1.85	6758.07	2533.30	4224.77	3958.61	266.16	2
.00	6960.95	2622.50	4338.45	4074.18	264.27	2

Time = 60. Degree of Consolidation = 9.%

Total Settlement = .130

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 60. = .130

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.84	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.84	.00	.00	.00	.00	.00	1
3.61	143.44	58.21	85.24	76.48	8.76	1
2.40	285.76	120.57	165.19	151.82	13.37	1
1.20	427.79	165.20	262.58	226.88	35.71	1
.00	569.70	186.80	382.89	301.82	81.08	1

Time = 60. Degree of Consolidation = 96.%

Total Settlement = .163

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 60. = .163

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 3.31

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.38	24.38	6.50	5.88	5.69	6
60.02	59.85	24.30	6.49	5.97	5.68	6
59.45	59.32	24.22	6.47	6.05	5.66	6
58.89	58.79	24.15	6.46	6.12	5.65	6
58.33	58.25	24.07	6.44	6.17	5.64	6
57.76	57.71	24.00	6.43	6.22	5.62	6
57.20	57.16	23.92	6.42	6.24	5.61	6
56.64	56.61	23.85	6.40	6.26	5.59	6
56.09	56.06	23.77	6.39	6.26	5.58	6
56.09	56.06	23.77	.89	.88	.87	5
54.84	54.82	23.11	.88	.88	.86	5
53.60	53.59	22.45	.88	.87	.85	5
52.37	52.35	21.79	.87	.87	.85	5
51.14	51.12	21.13	.86	.86	.84	5
49.91	49.90	20.47	.86	.86	.84	5
48.69	48.68	19.81	.85	.85	.84	5
48.69	48.68	19.81	1.88	1.88	1.81	4
46.67	46.66	19.11	1.86	1.86	1.79	4
44.67	44.66	18.41	1.84	1.84	1.77	4
42.68	42.68	17.71	1.82	1.82	1.75	4
40.71	40.71	17.01	1.80	1.80	1.72	4
38.76	38.75	16.31	1.78	1.78	1.70	4
36.82	36.81	15.61	1.76	1.76	1.68	4
34.90	34.89	14.91	1.73	1.73	1.66	4
32.99	32.98	14.21	1.71	1.71	1.63	4
31.09	31.09	13.50	1.69	1.69	1.61	4
31.09	31.09	13.50	1.42	1.42	1.38	3
29.70	29.70	12.93	1.41	1.41	1.37	3
28.32	28.32	12.35	1.40	1.40	1.36	3
26.94	26.94	11.78	1.39	1.39	1.35	3
25.57	25.57	11.20	1.38	1.38	1.34	3

24.20	24.20	10.63	1.37	1.37	1.33	3
22.84	22.84	10.05	1.36	1.36	1.32	3
21.49	21.49	9.48	1.35	1.35	1.31	3
20.14	20.14	8.90	1.34	1.34	1.30	3
18.80	18.79	8.33	1.33	1.33	1.29	3
18.80	18.79	8.33	1.30	1.30	1.27	2
16.88	16.88	7.50	1.29	1.29	1.26	2
14.98	14.98	6.66	1.28	1.28	1.25	2
13.09	13.09	5.83	1.27	1.27	1.25	2
11.20	11.20	5.00	1.26	1.26	1.24	2
9.32	9.32	4.16	1.26	1.26	1.23	2
7.44	7.44	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.71	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.23	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.38	569.57	204.36	365.21	301.69	63.52	6
59.85	606.85	175.62	431.23	334.35	96.88	6
59.32	644.52	149.35	495.17	367.40	127.77	6
58.79	682.54	126.51	556.03	400.80	155.23	6
58.25	720.85	107.87	612.99	434.49	178.49	6
57.71	759.40	93.89	665.52	468.42	197.09	6
57.16	798.12	84.72	713.40	502.52	210.88	6
56.61	836.93	80.22	756.71	536.71	220.00	6
56.06	875.77	79.93	795.84	570.93	224.91	6
56.06	875.77	79.93	795.84	570.93	224.91	5
54.82	1026.45	151.48	874.97	648.35	226.62	5
53.59	1176.90	222.65	954.25	725.52	228.73	5
52.35	1327.10	293.50	1033.61	802.47	231.14	5
51.12	1477.08	364.13	1112.95	879.18	233.77	5
49.90	1626.82	434.66	1192.16	955.65	236.51	5
48.68	1776.34	506.52	1269.81	1031.90	237.91	5
48.68	1776.34	506.52	1269.81	1031.90	237.91	4
46.66	1979.76	567.43	1412.33	1157.45	254.88	4
44.66	2182.39	636.23	1546.16	1282.21	263.96	4
42.68	2384.14	710.29	1673.86	1406.09	267.77	4
40.71	2584.96	788.05	1796.91	1529.03	267.88	4
38.75	2784.82	865.92	1918.90	1651.02	267.88	4
36.81	2983.73	943.80	2039.94	1772.06	267.88	4
34.89	3181.68	1022.32	2159.36	1892.14	267.22	4
32.98	3378.64	1101.54	2277.10	2011.23	265.87	4
31.09	3574.60	1180.76	2393.84	2129.31	264.53	4

31.09	3574.60	1180.76	2393.84	2129.31	264.53	3
29.70	3724.44	1245.17	2479.27	2215.99	263.27	3
28.32	3873.91	1308.70	2565.22	2302.32	262.90	3
26.94	4023.03	1371.73	2651.29	2388.27	263.02	3
25.57	4171.78	1434.64	2737.13	2473.87	263.26	3
24.20	4320.17	1497.41	2822.76	2559.11	263.65	3
22.84	4468.19	1560.16	2908.03	2643.98	264.05	3
21.49	4615.86	1622.87	2992.99	2728.50	264.49	3
20.14	4763.17	1685.47	3077.70	2812.66	265.05	3
18.79	4910.12	1747.85	3162.27	2896.45	265.82	3
18.79	4910.12	1747.85	3162.27	2896.45	265.82	2
16.88	5116.71	1833.54	3283.17	3015.73	267.44	2
14.98	5322.76	1920.41	3402.35	3134.47	267.88	2
13.09	5528.25	2007.72	3520.53	3252.65	267.88	2
11.20	5733.32	2097.30	3636.01	3370.41	265.61	2
9.32	5938.01	2185.27	3752.74	3487.79	264.95	2
7.44	6142.34	2272.75	3869.59	3604.81	264.78	2
5.57	6346.31	2360.06	3986.24	3721.47	264.78	2
3.71	6549.91	2447.37	4102.54	3837.76	264.78	2
1.85	6753.15	2535.37	4217.78	3953.69	264.09	2
.00	6956.02	2625.21	4330.81	4069.25	261.56	2

Time = 120. Degree of Consolidation = 14.%

Total Settlement = .207

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 120. = .207

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.43	60.70	82.73	76.46	6.27	1
2.40	285.72	128.24	157.48	151.78	5.70	1
1.20	427.71	176.71	251.00	226.80	24.20	1
.00	569.57	204.36	365.21	301.69	63.52	1

Time = 120. Degree of Consolidation = 98.%

Total Settlement = .165

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 120. = .165

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.23

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.29	24.38	6.50	5.85	5.69	6
60.02	59.77	24.30	6.49	5.90	5.68	6
59.45	59.25	24.22	6.47	5.95	5.66	6
58.89	58.72	24.15	6.46	6.00	5.65	6
58.33	58.19	24.07	6.44	6.04	5.64	6
57.76	57.66	24.00	6.43	6.08	5.62	6
57.20	57.12	23.92	6.42	6.11	5.61	6
56.64	56.58	23.85	6.40	6.14	5.59	6
56.09	56.04	23.77	6.39	6.16	5.58	6
56.09	56.04	23.77	.89	.88	.87	5
54.84	54.80	23.11	.88	.88	.86	5
53.60	53.57	22.45	.88	.87	.85	5

52.37	52.34	21.79	.87	.86	.85	5
51.14	51.11	21.13	.86	.86	.84	5
49.91	49.88	20.47	.86	.85	.84	5
48.69	48.66	19.81	.85	.85	.84	5
48.69	48.66	19.81	1.88	1.87	1.81	4
46.67	46.65	19.11	1.86	1.86	1.79	4
44.67	44.66	18.41	1.84	1.84	1.77	4
42.68	42.67	17.71	1.82	1.82	1.75	4
40.71	40.70	17.01	1.80	1.80	1.72	4
38.76	38.75	16.31	1.78	1.78	1.70	4
36.82	36.81	15.61	1.76	1.76	1.68	4
34.90	34.88	14.91	1.73	1.73	1.66	4
32.99	32.98	14.21	1.71	1.71	1.63	4
31.09	31.08	13.50	1.69	1.69	1.61	4
31.09	31.08	13.50	1.42	1.42	1.38	3
29.70	29.70	12.93	1.41	1.41	1.37	3
28.32	28.31	12.35	1.40	1.40	1.36	3
26.94	26.94	11.78	1.39	1.39	1.35	3
25.57	25.56	11.20	1.38	1.38	1.34	3
24.20	24.20	10.63	1.37	1.37	1.33	3
22.84	22.84	10.05	1.36	1.36	1.32	3
21.49	21.48	9.48	1.35	1.35	1.31	3
20.14	20.14	8.90	1.34	1.34	1.30	3
18.80	18.79	8.33	1.33	1.33	1.29	3
18.80	18.79	8.33	1.30	1.30	1.27	2
16.88	16.88	7.50	1.29	1.29	1.26	2
14.98	14.98	6.66	1.28	1.28	1.25	2
13.09	13.09	5.83	1.27	1.27	1.25	2
11.20	11.20	5.00	1.26	1.26	1.24	2
9.32	9.32	4.16	1.26	1.25	1.23	2
7.44	7.44	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.71	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.23	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.29	569.30	214.38	354.92	301.42	53.50	6
59.77	606.35	197.66	408.69	333.85	74.84	6
59.25	643.63	181.38	462.25	366.51	95.74	6
58.72	681.14	166.03	515.10	399.40	115.70	6
58.19	718.86	152.06	566.80	432.50	134.30	6
57.66	756.76	139.77	616.99	465.78	151.21	6
57.12	794.83	129.35	665.47	499.23	166.25	6

56.58	833.03	120.84	712.19	532.81	179.38	6
56.04	871.34	114.12	757.22	566.50	190.72	6
56.04	871.34	114.12	757.22	566.50	190.72	5
54.80	1021.91	183.24	838.67	643.80	194.87	5
53.57	1172.25	251.70	920.55	720.88	199.67	5
52.34	1322.37	319.57	1002.80	797.73	205.07	5
51.11	1472.26	386.90	1085.37	874.36	211.01	5
49.88	1621.94	453.76	1168.18	950.77	217.41	5
48.66	1771.40	525.35	1246.04	1026.96	219.08	5
48.66	1771.40	525.35	1246.04	1026.96	219.08	4
46.65	1974.61	582.62	1391.99	1152.30	239.69	4
44.66	2177.09	645.67	1531.41	1276.91	254.51	4
42.67	2378.76	714.39	1664.37	1400.70	263.67	4
40.70	2579.56	788.07	1791.48	1523.63	267.85	4
38.75	2779.42	865.92	1913.50	1645.62	267.88	4
36.81	2978.33	943.80	2034.54	1766.66	267.88	4
34.88	3176.28	1023.18	2153.10	1886.73	266.37	4
32.98	3373.22	1103.45	2269.77	2005.80	263.97	4
31.08	3569.14	1183.48	2385.66	2123.85	261.81	4
31.08	3569.14	1183.48	2385.66	2123.85	261.81	3
29.70	3718.97	1248.66	2470.31	2210.52	259.78	3
28.31	3868.42	1312.68	2555.74	2296.82	258.92	3
26.94	4017.51	1375.99	2641.52	2382.76	258.76	3
25.56	4166.23	1438.83	2727.40	2468.33	259.07	3
24.20	4314.60	1501.40	2813.20	2553.54	259.66	3
22.84	4462.61	1563.78	2898.83	2638.40	260.43	3
21.48	4610.26	1625.97	2984.29	2722.89	261.40	3
20.14	4757.55	1688.05	3069.50	2807.03	262.47	3
18.79	4904.49	1749.86	3154.62	2890.82	263.80	3
18.79	4904.49	1749.87	3154.62	2890.82	263.80	2
16.88	5111.06	1834.36	3276.71	3010.08	266.62	2
14.98	5317.12	1920.41	3396.70	3128.83	267.88	2
13.09	5522.61	2007.72	3514.88	3247.01	267.88	2
11.20	5727.67	2098.74	3628.93	3364.76	264.18	2
9.32	5932.35	2187.53	3744.83	3482.13	262.69	2
7.44	6136.67	2275.48	3861.19	3599.14	262.05	2
5.57	6340.63	2363.08	3977.55	3715.79	261.76	2
3.71	6544.22	2450.47	4093.75	3832.07	261.68	2
1.85	6747.44	2539.25	4208.19	3947.98	260.21	2
.00	6950.30	2629.51	4320.78	4063.53	257.26	2

Time = 240. Degree of Consolidation = 20.%

Total Settlement = .295

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 240. = .295

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 240. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 240. = .169

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.14

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.24	24.38	6.50	5.80	5.69	6
60.02	59.72	24.30	6.49	5.85	5.68	6
59.45	59.21	24.22	6.47	5.89	5.66	6
58.89	58.68	24.15	6.46	5.94	5.65	6
58.33	58.16	24.07	6.44	5.98	5.64	6
57.76	57.63	24.00	6.43	6.01	5.62	6
57.20	57.10	23.92	6.42	6.05	5.61	6
56.64	56.56	23.85	6.40	6.08	5.59	6
56.09	56.03	23.77	6.39	6.11	5.58	6
56.09	56.03	23.77	.89	.88	.87	5
54.84	54.79	23.11	.88	.87	.86	5
53.60	53.56	22.45	.88	.87	.85	5
52.37	52.32	21.79	.87	.86	.85	5
51.14	51.10	21.13	.86	.86	.84	5
49.91	49.87	20.47	.86	.85	.84	5
48.69	48.65	19.81	.85	.85	.84	5
48.69	48.65	19.81	1.88	1.87	1.81	4
46.67	46.65	19.11	1.86	1.85	1.79	4
44.67	44.65	18.41	1.84	1.84	1.77	4
42.68	42.67	17.71	1.82	1.82	1.75	4
40.71	40.70	17.01	1.80	1.80	1.72	4
38.76	38.74	16.31	1.78	1.78	1.70	4
36.82	36.80	15.61	1.76	1.76	1.68	4
34.90	34.88	14.91	1.73	1.73	1.66	4
32.99	32.97	14.21	1.71	1.71	1.63	4
31.09	31.08	13.50	1.69	1.69	1.61	4
31.09	31.08	13.50	1.42	1.42	1.38	3
29.70	29.69	12.93	1.41	1.41	1.37	3
28.32	28.31	12.35	1.40	1.40	1.36	3
26.94	26.93	11.78	1.39	1.39	1.35	3
25.57	25.56	11.20	1.38	1.38	1.34	3
24.20	24.20	10.63	1.37	1.37	1.33	3
22.84	22.84	10.05	1.36	1.36	1.32	3
21.49	21.48	9.48	1.35	1.35	1.31	3
20.14	20.13	8.90	1.34	1.34	1.30	3
18.80	18.79	8.33	1.33	1.33	1.29	3
18.80	18.79	8.33	1.30	1.30	1.27	2
16.88	16.88	7.50	1.29	1.29	1.26	2
14.98	14.98	6.66	1.28	1.28	1.25	2
13.09	13.08	5.83	1.27	1.27	1.25	2

11.20	11.20	5.00	1.26	1.26	1.24	2
9.32	9.32	4.16	1.26	1.25	1.23	2
7.44	7.44	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.71	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.23	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.24	569.30	230.27	339.02	301.42	37.60	6
59.72	606.11	215.09	391.02	333.61	57.41	6
59.21	643.13	200.40	442.73	366.01	76.72	6
58.68	680.36	186.40	493.96	398.62	95.34	6
58.16	717.78	173.22	544.56	431.42	113.14	6
57.63	755.38	160.96	594.42	464.40	130.02	6
57.10	793.15	149.66	643.49	497.55	145.94	6
56.56	831.08	139.31	691.76	530.85	160.91	6
56.03	869.14	129.84	739.30	564.30	175.00	6
56.03	869.14	129.84	739.30	564.30	175.00	5
54.79	1019.66	197.87	821.79	641.55	180.24	5
53.56	1169.96	265.13	904.83	718.58	186.24	5
52.32	1320.03	331.67	988.37	795.39	192.97	5
51.10	1469.89	397.53	1072.37	871.99	200.38	5
49.87	1619.53	462.76	1156.77	948.36	208.41	5
48.65	1768.96	534.41	1234.55	1024.53	210.02	5
48.65	1768.96	534.41	1234.55	1024.53	210.02	4
46.65	1972.06	592.32	1379.74	1149.75	229.99	4
44.65	2174.43	653.86	1520.57	1274.25	246.33	4
42.67	2376.01	719.71	1656.30	1397.96	258.34	4
40.70	2576.77	790.29	1786.48	1520.84	265.64	4
38.74	2776.62	865.92	1910.70	1642.82	267.88	4
36.80	2975.53	943.80	2031.74	1763.86	267.88	4
34.88	3173.47	1024.03	2149.44	1883.93	265.51	4
32.97	3370.40	1105.16	2265.24	2002.98	262.26	4
31.08	3566.30	1185.88	2380.41	2121.00	259.41	4
31.08	3566.30	1185.88	2380.41	2121.00	259.41	3
29.69	3716.10	1251.71	2464.40	2207.66	256.74	3
28.31	3865.54	1316.17	2549.36	2293.94	255.42	3
26.93	4014.61	1379.70	2634.91	2379.85	255.05	3
25.56	4163.31	1442.57	2720.74	2465.41	255.34	3
24.20	4311.65	1505.07	2806.58	2550.60	255.98	3
22.84	4459.64	1567.19	2892.45	2635.43	257.02	3
21.48	4607.27	1629.07	2978.21	2719.91	258.30	3
20.13	4754.55	1690.63	3063.92	2804.03	259.88	3

18.79	4901.47	1751.97	3149.50	2887.80	261.70	3
18.79	4901.47	1751.97	3149.50	2887.80	261.70	2
16.88	5108.04	1835.44	3272.60	3007.06	265.54	2
14.98	5314.09	1920.41	3393.68	3125.80	267.88	2
13.08	5519.58	2007.72	3511.86	3243.98	267.88	2
11.20	5724.64	2099.79	3624.84	3361.73	263.12	2
9.32	5929.32	2189.59	3739.72	3479.10	260.63	2
7.44	6133.63	2277.93	3855.70	3596.10	259.60	2
5.57	6337.57	2365.90	3971.67	3712.73	258.94	2
3.71	6541.15	2453.65	4087.50	3829.00	258.51	2
1.85	6744.36	2542.59	4201.77	3944.90	256.87	2
.00	6947.20	2633.01	4314.19	4060.43	253.76	2

Time = 360. Degree of Consolidation = 24.%

Total Settlement = .344

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 360. = .344

Settlement caused by Secondary Compression at time 360. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1

.00 569.30 267.88 301.42 301.42 .00 1

Time = 360. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 360. = .169

Settlement caused by Secondary Compression at time 360. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.09

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.21	24.38	6.50	5.79	5.69	6
60.02	59.69	24.30	6.49	5.83	5.68	6
59.45	59.17	24.22	6.47	5.87	5.66	6
58.89	58.65	24.15	6.46	5.90	5.65	6
58.33	58.13	24.07	6.44	5.94	5.64	6
57.76	57.61	24.00	6.43	5.98	5.62	6
57.20	57.08	23.92	6.42	6.01	5.61	6
56.64	56.55	23.85	6.40	6.04	5.59	6
56.09	56.01	23.77	6.39	6.08	5.58	6
56.09	56.01	23.77	.89	.88	.87	5
54.84	54.78	23.11	.88	.87	.86	5
53.60	53.54	22.45	.88	.87	.85	5
52.37	52.31	21.79	.87	.86	.85	5
51.14	51.08	21.13	.86	.86	.84	5
49.91	49.86	20.47	.86	.85	.84	5
48.69	48.64	19.81	.85	.85	.84	5
48.69	48.64	19.81	1.88	1.87	1.81	4
46.67	46.63	19.11	1.86	1.85	1.79	4
44.67	44.64	18.41	1.84	1.83	1.77	4
42.68	42.66	17.71	1.82	1.82	1.75	4
40.71	40.69	17.01	1.80	1.80	1.72	4

38.76	38.74	16.31	1.78	1.78	1.70	4
36.82	36.80	15.61	1.76	1.76	1.68	4
34.90	34.87	14.91	1.73	1.73	1.66	4
32.99	32.97	14.21	1.71	1.71	1.63	4
31.09	31.08	13.50	1.69	1.69	1.61	4
31.09	31.08	13.50	1.42	1.42	1.38	3
29.70	29.69	12.93	1.41	1.41	1.37	3
28.32	28.30	12.35	1.40	1.40	1.36	3
26.94	26.93	11.78	1.39	1.39	1.35	3
25.57	25.56	11.20	1.38	1.38	1.34	3
24.20	24.19	10.63	1.37	1.37	1.33	3
22.84	22.83	10.05	1.36	1.36	1.32	3
21.49	21.48	9.48	1.35	1.35	1.31	3
20.14	20.13	8.90	1.34	1.34	1.30	3
18.80	18.79	8.33	1.33	1.33	1.29	3
18.80	18.79	8.33	1.30	1.30	1.27	2
16.88	16.88	7.50	1.29	1.29	1.26	2
14.98	14.98	6.66	1.28	1.28	1.25	2
13.09	13.08	5.83	1.27	1.27	1.25	2
11.20	11.20	5.00	1.26	1.26	1.24	2
9.32	9.31	4.16	1.26	1.25	1.23	2
7.44	7.44	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.71	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.23	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.21	569.30	234.68	334.62	301.42	33.20	6
59.69	606.02	222.12	383.90	333.53	50.38	6
59.17	642.93	209.69	433.24	365.81	67.43	6
58.65	680.01	197.43	482.59	398.27	84.31	6
58.13	717.27	185.38	531.89	430.91	100.98	6
57.61	754.69	173.59	581.11	463.71	117.39	6
57.08	792.28	162.05	630.23	496.68	133.55	6
56.55	830.04	150.78	679.26	529.82	149.44	6
56.01	867.95	139.75	728.20	563.11	165.09	6
56.01	867.95	139.75	728.20	563.11	165.09	5
54.78	1018.44	207.13	811.30	640.33	170.97	5
53.54	1168.70	273.68	895.03	717.33	177.70	5
52.31	1318.75	339.42	979.34	794.12	185.22	5
51.08	1468.59	404.39	1064.20	870.68	193.51	5
49.86	1618.21	468.65	1149.56	947.04	202.52	5
48.64	1767.62	540.45	1227.17	1023.19	203.99	5

48.64	1767.62	540.45	1227.17	1023.19	203.99	4
46.63	1970.63	600.15	1370.49	1148.32	222.16	4
44.64	2172.90	661.75	1511.15	1272.72	238.44	4
42.66	2374.40	726.12	1648.28	1396.34	251.94	4
40.69	2575.08	794.02	1781.07	1519.16	261.91	4
38.74	2774.92	866.19	1908.73	1641.12	267.61	4
36.80	2973.83	943.80	2030.03	1762.16	267.88	4
34.87	3171.76	1025.16	2146.60	1882.22	264.39	4
32.97	3368.67	1107.33	2261.34	2001.25	260.09	4
31.08	3564.53	1188.94	2375.59	2119.24	256.35	4
31.08	3564.53	1188.94	2375.59	2119.24	256.35	3
29.69	3714.32	1255.59	2458.73	2205.88	252.86	3
28.30	3863.73	1320.66	2543.07	2292.13	250.94	3
26.93	4012.77	1384.55	2628.22	2378.02	250.20	3
25.56	4161.45	1447.52	2713.93	2463.54	250.39	3
24.19	4309.76	1509.90	2799.87	2548.71	251.16	3
22.83	4457.72	1571.79	2885.93	2633.51	252.42	3
21.48	4605.33	1633.21	2972.12	2717.97	254.15	3
20.13	4752.58	1694.31	3058.27	2802.07	256.20	3
18.79	4899.49	1755.03	3144.46	2885.82	258.64	3
18.79	4899.49	1755.03	3144.46	2885.82	258.64	2
16.88	5106.04	1837.18	3268.86	3005.06	263.80	2
14.98	5312.08	1920.77	3391.31	3123.79	267.52	2
13.08	5517.57	2007.72	3509.85	3241.97	267.88	2
11.20	5722.63	2101.36	3621.26	3359.72	261.55	2
9.31	5927.30	2192.42	3734.88	3477.08	257.80	2
7.44	6131.60	2281.38	3850.21	3594.06	256.15	2
5.57	6335.52	2369.96	3965.57	3710.68	254.88	2
3.71	6539.08	2458.29	4080.79	3826.93	253.86	2
1.85	6742.28	2547.24	4195.04	3942.82	252.22	2
.00	6945.10	2637.66	4307.44	4058.33	249.11	2

Time = 540. Degree of Consolidation = 26.%

Total Settlement = .378

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 540. = .378

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 540. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 540. = .169

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.05

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.19	24.38	6.50	5.79	5.69	6
60.02	59.68	24.30	6.49	5.82	5.68	6

59.45	59.16	24.22	6.47	5.86	5.66	6
58.89	58.64	24.15	6.46	5.89	5.65	6
58.33	58.12	24.07	6.44	5.93	5.64	6
57.76	57.59	24.00	6.43	5.96	5.62	6
57.20	57.07	23.92	6.42	6.00	5.61	6
56.64	56.54	23.85	6.40	6.03	5.59	6
56.09	56.00	23.77	6.39	6.07	5.58	6
56.09	56.00	23.77	.89	.88	.87	5
54.84	54.77	23.11	.88	.87	.86	5
53.60	53.53	22.45	.88	.87	.85	5
52.37	52.30	21.79	.87	.86	.85	5
51.14	51.07	21.13	.86	.86	.84	5
49.91	49.85	20.47	.86	.85	.84	5
48.69	48.63	19.81	.85	.85	.84	5
48.69	48.63	19.81	1.88	1.87	1.81	4
46.67	46.63	19.11	1.86	1.85	1.79	4
44.67	44.63	18.41	1.84	1.83	1.77	4
42.68	42.65	17.71	1.82	1.82	1.75	4
40.71	40.69	17.01	1.80	1.80	1.72	4
38.76	38.73	16.31	1.78	1.78	1.70	4
36.82	36.79	15.61	1.76	1.76	1.68	4
34.90	34.87	14.91	1.73	1.73	1.66	4
32.99	32.96	14.21	1.71	1.71	1.63	4
31.09	31.07	13.50	1.69	1.68	1.61	4
31.09	31.07	13.50	1.42	1.42	1.38	3
29.70	29.68	12.93	1.41	1.41	1.37	3
28.32	28.30	12.35	1.40	1.40	1.36	3
26.94	26.92	11.78	1.39	1.39	1.35	3
25.57	25.55	11.20	1.38	1.38	1.34	3
24.20	24.19	10.63	1.37	1.37	1.33	3
22.84	22.83	10.05	1.36	1.36	1.32	3
21.49	21.48	9.48	1.35	1.35	1.31	3
20.14	20.13	8.90	1.34	1.34	1.30	3
18.80	18.79	8.33	1.33	1.33	1.29	3
18.80	18.79	8.33	1.30	1.30	1.27	2
16.88	16.88	7.50	1.29	1.29	1.26	2
14.98	14.97	6.66	1.28	1.28	1.25	2
13.09	13.08	5.83	1.27	1.27	1.25	2
11.20	11.19	5.00	1.26	1.26	1.24	2
9.32	9.31	4.16	1.26	1.25	1.23	2
7.44	7.44	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.71	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.23	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.19	569.29	235.80	333.49	301.42	32.08	6
59.68	606.00	224.06	381.94	333.50	48.43	6
59.16	642.87	212.34	430.54	365.76	64.78	6
58.64	679.91	200.64	479.28	398.18	81.10	6
58.12	717.12	188.98	528.14	430.76	97.38	6
57.59	754.49	177.37	577.12	463.51	113.61	6
57.07	792.03	165.82	626.22	496.43	129.79	6
56.54	829.73	154.31	675.42	529.51	145.91	6
56.00	867.60	142.86	724.74	562.76	161.98	6
56.00	867.60	142.86	724.74	562.76	161.98	5
54.77	1018.07	210.06	808.01	639.97	168.04	5
53.53	1168.33	276.41	891.93	716.96	174.97	5
52.30	1318.37	341.92	976.45	793.73	182.72	5
51.07	1468.20	406.64	1061.56	870.30	191.26	5
49.85	1617.81	470.61	1147.20	946.64	200.56	5
48.63	1767.22	542.52	1224.70	1022.79	201.91	5
48.63	1767.22	542.52	1224.70	1022.79	201.91	4
46.63	1970.20	603.59	1366.61	1147.89	218.72	4
44.63	2172.42	665.84	1506.58	1272.24	234.34	4
42.65	2373.86	730.01	1643.85	1395.81	248.04	4
40.69	2574.51	797.00	1777.51	1518.58	258.92	4
38.73	2774.31	867.89	1906.43	1640.51	265.91	4
36.79	2973.22	944.25	2028.96	1761.54	267.42	4
34.87	3171.14	1026.22	2144.92	1881.59	263.32	4
32.96	3368.03	1109.19	2258.84	2000.61	258.23	4
31.07	3563.86	1191.51	2372.35	2118.57	253.78	4
31.07	3563.86	1191.51	2372.35	2118.57	253.78	3
29.68	3713.63	1258.80	2454.83	2205.19	249.64	3
28.30	3863.02	1324.44	2538.58	2291.43	247.15	3
26.92	4012.04	1388.68	2623.36	2377.29	246.07	3
25.55	4160.69	1451.83	2708.87	2462.79	246.08	3
24.19	4308.98	1514.16	2794.83	2547.93	246.90	3
22.83	4456.92	1575.86	2881.07	2632.71	248.36	3
21.48	4604.50	1637.04	2967.46	2717.14	250.32	3
20.13	4751.74	1697.70	3054.04	2801.22	252.82	3
18.79	4898.62	1757.98	3140.65	2884.95	255.69	3
18.79	4898.62	1757.98	3140.65	2884.95	255.69	2
16.88	5105.16	1839.19	3265.96	3004.18	261.79	2
14.97	5311.19	1921.81	3389.38	3122.90	266.48	2
13.08	5516.68	2007.72	3508.96	3241.08	267.88	2
11.19	5721.73	2102.91	3618.82	3358.82	260.00	2
9.31	5926.40	2194.79	3731.61	3476.18	255.43	2
7.44	6130.68	2284.54	3846.14	3593.15	252.99	2
5.57	6334.60	2373.87	3960.72	3709.76	250.97	2

3.71	6538.14	2462.94	4075.20	3825.99	249.21	2
1.85	6741.31	2551.89	4189.43	3941.85	247.58	2
.00	6944.11	2642.31	4301.80	4057.34	244.46	2

Time = 720. Degree of Consolidation = 27.%

Total Settlement = .394

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 720. = .394

Settlement caused by Secondary Compression at time 720. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.42	301.42	.00	1

Time = 720. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 720. = .169

Settlement caused by Secondary Compression at time 720. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.04

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.17	24.38	6.50	5.79	5.69	6
60.02	59.66	24.30	6.49	5.82	5.68	6
59.45	59.14	24.22	6.47	5.86	5.66	6
58.89	58.62	24.15	6.46	5.89	5.65	6
58.33	58.10	24.07	6.44	5.93	5.64	6
57.76	57.58	24.00	6.43	5.96	5.62	6
57.20	57.05	23.92	6.42	5.99	5.61	6
56.64	56.52	23.85	6.40	6.03	5.59	6
56.09	55.99	23.77	6.39	6.06	5.58	6
56.09	55.99	23.77	.89	.88	.87	5
54.84	54.75	23.11	.88	.87	.86	5
53.60	53.52	22.45	.88	.87	.85	5
52.37	52.29	21.79	.87	.86	.85	5
51.14	51.06	21.13	.86	.86	.84	5
49.91	49.84	20.47	.86	.85	.84	5
48.69	48.61	19.81	.85	.85	.84	5
48.69	48.61	19.81	1.88	1.87	1.81	4
46.67	46.61	19.11	1.86	1.85	1.79	4
44.67	44.62	18.41	1.84	1.83	1.77	4
42.68	42.64	17.71	1.82	1.81	1.75	4
40.71	40.67	17.01	1.80	1.80	1.72	4
38.76	38.72	16.31	1.78	1.78	1.70	4
36.82	36.78	15.61	1.76	1.75	1.68	4
34.90	34.86	14.91	1.73	1.73	1.66	4
32.99	32.95	14.21	1.71	1.71	1.63	4
31.09	31.06	13.50	1.69	1.68	1.61	4
31.09	31.06	13.50	1.42	1.42	1.38	3
29.70	29.67	12.93	1.41	1.41	1.37	3
28.32	28.29	12.35	1.40	1.40	1.36	3
26.94	26.92	11.78	1.39	1.39	1.35	3

25.57	25.55	11.20	1.38	1.38	1.34	3
24.20	24.18	10.63	1.37	1.37	1.33	3
22.84	22.83	10.05	1.36	1.36	1.32	3
21.49	21.47	9.48	1.35	1.35	1.31	3
20.14	20.13	8.90	1.34	1.34	1.30	3
18.80	18.78	8.33	1.33	1.33	1.29	3
18.80	18.78	8.33	1.30	1.30	1.27	2
16.88	16.87	7.50	1.29	1.29	1.26	2
14.98	14.97	6.66	1.28	1.28	1.25	2
13.09	13.08	5.83	1.27	1.27	1.25	2
11.20	11.19	5.00	1.26	1.26	1.24	2
9.32	9.31	4.16	1.26	1.25	1.23	2
7.44	7.44	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.71	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.23	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.17	569.29	236.04	333.25	301.41	31.84	6
59.66	605.99	224.66	381.34	333.49	47.84	6
59.14	642.86	213.24	429.61	365.74	63.88	6
58.62	679.88	201.80	478.08	398.14	79.94	6
58.10	717.07	190.33	526.74	430.71	96.03	6
57.58	754.42	178.83	575.59	463.44	112.15	6
57.05	791.94	167.30	624.63	496.34	128.30	6
56.52	829.62	155.75	673.87	529.40	144.47	6
55.99	867.46	144.17	723.29	562.62	160.67	6
55.99	867.46	144.17	723.29	562.62	160.67	5
54.75	1017.94	211.32	806.62	639.83	166.79	5
53.52	1168.19	277.60	890.60	716.82	173.78	5
52.29	1318.23	343.04	975.19	793.59	181.60	5
51.06	1468.05	407.68	1060.38	870.15	190.23	5
49.84	1617.66	471.56	1146.11	946.49	199.61	5
48.61	1767.07	543.58	1223.48	1022.63	200.85	5
48.61	1767.07	543.58	1223.48	1022.63	200.85	4
46.61	1970.02	606.11	1363.91	1147.71	216.20	4
44.62	2172.20	669.42	1502.78	1272.02	230.76	4
42.64	2373.60	734.18	1639.43	1395.55	243.88	4
40.67	2574.19	801.28	1772.92	1518.27	254.65	4
38.72	2773.95	872.01	1901.94	1640.15	261.79	4
36.78	2972.80	948.29	2024.51	1761.13	263.38	4
34.86	3170.67	1030.25	2140.43	1881.13	259.30	4
32.95	3367.51	1113.69	2253.82	2000.09	253.73	4

31.06	3563.28	1196.80	2366.48	2117.99	248.49	4
31.06	3563.28	1196.80	2366.48	2117.99	248.49	3
29.67	3713.02	1264.79	2448.23	2204.57	243.66	3
28.29	3862.37	1330.95	2531.42	2290.78	240.65	3
26.92	4011.35	1395.55	2615.80	2376.60	239.20	3
25.55	4159.96	1458.94	2701.02	2462.06	238.96	3
24.18	4308.21	1521.30	2786.92	2547.16	239.76	3
22.83	4456.11	1582.80	2873.31	2631.90	241.41	3
21.47	4603.65	1643.60	2960.05	2716.29	243.76	3
20.13	4750.85	1703.70	3047.15	2800.34	246.82	3
18.78	4897.71	1763.20	3134.50	2884.04	250.47	3
18.78	4897.71	1763.20	3134.50	2884.04	250.47	2
16.87	5104.21	1842.77	3261.44	3003.23	258.21	2
14.97	5310.23	1923.66	3386.57	3121.94	264.63	2
13.08	5515.72	2007.72	3508.00	3240.12	267.88	2
11.19	5720.76	2105.46	3615.31	3357.85	257.45	2
9.31	5925.41	2199.20	3726.21	3475.19	251.02	2
7.44	6129.68	2290.74	3838.94	3592.15	246.79	2
5.57	6333.56	2381.08	3952.49	3708.72	243.76	2
3.71	6537.07	2471.11	4065.96	3824.92	241.04	2
1.85	6740.21	2560.99	4179.21	3940.75	238.47	2
.00	6942.97	2650.86	4292.11	4056.20	235.91	2

Time = 1080. Degree of Consolidation = 28.%

Total Settlement = .412

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 1080. = .412

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1

.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 1080. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 1080. = .169

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.02

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.16	24.38	6.50	5.79	5.69	6
60.02	59.65	24.30	6.49	5.82	5.68	6
59.45	59.13	24.22	6.47	5.86	5.66	6
58.89	58.61	24.15	6.46	5.89	5.65	6
58.33	58.09	24.07	6.44	5.92	5.64	6
57.76	57.56	24.00	6.43	5.96	5.62	6
57.20	57.04	23.92	6.42	5.99	5.61	6
56.64	56.51	23.85	6.40	6.03	5.59	6
56.09	55.97	23.77	6.39	6.06	5.58	6
56.09	55.97	23.77	.89	.88	.87	5
54.84	54.74	23.11	.88	.87	.86	5

53.60	53.50	22.45	.88	.87	.85	5
52.37	52.27	21.79	.87	.86	.85	5
51.14	51.05	21.13	.86	.86	.84	5
49.91	49.82	20.47	.86	.85	.84	5
48.69	48.60	19.81	.85	.85	.84	5
48.69	48.60	19.81	1.88	1.87	1.81	4
46.67	46.60	19.11	1.86	1.85	1.79	4
44.67	44.61	18.41	1.84	1.83	1.77	4
42.68	42.63	17.71	1.82	1.81	1.75	4
40.71	40.66	17.01	1.80	1.79	1.72	4
38.76	38.71	16.31	1.78	1.77	1.70	4
36.82	36.77	15.61	1.76	1.75	1.68	4
34.90	34.85	14.91	1.73	1.73	1.66	4
32.99	32.94	14.21	1.71	1.71	1.63	4
31.09	31.05	13.50	1.69	1.68	1.61	4
31.09	31.05	13.50	1.42	1.42	1.38	3
29.70	29.67	12.93	1.41	1.41	1.37	3
28.32	28.29	12.35	1.40	1.40	1.36	3
26.94	26.91	11.78	1.39	1.39	1.35	3
25.57	25.54	11.20	1.38	1.38	1.34	3
24.20	24.18	10.63	1.37	1.37	1.33	3
22.84	22.82	10.05	1.36	1.36	1.32	3
21.49	21.47	9.48	1.35	1.35	1.31	3
20.14	20.12	8.90	1.34	1.34	1.30	3
18.80	18.78	8.33	1.33	1.33	1.29	3
18.80	18.78	8.33	1.30	1.30	1.27	2
16.88	16.87	7.50	1.29	1.29	1.26	2
14.98	14.97	6.66	1.28	1.28	1.25	2
13.09	13.08	5.83	1.27	1.27	1.25	2
11.20	11.19	5.00	1.26	1.26	1.24	2
9.32	9.31	4.16	1.26	1.25	1.23	2
7.44	7.44	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.71	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.16	569.29	236.04	333.25	301.41	31.84	6
59.65	605.99	224.68	381.31	333.49	47.82	6
59.13	642.85	213.28	429.57	365.73	63.83	6
58.61	679.88	201.86	478.01	398.14	79.88	6
58.09	717.07	190.42	526.65	430.71	95.94	6
57.56	754.42	178.94	575.48	463.44	112.04	6

57.04	791.93	167.42	624.51	496.33	128.18	6
56.51	829.61	155.88	673.73	529.39	144.34	6
55.97	867.45	144.30	723.16	562.61	160.54	6
55.97	867.45	144.30	723.16	562.61	160.54	5
54.74	1017.93	211.44	806.48	639.82	166.66	5
53.50	1168.18	277.72	890.46	716.81	173.65	5
52.27	1318.22	343.16	975.06	793.58	181.48	5
51.05	1468.04	407.80	1060.24	870.13	190.11	5
49.82	1617.65	471.68	1145.97	946.48	199.49	5
48.60	1767.05	543.74	1223.32	1022.62	200.70	5
48.60	1767.05	543.74	1223.31	1022.62	200.70	4
46.60	1970.00	607.04	1362.97	1147.69	215.27	4
44.61	2172.17	671.10	1501.07	1271.99	229.08	4
42.63	2373.54	736.55	1637.00	1395.49	241.51	4
40.66	2574.10	804.29	1769.82	1518.17	251.64	4
38.71	2773.81	875.65	1898.16	1640.01	258.15	4
36.77	2972.62	952.61	2020.01	1760.94	259.06	4
34.85	3170.43	1034.98	2135.45	1880.89	254.56	4
32.94	3367.21	1118.72	2248.48	1999.79	248.70	4
31.05	3562.91	1202.14	2360.78	2117.62	243.16	4
31.05	3562.91	1202.14	2360.78	2117.62	243.16	3
29.67	3712.62	1270.42	2442.20	2204.18	238.03	3
28.29	3861.94	1336.88	2525.06	2290.34	234.72	3
26.91	4010.89	1401.72	2609.16	2376.13	233.03	3
25.54	4159.46	1465.14	2694.33	2461.56	232.77	3
24.18	4307.68	1527.42	2780.26	2546.62	233.64	3
22.82	4455.54	1588.62	2866.91	2631.33	235.59	3
21.47	4603.05	1648.93	2954.13	2715.69	238.44	3
20.12	4750.22	1708.48	3041.74	2799.70	242.03	3
18.78	4897.05	1767.37	3129.68	2883.38	246.30	3
18.78	4897.05	1767.37	3129.68	2883.38	246.30	2
16.87	5103.53	1845.61	3257.92	3002.55	255.37	2
14.97	5309.54	1925.12	3384.42	3121.25	263.17	2
13.08	5515.02	2007.72	3507.30	3239.42	267.88	2
11.19	5720.06	2107.32	3612.75	3357.15	255.59	2
9.31	5924.70	2202.83	3721.87	3474.48	247.39	2
7.44	6128.95	2296.06	3832.88	3591.42	241.47	2
5.57	6332.81	2387.27	3945.54	3707.97	237.57	2
3.71	6536.29	2477.31	4058.99	3824.14	234.85	2
1.85	6739.40	2567.19	4172.22	3939.94	232.27	2
.00	6942.14	2657.06	4285.08	4055.37	229.71	2

Time = 1440. Degree of Consolidation = 29.%

Total Settlement = .425

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 1440. = .425

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 1440. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 1440. = .169

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.01

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.15	24.38	6.50	5.79	5.69	6
60.02	59.63	24.30	6.49	5.82	5.68	6
59.45	59.12	24.22	6.47	5.86	5.66	6
58.89	58.60	24.15	6.46	5.89	5.65	6
58.33	58.08	24.07	6.44	5.92	5.64	6
57.76	57.55	24.00	6.43	5.96	5.62	6
57.20	57.02	23.92	6.42	5.99	5.61	6
56.64	56.49	23.85	6.40	6.03	5.59	6
56.09	55.96	23.77	6.39	6.06	5.58	6
56.09	55.96	23.77	.89	.88	.87	5
54.84	54.73	23.11	.88	.87	.86	5
53.60	53.49	22.45	.88	.87	.85	5
52.37	52.26	21.79	.87	.86	.85	5
51.14	51.03	21.13	.86	.86	.84	5
49.91	49.81	20.47	.86	.85	.84	5
48.69	48.59	19.81	.85	.85	.84	5
48.69	48.59	19.81	1.88	1.87	1.81	4
46.67	46.59	19.11	1.86	1.85	1.79	4
44.67	44.59	18.41	1.84	1.83	1.77	4
42.68	42.62	17.71	1.82	1.81	1.75	4
40.71	40.65	17.01	1.80	1.79	1.72	4
38.76	38.70	16.31	1.78	1.77	1.70	4
36.82	36.76	15.61	1.76	1.75	1.68	4
34.90	34.84	14.91	1.73	1.73	1.66	4
32.99	32.93	14.21	1.71	1.70	1.63	4
31.09	31.05	13.50	1.69	1.68	1.61	4
31.09	31.05	13.50	1.42	1.42	1.38	3
29.70	29.66	12.93	1.41	1.41	1.37	3
28.32	28.28	12.35	1.40	1.40	1.36	3
26.94	26.91	11.78	1.39	1.38	1.35	3
25.57	25.54	11.20	1.38	1.37	1.34	3
24.20	24.17	10.63	1.37	1.36	1.33	3
22.84	22.82	10.05	1.36	1.36	1.32	3
21.49	21.47	9.48	1.35	1.35	1.31	3
20.14	20.12	8.90	1.34	1.34	1.30	3
18.80	18.78	8.33	1.33	1.33	1.29	3
18.80	18.78	8.33	1.30	1.30	1.27	2
16.88	16.87	7.50	1.29	1.29	1.26	2
14.98	14.97	6.66	1.28	1.28	1.25	2

13.09	13.07	5.83	1.27	1.27	1.25	2
11.20	11.19	5.00	1.26	1.26	1.24	2
9.32	9.31	4.16	1.26	1.25	1.23	2
7.44	7.43	3.33	1.25	1.25	1.23	2
5.57	5.57	2.50	1.24	1.24	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.15	569.29	236.04	333.25	301.41	31.84	6
59.63	605.99	224.69	381.30	333.49	47.81	6
59.12	642.85	213.31	429.54	365.73	63.81	6
58.60	679.88	201.91	477.97	398.14	79.83	6
58.08	717.06	190.47	526.59	430.70	95.89	6
57.55	754.41	179.01	575.40	463.43	111.97	6
57.02	791.93	167.51	624.41	496.33	128.09	6
56.49	829.60	155.98	673.62	529.38	144.24	6
55.96	867.44	144.42	723.03	562.60	160.42	6
55.96	867.44	144.42	723.03	562.60	160.42	5
54.73	1017.92	211.57	806.35	639.81	166.54	5
53.49	1168.17	277.85	890.32	716.80	173.52	5
52.26	1318.21	343.30	974.91	793.57	181.34	5
51.03	1468.03	407.94	1060.09	870.12	189.96	5
49.81	1617.64	471.83	1145.81	946.47	199.34	5
48.59	1767.04	543.93	1223.11	1022.61	200.50	5
48.59	1767.04	543.93	1223.11	1022.61	200.50	4
46.59	1969.98	607.76	1362.22	1147.68	214.55	4
44.59	2172.14	672.37	1499.77	1271.96	227.81	4
42.62	2373.49	738.43	1635.07	1395.44	239.63	4
40.65	2574.03	806.78	1767.25	1518.10	249.15	4
38.70	2773.70	878.70	1895.00	1639.90	255.10	4
36.76	2972.47	956.36	2016.11	1760.79	255.31	4
34.84	3170.23	1039.25	2130.98	1880.69	250.29	4
32.93	3366.95	1123.14	2243.81	1999.53	244.28	4
31.05	3562.60	1206.71	2355.89	2117.31	238.58	4
31.05	3562.60	1206.71	2355.89	2117.31	238.58	3
29.66	3712.28	1275.12	2437.16	2203.84	233.32	3
28.28	3861.57	1341.64	2519.94	2289.98	229.96	3
26.91	4010.49	1406.53	2603.96	2375.74	228.22	3
25.54	4159.04	1470.00	2689.04	2461.14	227.90	3
24.17	4307.23	1532.23	2775.00	2546.17	228.83	3
22.82	4455.06	1593.38	2861.69	2630.85	230.84	3
21.47	4602.55	1653.52	2949.02	2715.18	233.84	3

20.12	4749.69	1712.70	3036.99	2799.17	237.82	3
18.78	4896.49	1771.05	3125.44	2882.82	242.62	3
18.78	4896.49	1771.05	3125.44	2882.82	242.62	2
16.87	5102.96	1848.12	3254.84	3001.98	252.86	2
14.97	5308.95	1926.40	3382.55	3120.66	261.89	2
13.07	5514.44	2007.72	3506.72	3238.84	267.88	2
11.19	5719.48	2108.93	3610.55	3356.57	253.98	2
9.31	5924.10	2205.98	3718.12	3473.88	244.24	2
7.43	6128.33	2300.49	3827.84	3590.80	237.04	2
5.57	6332.17	2392.92	3939.25	3707.33	231.92	2
3.70	6535.63	2483.50	4052.13	3823.48	228.65	2
1.85	6738.72	2573.38	4165.34	3939.26	226.08	2
.00	6941.43	2663.16	4278.27	4054.66	223.61	2

Time = 1800. Degree of Consolidation = 30.%

Total Settlement = .437

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 1800. = .437

Settlement caused by Secondary Compression at time 1800. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1

1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 1800. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 1800. = .169

Settlement caused by Secondary Compression at time 1800. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.99

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.13	24.38	6.50	5.79	5.69	6
60.02	59.61	24.30	6.49	5.82	5.68	6
59.45	59.10	24.22	6.47	5.86	5.66	6
58.89	58.58	24.15	6.46	5.89	5.65	6
58.33	58.06	24.07	6.44	5.92	5.64	6
57.76	57.53	24.00	6.43	5.96	5.62	6
57.20	57.00	23.92	6.42	5.99	5.61	6
56.64	56.47	23.85	6.40	6.03	5.59	6
56.09	55.94	23.77	6.39	6.06	5.58	6
56.09	55.94	23.77	.89	.88	.87	5
54.84	54.71	23.11	.88	.87	.86	5
53.60	53.47	22.45	.88	.87	.85	5
52.37	52.24	21.79	.87	.86	.85	5
51.14	51.01	21.13	.86	.86	.84	5
49.91	49.79	20.47	.86	.85	.84	5
48.69	48.57	19.81	.85	.85	.84	5
48.69	48.57	19.81	1.88	1.87	1.81	4
46.67	46.57	19.11	1.86	1.85	1.79	4
44.67	44.58	18.41	1.84	1.83	1.77	4
42.68	42.60	17.71	1.82	1.81	1.75	4

40.71	40.63	17.01	1.80	1.79	1.72	4
38.76	38.68	16.31	1.78	1.77	1.70	4
36.82	36.74	15.61	1.76	1.75	1.68	4
34.90	34.82	14.91	1.73	1.73	1.66	4
32.99	32.92	14.21	1.71	1.70	1.63	4
31.09	31.04	13.50	1.69	1.68	1.61	4
31.09	31.04	13.50	1.42	1.42	1.38	3
29.70	29.65	12.93	1.41	1.40	1.37	3
28.32	28.27	12.35	1.40	1.39	1.36	3
26.94	26.90	11.78	1.39	1.38	1.35	3
25.57	25.53	11.20	1.38	1.37	1.34	3
24.20	24.17	10.63	1.37	1.36	1.33	3
22.84	22.81	10.05	1.36	1.35	1.32	3
21.49	21.46	9.48	1.35	1.34	1.31	3
20.14	20.11	8.90	1.34	1.33	1.30	3
18.80	18.77	8.33	1.33	1.33	1.29	3
18.80	18.77	8.33	1.30	1.30	1.27	2
16.88	16.87	7.50	1.29	1.29	1.26	2
14.98	14.96	6.66	1.28	1.28	1.25	2
13.09	13.07	5.83	1.27	1.27	1.25	2
11.20	11.18	5.00	1.26	1.26	1.24	2
9.32	9.30	4.16	1.26	1.25	1.23	2
7.44	7.43	3.33	1.25	1.25	1.23	2
5.57	5.56	2.50	1.24	1.24	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.13	569.29	236.04	333.25	301.41	31.84	6
59.61	605.99	224.71	381.28	333.49	47.79	6
59.10	642.85	213.34	429.51	365.73	63.78	6
58.58	679.87	201.95	477.92	398.13	79.79	6
58.06	717.06	190.53	526.53	430.70	95.83	6
57.53	754.41	179.09	575.32	463.43	111.90	6
57.00	791.92	167.60	624.32	496.32	128.00	6
56.47	829.60	156.09	673.51	529.38	144.13	6
55.94	867.44	144.54	722.90	562.60	160.30	6
55.94	867.44	144.54	722.90	562.60	160.30	5
54.71	1017.91	211.70	806.21	639.80	166.41	5
53.47	1168.16	277.98	890.18	716.79	173.39	5
52.24	1318.20	343.44	974.76	793.56	181.20	5
51.01	1468.02	408.09	1059.93	870.12	189.82	5
49.79	1617.63	471.98	1145.64	946.46	199.19	5

48.57	1767.03	544.14	1222.89	1022.60	200.30	5
48.57	1767.03	544.14	1222.89	1022.60	200.30	4
46.57	1969.97	608.78	1361.19	1147.66	213.53	4
44.58	2172.10	674.28	1497.82	1271.92	225.90	4
42.60	2373.43	741.31	1632.12	1395.37	236.74	4
40.63	2573.92	810.73	1763.19	1517.99	245.20	4
38.68	2773.54	883.93	1889.61	1639.74	249.87	4
36.74	2972.23	963.06	2009.17	1760.56	248.61	4
34.82	3169.91	1046.87	2123.04	1880.36	242.68	4
32.92	3366.52	1131.42	2235.11	1999.10	236.00	4
31.04	3562.06	1215.43	2346.63	2116.77	229.86	4
31.04	3562.06	1215.43	2346.63	2116.77	229.86	3
29.65	3711.69	1284.16	2427.54	2203.25	224.29	3
28.27	3860.94	1350.86	2510.08	2289.34	220.74	3
26.90	4009.80	1415.74	2594.06	2375.05	219.01	3
25.53	4158.30	1479.00	2679.30	2460.39	218.91	3
24.17	4306.43	1540.80	2765.63	2545.38	220.26	3
22.81	4454.22	1601.33	2852.89	2630.01	222.88	3
21.46	4601.66	1660.75	2940.91	2714.30	226.61	3
20.11	4748.76	1719.23	3029.54	2798.25	231.29	3
18.77	4895.53	1776.88	3118.66	2881.86	236.79	3
18.77	4895.53	1776.88	3118.66	2881.86	236.79	2
16.87	5101.97	1852.26	3249.71	3000.99	248.72	2
14.96	5307.94	1928.53	3379.41	3119.65	259.76	2
13.07	5513.42	2007.72	3505.70	3237.82	267.88	2
11.18	5718.46	2112.10	3606.36	3355.54	250.81	2
9.30	5923.06	2212.18	3710.88	3472.84	238.04	2
7.43	6127.26	2308.46	3818.80	3589.73	229.07	2
5.56	6331.06	2402.59	3928.47	3706.22	222.25	2
3.70	6534.48	2494.82	4039.67	3822.33	217.34	2
1.85	6737.52	2585.35	4152.17	3938.06	214.11	2
.00	6940.18	2674.40	4265.78	4053.41	212.37	2

Time = 2520. Degree of Consolidation = 31.%

Total Settlement = .457

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 2520. = .457

Settlement caused by Secondary Compression at time 2520. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 2520. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 2520. = .169

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.97

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.12	24.38	6.50	5.79	5.69	6

60.02	59.61	24.30	6.49	5.82	5.68	6
59.45	59.09	24.22	6.47	5.86	5.66	6
58.89	58.57	24.15	6.46	5.89	5.65	6
58.33	58.05	24.07	6.44	5.92	5.64	6
57.76	57.52	24.00	6.43	5.96	5.62	6
57.20	57.00	23.92	6.42	5.99	5.61	6
56.64	56.47	23.85	6.40	6.03	5.59	6
56.09	55.93	23.77	6.39	6.06	5.58	6
56.09	55.93	23.77	.89	.88	.87	5
54.84	54.70	23.11	.88	.87	.86	5
53.60	53.46	22.45	.88	.87	.85	5
52.37	52.23	21.79	.87	.86	.85	5
51.14	51.01	21.13	.86	.86	.84	5
49.91	49.78	20.47	.86	.85	.84	5
48.69	48.56	19.81	.85	.85	.84	5
48.69	48.56	19.81	1.88	1.87	1.81	4
46.67	46.56	19.11	1.86	1.85	1.79	4
44.67	44.57	18.41	1.84	1.83	1.77	4
42.68	42.59	17.71	1.82	1.81	1.75	4
40.71	40.62	17.01	1.80	1.79	1.72	4
38.76	38.67	16.31	1.78	1.77	1.70	4
36.82	36.74	15.61	1.76	1.75	1.68	4
34.90	34.82	14.91	1.73	1.73	1.66	4
32.99	32.92	14.21	1.71	1.70	1.63	4
31.09	31.03	13.50	1.69	1.68	1.61	4
31.09	31.03	13.50	1.42	1.42	1.38	3
29.70	29.65	12.93	1.41	1.40	1.37	3
28.32	28.27	12.35	1.40	1.39	1.36	3
26.94	26.89	11.78	1.39	1.38	1.35	3
25.57	25.53	11.20	1.38	1.37	1.34	3
24.20	24.16	10.63	1.37	1.36	1.33	3
22.84	22.81	10.05	1.36	1.35	1.32	3
21.49	21.46	9.48	1.35	1.34	1.31	3
20.14	20.11	8.90	1.34	1.33	1.30	3
18.80	18.77	8.33	1.33	1.33	1.29	3
18.80	18.77	8.33	1.30	1.30	1.27	2
16.88	16.86	7.50	1.29	1.29	1.26	2
14.98	14.96	6.66	1.28	1.28	1.25	2
13.09	13.07	5.83	1.27	1.27	1.25	2
11.20	11.18	5.00	1.26	1.26	1.24	2
9.32	9.30	4.16	1.26	1.25	1.23	2
7.44	7.43	3.33	1.25	1.25	1.23	2
5.57	5.56	2.50	1.24	1.24	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.12	569.29	236.04	333.25	301.41	31.84	6
59.61	605.99	224.72	381.27	333.49	47.78	6
59.09	642.85	213.37	429.48	365.73	63.75	6
58.57	679.87	202.00	477.87	398.13	79.74	6
58.05	717.06	190.60	526.46	430.70	95.76	6
57.52	754.41	179.16	575.25	463.43	111.82	6
57.00	791.92	167.70	624.22	496.32	127.91	6
56.47	829.59	156.20	673.40	529.37	144.02	6
55.93	867.43	144.66	722.77	562.59	160.18	6
55.93	867.43	144.66	722.77	562.59	160.18	5
54.70	1017.90	211.82	806.08	639.79	166.28	5
53.46	1168.15	278.12	890.04	716.78	173.25	5
52.23	1318.19	343.58	974.61	793.55	181.06	5
51.01	1468.01	408.24	1059.78	870.11	189.67	5
49.78	1617.62	472.14	1145.48	946.45	199.03	5
48.56	1767.02	544.34	1222.68	1022.59	200.09	5
48.56	1767.02	544.34	1222.68	1022.59	200.09	4
46.56	1969.95	609.32	1360.63	1147.64	212.99	4
44.57	2172.08	675.20	1496.88	1271.90	224.99	4
42.59	2373.39	742.62	1630.77	1395.34	235.43	4
40.62	2573.86	812.50	1761.36	1517.94	243.43	4
38.67	2773.46	886.14	1887.32	1639.66	247.66	4
36.74	2972.12	965.85	2006.27	1760.45	245.82	4
34.82	3169.76	1050.09	2119.67	1880.21	239.46	4
32.92	3366.33	1134.77	2231.56	1998.91	232.65	4
31.03	3561.83	1218.66	2343.17	2116.54	226.63	4
31.03	3561.83	1218.66	2343.17	2116.54	226.63	3
29.65	3711.44	1287.36	2424.09	2203.00	221.09	3
28.27	3860.67	1354.02	2506.64	2289.07	217.57	3
26.89	4009.51	1418.88	2590.63	2374.76	215.87	3
25.53	4157.99	1482.11	2675.88	2460.09	215.79	3
24.16	4306.11	1543.91	2762.20	2545.05	217.15	3
22.81	4453.88	1604.43	2849.45	2629.67	219.78	3
21.46	4601.30	1663.85	2937.45	2713.94	223.51	3
20.11	4748.39	1722.22	3026.17	2797.87	228.30	3
18.77	4895.14	1779.54	3115.60	2881.47	234.13	3
18.77	4895.14	1779.54	3115.60	2881.47	234.13	2
16.86	5101.56	1854.33	3247.23	3000.58	246.65	2
14.96	5307.52	1929.58	3377.94	3119.23	258.71	2
13.07	5513.00	2007.72	3505.28	3237.40	267.88	2
11.18	5718.03	2113.23	3604.81	3355.12	249.68	2
9.30	5922.63	2214.38	3708.25	3472.41	235.84	2
7.43	6126.82	2311.56	3815.27	3589.29	225.97	2

5.56	6330.61	2405.69	3924.92	3705.77	219.15	2
3.70	6534.02	2497.91	4036.10	3821.87	214.24	2
1.85	6737.04	2588.45	4148.59	3937.58	211.01	2
.00	6939.69	2677.50	4262.19	4052.92	209.27	2

Time = 2880. Degree of Consolidation = 32.%

Total Settlement = .465

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 2880. = .465

Settlement caused by Secondary Compression at time 2880. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 2880. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 2880. = .169

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.97

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.11	24.38	6.50	5.79	5.69	6
60.02	59.60	24.30	6.49	5.82	5.68	6
59.45	59.08	24.22	6.47	5.86	5.66	6
58.89	58.56	24.15	6.46	5.89	5.65	6
58.33	58.04	24.07	6.44	5.92	5.64	6
57.76	57.52	24.00	6.43	5.96	5.62	6
57.20	56.99	23.92	6.42	5.99	5.61	6
56.64	56.46	23.85	6.40	6.03	5.59	6
56.09	55.93	23.77	6.39	6.06	5.58	6
56.09	55.93	23.77	.89	.88	.87	5
54.84	54.69	23.11	.88	.87	.86	5
53.60	53.46	22.45	.88	.87	.85	5
52.37	52.23	21.79	.87	.86	.85	5
51.14	51.00	21.13	.86	.86	.84	5
49.91	49.78	20.47	.86	.85	.84	5
48.69	48.56	19.81	.85	.85	.84	5
48.69	48.56	19.81	1.88	1.87	1.81	4
46.67	46.55	19.11	1.86	1.85	1.79	4
44.67	44.56	18.41	1.84	1.83	1.77	4
42.68	42.58	17.71	1.82	1.81	1.75	4
40.71	40.62	17.01	1.80	1.79	1.72	4
38.76	38.67	16.31	1.78	1.77	1.70	4
36.82	36.73	15.61	1.76	1.75	1.68	4
34.90	34.81	14.91	1.73	1.72	1.66	4
32.99	32.91	14.21	1.71	1.70	1.63	4
31.09	31.03	13.50	1.69	1.68	1.61	4
31.09	31.03	13.50	1.42	1.41	1.38	3
29.70	29.64	12.93	1.41	1.40	1.37	3
28.32	28.26	12.35	1.40	1.39	1.36	3

26.94	26.89	11.78	1.39	1.38	1.35	3
25.57	25.52	11.20	1.38	1.37	1.34	3
24.20	24.16	10.63	1.37	1.36	1.33	3
22.84	22.81	10.05	1.36	1.35	1.32	3
21.49	21.46	9.48	1.35	1.34	1.31	3
20.14	20.11	8.90	1.34	1.33	1.30	3
18.80	18.77	8.33	1.33	1.32	1.29	3
18.80	18.77	8.33	1.30	1.30	1.27	2
16.88	16.86	7.50	1.29	1.29	1.26	2
14.98	14.96	6.66	1.28	1.28	1.25	2
13.09	13.07	5.83	1.27	1.27	1.25	2
11.20	11.18	5.00	1.26	1.26	1.24	2
9.32	9.30	4.16	1.26	1.25	1.23	2
7.44	7.43	3.33	1.25	1.24	1.23	2
5.57	5.56	2.50	1.24	1.24	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
60.11	569.29	236.04	333.25	301.41	31.84	6
59.60	605.99	224.73	381.26	333.49	47.77	6
59.08	642.85	213.39	429.46	365.73	63.73	6
58.56	679.87	202.03	477.84	398.13	79.71	6
58.04	717.06	190.63	526.42	430.70	95.73	6
57.52	754.40	179.21	575.19	463.42	111.77	6
56.99	791.91	167.76	624.16	496.31	127.85	6
56.46	829.59	156.27	673.32	529.37	143.95	6
55.93	867.43	144.74	722.68	562.58	160.10	6
55.93	867.43	144.74	722.68	562.58	160.10	5
54.69	1017.90	211.91	805.99	639.79	166.20	5
53.46	1168.15	278.21	889.94	716.78	173.17	5
52.23	1318.18	343.67	974.52	793.55	180.97	5
51.00	1468.01	408.33	1059.68	870.10	189.58	5
49.78	1617.61	472.24	1145.38	946.44	198.93	5
48.56	1767.02	544.47	1222.55	1022.58	199.97	5
48.56	1767.02	544.47	1222.54	1022.58	199.96	4
46.55	1969.94	609.77	1360.17	1147.63	212.54	4
44.56	2172.06	676.01	1496.05	1271.88	224.17	4
42.58	2373.36	743.76	1629.60	1395.31	234.29	4
40.62	2573.82	814.02	1759.79	1517.89	241.90	4
38.67	2773.39	888.11	1885.28	1639.59	245.69	4
36.73	2972.03	968.39	2003.64	1760.35	243.29	4
34.81	3169.63	1052.84	2116.79	1880.08	236.71	4

32.91	3366.17	1137.62	2228.54	1998.75	229.80	4
31.03	3561.63	1221.63	2340.00	2116.34	223.66	4
31.03	3561.63	1221.63	2340.00	2116.34	223.66	3
29.64	3711.23	1290.46	2420.77	2202.78	217.99	3
28.26	3860.43	1357.12	2503.31	2288.83	214.47	3
26.89	4009.26	1421.98	2587.28	2374.51	212.77	3
25.52	4157.72	1485.21	2672.51	2459.81	212.69	3
24.16	4305.82	1547.01	2758.81	2544.76	214.05	3
22.81	4453.57	1607.53	2846.04	2629.36	216.68	3
21.46	4600.98	1666.79	2934.19	2713.61	220.57	3
20.11	4748.05	1724.88	3023.17	2797.53	225.64	3
18.77	4894.79	1781.93	3112.85	2881.12	231.74	3
18.77	4894.79	1781.93	3112.86	2881.12	231.74	2
16.86	5101.20	1856.13	3245.06	3000.22	244.85	2
14.96	5307.15	1930.51	3376.64	3118.86	257.79	2
13.07	5512.63	2007.72	3504.90	3237.03	267.88	2
11.18	5717.65	2114.22	3603.44	3354.74	248.69	2
9.30	5922.25	2216.32	3705.93	3472.03	233.90	2
7.43	6126.43	2314.40	3812.03	3588.90	223.13	2
5.56	6330.20	2408.79	3921.42	3705.36	216.05	2
3.70	6533.59	2501.01	4032.58	3821.44	211.14	2
1.85	6736.60	2591.55	4145.06	3937.14	207.91	2
.00	6939.24	2680.60	4258.64	4052.47	206.17	2

Time = 3240. Degree of Consolidation = 32.%

Total Settlement = .472

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 3240. = .472

Settlement caused by Secondary Compression at time 3240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1

1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 3240. = .169

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.96

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.11	24.38	6.50	5.79	5.69	6
60.02	59.59	24.30	6.49	5.82	5.68	6
59.45	59.08	24.22	6.47	5.86	5.66	6
58.89	58.56	24.15	6.46	5.89	5.65	6
58.33	58.03	24.07	6.44	5.92	5.64	6
57.76	57.51	24.00	6.43	5.96	5.62	6
57.20	56.98	23.92	6.42	5.99	5.61	6
56.64	56.45	23.85	6.40	6.03	5.59	6
56.09	55.92	23.77	6.39	6.06	5.58	6
56.09	55.92	23.77	.89	.88	.87	5

54.84	54.68	23.11	.88	.87	.86	5
53.60	53.45	22.45	.88	.87	.85	5
52.37	52.22	21.79	.87	.86	.85	5
51.14	50.99	21.13	.86	.86	.84	5
49.91	49.77	20.47	.86	.85	.84	5
48.69	48.55	19.81	.85	.85	.84	5
48.69	48.55	19.81	1.88	1.87	1.81	4
46.67	46.55	19.11	1.86	1.85	1.79	4
44.67	44.55	18.41	1.84	1.83	1.77	4
42.68	42.58	17.71	1.82	1.81	1.75	4
40.71	40.61	17.01	1.80	1.79	1.72	4
38.76	38.66	16.31	1.78	1.77	1.70	4
36.82	36.73	15.61	1.76	1.75	1.68	4
34.90	34.81	14.91	1.73	1.72	1.66	4
32.99	32.91	14.21	1.71	1.70	1.63	4
31.09	31.02	13.50	1.69	1.67	1.61	4
31.09	31.02	13.50	1.42	1.41	1.38	3
29.70	29.64	12.93	1.41	1.40	1.37	3
28.32	28.26	12.35	1.40	1.39	1.36	3
26.94	26.89	11.78	1.39	1.38	1.35	3
25.57	25.52	11.20	1.38	1.37	1.34	3
24.20	24.16	10.63	1.37	1.36	1.33	3
22.84	22.80	10.05	1.36	1.35	1.32	3
21.49	21.45	9.48	1.35	1.34	1.31	3
20.14	20.11	8.90	1.34	1.33	1.30	3
18.80	18.77	8.33	1.33	1.32	1.29	3
18.80	18.77	8.33	1.30	1.30	1.27	2
16.88	16.86	7.50	1.29	1.29	1.26	2
14.98	14.96	6.66	1.28	1.28	1.25	2
13.09	13.07	5.83	1.27	1.27	1.25	2
11.20	11.18	5.00	1.26	1.26	1.24	2
9.32	9.30	4.16	1.26	1.25	1.23	2
7.44	7.43	3.33	1.25	1.24	1.23	2
5.57	5.56	2.50	1.24	1.24	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.22	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.11	569.29	236.04	333.25	301.41	31.84	6
59.59	605.99	224.74	381.25	333.49	47.76	6
59.08	642.85	213.41	429.44	365.73	63.71	6
58.56	679.87	202.05	477.82	398.13	79.69	6
58.03	717.06	190.66	526.39	430.70	95.70	6

57.51	754.40	179.25	575.16	463.42	111.73	6
56.98	791.91	167.80	624.12	496.31	127.80	6
56.45	829.59	156.32	673.27	529.37	143.90	6
55.92	867.42	144.80	722.62	562.58	160.04	6
55.92	867.42	144.80	722.62	562.58	160.04	5
54.68	1017.89	211.97	805.93	639.79	166.14	5
53.45	1168.15	278.27	889.88	716.77	173.10	5
52.22	1318.18	343.73	974.45	793.54	180.91	5
50.99	1468.00	408.40	1059.60	870.10	189.50	5
49.77	1617.61	472.31	1145.30	946.44	198.86	5
48.55	1767.01	544.57	1222.44	1022.58	199.86	5
48.55	1767.01	544.57	1222.44	1022.58	199.86	4
46.55	1969.93	610.12	1359.81	1147.63	212.19	4
44.55	2172.05	676.64	1495.41	1271.87	223.55	4
42.58	2373.34	744.70	1628.64	1395.29	233.35	4
40.61	2573.78	815.34	1758.44	1517.85	240.59	4
38.66	2773.34	889.88	1883.46	1639.54	243.92	4
36.73	2971.95	970.61	2001.34	1760.27	241.06	4
34.81	3169.52	1055.40	2114.12	1879.98	234.14	4
32.91	3366.02	1140.34	2225.68	1998.61	227.07	4
31.02	3561.45	1224.52	2336.94	2116.16	220.77	4
31.02	3561.45	1224.52	2336.94	2116.16	220.77	3
29.64	3711.03	1293.49	2417.54	2202.59	214.96	3
28.26	3860.22	1360.22	2499.99	2288.62	211.37	3
26.89	4009.03	1425.08	2583.95	2374.28	209.67	3
25.52	4157.47	1488.31	2669.16	2459.57	209.59	3
24.16	4305.55	1550.08	2755.47	2544.50	210.98	3
22.80	4453.29	1610.35	2842.93	2629.08	213.86	3
21.45	4600.68	1669.30	2931.38	2713.32	218.06	3
20.11	4747.74	1727.08	3020.66	2797.22	223.44	3
18.77	4894.46	1783.84	3110.62	2880.79	229.83	3
18.77	4894.46	1783.84	3110.62	2880.79	229.83	2
16.86	5100.86	1857.43	3243.43	2999.88	243.55	2
14.96	5306.81	1931.17	3375.64	3118.52	257.12	2
13.07	5512.29	2007.72	3504.56	3236.69	267.88	2
11.18	5717.31	2115.04	3602.27	3354.40	247.87	2
9.30	5921.90	2217.94	3703.96	3471.68	232.28	2
7.43	6126.07	2316.77	3809.30	3588.54	220.76	2
5.56	6329.84	2411.89	3917.95	3705.00	212.95	2
3.70	6533.21	2504.11	4029.10	3821.06	208.04	2
1.85	6736.21	2594.65	4141.56	3936.75	204.81	2
.00	6938.84	2683.70	4255.14	4052.06	203.07	2

Time = 3600. Degree of Consolidation = 33.%

Total Settlement = .478

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 3600. = .478

Settlement caused by Secondary Compression at time 3600. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 3600. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 3600. = .169

Settlement caused by Secondary Compression at time 3600. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.95

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.09	24.38	6.50	5.79	5.69	6
60.02	59.58	24.30	6.49	5.82	5.68	6
59.45	59.06	24.22	6.47	5.86	5.66	6
58.89	58.54	24.15	6.46	5.89	5.65	6
58.33	58.02	24.07	6.44	5.92	5.64	6
57.76	57.50	24.00	6.43	5.96	5.62	6
57.20	56.97	23.92	6.42	5.99	5.61	6
56.64	56.44	23.85	6.40	6.03	5.59	6
56.09	55.91	23.77	6.39	6.06	5.58	6
56.09	55.91	23.77	.89	.88	.87	5
54.84	54.67	23.11	.88	.87	.86	5
53.60	53.44	22.45	.88	.87	.85	5
52.37	52.21	21.79	.87	.86	.85	5
51.14	50.98	21.13	.86	.86	.84	5
49.91	49.76	20.47	.86	.85	.84	5
48.69	48.54	19.81	.85	.85	.84	5
48.69	48.54	19.81	1.88	1.87	1.81	4
46.67	46.53	19.11	1.86	1.85	1.79	4
44.67	44.54	18.41	1.84	1.83	1.77	4
42.68	42.56	17.71	1.82	1.81	1.75	4
40.71	40.60	17.01	1.80	1.79	1.72	4
38.76	38.65	16.31	1.78	1.77	1.70	4
36.82	36.72	15.61	1.76	1.75	1.68	4
34.90	34.80	14.91	1.73	1.72	1.66	4
32.99	32.90	14.21	1.71	1.70	1.63	4
31.09	31.02	13.50	1.69	1.67	1.61	4
31.09	31.02	13.50	1.42	1.41	1.38	3
29.70	29.63	12.93	1.41	1.40	1.37	3
28.32	28.25	12.35	1.40	1.39	1.36	3
26.94	26.88	11.78	1.39	1.38	1.35	3
25.57	25.52	11.20	1.38	1.37	1.34	3
24.20	24.15	10.63	1.37	1.36	1.33	3
22.84	22.80	10.05	1.36	1.35	1.32	3
21.49	21.45	9.48	1.35	1.34	1.31	3
20.14	20.11	8.90	1.34	1.33	1.30	3
18.80	18.77	8.33	1.33	1.32	1.29	3
18.80	18.77	8.33	1.30	1.30	1.27	2
16.88	16.86	7.50	1.29	1.29	1.26	2

14.98	14.96	6.66	1.28	1.28	1.25	2
13.09	13.06	5.83	1.27	1.27	1.25	2
11.20	11.18	5.00	1.26	1.26	1.24	2
9.32	9.30	4.16	1.26	1.25	1.23	2
7.44	7.43	3.33	1.25	1.24	1.23	2
5.57	5.56	2.50	1.24	1.24	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.21	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.09	569.29	236.04	333.25	301.41	31.84	6
59.58	605.99	224.75	381.24	333.49	47.75	6
59.06	642.85	213.42	429.43	365.73	63.70	6
58.54	679.87	202.07	477.80	398.13	79.67	6
58.02	717.06	190.70	526.36	430.70	95.66	6
57.50	754.40	179.29	575.11	463.42	111.69	6
56.97	791.91	167.85	624.06	496.31	127.75	6
56.44	829.58	156.38	673.21	529.36	143.85	6
55.91	867.42	144.87	722.55	562.58	159.97	6
55.91	867.42	144.87	722.55	562.58	159.97	5
54.67	1017.89	212.04	805.85	639.78	166.07	5
53.44	1168.14	278.34	889.80	716.77	173.03	5
52.21	1318.18	343.81	974.36	793.54	180.83	5
50.98	1468.00	408.48	1059.52	870.09	189.42	5
49.76	1617.60	472.40	1145.21	946.43	198.77	5
48.54	1767.01	544.68	1222.32	1022.57	199.75	5
48.54	1767.01	544.68	1222.32	1022.57	199.75	4
46.53	1969.93	610.73	1359.19	1147.62	211.58	4
44.54	2172.03	677.79	1494.24	1271.85	222.39	4
42.56	2373.30	746.48	1626.82	1395.25	231.57	4
40.60	2573.72	817.68	1756.04	1517.79	238.25	4
38.65	2773.24	892.92	1880.32	1639.44	240.88	4
36.72	2971.81	974.58	1997.23	1760.13	237.10	4
34.80	3169.33	1060.07	2109.26	1879.78	229.48	4
32.90	3365.77	1145.46	2220.31	1998.35	221.96	4
31.02	3561.13	1229.83	2331.30	2115.84	215.46	4
31.02	3561.13	1229.83	2331.30	2115.84	215.46	3
29.63	3710.68	1298.98	2411.70	2202.23	209.46	3
28.25	3859.83	1365.91	2493.93	2288.23	205.69	3
26.88	4008.61	1430.81	2577.80	2373.86	203.94	3
25.52	4157.02	1493.89	2663.13	2459.12	204.02	3
24.15	4305.07	1555.32	2749.75	2544.01	205.74	3
22.80	4452.78	1615.28	2837.50	2628.57	208.93	3

21.45	4600.14	1673.92	2926.22	2712.78	213.44	3
20.11	4747.17	1731.41	3015.76	2796.65	219.10	3
18.77	4893.87	1787.90	3105.98	2880.20	225.77	3
18.77	4893.87	1787.90	3105.98	2880.20	225.77	2
16.86	5100.25	1860.73	3239.52	2999.27	240.25	2
14.96	5306.18	1933.98	3372.20	3117.89	254.31	2
13.06	5511.64	2011.17	3500.47	3236.04	264.43	2
11.18	5716.65	2119.19	3597.46	3353.74	243.72	2
9.30	5921.22	2222.75	3698.47	3471.00	227.47	2
7.43	6125.37	2322.24	3803.13	3587.84	215.29	2
5.56	6329.11	2417.99	3911.12	3704.27	206.85	2
3.70	6532.46	2510.31	4022.15	3820.31	201.84	2
1.85	6735.43	2600.84	4134.59	3935.97	198.62	2
.00	6938.03	2689.61	4248.42	4051.26	197.16	2

Time = 4320. Degree of Consolidation = 34.%

Total Settlement = .491

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 4320. = .491

Settlement caused by Secondary Compression at time 4320. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1

2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 4320. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 4320. = .169

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.94

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.08	24.38	6.50	5.79	5.69	6
60.02	59.57	24.30	6.49	5.82	5.68	6
59.45	59.05	24.22	6.47	5.86	5.66	6
58.89	58.53	24.15	6.46	5.89	5.65	6
58.33	58.01	24.07	6.44	5.92	5.64	6
57.76	57.49	24.00	6.43	5.96	5.62	6
57.20	56.96	23.92	6.42	5.99	5.61	6
56.64	56.43	23.85	6.40	6.03	5.59	6
56.09	55.90	23.77	6.39	6.06	5.58	6
56.09	55.90	23.77	.89	.88	.87	5
54.84	54.66	23.11	.88	.87	.86	5
53.60	53.43	22.45	.88	.87	.85	5
52.37	52.20	21.79	.87	.86	.85	5
51.14	50.97	21.13	.86	.86	.84	5
49.91	49.75	20.47	.86	.85	.84	5
48.69	48.53	19.81	.85	.85	.84	5
48.69	48.53	19.81	1.88	1.87	1.81	4
46.67	46.52	19.11	1.86	1.85	1.79	4
44.67	44.53	18.41	1.84	1.83	1.77	4

42.68	42.55	17.71	1.82	1.81	1.75	4
40.71	40.59	17.01	1.80	1.79	1.72	4
38.76	38.64	16.31	1.78	1.77	1.70	4
36.82	36.71	15.61	1.76	1.75	1.68	4
34.90	34.79	14.91	1.73	1.72	1.66	4
32.99	32.89	14.21	1.71	1.70	1.63	4
31.09	31.01	13.50	1.69	1.67	1.61	4
31.09	31.01	13.50	1.42	1.41	1.38	3
29.70	29.63	12.93	1.41	1.40	1.37	3
28.32	28.25	12.35	1.40	1.39	1.36	3
26.94	26.88	11.78	1.39	1.38	1.35	3
25.57	25.51	11.20	1.38	1.37	1.34	3
24.20	24.15	10.63	1.37	1.36	1.33	3
22.84	22.79	10.05	1.36	1.35	1.32	3
21.49	21.45	9.48	1.35	1.34	1.31	3
20.14	20.10	8.90	1.34	1.33	1.30	3
18.80	18.76	8.33	1.33	1.32	1.29	3
18.80	18.76	8.33	1.30	1.29	1.27	2
16.88	16.86	7.50	1.29	1.29	1.26	2
14.98	14.95	6.66	1.28	1.28	1.25	2
13.09	13.06	5.83	1.27	1.27	1.25	2
11.20	11.18	5.00	1.26	1.26	1.24	2
9.32	9.30	4.16	1.26	1.25	1.23	2
7.44	7.43	3.33	1.25	1.24	1.23	2
5.57	5.56	2.50	1.24	1.24	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.21	1.20	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.08	569.29	236.04	333.25	301.41	31.84	6
59.57	605.99	224.76	381.23	333.49	47.74	6
59.05	642.85	213.45	429.40	365.73	63.67	6
58.53	679.87	202.11	477.76	398.13	79.63	6
58.01	717.05	190.74	526.31	430.69	95.62	6
57.49	754.40	179.34	575.06	463.42	111.64	6
56.96	791.91	167.92	623.99	496.31	127.69	6
56.43	829.58	156.45	673.12	529.36	143.77	6
55.90	867.41	144.96	722.45	562.57	159.88	6
55.90	867.41	144.96	722.45	562.57	159.88	5
54.66	1017.88	212.13	805.75	639.78	165.97	5
53.43	1168.14	278.44	889.70	716.76	172.93	5
52.20	1318.17	343.91	974.26	793.53	180.73	5
50.97	1467.99	408.59	1059.40	870.09	189.32	5

49.75	1617.60	472.51	1145.09	946.43	198.66	5
48.53	1767.00	544.83	1222.17	1022.56	199.61	5
48.53	1767.00	544.83	1222.17	1022.56	199.61	4
46.52	1969.91	611.23	1358.69	1147.60	211.08	4
44.53	2172.01	678.68	1493.33	1271.83	221.51	4
42.55	2373.27	747.81	1625.46	1395.21	230.25	4
40.59	2573.66	819.53	1754.14	1517.74	236.40	4
38.64	2773.16	895.30	1877.86	1639.36	238.50	4
36.71	2971.70	977.67	1994.03	1760.02	234.01	4
34.79	3169.18	1063.51	2105.67	1879.63	226.04	4
32.89	3365.57	1148.88	2216.70	1998.15	218.54	4
31.01	3560.89	1233.10	2327.80	2115.60	212.20	4
31.01	3560.89	1233.10	2327.80	2115.60	212.20	3
29.63	3710.42	1302.30	2408.12	2201.97	206.15	3
28.25	3859.56	1369.29	2490.27	2287.96	202.31	3
26.88	4008.31	1434.26	2574.05	2373.56	200.49	3
25.51	4156.70	1497.41	2659.29	2458.80	200.49	3
24.15	4304.73	1558.93	2745.81	2543.68	202.13	3
22.79	4452.42	1618.98	2833.44	2628.21	205.23	3
21.45	4599.76	1677.72	2922.04	2712.40	209.64	3
20.10	4746.77	1735.32	3011.45	2796.25	215.20	3
18.76	4893.45	1791.91	3101.54	2879.78	221.76	3
18.76	4893.45	1791.91	3101.54	2879.78	221.76	2
16.86	5099.80	1864.86	3234.94	2998.82	236.12	2
14.95	5305.70	1938.11	3367.59	3117.41	250.18	2
13.06	5511.14	2017.36	3493.78	3235.54	258.24	2
11.18	5716.12	2125.36	3590.77	3353.21	237.55	2
9.30	5920.67	2228.91	3691.76	3470.45	221.31	2
7.43	6124.79	2328.40	3796.39	3587.26	209.13	2
5.56	6328.51	2424.16	3904.35	3703.67	200.68	2
3.70	6531.83	2516.50	4015.34	3819.68	195.65	2
1.85	6734.78	2607.03	4127.75	3935.32	192.43	2
.00	6937.35	2695.41	4241.94	4050.58	191.36	2

Time = 5040. Degree of Consolidation = 34.%

Total Settlement = .502

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 5040. = .502

Settlement caused by Secondary Compression at time 5040. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 5040. = .169

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.93

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material

60.58	60.07	24.38	6.50	5.79	5.69	6
60.02	59.56	24.30	6.49	5.82	5.68	6
59.45	59.04	24.22	6.47	5.86	5.66	6
58.89	58.52	24.15	6.46	5.89	5.65	6
58.33	58.00	24.07	6.44	5.92	5.64	6
57.76	57.48	24.00	6.43	5.96	5.62	6
57.20	56.95	23.92	6.42	5.99	5.61	6
56.64	56.42	23.85	6.40	6.03	5.59	6
56.09	55.89	23.77	6.39	6.06	5.58	6
56.09	55.89	23.77	.89	.88	.87	5
54.84	54.65	23.11	.88	.87	.86	5
53.60	53.42	22.45	.88	.87	.85	5
52.37	52.19	21.79	.87	.86	.85	5
51.14	50.96	21.13	.86	.86	.84	5
49.91	49.74	20.47	.86	.85	.84	5
48.69	48.52	19.81	.85	.85	.84	5
48.69	48.52	19.81	1.88	1.87	1.81	4
46.67	46.51	19.11	1.86	1.85	1.79	4
44.67	44.52	18.41	1.84	1.83	1.77	4
42.68	42.54	17.71	1.82	1.81	1.75	4
40.71	40.58	17.01	1.80	1.79	1.72	4
38.76	38.63	16.31	1.78	1.77	1.70	4
36.82	36.70	15.61	1.76	1.75	1.68	4
34.90	34.78	14.91	1.73	1.72	1.66	4
32.99	32.88	14.21	1.71	1.70	1.63	4
31.09	31.00	13.50	1.69	1.67	1.61	4
31.09	31.00	13.50	1.42	1.41	1.38	3
29.70	29.62	12.93	1.41	1.40	1.37	3
28.32	28.24	12.35	1.40	1.39	1.36	3
26.94	26.87	11.78	1.39	1.38	1.35	3
25.57	25.50	11.20	1.38	1.37	1.34	3
24.20	24.14	10.63	1.37	1.36	1.33	3
22.84	22.79	10.05	1.36	1.35	1.32	3
21.49	21.44	9.48	1.35	1.34	1.31	3
20.14	20.10	8.90	1.34	1.33	1.30	3
18.80	18.76	8.33	1.33	1.32	1.29	3
18.80	18.76	8.33	1.30	1.29	1.27	2
16.88	16.85	7.50	1.29	1.29	1.26	2
14.98	14.95	6.66	1.28	1.28	1.25	2
13.09	13.06	5.83	1.27	1.27	1.25	2
11.20	11.17	5.00	1.26	1.26	1.24	2
9.32	9.29	4.16	1.26	1.25	1.23	2
7.44	7.42	3.33	1.25	1.24	1.23	2
5.57	5.56	2.50	1.24	1.24	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.21	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.07	569.29	236.04	333.25	301.41	31.84	6
59.56	605.99	224.77	381.22	333.49	47.73	6
59.04	642.85	213.46	429.39	365.73	63.66	6
58.52	679.87	202.13	477.74	398.13	79.61	6
58.00	717.05	190.77	526.28	430.69	95.59	6
57.48	754.40	179.38	575.02	463.42	111.60	6
56.95	791.91	167.96	623.94	496.31	127.64	6
56.42	829.58	156.51	673.07	529.36	143.71	6
55.89	867.41	145.02	722.39	562.57	159.82	6
55.89	867.41	145.02	722.39	562.57	159.82	5
54.65	1017.88	212.20	805.68	639.77	165.91	5
53.42	1168.13	278.51	889.62	716.76	172.86	5
52.19	1318.17	343.98	974.18	793.53	180.65	5
50.96	1467.99	408.66	1059.32	870.08	189.24	5
49.74	1617.59	472.59	1145.00	946.42	198.58	5
48.52	1766.99	544.94	1222.06	1022.56	199.50	5
48.52	1766.99	544.94	1222.06	1022.56	199.50	4
46.51	1969.91	611.61	1358.29	1147.60	210.69	4
44.52	2171.99	679.37	1492.62	1271.81	220.81	4
42.54	2373.24	748.86	1624.38	1395.19	229.19	4
40.58	2573.62	821.00	1752.62	1517.70	234.92	4
38.63	2773.10	897.23	1875.87	1639.30	236.57	4
36.70	2971.61	980.12	1991.49	1759.93	231.56	4
34.78	3169.05	1066.35	2102.71	1879.51	223.20	4
32.88	3365.41	1152.02	2213.40	1997.99	215.40	4
31.00	3560.69	1236.42	2324.27	2115.40	208.87	4
31.00	3560.69	1236.42	2324.27	2115.40	208.87	3
29.62	3710.20	1305.70	2404.50	2201.75	202.74	3
28.24	3859.32	1372.73	2486.59	2287.72	198.87	3
26.87	4008.05	1437.75	2570.31	2373.30	197.01	3
25.50	4156.42	1500.95	2655.47	2458.52	196.95	3
24.14	4304.44	1562.52	2741.91	2543.38	198.53	3
22.79	4452.10	1622.64	2829.46	2627.89	201.57	3
21.44	4599.42	1681.46	2917.96	2712.05	205.91	3
20.10	4746.41	1739.13	3007.27	2795.89	211.38	3
18.76	4893.06	1795.82	3097.24	2879.39	217.85	3
18.76	4893.06	1795.82	3097.24	2879.39	217.85	2
16.85	5099.39	1868.93	3230.46	2998.41	232.05	2
14.95	5305.26	1942.23	3363.03	3116.97	246.06	2
13.06	5510.68	2023.55	3487.13	3235.08	252.05	2
11.17	5715.64	2131.53	3584.11	3352.73	231.39	2
9.29	5920.15	2235.07	3685.09	3469.93	215.15	2

7.42	6124.25	2334.56	3789.69	3586.72	202.97	2
5.56	6327.94	2430.33	3897.62	3703.10	194.51	2
3.70	6531.24	2522.69	4008.56	3819.09	189.46	2
1.85	6734.16	2613.22	4120.94	3934.70	186.24	2
.00	6936.71	2701.22	4235.49	4049.94	185.55	2

Time = 5760. Degree of Consolidation = 35.%

Total Settlement = .512

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 5760. = .512

Settlement caused by Secondary Compression at time 5760. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 5760. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 5760. = .169

Settlement caused by Secondary Compression at time 5760. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.92

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.06	24.38	6.50	5.79	5.69	6
60.02	59.55	24.30	6.49	5.82	5.68	6
59.45	59.03	24.22	6.47	5.86	5.66	6
58.89	58.51	24.15	6.46	5.89	5.65	6
58.33	57.99	24.07	6.44	5.92	5.64	6
57.76	57.47	24.00	6.43	5.96	5.62	6
57.20	56.94	23.92	6.42	5.99	5.61	6
56.64	56.41	23.85	6.40	6.03	5.59	6
56.09	55.88	23.77	6.39	6.06	5.58	6
56.09	55.88	23.77	.89	.88	.87	5
54.84	54.64	23.11	.88	.87	.86	5
53.60	53.41	22.45	.88	.87	.85	5
52.37	52.18	21.79	.87	.86	.85	5
51.14	50.95	21.13	.86	.86	.84	5
49.91	49.73	20.47	.86	.85	.84	5
48.69	48.51	19.81	.85	.85	.84	5
48.69	48.51	19.81	1.88	1.87	1.81	4
46.67	46.50	19.11	1.86	1.85	1.79	4
44.67	44.51	18.41	1.84	1.83	1.77	4
42.68	42.53	17.71	1.82	1.81	1.75	4
40.71	40.57	17.01	1.80	1.79	1.72	4
38.76	38.62	16.31	1.78	1.77	1.70	4
36.82	36.69	15.61	1.76	1.74	1.68	4
34.90	34.77	14.91	1.73	1.72	1.66	4
32.99	32.88	14.21	1.71	1.70	1.63	4
31.09	31.00	13.50	1.69	1.67	1.61	4
31.09	31.00	13.50	1.42	1.41	1.38	3
29.70	29.61	12.93	1.41	1.40	1.37	3

28.32	28.23	12.35	1.40	1.39	1.36	3
26.94	26.86	11.78	1.39	1.38	1.35	3
25.57	25.50	11.20	1.38	1.37	1.34	3
24.20	24.14	10.63	1.37	1.36	1.33	3
22.84	22.78	10.05	1.36	1.35	1.32	3
21.49	21.44	9.48	1.35	1.34	1.31	3
20.14	20.09	8.90	1.34	1.33	1.30	3
18.80	18.75	8.33	1.33	1.32	1.29	3
18.80	18.75	8.33	1.30	1.29	1.27	2
16.88	16.85	7.50	1.29	1.29	1.26	2
14.98	14.95	6.66	1.28	1.28	1.25	2
13.09	13.06	5.83	1.27	1.27	1.25	2
11.20	11.17	5.00	1.26	1.26	1.24	2
9.32	9.29	4.16	1.26	1.25	1.23	2
7.44	7.42	3.33	1.25	1.24	1.23	2
5.57	5.56	2.50	1.24	1.24	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.21	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.06	569.29	236.04	333.25	301.41	31.84	6
59.55	605.99	224.77	381.22	333.49	47.73	6
59.03	642.85	213.48	429.37	365.73	63.64	6
58.51	679.87	202.15	477.72	398.13	79.59	6
57.99	717.05	190.80	526.25	430.69	95.56	6
57.47	754.40	179.42	574.98	463.42	111.56	6
56.94	791.90	168.01	623.90	496.30	127.60	6
56.41	829.57	156.56	673.01	529.35	143.66	6
55.88	867.41	145.08	722.33	562.57	159.76	6
55.88	867.41	145.08	722.33	562.57	159.76	5
54.64	1017.88	212.26	805.62	639.77	165.85	5
53.41	1168.13	278.57	889.56	716.76	172.80	5
52.18	1318.16	344.05	974.11	793.52	180.59	5
50.95	1467.98	408.73	1059.25	870.08	189.17	5
49.73	1617.59	472.66	1144.93	946.42	198.51	5
48.51	1766.99	545.03	1221.96	1022.55	199.41	5
48.51	1766.99	545.03	1221.96	1022.55	199.41	4
46.50	1969.90	611.93	1357.97	1147.59	210.38	4
44.51	2171.98	679.94	1492.04	1271.80	220.24	4
42.53	2373.22	749.72	1623.50	1395.17	228.33	4
40.57	2573.59	822.20	1751.39	1517.66	233.72	4
38.62	2773.05	898.86	1874.20	1639.25	234.95	4
36.69	2971.53	982.19	1989.34	1759.86	229.48	4

34.77	3168.95	1068.75	2100.20	1879.41	220.79	4
32.88	3365.28	1154.68	2210.60	1997.86	212.74	4
31.00	3560.52	1239.36	2321.16	2115.23	205.93	4
31.00	3560.52	1239.36	2321.16	2115.23	205.93	3
29.61	3710.01	1308.82	2401.19	2201.57	199.63	3
28.23	3859.11	1375.90	2483.22	2287.51	195.70	3
26.86	4007.83	1440.97	2566.86	2373.08	193.78	3
25.50	4156.18	1504.24	2651.94	2458.28	193.66	3
24.14	4304.17	1565.89	2738.29	2543.12	195.17	3
22.78	4451.82	1626.08	2825.74	2627.61	198.13	3
21.44	4599.12	1684.98	2914.14	2711.75	202.38	3
20.09	4746.08	1742.75	3003.33	2795.57	207.77	3
18.75	4892.72	1799.54	3093.18	2879.05	214.13	3
18.75	4892.72	1799.54	3093.18	2879.05	214.13	2
16.85	5099.03	1872.85	3226.17	2998.05	228.13	2
14.95	5304.87	1946.36	3358.51	3116.58	241.93	2
13.06	5510.26	2029.74	3480.52	3234.66	245.86	2
11.17	5715.19	2137.69	3577.50	3352.28	225.22	2
9.29	5919.69	2241.23	3678.46	3469.47	208.99	2
7.42	6123.76	2340.72	3783.04	3586.23	196.81	2
5.56	6327.42	2436.50	3890.93	3702.58	188.34	2
3.70	6530.70	2528.88	4001.82	3818.55	183.27	2
1.85	6733.59	2619.40	4114.19	3934.13	180.06	2
.00	6936.12	2707.02	4229.10	4049.35	179.76	2

Time = 6480. Degree of Consolidation = 36.%

Total Settlement = .522

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 6480. = .522

Settlement caused by Secondary Compression at time 6480. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1

2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 6480. = .169

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.91

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.05	24.38	6.50	5.79	5.69	6
60.02	59.54	24.30	6.49	5.82	5.68	6
59.45	59.02	24.22	6.47	5.86	5.66	6
58.89	58.50	24.15	6.46	5.89	5.65	6
58.33	57.98	24.07	6.44	5.92	5.64	6
57.76	57.46	24.00	6.43	5.96	5.62	6
57.20	56.93	23.92	6.42	5.99	5.61	6
56.64	56.40	23.85	6.40	6.03	5.59	6
56.09	55.87	23.77	6.39	6.06	5.58	6

56.09	55.87	23.77	.89	.88	.87	5
54.84	54.63	23.11	.88	.87	.86	5
53.60	53.40	22.45	.88	.87	.85	5
52.37	52.17	21.79	.87	.86	.85	5
51.14	50.94	21.13	.86	.86	.84	5
49.91	49.72	20.47	.86	.85	.84	5
48.69	48.50	19.81	.85	.85	.84	5
48.69	48.50	19.81	1.88	1.87	1.81	4
46.67	46.49	19.11	1.86	1.85	1.79	4
44.67	44.50	18.41	1.84	1.83	1.77	4
42.68	42.53	17.71	1.82	1.81	1.75	4
40.71	40.56	17.01	1.80	1.79	1.72	4
38.76	38.61	16.31	1.78	1.77	1.70	4
36.82	36.68	15.61	1.76	1.74	1.68	4
34.90	34.77	14.91	1.73	1.72	1.66	4
32.99	32.87	14.21	1.71	1.69	1.63	4
31.09	30.99	13.50	1.69	1.67	1.61	4
31.09	30.99	13.50	1.42	1.41	1.38	3
29.70	29.61	12.93	1.41	1.40	1.37	3
28.32	28.23	12.35	1.40	1.39	1.36	3
26.94	26.86	11.78	1.39	1.38	1.35	3
25.57	25.49	11.20	1.38	1.37	1.34	3
24.20	24.13	10.63	1.37	1.36	1.33	3
22.84	22.78	10.05	1.36	1.35	1.32	3
21.49	21.43	9.48	1.35	1.34	1.31	3
20.14	20.09	8.90	1.34	1.33	1.30	3
18.80	18.75	8.33	1.33	1.32	1.29	3
18.80	18.75	8.33	1.30	1.29	1.27	2
16.88	16.84	7.50	1.29	1.28	1.26	2
14.98	14.94	6.66	1.28	1.28	1.25	2
13.09	13.05	5.83	1.27	1.27	1.25	2
11.20	11.17	5.00	1.26	1.26	1.24	2
9.32	9.29	4.16	1.26	1.25	1.23	2
7.44	7.42	3.33	1.25	1.24	1.23	2
5.57	5.56	2.50	1.24	1.23	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.21	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.05	569.29	236.04	333.25	301.41	31.84	6
59.54	605.99	224.78	381.21	333.49	47.72	6
59.02	642.85	213.49	429.36	365.73	63.63	6
58.50	679.87	202.17	477.70	398.13	79.57	6

57.98	717.05	190.82	526.23	430.69	95.54	6
57.46	754.40	179.44	574.95	463.42	111.54	6
56.93	791.90	168.03	623.87	496.30	127.57	6
56.40	829.57	156.59	672.98	529.35	143.63	6
55.87	867.40	145.12	722.28	562.56	159.72	6
55.87	867.40	145.12	722.28	562.56	159.72	5
54.63	1017.88	212.30	805.57	639.77	165.81	5
53.40	1168.13	278.61	889.51	716.75	172.76	5
52.17	1318.16	344.09	974.06	793.52	180.54	5
50.94	1467.98	408.78	1059.20	870.07	189.12	5
49.72	1617.59	472.71	1144.87	946.42	198.46	5
48.50	1766.99	545.10	1221.89	1022.55	199.34	5
48.50	1766.99	545.10	1221.89	1022.55	199.34	4
46.49	1969.89	612.18	1357.71	1147.59	210.12	4
44.50	2171.97	680.40	1491.57	1271.79	219.78	4
42.53	2373.21	750.41	1622.79	1395.15	227.64	4
40.56	2573.56	823.17	1750.39	1517.64	232.75	4
38.61	2773.01	900.18	1872.83	1639.21	233.62	4
36.68	2971.47	983.99	1987.49	1759.80	227.68	4
34.77	3168.87	1070.88	2097.99	1879.32	218.66	4
32.87	3365.17	1157.08	2208.09	1997.75	210.34	4
30.99	3560.38	1242.04	2318.33	2115.09	203.25	4
30.99	3560.38	1242.04	2318.33	2115.09	203.25	3
29.61	3709.85	1311.73	2398.12	2201.41	196.71	3
28.23	3858.93	1378.99	2479.94	2287.33	192.61	3
26.86	4007.63	1444.12	2563.51	2372.88	190.63	3
25.49	4155.97	1507.45	2648.52	2458.06	190.45	3
24.13	4303.94	1569.16	2734.78	2542.88	191.89	3
22.78	4451.56	1629.43	2822.14	2627.35	194.78	3
21.43	4598.85	1688.41	2910.43	2711.48	198.95	3
20.09	4745.79	1746.27	2999.52	2795.28	204.24	3
18.75	4892.41	1803.16	3089.25	2878.74	210.51	3
18.75	4892.41	1803.16	3089.25	2878.74	210.51	2
16.84	5098.69	1876.67	3222.02	2997.71	224.31	2
14.94	5304.51	1950.38	3354.13	3116.22	237.91	2
13.05	5509.87	2035.93	3473.95	3234.27	239.67	2
11.17	5714.78	2143.86	3570.92	3351.87	219.05	2
9.29	5919.25	2247.39	3671.86	3469.03	202.83	2
7.42	6123.29	2346.88	3776.42	3585.76	190.66	2
5.56	6326.93	2442.67	3884.27	3702.09	182.17	2
3.70	6530.18	2535.06	3995.12	3818.03	177.09	2
1.85	6733.05	2625.21	4107.84	3933.59	174.25	2
.00	6935.55	2712.46	4223.09	4048.78	174.31	2

Time = 7200. Degree of Consolidation = 36.%

Total Settlement = .531

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 7200. = .531

Settlement caused by Secondary Compression at time 7200. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 7200. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 7200. = .169

Settlement caused by Secondary Compression at time 7200. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.90

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.03	24.38	6.50	5.79	5.69	6
60.02	59.52	24.30	6.49	5.82	5.68	6
59.45	59.00	24.22	6.47	5.86	5.66	6
58.89	58.48	24.15	6.46	5.89	5.65	6
58.33	57.96	24.07	6.44	5.92	5.64	6
57.76	57.44	24.00	6.43	5.96	5.62	6
57.20	56.91	23.92	6.42	5.99	5.61	6
56.64	56.38	23.85	6.40	6.03	5.59	6
56.09	55.85	23.77	6.39	6.06	5.58	6
56.09	55.85	23.77	.89	.88	.87	5
54.84	54.61	23.11	.88	.87	.86	5
53.60	53.38	22.45	.88	.87	.85	5
52.37	52.15	21.79	.87	.86	.85	5
51.14	50.92	21.13	.86	.86	.84	5
49.91	49.70	20.47	.86	.85	.84	5
48.69	48.48	19.81	.85	.85	.84	5
48.69	48.48	19.81	1.88	1.87	1.81	4
46.67	46.47	19.11	1.86	1.85	1.79	4
44.67	44.48	18.41	1.84	1.83	1.77	4
42.68	42.50	17.71	1.82	1.81	1.75	4
40.71	40.54	17.01	1.80	1.79	1.72	4
38.76	38.59	16.31	1.78	1.77	1.70	4
36.82	36.66	15.61	1.76	1.74	1.68	4
34.90	34.75	14.91	1.73	1.72	1.66	4
32.99	32.85	14.21	1.71	1.69	1.63	4
31.09	30.97	13.50	1.69	1.67	1.61	4
31.09	30.97	13.50	1.42	1.41	1.38	3
29.70	29.59	12.93	1.41	1.40	1.37	3
28.32	28.21	12.35	1.40	1.39	1.36	3
26.94	26.84	11.78	1.39	1.38	1.35	3
25.57	25.48	11.20	1.38	1.37	1.34	3
24.20	24.12	10.63	1.37	1.36	1.33	3
22.84	22.77	10.05	1.36	1.35	1.32	3
21.49	21.42	9.48	1.35	1.34	1.31	3
20.14	20.08	8.90	1.34	1.33	1.30	3
18.80	18.74	8.33	1.33	1.32	1.29	3
18.80	18.74	8.33	1.30	1.29	1.27	2

16.88	16.84	7.50	1.29	1.28	1.26	2
14.98	14.94	6.66	1.28	1.27	1.25	2
13.09	13.05	5.83	1.27	1.27	1.25	2
11.20	11.16	5.00	1.26	1.26	1.24	2
9.32	9.29	4.16	1.26	1.25	1.23	2
7.44	7.42	3.33	1.25	1.24	1.23	2
5.57	5.55	2.50	1.24	1.23	1.22	2
3.71	3.70	1.67	1.23	1.23	1.21	2
1.85	1.85	.83	1.23	1.22	1.21	2
.00	.00	.00	1.22	1.21	1.20	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.03	569.29	236.04	333.25	301.41	31.84	6
59.52	605.99	224.78	381.20	333.49	47.72	6
59.00	642.85	213.50	429.35	365.73	63.62	6
58.48	679.87	202.19	477.68	398.13	79.55	6
57.96	717.05	190.85	526.20	430.69	95.51	6
57.44	754.40	179.48	574.92	463.41	111.50	6
56.91	791.90	168.08	623.82	496.30	127.52	6
56.38	829.57	156.64	672.92	529.35	143.58	6
55.85	867.40	145.18	722.22	562.56	159.66	6
55.85	867.40	145.18	722.22	562.56	159.66	5
54.61	1017.87	212.36	805.51	639.76	165.75	5
53.38	1168.12	278.68	889.44	716.75	172.70	5
52.15	1318.16	344.16	973.99	793.52	180.48	5
50.92	1467.97	408.85	1059.13	870.07	189.06	5
49.70	1617.58	472.78	1144.80	946.41	198.39	5
48.48	1766.98	545.19	1221.79	1022.55	199.25	5
48.48	1766.98	545.19	1221.79	1022.55	199.25	4
46.47	1969.89	612.71	1357.18	1147.58	209.60	4
44.48	2171.96	681.41	1490.55	1271.77	218.77	4
42.50	2373.17	751.97	1621.20	1395.12	226.08	4
40.54	2573.51	825.39	1748.11	1517.58	230.54	4
38.59	2772.92	903.22	1869.70	1639.12	230.58	4
36.66	2971.34	988.16	1983.18	1759.67	223.51	4
34.75	3168.68	1075.81	2092.87	1879.13	213.74	4
32.85	3364.91	1162.61	2202.29	1997.49	204.80	4
30.97	3560.05	1248.22	2311.82	2114.75	197.07	4
30.97	3560.05	1248.22	2311.82	2114.75	197.07	3
29.59	3709.48	1318.46	2391.02	2201.04	189.98	3
28.21	3858.52	1386.27	2472.25	2286.93	185.32	3
26.84	4007.18	1451.87	2555.31	2372.43	182.88	3
25.48	4155.47	1515.48	2639.99	2457.57	182.42	3
24.12	4303.40	1577.50	2725.90	2542.34	183.56	3

22.77	4450.97	1638.08	2812.90	2626.76	186.13	3
21.42	4598.20	1697.39	2900.81	2710.84	189.97	3
20.08	4745.10	1755.60	2989.50	2794.58	194.92	3
18.74	4891.66	1812.86	3078.80	2877.99	200.81	3
18.74	4891.66	1812.86	3078.80	2877.99	200.81	2
16.84	5097.88	1886.60	3211.28	2996.90	214.38	2
14.94	5303.64	1960.59	3343.05	3115.35	227.70	2
13.05	5508.94	2051.42	3457.51	3233.34	224.18	2
11.16	5713.78	2159.15	3554.63	3350.87	203.76	2
9.29	5918.18	2262.51	3655.68	3467.96	187.71	2
7.42	6122.17	2361.86	3760.31	3584.64	175.67	2
5.55	6325.75	2457.54	3868.20	3700.90	167.30	2
3.70	6528.93	2549.86	3979.07	3816.78	162.29	2
1.85	6731.74	2639.09	4092.65	3932.28	160.37	2
.00	6934.19	2725.49	4208.70	4047.42	161.28	2

Time = 9000. Degree of Consolidation = 38.%

Total Settlement = .553

Settlement at End of Primary Consolidation = 1.461

Settlement caused by Primary Consolidation at time 9000. = .553

Settlement caused by Secondary Compression at time 9000. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1

3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 9000. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 9000. = .169

Settlement caused by Secondary Compression at time 9000. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.88

APPENDIX III

PSDDF sample calculation and output file for CASE B 5.0 ft thick fill in Bayou Dupont Marsh

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**********************************************************
Consolidation and desiccation of soft layers---dredged fill
**********************************************************

 Problem    Bayou Dupont Marsh Creation BA-48 5.0 ft Fill



**********Soil data for compressible foundation**********

 Material   Layer      Numbers of     Ca/Cc    Cr/Cc
 Type       Thickness  Sub-layers

  2         18.80      10             .015     .113

  3         12.30      9              .021     .135

  4         17.60      9              .014     .140

  5          7.40      6              .019     .147

  6          4.50      8              .040     .215

 Material type :   2              Specific Gravity of Solids:   2.68


     Void  Effective   Perm-    k/1+e
  I Ratio   Stress  eability   PK      Beta      Dsde     Alpha
  1 1.510  .000E+00 .100E-02  .398E-03  .650E-02 -.100E+05 -.398E+01
  2 1.460  .500E+03 .180E-03  .732E-04  .287E-02 -.833E+04 -.610E+00
  3 1.390  .100E+04 .130E-03  .544E-04  .263E-03 -.789E+04 -.429E+00
  4 1.270  .200E+04 .526E-04  .232E-04  .150E-03 -.107E+05 -.248E+00
  5 1.110  .400E+04 .263E-04  .125E-04  .530E-04 -.194E+05 -.241E+00
  6  .960  .800E+04 .132E-04  .673E-05  .294E-04 -.400E+05 -.269E+00
  7  .810  .160E+05 .658E-05  .364E-05  .171E-04 -.857E+05 -.312E+00
```

8	.680	.320E+05	.329E-05	.196E-05	.129E-04	-.123E+06	-.241E+00

Material type : 3 Specific Gravity of Solids: 2.76

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.620	.000E+00	.500E-03	.191E-03	.663E-03	-.625E+04	-.119E+01
2	1.540	.500E+03	.350E-03	.138E-03	.717E-03	-.588E+04	-.811E+00
3	1.450	.100E+04	.169E-03	.690E-04	.403E-03	-.600E+04	-.414E+00
4	1.290	.200E+04	.848E-04	.370E-04	.144E-03	-.882E+04	-.327E+00
5	1.110	.400E+04	.424E-04	.201E-04	.929E-04	-.176E+05	-.355E+00
6	.950	.800E+04	.106E-04	.544E-05	.535E-04	-.375E+05	-.204E+00
7	.790	.160E+05	.530E-05	.296E-05	.128E-04	-.800E+05	-.237E+00
8	.650	.320E+05	.265E-05	.161E-05	.968E-05	-.114E+06	-.184E+00

Material type : 4 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	1.960	.000E+00	.600E-03	.203E-03	.798E-03	-.625E+04	-.127E+01
2	1.880	.500E+03	.400E-03	.139E-03	.545E-03	-.455E+04	-.631E+00
3	1.740	.100E+04	.227E-03	.828E-04	.269E-03	-.349E+04	-.289E+00
4	1.450	.200E+04	.567E-04	.231E-04	.125E-03	-.536E+04	-.124E+00
5	1.180	.400E+04	.283E-04	.130E-04	.325E-04	-.122E+05	-.159E+00
6	.960	.800E+04	.141E-04	.719E-05	.225E-04	-.300E+05	-.216E+00
7	.780	.160E+05	.708E-05	.398E-05	.147E-04	-.706E+05	-.281E+00
8	.620	.320E+05	.354E-05	.219E-05	.112E-04	-.100E+06	-.219E+00

Material type : 5 Specific Gravity of Solids: 2.78

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	4.600	.000E+00	.360E-02	.643E-03	.185E-03	-.403E+03	-.259E+00
2	3.360	.500E+03	.180E-02	.413E-03	.329E-03	-.552E+03	-.228E+00
3	2.790	.100E+04	.180E-03	.475E-04	.341E-03	-.134E+04	-.636E-01

4	2.240	.200E+04	.100E-03	.309E-04	.285E-04	-.319E+04	-.985E-01
5	1.850	.400E+04	.590E-04	.207E-04	.229E-04	-.800E+04	-.166E+00
6	1.490	.800E+04	.340E-04	.137E-04	.204E-04	-.200E+05	-.273E+00
7	1.250	.160E+05	.190E-04	.844E-05	.143E-04	-.333E+05	-.281E+00
8	.770	.320E+05	.590E-05	.333E-05	.106E-04	-.333E+05	-.111E+00

Material type : 6 Specific Gravity of Solids: 1.98

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	6.500	.000E+00	.900E-03	.120E-03	.551E-05	-.331E+03	-.397E-01
2	4.990	.500E+03	.669E-03	.112E-03	.437E-04	-.442E+03	-.494E-01
3	4.240	.100E+04	.111E-03	.212E-04	.686E-04	-.103E+04	-.219E-01
4	3.540	.200E+04	.557E-04	.123E-04	.135E-04	-.229E+04	-.281E-01
5	2.930	.400E+04	.139E-04	.354E-05	.922E-05	-.541E+04	-.191E-01
6	2.430	.800E+04	.697E-05	.203E-05	.341E-05	-.167E+05	-.339E-01
7	2.210	.160E+05	.348E-05	.108E-05	.182E-05	-.316E+05	-.342E-01
8	1.670	.320E+05	.174E-05	.652E-06	.801E-06	-.296E+05	-.193E-01

**********Soil data for dredged fill**********

Material Type	Specific Gravity	Ca/Cc	Cr/Cc	Saturation Limit	Disication Limit
1	2.700	.020	.276	.920	.950

Material type : 1

I	Void Ratio	Effective Stress	Perm-eability	k/1+e PK	Beta	Dsde	Alpha
1	.980	.000E+00	.200E+00	.101E+00	.122E+01	-.324E+03	-.327E+02
2	.960	.648E+01	.150E+00	.765E-01	.124E+01	-.375E+03	-.287E+02
3	.940	.150E+02	.100E+00	.515E-01	.139E+01	-.784E+03	-.404E+02
4	.930	.300E+02	.672E-01	.348E-01	.156E+01	-.175E+04	-.609E+02

5	.920	.500E+02	.390E-01	.203E-01	.142E+01	-.350E+04	-.711E+02
6	.910	.100E+03	.123E-01	.644E-02	.855E+00	-.750E+04	-.483E+02
7	.900	.200E+03	.610E-02	.321E-02	.296E+00	-.125E+05	-.401E+02
8	.890	.350E+03	.100E-02	.529E-03	.268E+00	-.150E+05	-.794E+01

Summary of lifts and print detail

Time days	Material Type	Fill Height	# Sub-layers	Void ratio	Start Day	Dessic. Month	Print detai
0.	1	5.0	4	.98	120.	4	1
30.				120.	4	1	
60.				120.	4	1	
120.				120.	4	1	
240.				120.	4	1	
360.				120.	4	1	
540.				120.	4	1	
720.				120.	4	1	
1080.				120.	4	1	
1440.				120.	4	1	
1800.				120.	4	1	
2520.				120.	4	1	
2880.				120.	4	1	
3240.				120.	4	1	
3600.				120.	4	1	
4320.				120.	4	1	
5040.				120.	4	1	
5760.				120.	4	1	
6480.				120.	4	1	
7200.				120.	4	1	
9000.				120.	4	1	

Summary of monthly rainfall and evaporation potential

Month	Rainfall	Evaporation
1	.400	.200
2	.370	.250

3	.400	.380
4	.360	.480
5	.400	.560
6	.550	.550
7	.670	.540
8	.590	.490
9	.550	.450
10	.300	.370
11	.340	.250
12	.390	.200

**********Calculation data**********

tau	Lower layer Void ratio	Lower layer Permeability	drainage path Length
.173	1.106	.30000E-04	z = 14.25

Summary of desiccation parameters

Parameter	Value
Surface Drainage Efficiency	.80
maximum evaporation efficiency	.80
saturation at desiccation limit	.75
maximum crust thickness	.10
time to desic. after initial fill	120.00
month of initial desiccation	4

elevation of fixed water table .00
elevation of top of incompres. found. -62.00
==========

**********Initial Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material	
60.58	60.58	21.42	6.50	6.50	5.69	6
60.02	60.02	21.35	6.49	6.49	5.68	6
59.45	59.45	21.27	6.47	6.47	5.66	6
58.89	58.89	21.20	6.46	6.46	5.65	6
58.33	58.33	21.12	6.44	6.44	5.64	6
57.76	57.76	21.05	6.43	6.43	5.62	6
57.20	57.20	20.97	6.42	6.42	5.61	6
56.64	56.64	20.90	6.40	6.40	5.59	6
56.08	56.08	20.82	6.39	6.39	5.58	6
56.08	56.08	20.82	4.51	4.51	3.84	5
54.82	54.82	20.59	4.44	4.44	3.78	5
53.56	53.56	20.36	4.38	4.38	3.72	5
52.32	52.32	20.12	4.32	4.32	3.65	5
51.10	51.10	19.89	4.25	4.25	3.59	5
49.88	49.88	19.66	4.19	4.19	3.52	5
48.69	48.69	19.43	4.13	4.13	3.46	5
48.69	48.69	19.43	1.93	1.93	1.89	4
46.69	46.69	18.75	1.92	1.92	1.87	4
44.70	44.70	18.06	1.91	1.91	1.85	4
42.72	42.72	17.38	1.89	1.89	1.83	4
40.75	40.75	16.70	1.88	1.88	1.81	4
38.79	38.79	16.01	1.86	1.86	1.79	4
36.85	36.85	15.33	1.84	1.84	1.76	4
34.91	34.91	14.65	1.82	1.82	1.74	4
33.00	33.00	13.97	1.80	1.80	1.72	4
31.09	31.09	13.28	1.78	1.78	1.70	4
31.09	31.09	13.28	1.47	1.47	1.43	3
29.70	29.70	12.72	1.46	1.46	1.42	3
28.32	28.32	12.16	1.45	1.45	1.41	3
26.94	26.94	11.59	1.44	1.44	1.40	3
25.57	25.57	11.03	1.43	1.43	1.39	3
24.21	24.21	10.47	1.42	1.42	1.38	3
22.84	22.84	9.90	1.41	1.41	1.37	3

21.49	21.49	9.34	1.40	1.40	1.36	3
20.14	20.14	8.78	1.39	1.39	1.35	3
18.80	18.80	8.21	1.38	1.38	1.34	3
18.80	18.80	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.43	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.25	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.58	579.88	.00	579.88	312.00	267.88	6
60.02	619.83	4.62	615.21	347.33	267.88	6
59.45	659.71	9.24	650.47	382.59	267.88	6
58.89	699.52	13.86	685.66	417.78	267.88	6
58.33	739.27	18.48	720.79	452.91	267.88	6
57.76	778.96	23.10	755.86	487.98	267.88	6
57.20	818.58	27.72	790.85	522.98	267.88	6
56.64	858.13	32.34	825.79	557.91	267.88	6
56.08	897.62	36.96	860.65	592.77	267.88	6
56.08	897.62	36.96	860.65	592.77	267.88	5
54.82	1002.59	62.71	939.88	672.00	267.88	5
53.56	1106.64	88.46	1018.18	750.30	267.88	5
52.32	1209.76	114.21	1095.55	827.67	267.88	5
51.10	1311.97	139.96	1172.00	904.12	267.88	5
49.88	1413.24	165.71	1247.53	979.65	267.88	5
48.69	1513.60	191.46	1322.14	1054.26	267.88	5
48.69	1513.60	191.46	1322.14	1054.26	267.88	4
46.69	1714.04	267.32	1446.72	1178.84	267.88	4
44.70	1913.98	343.18	1570.80	1302.92	267.88	4
42.72	2113.37	419.04	1694.33	1426.46	267.88	4
40.75	2312.32	494.90	1817.42	1549.54	267.88	4
38.79	2510.52	570.76	1939.76	1671.88	267.88	4
36.85	2707.82	646.62	2061.20	1793.32	267.88	4
34.91	2904.21	722.48	2181.74	1913.86	267.88	4
33.00	3099.70	798.34	2301.37	2033.49	267.88	4
31.09	3294.29	874.19	2420.09	2152.22	267.88	4
31.09	3294.29	874.19	2420.09	2152.22	267.88	3
29.70	3442.86	936.05	2506.81	2238.93	267.88	3

28.32	3591.03	997.91	2593.12	2325.24	267.88	3
26.94	3738.84	1059.77	2679.07	2411.19	267.88	3
25.57	3886.30	1121.63	2764.67	2496.79	267.88	3
24.21	4033.41	1183.49	2849.92	2582.04	267.88	3
22.84	4180.17	1245.35	2934.82	2666.94	267.88	3
21.49	4326.58	1307.21	3019.38	2751.50	267.88	3
20.14	4472.65	1369.06	3103.59	2835.71	267.88	3
18.80	4618.37	1430.92	3187.45	2919.57	267.88	3
18.80	4618.37	1430.92	3187.45	2919.57	267.88	2
16.88	4824.04	1517.02	3307.02	3039.14	267.88	2
14.97	5029.18	1603.12	3426.06	3158.18	267.88	2
13.07	5233.79	1689.22	3544.57	3276.69	267.88	2
11.18	5437.87	1775.31	3662.55	3394.67	267.88	2
9.30	5641.42	1861.41	3780.01	3512.13	267.88	2
7.43	5844.44	1947.51	3896.93	3629.05	267.88	2
5.56	6046.94	2033.61	4013.34	3745.46	267.88	2
3.70	6249.06	2119.71	4129.36	3861.48	267.88	2
1.85	6450.83	2205.80	4245.02	3977.14	267.88	2
.00	6652.24	2291.90	4360.34	4092.46	267.88	2

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Initial Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	5.00	2.53	.98	.98	.98	1
3.75	3.75	1.89	.98	.98	.92	1
2.50	2.50	1.26	.98	.98	.91	1
1.25	1.25	.63	.98	.98	.90	1
.00	.00	.00	.98	.98	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
5.00	.00	.00	.00	.00	.00	1
3.75	144.97	.00	144.97	78.00	66.97	1
2.50	289.94	.00	289.94	156.00	133.94	1
1.25	434.91	.00	434.91	234.00	200.91	1
.00	579.88	.00	579.88	312.00	267.88	1

Time = 0. Degree of Consolidation = 0.%

Total Settlement = .000

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 0. = .000

Settlement caused by Secondary Compression at time 0. = .000

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.50	21.42	6.50	5.99	5.69	6
60.02	59.97	21.35	6.49	6.15	5.68	6
59.45	59.42	21.27	6.47	6.27	5.66	6
58.89	58.87	21.20	6.46	6.35	5.65	6
58.33	58.31	21.12	6.44	6.39	5.64	6
57.76	57.75	21.05	6.43	6.41	5.62	6
57.20	57.19	20.97	6.42	6.41	5.61	6
56.64	56.64	20.90	6.40	6.40	5.59	6
56.08	56.08	20.82	6.39	6.39	5.58	6
56.08	56.08	20.82	4.51	4.51	3.84	5
54.82	54.81	20.59	4.44	4.44	3.78	5
53.56	53.55	20.36	4.38	4.38	3.72	5
52.32	52.31	20.12	4.32	4.31	3.65	5
51.10	51.09	19.89	4.25	4.25	3.59	5
49.88	49.88	19.66	4.19	4.19	3.52	5
48.69	48.68	19.43	4.13	4.12	3.46	5
48.69	48.68	19.43	1.93	1.93	1.89	4
46.69	46.69	18.75	1.92	1.92	1.87	4

44.70	44.70	18.06	1.91	1.91	1.85	4
42.72	42.72	17.38	1.89	1.89	1.83	4
40.75	40.75	16.70	1.88	1.88	1.81	4
38.79	38.79	16.01	1.86	1.86	1.79	4
36.85	36.84	15.33	1.84	1.84	1.76	4
34.91	34.91	14.65	1.82	1.82	1.74	4
33.00	33.00	13.97	1.80	1.80	1.72	4
31.09	31.09	13.28	1.78	1.78	1.70	4
31.09	31.09	13.28	1.47	1.47	1.43	3
29.70	29.70	12.72	1.46	1.46	1.42	3
28.32	28.32	12.16	1.45	1.45	1.41	3
26.94	26.94	11.59	1.44	1.44	1.40	3
25.57	25.57	11.03	1.43	1.43	1.39	3
24.21	24.20	10.47	1.42	1.42	1.38	3
22.84	22.84	9.90	1.41	1.41	1.37	3
21.49	21.49	9.34	1.40	1.40	1.36	3
20.14	20.14	8.78	1.39	1.39	1.35	3
18.80	18.80	8.21	1.38	1.38	1.34	3
18.80	18.80	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.43	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.25	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.50	569.86	168.28	401.57	301.98	99.60	6
59.97	607.82	116.28	491.54	335.32	156.22	6
59.42	646.45	76.21	570.23	369.33	200.91	6
58.87	685.55	49.98	635.56	403.81	231.76	6
58.31	724.93	36.03	688.90	438.57	250.33	6
57.75	764.44	30.85	733.59	473.46	260.13	6
57.19	803.98	30.95	773.04	508.38	264.65	6
56.64	843.50	33.81	809.69	543.28	266.41	6
56.08	882.97	38.05	844.93	578.13	266.79	6
56.08	882.97	38.05	844.93	578.13	266.79	5
54.81	987.91	63.58	924.33	657.32	267.01	5
53.55	1091.93	89.33	1002.60	735.59	267.01	5
52.31	1195.03	115.12	1079.91	812.94	266.97	5

51.09	1297.20	140.89	1156.30	889.35	266.95	5
49.88	1398.44	166.62	1231.82	964.85	266.97	5
48.68	1498.76	192.28	1306.48	1039.42	267.06	5
48.68	1498.76	192.28	1306.48	1039.42	267.06	4
46.69	1699.20	267.32	1431.88	1164.00	267.88	4
44.70	1899.13	343.18	1555.95	1288.07	267.88	4
42.72	2098.53	421.74	1676.79	1411.61	265.18	4
40.75	2297.37	507.75	1789.62	1534.59	255.03	4
38.79	2495.49	573.59	1921.90	1656.85	265.04	4
36.84	2692.78	646.64	2046.13	1778.28	267.85	4
34.91	2889.17	722.48	2166.70	1898.82	267.88	4
33.00	3084.66	798.34	2286.33	2018.45	267.88	4
31.09	3279.25	874.20	2405.05	2137.17	267.88	4
31.09	3279.25	874.20	2405.05	2137.17	267.88	3
29.70	3427.82	936.05	2491.76	2223.88	267.88	3
28.32	3575.99	997.91	2578.08	2310.20	267.88	3
26.94	3723.79	1060.98	2662.81	2396.14	266.66	3
25.57	3871.24	1123.18	2748.07	2481.73	266.33	3
24.20	4018.34	1185.03	2833.31	2566.98	266.33	3
22.84	4165.10	1246.77	2918.33	2651.87	266.45	3
21.49	4311.51	1308.53	3002.97	2736.42	266.55	3
20.14	4457.57	1370.27	3087.30	2820.62	266.67	3
18.80	4603.28	1431.77	3171.51	2904.48	267.03	3
18.80	4603.28	1431.77	3171.51	2904.48	267.03	2
16.88	4808.95	1517.20	3291.75	3024.05	267.70	2
14.97	5014.08	1603.18	3410.91	3143.09	267.82	2
13.07	5218.69	1689.22	3529.48	3261.60	267.88	2
11.18	5422.77	1775.31	3647.46	3379.58	267.88	2
9.30	5626.33	1861.41	3764.91	3497.03	267.88	2
7.43	5829.34	1947.51	3881.83	3613.95	267.88	2
5.56	6031.85	2033.61	3998.24	3730.36	267.88	2
3.70	6233.97	2120.48	4113.48	3846.38	267.10	2
1.85	6435.73	2206.90	4228.83	3962.05	266.79	2
.00	6637.13	2296.96	4340.17	4077.35	262.82	2

Time = 30. Degree of Consolidation = 4.%

Total Settlement = .082

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 30. = .082

Settlement caused by Secondary Compression at time 30. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.84	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.41	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.84	.00	.00	.00	.00	.00	1
3.61	143.46	54.95	88.51	76.49	12.02	1
2.41	285.80	110.72	175.08	151.86	23.22	1
1.20	427.88	150.98	276.90	226.97	49.93	1
.00	569.86	168.28	401.57	301.98	99.60	1

Time = 30. Degree of Consolidation = 95.%

Total Settlement = .161

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 30. = .161

Settlement caused by Secondary Compression at time 30. = .000

Surface Elevation = 3.36

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.45	21.42	6.50	5.94	5.69	6

60.02	59.92	21.35	6.49	6.06	5.68	6
59.45	59.39	21.27	6.47	6.16	5.66	6
58.89	58.84	21.20	6.46	6.25	5.65	6
58.33	58.29	21.12	6.44	6.31	5.64	6
57.76	57.74	21.05	6.43	6.35	5.62	6
57.20	57.18	20.97	6.42	6.37	5.61	6
56.64	56.63	20.90	6.40	6.37	5.59	6
56.08	56.07	20.82	6.39	6.37	5.58	6
56.08	56.07	20.82	4.51	4.49	3.84	5
54.82	54.80	20.59	4.44	4.44	3.78	5
53.56	53.55	20.36	4.38	4.37	3.72	5
52.32	52.31	20.12	4.32	4.31	3.65	5
51.10	51.09	19.89	4.25	4.25	3.59	5
49.88	49.88	19.66	4.19	4.18	3.52	5
48.69	48.68	19.43	4.13	4.12	3.46	5
48.69	48.68	19.43	1.93	1.93	1.89	4
46.69	46.68	18.75	1.92	1.92	1.87	4
44.70	44.70	18.06	1.91	1.91	1.85	4
42.72	42.72	17.38	1.89	1.89	1.83	4
40.75	40.75	16.70	1.88	1.88	1.81	4
38.79	38.79	16.01	1.86	1.86	1.79	4
36.85	36.84	15.33	1.84	1.84	1.76	4
34.91	34.91	14.65	1.82	1.82	1.74	4
33.00	32.99	13.97	1.80	1.80	1.72	4
31.09	31.09	13.28	1.78	1.78	1.70	4
31.09	31.09	13.28	1.47	1.47	1.43	3
29.70	29.70	12.72	1.46	1.46	1.42	3
28.32	28.32	12.16	1.45	1.45	1.41	3
26.94	26.94	11.59	1.44	1.44	1.40	3
25.57	25.57	11.03	1.43	1.43	1.39	3
24.21	24.20	10.47	1.42	1.42	1.38	3
22.84	22.84	9.90	1.41	1.41	1.37	3
21.49	21.49	9.34	1.40	1.40	1.36	3
20.14	20.14	8.78	1.39	1.39	1.35	3
18.80	18.80	8.21	1.38	1.38	1.34	3
18.80	18.80	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.43	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.25	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.45	569.70	186.67	383.03	301.82	81.21	6
59.92	607.31	146.63	460.68	334.81	125.87	6
59.39	645.46	111.98	533.48	368.34	165.14	6
58.84	684.05	84.31	599.74	402.31	197.43	6
58.29	722.98	64.23	658.75	436.62	222.13	6
57.74	762.15	51.30	710.84	471.17	239.68	6
57.18	801.45	44.37	757.08	505.85	251.23	6
56.63	840.82	41.96	798.86	540.60	258.26	6
56.07	880.20	42.64	837.56	575.36	262.20	6
56.07	880.20	42.64	837.56	575.36	262.20	5
54.80	985.02	66.10	918.92	654.43	264.49	5
53.55	1088.97	90.86	998.11	732.63	265.48	5
52.31	1192.01	116.22	1075.79	809.92	265.87	5
51.09	1294.15	141.82	1152.33	886.31	266.02	5
49.88	1395.36	167.46	1227.90	961.77	266.13	5
48.68	1495.66	193.04	1302.62	1036.31	266.31	5
48.68	1495.66	193.04	1302.62	1036.31	266.31	4
46.68	1696.09	267.32	1428.77	1160.89	267.88	4
44.70	1896.02	343.57	1552.45	1284.96	267.49	4
42.72	2095.41	426.42	1668.99	1408.49	260.50	4
40.75	2294.19	512.82	1781.37	1531.41	249.96	4
38.79	2492.26	577.04	1915.21	1653.62	261.59	4
36.84	2689.52	647.56	2041.96	1775.03	266.93	4
34.91	2885.91	722.48	2163.44	1895.56	267.88	4
32.99	3081.40	798.34	2283.07	2015.19	267.88	4
31.09	3275.99	874.20	2401.79	2133.91	267.88	4
31.09	3275.99	874.20	2401.79	2133.91	267.88	3
29.70	3424.56	936.05	2488.50	2220.63	267.88	3
28.32	3572.73	997.91	2574.82	2306.94	267.88	3
26.94	3720.53	1061.83	2658.70	2392.88	265.82	3
25.57	3867.98	1124.49	2743.48	2478.47	265.01	3
24.20	4015.07	1186.45	2828.62	2563.70	264.92	3
22.84	4161.82	1248.19	2913.63	2648.59	265.04	3
21.49	4308.22	1309.82	2998.40	2733.13	265.26	3
20.14	4454.27	1371.37	3082.90	2817.33	265.57	3
18.80	4599.98	1432.62	3167.35	2901.18	266.18	3
18.80	4599.98	1432.62	3167.35	2901.18	266.18	2
16.88	4805.64	1517.54	3288.10	3020.74	267.36	2
14.97	5010.78	1603.35	3407.43	3139.78	267.65	2
13.07	5215.38	1689.22	3526.17	3258.29	267.88	2
11.18	5419.46	1775.31	3644.15	3376.27	267.88	2
9.30	5623.02	1861.41	3761.61	3493.73	267.88	2
7.43	5826.03	1947.51	3878.52	3610.64	267.88	2

5.56	6028.54	2033.61	3994.94	3727.06	267.88	2
3.70	6230.66	2121.26	4109.40	3843.07	266.33	2
1.85	6432.42	2208.42	4224.00	3958.73	265.26	2
.00	6633.81	2300.82	4332.99	4074.03	258.97	2

Time = 60. Degree of Consolidation = 6.%

Total Settlement = .132

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 60. = .132

Settlement caused by Secondary Compression at time 60. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.84	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.84	.00	.00	.00	.00	.00	1
3.61	143.44	58.19	85.26	76.48	8.78	1
2.40	285.76	120.50	165.26	151.82	13.44	1
1.20	427.79	165.10	262.68	226.88	35.81	1
.00	569.70	186.67	383.03	301.82	81.21	1

Time = 60. Degree of Consolidation = 96.%

Total Settlement = .163

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 60. = .163

Settlement caused by Secondary Compression at time 60. = .000

Surface Elevation = 3.30

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.37	21.42	6.50	5.89	5.69	6
60.02	59.85	21.35	6.49	5.97	5.68	6
59.45	59.32	21.27	6.47	6.06	5.66	6
58.89	58.78	21.20	6.46	6.13	5.65	6
58.33	58.24	21.12	6.44	6.19	5.64	6
57.76	57.69	21.05	6.43	6.24	5.62	6
57.20	57.14	20.97	6.42	6.28	5.61	6
56.64	56.59	20.90	6.40	6.31	5.59	6
56.08	56.04	20.82	6.39	6.33	5.58	6
56.08	56.04	20.82	4.51	4.46	3.84	5
54.82	54.78	20.59	4.44	4.41	3.78	5
53.56	53.53	20.36	4.38	4.36	3.72	5
52.32	52.30	20.12	4.32	4.30	3.65	5
51.10	51.08	19.89	4.25	4.24	3.59	5
49.88	49.87	19.66	4.19	4.18	3.52	5
48.69	48.68	19.43	4.13	4.11	3.46	5
48.69	48.68	19.43	1.93	1.93	1.89	4
46.69	46.68	18.75	1.92	1.92	1.87	4
44.70	44.69	18.06	1.91	1.90	1.85	4
42.72	42.71	17.38	1.89	1.89	1.83	4
40.75	40.74	16.70	1.88	1.87	1.81	4
38.79	38.79	16.01	1.86	1.86	1.79	4
36.85	36.84	15.33	1.84	1.84	1.76	4
34.91	34.91	14.65	1.82	1.82	1.74	4
33.00	32.99	13.97	1.80	1.80	1.72	4
31.09	31.09	13.28	1.78	1.78	1.70	4
31.09	31.09	13.28	1.47	1.47	1.43	3
29.70	29.70	12.72	1.46	1.46	1.42	3
28.32	28.32	12.16	1.45	1.45	1.41	3
26.94	26.94	11.59	1.44	1.44	1.40	3
25.57	25.57	11.03	1.43	1.43	1.39	3

24.21	24.20	10.47	1.42	1.42	1.38	3
22.84	22.84	9.90	1.41	1.41	1.37	3
21.49	21.49	9.34	1.40	1.40	1.36	3
20.14	20.14	8.78	1.39	1.39	1.35	3
18.80	18.79	8.21	1.38	1.38	1.34	3
18.80	18.79	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.43	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.25	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.37	569.57	203.47	366.10	301.69	64.41	6
59.85	606.87	174.13	432.74	334.37	98.37	6
59.32	644.56	146.97	497.59	367.44	130.14	6
58.78	682.63	122.85	559.77	400.89	158.89	6
58.24	721.01	102.36	618.65	434.65	184.00	6
57.69	759.65	85.76	673.90	468.67	205.23	6
57.14	798.51	72.98	725.53	502.91	222.62	6
56.59	837.52	63.68	773.84	537.30	236.54	6
56.04	876.64	57.26	819.38	571.80	247.58	6
56.04	876.64	57.26	819.38	571.80	247.58	5
54.78	981.01	76.48	904.53	650.42	254.11	5
53.53	1084.65	97.97	986.68	728.31	258.37	5
52.30	1187.49	121.09	1066.39	805.39	261.00	5
51.08	1289.47	145.30	1144.17	881.63	262.54	5
49.87	1390.57	170.22	1220.35	956.98	263.37	5
48.68	1490.77	195.64	1295.13	1031.43	263.70	5
48.68	1490.77	195.64	1295.13	1031.43	263.70	4
46.68	1691.20	268.60	1422.60	1156.00	266.60	4
44.69	1891.11	347.11	1544.00	1280.05	263.95	4
42.71	2090.46	433.99	1656.47	1403.54	252.93	4
40.74	2289.18	518.98	1770.20	1526.40	243.80	4
38.79	2487.18	582.40	1904.78	1648.54	256.24	4
36.84	2684.39	650.38	2034.01	1769.89	264.12	4
34.91	2880.77	722.58	2158.18	1890.41	267.77	4
32.99	3076.26	798.34	2277.92	2010.04	267.88	4
31.09	3270.84	874.20	2396.65	2128.77	267.88	4

31.09	3270.84	874.20	2396.65	2128.77	267.88	3
29.70	3419.41	936.05	2483.36	2215.48	267.88	3
28.32	3567.58	997.91	2569.67	2301.79	267.88	3
26.94	3715.38	1063.07	2652.31	2387.73	264.58	3
25.57	3862.82	1126.63	2736.19	2473.31	262.88	3
24.20	4009.90	1189.02	2820.88	2558.53	262.35	3
22.84	4156.63	1250.83	2905.80	2643.40	262.40	3
21.49	4303.01	1312.26	2990.76	2727.93	262.83	3
20.14	4449.06	1373.45	3075.60	2812.11	263.49	3
18.79	4594.75	1434.28	3160.47	2895.95	264.52	3
18.79	4594.75	1434.28	3160.47	2895.95	264.52	2
16.88	4800.41	1518.37	3282.04	3015.51	266.53	2
14.97	5005.54	1603.69	3401.85	3134.54	267.30	2
13.07	5210.15	1689.36	3520.79	3253.05	267.74	2
11.18	5414.23	1775.31	3638.91	3371.03	267.88	2
9.30	5617.78	1861.41	3756.37	3488.49	267.88	2
7.43	5820.80	1947.51	3873.29	3605.41	267.88	2
5.56	6023.31	2033.61	3989.70	3721.82	267.88	2
3.70	6225.42	2122.81	4102.61	3837.83	264.78	2
1.85	6427.17	2212.03	4215.13	3953.48	261.65	2
.00	6628.54	2306.63	4321.90	4068.76	253.15	2

Time = 120. Degree of Consolidation = 9.%

Total Settlement = .215

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 120. = .215

Settlement caused by Secondary Compression at time 120. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.43	60.63	82.81	76.46	6.34	1
2.40	285.72	128.00	157.72	151.78	5.94	1
1.20	427.71	176.33	251.38	226.80	24.58	1
.00	569.57	203.47	366.10	301.69	64.41	1

Time = 120. Degree of Consolidation = 97.%

Total Settlement = .165

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 120. = .165

Settlement caused by Secondary Compression at time 120. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.22

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.24	21.42	6.50	5.85	5.69	6
60.02	59.72	21.35	6.49	5.91	5.68	6
59.45	59.20	21.27	6.47	5.97	5.66	6
58.89	58.67	21.20	6.46	6.03	5.65	6
58.33	58.13	21.12	6.44	6.08	5.64	6
57.76	57.60	21.05	6.43	6.13	5.62	6
57.20	57.06	20.97	6.42	6.17	5.61	6
56.64	56.51	20.90	6.40	6.21	5.59	6
56.08	55.97	20.82	6.39	6.25	5.58	6
56.08	55.97	20.82	4.51	4.39	3.84	5
54.82	54.72	20.59	4.44	4.35	3.78	5
53.56	53.48	20.36	4.38	4.31	3.72	5

52.32	52.26	20.12	4.32	4.26	3.65	5
51.10	51.05	19.89	4.25	4.20	3.59	5
49.88	49.85	19.66	4.19	4.14	3.52	5
48.69	48.66	19.43	4.13	4.08	3.46	5
48.69	48.66	19.43	1.93	1.93	1.89	4
46.69	46.67	18.75	1.92	1.92	1.87	4
44.70	44.68	18.06	1.91	1.90	1.85	4
42.72	42.70	17.38	1.89	1.89	1.83	4
40.75	40.74	16.70	1.88	1.87	1.81	4
38.79	38.78	16.01	1.86	1.85	1.79	4
36.85	36.84	15.33	1.84	1.84	1.76	4
34.91	34.91	14.65	1.82	1.82	1.74	4
33.00	32.99	13.97	1.80	1.80	1.72	4
31.09	31.09	13.28	1.78	1.78	1.70	4
31.09	31.09	13.28	1.47	1.47	1.43	3
29.70	29.70	12.72	1.46	1.46	1.42	3
28.32	28.31	12.16	1.45	1.45	1.41	3
26.94	26.94	11.59	1.44	1.44	1.40	3
25.57	25.56	11.03	1.43	1.43	1.39	3
24.21	24.20	10.47	1.42	1.42	1.38	3
22.84	22.84	9.90	1.41	1.41	1.37	3
21.49	21.49	9.34	1.40	1.40	1.36	3
20.14	20.14	8.78	1.39	1.39	1.35	3
18.80	18.79	8.21	1.38	1.38	1.34	3
18.80	18.79	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.24	569.30	214.36	354.94	301.42	53.52	6
59.72	606.37	194.44	411.93	333.87	78.06	6
59.20	643.72	174.87	468.85	366.60	102.25	6
58.67	681.35	156.08	525.26	399.61	125.65	6
58.13	719.23	138.46	580.77	432.87	147.90	6
57.60	757.36	122.27	635.09	466.38	168.71	6
57.06	795.70	107.69	688.01	500.10	187.91	6

56.51	834.24	94.79	739.45	534.02	205.43	6
55.97	872.96	83.56	789.39	568.12	221.28	6
55.97	872.96	83.56	789.39	568.12	221.28	5
54.72	976.44	99.75	876.68	645.84	230.84	5
53.48	1079.30	118.06	961.24	722.95	238.28	5
52.26	1181.46	138.32	1043.14	799.37	243.77	5
51.05	1282.87	160.36	1122.52	875.03	247.49	5
49.85	1383.46	184.02	1199.45	949.87	249.58	5
48.66	1483.17	209.19	1273.99	1023.83	250.15	5
48.66	1483.17	209.19	1273.99	1023.83	250.15	4
46.67	1683.52	279.97	1403.55	1148.32	255.23	4
44.68	1883.35	358.34	1525.01	1272.29	252.72	4
42.70	2082.62	446.75	1635.87	1395.70	240.17	4
40.74	2281.25	526.93	1754.31	1518.47	235.85	4
38.78	2479.15	589.52	1889.63	1640.52	249.12	4
36.84	2676.29	655.44	2020.85	1761.79	259.06	4
34.91	2872.62	724.98	2147.65	1882.27	265.38	4
32.99	3068.10	798.34	2269.77	2001.89	267.88	4
31.09	3262.69	874.20	2388.49	2120.61	267.88	4
31.09	3262.69	874.20	2388.49	2120.61	267.88	3
29.70	3411.26	936.05	2475.20	2207.32	267.88	3
28.31	3559.43	997.91	2561.52	2293.64	267.88	3
26.94	3707.23	1064.80	2642.43	2379.58	262.85	3
25.56	3854.65	1129.71	2724.94	2465.14	259.80	3
24.20	4001.71	1193.03	2808.68	2550.34	258.34	3
22.84	4148.42	1255.22	2893.19	2635.19	258.00	3
21.49	4294.78	1316.60	2978.17	2719.69	258.48	3
20.14	4440.79	1377.34	3063.45	2803.85	259.60	3
18.79	4586.47	1437.57	3148.90	2887.67	261.24	3
18.79	4586.47	1437.57	3148.90	2887.67	261.24	2
16.88	4792.11	1520.43	3271.67	3007.21	264.47	2
14.97	4997.23	1604.78	3392.45	3126.23	266.22	2
13.07	5201.83	1689.91	3511.93	3244.74	267.19	2
11.18	5405.91	1775.38	3630.53	3362.72	267.81	2
9.30	5609.47	1861.41	3748.05	3480.17	267.88	2
7.42	5812.48	1947.51	3864.97	3597.09	267.88	2
5.56	6014.99	2033.61	3981.39	3713.51	267.88	2
3.70	6217.10	2125.91	4091.19	3829.51	261.68	2
1.85	6418.83	2218.37	4200.46	3945.14	255.32	2
.00	6620.17	2314.69	4305.47	4060.39	245.09	2

Time = 240. Degree of Consolidation = 15.%

Total Settlement = .344

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 240. = .344

Settlement caused by Secondary Compression at time 240. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 240. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 240. = .169

Settlement caused by Secondary Compression at time 240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 3.09

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	60.13	21.42	6.50	5.82	5.69	6
60.02	59.61	21.35	6.49	5.87	5.68	6
59.45	59.09	21.27	6.47	5.93	5.66	6
58.89	58.56	21.20	6.46	5.98	5.65	6
58.33	58.03	21.12	6.44	6.02	5.64	6
57.76	57.50	21.05	6.43	6.07	5.62	6
57.20	56.97	20.97	6.42	6.11	5.61	6
56.64	56.43	20.90	6.40	6.15	5.59	6
56.08	55.89	20.82	6.39	6.18	5.58	6
56.08	55.89	20.82	4.51	4.34	3.84	5
54.82	54.65	20.59	4.44	4.30	3.78	5
53.56	53.43	20.36	4.38	4.26	3.72	5
52.32	52.21	20.12	4.32	4.21	3.65	5
51.10	51.01	19.89	4.25	4.16	3.59	5
49.88	49.82	19.66	4.19	4.10	3.52	5
48.69	48.65	19.43	4.13	4.04	3.46	5
48.69	48.65	19.43	1.93	1.92	1.89	4
46.69	46.66	18.75	1.92	1.91	1.87	4
44.70	44.67	18.06	1.91	1.90	1.85	4
42.72	42.70	17.38	1.89	1.89	1.83	4
40.75	40.73	16.70	1.88	1.87	1.81	4
38.79	38.78	16.01	1.86	1.85	1.79	4
36.85	36.83	15.33	1.84	1.84	1.76	4
34.91	34.90	14.65	1.82	1.82	1.74	4
33.00	32.99	13.97	1.80	1.80	1.72	4
31.09	31.08	13.28	1.78	1.78	1.70	4
31.09	31.08	13.28	1.47	1.47	1.43	3
29.70	29.69	12.72	1.46	1.46	1.42	3
28.32	28.31	12.16	1.45	1.45	1.41	3
26.94	26.93	11.59	1.44	1.44	1.40	3
25.57	25.56	11.03	1.43	1.43	1.39	3
24.21	24.20	10.47	1.42	1.42	1.38	3
22.84	22.84	9.90	1.41	1.41	1.37	3
21.49	21.48	9.34	1.40	1.40	1.36	3
20.14	20.14	8.78	1.39	1.39	1.35	3
18.80	18.79	8.21	1.38	1.38	1.34	3
18.80	18.79	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2

11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
60.13	569.30	225.47	343.82	301.42	42.40	6
59.61	606.20	207.63	398.56	333.70	64.87	6
59.09	643.34	190.24	453.11	366.22	86.88	6
58.56	680.74	173.47	507.27	399.00	108.27	6
58.03	718.36	157.51	560.85	432.00	128.85	6
57.50	756.21	142.51	613.69	465.23	148.47	6
56.97	794.26	128.61	665.65	498.66	166.99	6
56.43	832.50	115.91	716.59	532.28	184.31	6
55.89	870.91	104.49	766.42	566.07	200.35	6
55.89	870.91	104.49	766.42	566.07	200.35	5
54.65	973.64	120.44	853.21	643.05	210.15	5
53.43	1075.77	138.25	937.52	719.43	218.09	5
52.21	1177.22	157.92	1019.30	795.13	224.17	5
51.01	1277.94	179.39	1098.55	870.10	228.45	5
49.82	1377.85	202.62	1175.23	944.26	230.97	5
48.65	1476.90	227.55	1249.36	1017.56	231.79	5
48.65	1476.90	227.55	1249.36	1017.56	231.79	4
46.66	1677.13	296.14	1380.99	1141.93	239.06	4
44.67	1876.86	372.87	1503.99	1265.80	238.19	4
42.70	2076.03	460.28	1615.75	1389.11	226.63	4
40.73	2274.57	534.01	1740.56	1511.79	228.77	4
38.78	2472.40	595.31	1877.09	1633.76	243.33	4
36.83	2669.48	659.69	2009.78	1754.98	254.80	4
34.90	2865.77	727.38	2138.39	1875.41	262.97	4
32.99	3061.23	798.67	2262.56	1995.02	267.54	4
31.08	3255.82	874.36	2381.46	2113.75	267.72	4
31.08	3255.82	874.36	2381.46	2113.75	267.72	3
29.69	3404.39	936.05	2468.33	2200.46	267.88	3
28.31	3552.57	997.91	2554.65	2286.77	267.88	3
26.93	3700.35	1065.97	2634.38	2372.70	261.68	3
25.56	3847.76	1131.97	2715.79	2458.26	257.54	3
24.20	3994.81	1196.01	2798.81	2543.44	255.36	3
22.84	4141.50	1258.62	2882.88	2628.27	254.60	3
21.48	4287.84	1320.07	2967.77	2712.76	255.01	3
20.14	4433.84	1380.66	3053.18	2796.90	256.28	3

18.79	4579.50	1440.46	3139.04	2880.70	258.34	3
18.79	4579.50	1440.46	3139.04	2880.70	258.34	2
16.88	4785.12	1522.50	3262.62	3000.22	262.40	2
14.97	4990.23	1606.16	3384.08	3119.24	264.84	2
13.07	5194.83	1690.59	3504.24	3237.73	266.50	2
11.18	5398.90	1775.74	3623.17	3355.71	267.46	2
9.30	5602.46	1861.41	3741.05	3473.17	267.88	2
7.42	5805.47	1947.51	3857.96	3590.08	267.88	2
5.56	6007.99	2033.61	3974.38	3706.50	267.88	2
3.70	6210.09	2129.01	4081.08	3822.50	258.58	2
1.85	6411.80	2223.62	4188.18	3938.11	250.06	2
.00	6613.12	2320.42	4292.70	4053.33	239.36	2

Time = 360. Degree of Consolidation = 20.%

Total Settlement = .457

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 360. = .457

Settlement caused by Secondary Compression at time 360. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1

.00 569.30 267.88 301.42 301.42 .00 1

Time = 360. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 360. = .169

Settlement caused by Secondary Compression at time 360. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.97

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.98	21.42	6.50	5.80	5.69	6
60.02	59.46	21.35	6.49	5.85	5.68	6
59.45	58.94	21.27	6.47	5.89	5.66	6
58.89	58.42	21.20	6.46	5.93	5.65	6
58.33	57.90	21.12	6.44	5.97	5.64	6
57.76	57.37	21.05	6.43	6.01	5.62	6
57.20	56.84	20.97	6.42	6.04	5.61	6
56.64	56.31	20.90	6.40	6.07	5.59	6
56.08	55.77	20.82	6.39	6.10	5.58	6
56.08	55.77	20.82	4.51	4.28	3.84	5
54.82	54.55	20.59	4.44	4.23	3.78	5
53.56	53.34	20.36	4.38	4.19	3.72	5
52.32	52.15	20.12	4.32	4.14	3.65	5
51.10	50.96	19.89	4.25	4.09	3.59	5
49.88	49.79	19.66	4.19	4.03	3.52	5
48.69	48.63	19.43	4.13	3.97	3.46	5
48.69	48.63	19.43	1.93	1.92	1.89	4
46.69	46.64	18.75	1.92	1.91	1.87	4
44.70	44.66	18.06	1.91	1.90	1.85	4
42.72	42.68	17.38	1.89	1.88	1.83	4
40.75	40.72	16.70	1.88	1.87	1.81	4

38.79	38.77	16.01	1.86	1.85	1.79	4
36.85	36.83	15.33	1.84	1.83	1.76	4
34.91	34.90	14.65	1.82	1.82	1.74	4
33.00	32.98	13.97	1.80	1.80	1.72	4
31.09	31.08	13.28	1.78	1.77	1.70	4
31.09	31.08	13.28	1.47	1.47	1.43	3
29.70	29.69	12.72	1.46	1.46	1.42	3
28.32	28.31	12.16	1.45	1.45	1.41	3
26.94	26.93	11.59	1.44	1.44	1.40	3
25.57	25.56	11.03	1.43	1.43	1.39	3
24.21	24.19	10.47	1.42	1.42	1.38	3
22.84	22.83	9.90	1.41	1.41	1.37	3
21.49	21.48	9.34	1.40	1.40	1.36	3
20.14	20.13	8.78	1.39	1.39	1.35	3
18.80	18.79	8.21	1.38	1.38	1.34	3
18.80	18.79	8.21	1.34	1.34	1.31	2
16.88	16.88	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
59.98	569.30	231.26	338.03	301.42	36.61	6
59.46	606.09	216.83	389.25	333.59	55.66	6
58.94	643.08	202.70	440.39	365.96	74.42	6
58.42	680.27	188.97	491.30	398.53	92.77	6
57.90	717.66	175.80	541.86	431.30	110.56	6
57.37	755.23	163.29	591.93	464.24	127.69	6
56.84	792.96	151.58	641.39	497.36	144.02	6
56.31	830.86	140.76	690.10	530.64	159.46	6
55.77	868.91	130.97	737.94	564.07	173.87	6
55.77	868.91	130.97	737.94	564.07	173.87	5
54.55	970.68	147.75	822.93	640.09	182.84	5
53.34	1071.81	166.09	905.73	715.47	190.25	5
52.15	1172.26	186.02	986.24	790.17	196.07	5
50.96	1271.97	207.55	1064.42	864.13	200.29	5
49.79	1370.88	230.68	1140.19	937.28	202.91	5
48.63	1468.92	255.38	1213.54	1009.58	203.96	5

48.63	1468.92	255.38	1213.54	1009.58	203.96	4
46.64	1668.97	321.87	1347.10	1133.77	213.33	4
44.66	1868.53	396.62	1471.91	1257.47	214.44	4
42.68	2067.55	482.35	1585.19	1380.63	204.57	4
40.72	2265.94	545.19	1720.75	1503.16	217.59	4
38.77	2463.65	604.24	1859.41	1625.01	234.40	4
36.83	2660.63	666.43	1994.20	1746.14	248.06	4
34.90	2856.86	732.04	2124.81	1866.50	258.31	4
32.98	3052.27	801.51	2250.76	1986.06	264.70	4
31.08	3246.84	875.73	2371.11	2104.76	266.35	4
31.08	3246.84	875.73	2371.11	2104.76	266.35	3
29.69	3395.40	936.05	2459.35	2191.47	267.88	3
28.31	3543.58	997.91	2545.67	2277.79	267.88	3
26.93	3691.36	1067.35	2624.02	2363.72	260.30	3
25.56	3838.77	1134.48	2704.28	2449.26	255.02	3
24.19	3985.79	1199.40	2786.39	2534.43	251.97	3
22.83	4132.46	1262.56	2869.90	2619.24	250.66	3
21.48	4278.78	1324.27	2954.52	2703.70	250.82	3
20.13	4424.76	1384.78	3039.97	2787.81	252.16	3
18.79	4570.39	1444.24	3126.15	2871.59	254.56	3
18.79	4570.39	1444.24	3126.15	2871.59	254.56	2
16.88	4775.99	1525.60	3250.40	2991.09	259.30	2
14.97	4981.09	1608.22	3372.87	3110.09	262.77	2
13.07	5185.68	1691.82	3493.86	3228.58	265.27	2
11.18	5389.75	1776.43	3613.32	3346.55	266.77	2
9.30	5593.30	1861.55	3731.75	3464.01	267.74	2
7.42	5796.31	1947.51	3848.80	3580.92	267.88	2
5.56	5998.83	2033.61	3965.22	3697.34	267.88	2
3.70	6200.92	2132.26	4068.66	3813.34	255.32	2
1.85	6402.61	2229.38	4173.23	3928.93	244.30	2
.00	6603.91	2326.99	4276.91	4044.12	232.79	2

Time = 540. Degree of Consolidation = 27.%

Total Settlement = .605

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 540. = .605

Settlement caused by Secondary Compression at time 540. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 540. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 540. = .169

Settlement caused by Secondary Compression at time 540. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.83

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.85	21.42	6.50	5.79	5.69	6
60.02	59.33	21.35	6.49	5.82	5.68	6

59.45	58.82	21.27	6.47	5.86	5.66	6
58.89	58.30	21.20	6.46	5.89	5.65	6
58.33	57.78	21.12	6.44	5.93	5.64	6
57.76	57.25	21.05	6.43	5.96	5.62	6
57.20	56.72	20.97	6.42	5.99	5.61	6
56.64	56.20	20.90	6.40	6.01	5.59	6
56.08	55.66	20.82	6.39	6.04	5.58	6
56.08	55.66	20.82	4.51	4.22	3.84	5
54.82	54.46	20.59	4.44	4.17	3.78	5
53.56	53.27	20.36	4.38	4.13	3.72	5
52.32	52.08	20.12	4.32	4.08	3.65	5
51.10	50.91	19.89	4.25	4.02	3.59	5
49.88	49.75	19.66	4.19	3.96	3.52	5
48.69	48.61	19.43	4.13	3.90	3.46	5
48.69	48.61	19.43	1.93	1.92	1.89	4
46.69	46.62	18.75	1.92	1.90	1.87	4
44.70	44.64	18.06	1.91	1.89	1.85	4
42.72	42.67	17.38	1.89	1.88	1.83	4
40.75	40.71	16.70	1.88	1.86	1.81	4
38.79	38.76	16.01	1.86	1.85	1.79	4
36.85	36.82	15.33	1.84	1.83	1.76	4
34.91	34.89	14.65	1.82	1.81	1.74	4
33.00	32.98	13.97	1.80	1.79	1.72	4
31.09	31.08	13.28	1.78	1.77	1.70	4
31.09	31.08	13.28	1.47	1.47	1.43	3
29.70	29.69	12.72	1.46	1.46	1.42	3
28.32	28.30	12.16	1.45	1.45	1.41	3
26.94	26.93	11.59	1.44	1.44	1.40	3
25.57	25.56	11.03	1.43	1.43	1.39	3
24.21	24.19	10.47	1.42	1.42	1.38	3
22.84	22.83	9.90	1.41	1.41	1.37	3
21.49	21.48	9.34	1.40	1.40	1.36	3
20.14	20.13	8.78	1.39	1.39	1.35	3
18.80	18.79	8.21	1.38	1.38	1.34	3
18.80	18.79	8.21	1.34	1.34	1.31	2
16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.85	569.30	235.69	333.60	301.42	32.19	6
59.33	606.00	223.79	382.21	333.51	48.71	6
58.82	642.88	212.15	430.73	365.76	64.97	6
58.30	679.92	200.88	479.04	398.18	80.86	6
57.78	717.12	190.08	527.04	430.76	96.28	6
57.25	754.47	179.85	574.61	463.49	111.13	6
56.72	791.96	170.31	621.64	496.35	125.29	6
56.20	829.57	161.55	668.02	529.35	138.67	6
55.66	867.31	153.67	713.64	562.47	151.17	6
55.66	867.31	153.67	713.64	562.47	151.17	5
54.46	968.24	171.53	796.71	637.65	159.06	5
53.27	1068.51	190.70	877.81	712.17	165.64	5
52.08	1168.07	211.21	956.86	785.98	170.89	5
50.91	1266.86	233.08	1033.78	859.02	174.76	5
49.75	1364.85	256.32	1108.53	931.26	177.27	5
48.61	1461.98	280.91	1181.07	1002.64	178.43	5
48.61	1461.98	280.91	1181.07	1002.64	178.43	4
46.62	1661.85	346.44	1315.41	1126.65	188.77	4
44.64	1861.25	420.09	1441.16	1250.19	190.97	4
42.67	2060.11	502.75	1557.36	1373.19	184.17	4
40.71	2258.35	556.77	1701.59	1495.58	206.01	4
38.76	2455.94	613.81	1842.13	1617.30	224.83	4
36.82	2652.82	674.01	1978.81	1738.32	240.49	4
34.89	2848.97	737.67	2111.30	1858.61	252.69	4
32.98	3044.33	805.29	2239.04	1978.11	260.93	4
31.08	3238.85	877.76	2361.10	2096.78	264.32	4
31.08	3238.85	877.75	2361.10	2096.78	264.32	3
29.69	3387.41	936.47	2450.95	2183.48	267.46	3
28.30	3535.59	998.26	2537.33	2269.80	267.53	3
26.93	3683.37	1068.45	2614.92	2355.72	259.20	3
25.56	3830.76	1136.32	2694.44	2441.25	253.19	3
24.19	3977.78	1201.91	2775.87	2526.41	249.46	3
22.83	4124.43	1265.57	2858.86	2611.21	247.65	3
21.48	4270.73	1327.56	2943.18	2695.65	247.53	3
20.13	4416.69	1388.07	3028.61	2779.75	248.87	3
18.79	4562.31	1447.31	3115.00	2863.51	251.50	3
18.79	4562.31	1447.31	3115.00	2863.51	251.50	2
16.87	4767.89	1528.23	3239.66	2982.99	256.67	2
14.97	4972.97	1610.29	3362.69	3101.98	260.71	2
13.07	5177.55	1693.38	3484.17	3220.45	263.71	2
11.18	5381.61	1777.46	3604.15	3338.42	265.73	2
9.30	5585.16	1862.08	3723.08	3455.87	267.21	2
7.42	5788.17	1947.51	3840.66	3572.78	267.88	2
5.56	5990.69	2033.61	3957.08	3689.20	267.88	2

3.70	6192.78	2135.03	4057.75	3805.19	252.56	2
1.85	6394.45	2233.81	4160.65	3920.77	239.88	2
.00	6595.73	2331.64	4264.08	4035.94	228.14	2

Time = 720. Degree of Consolidation = 33.%

Total Settlement = .736

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 720. = .736

Settlement caused by Secondary Compression at time 720. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.90	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.30	267.88	301.42	301.42	.00	1

Time = 720. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 720. = .169

Settlement caused by Secondary Compression at time 720. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.69

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.62	21.42	6.50	5.77	5.69	6
60.02	59.11	21.35	6.49	5.79	5.68	6
59.45	58.59	21.27	6.47	5.81	5.66	6
58.89	58.08	21.20	6.46	5.83	5.65	6
58.33	57.56	21.12	6.44	5.85	5.64	6
57.76	57.04	21.05	6.43	5.87	5.62	6
57.20	56.52	20.97	6.42	5.89	5.61	6
56.64	56.00	20.90	6.40	5.91	5.59	6
56.08	55.48	20.82	6.39	5.92	5.58	6
56.08	55.48	20.82	4.51	4.13	3.84	5
54.82	54.30	20.59	4.44	4.08	3.78	5
53.56	53.13	20.36	4.38	4.02	3.72	5
52.32	51.97	20.12	4.32	3.97	3.65	5
51.10	50.82	19.89	4.25	3.91	3.59	5
49.88	49.69	19.66	4.19	3.86	3.52	5
48.69	48.57	19.43	4.13	3.79	3.46	5
48.69	48.57	19.43	1.93	1.91	1.89	4
46.69	46.59	18.75	1.92	1.90	1.87	4
44.70	44.61	18.06	1.91	1.89	1.85	4
42.72	42.65	17.38	1.89	1.87	1.83	4
40.75	40.69	16.70	1.88	1.86	1.81	4
38.79	38.74	16.01	1.86	1.84	1.79	4
36.85	36.81	15.33	1.84	1.83	1.76	4
34.91	34.88	14.65	1.82	1.81	1.74	4
33.00	32.97	13.97	1.80	1.79	1.72	4
31.09	31.07	13.28	1.78	1.77	1.70	4
31.09	31.07	13.28	1.47	1.47	1.43	3
29.70	29.68	12.72	1.46	1.46	1.42	3
28.32	28.30	12.16	1.45	1.45	1.41	3
26.94	26.92	11.59	1.44	1.44	1.40	3

25.57	25.55	11.03	1.43	1.43	1.39	3
24.21	24.19	10.47	1.42	1.42	1.38	3
22.84	22.83	9.90	1.41	1.41	1.37	3
21.49	21.48	9.34	1.40	1.40	1.36	3
20.14	20.13	8.78	1.39	1.39	1.35	3
18.80	18.79	8.21	1.38	1.38	1.34	3
18.80	18.79	8.21	1.34	1.34	1.31	2
16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.97	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.30	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.62	569.29	243.22	326.07	301.41	24.66	6
59.11	605.87	235.40	370.47	333.37	37.10	6
58.59	642.55	227.80	414.75	365.43	49.32	6
58.08	679.34	220.51	458.83	397.60	61.23	6
57.56	716.23	213.60	502.63	429.87	72.76	6
57.04	753.21	207.17	546.04	462.23	83.81	6
56.52	790.29	201.29	589.00	494.69	94.31	6
56.00	827.44	196.03	631.41	527.22	104.19	6
55.48	864.66	191.47	673.19	559.82	113.37	6
55.48	864.66	191.47	673.19	559.82	113.37	5
54.30	964.20	211.28	752.92	633.61	119.31	5
53.13	1063.01	232.01	831.00	706.67	124.33	5
51.97	1161.07	253.71	907.36	778.97	128.38	5
50.82	1258.32	276.38	981.94	850.48	131.46	5
49.69	1354.75	300.03	1054.72	921.15	133.56	5
48.57	1450.30	324.65	1125.65	990.96	134.69	5
48.57	1450.30	324.65	1125.65	990.96	134.69	4
46.59	1649.88	390.45	1259.42	1114.68	144.75	4
44.61	1848.98	464.49	1384.48	1237.92	146.57	4
42.65	2047.54	527.27	1520.26	1360.62	159.65	4
40.69	2245.50	578.69	1666.82	1482.73	184.09	4
38.74	2442.84	632.95	1809.89	1604.20	205.69	4
36.81	2639.51	690.31	1949.20	1725.02	224.19	4
34.88	2835.48	751.17	2084.31	1845.13	239.18	4
32.97	3030.70	816.30	2214.40	1964.48	249.92	4

31.07	3225.10	886.91	2338.20	2083.03	255.17	4
31.07	3225.10	886.91	2338.20	2083.03	255.17	3
29.68	3373.61	943.87	2429.74	2169.68	260.06	3
28.30	3521.75	1004.83	2516.92	2255.96	260.96	3
26.92	3669.49	1074.15	2595.34	2341.84	253.50	3
25.55	3816.85	1141.44	2675.42	2427.35	248.07	3
24.19	3963.84	1206.89	2756.95	2512.47	244.48	3
22.83	4110.47	1270.49	2839.98	2597.24	242.73	3
21.48	4256.74	1332.42	2924.32	2681.66	242.66	3
20.13	4402.67	1392.86	3009.81	2765.73	244.08	3
18.79	4548.26	1451.90	3096.36	2849.46	246.90	3
18.79	4548.26	1451.90	3096.36	2849.46	246.90	2
16.87	4753.82	1532.51	3221.31	2968.92	252.39	2
14.97	4958.88	1614.08	3344.80	3087.88	256.92	2
13.07	5163.43	1696.31	3467.12	3206.33	260.78	2
11.18	5367.48	1779.51	3587.97	3324.28	263.69	2
9.30	5571.01	1863.13	3707.88	3441.72	266.16	2
7.42	5774.02	1947.51	3826.51	3558.63	267.88	2
5.56	5976.54	2033.61	3942.94	3675.06	267.88	2
3.70	6178.62	2138.17	4040.45	3791.04	249.42	2
1.85	6380.28	2238.97	4141.31	3906.60	234.72	2
.00	6581.53	2337.31	4244.22	4021.75	222.47	2

Time = 1080. Degree of Consolidation = 43.%

Total Settlement = .964

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 1080. = .964

Settlement caused by Secondary Compression at time 1080. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1

.00	.00	.00	.98	.89	.90	1

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.42	301.42	.00	1

Time = 1080. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 1080. = .169

Settlement caused by Secondary Compression at time 1080. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.47

**********Current Conditions in Compressible Foundation**********

	***** Coordinates *****		***** Void Ratios *****			
A	XI	Z	Einitial	E	Eeop	Material
60.58	59.43	21.42	6.50	5.75	5.69	6
60.02	58.92	21.35	6.49	5.76	5.68	6
59.45	58.41	21.27	6.47	5.77	5.66	6
58.89	57.90	21.20	6.46	5.79	5.65	6
58.33	57.38	21.12	6.44	5.80	5.64	6
57.76	56.87	21.05	6.43	5.81	5.62	6
57.20	56.35	20.97	6.42	5.82	5.61	6
56.64	55.84	20.90	6.40	5.82	5.59	6
56.08	55.32	20.82	6.39	5.83	5.58	6
56.08	55.32	20.82	4.51	4.05	3.84	5
54.82	54.16	20.59	4.44	4.00	3.78	5

53.56	53.01	20.36	4.38	3.94	3.72	5
52.32	51.87	20.12	4.32	3.89	3.65	5
51.10	50.74	19.89	4.25	3.83	3.59	5
49.88	49.63	19.66	4.19	3.77	3.52	5
48.69	48.53	19.43	4.13	3.71	3.46	5
48.69	48.53	19.43	1.93	1.90	1.89	4
46.69	46.55	18.75	1.92	1.89	1.87	4
44.70	44.58	18.06	1.91	1.88	1.85	4
42.72	42.62	17.38	1.89	1.87	1.83	4
40.75	40.67	16.70	1.88	1.85	1.81	4
38.79	38.72	16.01	1.86	1.84	1.79	4
36.85	36.79	15.33	1.84	1.82	1.76	4
34.91	34.87	14.65	1.82	1.81	1.74	4
33.00	32.96	13.97	1.80	1.79	1.72	4
31.09	31.06	13.28	1.78	1.77	1.70	4
31.09	31.06	13.28	1.47	1.47	1.43	3
29.70	29.67	12.72	1.46	1.46	1.42	3
28.32	28.29	12.16	1.45	1.45	1.41	3
26.94	26.92	11.59	1.44	1.44	1.40	3
25.57	25.55	11.03	1.43	1.43	1.39	3
24.21	24.18	10.47	1.42	1.42	1.38	3
22.84	22.83	9.90	1.41	1.41	1.37	3
21.49	21.47	9.34	1.40	1.40	1.36	3
20.14	20.13	8.78	1.39	1.39	1.35	3
18.80	18.78	8.21	1.38	1.38	1.34	3
18.80	18.78	8.21	1.34	1.34	1.31	2
16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.43	569.29	249.36	319.93	301.41	18.52	6
58.92	605.75	244.79	360.96	333.26	27.71	6
58.41	642.28	240.42	401.86	365.16	36.70	6
57.90	678.87	236.31	442.56	397.13	45.43	6
57.38	715.51	232.52	482.99	429.15	53.84	6
56.87	752.21	229.11	523.09	461.22	61.87	6

56.35	788.94	226.15	562.79	493.34	69.45	6
55.84	825.72	223.70	602.02	525.50	76.52	6
55.32	862.53	221.81	640.72	557.69	83.03	6
55.32	862.53	221.81	640.72	557.69	83.03	5
54.16	960.95	243.26	717.69	630.36	87.33	5
53.01	1058.59	265.34	793.25	702.25	91.00	5
51.87	1155.43	288.09	867.34	773.34	94.00	5
50.74	1251.44	311.51	939.92	843.59	96.33	5
49.63	1346.59	335.62	1010.97	913.00	97.97	5
48.53	1440.87	360.40	1080.46	981.53	98.94	5
48.53	1440.87	360.40	1080.46	981.53	98.94	4
46.55	1640.19	427.72	1212.48	1104.99	107.48	4
44.58	1839.03	501.94	1337.09	1227.97	109.12	4
42.62	2037.33	549.42	1487.90	1350.41	137.49	4
40.67	2235.04	599.23	1635.81	1472.26	163.55	4
38.72	2432.14	651.70	1780.44	1593.50	186.94	4
36.79	2628.60	707.23	1921.37	1714.10	207.26	4
34.87	2824.38	766.39	2057.99	1834.02	223.97	4
32.96	3019.42	829.95	2189.47	1953.21	236.26	4
31.06	3213.67	899.34	2314.33	2071.60	242.73	4
31.06	3213.67	899.34	2314.33	2071.60	242.73	3
29.67	3362.10	955.13	2406.98	2158.17	248.80	3
28.29	3510.17	1015.89	2494.28	2244.38	249.90	3
26.92	3657.86	1083.40	2574.46	2330.21	244.24	3
25.55	3805.18	1149.36	2655.81	2415.67	240.15	3
24.18	3952.12	1213.75	2738.38	2500.76	237.62	3
22.83	4098.71	1276.61	2822.10	2585.49	236.62	3
21.47	4244.95	1338.05	2906.90	2669.87	237.03	3
20.13	4390.85	1398.05	2992.80	2753.91	238.90	3
18.78	4536.41	1456.73	3079.68	2837.61	242.07	3
18.78	4536.41	1456.73	3079.68	2837.61	242.07	2
16.87	4741.94	1536.64	3205.30	2957.04	248.26	2
14.96	4946.98	1617.44	3329.54	3075.98	253.56	2
13.07	5151.51	1698.89	3452.62	3194.42	258.21	2
11.18	5355.54	1781.26	3574.28	3312.35	261.93	2
9.29	5559.07	1864.04	3695.04	3429.78	265.25	2
7.42	5762.08	1947.51	3814.57	3546.69	267.88	2
5.56	5964.60	2033.61	3931.00	3663.12	267.88	2
3.70	6166.68	2139.98	4026.70	3779.09	247.60	2
1.85	6368.33	2242.06	4126.26	3894.64	231.62	2
.00	6569.57	2340.41	4229.16	4009.78	219.37	2

Time = 1440. Degree of Consolidation = 51.%

Total Settlement = 1.155

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 1440. = 1.155

Settlement caused by Secondary Compression at time 1440. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 1440. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 1440. = .169

Settlement caused by Secondary Compression at time 1440. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.28

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	59.26	21.42	6.50	5.73	5.69	6
60.02	58.76	21.35	6.49	5.74	5.68	6
59.45	58.25	21.27	6.47	5.74	5.66	6
58.89	57.74	21.20	6.46	5.75	5.65	6
58.33	57.23	21.12	6.44	5.75	5.64	6
57.76	56.72	21.05	6.43	5.75	5.62	6
57.20	56.21	20.97	6.42	5.76	5.61	6
56.64	55.70	20.90	6.40	5.76	5.59	6
56.08	55.19	20.82	6.39	5.75	5.58	6
56.08	55.19	20.82	4.51	3.99	3.84	5
54.82	54.04	20.59	4.44	3.93	3.78	5
53.56	52.90	20.36	4.38	3.87	3.72	5
52.32	51.78	20.12	4.32	3.81	3.65	5
51.10	50.67	19.89	4.25	3.76	3.59	5
49.88	49.57	19.66	4.19	3.69	3.52	5
48.69	48.49	19.43	4.13	3.63	3.46	5
48.69	48.49	19.43	1.93	1.90	1.89	4
46.69	46.52	18.75	1.92	1.89	1.87	4
44.70	44.55	18.06	1.91	1.87	1.85	4
42.72	42.59	17.38	1.89	1.86	1.83	4
40.75	40.64	16.70	1.88	1.85	1.81	4
38.79	38.70	16.01	1.86	1.83	1.79	4
36.85	36.77	15.33	1.84	1.82	1.76	4
34.91	34.85	14.65	1.82	1.80	1.74	4
33.00	32.95	13.97	1.80	1.78	1.72	4
31.09	31.05	13.28	1.78	1.76	1.70	4
31.09	31.05	13.28	1.47	1.47	1.43	3
29.70	29.66	12.72	1.46	1.46	1.42	3
28.32	28.28	12.16	1.45	1.45	1.41	3
26.94	26.91	11.59	1.44	1.43	1.40	3
25.57	25.54	11.03	1.43	1.42	1.39	3
24.21	24.18	10.47	1.42	1.41	1.38	3
22.84	22.82	9.90	1.41	1.40	1.37	3
21.49	21.47	9.34	1.40	1.39	1.36	3
20.14	20.12	8.78	1.39	1.39	1.35	3
18.80	18.78	8.21	1.38	1.38	1.34	3
18.80	18.78	8.21	1.34	1.33	1.31	2
16.88	16.87	7.39	1.33	1.33	1.30	2
14.97	14.96	6.57	1.32	1.32	1.29	2

13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
59.26	569.29	254.49	314.80	301.41	13.39	6
58.76	605.66	252.59	353.07	333.16	19.91	6
58.25	642.06	250.85	391.21	364.94	26.27	6
57.74	678.48	249.32	429.16	396.74	32.42	6
57.23	714.92	248.07	466.85	428.56	38.29	6
56.72	751.37	247.13	504.24	460.39	43.85	6
56.21	787.84	246.56	541.28	492.24	49.04	6
55.70	824.31	246.41	577.90	524.09	53.81	6
55.19	860.78	246.72	614.06	555.94	58.12	6
55.19	860.78	246.72	614.06	555.94	58.12	5
54.04	958.28	269.57	688.71	627.69	61.02	5
52.90	1054.95	292.84	762.12	698.61	63.51	5
51.78	1150.79	316.54	834.24	768.70	65.55	5
50.67	1245.76	340.70	905.06	837.92	67.14	5
49.57	1339.86	365.32	974.53	906.27	68.27	5
48.49	1433.06	390.40	1042.67	973.72	68.94	5
48.49	1433.06	390.40	1042.67	973.72	68.94	4
46.52	1632.17	460.32	1171.85	1096.97	74.88	4
44.55	1830.78	521.44	1309.34	1219.72	89.62	4
42.59	2028.85	568.59	1460.26	1341.93	118.33	4
40.64	2226.33	617.80	1608.54	1463.56	144.98	4
38.70	2423.22	669.42	1753.80	1584.58	169.22	4
36.77	2619.47	723.95	1895.52	1704.98	190.54	4
34.85	2815.06	782.03	2033.02	1824.70	208.32	4
32.95	3009.92	844.59	2165.33	1943.71	221.62	4
31.05	3204.00	913.11	2290.89	2061.93	228.96	4
31.05	3204.00	913.11	2290.89	2061.93	228.96	3
29.66	3352.35	968.03	2384.32	2148.42	235.90	3
28.28	3500.34	1029.04	2471.30	2234.55	236.75	3
26.91	3647.96	1094.71	2553.25	2320.31	232.94	3
25.54	3795.21	1159.11	2636.11	2405.71	230.40	3
24.18	3942.11	1222.21	2719.90	2490.74	229.16	3
22.82	4088.65	1283.98	2804.68	2575.43	229.25	3
21.47	4234.86	1344.57	2890.29	2659.77	230.52	3

20.12	4380.72	1403.94	2976.78	2743.78	233.00	3
18.78	4526.25	1462.12	3064.13	2827.45	236.68	3
18.78	4526.25	1462.12	3064.13	2827.45	236.68	2
16.87	4731.75	1541.00	3190.75	2946.85	243.90	2
14.96	4936.76	1620.99	3315.77	3065.76	250.01	2
13.07	5141.28	1701.61	3439.67	3184.18	255.49	2
11.18	5345.30	1783.12	3562.18	3302.10	260.08	2
9.29	5548.82	1864.99	3683.83	3419.52	264.30	2
7.42	5751.82	1947.51	3804.31	3536.43	267.88	2
5.56	5954.34	2033.61	3920.74	3652.86	267.88	2
3.70	6156.42	2140.58	4015.84	3768.83	247.01	2
1.85	6358.06	2243.22	4114.84	3884.38	230.46	2
.00	6559.29	2341.91	4217.38	3999.51	217.87	2

Time = 1800. Degree of Consolidation = 58.%

Total Settlement = 1.320

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 1800. = 1.320

Settlement caused by Secondary Compression at time 1800. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1

1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 1800. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 1800. = .169

Settlement caused by Secondary Compression at time 1800. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 2.11

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.95	21.42	6.50	5.69	5.69	6
60.02	58.45	21.35	6.49	5.68	5.68	6
59.45	57.94	21.27	6.47	5.66	5.66	6
58.89	57.44	21.20	6.46	5.65	5.65	6
58.33	56.94	21.12	6.44	5.64	5.64	6
57.76	56.44	21.05	6.43	5.62	5.62	6
57.20	55.94	20.97	6.42	5.61	5.61	6
56.64	55.44	20.90	6.40	5.59	5.59	6
56.08	54.94	20.82	6.39	5.58	5.58	6
56.08	54.94	20.82	4.51	3.84	3.84	5
54.82	53.82	20.59	4.44	3.80	3.78	5
53.56	52.72	20.36	4.38	3.75	3.72	5
52.32	51.62	20.12	4.32	3.70	3.65	5
51.10	50.54	19.89	4.25	3.64	3.59	5
49.88	49.47	19.66	4.19	3.58	3.52	5
48.69	48.42	19.43	4.13	3.52	3.46	5
48.69	48.42	19.43	1.93	1.89	1.89	4
46.69	46.45	18.75	1.92	1.88	1.87	4
44.70	44.49	18.06	1.91	1.87	1.85	4
42.72	42.53	17.38	1.89	1.85	1.83	4

40.75	40.59	16.70	1.88	1.84	1.81	4
38.79	38.66	16.01	1.86	1.82	1.79	4
36.85	36.73	15.33	1.84	1.81	1.76	4
34.91	34.82	14.65	1.82	1.79	1.74	4
33.00	32.92	13.97	1.80	1.78	1.72	4
31.09	31.03	13.28	1.78	1.76	1.70	4
31.09	31.03	13.28	1.47	1.46	1.43	3
29.70	29.65	12.72	1.46	1.45	1.42	3
28.32	28.27	12.16	1.45	1.44	1.41	3
26.94	26.90	11.59	1.44	1.43	1.40	3
25.57	25.53	11.03	1.43	1.42	1.39	3
24.21	24.17	10.47	1.42	1.41	1.38	3
22.84	22.81	9.90	1.41	1.40	1.37	3
21.49	21.46	9.34	1.40	1.39	1.36	3
20.14	20.12	8.78	1.39	1.38	1.35	3
18.80	18.78	8.21	1.38	1.37	1.34	3
18.80	18.78	8.21	1.34	1.33	1.31	2
16.88	16.87	7.39	1.33	1.32	1.30	2
14.97	14.96	6.57	1.32	1.31	1.29	2
13.07	13.07	5.75	1.31	1.31	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.95	569.29	267.88	301.41	301.41	.00	6
58.45	605.42	272.50	332.92	332.92	.00	6
57.94	641.49	277.12	364.37	364.37	.00	6
57.44	677.49	281.74	395.75	395.75	.00	6
56.94	713.42	286.36	427.06	427.06	.00	6
56.44	749.29	290.98	458.31	458.31	.00	6
55.94	785.10	295.60	489.50	489.50	.00	6
55.44	820.84	300.22	520.61	520.61	.00	6
54.94	856.51	304.84	551.67	551.67	.00	6
54.94	856.51	304.84	551.67	551.67	.00	5
53.82	952.01	323.09	628.91	621.41	7.50	5
52.72	1046.83	342.55	704.28	690.49	13.79	5
51.62	1140.93	363.97	776.95	758.84	18.12	5
50.54	1234.22	387.16	847.06	826.38	20.68	5
49.47	1326.65	411.54	915.11	893.06	22.05	5

48.42	1418.20	436.66	981.54	958.86	22.68	5
48.42	1418.20	436.66	981.54	958.86	22.68	4
46.45	1616.98	507.02	1109.95	1081.78	28.18	4
44.49	1815.22	553.22	1262.00	1204.16	57.84	4
42.53	2012.90	600.61	1412.29	1325.98	86.31	4
40.59	2210.00	649.62	1560.38	1447.23	113.16	4
38.66	2406.51	700.68	1705.83	1567.88	137.96	4
36.73	2602.40	754.41	1847.99	1687.90	160.08	4
34.82	2797.62	811.57	1986.05	1807.27	178.78	4
32.92	2992.14	873.27	2118.88	1925.93	192.95	4
31.03	3185.89	941.12	2244.77	2043.81	200.96	4
31.03	3185.89	941.12	2244.77	2043.81	200.96	3
29.65	3334.06	995.29	2338.76	2130.12	208.64	3
28.27	3481.88	1057.77	2424.11	2216.09	208.02	3
26.90	3629.35	1120.22	2509.13	2301.70	207.43	3
25.53	3776.47	1181.76	2594.70	2386.96	207.75	3
24.17	3923.24	1242.34	2680.90	2471.87	209.02	3
22.81	4069.68	1301.96	2767.72	2556.45	211.27	3
21.46	4215.78	1360.72	2855.07	2640.70	214.37	3
20.12	4361.56	1418.56	2943.00	2724.62	218.39	3
18.78	4507.02	1475.48	3031.53	2808.21	223.32	3
18.78	4507.02	1475.48	3031.53	2808.21	223.32	2
16.87	4712.44	1551.83	3160.61	2927.54	233.07	2
14.96	4917.39	1629.23	3288.16	3046.39	241.77	2
13.07	5121.86	1707.83	3414.04	3164.77	249.27	2
11.18	5325.85	1787.25	3538.60	3282.66	255.95	2
9.29	5529.35	1867.11	3662.24	3400.06	262.18	2
7.42	5732.35	1947.51	3784.84	3516.96	267.88	2
5.56	5934.87	2033.61	3901.26	3633.38	267.88	2
3.70	6136.95	2140.58	3996.37	3749.36	247.01	2
1.85	6338.59	2243.22	4095.37	3864.91	230.46	2
.00	6539.82	2341.91	4197.91	3980.04	217.87	2

Time = 2520. Degree of Consolidation = 72.%

Total Settlement = 1.632

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 2520. = 1.632

Settlement caused by Secondary Compression at time 2520. = .000

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 2520. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 2520. = .169

Settlement caused by Secondary Compression at time 2520. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.80

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.86	21.42	6.50	5.69	5.69	6

60.02	58.35	21.35	6.49	5.67	5.68	6
59.45	57.85	21.27	6.47	5.66	5.66	6
58.89	57.35	21.20	6.46	5.65	5.65	6
58.33	56.85	21.12	6.44	5.63	5.64	6
57.76	56.34	21.05	6.43	5.62	5.62	6
57.20	55.84	20.97	6.42	5.61	5.61	6
56.64	55.35	20.90	6.40	5.59	5.59	6
56.08	54.85	20.82	6.39	5.58	5.58	6
56.08	54.85	20.82	4.51	3.84	3.84	5
54.82	53.73	20.59	4.44	3.78	3.78	5
53.56	52.63	20.36	4.38	3.72	3.72	5
52.32	51.55	20.12	4.32	3.65	3.65	5
51.10	50.48	19.89	4.25	3.59	3.59	5
49.88	49.42	19.66	4.19	3.52	3.52	5
48.69	48.38	19.43	4.13	3.46	3.46	5
48.69	48.38	19.43	1.93	1.89	1.89	4
46.69	46.41	18.75	1.92	1.87	1.87	4
44.70	44.45	18.06	1.91	1.86	1.85	4
42.72	42.50	17.38	1.89	1.85	1.83	4
40.75	40.56	16.70	1.88	1.83	1.81	4
38.79	38.63	16.01	1.86	1.82	1.79	4
36.85	36.71	15.33	1.84	1.80	1.76	4
34.91	34.80	14.65	1.82	1.79	1.74	4
33.00	32.90	13.97	1.80	1.77	1.72	4
31.09	31.02	13.28	1.78	1.75	1.70	4
31.09	31.02	13.28	1.47	1.46	1.43	3
29.70	29.64	12.72	1.46	1.45	1.42	3
28.32	28.26	12.16	1.45	1.44	1.41	3
26.94	26.89	11.59	1.44	1.43	1.40	3
25.57	25.52	11.03	1.43	1.42	1.39	3
24.21	24.16	10.47	1.42	1.41	1.38	3
22.84	22.81	9.90	1.41	1.40	1.37	3
21.49	21.46	9.34	1.40	1.39	1.36	3
20.14	20.12	8.78	1.39	1.38	1.35	3
18.80	18.78	8.21	1.38	1.37	1.34	3
18.80	18.78	8.21	1.34	1.33	1.31	2
16.88	16.87	7.39	1.33	1.32	1.30	2
14.97	14.96	6.57	1.32	1.31	1.29	2
13.07	13.06	5.75	1.31	1.30	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.86	569.29	267.88	301.41	301.41	.00	6
58.35	605.42	272.50	332.92	332.92	.00	6
57.85	641.47	277.12	364.35	364.35	.00	6
57.35	677.47	281.74	395.73	395.73	.00	6
56.85	713.39	286.36	427.03	427.03	.00	6
56.34	749.25	290.98	458.27	458.27	.00	6
55.84	785.04	295.60	489.44	489.44	.00	6
55.35	820.77	300.22	520.55	520.55	.00	6
54.85	856.44	304.84	551.59	551.59	.00	6
54.85	856.44	304.84	551.59	551.59	.00	5
53.73	951.78	330.59	621.19	621.19	.00	5
52.63	1046.21	356.34	689.87	689.87	.00	5
51.55	1139.71	382.09	757.62	757.62	.00	5
50.48	1232.29	407.84	824.45	824.45	.00	5
49.42	1323.94	433.59	890.35	890.35	.00	5
48.38	1414.67	459.34	955.33	955.33	.00	5
48.38	1414.67	459.34	955.33	955.33	.00	4
46.41	1613.28	522.38	1090.90	1078.08	12.82	4
44.45	1811.33	569.20	1242.13	1200.27	41.86	4
42.50	2008.82	616.58	1392.24	1321.90	70.34	4
40.56	2205.74	665.23	1540.50	1442.96	97.54	4
38.63	2402.06	715.85	1686.21	1563.43	122.79	4
36.71	2597.77	769.14	1828.63	1683.27	145.36	4
34.80	2792.82	826.02	1966.80	1802.46	164.34	4
32.90	2987.17	887.65	2099.51	1920.95	178.56	4
31.02	3180.74	956.13	2224.61	2038.66	185.95	4
31.02	3180.74	956.13	2224.61	2038.66	185.95	3
29.64	3328.81	1010.85	2317.97	2124.88	193.08	3
28.26	3476.55	1072.67	2403.87	2210.76	193.12	3
26.89	3623.94	1133.71	2490.23	2296.29	193.94	3
25.52	3770.98	1193.91	2577.07	2381.47	195.60	3
24.16	3917.69	1253.27	2664.42	2466.33	198.09	3
22.81	4064.07	1311.90	2752.17	2550.85	201.32	3
21.46	4210.12	1369.73	2840.40	2635.04	205.36	3
20.12	4355.85	1426.70	2929.15	2718.91	210.24	3
18.78	4501.26	1482.94	3018.32	2802.46	215.86	3
18.78	4501.26	1482.94	3018.32	2802.46	215.86	2
16.87	4706.65	1557.84	3148.81	2921.75	227.06	2
14.96	4911.57	1633.87	3277.69	3040.57	237.12	2
13.06	5116.01	1711.20	3404.81	3158.92	245.89	2
11.18	5319.98	1789.31	3530.67	3276.79	253.88	2
9.29	5523.47	1868.17	3655.30	3394.18	261.12	2
7.42	5726.47	1947.51	3778.96	3511.08	267.88	2

5.56	5928.99	2033.61	3895.38	3627.50	267.88	2
3.70	6131.07	2140.58	3990.49	3743.48	247.01	2
1.85	6332.71	2243.22	4089.49	3859.03	230.46	2
.00	6533.94	2341.91	4192.03	3974.16	217.87	2

Time = 2880. Degree of Consolidation = 76.%

Total Settlement = 1.726

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 2880. = 1.724

Settlement caused by Secondary Compression at time 2880. = .003

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 2880. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 2880. = .169

Settlement caused by Secondary Compression at time 2880. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.70

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.83	21.42	6.50	5.69	5.69	6
60.02	58.32	21.35	6.49	5.67	5.68	6
59.45	57.82	21.27	6.47	5.66	5.66	6
58.89	57.32	21.20	6.46	5.64	5.65	6
58.33	56.81	21.12	6.44	5.63	5.64	6
57.76	56.31	21.05	6.43	5.62	5.62	6
57.20	55.81	20.97	6.42	5.60	5.61	6
56.64	55.32	20.90	6.40	5.59	5.59	6
56.08	54.82	20.82	6.39	5.58	5.58	6
56.08	54.82	20.82	4.51	3.84	3.84	5
54.82	53.70	20.59	4.44	3.78	3.78	5
53.56	52.60	20.36	4.38	3.71	3.72	5
52.32	51.52	20.12	4.32	3.65	3.65	5
51.10	50.45	19.89	4.25	3.59	3.59	5
49.88	49.39	19.66	4.19	3.52	3.52	5
48.69	48.35	19.43	4.13	3.46	3.46	5
48.69	48.35	19.43	1.93	1.89	1.89	4
46.69	46.38	18.75	1.92	1.87	1.87	4
44.70	44.43	18.06	1.91	1.86	1.85	4
42.72	42.48	17.38	1.89	1.85	1.83	4
40.75	40.54	16.70	1.88	1.83	1.81	4
38.79	38.61	16.01	1.86	1.82	1.79	4
36.85	36.69	15.33	1.84	1.80	1.76	4
34.91	34.78	14.65	1.82	1.78	1.74	4
33.00	32.89	13.97	1.80	1.77	1.72	4
31.09	31.01	13.28	1.78	1.75	1.70	4
31.09	31.01	13.28	1.47	1.46	1.43	3
29.70	29.63	12.72	1.46	1.45	1.42	3
28.32	28.25	12.16	1.45	1.44	1.41	3

26.94	26.88	11.59	1.44	1.43	1.40	3
25.57	25.52	11.03	1.43	1.42	1.39	3
24.21	24.16	10.47	1.42	1.41	1.38	3
22.84	22.80	9.90	1.41	1.40	1.37	3
21.49	21.46	9.34	1.40	1.39	1.36	3
20.14	20.11	8.78	1.39	1.38	1.35	3
18.80	18.78	8.21	1.38	1.37	1.34	3
18.80	18.78	8.21	1.34	1.33	1.31	2
16.88	16.86	7.39	1.33	1.32	1.30	2
14.97	14.96	6.57	1.32	1.31	1.29	2
13.07	13.06	5.75	1.31	1.30	1.28	2
11.18	11.18	4.93	1.30	1.30	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.83	569.29	267.88	301.41	301.41	.00	6
58.32	605.41	272.50	332.91	332.91	.00	6
57.82	641.46	277.12	364.34	364.34	.00	6
57.32	677.44	281.74	395.70	395.70	.00	6
56.81	713.36	286.36	427.00	427.00	.00	6
56.31	749.21	290.98	458.23	458.23	.00	6
55.81	784.99	295.60	489.39	489.39	.00	6
55.32	820.71	300.22	520.49	520.49	.00	6
54.82	856.36	304.84	551.52	551.52	.00	6
54.82	856.36	304.84	551.52	551.52	.00	5
53.70	951.71	330.59	621.11	621.11	.00	5
52.60	1046.12	356.34	689.78	689.78	.00	5
51.52	1139.61	382.09	757.52	757.52	.00	5
50.45	1232.18	407.84	824.34	824.34	.00	5
49.39	1323.83	433.59	890.23	890.24	.00	5
48.35	1414.55	459.34	955.20	955.20	.00	5
48.35	1414.55	459.34	955.20	955.20	.00	4
46.38	1613.13	525.20	1087.93	1077.93	10.00	4
44.43	1811.13	574.82	1236.32	1200.07	36.24	4
42.48	2008.54	624.72	1383.82	1321.62	62.20	4
40.54	2205.35	675.46	1529.89	1442.57	87.32	4
38.61	2401.54	727.66	1673.89	1562.91	110.98	4
36.69	2597.10	782.11	1814.99	1682.61	132.38	4
34.78	2791.99	839.90	1952.09	1801.64	150.45	4

32.89	2986.17	902.42	2083.75	1919.95	163.80	4
31.01	3179.55	972.08	2207.47	2037.48	169.99	4
31.01	3179.55	972.08	2207.47	2037.48	169.99	3
29.63	3327.53	1027.90	2299.63	2123.60	176.03	3
28.25	3475.18	1088.11	2387.06	2209.39	177.68	3
26.88	3622.48	1147.62	2474.86	2294.83	180.03	3
25.52	3769.45	1206.46	2562.99	2379.95	183.05	3
24.16	3916.10	1264.69	2651.41	2464.73	186.68	3
22.80	4062.42	1322.24	2740.18	2549.19	190.99	3
21.46	4208.41	1379.03	2829.39	2633.33	196.06	3
20.11	4354.09	1435.20	2918.89	2717.15	201.74	3
18.78	4499.46	1490.68	3008.77	2800.66	208.12	3
18.78	4499.46	1490.68	3008.77	2800.66	208.12	2
16.86	4704.80	1564.04	3140.76	2919.90	220.86	2
14.96	4909.68	1638.79	3270.89	3038.68	232.21	2
13.06	5114.10	1714.80	3399.30	3157.01	242.30	2
11.18	5318.05	1791.55	3526.51	3274.86	251.65	2
9.29	5521.53	1869.31	3652.22	3392.24	259.98	2
7.42	5724.53	1947.51	3777.02	3509.14	267.88	2
5.56	5927.05	2033.61	3893.44	3625.56	267.88	2
3.70	6129.12	2140.58	3988.55	3741.54	247.01	2
1.85	6330.77	2243.22	4087.54	3857.08	230.46	2
.00	6532.00	2341.91	4190.09	3972.22	217.87	2

Time = 3240. Degree of Consolidation = 78.%

Total Settlement = 1.757

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 3240. = 1.753

Settlement caused by Secondary Compression at time 3240. = .005

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1

1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 3240. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 3240. = .169

Settlement caused by Secondary Compression at time 3240. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.67

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.80	21.42	6.50	5.69	5.69	6
60.02	58.29	21.35	6.49	5.67	5.68	6
59.45	57.79	21.27	6.47	5.66	5.66	6
58.89	57.29	21.20	6.46	5.64	5.65	6
58.33	56.79	21.12	6.44	5.63	5.64	6
57.76	56.29	21.05	6.43	5.62	5.62	6
57.20	55.79	20.97	6.42	5.60	5.61	6
56.64	55.29	20.90	6.40	5.59	5.59	6
56.08	54.79	20.82	6.39	5.57	5.58	6
56.08	54.79	20.82	4.51	3.84	3.84	5

54.82	53.68	20.59	4.44	3.78	3.78	5
53.56	52.58	20.36	4.38	3.71	3.72	5
52.32	51.49	20.12	4.32	3.65	3.65	5
51.10	50.42	19.89	4.25	3.59	3.59	5
49.88	49.36	19.66	4.19	3.52	3.52	5
48.69	48.32	19.43	4.13	3.46	3.46	5
48.69	48.32	19.43	1.93	1.89	1.89	4
46.69	46.36	18.75	1.92	1.87	1.87	4
44.70	44.40	18.06	1.91	1.86	1.85	4
42.72	42.45	17.38	1.89	1.84	1.83	4
40.75	40.52	16.70	1.88	1.83	1.81	4
38.79	38.59	16.01	1.86	1.81	1.79	4
36.85	36.67	15.33	1.84	1.80	1.76	4
34.91	34.77	14.65	1.82	1.78	1.74	4
33.00	32.87	13.97	1.80	1.76	1.72	4
31.09	30.99	13.28	1.78	1.74	1.70	4
31.09	30.99	13.28	1.47	1.45	1.43	3
29.70	29.61	12.72	1.46	1.44	1.42	3
28.32	28.24	12.16	1.45	1.43	1.41	3
26.94	26.87	11.59	1.44	1.42	1.40	3
25.57	25.51	11.03	1.43	1.41	1.39	3
24.21	24.15	10.47	1.42	1.41	1.38	3
22.84	22.80	9.90	1.41	1.40	1.37	3
21.49	21.45	9.34	1.40	1.39	1.36	3
20.14	20.11	8.78	1.39	1.38	1.35	3
18.80	18.77	8.21	1.38	1.37	1.34	3
18.80	18.77	8.21	1.34	1.33	1.31	2
16.88	16.86	7.39	1.33	1.32	1.30	2
14.97	14.96	6.57	1.32	1.31	1.29	2
13.07	13.06	5.75	1.31	1.30	1.28	2
11.18	11.18	4.93	1.30	1.29	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

***** Stresses *****		***** Pore Pressures *****				
XI	Total	Effective	Total	Static	Excess	Material
58.80	569.29	267.88	301.41	301.41	.00	6
58.29	605.40	272.50	332.90	332.90	.00	6
57.79	641.44	277.12	364.32	364.32	.00	6
57.29	677.41	281.74	395.68	395.68	.00	6
56.79	713.32	286.36	426.96	426.96	.00	6

56.29	749.16	290.98	458.18	458.18	.00	6
55.79	784.94	295.60	489.34	489.34	.00	6
55.29	820.65	300.22	520.43	520.43	.00	6
54.79	856.29	304.84	551.45	551.45	.00	6
54.79	856.29	304.84	551.45	551.45	.00	5
53.68	951.63	330.59	621.03	621.04	.00	5
52.58	1046.04	356.34	689.69	689.69	.00	5
51.49	1139.52	382.09	757.43	757.43	.00	5
50.42	1232.08	407.84	824.24	824.24	.00	5
49.36	1323.72	433.59	890.13	890.13	.00	5
48.32	1414.43	459.34	955.09	955.09	.00	5
48.32	1414.43	459.34	955.09	955.09	.00	4
46.36	1613.01	527.05	1085.96	1077.81	8.15	4
44.40	1810.97	578.58	1232.39	1199.92	32.48	4
42.45	2008.33	630.35	1377.98	1321.41	56.57	4
40.52	2205.06	682.83	1522.23	1442.28	79.95	4
38.59	2401.15	736.65	1664.50	1562.52	101.99	4
36.67	2596.60	792.64	1803.96	1682.10	121.86	4
34.77	2791.35	851.81	1939.54	1801.00	138.54	4
32.87	2985.37	915.73	2069.64	1919.16	150.48	4
30.99	3178.59	986.93	2191.66	2036.52	155.14	4
30.99	3178.59	986.93	2191.66	2036.52	155.14	3
29.61	3326.48	1044.21	2282.28	2122.55	159.73	3
28.24	3474.03	1103.20	2370.83	2208.24	162.59	3
26.87	3621.26	1161.57	2459.69	2293.61	166.08	3
25.51	3768.16	1219.30	2548.86	2378.65	170.21	3
24.15	3914.73	1276.47	2638.26	2463.36	174.90	3
22.80	4060.99	1333.02	2727.97	2547.76	180.21	3
21.45	4206.92	1388.92	2818.01	2631.84	186.17	3
20.11	4352.55	1444.25	2908.30	2715.61	192.69	3
18.77	4497.87	1498.93	2998.94	2799.06	199.87	3
18.77	4497.87	1498.93	2998.94	2799.06	199.87	2
16.86	4703.16	1570.65	3132.51	2918.26	214.24	2
14.96	4908.01	1644.10	3263.91	3037.01	226.90	2
13.06	5112.40	1718.77	3393.63	3155.31	238.32	2
11.18	5316.33	1794.25	3522.08	3273.14	248.94	2
9.29	5519.80	1870.70	3649.10	3390.50	258.59	2
7.42	5722.79	1947.51	3775.28	3507.40	267.88	2
5.56	5925.31	2033.61	3891.70	3623.82	267.88	2
3.70	6127.39	2140.58	3986.81	3739.80	247.01	2
1.85	6329.03	2243.22	4085.81	3855.35	230.46	2
.00	6530.26	2341.91	4188.35	3970.48	217.87	2

Time = 3600. Degree of Consolidation = 79.%

Total Settlement = 1.785

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 3600. = 1.779

Settlement caused by Secondary Compression at time 3600. = .006

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 3600. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 3600. = .169

Settlement caused by Secondary Compression at time 3600. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.65

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.75	21.42	6.50	5.69	5.69	6
60.02	58.25	21.35	6.49	5.67	5.68	6
59.45	57.74	21.27	6.47	5.65	5.66	6
58.89	57.24	21.20	6.46	5.64	5.65	6
58.33	56.74	21.12	6.44	5.63	5.64	6
57.76	56.24	21.05	6.43	5.61	5.62	6
57.20	55.74	20.97	6.42	5.60	5.61	6
56.64	55.24	20.90	6.40	5.58	5.59	6
56.08	54.75	20.82	6.39	5.57	5.58	6
56.08	54.75	20.82	4.51	3.84	3.84	5
54.82	53.63	20.59	4.44	3.78	3.78	5
53.56	52.53	20.36	4.38	3.71	3.72	5
52.32	51.45	20.12	4.32	3.65	3.65	5
51.10	50.38	19.89	4.25	3.59	3.59	5
49.88	49.32	19.66	4.19	3.52	3.52	5
48.69	48.28	19.43	4.13	3.46	3.46	5
48.69	48.28	19.43	1.93	1.89	1.89	4
46.69	46.31	18.75	1.92	1.87	1.87	4
44.70	44.36	18.06	1.91	1.86	1.85	4
42.72	42.41	17.38	1.89	1.84	1.83	4
40.75	40.48	16.70	1.88	1.83	1.81	4
38.79	38.55	16.01	1.86	1.81	1.79	4
36.85	36.64	15.33	1.84	1.79	1.76	4
34.91	34.74	14.65	1.82	1.78	1.74	4
33.00	32.85	13.97	1.80	1.76	1.72	4
31.09	30.97	13.28	1.78	1.74	1.70	4
31.09	30.97	13.28	1.47	1.45	1.43	3
29.70	29.59	12.72	1.46	1.44	1.42	3
28.32	28.22	12.16	1.45	1.43	1.41	3
26.94	26.86	11.59	1.44	1.42	1.40	3
25.57	25.50	11.03	1.43	1.41	1.39	3
24.21	24.14	10.47	1.42	1.40	1.38	3
22.84	22.79	9.90	1.41	1.39	1.37	3
21.49	21.44	9.34	1.40	1.38	1.36	3
20.14	20.10	8.78	1.39	1.38	1.35	3
18.80	18.77	8.21	1.38	1.37	1.34	3
18.80	18.77	8.21	1.34	1.33	1.31	2
16.88	16.86	7.39	1.33	1.32	1.30	2

14.97	14.96	6.57	1.32	1.31	1.29	2
13.07	13.06	5.75	1.31	1.30	1.28	2
11.18	11.17	4.93	1.30	1.29	1.27	2
9.30	9.29	4.11	1.29	1.29	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.56	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.85	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.75	569.29	267.88	301.41	301.41	.00	6
58.25	605.40	272.50	332.90	332.90	.00	6
57.74	641.42	277.12	364.31	364.31	.00	6
57.24	677.39	281.74	395.65	395.65	.00	6
56.74	713.28	286.36	426.92	426.92	.00	6
56.24	749.11	290.98	458.13	458.13	.00	6
55.74	784.88	295.60	489.28	489.28	.00	6
55.24	820.58	300.22	520.35	520.35	.00	6
54.75	856.21	304.84	551.37	551.37	.00	6
54.75	856.21	304.84	551.37	551.37	.00	5
53.63	951.53	330.59	620.94	620.94	.00	5
52.53	1045.92	356.34	689.58	689.58	.00	5
51.45	1139.39	382.09	757.30	757.30	.00	5
50.38	1231.94	407.84	824.10	824.10	.00	5
49.32	1323.56	433.59	889.97	889.97	.00	5
48.28	1414.26	459.34	954.92	954.92	.00	5
48.28	1414.26	459.34	954.92	954.92	.00	4
46.31	1612.82	529.61	1083.21	1077.62	5.59	4
44.36	1810.74	583.90	1226.84	1199.68	27.16	4
42.41	2008.01	638.45	1369.56	1321.10	48.47	4
40.48	2204.63	693.72	1510.92	1441.85	69.06	4
38.55	2400.58	750.34	1650.24	1561.94	88.30	4
36.64	2595.84	809.05	1786.79	1681.35	105.44	4
34.74	2790.39	871.03	1919.36	1800.03	119.33	4
32.85	2984.16	937.93	2046.23	1917.95	128.28	4
30.97	3177.10	1011.55	2165.55	2035.03	130.53	4
30.97	3177.10	1011.55	2165.55	2035.03	130.53	3
29.59	3324.84	1071.19	2253.65	2120.90	132.74	3
28.22	3472.24	1129.53	2342.71	2206.45	136.26	3
26.86	3619.32	1186.89	2432.43	2291.67	140.76	3
25.50	3766.08	1243.42	2522.66	2376.57	146.09	3
24.14	3912.52	1299.21	2613.31	2461.15	152.16	3
22.79	4058.65	1354.24	2704.41	2545.43	158.99	3

21.44	4204.48	1408.65	2795.83	2629.39	166.44	3
20.10	4349.99	1462.54	2887.45	2713.05	174.40	3
18.77	4495.21	1515.85	2979.36	2796.41	182.95	3
18.77	4495.21	1515.85	2979.36	2796.41	182.95	2
16.86	4700.41	1584.73	3115.68	2915.51	200.17	2
14.96	4905.18	1655.30	3249.89	3034.18	215.70	2
13.06	5109.51	1727.03	3382.48	3152.42	230.06	2
11.17	5313.40	1800.08	3513.32	3270.21	243.11	2
9.29	5516.84	1874.01	3642.82	3387.54	255.28	2
7.42	5719.82	1948.25	3771.56	3504.43	267.14	2
5.56	5922.34	2033.61	3888.73	3620.85	267.88	2
3.70	6124.41	2140.58	3983.84	3736.83	247.01	2
1.85	6326.06	2243.22	4082.83	3852.37	230.46	2
.00	6527.29	2341.91	4185.38	3967.51	217.87	2

Time = 4320. Degree of Consolidation = 81.%

Total Settlement = 1.833

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 4320. = 1.824

Settlement caused by Secondary Compression at time 4320. = .009

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1

2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 4320. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 4320. = .169

Settlement caused by Secondary Compression at time 4320. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.60

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.71	21.42	6.50	5.69	5.69	6
60.02	58.21	21.35	6.49	5.67	5.68	6
59.45	57.71	21.27	6.47	5.65	5.66	6
58.89	57.20	21.20	6.46	5.64	5.65	6
58.33	56.70	21.12	6.44	5.62	5.64	6
57.76	56.20	21.05	6.43	5.61	5.62	6
57.20	55.70	20.97	6.42	5.60	5.61	6
56.64	55.21	20.90	6.40	5.58	5.59	6
56.08	54.71	20.82	6.39	5.57	5.58	6
56.08	54.71	20.82	4.51	3.84	3.84	5
54.82	53.59	20.59	4.44	3.78	3.78	5
53.56	52.49	20.36	4.38	3.71	3.72	5
52.32	51.41	20.12	4.32	3.65	3.65	5
51.10	50.34	19.89	4.25	3.58	3.59	5
49.88	49.28	19.66	4.19	3.52	3.52	5
48.69	48.24	19.43	4.13	3.46	3.46	5
48.69	48.24	19.43	1.93	1.89	1.89	4
46.69	46.28	18.75	1.92	1.87	1.87	4
44.70	44.32	18.06	1.91	1.86	1.85	4

42.72	42.38	17.38	1.89	1.84	1.83	4
40.75	40.44	16.70	1.88	1.82	1.81	4
38.79	38.52	16.01	1.86	1.81	1.79	4
36.85	36.61	15.33	1.84	1.79	1.76	4
34.91	34.71	14.65	1.82	1.77	1.74	4
33.00	32.82	13.97	1.80	1.75	1.72	4
31.09	30.95	13.28	1.78	1.73	1.70	4
31.09	30.95	13.28	1.47	1.45	1.43	3
29.70	29.57	12.72	1.46	1.44	1.42	3
28.32	28.20	12.16	1.45	1.43	1.41	3
26.94	26.84	11.59	1.44	1.42	1.40	3
25.57	25.48	11.03	1.43	1.41	1.39	3
24.21	24.13	10.47	1.42	1.40	1.38	3
22.84	22.78	9.90	1.41	1.39	1.37	3
21.49	21.44	9.34	1.40	1.38	1.36	3
20.14	20.10	8.78	1.39	1.37	1.35	3
18.80	18.76	8.21	1.38	1.37	1.34	3
18.80	18.76	8.21	1.34	1.33	1.31	2
16.88	16.85	7.39	1.33	1.32	1.30	2
14.97	14.95	6.57	1.32	1.31	1.29	2
13.07	13.06	5.75	1.31	1.30	1.28	2
11.18	11.17	4.93	1.30	1.29	1.27	2
9.30	9.29	4.11	1.29	1.28	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
58.71	569.29	267.88	301.41	301.41	.00	6
58.21	605.39	272.50	332.89	332.89	.00	6
57.71	641.41	277.12	364.29	364.29	.00	6
57.20	677.36	281.74	395.62	395.62	.00	6
56.70	713.25	286.36	426.89	426.89	.00	6
56.20	749.07	290.98	458.09	458.09	.00	6
55.70	784.82	295.60	489.22	489.22	.00	6
55.21	820.51	300.22	520.29	520.29	.00	6
54.71	856.14	304.84	551.29	551.29	.00	6
54.71	856.14	304.84	551.29	551.29	.00	5
53.59	951.44	330.59	620.85	620.85	.00	5
52.49	1045.82	356.34	689.48	689.48	.00	5
51.41	1139.28	382.09	757.19	757.19	.00	5
50.34	1231.81	407.84	823.97	823.97	.00	5

49.28	1323.42	433.59	889.83	889.83	.00	5
48.24	1414.10	459.34	954.76	954.76	.00	5
48.24	1414.10	459.34	954.76	954.76	.00	4
46.28	1612.65	531.44	1081.21	1077.45	3.76	4
44.32	1810.54	587.64	1222.90	1199.48	23.42	4
42.38	2007.76	644.18	1363.58	1320.84	42.74	4
40.44	2204.29	701.51	1502.79	1441.51	61.27	4
38.52	2400.14	760.21	1639.92	1561.50	78.42	4
36.61	2595.27	821.09	1774.18	1680.77	93.41	4
34.71	2789.66	885.29	1904.36	1799.30	105.06	4
32.82	2983.25	954.60	2028.65	1917.03	111.62	4
30.95	3175.98	1029.12	2146.86	2033.90	112.95	4
30.95	3175.98	1029.12	2146.86	2033.90	112.95	3
29.57	3323.61	1089.66	2233.95	2119.68	114.28	3
28.20	3470.91	1148.61	2322.30	2205.12	117.18	3
26.84	3617.88	1206.19	2411.68	2290.23	121.45	3
25.48	3764.53	1262.56	2501.97	2375.02	126.95	3
24.13	3910.86	1317.86	2593.01	2459.50	133.51	3
22.78	4056.89	1372.23	2684.66	2543.67	141.00	3
21.44	4202.62	1425.81	2776.81	2627.53	149.28	3
20.10	4348.04	1478.73	2869.32	2711.10	158.22	3
18.76	4493.17	1530.98	2962.19	2794.37	167.82	3
18.76	4493.17	1530.98	2962.19	2794.37	167.82	2
16.85	4698.28	1597.75	3100.53	2913.39	187.15	2
14.95	4902.98	1666.19	3236.79	3031.98	204.81	2
13.06	5107.25	1735.77	3371.49	3150.16	221.33	2
11.17	5311.09	1806.73	3504.36	3267.90	236.46	2
9.29	5514.50	1878.51	3635.99	3385.20	250.78	2
7.42	5717.45	1951.36	3766.09	3502.06	264.03	2
5.55	5919.96	2036.60	3883.36	3618.47	264.89	2
3.70	6122.02	2143.36	3978.67	3734.44	244.23	2
1.84	6323.66	2245.81	4077.84	3849.97	227.87	2
.00	6524.88	2344.32	4180.56	3965.10	215.46	2

Time = 5040. Degree of Consolidation = 83.%

Total Settlement = 1.871

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 5040. = 1.860

Settlement caused by Secondary Compression at time 5040. = .012

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 5040. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 5040. = .169

Settlement caused by Secondary Compression at time 5040. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.56

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material

60.58	58.68	21.42	6.50	5.69	5.69	6
60.02	58.18	21.35	6.49	5.66	5.68	6
59.45	57.67	21.27	6.47	5.65	5.66	6
58.89	57.17	21.20	6.46	5.64	5.65	6
58.33	56.67	21.12	6.44	5.62	5.64	6
57.76	56.17	21.05	6.43	5.61	5.62	6
57.20	55.67	20.97	6.42	5.59	5.61	6
56.64	55.17	20.90	6.40	5.58	5.59	6
56.08	54.68	20.82	6.39	5.57	5.58	6
56.08	54.68	20.82	4.51	3.84	3.84	5
54.82	53.56	20.59	4.44	3.78	3.78	5
53.56	52.46	20.36	4.38	3.71	3.72	5
52.32	51.38	20.12	4.32	3.65	3.65	5
51.10	50.31	19.89	4.25	3.58	3.59	5
49.88	49.25	19.66	4.19	3.52	3.52	5
48.69	48.21	19.43	4.13	3.46	3.46	5
48.69	48.21	19.43	1.93	1.89	1.89	4
46.69	46.25	18.75	1.92	1.87	1.87	4
44.70	44.29	18.06	1.91	1.85	1.85	4
42.72	42.35	17.38	1.89	1.84	1.83	4
40.75	40.41	16.70	1.88	1.82	1.81	4
38.79	38.49	16.01	1.86	1.81	1.79	4
36.85	36.58	15.33	1.84	1.79	1.76	4
34.91	34.68	14.65	1.82	1.77	1.74	4
33.00	32.80	13.97	1.80	1.75	1.72	4
31.09	30.93	13.28	1.78	1.73	1.70	4
31.09	30.93	13.28	1.47	1.44	1.43	3
29.70	29.56	12.72	1.46	1.43	1.42	3
28.32	28.19	12.16	1.45	1.42	1.41	3
26.94	26.83	11.59	1.44	1.41	1.40	3
25.57	25.47	11.03	1.43	1.41	1.39	3
24.21	24.12	10.47	1.42	1.40	1.38	3
22.84	22.77	9.90	1.41	1.39	1.37	3
21.49	21.43	9.34	1.40	1.38	1.36	3
20.14	20.09	8.78	1.39	1.37	1.35	3
18.80	18.75	8.21	1.38	1.36	1.34	3
18.80	18.75	8.21	1.34	1.32	1.31	2
16.88	16.85	7.39	1.33	1.32	1.30	2
14.97	14.95	6.57	1.32	1.31	1.29	2
13.07	13.06	5.75	1.31	1.30	1.28	2
11.18	11.17	4.93	1.30	1.29	1.27	2
9.30	9.29	4.11	1.29	1.28	1.26	2
7.43	7.42	3.29	1.28	1.28	1.25	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.68	569.29	267.88	301.41	301.41	.00	6
58.18	605.38	272.50	332.89	332.89	.00	6
57.67	641.39	277.12	364.27	364.27	.00	6
57.17	677.34	281.74	395.60	395.60	.00	6
56.67	713.21	286.36	426.85	426.85	.00	6
56.17	749.03	290.98	458.04	458.05	.00	6
55.67	784.77	295.60	489.17	489.17	.00	6
55.17	820.45	300.22	520.23	520.23	.00	6
54.68	856.06	304.84	551.22	551.22	.00	6
54.68	856.06	304.84	551.22	551.22	.00	5
53.56	951.36	330.59	620.76	620.76	.00	5
52.46	1045.72	356.34	689.38	689.38	.00	5
51.38	1139.17	382.09	757.07	757.07	.00	5
50.31	1231.68	407.84	823.84	823.84	.00	5
49.25	1323.28	433.59	889.69	889.69	.00	5
48.21	1413.95	459.34	954.60	954.60	.00	5
48.21	1413.95	459.34	954.60	954.60	.00	4
46.25	1612.49	532.77	1079.71	1077.29	2.43	4
44.29	1810.35	590.41	1219.94	1199.29	20.65	4
42.35	2007.52	648.45	1359.08	1320.61	38.47	4
40.41	2204.00	707.36	1496.64	1441.22	55.42	4
38.49	2399.76	767.68	1632.09	1561.13	70.96	4
36.58	2594.80	830.19	1764.61	1680.30	84.31	4
34.68	2789.07	896.10	1892.97	1798.71	94.26	4
32.80	2982.52	967.30	2015.22	1916.30	98.91	4
30.93	3175.09	1042.57	2132.52	2033.01	99.51	4
30.93	3175.09	1042.57	2132.52	2033.01	99.51	3
29.56	3322.64	1103.87	2218.77	2118.71	100.06	3
28.19	3469.86	1163.41	2306.45	2204.07	102.38	3
26.83	3616.74	1221.38	2395.37	2289.10	106.27	3
25.47	3763.31	1277.94	2485.37	2373.80	111.57	3
24.12	3909.56	1333.24	2576.32	2458.19	118.13	3
22.77	4055.50	1387.43	2668.07	2542.27	125.79	3
21.43	4201.14	1440.65	2760.49	2626.06	134.44	3
20.09	4346.48	1493.01	2853.47	2709.54	143.93	3
18.75	4491.53	1544.66	2946.87	2792.73	154.14	3
18.75	4491.53	1544.66	2946.87	2792.73	154.14	2
16.85	4696.57	1610.19	3086.38	2911.67	174.71	2
14.95	4901.19	1677.17	3224.02	3030.19	193.83	2
13.06	5105.40	1745.29	3360.11	3148.31	211.81	2
11.17	5309.19	1814.77	3494.42	3265.99	228.43	2
9.29	5512.54	1885.10	3627.44	3383.25	244.19	2

7.42	5715.46	1956.47	3758.99	3500.07	258.92	2
5.55	5917.94	2042.70	3875.25	3616.46	258.79	2
3.70	6119.98	2149.04	3970.94	3732.40	238.55	2
1.84	6321.59	2251.10	4070.49	3847.91	222.58	2
.00	6522.79	2349.25	4173.55	3963.01	210.53	2

Time = 5760. Degree of Consolidation = 84.%

Total Settlement = 1.905

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 5760. = 1.891

Settlement caused by Secondary Compression at time 5760. = .014

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 5760. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 5760. = .169

Settlement caused by Secondary Compression at time 5760. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.53

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.65	21.42	6.50	5.69	5.69	6
60.02	58.15	21.35	6.49	5.66	5.68	6
59.45	57.64	21.27	6.47	5.65	5.66	6
58.89	57.14	21.20	6.46	5.63	5.65	6
58.33	56.64	21.12	6.44	5.62	5.64	6
57.76	56.14	21.05	6.43	5.61	5.62	6
57.20	55.64	20.97	6.42	5.59	5.61	6
56.64	55.15	20.90	6.40	5.58	5.59	6
56.08	54.65	20.82	6.39	5.56	5.58	6
56.08	54.65	20.82	4.51	3.84	3.84	5
54.82	53.53	20.59	4.44	3.77	3.78	5
53.56	52.44	20.36	4.38	3.71	3.72	5
52.32	51.35	20.12	4.32	3.65	3.65	5
51.10	50.28	19.89	4.25	3.58	3.59	5
49.88	49.23	19.66	4.19	3.52	3.52	5
48.69	48.19	19.43	4.13	3.45	3.46	5
48.69	48.19	19.43	1.93	1.89	1.89	4
46.69	46.22	18.75	1.92	1.87	1.87	4
44.70	44.26	18.06	1.91	1.85	1.85	4
42.72	42.32	17.38	1.89	1.84	1.83	4
40.75	40.39	16.70	1.88	1.82	1.81	4
38.79	38.47	16.01	1.86	1.80	1.79	4
36.85	36.56	15.33	1.84	1.79	1.76	4
34.91	34.66	14.65	1.82	1.77	1.74	4
33.00	32.78	13.97	1.80	1.75	1.72	4
31.09	30.91	13.28	1.78	1.72	1.70	4
31.09	30.91	13.28	1.47	1.44	1.43	3
29.70	29.54	12.72	1.46	1.43	1.42	3

28.32	28.17	12.16	1.45	1.42	1.41	3
26.94	26.81	11.59	1.44	1.41	1.40	3
25.57	25.46	11.03	1.43	1.40	1.39	3
24.21	24.10	10.47	1.42	1.39	1.38	3
22.84	22.76	9.90	1.41	1.39	1.37	3
21.49	21.42	9.34	1.40	1.38	1.36	3
20.14	20.08	8.78	1.39	1.37	1.35	3
18.80	18.75	8.21	1.38	1.36	1.34	3
18.80	18.75	8.21	1.34	1.32	1.31	2
16.88	16.84	7.39	1.33	1.32	1.30	2
14.97	14.94	6.57	1.32	1.31	1.29	2
13.07	13.05	5.75	1.31	1.30	1.28	2
11.18	11.17	4.93	1.30	1.29	1.27	2
9.30	9.29	4.11	1.29	1.28	1.26	2
7.43	7.42	3.29	1.28	1.27	1.25	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.70	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.65	569.29	267.88	301.41	301.41	.00	6
58.15	605.38	272.50	332.88	332.88	.00	6
57.64	641.38	277.12	364.26	364.26	.00	6
57.14	677.31	281.74	395.57	395.57	.00	6
56.64	713.18	286.36	426.82	426.82	.00	6
56.14	748.98	290.98	458.00	458.00	.00	6
55.64	784.72	295.60	489.12	489.12	.00	6
55.15	820.39	300.22	520.17	520.17	.00	6
54.65	855.99	304.84	551.15	551.15	.00	6
54.65	855.99	304.84	551.15	551.15	.00	5
53.53	951.27	330.59	620.68	620.68	.00	5
52.44	1045.62	356.34	689.28	689.28	.00	5
51.35	1139.05	382.09	756.96	756.96	.00	5
50.28	1231.55	407.84	823.71	823.71	.00	5
49.23	1323.13	433.59	889.54	889.54	.00	5
48.19	1413.79	459.34	954.45	954.45	.00	5
48.19	1413.79	459.34	954.45	954.45	.00	4
46.22	1612.33	533.74	1078.59	1077.13	1.46	4
44.26	1810.17	592.44	1217.73	1199.11	18.62	4
42.32	2007.31	651.62	1355.69	1320.39	35.30	4
40.39	2203.74	711.66	1492.08	1440.97	51.12	4
38.47	2399.45	773.21	1626.24	1560.81	65.43	4
36.56	2594.41	836.99	1757.42	1679.91	77.51	4

34.66	2788.59	904.28	1884.30	1798.23	86.07	4
32.78	2981.93	977.13	2004.80	1915.72	89.08	4
30.91	3174.38	1053.20	2121.17	2032.30	88.87	4
30.91	3174.38	1053.20	2121.17	2032.30	88.87	3
29.54	3321.87	1115.23	2206.64	2117.94	88.70	3
28.17	3469.02	1175.31	2293.71	2203.23	90.48	3
26.81	3615.84	1233.62	2382.22	2288.19	94.03	3
25.46	3762.33	1290.32	2472.01	2372.83	99.19	3
24.10	3908.51	1345.62	2562.89	2457.15	105.74	3
22.76	4054.39	1399.82	2654.57	2541.16	113.41	3
21.42	4199.96	1453.03	2746.92	2624.87	122.05	3
20.08	4345.23	1505.32	2839.91	2708.29	131.62	3
18.75	4490.21	1556.69	2933.52	2791.41	142.11	3
18.75	4490.21	1556.69	2933.52	2791.41	142.11	2
16.84	4695.17	1621.67	3073.50	2910.27	163.22	2
14.94	4899.73	1687.58	3212.15	3028.73	183.41	2
13.05	5103.88	1754.62	3349.26	3146.78	202.48	2
11.17	5307.61	1823.02	3484.59	3264.42	220.17	2
9.29	5510.92	1892.41	3618.51	3381.63	236.88	2
7.42	5713.80	1962.81	3750.99	3498.41	252.58	2
5.55	5916.24	2050.53	3865.71	3614.75	250.95	2
3.70	6118.25	2155.19	3963.06	3730.66	232.39	2
1.84	6319.84	2256.84	4063.00	3846.15	216.85	2
.00	6521.02	2354.59	4166.43	3961.23	205.19	2

Time = 6480. Degree of Consolidation = 85.%

Total Settlement = 1.933

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 6480. = 1.917

Settlement caused by Secondary Compression at time 6480. = .017

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1

2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 6480. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 6480. = .169

Settlement caused by Secondary Compression at time 6480. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.50

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.63	21.42	6.50	5.69	5.69	6
60.02	58.12	21.35	6.49	5.66	5.68	6
59.45	57.62	21.27	6.47	5.65	5.66	6
58.89	57.12	21.20	6.46	5.63	5.65	6
58.33	56.62	21.12	6.44	5.62	5.64	6
57.76	56.12	21.05	6.43	5.60	5.62	6
57.20	55.62	20.97	6.42	5.59	5.61	6
56.64	55.12	20.90	6.40	5.58	5.59	6
56.08	54.62	20.82	6.39	5.56	5.58	6

56.08	54.62	20.82	4.51	3.84	3.84	5
54.82	53.51	20.59	4.44	3.77	3.78	5
53.56	52.41	20.36	4.38	3.71	3.72	5
52.32	51.33	20.12	4.32	3.65	3.65	5
51.10	50.26	19.89	4.25	3.58	3.59	5
49.88	49.20	19.66	4.19	3.52	3.52	5
48.69	48.16	19.43	4.13	3.45	3.46	5
48.69	48.16	19.43	1.93	1.89	1.89	4
46.69	46.20	18.75	1.92	1.87	1.87	4
44.70	44.24	18.06	1.91	1.85	1.85	4
42.72	42.30	17.38	1.89	1.84	1.83	4
40.75	40.37	16.70	1.88	1.82	1.81	4
38.79	38.45	16.01	1.86	1.80	1.79	4
36.85	36.54	15.33	1.84	1.78	1.76	4
34.91	34.64	14.65	1.82	1.76	1.74	4
33.00	32.76	13.97	1.80	1.74	1.72	4
31.09	30.90	13.28	1.78	1.72	1.70	4
31.09	30.90	13.28	1.47	1.44	1.43	3
29.70	29.53	12.72	1.46	1.43	1.42	3
28.32	28.16	12.16	1.45	1.42	1.41	3
26.94	26.80	11.59	1.44	1.41	1.40	3
25.57	25.44	11.03	1.43	1.40	1.39	3
24.21	24.09	10.47	1.42	1.39	1.38	3
22.84	22.75	9.90	1.41	1.38	1.37	3
21.49	21.41	9.34	1.40	1.38	1.36	3
20.14	20.07	8.78	1.39	1.37	1.35	3
18.80	18.74	8.21	1.38	1.36	1.34	3
18.80	18.74	8.21	1.34	1.32	1.31	2
16.88	16.84	7.39	1.33	1.31	1.30	2
14.97	14.94	6.57	1.32	1.31	1.29	2
13.07	13.05	5.75	1.31	1.30	1.28	2
11.18	11.16	4.93	1.30	1.29	1.27	2
9.30	9.29	4.11	1.29	1.28	1.26	2
7.43	7.42	3.29	1.28	1.27	1.25	2
5.56	5.55	2.46	1.27	1.27	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

***** Stresses *****			***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.63	569.29	267.88	301.41	301.41	.00	6
58.12	605.37	272.50	332.87	332.87	.00	6
57.62	641.36	277.12	364.24	364.24	.00	6
57.12	677.29	281.74	395.55	395.55	.00	6

56.62	713.15	286.36	426.79	426.79	.00	6
56.12	748.94	290.98	457.96	457.96	.00	6
55.62	784.67	295.60	489.06	489.06	.00	6
55.12	820.33	300.22	520.10	520.11	.00	6
54.62	855.92	304.84	551.08	551.08	.00	6
54.62	855.92	304.84	551.08	551.08	.00	5
53.51	951.18	330.59	620.59	620.59	.00	5
52.41	1045.52	356.34	689.18	689.18	.00	5
51.33	1138.94	382.09	756.84	756.85	.00	5
50.26	1231.43	407.84	823.58	823.58	.00	5
49.20	1322.99	433.59	889.40	889.40	.00	5
48.16	1413.63	459.34	954.29	954.29	.00	5
48.16	1413.63	459.34	954.29	954.29	.00	4
46.20	1612.16	534.54	1077.63	1076.96	.66	4
44.24	1809.99	594.12	1215.87	1198.93	16.94	4
42.30	2007.11	654.15	1352.96	1320.19	32.77	4
40.37	2203.51	715.13	1488.38	1440.73	47.65	4
38.45	2399.17	777.59	1621.57	1560.53	61.04	4
36.54	2594.06	842.47	1751.60	1679.57	72.03	4
34.64	2788.17	910.93	1877.25	1797.82	79.43	4
32.76	2981.43	985.13	1996.30	1915.21	81.08	4
30.90	3173.77	1061.93	2111.84	2031.70	80.14	4
30.90	3173.77	1061.93	2111.84	2031.70	80.14	3
29.53	3321.21	1124.63	2196.58	2117.28	79.30	3
28.16	3468.31	1185.18	2283.13	2202.52	80.61	3
26.80	3615.07	1243.81	2371.26	2287.42	83.83	3
25.44	3761.51	1300.85	2460.66	2372.00	88.66	3
24.09	3907.63	1356.43	2551.19	2456.26	94.93	3
22.75	4053.44	1410.72	2642.72	2540.21	102.51	3
21.41	4198.95	1463.84	2735.11	2623.86	111.24	3
20.07	4344.16	1515.93	2828.23	2707.22	121.01	3
18.74	4489.08	1567.03	2922.05	2790.28	131.77	3
18.74	4489.08	1567.03	2922.05	2790.28	131.77	2
16.84	4693.98	1631.47	3062.51	2909.08	153.43	2
14.94	4898.48	1696.85	3201.63	3027.48	174.15	2
13.05	5102.58	1763.37	3339.20	3145.48	193.72	2
11.16	5306.26	1831.26	3475.00	3263.06	211.94	2
9.29	5509.52	1899.91	3609.60	3380.22	229.38	2
7.42	5712.35	1969.58	3742.77	3496.96	245.81	2
5.55	5914.75	2059.34	3855.41	3613.27	242.15	2
3.69	6116.73	2162.48	3954.25	3729.15	225.10	2
1.84	6318.29	2262.94	4055.35	3844.61	210.74	2
.00	6519.45	2360.28	4159.17	3959.66	199.51	2

Time = 7200. Degree of Consolidation = 86.%

Total Settlement = 1.958

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 7200. = 1.939

Settlement caused by Secondary Compression at time 7200. = .019

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1
3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 7200. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 7200. = .169

Settlement caused by Secondary Compression at time 7200. = .000

Settlement Due to Desiccation = .000

Surface Elevation = 1.47

**********Current Conditions in Compressible Foundation**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
60.58	58.58	21.42	6.50	5.69	5.69	6
60.02	58.07	21.35	6.49	5.66	5.68	6
59.45	57.57	21.27	6.47	5.64	5.66	6
58.89	57.07	21.20	6.46	5.63	5.65	6
58.33	56.57	21.12	6.44	5.61	5.64	6
57.76	56.07	21.05	6.43	5.60	5.62	6
57.20	55.57	20.97	6.42	5.59	5.61	6
56.64	55.07	20.90	6.40	5.57	5.59	6
56.08	54.58	20.82	6.39	5.56	5.58	6
56.08	54.58	20.82	4.51	3.84	3.84	5
54.82	53.46	20.59	4.44	3.77	3.78	5
53.56	52.36	20.36	4.38	3.71	3.72	5
52.32	51.28	20.12	4.32	3.64	3.65	5
51.10	50.21	19.89	4.25	3.58	3.59	5
49.88	49.16	19.66	4.19	3.52	3.52	5
48.69	48.12	19.43	4.13	3.45	3.46	5
48.69	48.12	19.43	1.93	1.89	1.89	4
46.69	46.15	18.75	1.92	1.87	1.87	4
44.70	44.20	18.06	1.91	1.85	1.85	4
42.72	42.26	17.38	1.89	1.84	1.83	4
40.75	40.32	16.70	1.88	1.82	1.81	4
38.79	38.41	16.01	1.86	1.80	1.79	4
36.85	36.50	15.33	1.84	1.78	1.76	4
34.91	34.61	14.65	1.82	1.76	1.74	4
33.00	32.73	13.97	1.80	1.74	1.72	4
31.09	30.86	13.28	1.78	1.72	1.70	4
31.09	30.86	13.28	1.47	1.44	1.43	3
29.70	29.49	12.72	1.46	1.43	1.42	3
28.32	28.13	12.16	1.45	1.42	1.41	3
26.94	26.77	11.59	1.44	1.41	1.40	3
25.57	25.42	11.03	1.43	1.40	1.39	3
24.21	24.07	10.47	1.42	1.39	1.38	3
22.84	22.72	9.90	1.41	1.38	1.37	3
21.49	21.39	9.34	1.40	1.37	1.36	3
20.14	20.05	8.78	1.39	1.36	1.35	3
18.80	18.72	8.21	1.38	1.36	1.34	3
18.80	18.72	8.21	1.34	1.32	1.31	2

16.88	16.82	7.39	1.33	1.31	1.30	2
14.97	14.93	6.57	1.32	1.30	1.29	2
13.07	13.04	5.75	1.31	1.30	1.28	2
11.18	11.15	4.93	1.30	1.29	1.27	2
9.30	9.28	4.11	1.29	1.28	1.26	2
7.43	7.41	3.29	1.28	1.27	1.25	2
5.56	5.55	2.46	1.27	1.26	1.25	2
3.70	3.69	1.64	1.26	1.26	1.24	2
1.85	1.84	.82	1.25	1.25	1.23	2
.00	.00	.00	1.25	1.24	1.23	2

	***** Stresses *****		***** Pore Pressures *****			
XI	Total	Effective	Total	Static	Excess	Material
58.58	569.29	267.88	301.41	301.41	.00	6
58.07	605.36	272.50	332.86	332.86	.00	6
57.57	641.32	277.12	364.20	364.20	.00	6
57.07	677.22	281.74	395.48	395.48	.00	6
56.57	713.06	286.36	426.70	426.70	.00	6
56.07	748.83	290.98	457.85	457.85	.00	6
55.57	784.53	295.60	488.93	488.93	.00	6
55.07	820.17	300.22	519.95	519.95	.00	6
54.58	855.74	304.84	550.90	550.90	.00	6
54.58	855.74	304.84	550.90	550.90	.00	5
53.46	950.98	330.59	620.38	620.38	.00	5
52.36	1045.28	356.34	688.94	688.94	.00	5
51.28	1138.66	382.09	756.57	756.57	.00	5
50.21	1231.12	407.84	823.27	823.27	.00	5
49.16	1322.64	433.59	889.05	889.05	.00	5
48.12	1413.25	459.34	953.91	953.91	.00	5
48.12	1413.25	459.34	953.91	953.91	.00	4
46.15	1611.78	535.20	1076.58	1076.58	.00	4
44.20	1809.59	596.27	1213.32	1198.53	14.79	4
42.26	2006.67	657.92	1348.75	1319.75	29.00	4
40.32	2203.01	720.56	1482.45	1440.24	42.21	4
38.41	2398.60	784.78	1613.82	1559.96	53.86	4
36.50	2593.40	851.55	1741.85	1678.90	62.95	4
34.61	2787.39	922.19	1865.20	1797.03	68.17	4
32.73	2980.49	999.05	1981.44	1914.28	67.16	4
30.86	3172.66	1077.19	2095.46	2030.58	64.88	4
30.86	3172.66	1077.19	2095.46	2030.58	64.88	3
29.49	3320.01	1141.40	2178.61	2116.08	62.54	3
28.13	3467.01	1203.22	2263.79	2201.22	62.57	3
26.77	3613.67	1262.86	2350.80	2286.02	64.79	3
25.42	3759.99	1320.70	2439.30	2370.48	68.81	3
24.07	3906.00	1376.89	2529.10	2454.63	74.47	3

22.72	4051.69	1431.61	2620.09	2538.47	81.62	3
21.39	4197.08	1484.97	2712.11	2622.00	90.11	3
20.05	4342.18	1537.13	2805.05	2705.24	99.81	3
18.72	4486.98	1588.20	2898.78	2788.18	110.60	3
18.72	4486.98	1588.20	2898.78	2788.18	110.60	2
16.82	4691.75	1652.88	3038.86	2906.85	132.01	2
14.93	4896.12	1717.88	3178.24	3025.12	153.12	2
13.04	5100.08	1783.93	3316.15	3142.99	173.17	2
11.15	5303.64	1850.55	3453.09	3260.45	192.65	2
9.28	5506.78	1917.94	3588.84	3377.49	211.35	2
7.41	5709.51	1986.35	3723.16	3494.12	229.04	2
5.55	5911.82	2082.09	3829.73	3610.33	219.40	2
3.69	6113.71	2182.34	3931.37	3726.12	205.24	2
1.84	6315.19	2280.08	4035.11	3841.51	193.60	2
.00	6516.28	2375.56	4140.72	3956.50	184.22	2

Time = 9000. Degree of Consolidation = 89.%

Total Settlement = 2.009

Settlement at End of Primary Consolidation = 2.265

Settlement caused by Primary Consolidation at time 9000. = 1.984

Settlement caused by Secondary Compression at time 9000. = .025

**********Current Conditions in Dredged Fill**********

***** Coordinates ***** ***** Void Ratios *****

A	XI	Z	Einitial	E	Eeop	Material
5.00	4.83	2.53	.98	.98	.98	1
3.75	3.61	1.89	.98	.92	.92	1
2.50	2.40	1.26	.98	.91	.91	1
1.25	1.20	.63	.98	.90	.90	1
.00	.00	.00	.98	.89	.90	1

***** Stresses ***** ***** Pore Pressures *****

XI	Total	Effective	Total	Static	Excess	Material
4.83	.00	.00	.00	.00	.00	1

3.61	143.38	66.97	76.41	76.41	.00	1
2.40	285.64	133.94	151.70	151.70	.00	1
1.20	427.58	200.91	226.67	226.67	.00	1
.00	569.29	267.88	301.41	301.41	.00	1

Time = 9000. Degree of Consolidation = 100.%

Total Settlement = .170

Settlement at End of Primary Consolidation = .169

Settlement caused by Primary Consolidation at time 9000. = .169

Settlement caused by Secondary Compression at time 9000. = .000

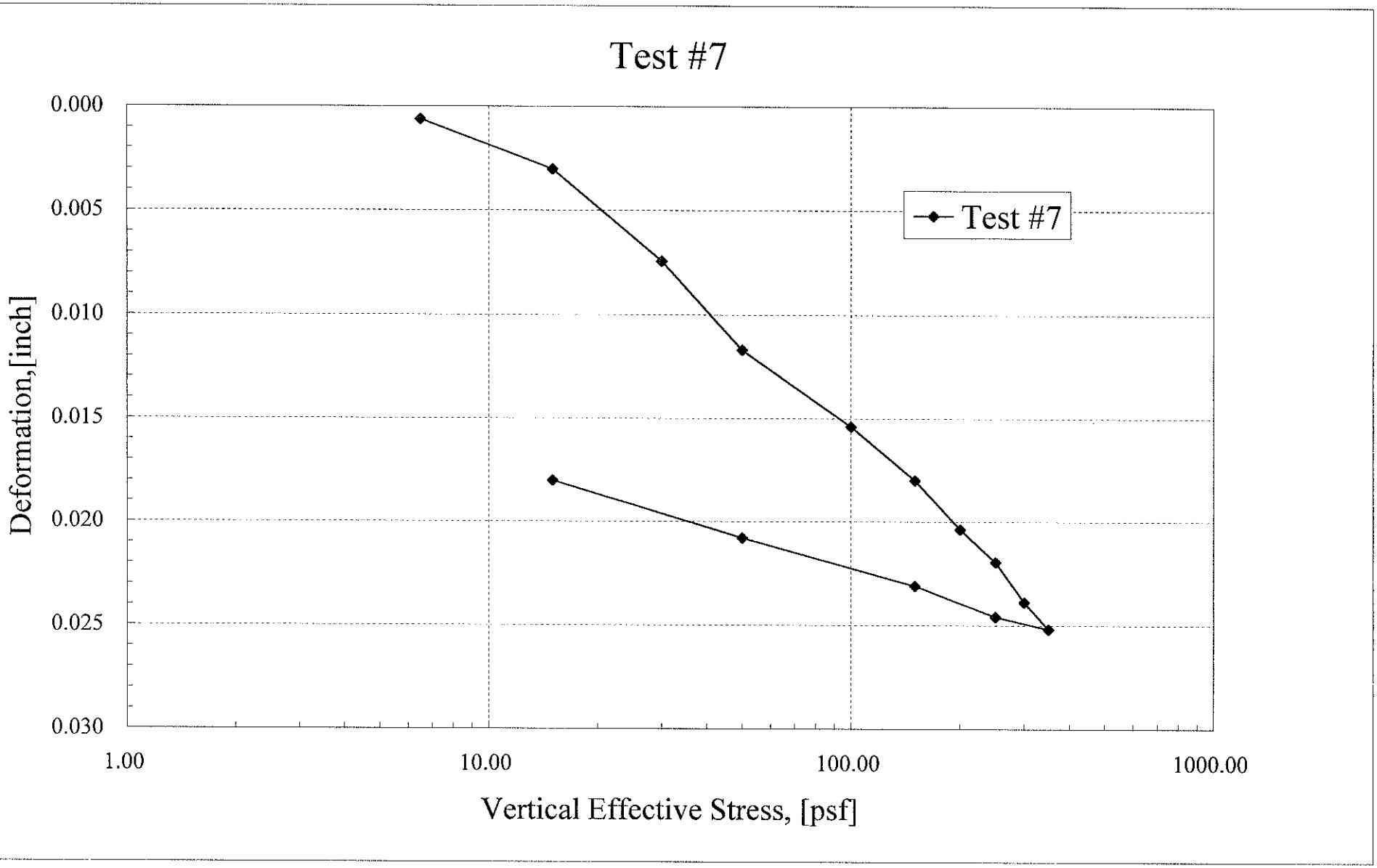
Settlement Due to Desiccation = .000

Surface Elevation = 1.42

Results of Oedometer Test No. #7

Loading Steps	Load Increment(psf)	Deformation at EOP (inch)	Secondary Deformation (inch)	Subtotal Deformation Δ H(inch)	Accumulative Deformation Σ Δ H(inch)	ε_v %	H (inch)	$e = \frac{H - H_s}{H_s}$	m_v (ft^2/lb)	k (ft/day)
1	6.48			0.00063	0.00063	0.06	0.99937	0.9411		
2	15.00			0.00240	0.00303	0.30	0.99697	0.9365	2.8199E-04	2.0741E-02
3	30.00			0.00440	0.00743	0.74	0.99257	0.9279	2.9434E-04	2.1489E-02
4	50.00			0.00427	0.01170	1.17	0.98830	0.9196	2.1515E-04	1.5583E-02
5	100.00			0.00371	0.01541	1.54	0.98459	0.9124	7.5055E-05	5.3928E-03
6	150.00			0.00261	0.01802	1.80	0.98198	0.9074	5.2931E-05	3.7783E-03
7	200.00			0.00237	0.02039	2.04	0.97961	0.9028	4.8256E-05	3.4283E-03
8	250.00			0.00157	0.02195	2.20	0.97805	0.8997	3.1988E-05	2.2625E-03
9	300.00			0.00193	0.02389	2.39	0.97611	0.8960	3.9534E-05	2.7870E-03
10	350.00			0.00131	0.02520	2.52	0.97480	0.8934	2.6841E-05	1.8851E-03
11	250.00			-0.00060	0.02460	2.46	0.97540	0.8946	6.1475E-06	0.0000E+00
12	150.00			-0.00148	0.02311	2.31	0.97689	0.8975	1.5219E-05	0.0000E+00
13	50.00			-0.00231	0.02081	2.08	0.97919	0.9019	2.3609E-05	0.0000E+00
14	15.00			-0.00277	0.01803	1.80	0.98197	0.9073	8.0901E-05	0.0000E+00

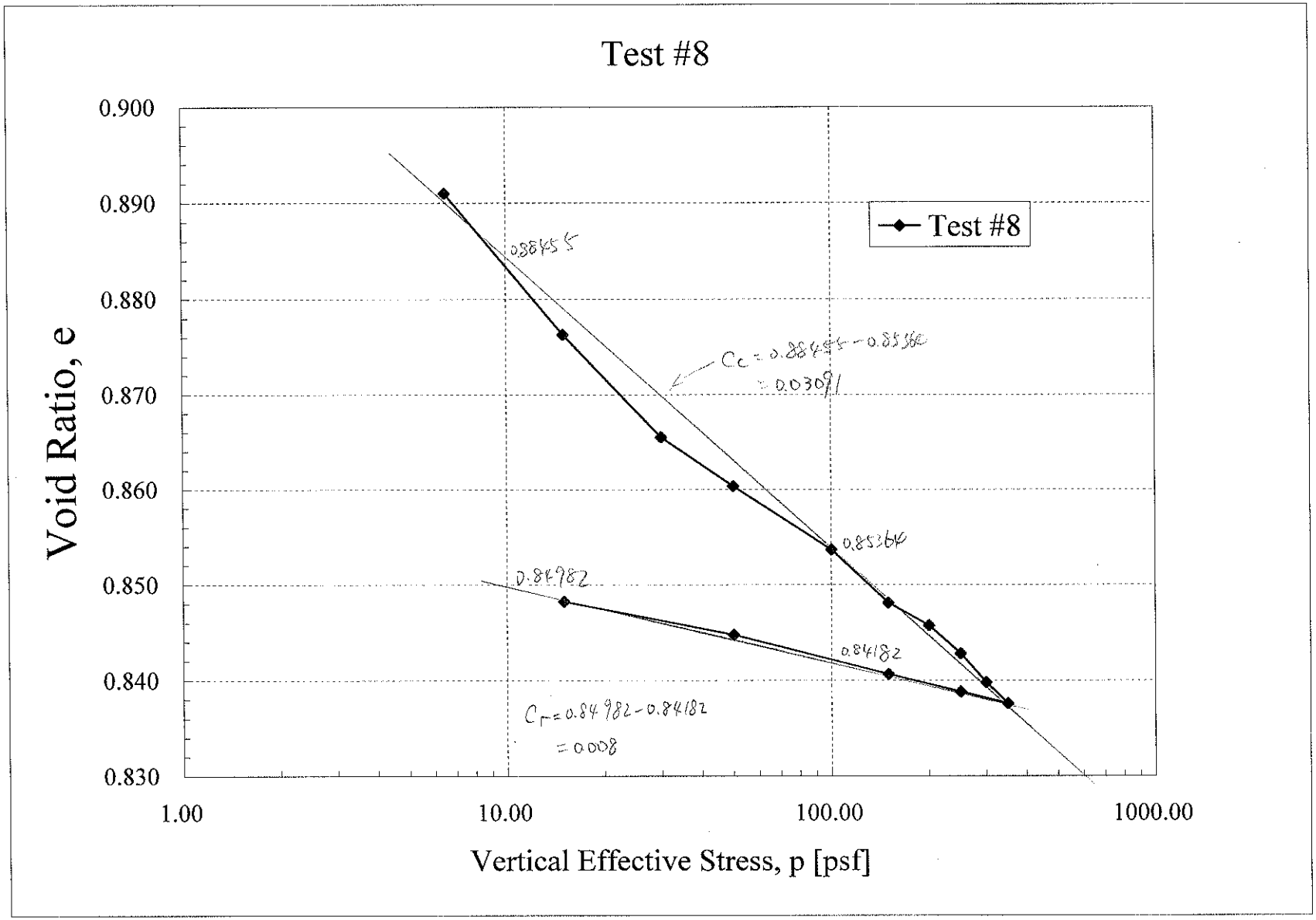
Cr= 0.0102 Cc= 0.03147


Test #7
Test #7
0.000
0.005
0.010
0.015
0.020
0.025
0.030
Deformation,[inch]
1.00
10.00
100.00
1000.00
Vertical Effective Stress, [psf]

Results of Self-weight Consolidation (Contract No. 2503-05-44) Test #8

Loading Steps	Load Increment(psf)	Subtotal Deformation Δ H(inch)	Accumulative Deformation Σ Δ H(inch)	ε_v %	H (inch)	$e = \frac{H - H_s}{H_s}$	m_v (ft^2/lb)	k (ft/sec)
1	6.48	0.00146	0.00146	0.15	0.99854	0.8910		
2	15.00	0.00776	0.00922	0.92	0.99078	0.8763	9.1240E-04	3.3525E-01
3	30.00	0.00570	0.01492	1.49	0.98508	0.8655	3.8347E-04	8.6570E-02
4	50.00	0.00272	0.01764	1.76	0.98236	0.8603	1.3783E-04	3.0799E-02
5	100.00	0.00353	0.02117	2.12	0.97883	0.8537	7.1874E-05	1.1599E-02
6	150.00	0.00295	0.02412	2.41	0.97588	0.8481	6.0343E-05	8.8691E-03
7	200.00	0.00124	0.02536	2.54	0.97464	0.8457	2.5384E-05	3.7128E-03
8	250.00	0.00155	0.02691	2.69	0.97309	0.8428	3.1882E-05	3.2827E-03
9	300.00	0.00158	0.02850	2.85	0.97150	0.8398	3.2525E-05	2.8376E-03
10	350.00	0.00116	0.02965	2.97	0.97035	0.8376	2.3788E-05	1.6555E-03
11	250.00	-0.00065	0.02901	2.90	0.97099	0.8388	6.6525E-06	
12	150.00	-0.00096	0.02805	2.80	0.97195	0.8406	9.8895E-06	
13	50.00	-0.00218	0.02586	2.59	0.97414	0.8448	2.2447E-05	
14	15.00	-0.00183	0.02403	2.40	0.97597	0.8482	5.3818E-05	

Cc=0.031 Cr=0.008 $C_\alpha = 0.0005$


Test #8
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0.890
0.880
0.870
0.860
0.850
0.840
0.830
Void Ratio, e
1.00
10.00
100.00
1000.00
Vertical Effective Stress, p [psf]
Test #8
0.88455
Cc = 0.88455 - 0.85364
= 0.03091
0.85364
0.84982
0.84182
Cr = 0.84982 - 0.84182
= 0.008

APPENDIX F

URS

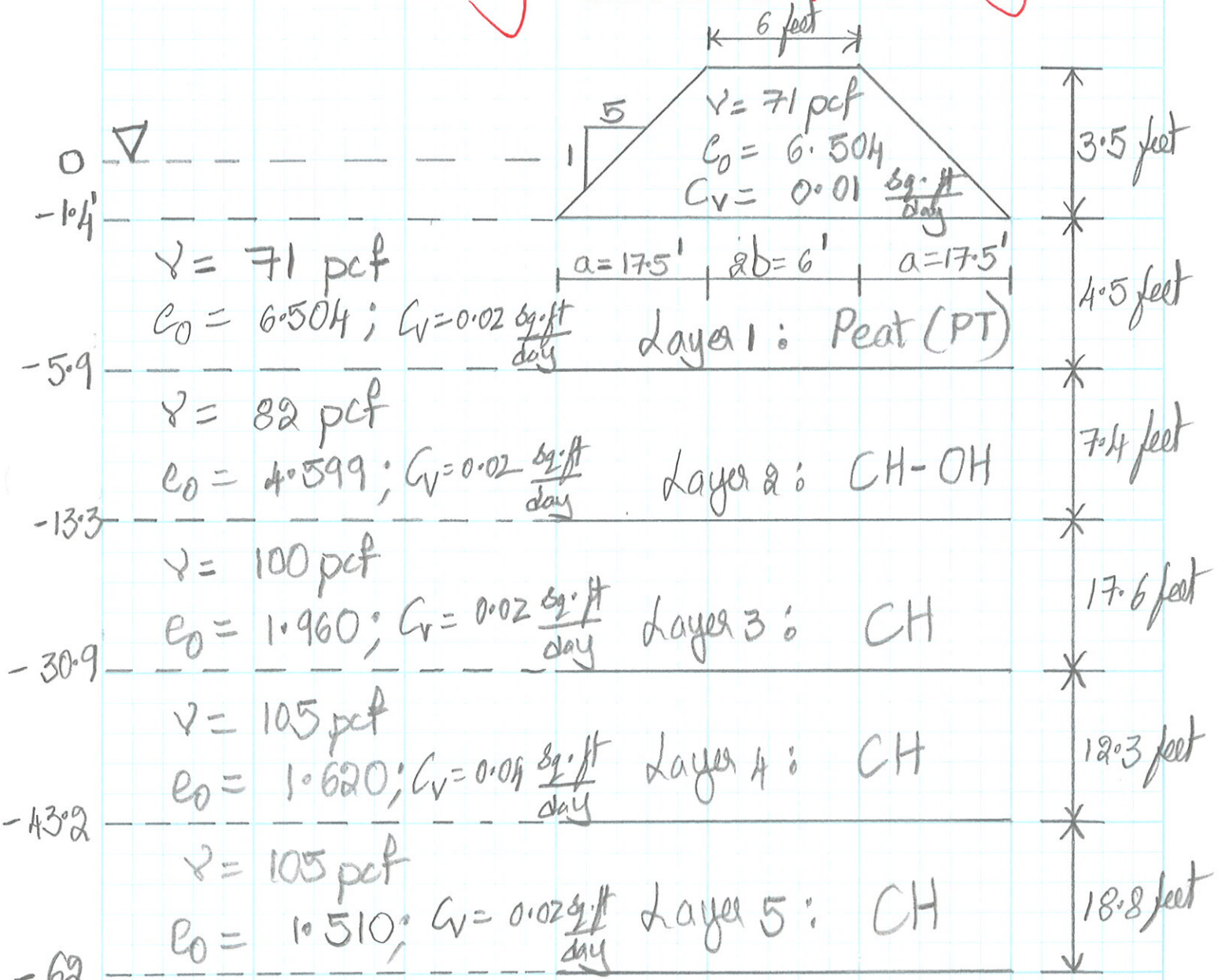
Job Bayou Dupont | Project No. 19228456 | Page 1 of 8

Description Dike Settlement Calculations | Computed by Ananth | Date 06/03/09

Checked by Feng Zhu | Date 07/10/09

Reference

Using Boussinesq's Theory



(*) Settlement were calculated at the center of each layer based on the effective stress and void-ratio at the center of the layer.

Ultimate Settlement, $S = \frac{(H)_{layer} * \Delta e}{1 + (e_0)_{middle}}$

Settlement of Dike :-

Dike height, $H = 3.5$ feet

$e_0 = 6.504$

$\gamma = 71$ pcf

e_0 @ zero effective stress $= (e_0)_M = 6.385$ ($e_{00} = 0.9817 e_0$ Morris (2007))

Effective stress @ mid-pt. of dike $= 71 * \frac{3.5}{2}$

$\sigma_0' = 124.25$ psf

From Consolidation data for B-9 (2-4'):

@ $\sigma_0' = 124.25$, $(e_f)_{middle} = 6.125$

$\Delta e = (e_f)_M - (e_0)_M = 0.26$

$$S_{Dike} = \frac{3.5 * 0.26}{1 + 6.385} = 0.123 \text{ feet}$$

(*) To calculate settlement of soil layers, we divided each layer into several sub-layers.

Settlement of Layer 1 :-

Layer depth, H = 4.5 feet

No. of sub-layers = 8, H_i = 0.5625 feet

Surcharge from dike, $\Delta\sigma = (71 - 62.4)1.4 + 71*(3.5-1.4$

$\Delta\sigma$ = 161.14 psf

γ of layer 1 = 71 pcf

C_c = 6.504

Depth	$(\sigma_o')_{mid}$	$(e_o)_{mid}$	I	$\sigma_{o_m}' + 2I\Delta\sigma$	$(C_r)_m$	$\Delta e = (C_c)_m - (C_r)_m$	$S = \frac{H_i \times \Delta e}{1+(e_o)_m}$
0.5625	2.42	6.49	0.5	163.56	6.0061	0.4866	0.0365
1.1250	7.00	6.48	0.497	167.18	5.9951	0.4837	0.0364
1.6875	11.59	6.46	0.495	171.12	5.9832	0.4818	0.0363
2.2500	16.17	6.45	0.493	175.06	5.9713	0.4798	0.0362
2.8125	20.76	6.44	0.490	178.67	5.9604	0.4769	0.0361
3.3750	25.34	6.42	0.487	182.29	5.9495	0.4740	0.0359
3.9375	29.93	6.41	0.482	185.86	5.9405	0.4691	0.0356
4.500	34.09	6.40	0.475	187.59	5.9335	0.4683	0.0352

S_1 = 0.2888 feet

Settlement of layer-2 :

Layer Depth = 7.4 feet

No. of sublayers = 6, H_i = 1.233 feet

γ = 82 psf

e_0 = 4.599 ; $\Delta\sigma$ = 161.14 psf

Depth	$(\sigma_0')_{mid}$	$(e_0)_{mid}$	I	$(\sigma_0)_m' + 2I\Delta\sigma$	$(e_f)_m$	$\Delta e = (e_0)_m - (e_f)_m$	$\delta = \frac{H_i \Delta e}{1+(e_0)_m}$
5.733	48.76	4.48	0.465	198.62	4.1074	0.3717	0.0837
6.966	72.93	4.42	0.453	218.93	4.0571	0.3621	0.0824
8.199	97.11	4.36	0.437	237.94	4.0099	0.3493	0.0804
9.433	121.28	4.30	0.410	253.41	3.9715	0.3277	0.0763
10.666	145.45	4.24	0.402	275.01	3.9180	0.3213	0.0756
11.900	169.62	4.18	0.375	290.48	3.8796	0.2997	0.0714

δ_2 = 0.4697 feet

Settlement of Layer-3:

Layer Depth = 17.6 feet

No. of sub-layers = 9

$H_i = \frac{17.6}{9} = 1.956$ feet

$\gamma = 100$ pcf

$e_0 = 1.960$

$\Delta\sigma = 161.14$ psf

Depth	$(\sigma_0')_{mid}$	$(e_0)_{mid}$	I	$(\sigma_0')_m + 2I\Delta\sigma$	$(e_f)_m$	$\Delta e = (e_0)_m - (e_f)_m$	$S = \frac{H_i \Delta e}{1+e_0}$
13.856	220.19	1.985	0.360	336.21	1.9062	0.0186	0.0124
15.812	293.57	1.913	0.340	403.15	1.8955	0.0175	0.0118
17.768	366.96	1.901	0.320	470.09	1.8848	0.0165	0.0111
19.724	440.35	1.889	0.308	539.62	1.8689	0.0206	0.0140
21.68	513.74	1.876	0.285	605.59	1.8504	0.0257	0.0175
23.636	587.52	1.856	0.265	672.54	1.8317	0.0239	0.0164
25.592	660.52	1.835	0.250	741.09	1.8125	0.0226	0.0156
27.548	733.91	1.814	0.235	809.65	1.7933	0.0218	0.0147
29.504	807.30	1.794	0.220	878.20	1.7741	0.0199	0.0139

$S_3 = 0.1274$ feet

Settlement of Layer - 4 :

Layer Depth = 12.3 feet

No. of sub-layers = 9

$H_i = \frac{12.3}{9} = 1.367$

$\gamma = 105$ pcf

$e_0 = 1.620$

$\Delta\sigma = 161.14$ psf

Depth	$(\sigma_0')_{mid}$	$(e_0)_{mid}$	I	$(\sigma_0')_M + 2I\Delta\sigma$	$(e_f)_M$	$\Delta e = (e_0)_M - (e_f)_M$	$S = \frac{H_i \Delta e}{1+e_0}$
30.8667	843.843	1.473	0.217	948.48	1.4604	0.0126	0.0070
32.2334	901.135	1.463	0.210	997.46	1.4504	0.0122	0.0068
33.6001	958.427	1.458	0.205	1053.14	1.4415	0.0108	0.0060
34.9668	1015.719	1.443	0.195	1107.21	1.4328	0.0101	0.0056
36.3335	1073.011	1.434	0.185	1161.28	1.4242	0.0095	0.0054
37.7002	1130.303	1.425	0.183	1217.93	1.4151	0.0094	0.0053
39.0669	1187.595	1.415	0.175	1272.64	1.4064	0.0090	0.0051
40.4336	1244.887	1.406	0.170	1328.92	1.3975	0.0088	0.0050
41.8003	1302.180	1.397	0.165	1384.00	1.3886	0.0085	0.0049

$S_4 = 0.0510$ feet

Settlement of Layer-5 :

Layer Depth = 18.8 feet

No. of Sub-layers = 10

$H_i = \frac{18.8}{10} = 1.88$

$\gamma = 105$ pcf

$e_0 = 1.510$

$\Delta\sigma = 161.14$ psf

Depth	$(\sigma_0')_{mid}$	$(e_0)_{mid}$	I	$(\sigma_0')_M + 2I\Delta\sigma$	$(e_f)_M$	$\Delta e = (e_0)_M - (e_f)_M$	$S = \frac{H_i \Delta e}{1+e_0}$
43.68	1398.72	1.3422	0.760	1450.29	1.3360	0.0062	0.0050
45.56	1477.25	1.3327	0.155	1527.20	1.3267	0.0060	0.0156
47.44	1555.78	1.3323	0.150	1604.12	1.3175	0.0058	0.0156
49.32	1634.31	1.3139	0.145	1681.04	1.3083	0.0056	0.0157
51.20	1712.83	1.3045	0.140	1757.95	1.2990	0.0054	0.0158
53.08	1791.36	1.2950	0.135	1834.87	1.2898	0.0052	0.0158
54.96	1869.89	1.2856	0.130	1911.78	1.2806	0.0050	0.0159
56.84	1948.42	1.2762	0.125	1988.70	1.2709	0.0053	0.01624
58.72	2026.94	1.2678	0.120	2065.62	1.2648	0.0031	0.0107
60.60	2105.47	1.2616	0.115	2142.53	1.2586	0.0030	0.0107

$S = 0.1332$ feet

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Description Settlement Calculations | Computed by Ananth T.B | Date 6/3/09

Checked by | Date

Reference

Ultimate Settlement of the soil layers due to the placement of 3.5 feet of Dike is;

$$\delta_U = \delta_{Dike} + \delta_1 + \delta_2 + \delta_3 + \delta_4 + \delta_5$$

$$= 0.123 + 0.2882 + 0.4697 + 0.1274 + 0.051 + 0.1332$$

Ultimate Settlement, $\delta_U = 1.192$ feet

EMBANKMENT

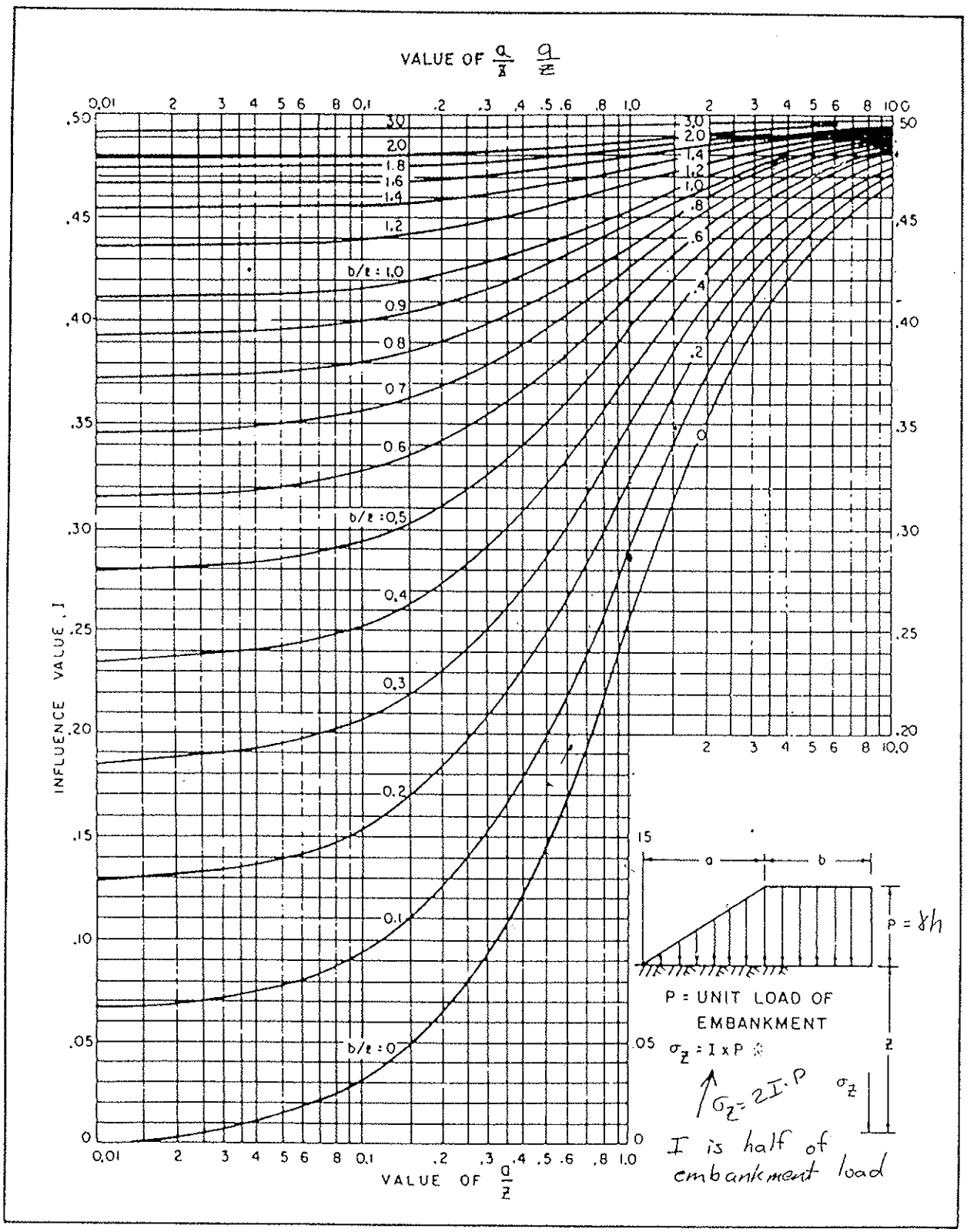
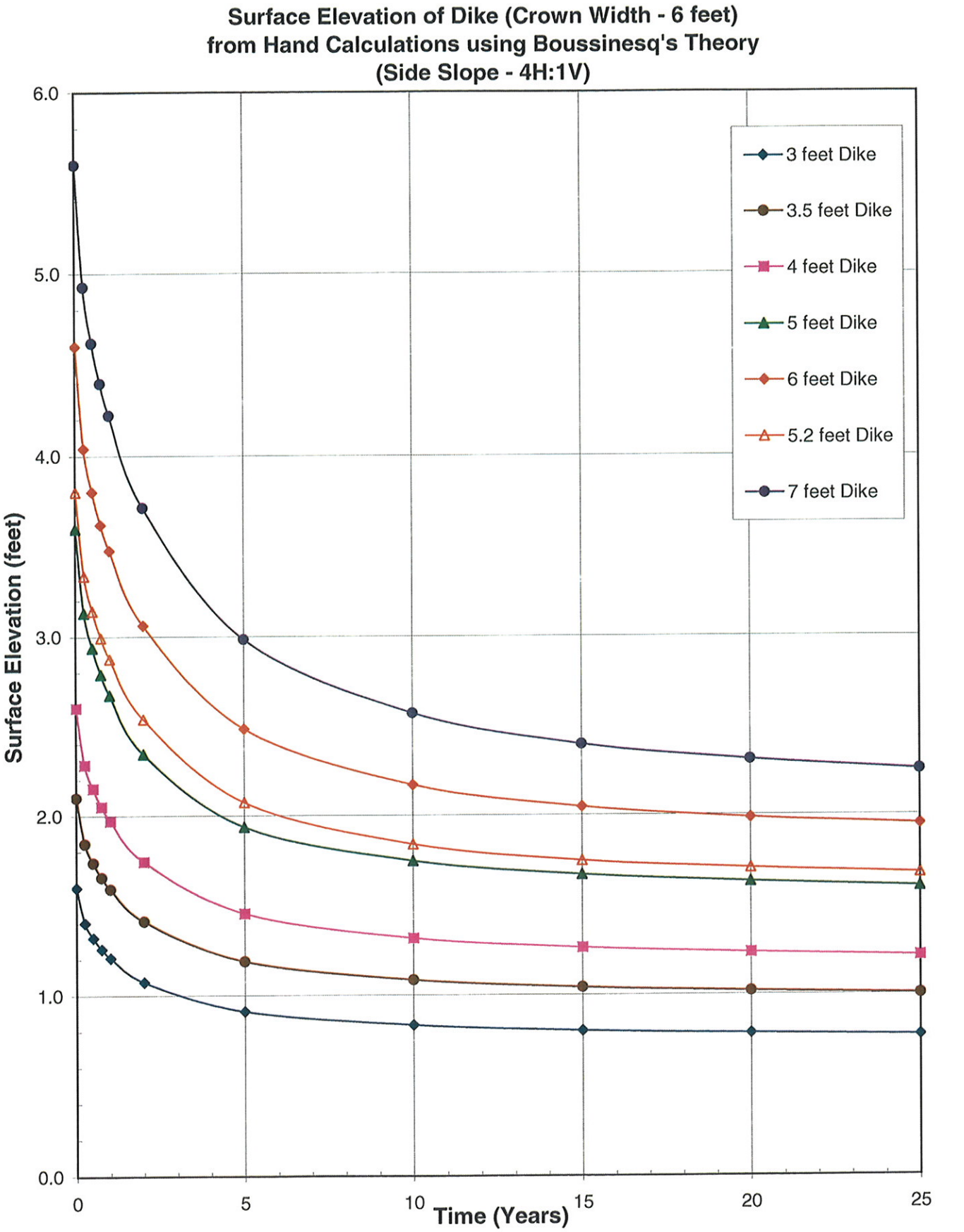


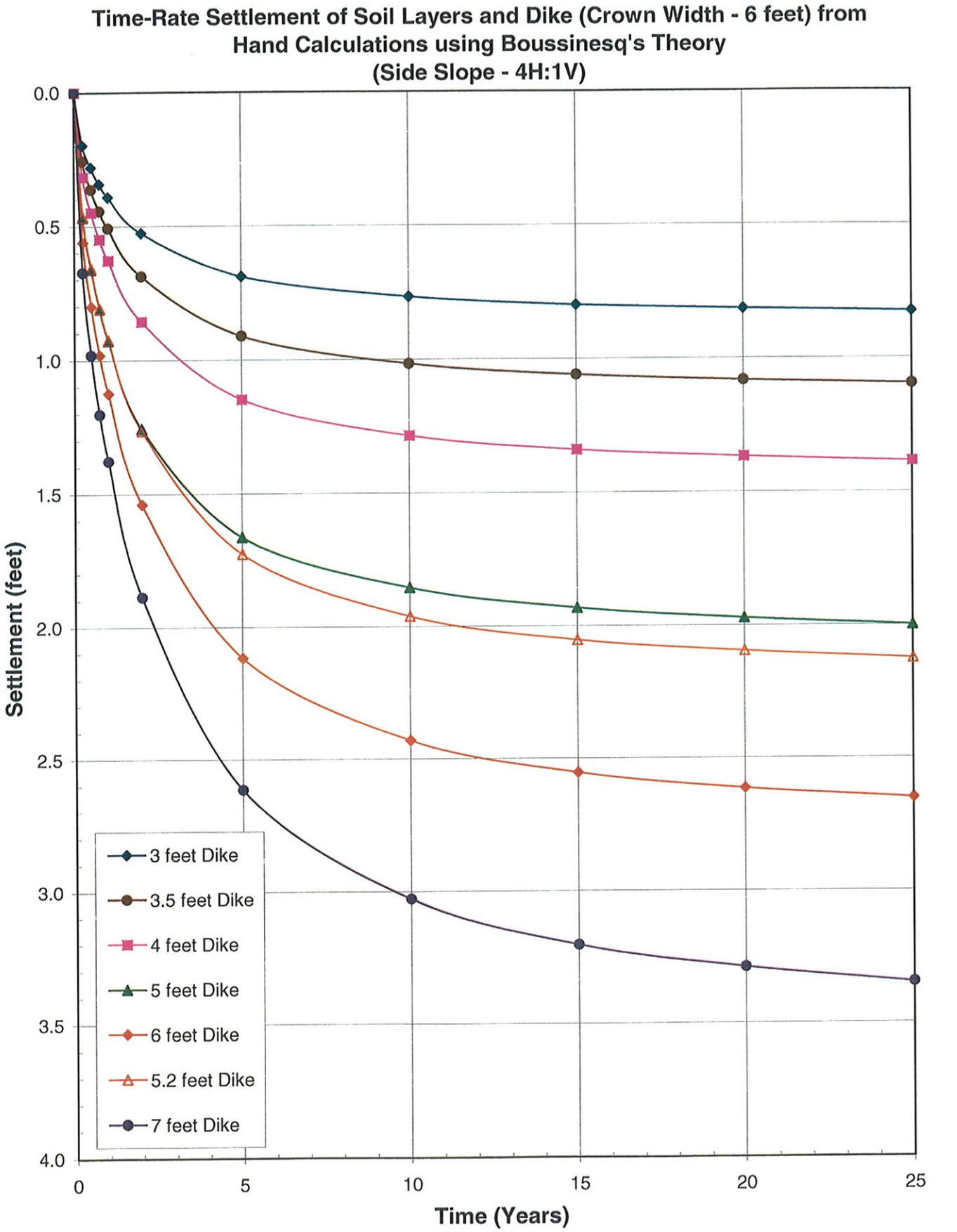
FIGURE 6
Influence Value for Vertical Stress Under Embankment Load of Infinite Length
(Boussinesq Case)

Figure No. 12



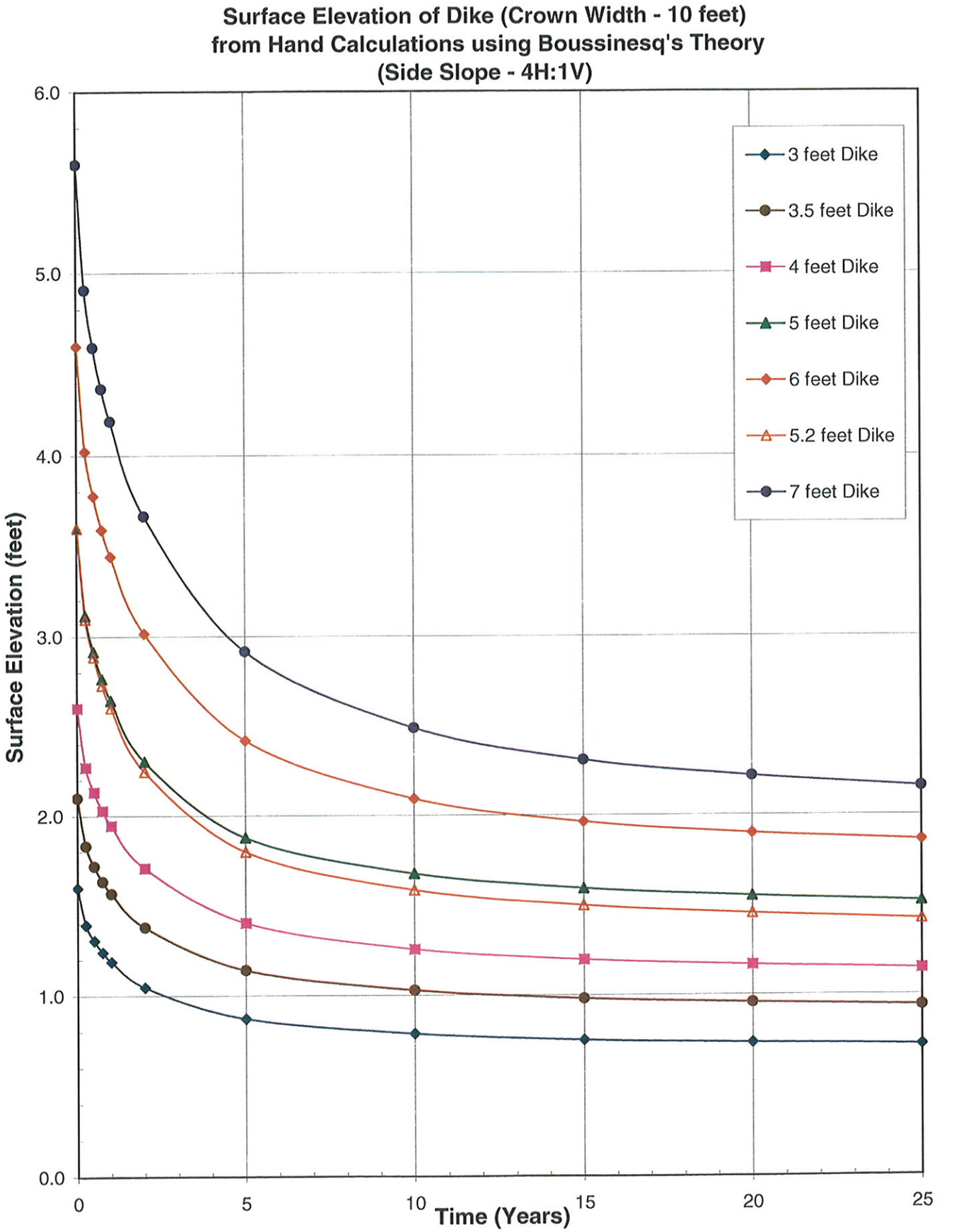
URS CORP.

Figure No. 13



URS CORP.

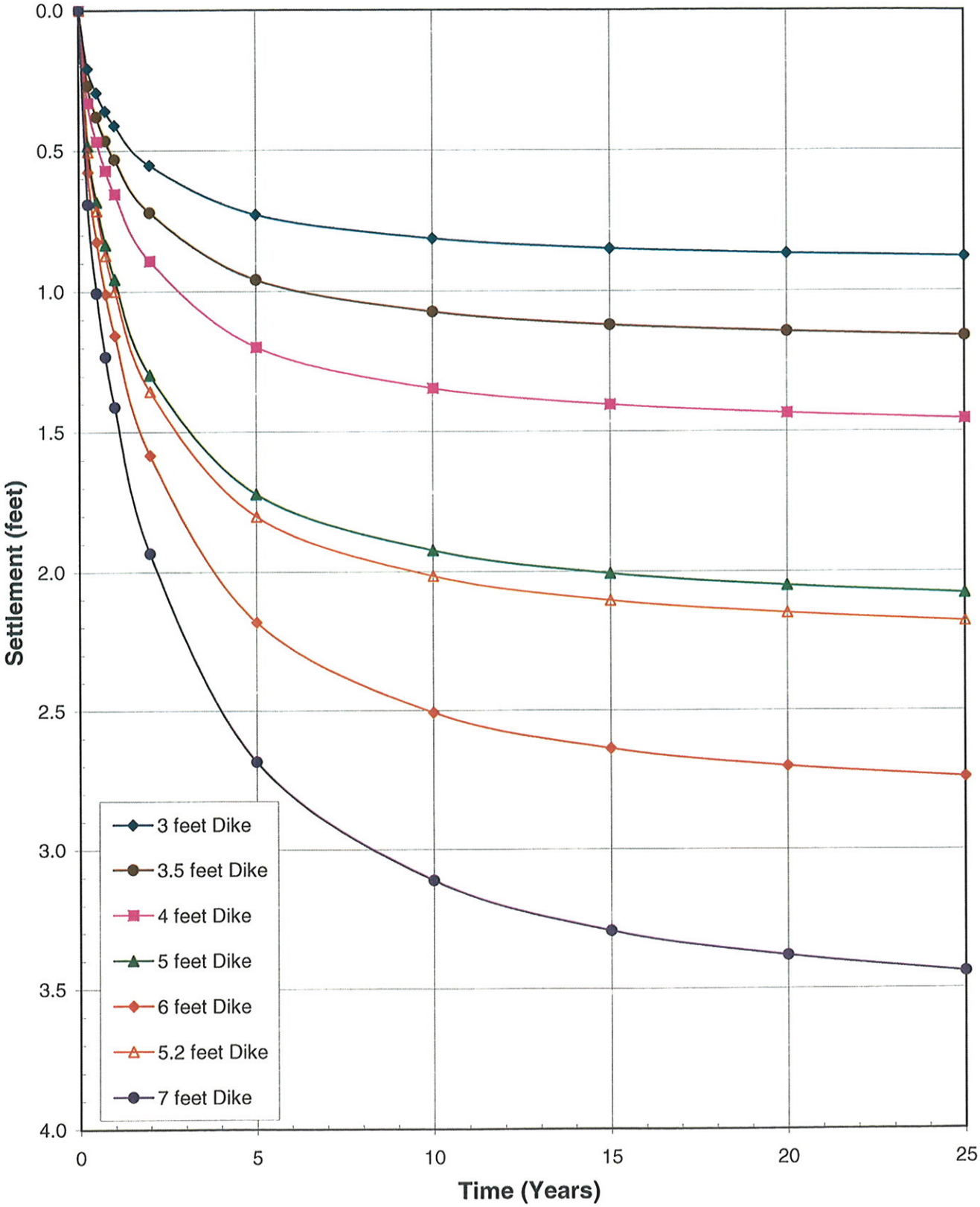
Figure No. 14



URS CORP.

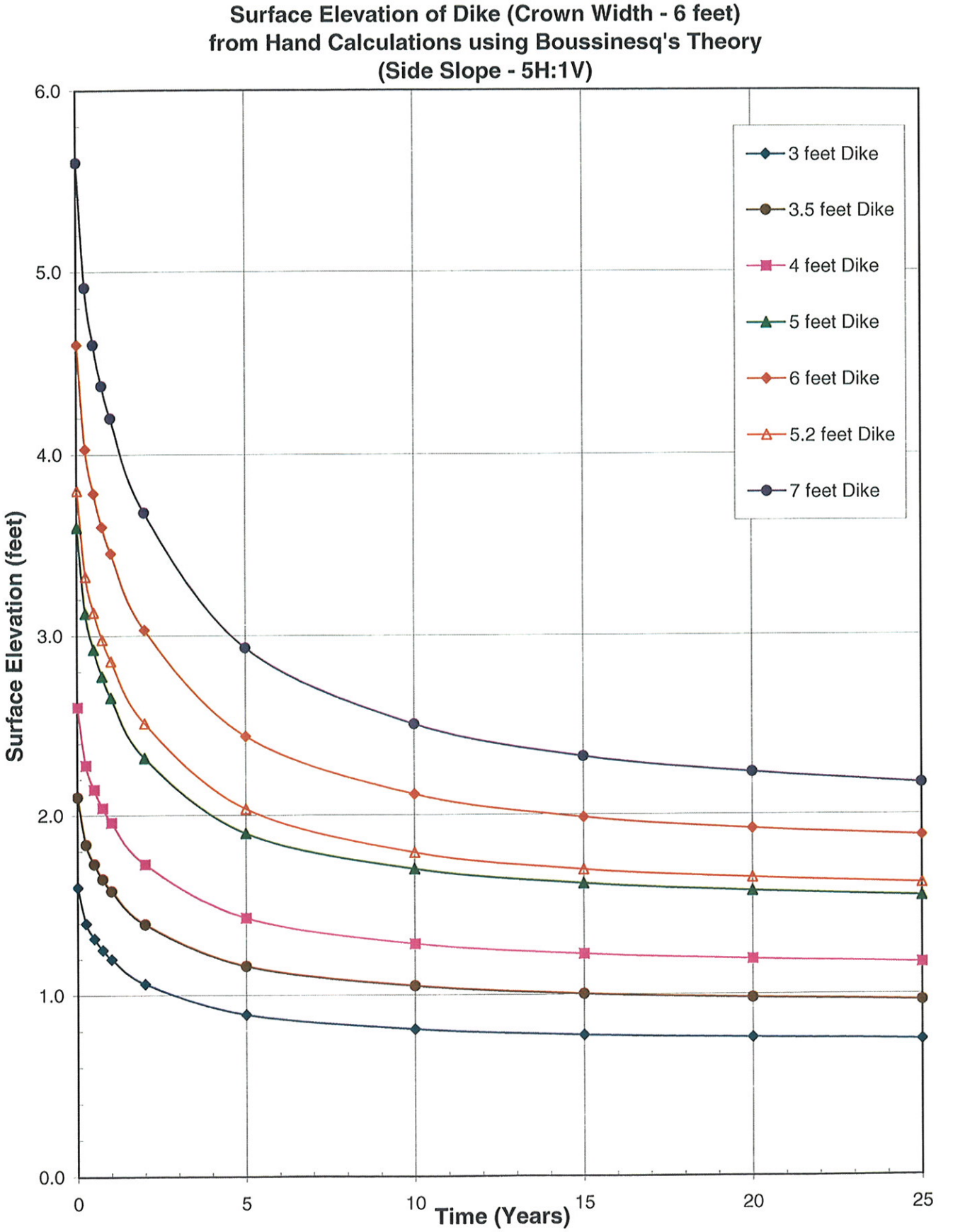
Figure No. 15

Time-Rate Settlement of Soil Layers and Dike (Crown Width - 10 feet) from Hand Calculations using Boussinesq's Theory (Side Slope - 4H:1V)



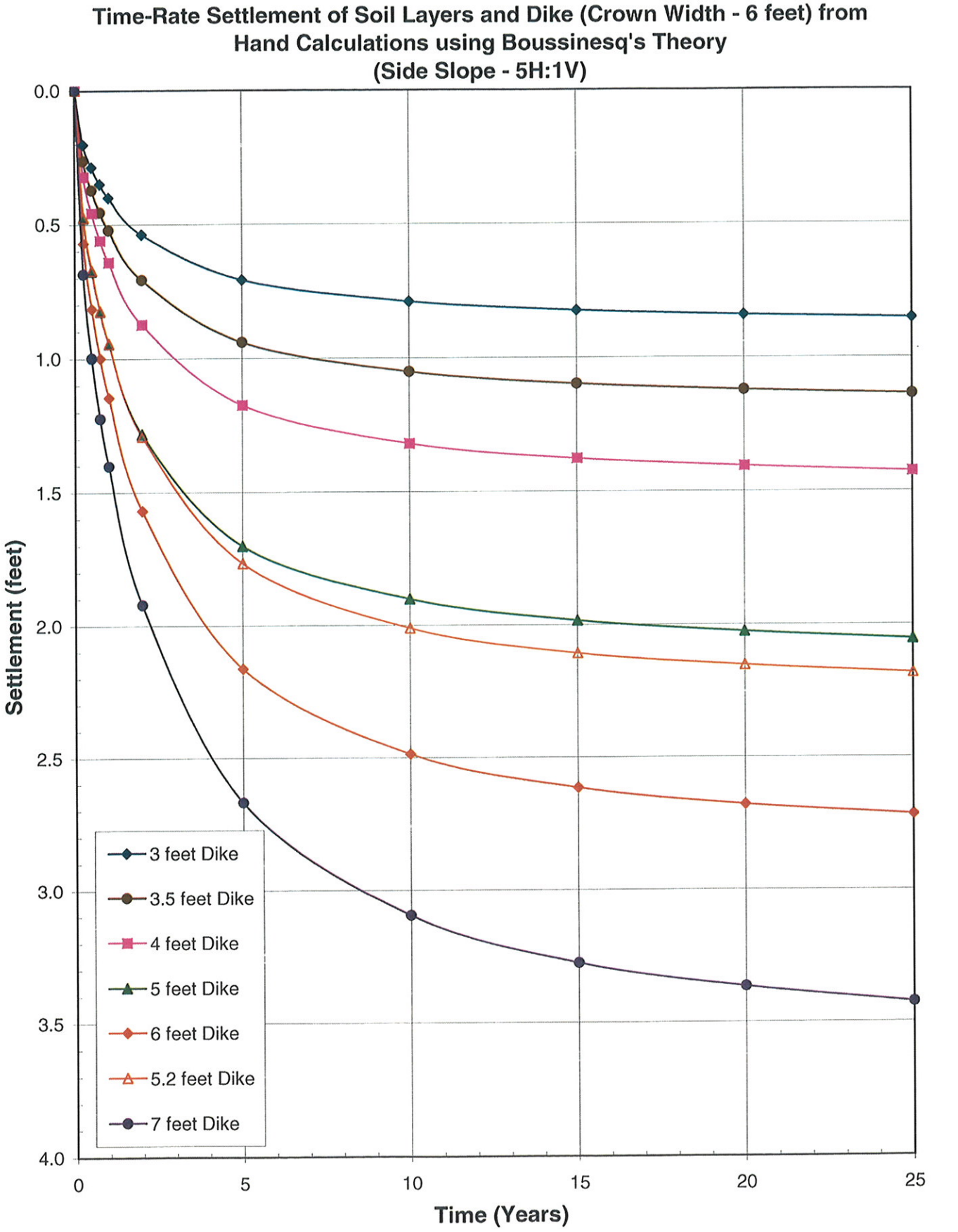
URS CORP.

Figure No. 16



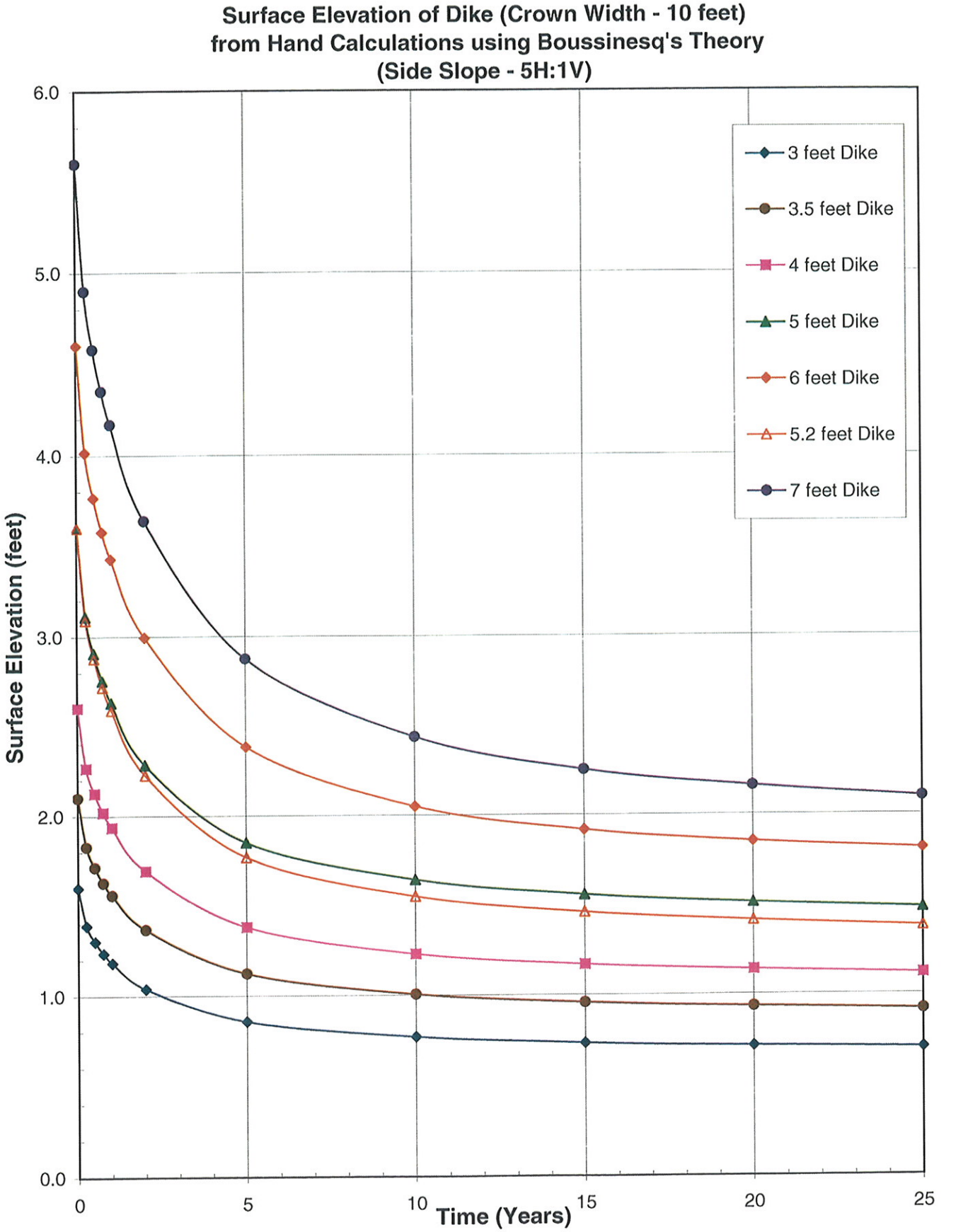
URS CORP.

Figure No. 17



URS CORP.

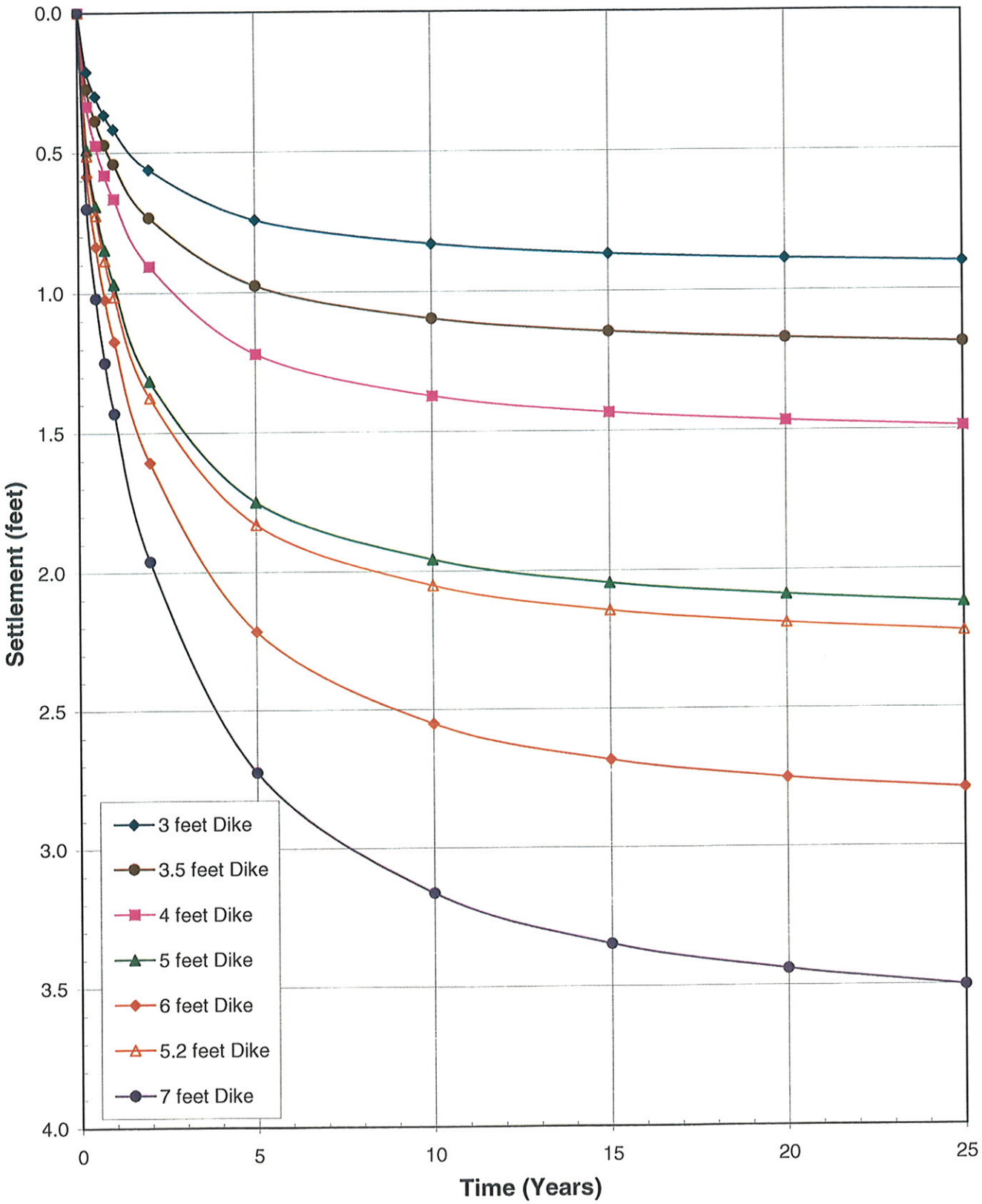
Figure No. 18



URS CORP.

Figure No. 19

Time-Rate Settlement of Soil Layers and Dike (Crown Width - 10 feet) from Hand Calculations using Boussinesq's Theory (Side Slope - 5H:1V)



URS CORP.

(*) Based on the ultimate settlements calculated from the Boussineq's theory, settlement at and time can be computed using,

$$S_t = U * S_U$$

where, U - Degree of Consolidation

→ U is a function of Time-factor

$$\text{Time factor, } T_V = \frac{C_V t}{H_{dr}^2}$$

where, C_V is the coefficient of consolidation which is assured a constant for each layer. Table showing variation of T_V & U is attached.

(*) It is assured that drainage is only in one direction so H_{dr} is the depth of layer

t - time in days @ which "S" is computed.

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Description Time-rate Settlement of Dike | Computed by Ananth T.B | Date 6/3/09 | Sheet ___ of ___

Checked by ___ | Date ___ | Reference

Settlement of Dike

Height of Dike = 35 feet

C_v = 0.01 sq. ft/day

δ_v = 0.123 feet (Ultimate Settlement from Boussinesq's theo

Time (Days)	$T_v = \frac{C_v t}{H_{dr}^2}$	U (%)	$\delta_T = \frac{U}{100} \times \delta_v$
0	0	0	0
90	0.0735	30.7	0.038
180	0.0469	43.6	0.054
270	0.2204	53.2	0.065
365	0.2980	61.1	0.075
730	0.5959	81.4	0.100
1825	1.4898	98	0.121
3650	2.9796	100	0.123
5475	4.4694	100	0.123
7300	5.9592	100	0.123
9000	7.3469	100	0.123

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Description Time-rate Settlement of Dike | Computed by Ananth T.B | Date 6/3/09 | Sheet ___ of ___

Checked by ___ | Date ___ | Reference

Settlement of Layer 1

Height of Layer 1 = 4.5 feet

C_v = 0.02 sq.ft/day

δ_v = 0.2882 feet (Ultimate Settlement from Boussinesq's theo

Time (Days)	$T_v = \frac{C_v t}{H_{dr}^2}$	U (%)	$\delta_T = \frac{U}{100} \times \delta_v$
0	0	0	0
90	0.089	34	0.098
180	0.178	48	0.1383
270	0.267	58.4	0.1683
365	0.360	66.7	0.1922
730	0.721	86.3	0.2487
1825	1.802	100	0.2882
3650	3.605	100	0.2882
5475	5.407	100	0.2882
7300	7.210	100	0.2882
9000	8.889	100	0.2882

URS

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Description Time-rate Settlement of Dike | Computed by Ananth T.B | Date 6/3/09 | Sheet ___ of ___

Checked by ___ | Date ___ | Reference

Settlement of Layer 2

Height of Layer 2 = 7.4 feet

C_v = 0.02 sq.ft/day

δ_v = 0.4697 feet (Ultimate Settlement from Boussinesq's theo

Time (Days)	$T_v = \frac{C_v t}{H_{dr}^2}$	U (%)	$\delta_T = \frac{U}{100} \times \delta_v$
0	0	0	0
90	0.033	20.5	0.0963
180	0.066	29.2	0.1372
270	0.099	36.0	0.1691
365	0.133	41.0	0.1926
730	0.267	58.0	0.2724
1825	0.667	84.3	0.3960
3650	1.333	97.0	0.4556
5475	2.000	100	0.4697
7300	2.666	100	0.4697
9000	3.287	100	0.4697

Settlement of Layer 3

Height of Layer 3 = 17.6 feet

C_v = 0.02 Sq. ft/day

δ_v = 0.1274 feet (Ultimate Settlement from Boussinesq's Theo

Time (Days)	$T_v = \frac{C_v t}{H_{dr}^2}$	U (%)	$\delta_T = \frac{U}{100} \times \delta_v$
0	0	0	0
90	0.006	8.7	0.011
180	0.012	12.6	0.016
270	0.017	15.1	0.019
365	0.024	17.5	0.022
730	0.047	24.4	0.031
1825	0.118	38.8	0.049
3650	0.236	54.6	0.070
5475	0.353	66.1	0.084
7300	0.471	74.7	0.095
9000	0.581	80.7	0.103

Settlement of Layer 4

Height of Layer 4 = 12.3 feet

C_v = 0.04 sq.ft/day

δ_v = 0.051 feet (Ultimate Settlement from Boussinesq's Theo

Time (Days)	$T_v = \frac{C_v t}{H_{dr}^2}$	U (%)	$\delta_T = \frac{U}{100} \times \delta_v$
0	0	0	0
90	0.024	17.5	0.009
180	0.048	24.4	0.012
270	0.071	30.1	0.015
365	0.097	35.2	0.018
730	0.193	49.5	0.025
1825	0.483	75.3	0.038
3650	0.965	92.5	0.047
5475	1.448	97.7	0.050
7300	1.930	100	0.051
9000	2.380	100	0.051

Settlement of Layer 5 :-

Height of Layer 5 = 18.8 feet

C_v = 0.02 sq.ft/day

δ_v = 0.1332 feet (Ultimate Settlement from Boussinesq's Theo

Time (Days)	$T_v = \frac{C_v t}{H_{dr}^2}$	U (%)	$\delta_T = \frac{U}{100} \times \delta_v$
0	0	0	0
90	0.005	8.0	0.0107
180	0.010	11.2	0.0149
270	0.015	13.8	0.0184
365	0.021	16.3	0.0217
730	0.041	22.8	0.0304
1825	0.103	36.2	0.0482
3650	0.207	51.4	0.0685
5475	0.310	62.3	0.0830
7300	0.413	70.8	0.0943
9000	0.509	76.9	0.1024

Table 10.5 Variation of T_v with U

U (%)	T_v	U (%)	T_v	U (%)	T_v
0	0	34	0.0907	68	0.377
1	0.00008	35	0.0962	69	0.390
2	0.0003	36	0.102	70	0.403
3	0.00071	37	0.107	71	0.417
4	0.00126	38	0.113	72	0.431
5	0.00196	39	0.119	73	0.446
6	0.00283	40	0.126	74	0.461
7	0.00385	41	0.132	75	0.477
8	0.00502	42	0.138	76	0.493
9	0.00636	43	0.145	77	0.511
10	0.00785	44	0.152	78	0.529
11	0.0095	45	0.159	79	0.547
12	0.0113	46	0.166	80	0.567
13	0.0133	47	0.173	81	0.588
14	0.0154	48	0.181	82	0.610
15	0.0177	49	0.188	83	0.633
16	0.0201	50	0.197	84	0.658
17	0.0227	51	0.204	85	0.684
18	0.0254	52	0.212	86	0.712
19	0.0283	53	0.221	87	0.742
20	0.0314	54	0.230	88	0.774
21	0.0346	55	0.239	89	0.809
22	0.0380	56	0.248	90	0.848
23	0.0415	57	0.257	91	0.891
24	0.0452	58	0.267	92	0.938
25	0.0491	59	0.276	93	0.993
26	0.0531	60	0.286	94	1.055
27	0.0572	61	0.297	95	1.129
28	0.0615	62	0.307	96	1.219
29	0.0660	63	0.318	97	1.336
30	0.0707	64	0.329	98	1.500
31	0.0754	65	0.304	99	1.781
32	0.0803	66	0.352	100	∞
33	0.0855	67	0.364		

Logarithm-of-Time Method

For a given incremental loading of the laboratory test, the specimen deformation against log-of-time plot is shown in Figure 10.25. The following constructions are needed to determine c_v:

1. Extend the straight-line portions of primary and secondary consolidations to intersect at A. The ordinate of A is represented by d_{100} – that is, the deformation at the end of 100% primary consolidation.
2. The initial curved portion of the plot of deformation versus log t is approximated to be a parabola on the natural scale. Select times t_1 and t_2 on the curved portion such that $t_2 = 4t_1$. Let the diff-

APPENDIX G

URS

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Description Slope Stability Analysis | Computed by Ananth | Date 6/30/09 | Sheet ___ of ___

Checked by Mahendra | Date 6/30/09 | Reference

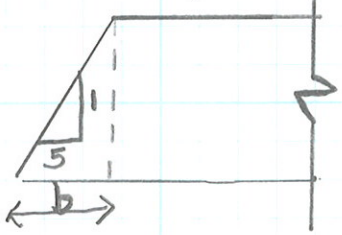
Factor of Safety against Sliding of Dike

Height of the Dike = 5 feet

Side slope = 5H : 1V

Long term angle of internal friction, $\phi' = 12^0$

$K_a = \tan^2\left(45 - \frac{\phi'}{2}\right) = \tan^2 39 = 0.66$

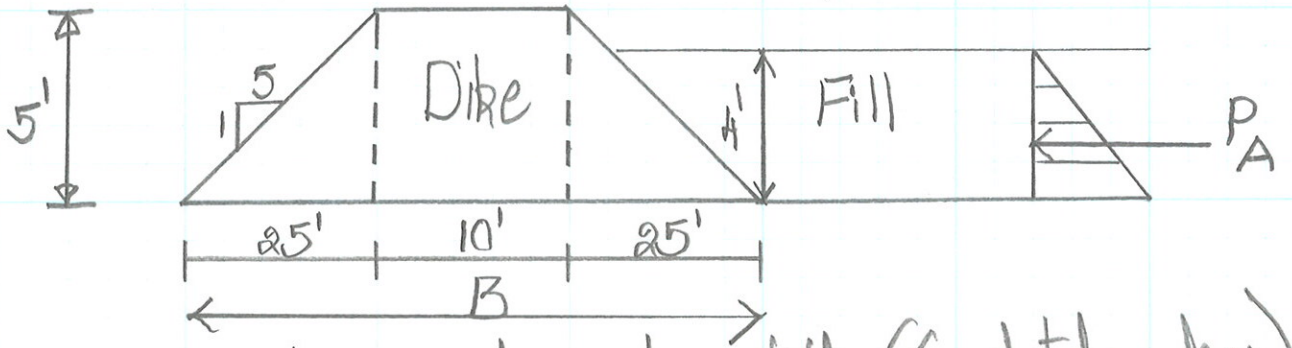


$b = 5 \times 5 = 25$

Factor of Safety $(FS) = \frac{b \tan\phi'}{K_a H} = \frac{25 \tan 12^0}{0.66 * 5}$

$FS = 1.61 > 1.5$ (O.K)

Factor of Safety against sliding of Dike due to Fill



Active force due to fill (Completely dry):

$\phi' = 30^\circ$, $\gamma = 116$ pcf, $H_{fill} = 4'$

$$K_a = \tan^2\left(45 - \frac{\phi}{2}\right) = \tan^2 30^\circ = 0.33$$

$$(P_A)_F = \frac{1}{2} K_a \gamma H_{fill}^2 = 306.24 \text{ lb/ft}$$

Active force from dike:

$(K_a)_{dike} = 0.66$, $\gamma = 71$ pcf, $H_{Dike} = 5'$

$$(P_A)_{Dike} = \frac{1}{2} K_a \gamma H_{Dike}^2 = 585.75 \text{ lb/ft}$$

Total Active force, $P_A = 892$ lb/ft

Resisting force, $P_R = B * S_U$

S_U (Strength of top soil layer) = 75 psf

$B = 25 + 10 + 25 = 60$ feet

$P_R = 60 * 75 = 4500$ lb/ft

(or) due to Weight of Dike

Dike Area $= \left[\left(\frac{1}{2} * 25 * 5\right) * 2\right] + [10 \times 5]$

$A = 175$ sq. ft

Weight of Dike $= \gamma * A = 71 * 175 = 12425$ lb/ft

$\phi' = 12^0$

Resisting force $= \gamma A \tan\phi' = 8640$ lb/ft

Resisting force, $P_R = 2640$ lb/ft

Factor of Safety $= \frac{P_R}{P_A} = \frac{2640}{892} = 2.96 > 1.5$

Long-term Stability :-

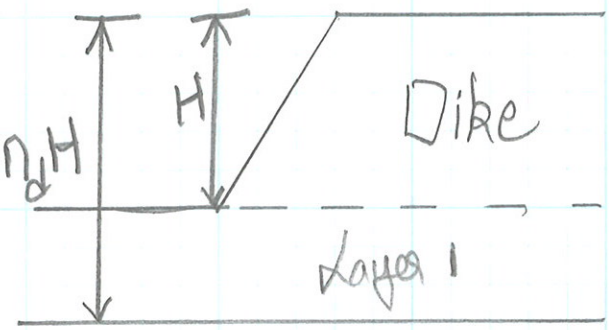
$\phi' = 12^\circ$, Side slope, $\beta = \tan^{-1}\left(\frac{1}{5}\right) = 11.3^\circ$

$F.S = \frac{\tan\phi'}{\tan\beta} = 1.06$ (OK)

Short-term stability :-

Height of Dike = 5'

$n_d * H = 9.5$



$n_d = 1.9$

$N_s = 7.2$ (for $\beta = 11.31^\circ$ & $n_d = 1.9$)*

* - Refer following chart

$$H' = \frac{N_s * C}{\gamma} = \frac{7.2 * 75}{71} = 7.6$$

$$FS = \frac{H'}{H} = \frac{7.6}{5} = 1.52 \text{ (OK)}$$

From the calculations, the dike is safe against sliding due to the placement of fill.

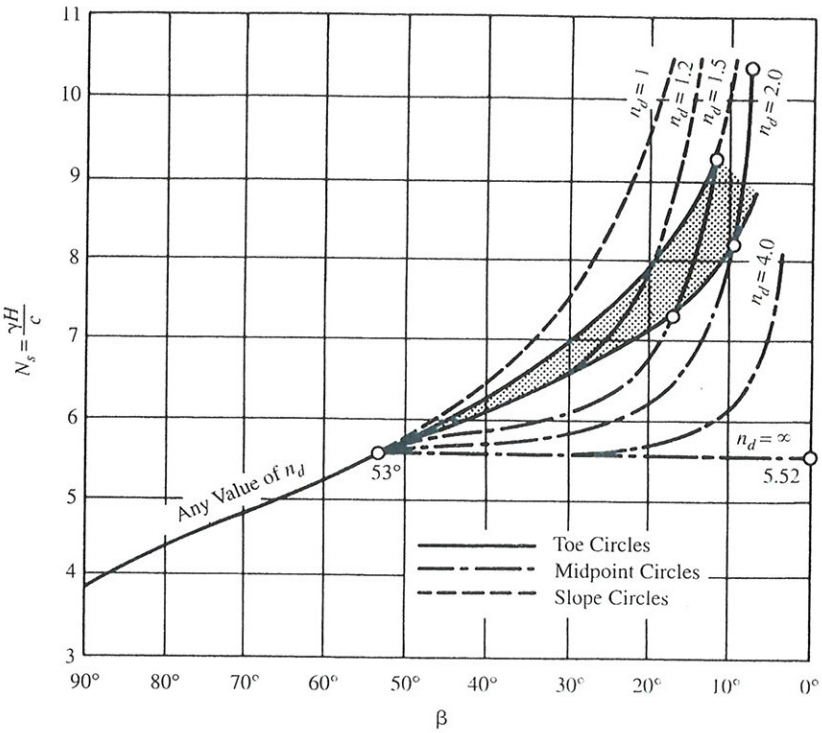


FIGURE 14–9 Stability numbers and types of slope failures for $\phi = 0$ [5, 6].

Reference : Soils and Foundations Textbook
Authors: Cheng Liu and Jack · B · Evett

EXAMPLE 14–4

Given

The slope and data shown in Figure 14–11.

Required

Factor of safety against failure, by the stability number method.

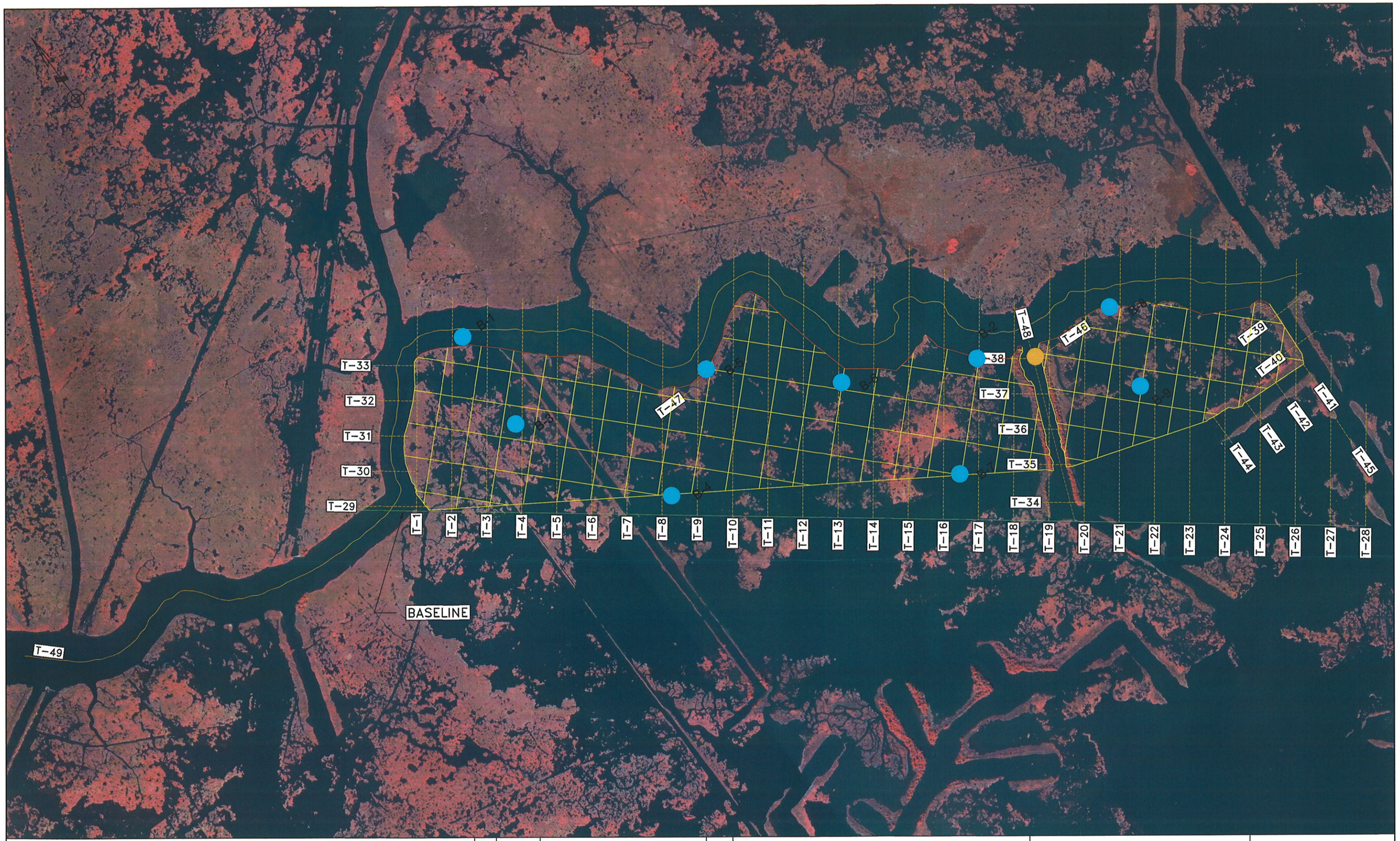
Solution

Because the given angle of internal friction (ϕ) of 10° is greater than 3°, the failure surface will be a toe circle.

Try F.S.$_\phi$ = 1

$$\tan \phi_{\text{required}} = \frac{\tan \phi_{\text{given}}}{\text{F.S.}_\phi} = \frac{\tan 10°}{1}$$

$$\phi_{\text{required}} = 10°$$



1000' 500' 0' 1000' 2000'

REV.	DATE	DESCRIPTION	BY

URS
7389 Florida Blvd., Suite 300
Baton Rouge, Louisiana 70806
225/922-5700

DRAWN BY: ESL
DESIGNED BY:

BAYOU DUPONT MARSH CREATION & RIDGE RESTORATION PROJECT

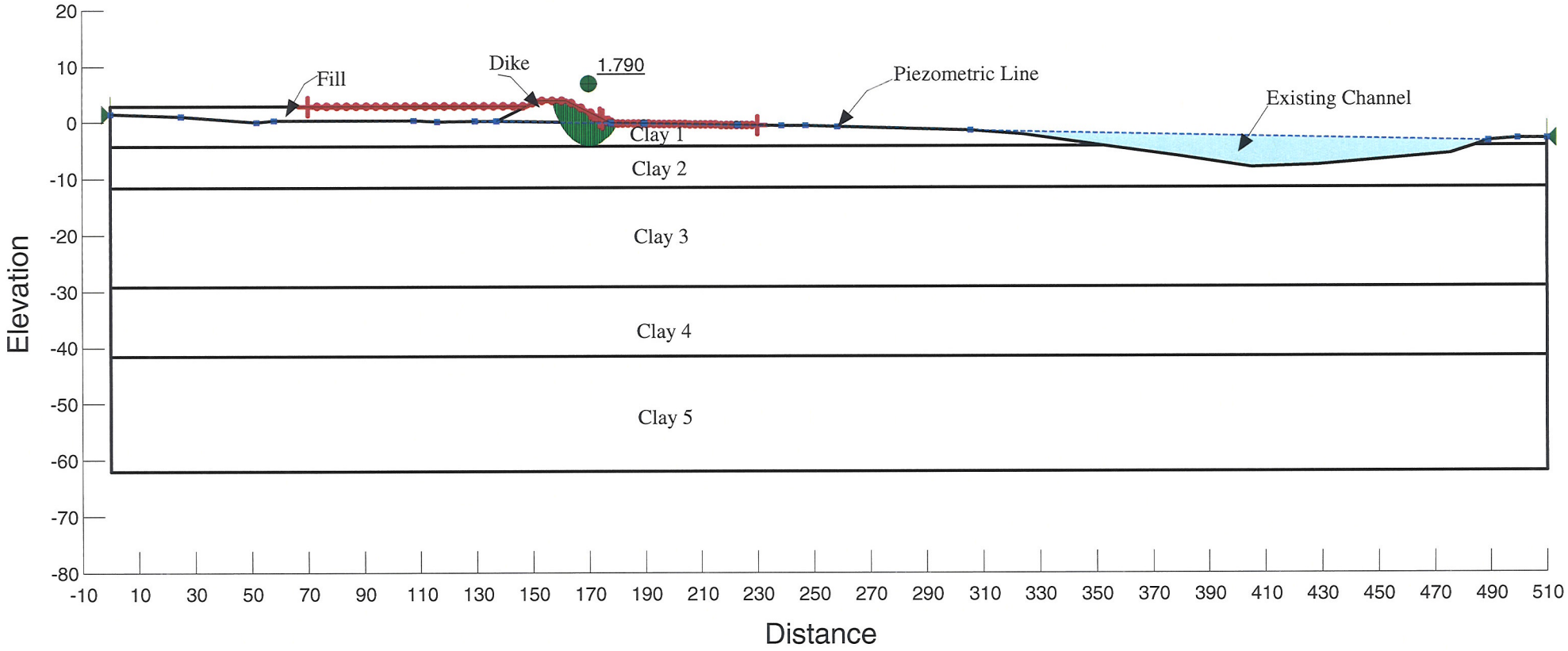
STATE PROJECT NUMBER: BA-48
FEDERAL PROJECT NUMBER: BA-48
APPROVED BY:

TRANSECT LAYOUT VICINITY MAP

DATE: DECEMBER 2008
FIGURE NO. 20

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: CIRCULAR
SLOPE: 4H TO 1V
DIKE Ht: 4.0'; FILL Ht: 3.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

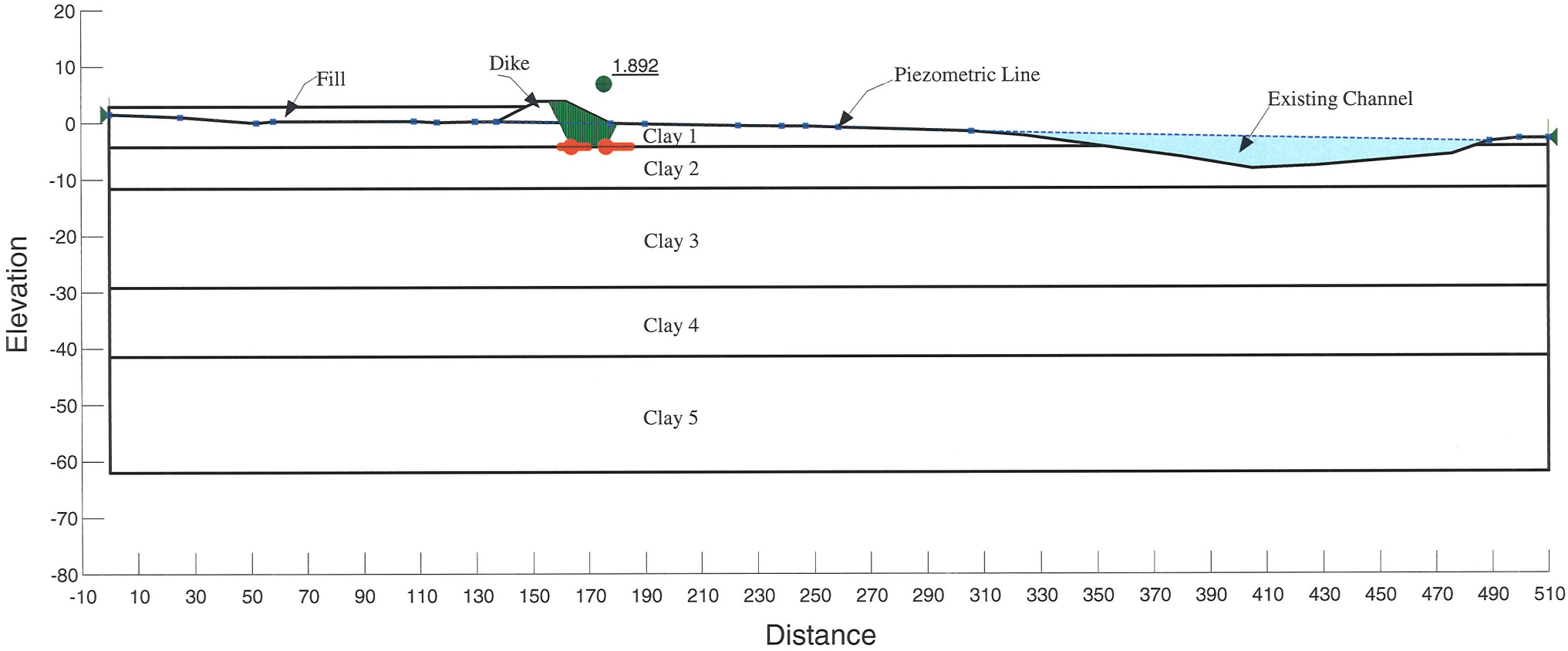


URS CORP.

Figure 21

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: WEDGE
SLOPE: 4H TO 1V
DIKE Ht: 4.0'; FILL Ht: 3.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

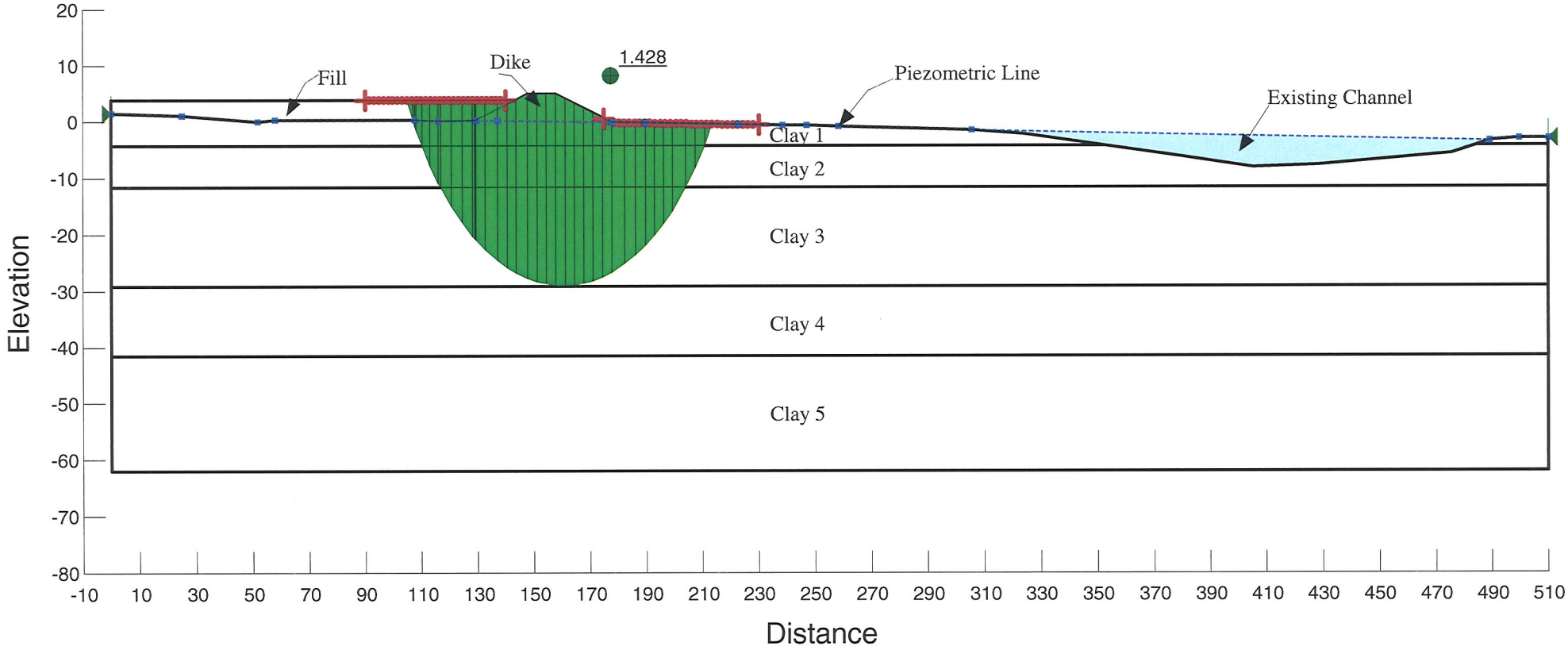


URS CORP.

Figure 22

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: CIRCULAR
SLOPE: 4H TO 1V
DIKE Ht: 5.0'; FILL Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

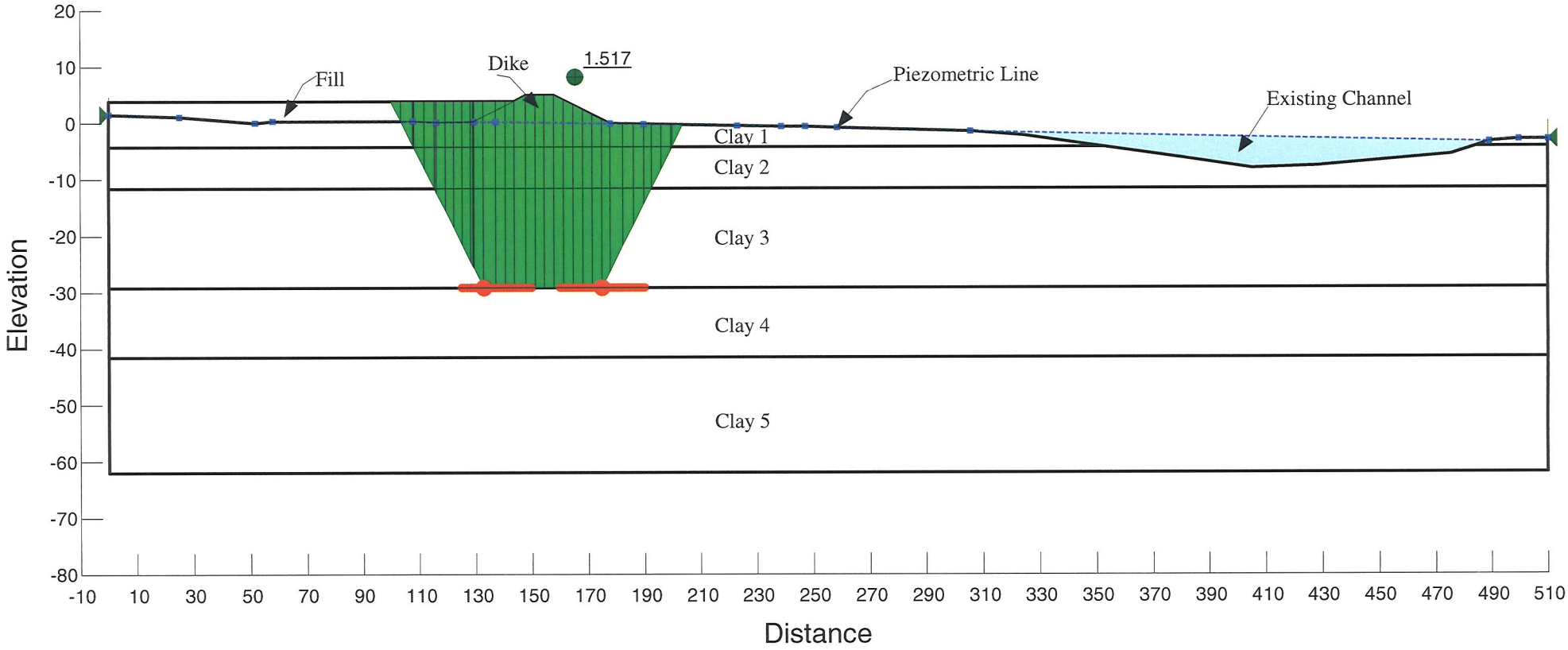


URS CORP.

Figure 23

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: WEDGE
SLOPE: 4H TO 1V
DIKE Ht: 5.0'; FILL Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

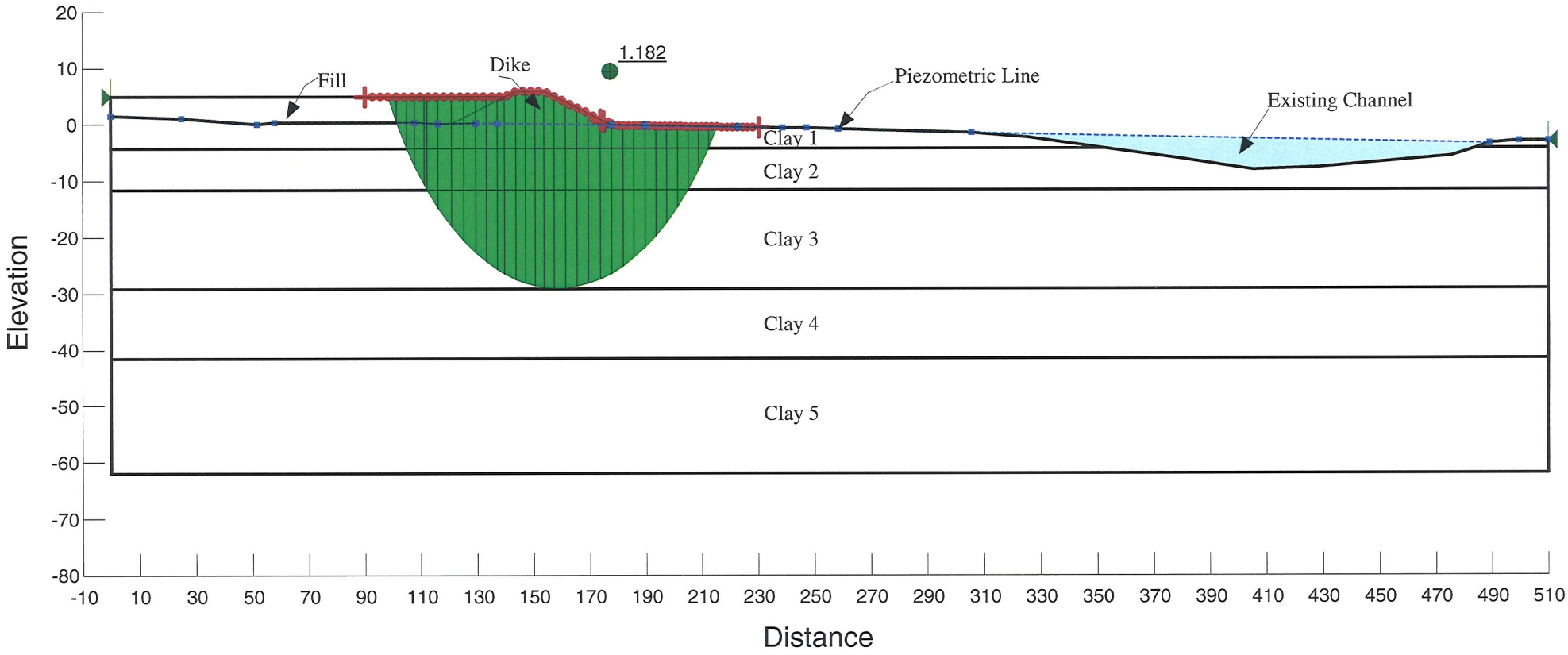


URS CORP.

Figure 24

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: CIRCULAR
SLOPE: 4H TO 1V
DIKE Ht: 6.0'; FILL Ht: 5.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

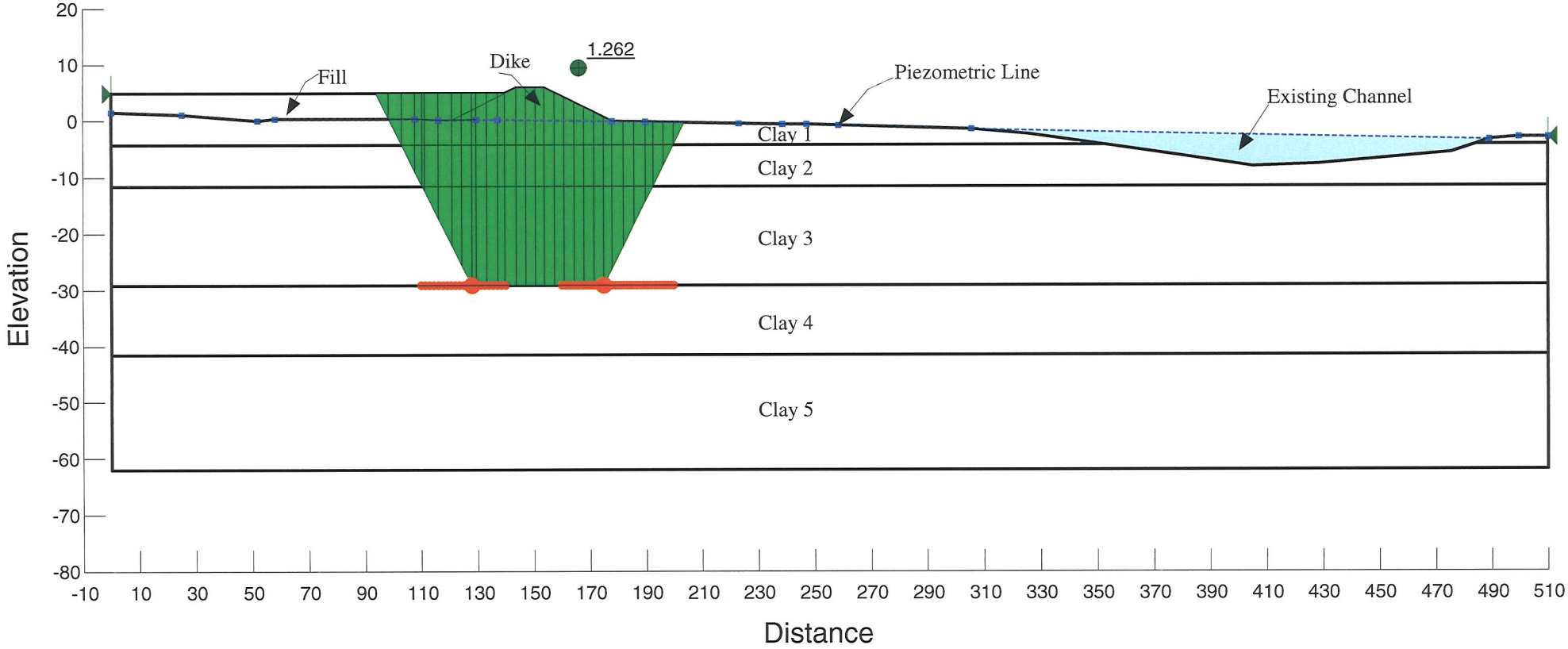


URS CORP.

Figure 25

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: WEDGE
SLOPE: 4H TO 1V
DIKE Ht: 6.0'; FILL Ht: 5.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

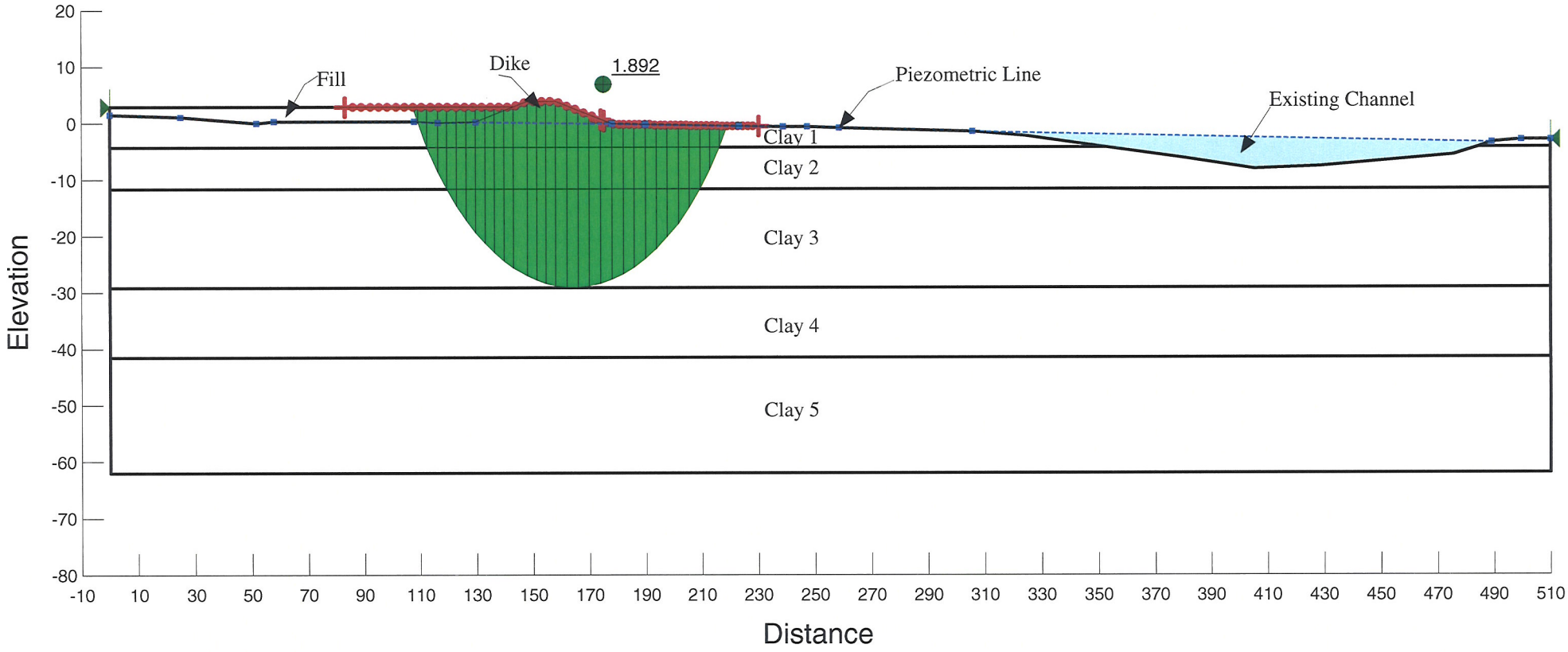


URS CORP.

Figure 26

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: CIRCULAR
SLOPE: 5H TO 1V
DIKE Ht: 4.0'; FILL Ht: 3.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

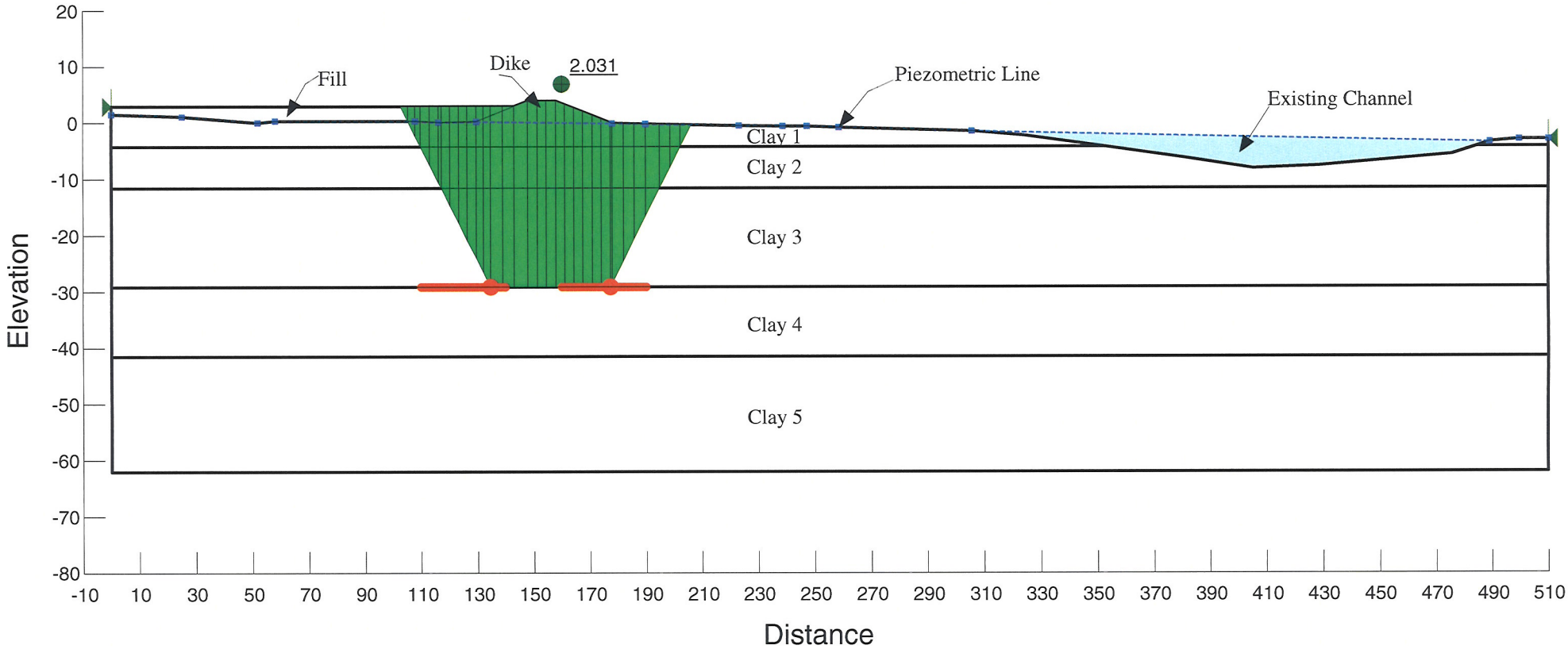


URS CORP.

Figure 27

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: WEDGE
SLOPE: 5H TO 1V
DIKE Ht: 4.0'; FILL Ht: 3.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

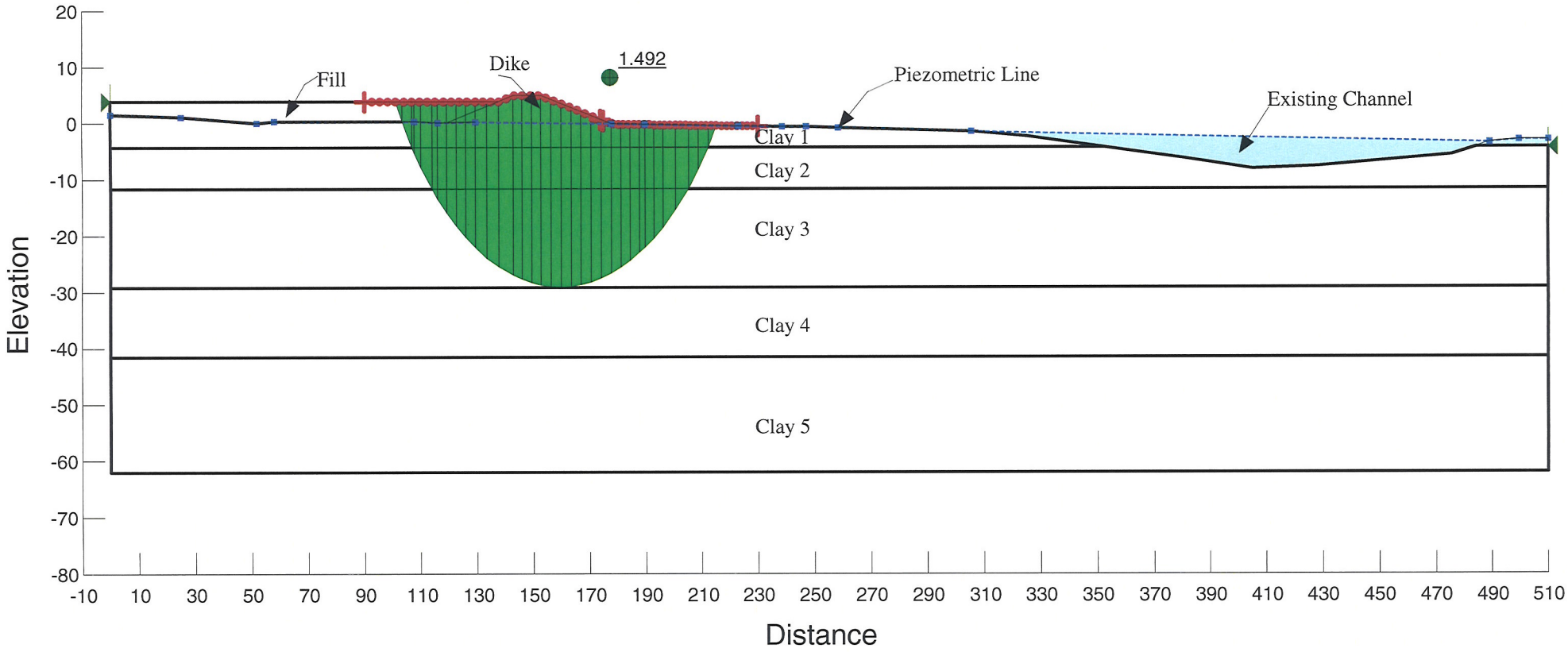


URS CORP.

Figure 28

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: CIRCULAR
SLOPE: 5H TO 1V
DIKE Ht: 5.0'; FILL Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °



URS CORP.

Figure 29

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: WEDGE
SLOPE: 5H TO 1V
DIKE Ht: 5.0'; FILL Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

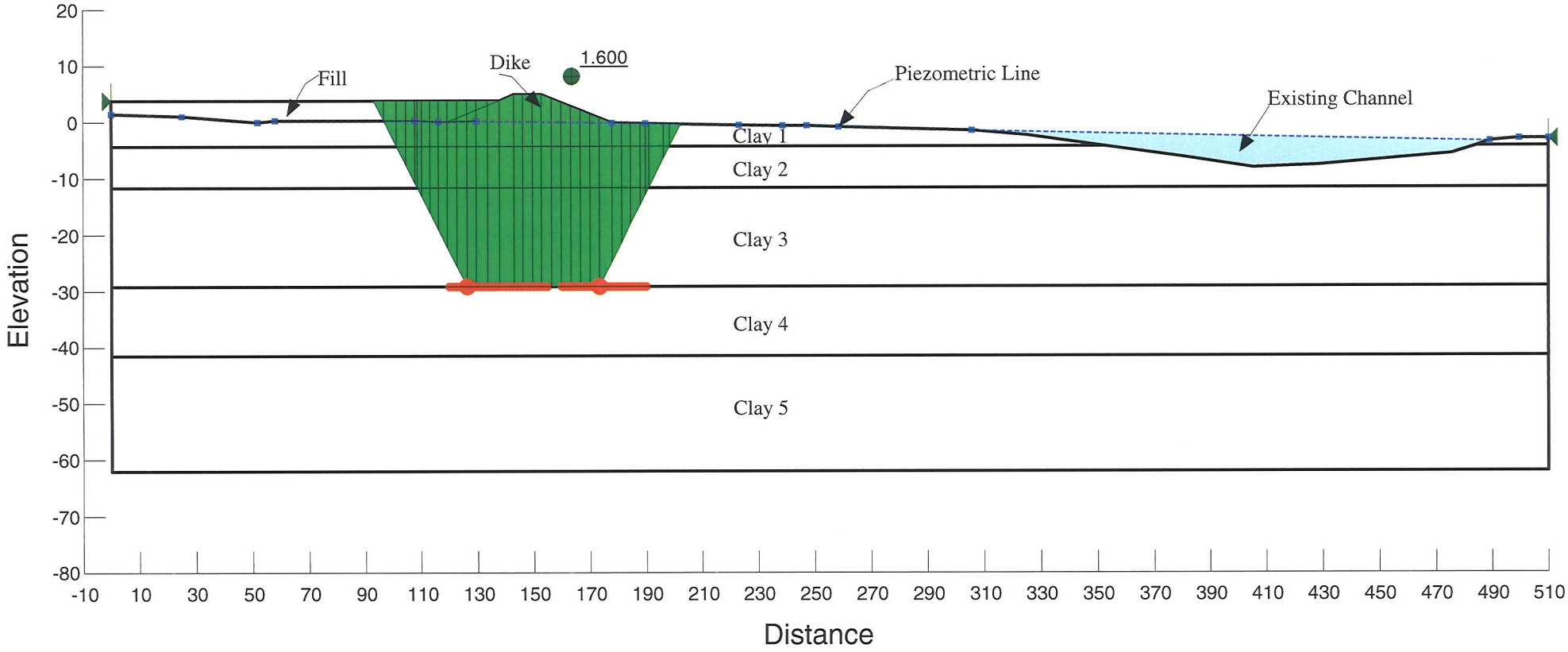


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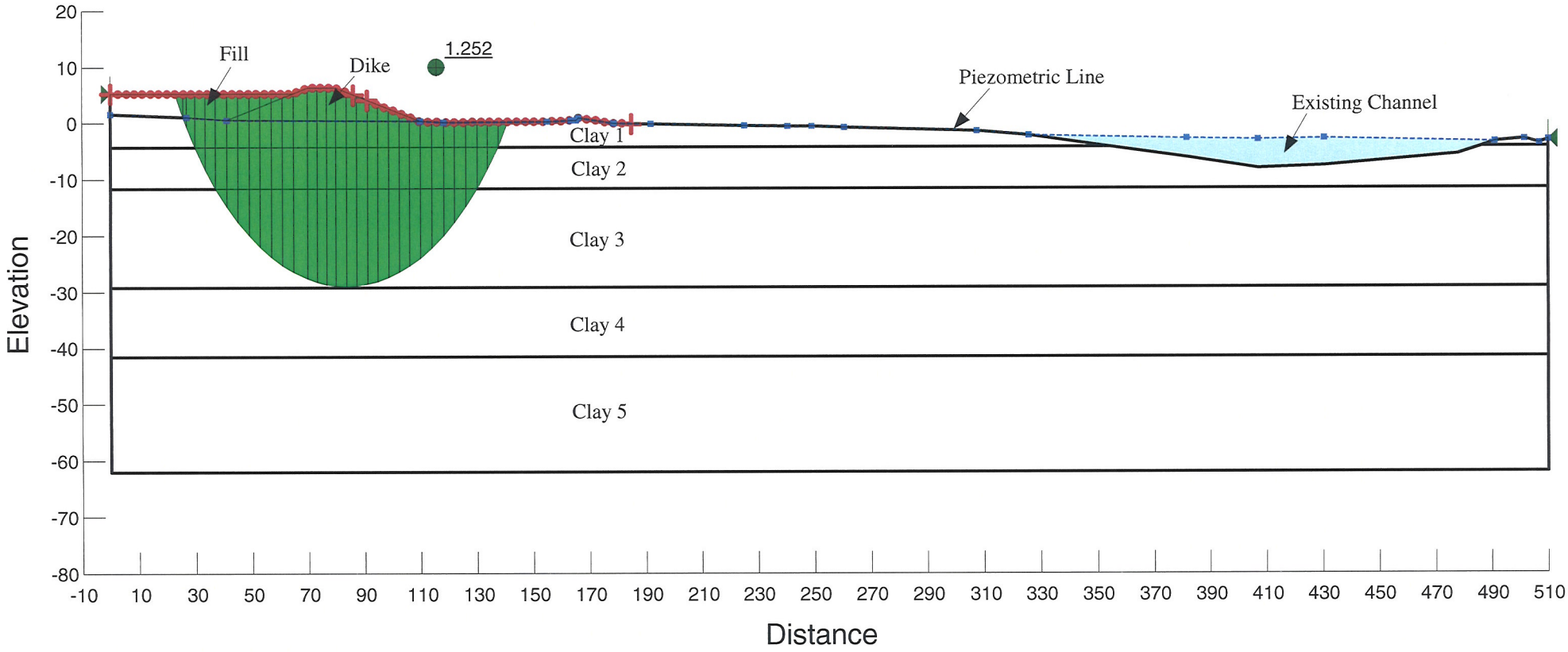
Figure 30

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: CIRCULAR
SLOPE: 5H TO 1V
DIKE Ht: 6.0'; FILL Ht: 5.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Fill	Unit Weight: 116 pcf	Cohesion: 0 psf	Phi: 30 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

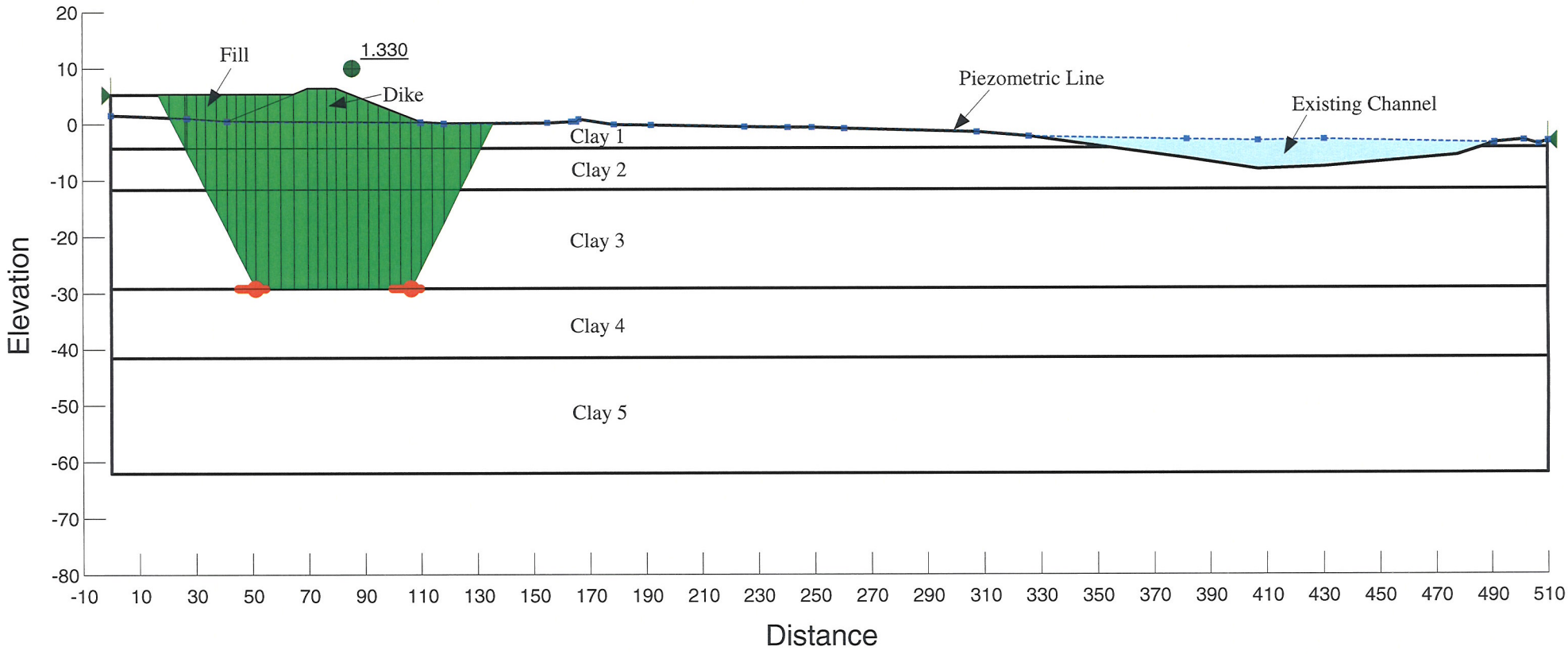


URS CORP.

Figure 31

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: WEDGE
SLOPE: 5H TO 1V
DIKE Ht: 6.0'; FILL Ht: 5.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Fill	Unit Weight: 116 pcf	Cohesion: 0 psf	Phi: 30 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

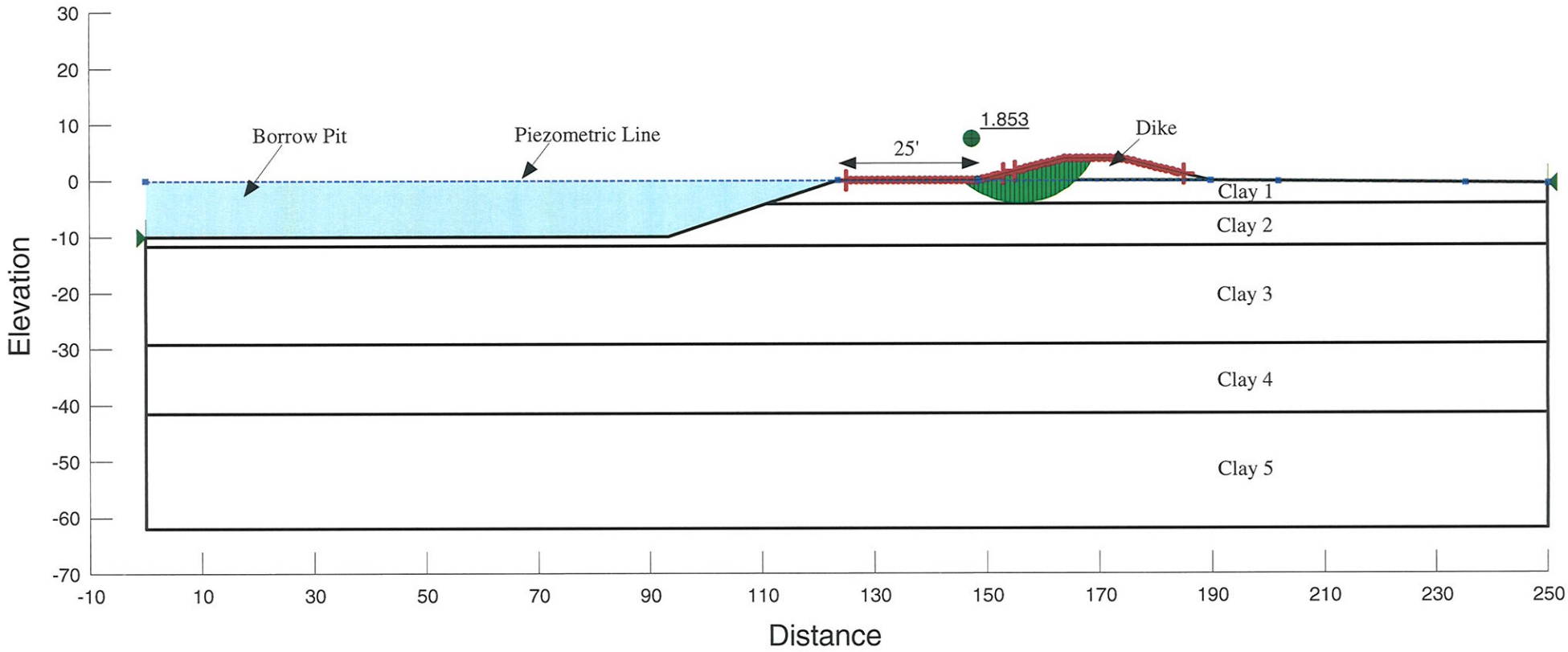


URS CORP.

Figure 32

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 4H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

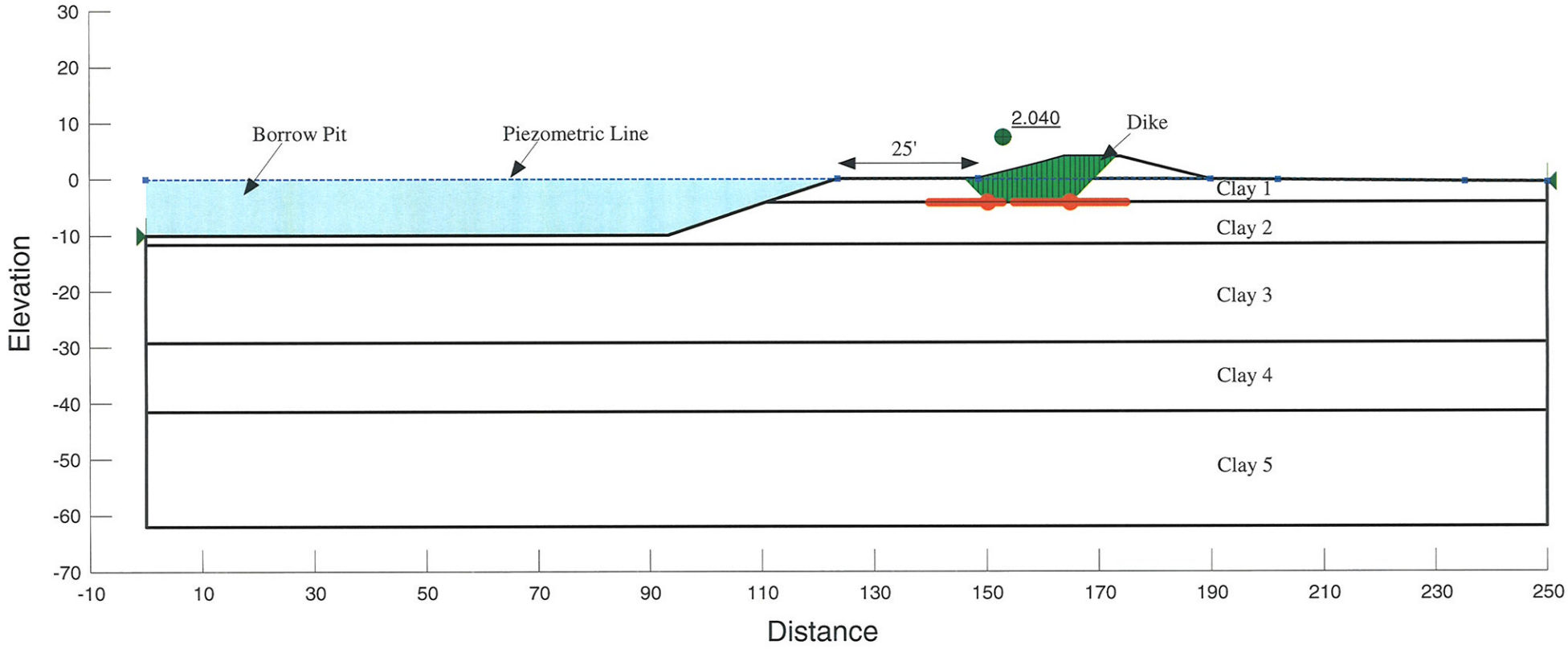


URS CORP.

Figure 33

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 4H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

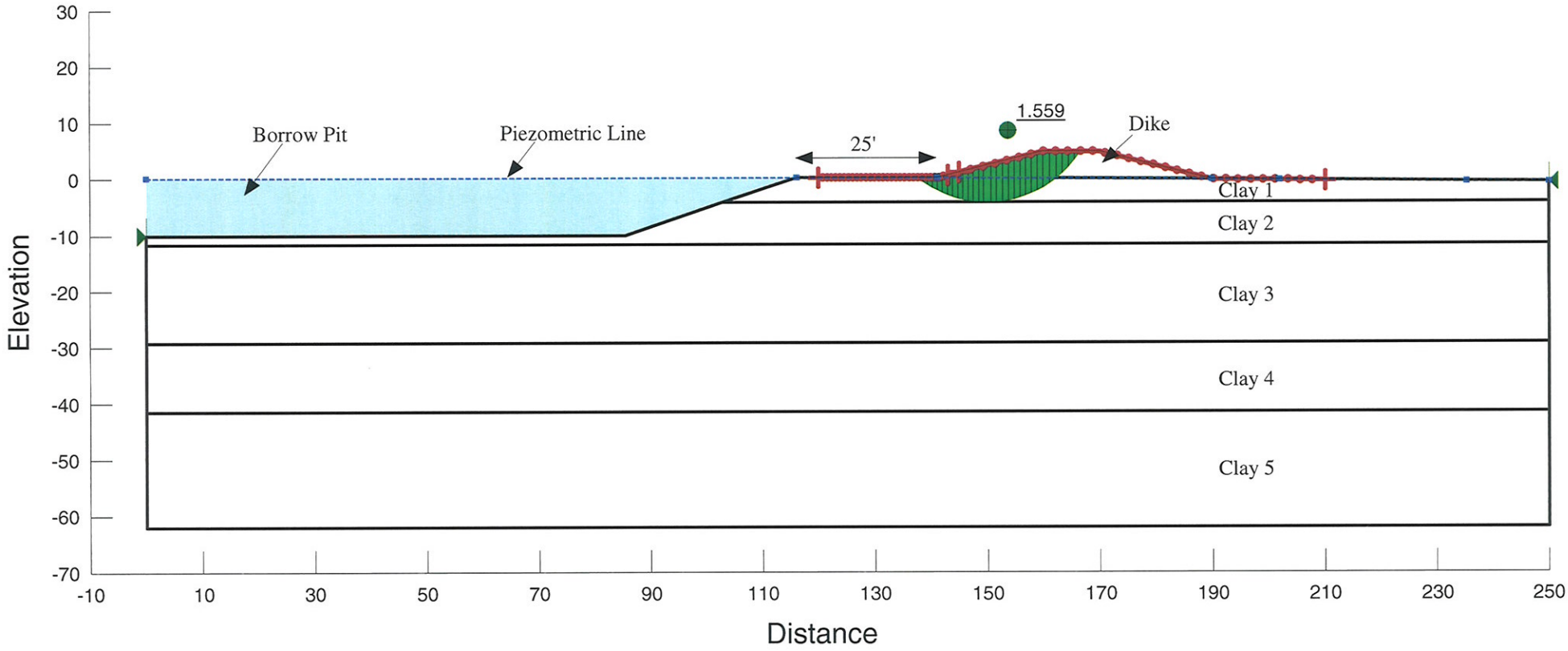


URS CORP.

Figure 34

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 4H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 5.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

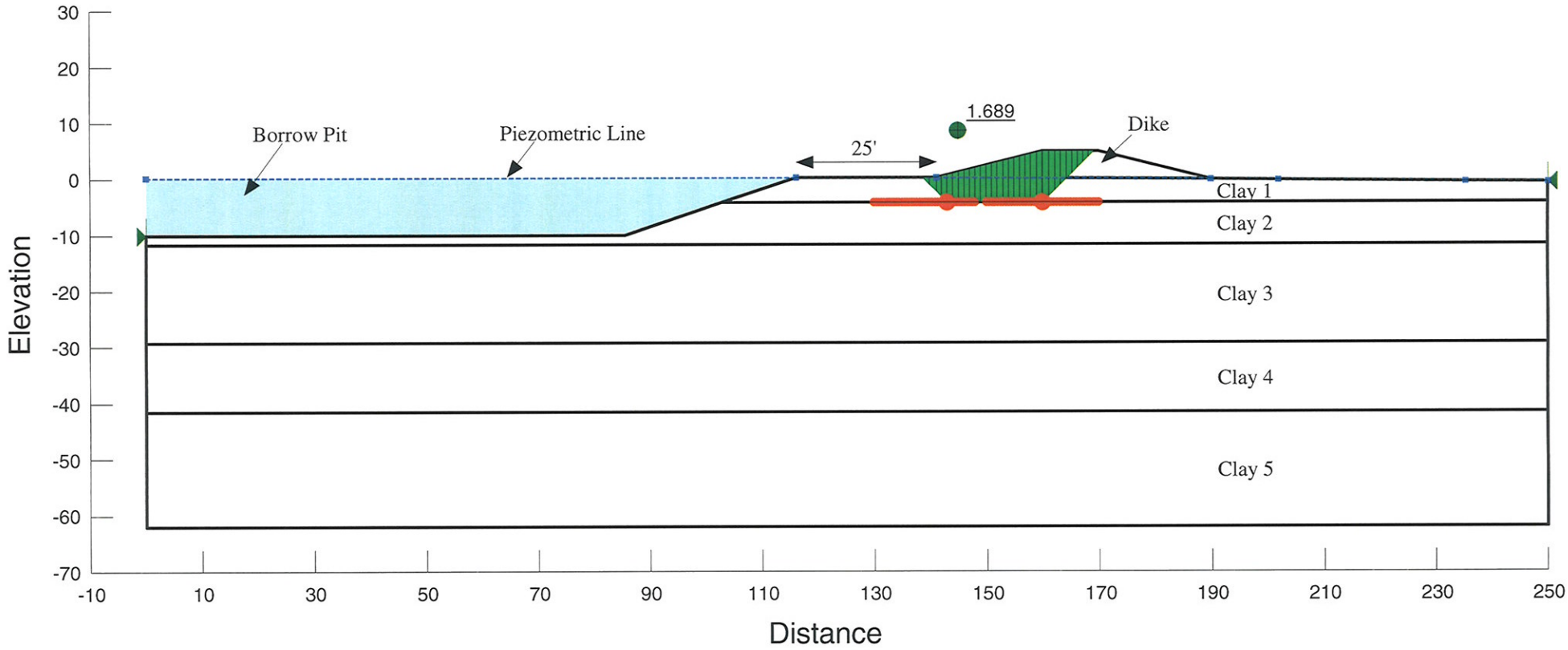


URS CORP.

Figure 35

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 4H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 5.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

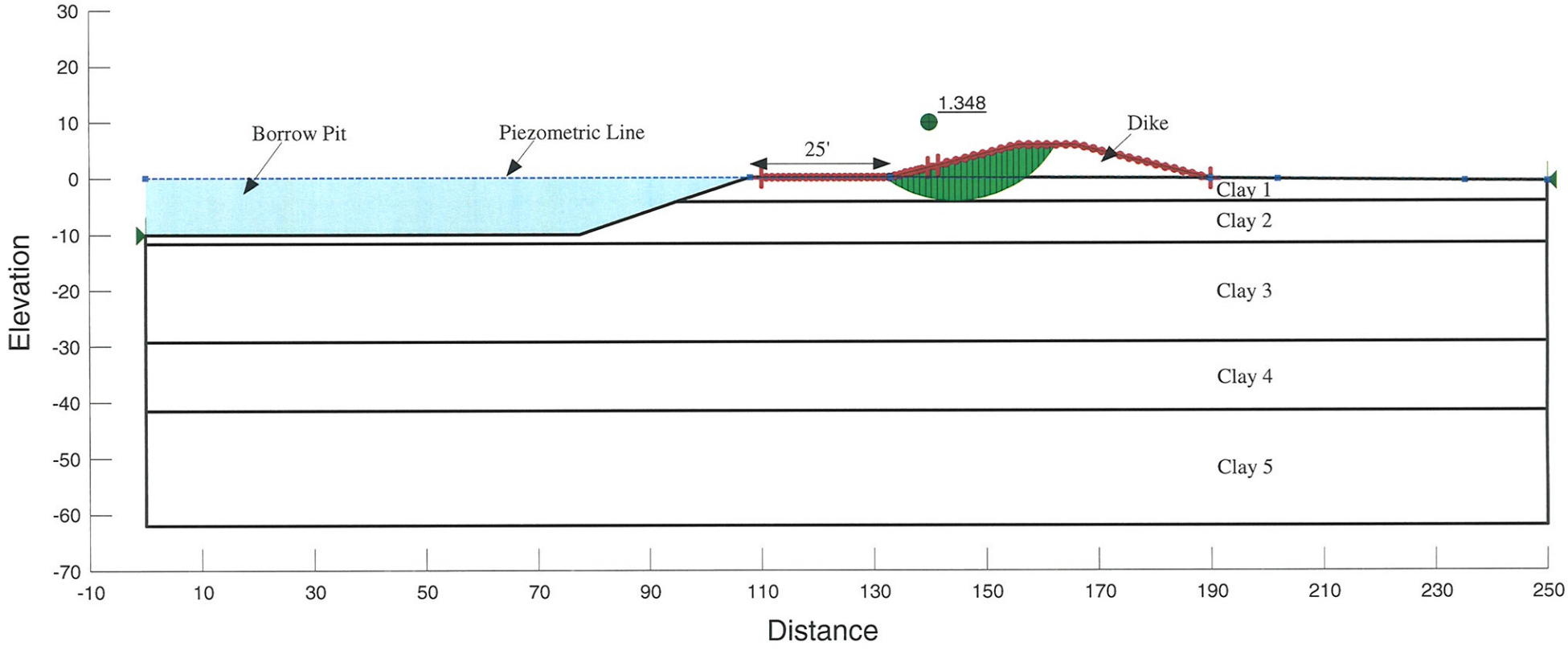


URS CORP.

Figure 36

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 4H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 6.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

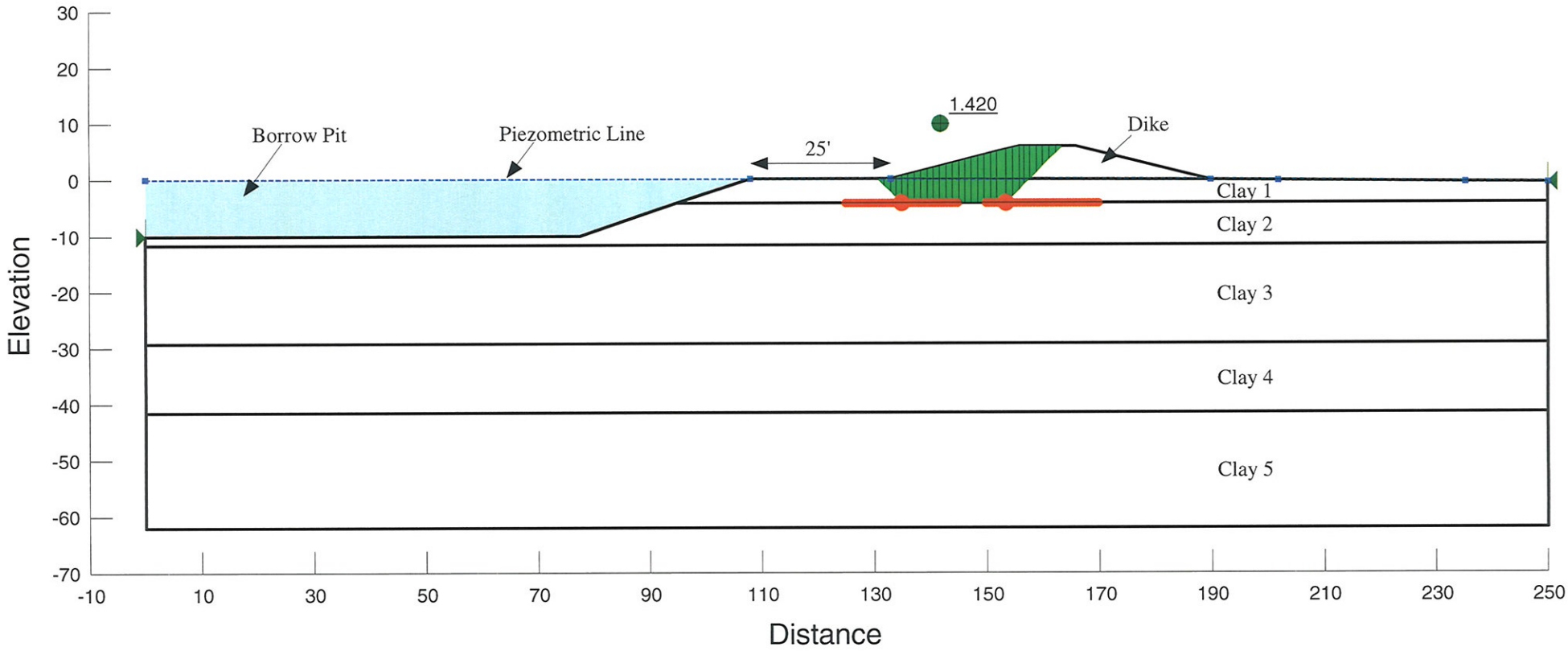


URS CORP.

Figure 37

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 4H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 6.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °



URS CORP.

Figure 38

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 5H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

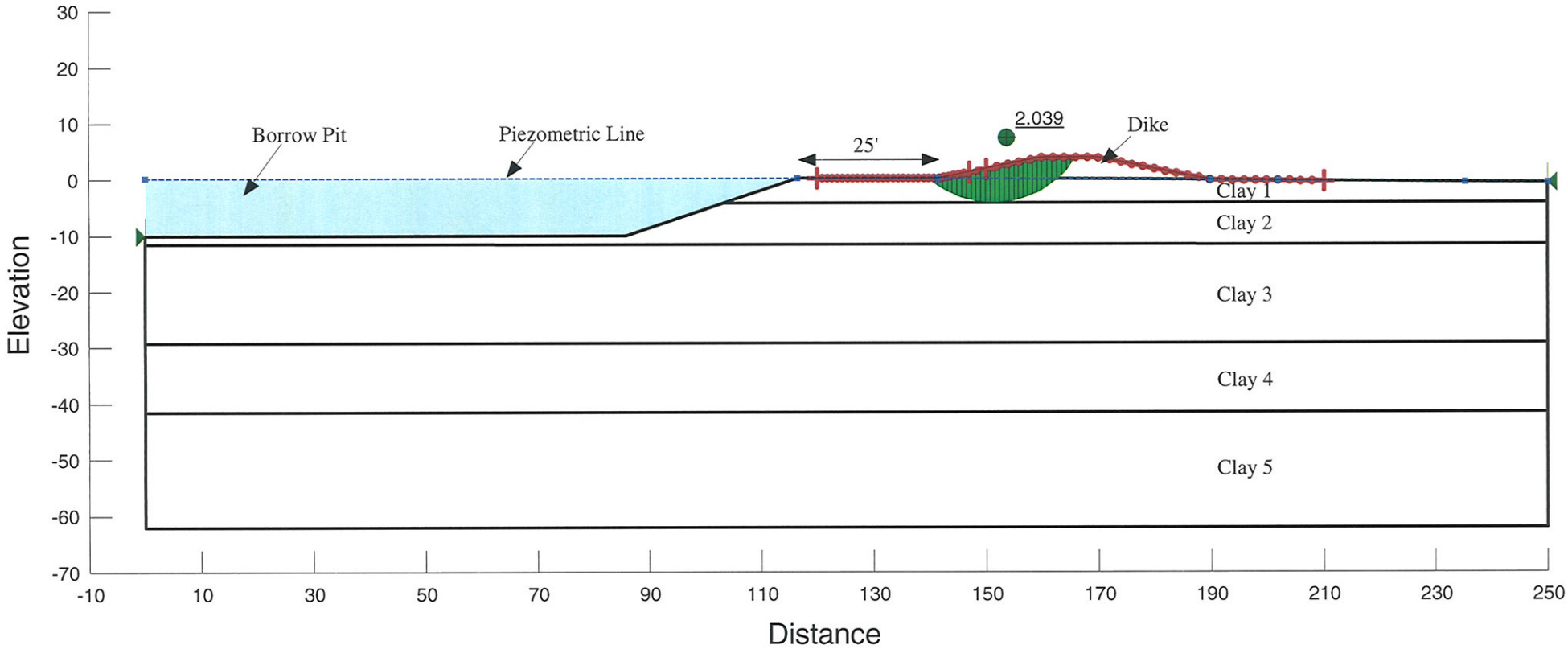


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Figure 39

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 5H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

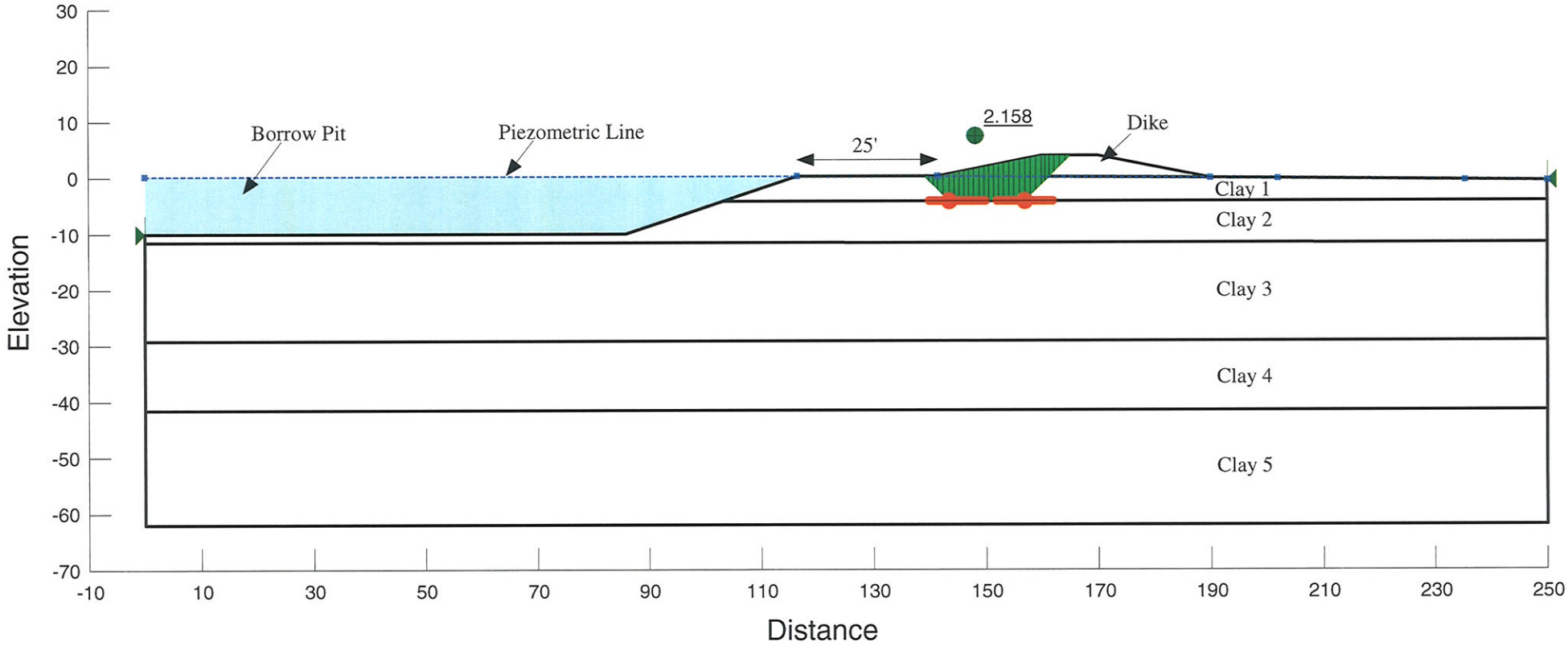

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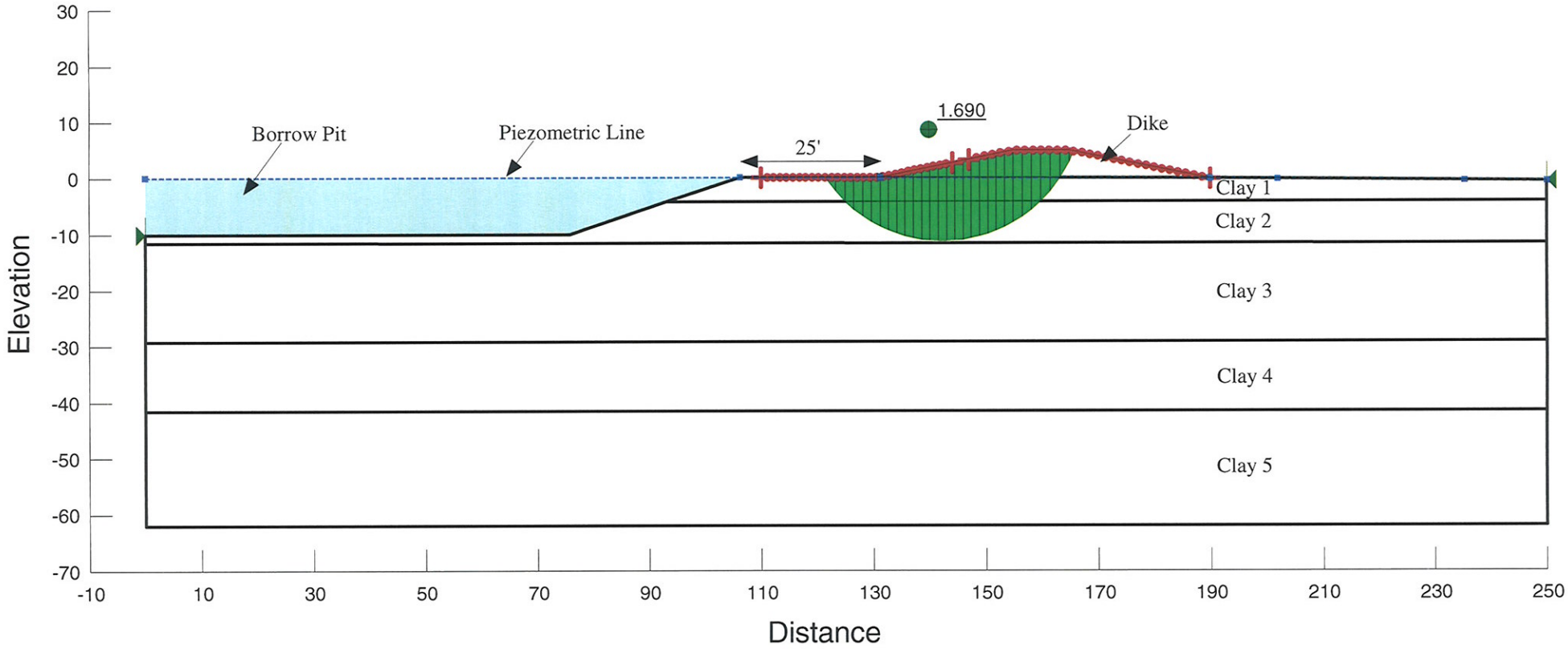
Figure 40

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 5H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 5.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

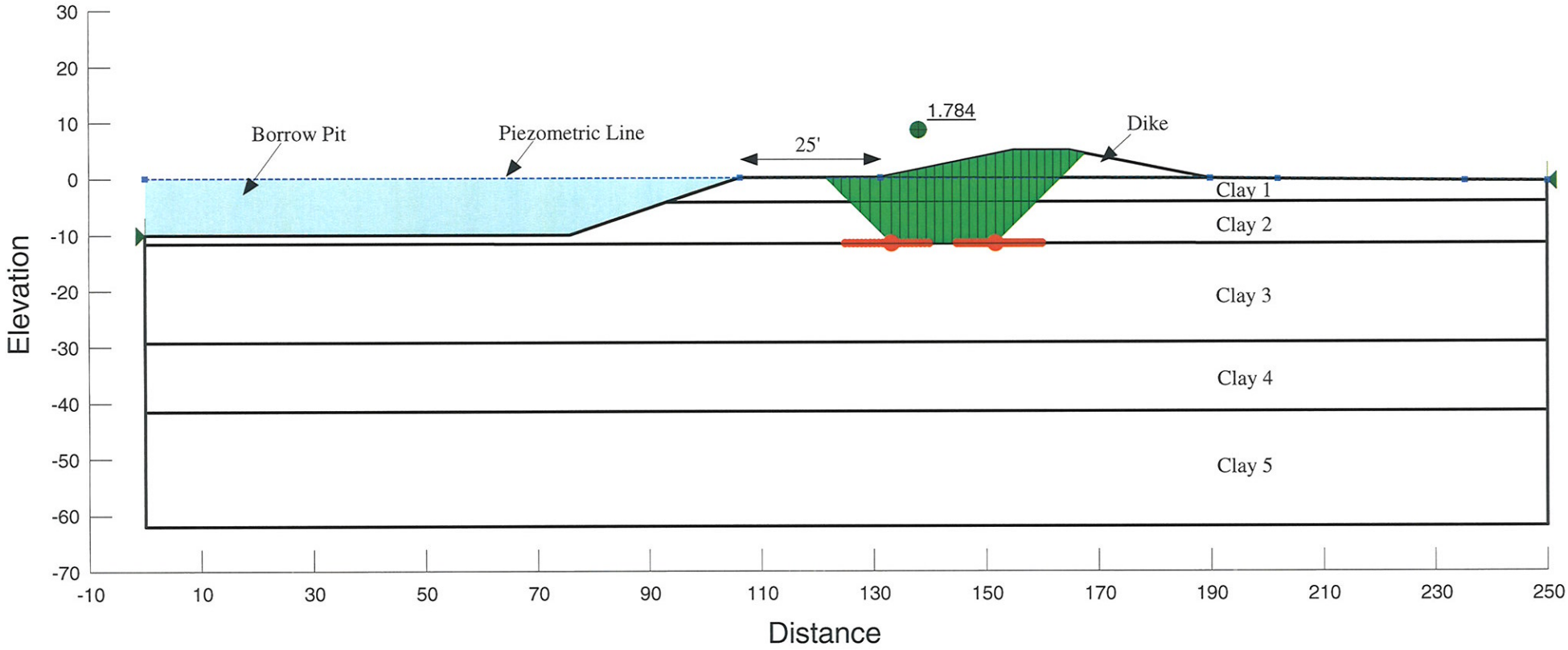


URS CORP.

Figure 41

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 5H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 5.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °

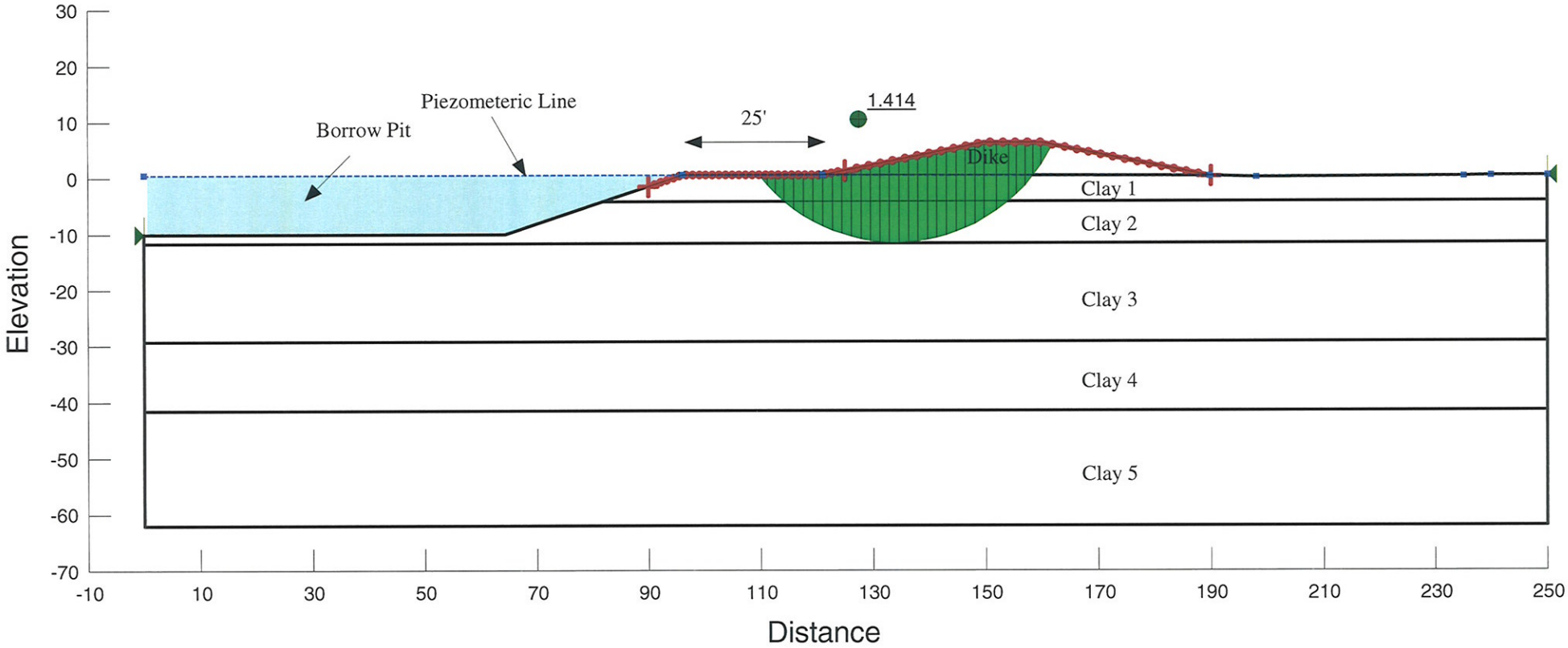


URS CORP.

Figure 42

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 5H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 6.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °



URS CORP.

Figure 43

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 5H TO 1V
BORROW PIT AT EL. -10'; DIKE Ht: 6.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

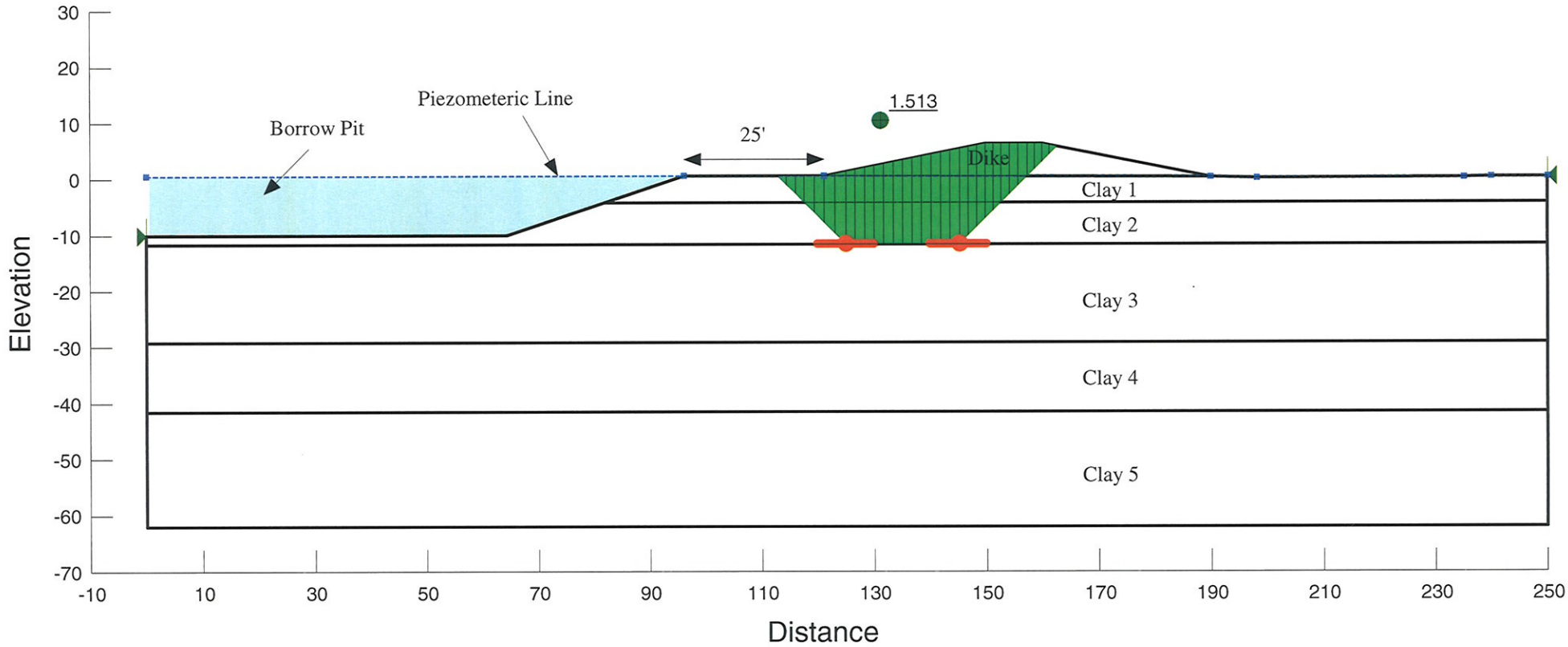


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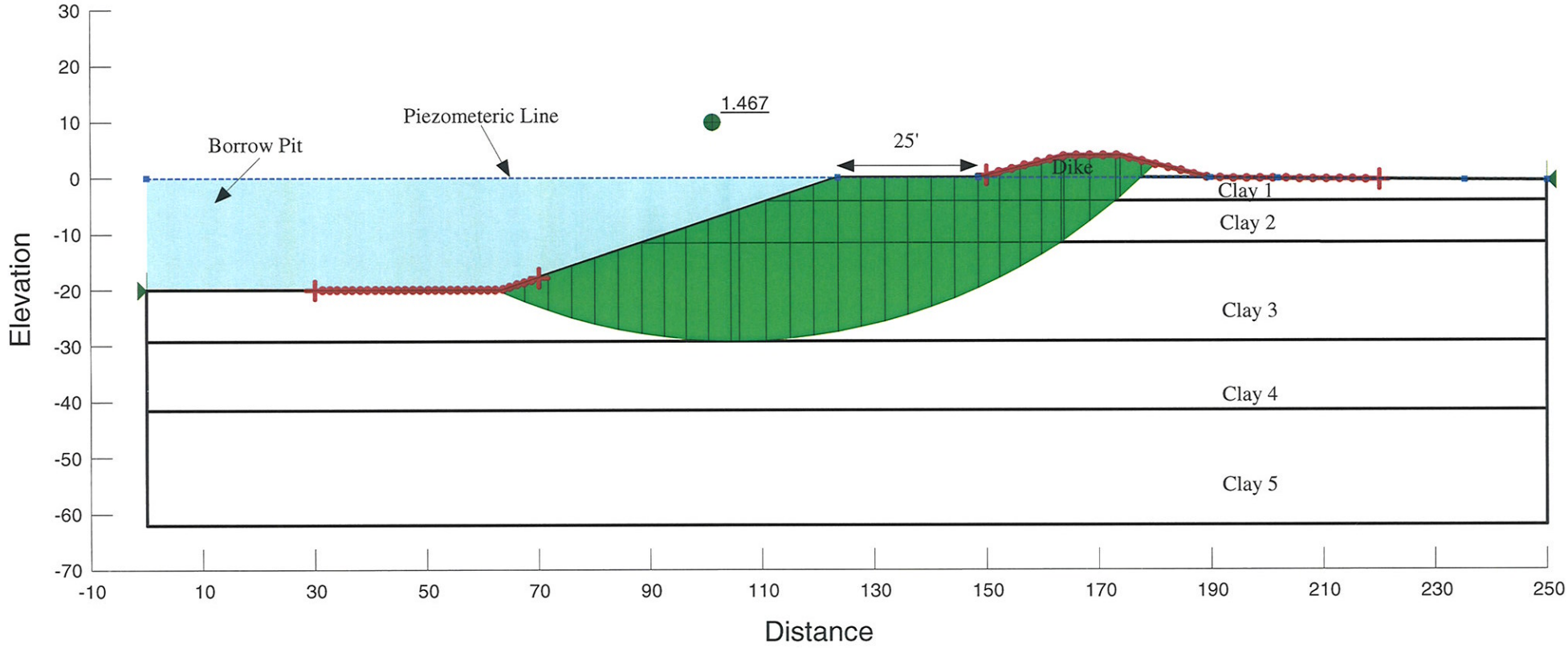
Figure 44

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 4H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 4.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °



URS CORP.

Figure 45

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 4H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 4.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

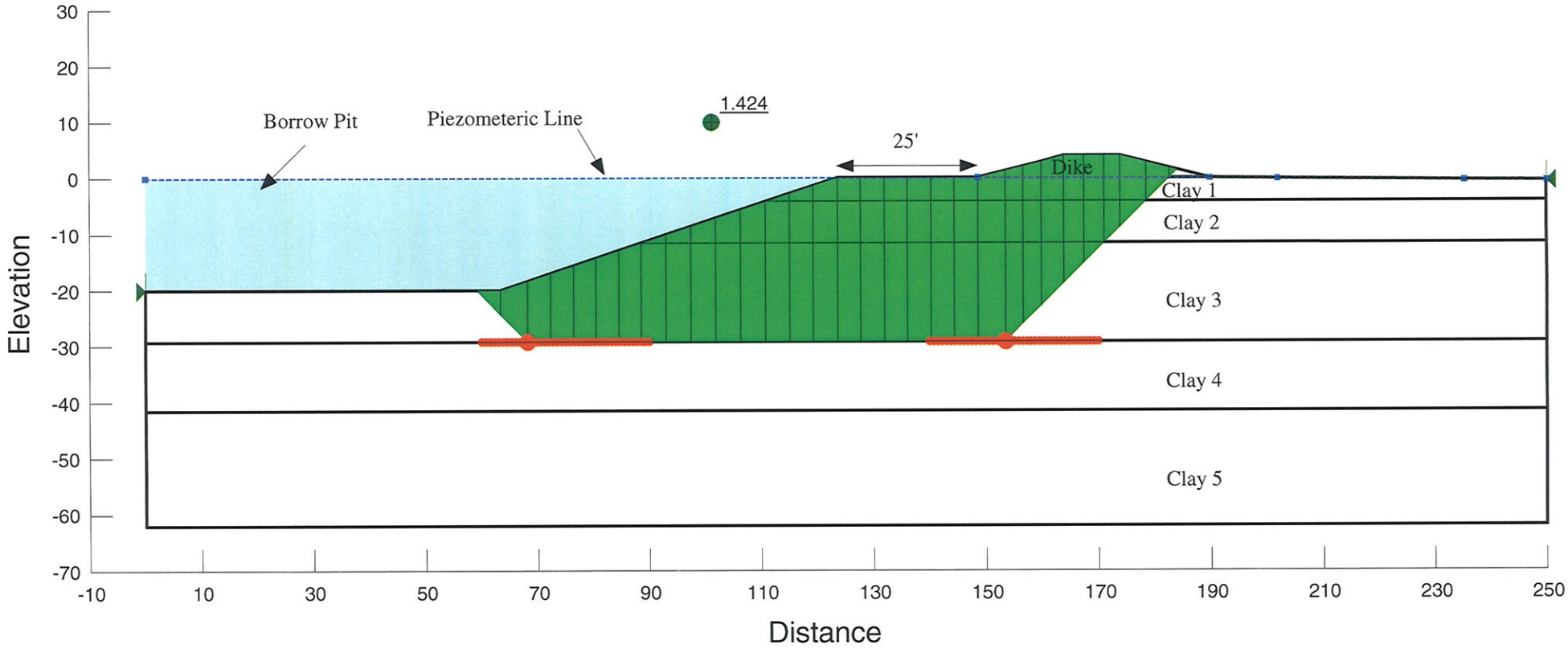


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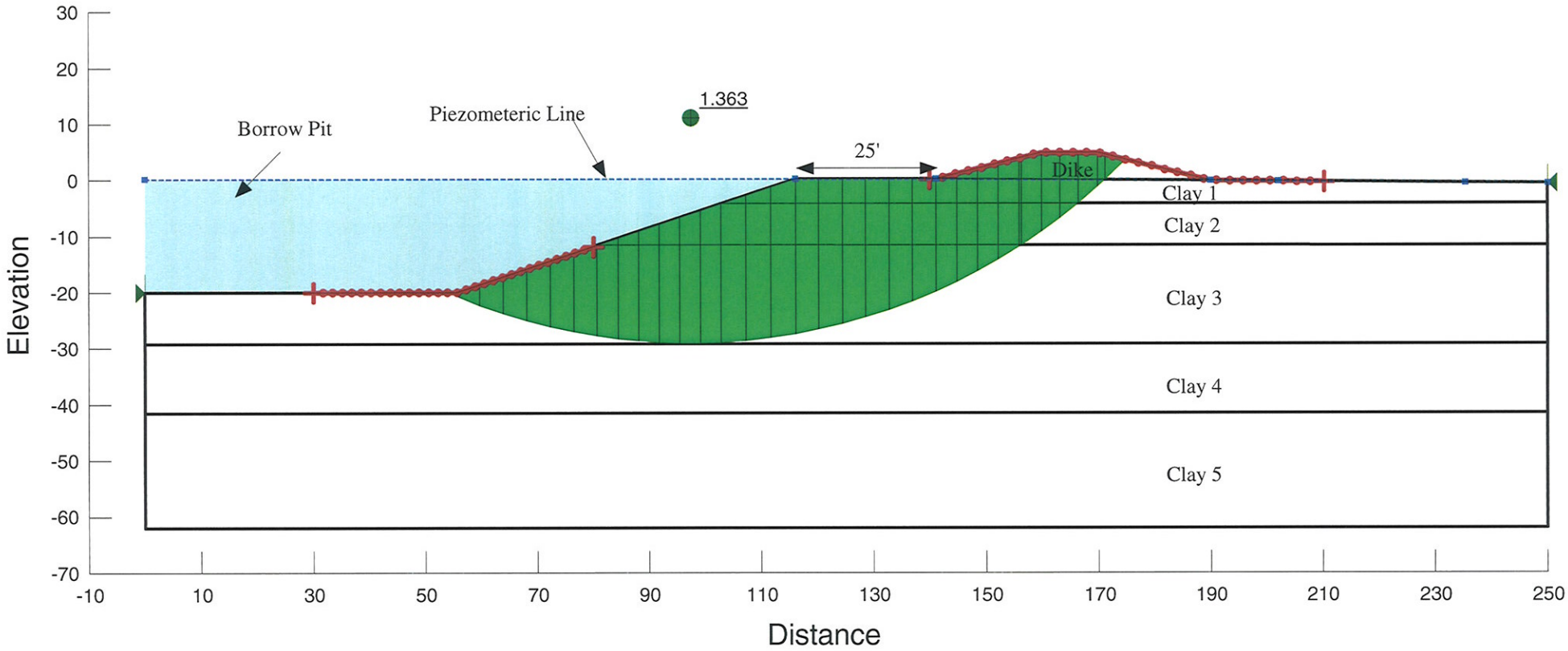
Figure 46

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 4H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 5.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

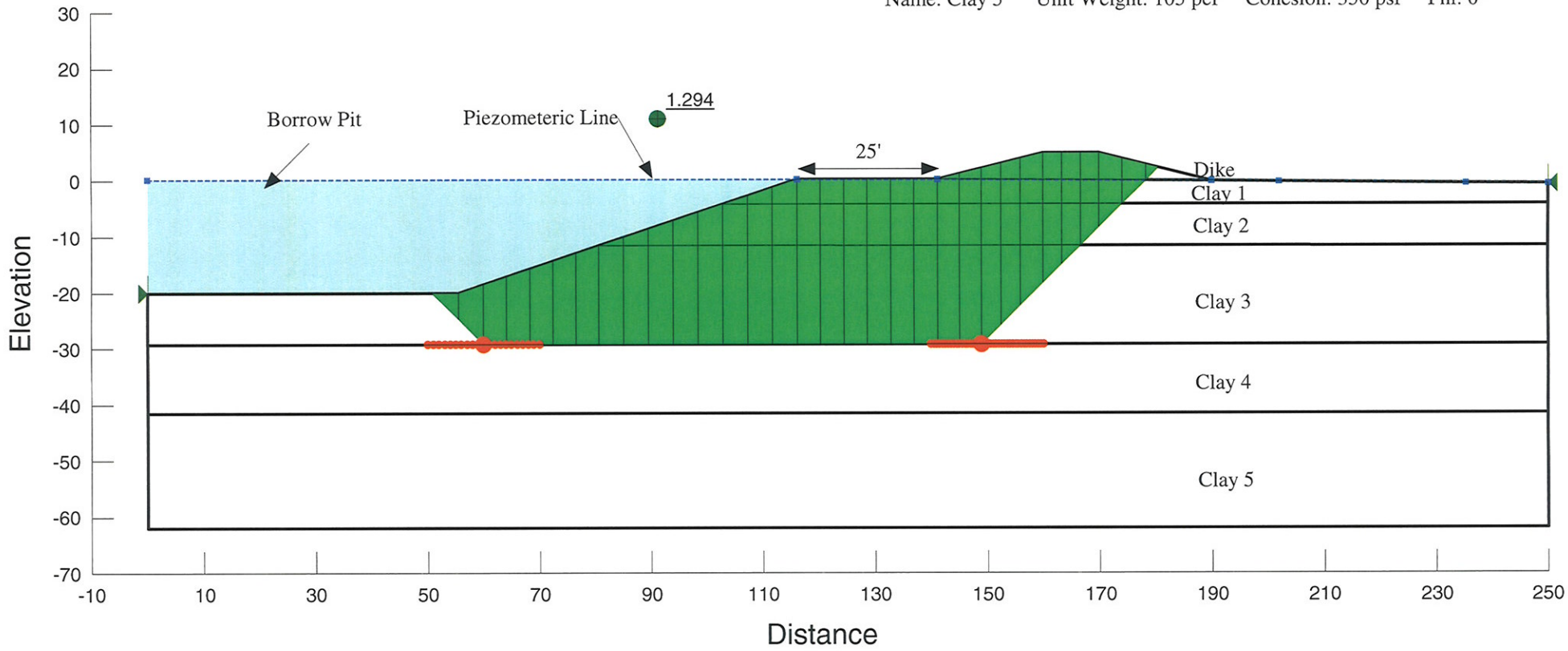


URS CORP.

Figure 47

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 4H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 5.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

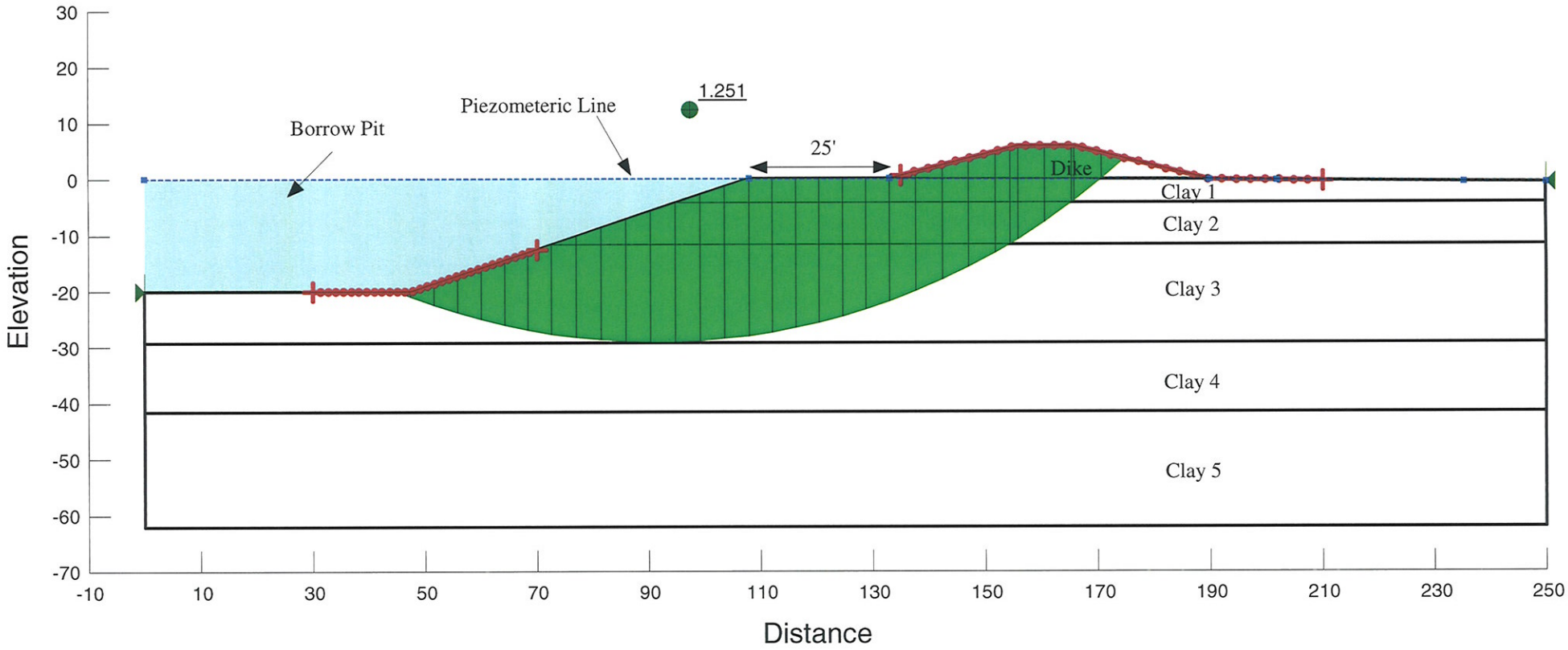


URS CORP.

Figure 48

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 4H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 6.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °



URS CORP.

Figure 49

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 4H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 6.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

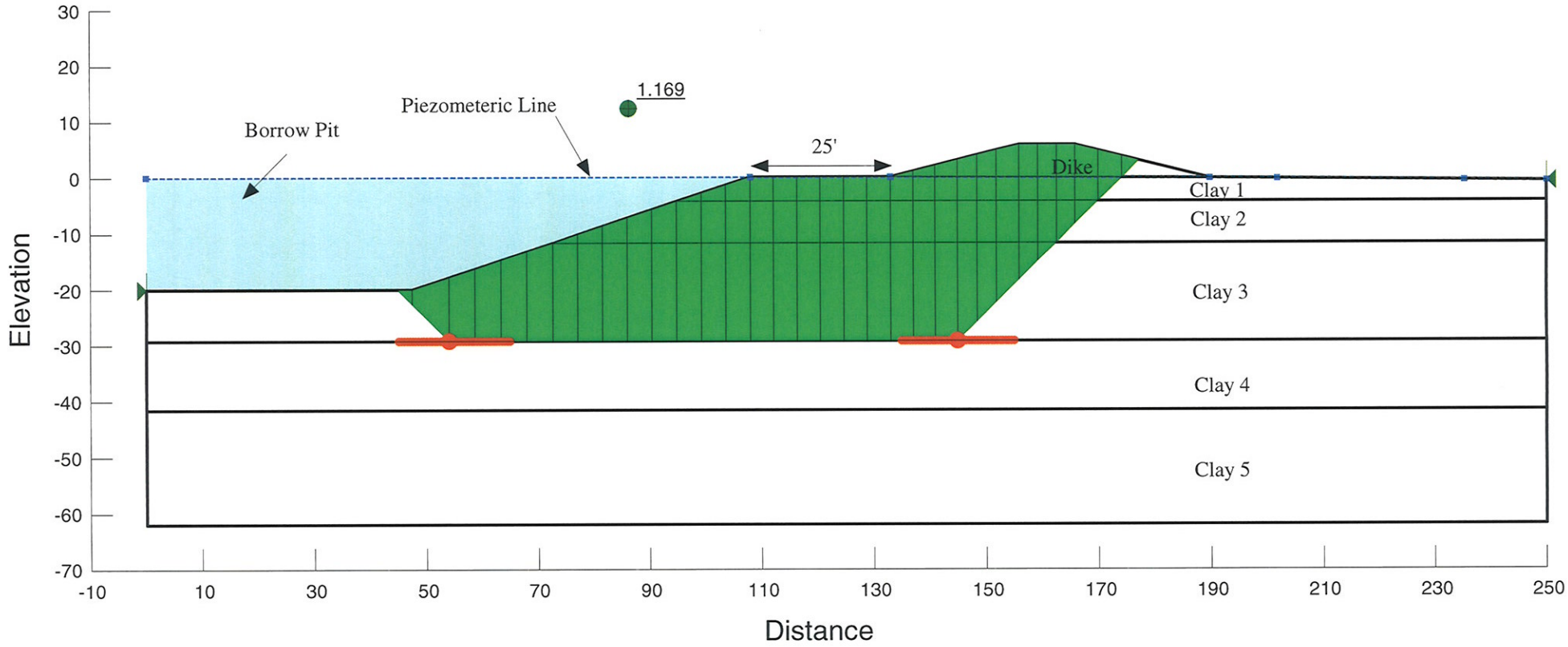


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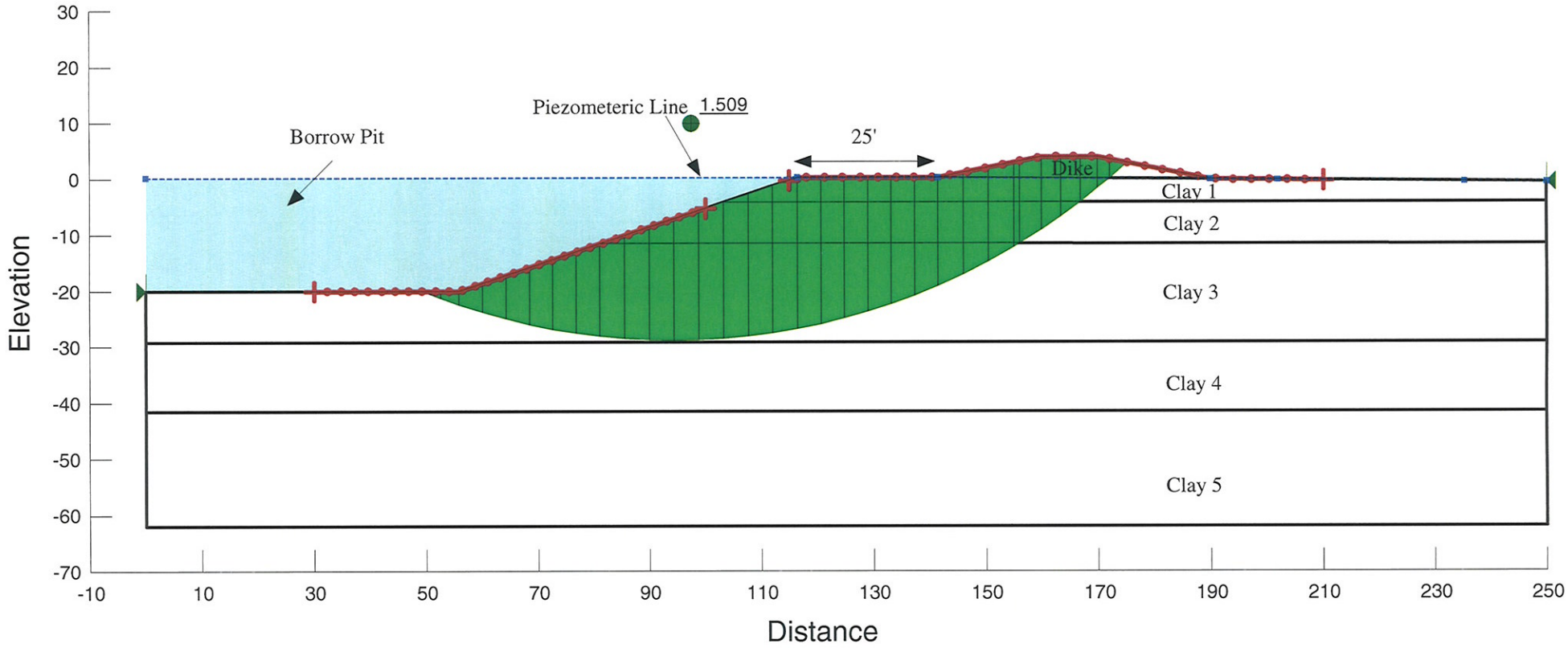
Figure 50

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 5H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 4.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

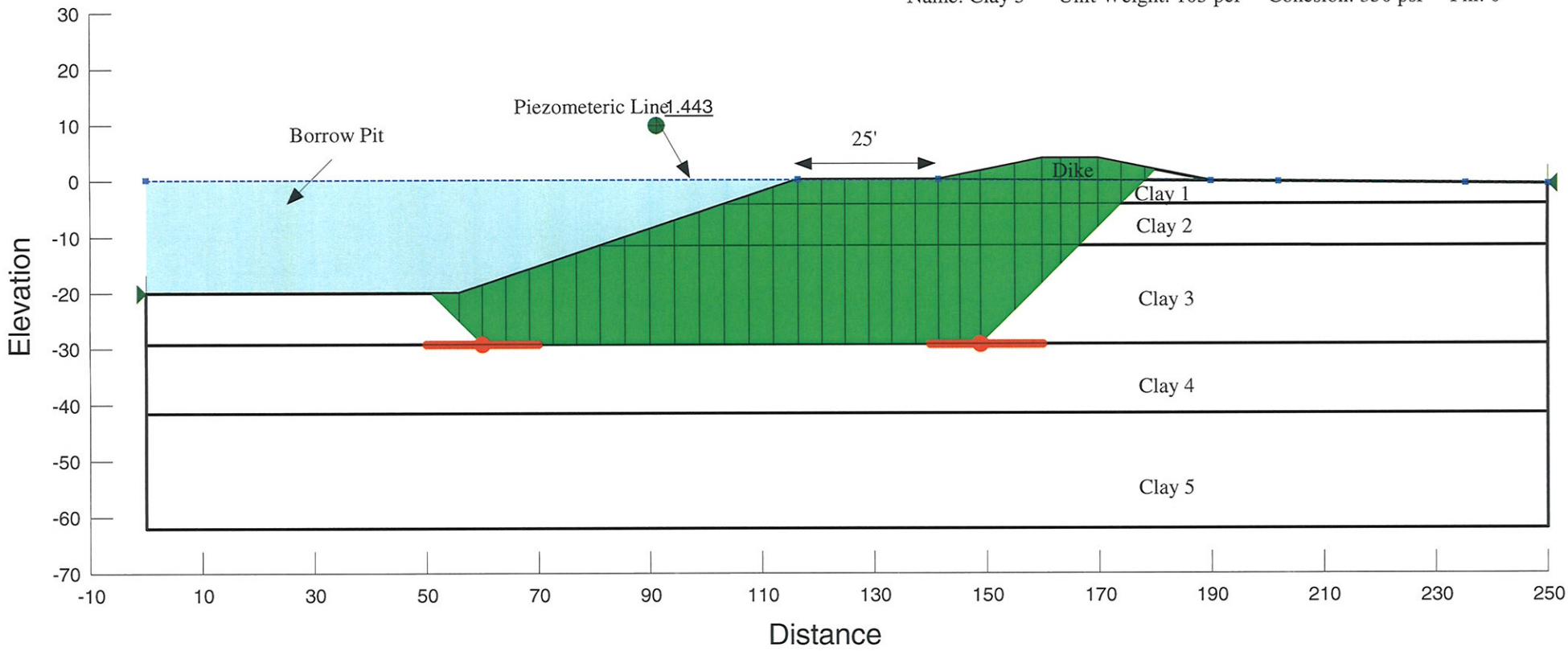


URS CORP.

Figure 51

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 5H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 4.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

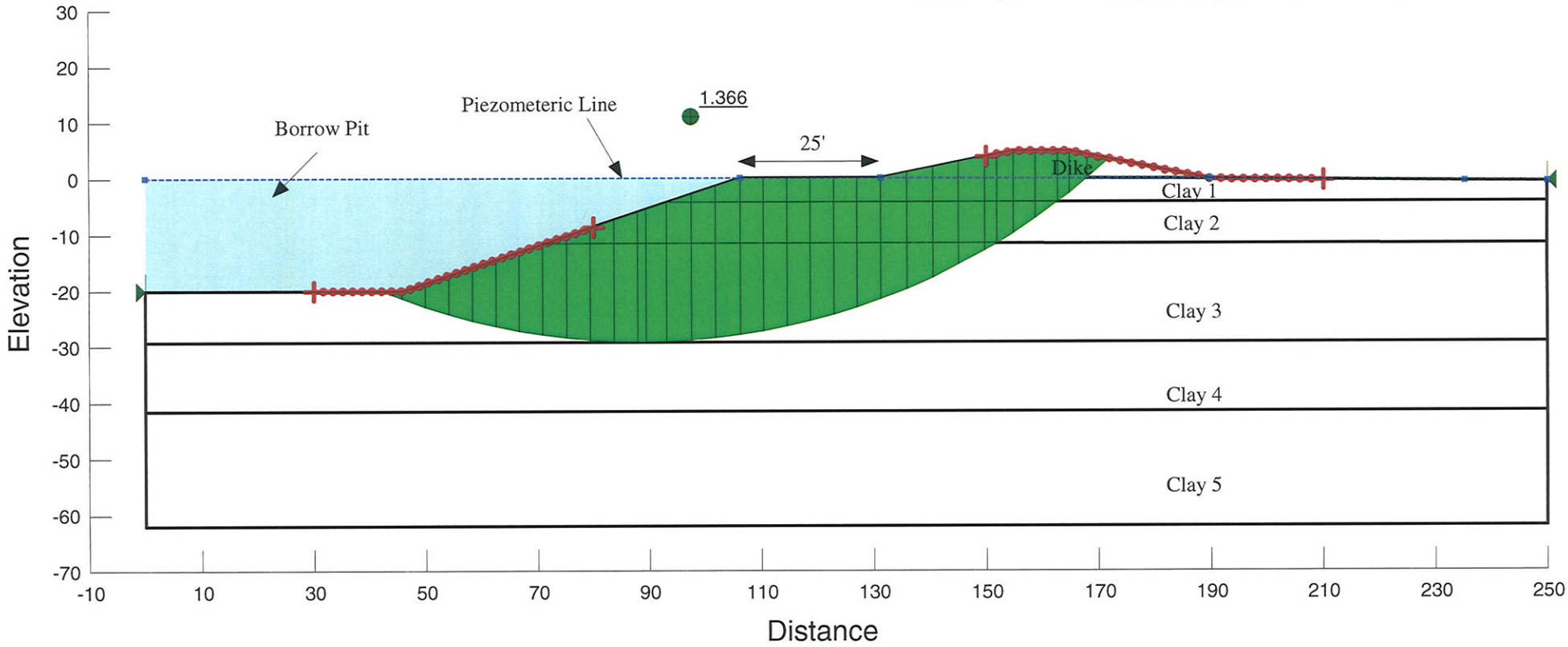


URS CORP.

Figure 52

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 5H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 5.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

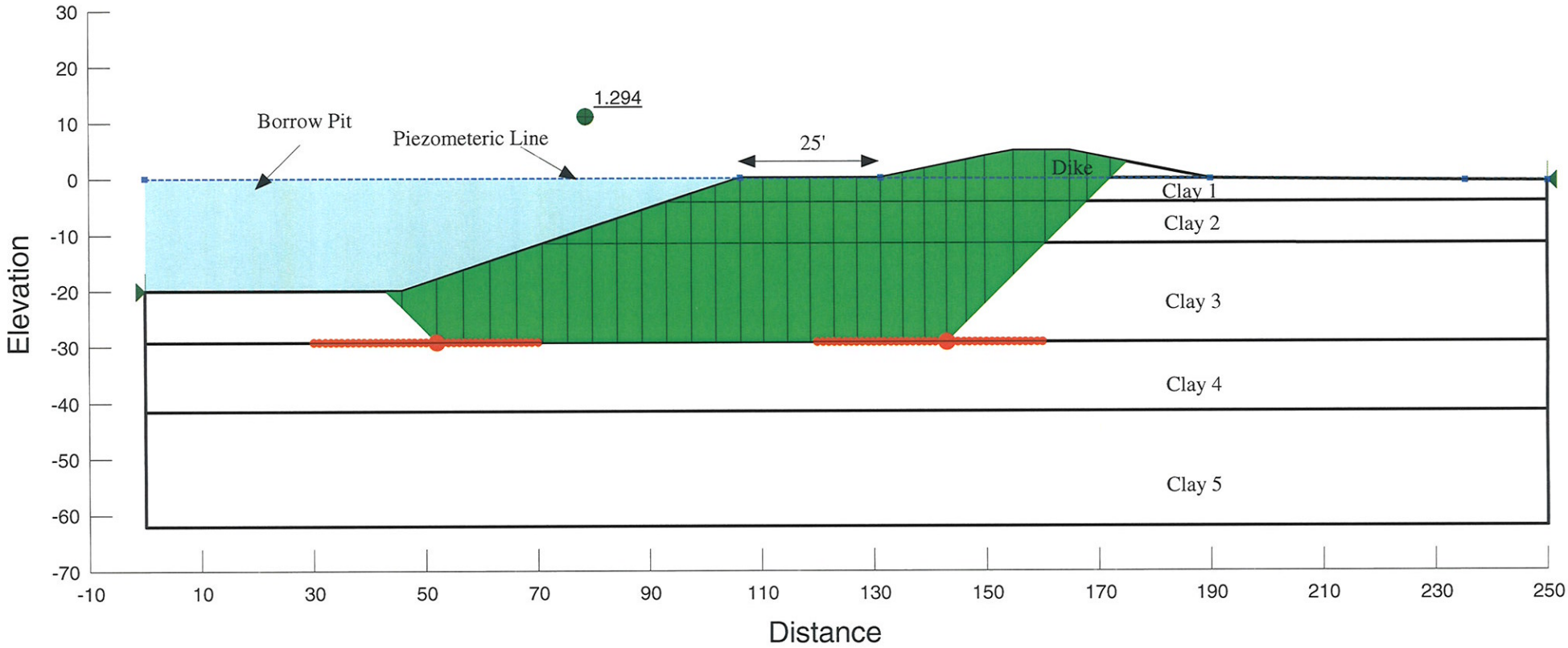


URS CORP.

Figure 53

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 5H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 5.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

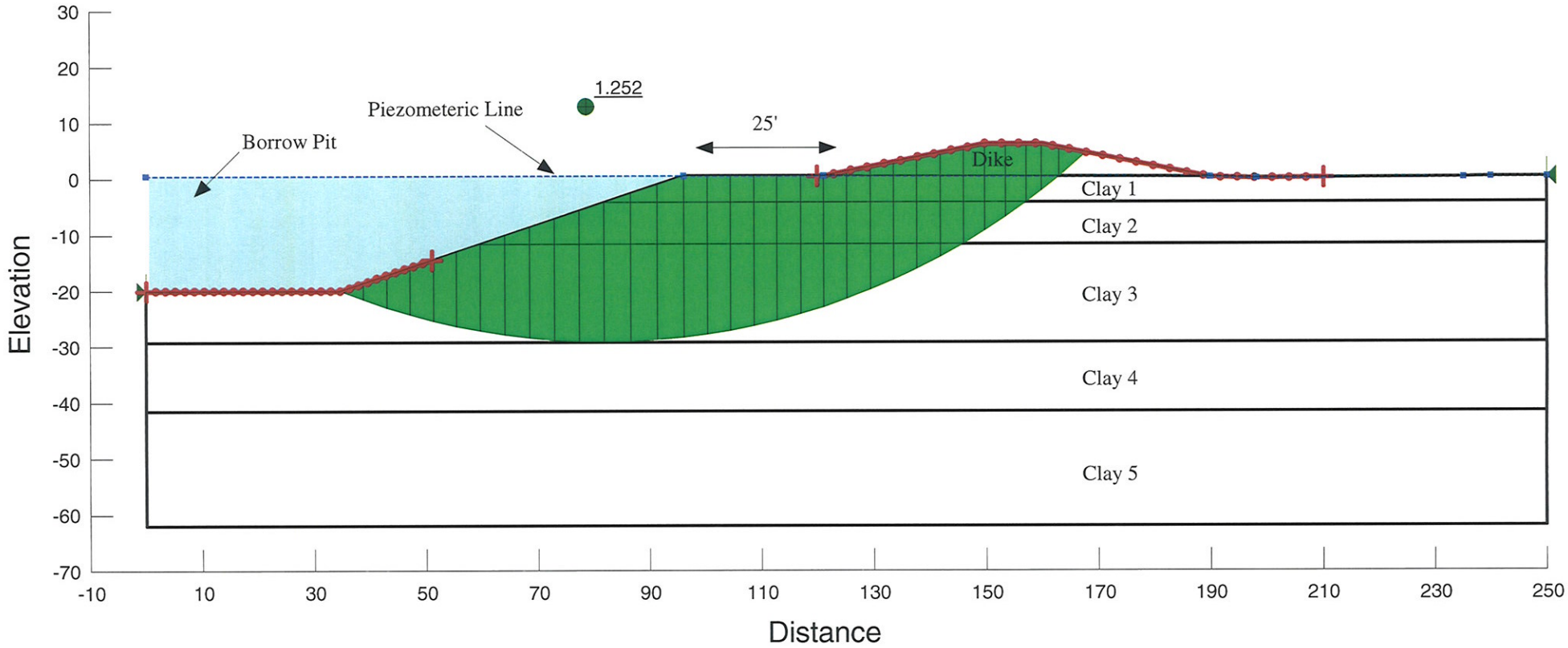


URS CORP.

Figure 54

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
SLOPE: 5H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 6.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °



URS CORP.

Figure 55

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
SLOPE: 5H TO 1V
BORROW PIT AT EL. -20'; DIKE Ht: 6.0'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

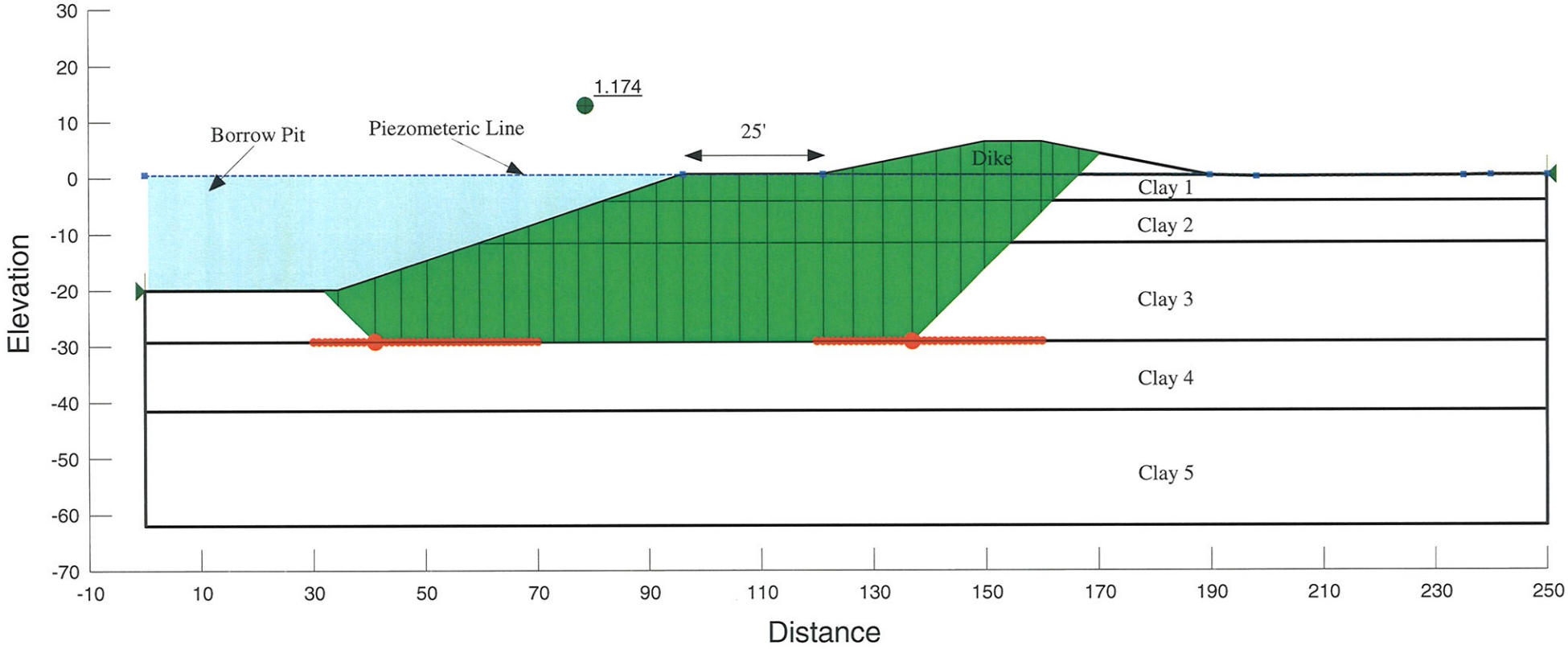


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Figure 56

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: CIRCULAR
DIKE Ht: 4.0'; FILL Ht: 3.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °

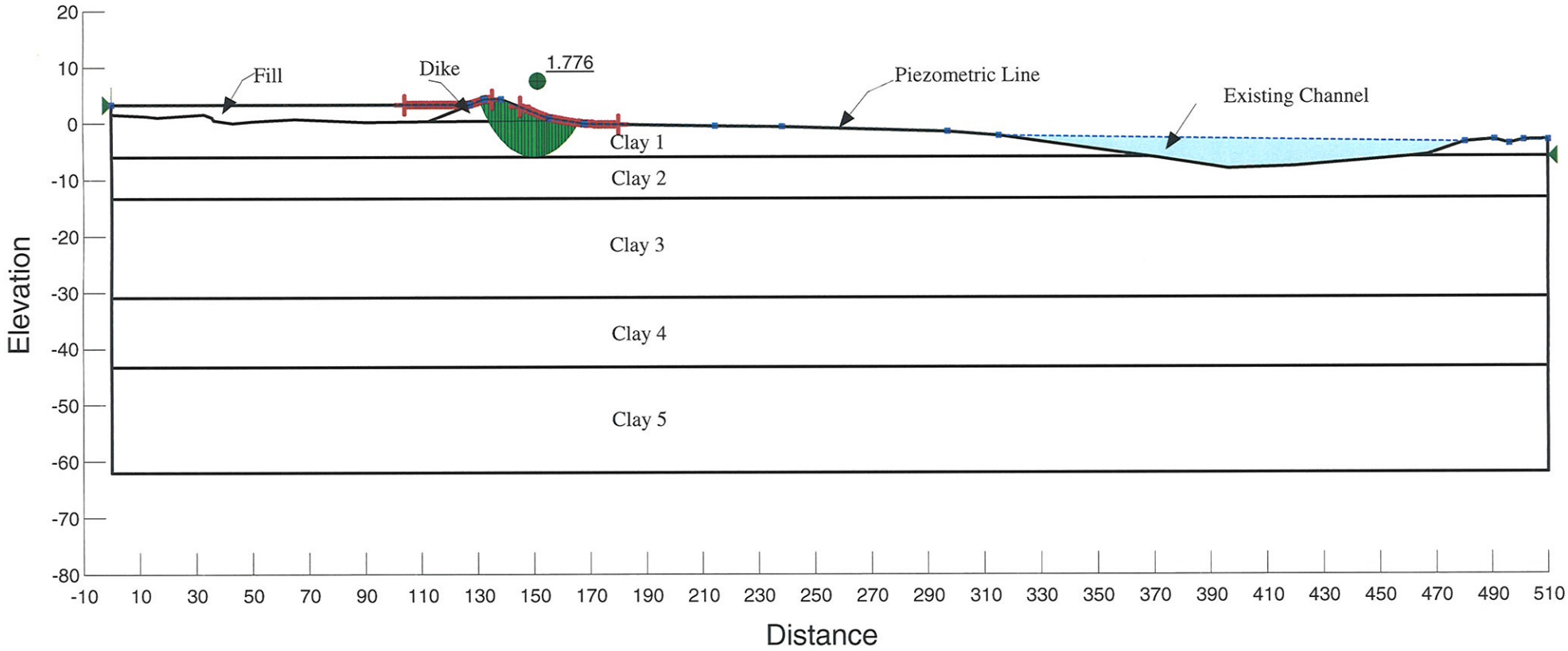

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Figure 57

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: WEDGE
DIKE Ht: 4.0'; FILL Ht: 3.0'

Name: Dike Unit Weight: 70.55 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay Material 2 Unit Weight: 82.24 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay Material 3 Unit Weight: 99.92 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay Material 4 Unit Weight: 104.32 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay Material 5 Unit Weight: 104.17 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay Material 1 Unit Weight: 70.55 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °

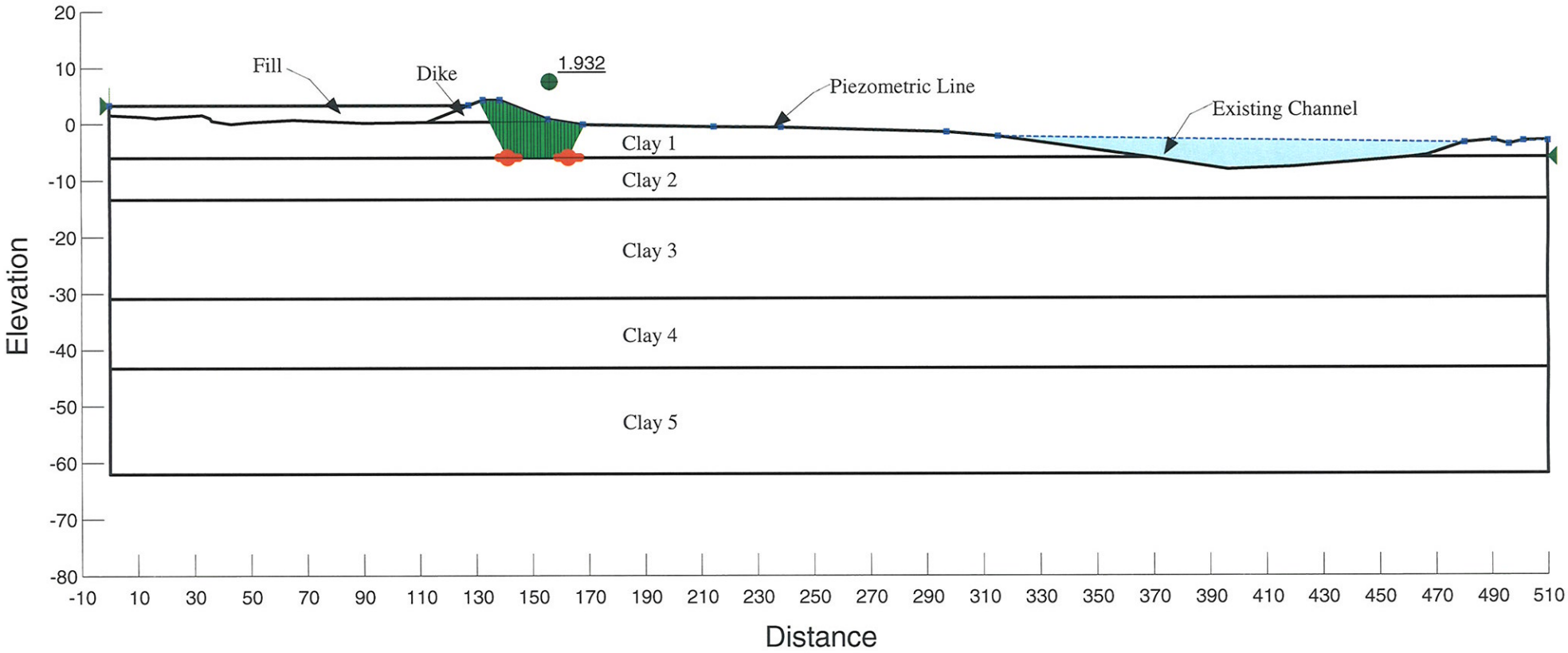

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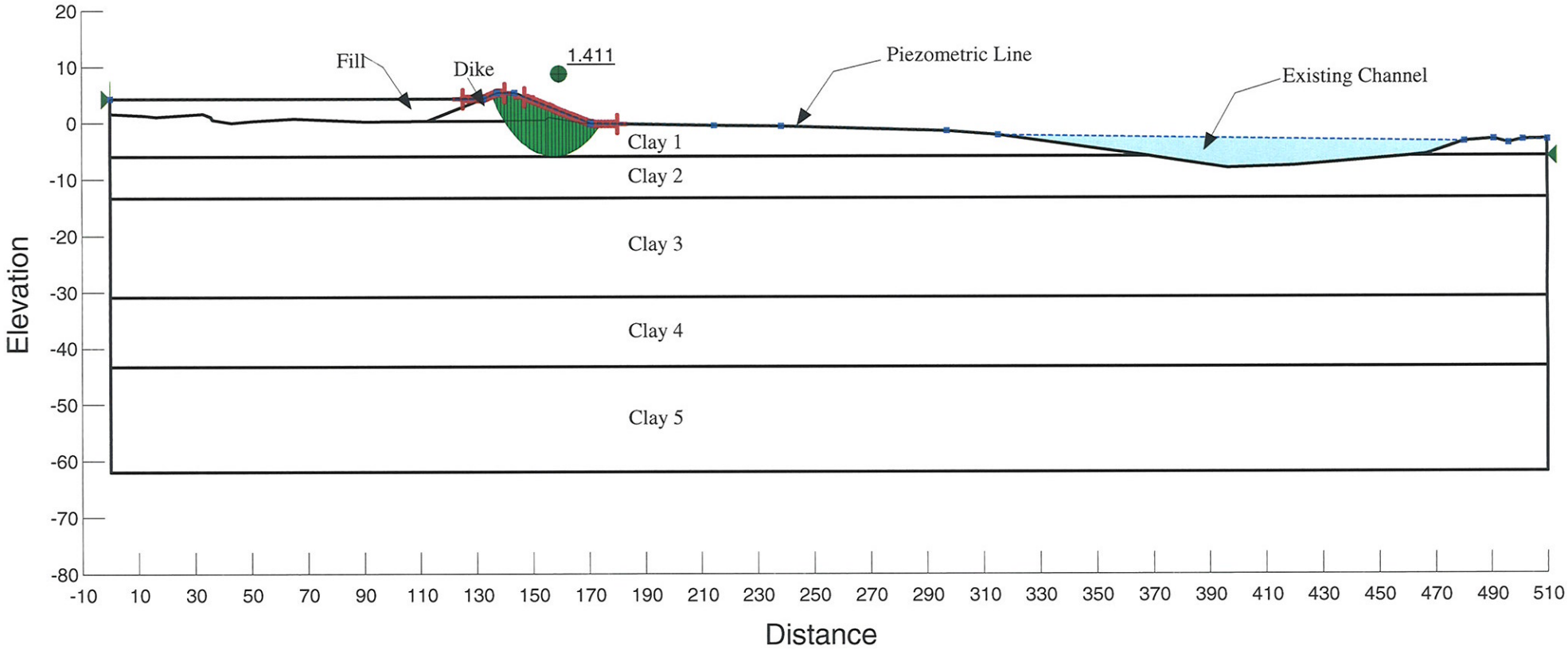
Figure 58

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: CIRCULAR
DIKE Ht: 5.0'; FILL Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °



URS CORP.

Figure 59

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: WEDGE
DIKE Ht: 5.0'; FILL Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °

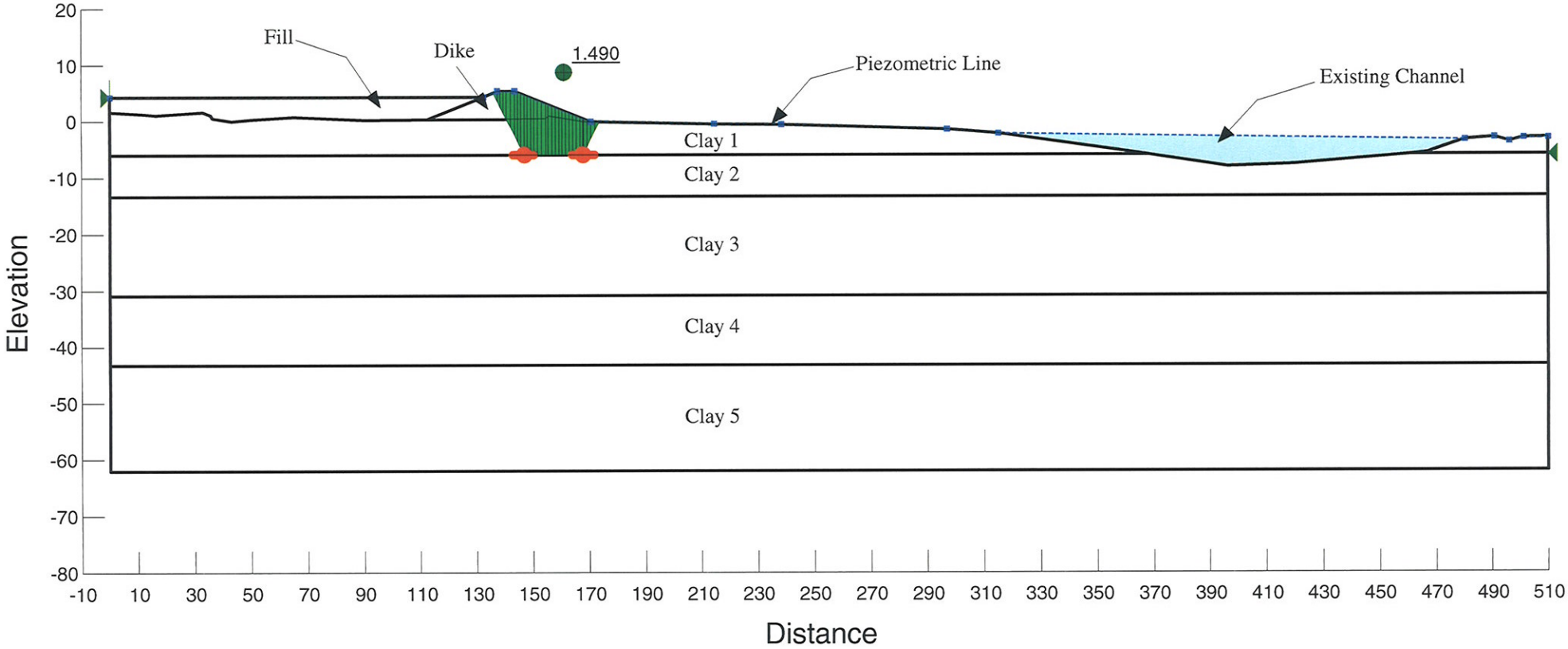


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Figure 60

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: CIRCULAR
DIKE Ht: 6.0'; FILL Ht: 5.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °

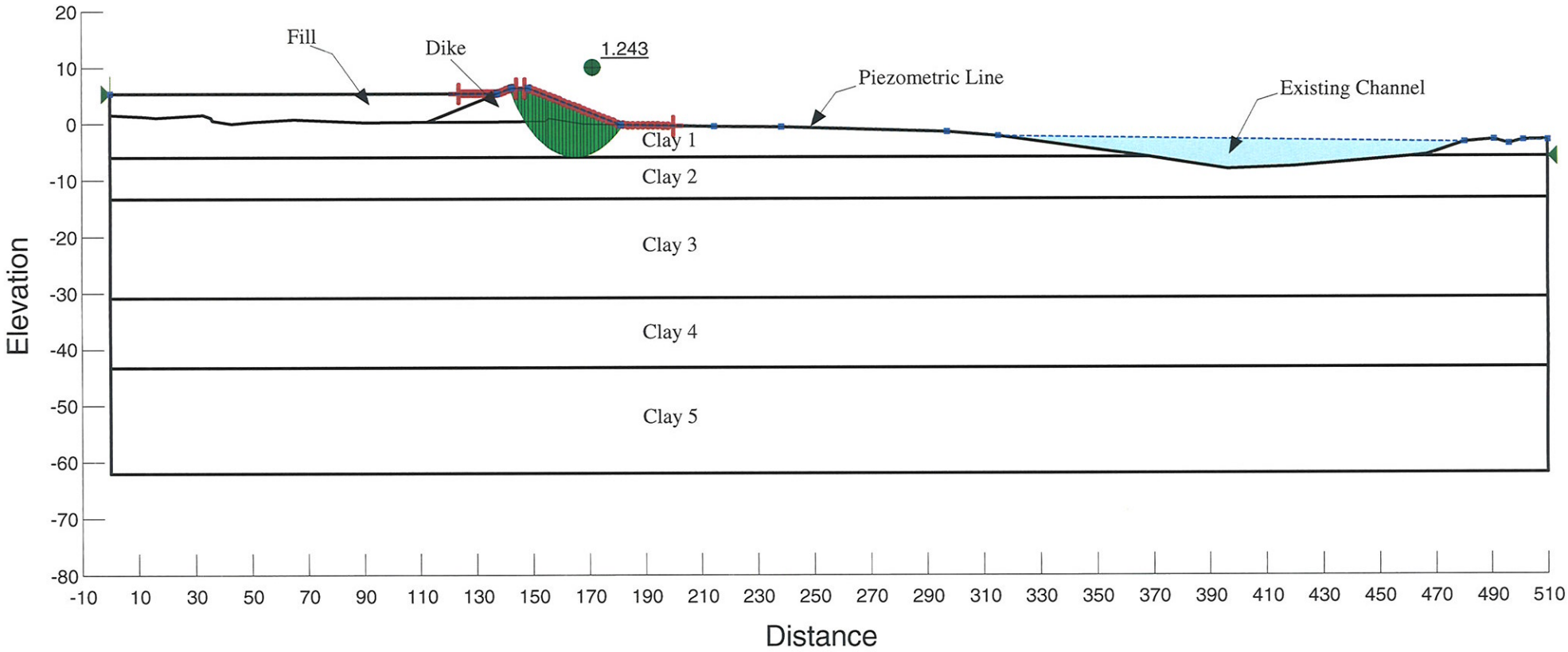

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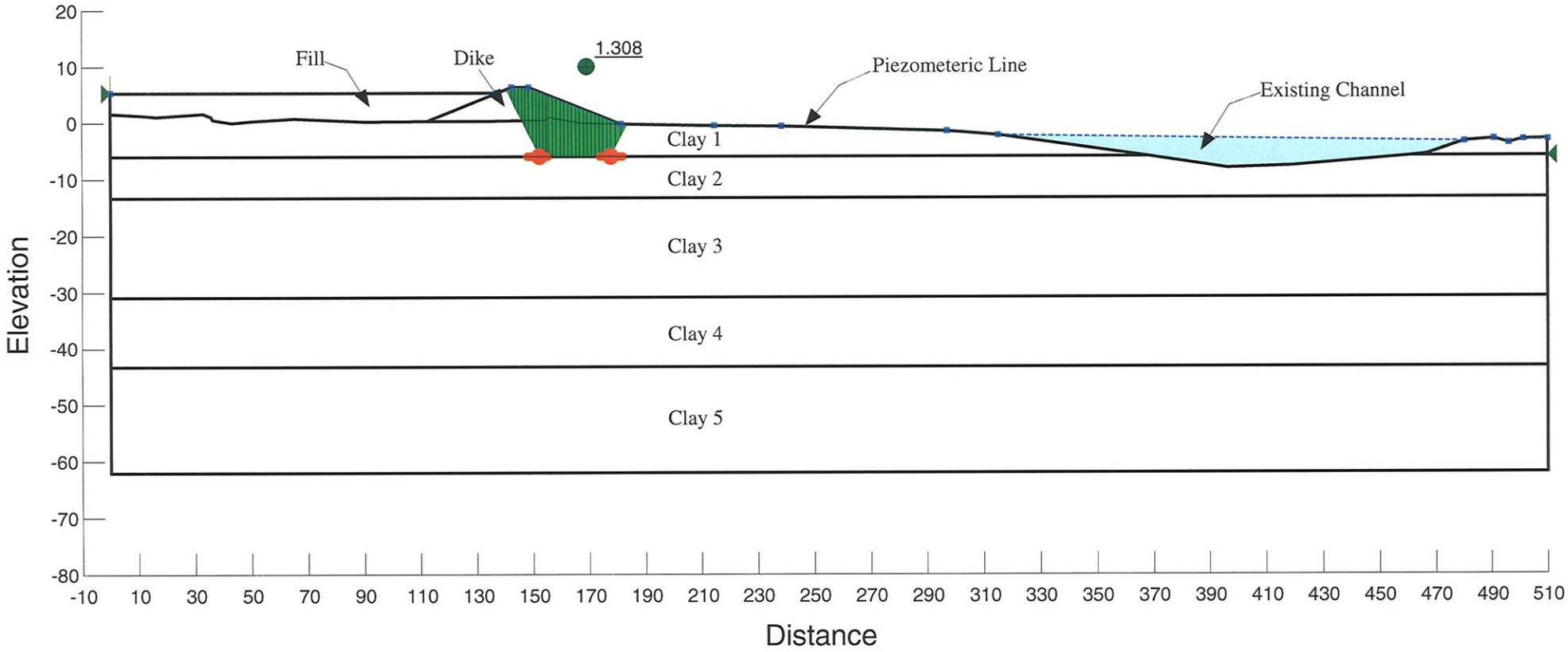
Figure 61

STABILITY ANALYSIS OF DIKE AGAINST CHANNEL
FAILURE TYPE: WEDGE
DIKE Ht: 6.0'; FILL Ht: 5.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °

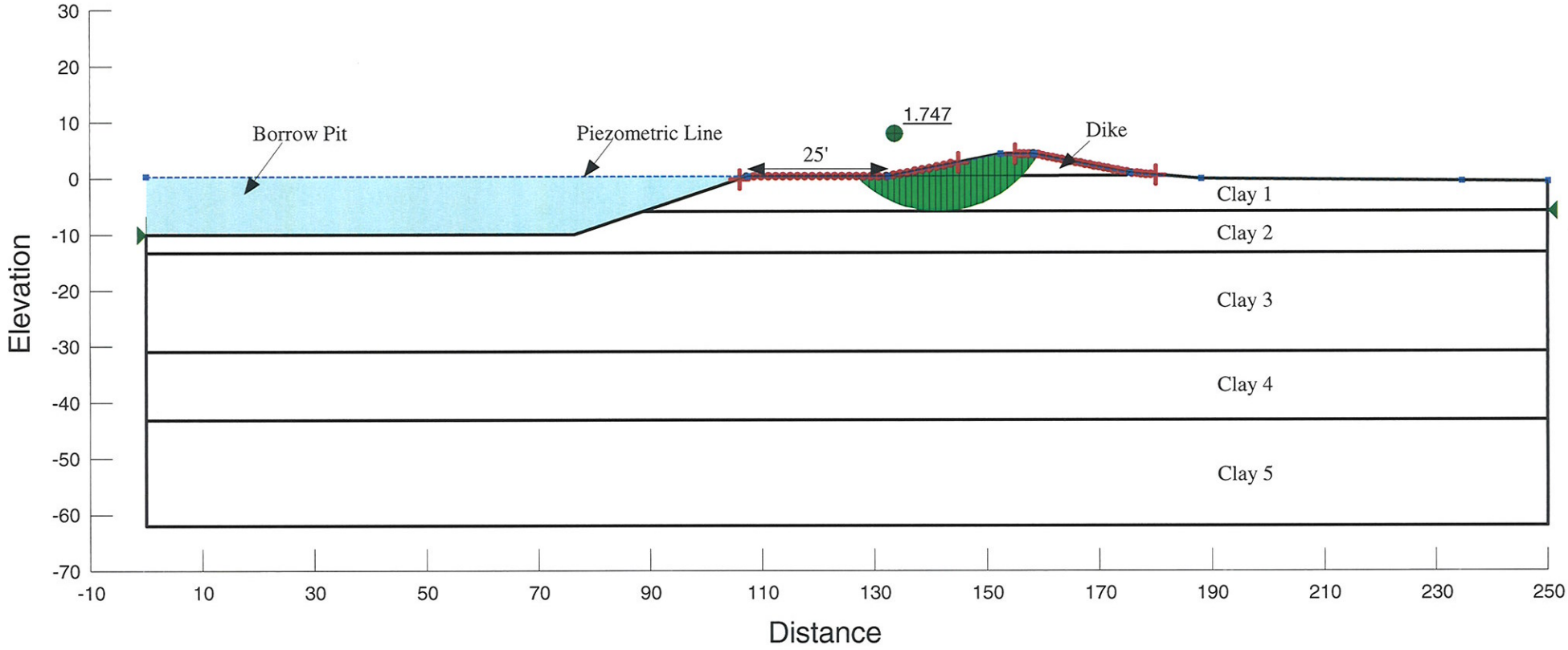


URS CORP.

Figure 62

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
BORROW PIT AT EL. -10'; DIKE Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °

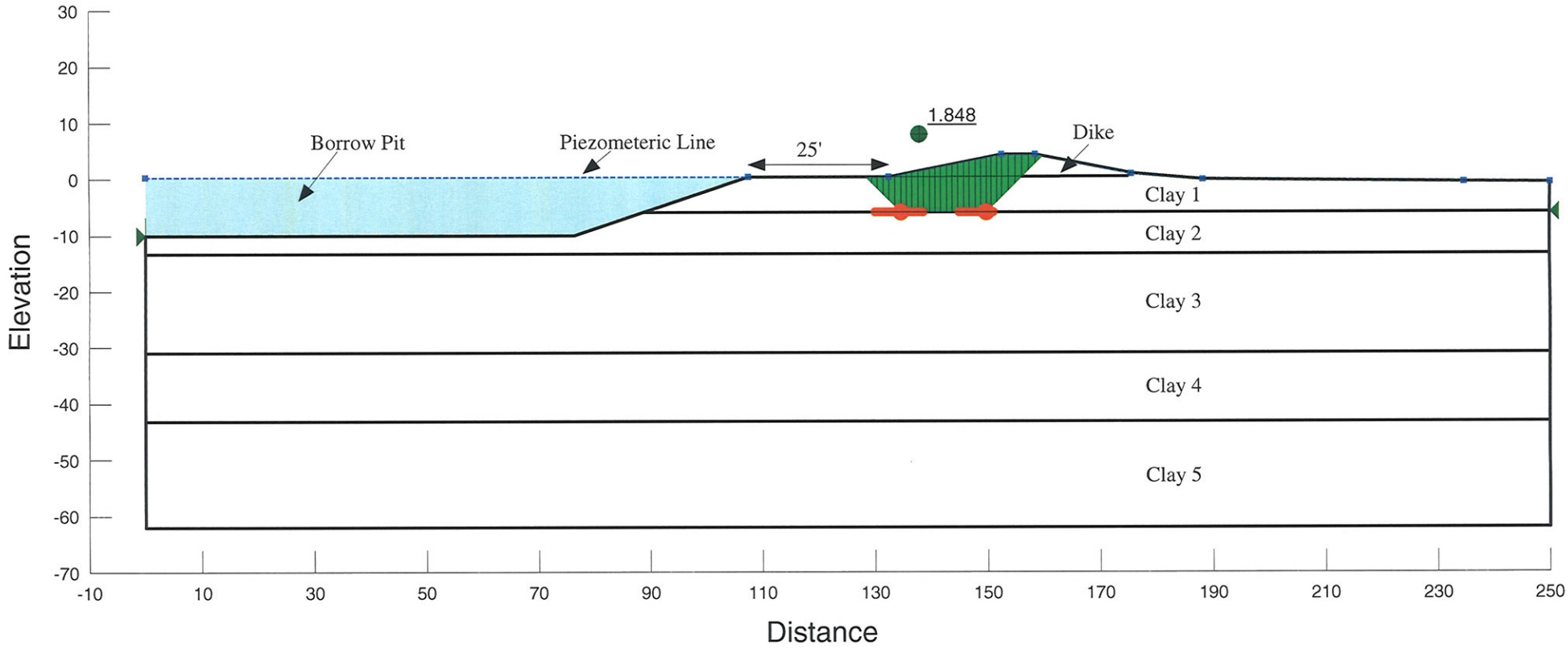


URS CORP.

Figure 63

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
BORROW PIT AT EL. -10'; DIKE Ht: 4.0'

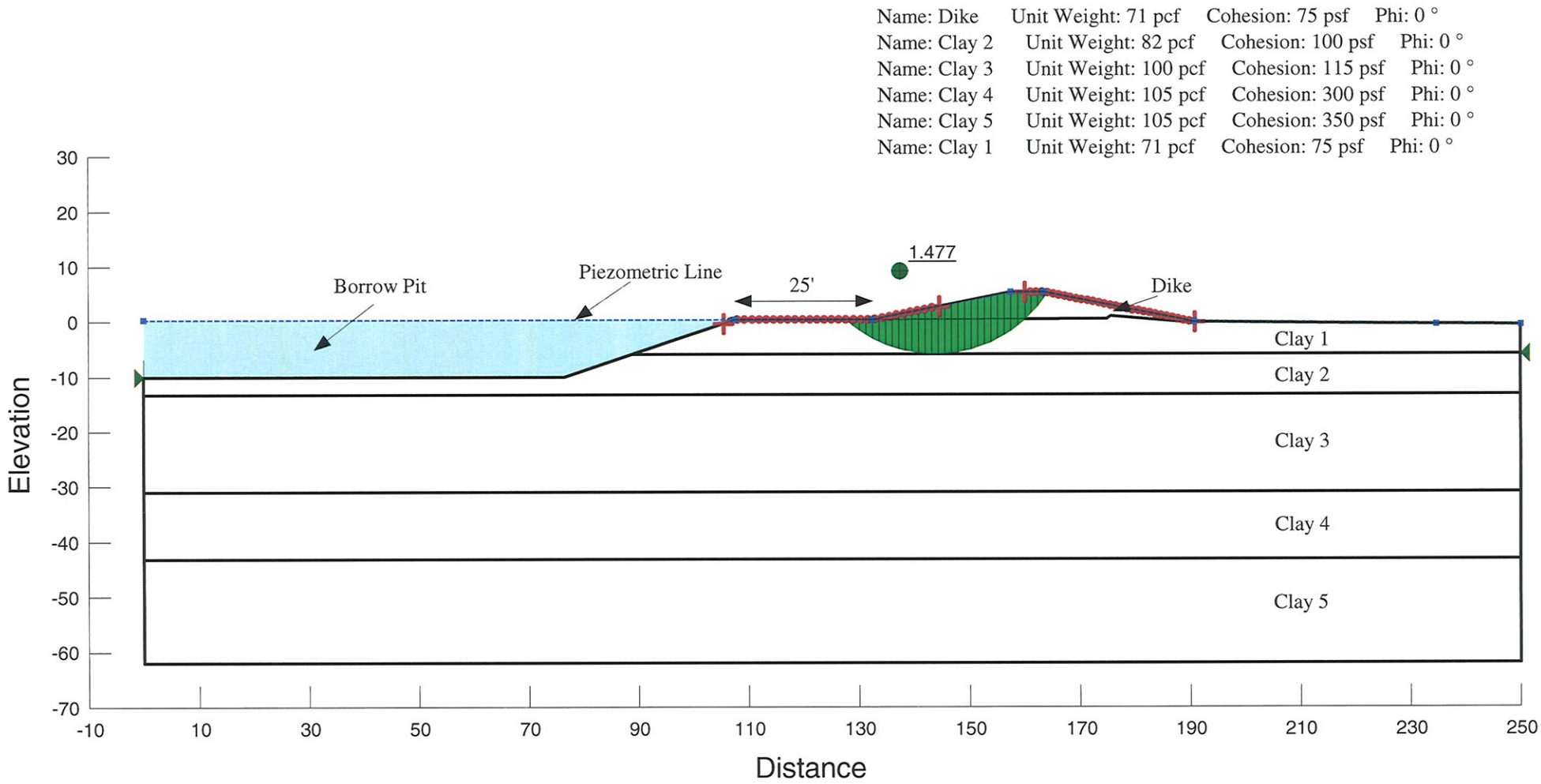
Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °



URS CORP.

Figure 64

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
BORROW PIT AT EL. -10'; DIKE Ht: 5.0'

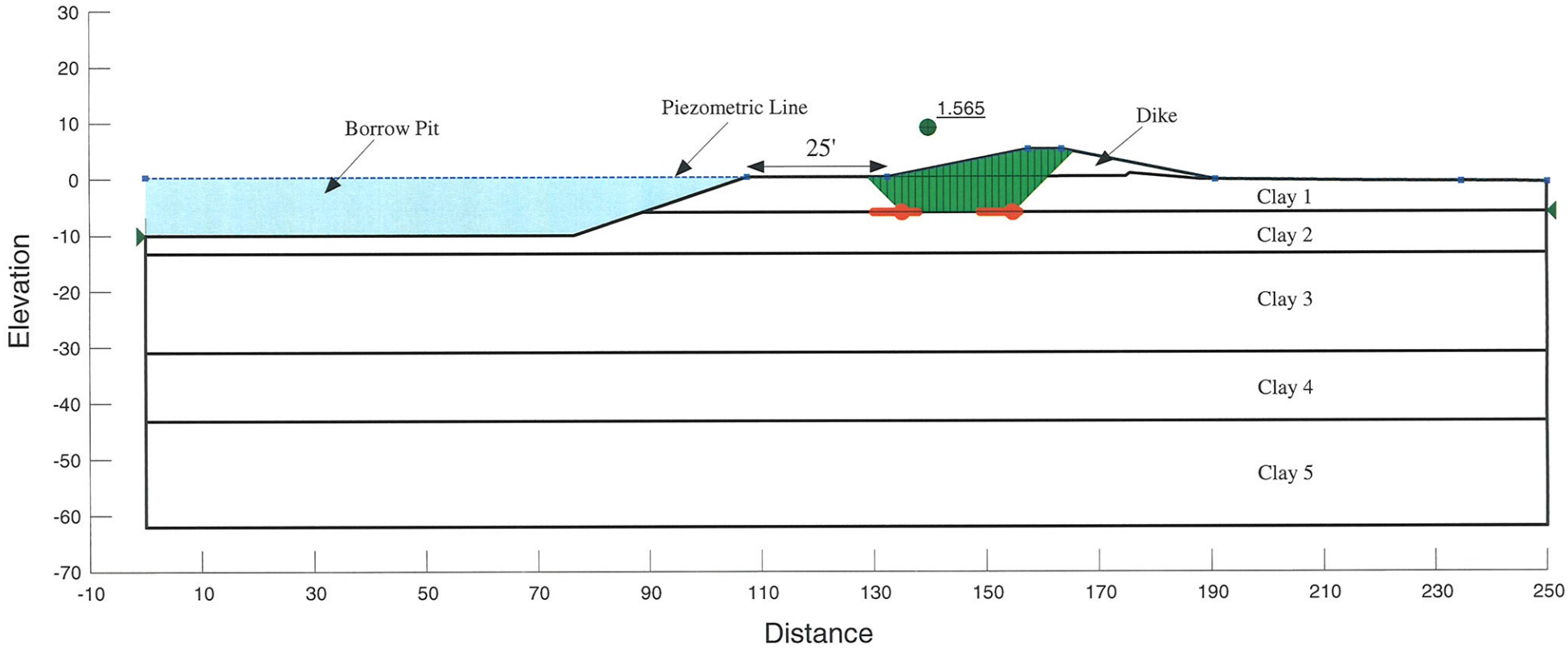


URS CORP.

Figure 65

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
BORROW PIT AT EL. -10'; DIKE Ht: 5.0'

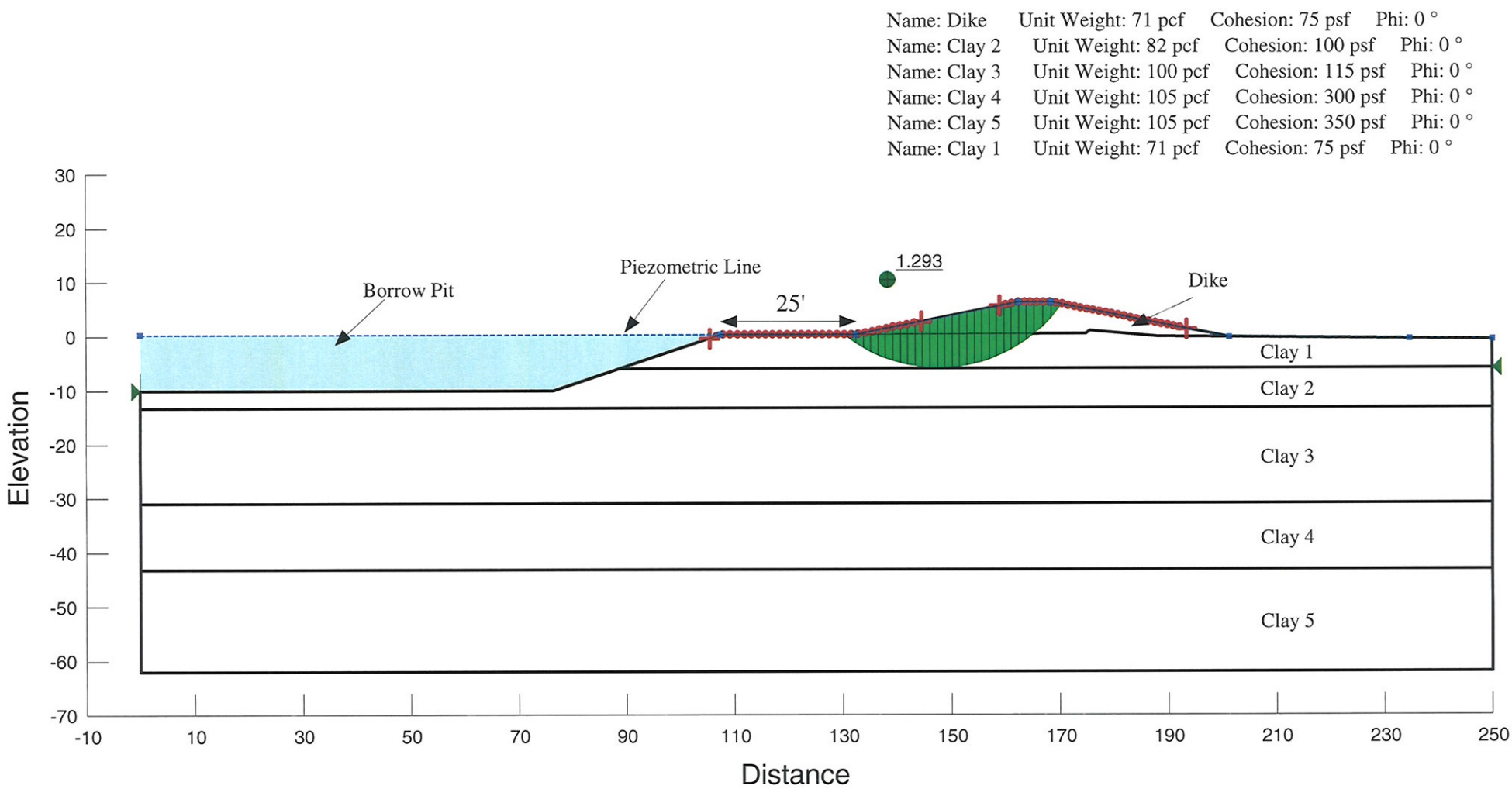
Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °



URS CORP.

Figure 66

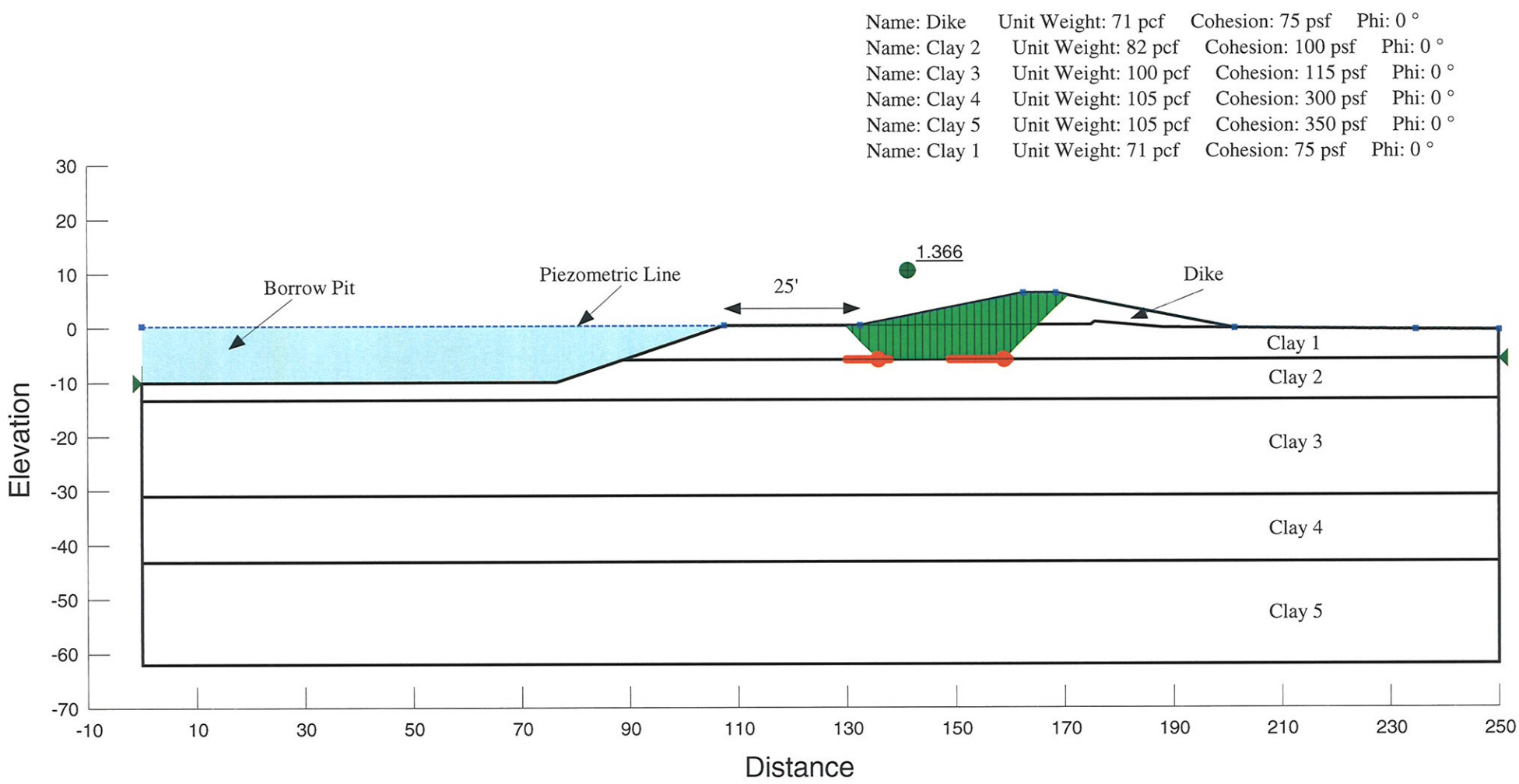
STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
BORROW PIT AT EL. -10'; DIKE Ht: 6.0'



URS CORP.

Figure 67

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
BORROW PIT AT EL. -10'; DIKE Ht: 6.0'

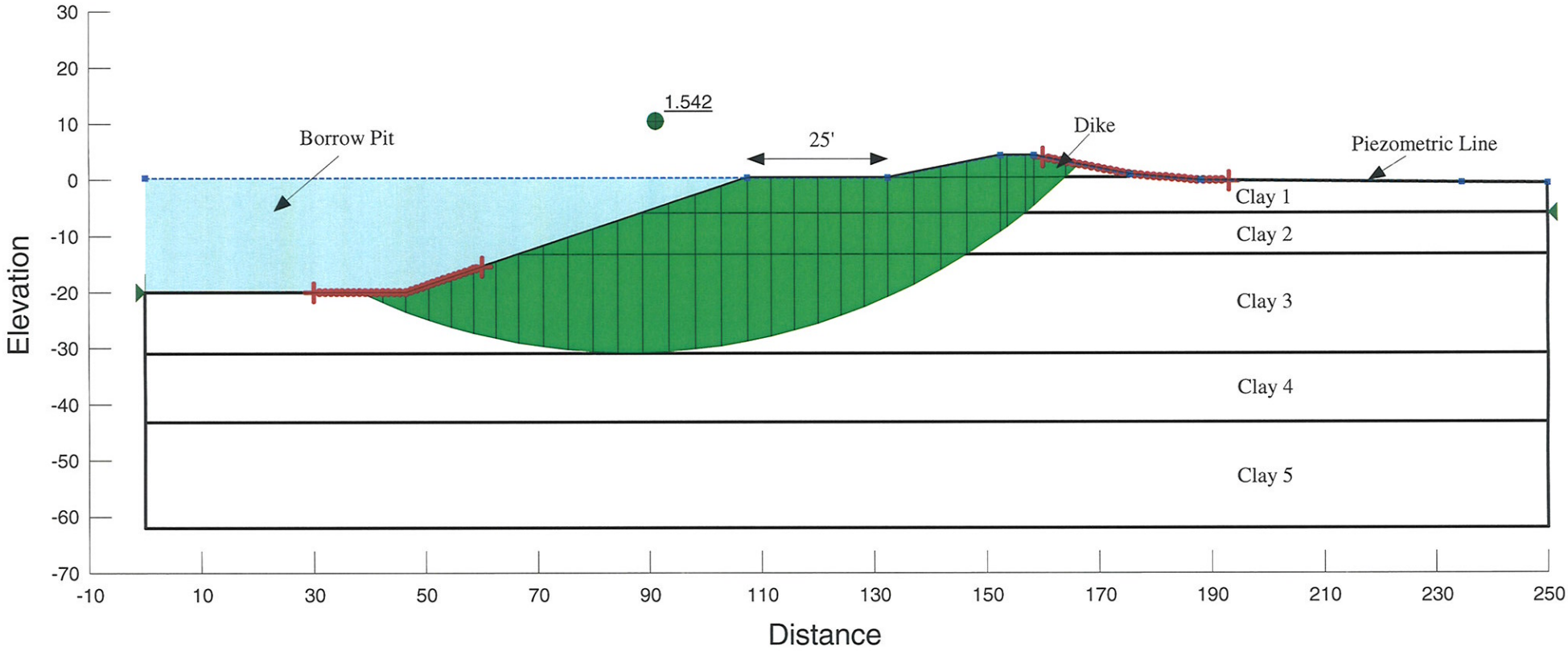


URS CORP.

Figure 68

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
BORROW PIT AT EL. -20'; DIKE Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °

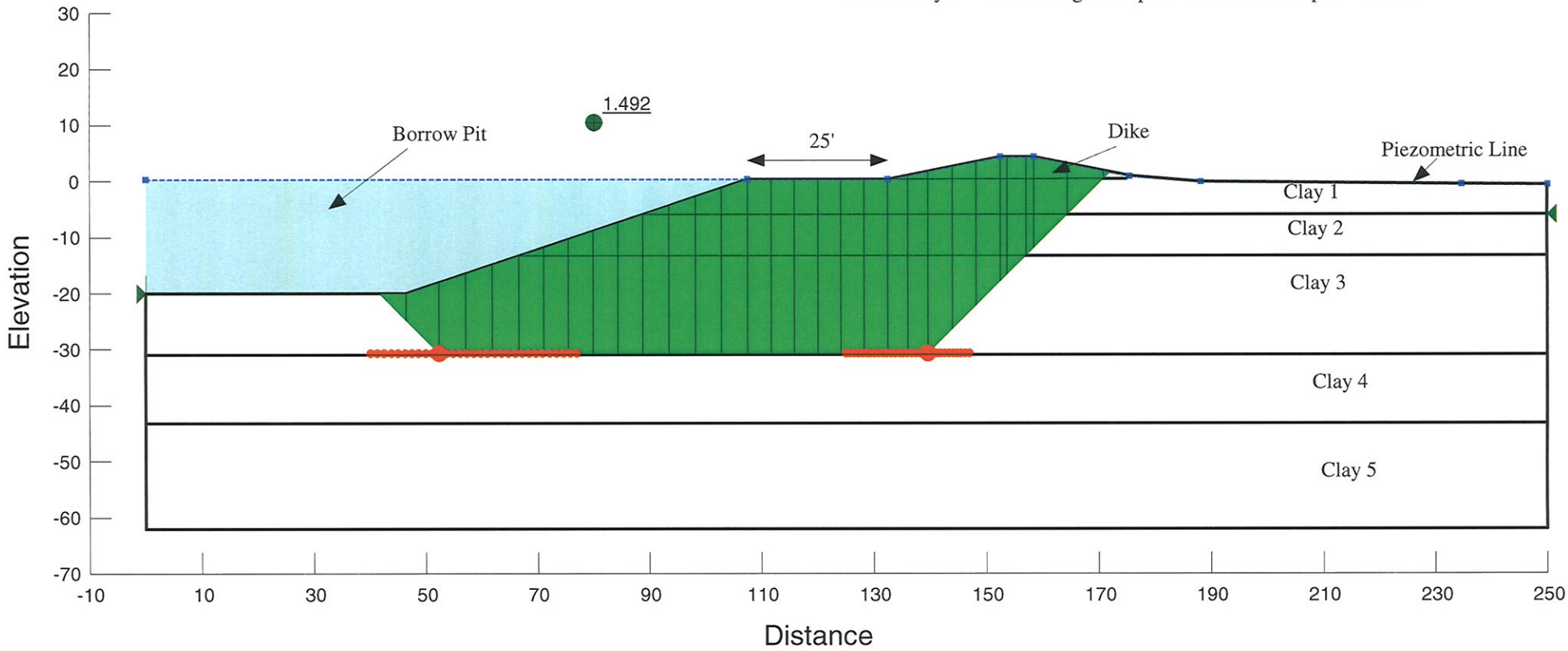


URS CORP.

Figure 69

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
BORROW PIT AT EL. -20'; DIKE Ht: 4.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °

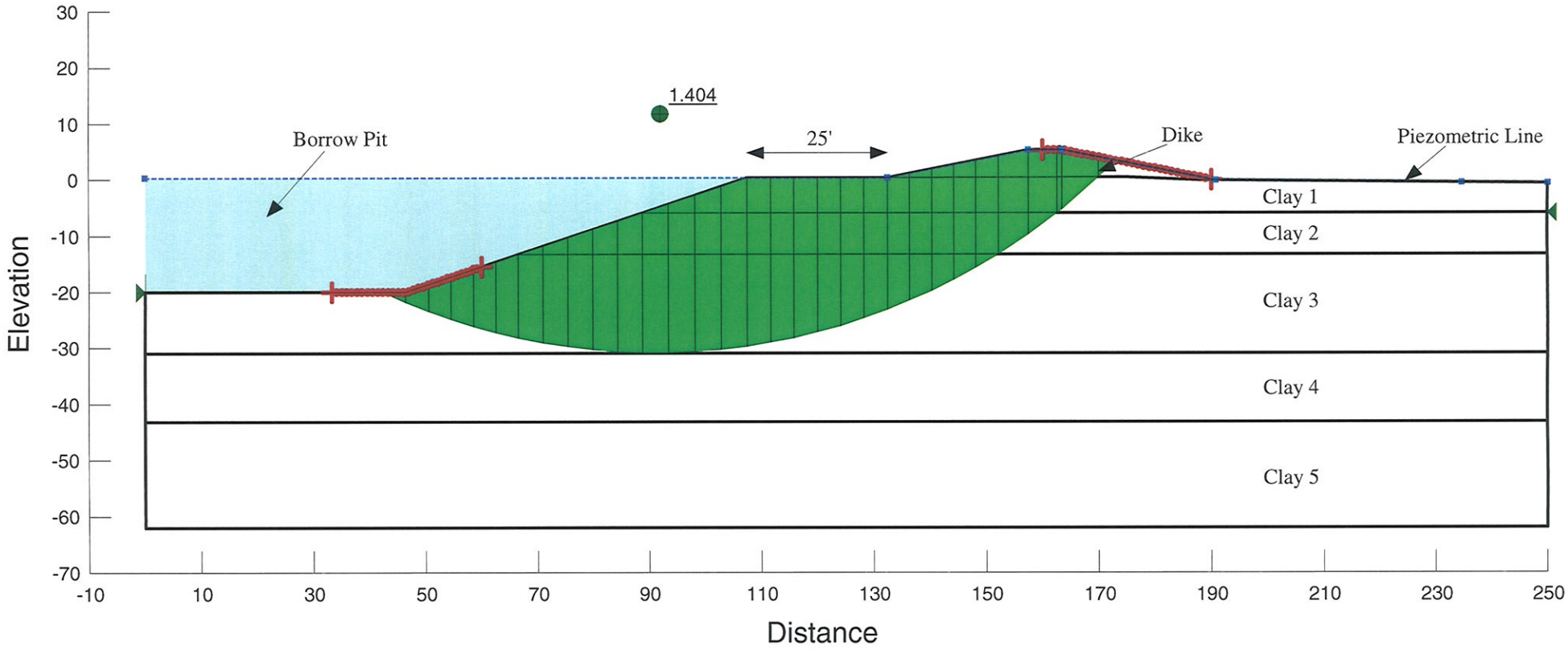


URS CORP.

Figure 70

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
BORROW PIT AT EL. -20'; DIKE Ht: 5.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °

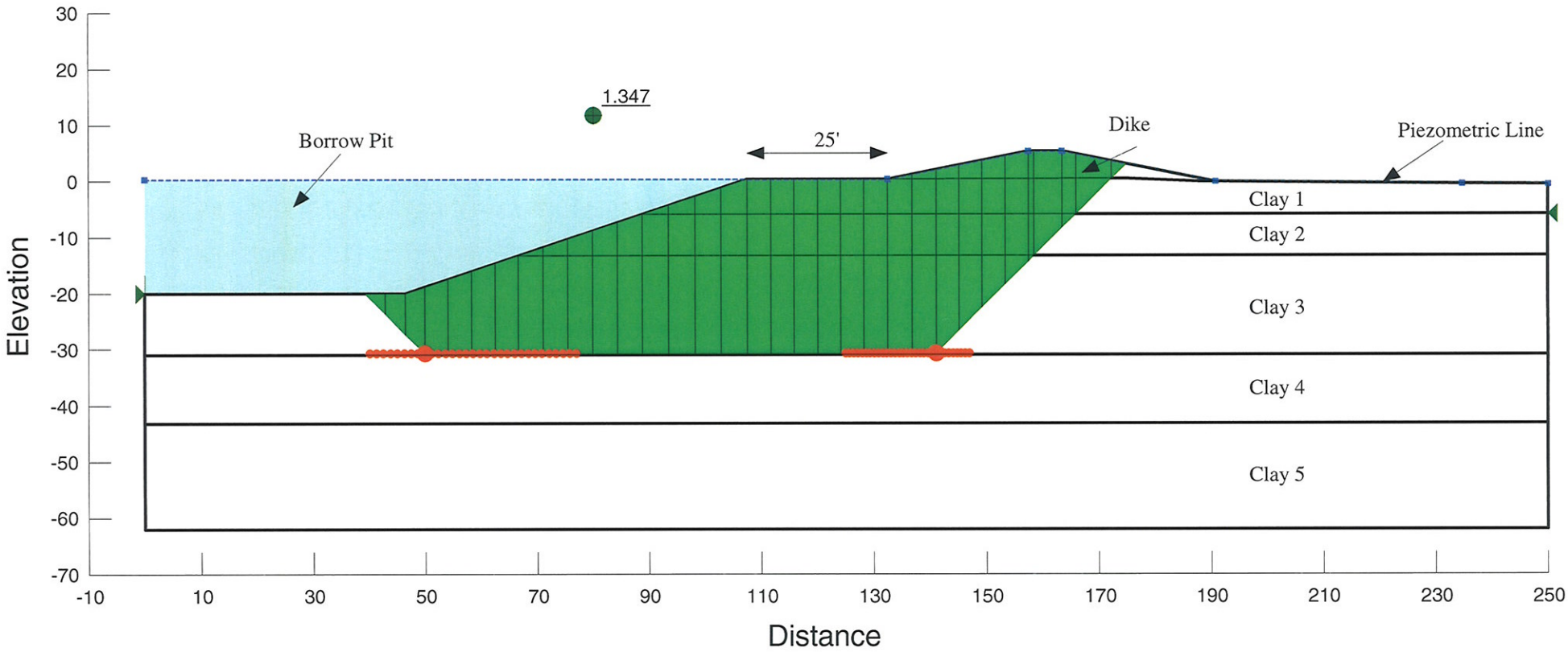


URS CORP.

Figure 71

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
BORROW PIT AT EL. -20'; DIKE Ht: 5.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °

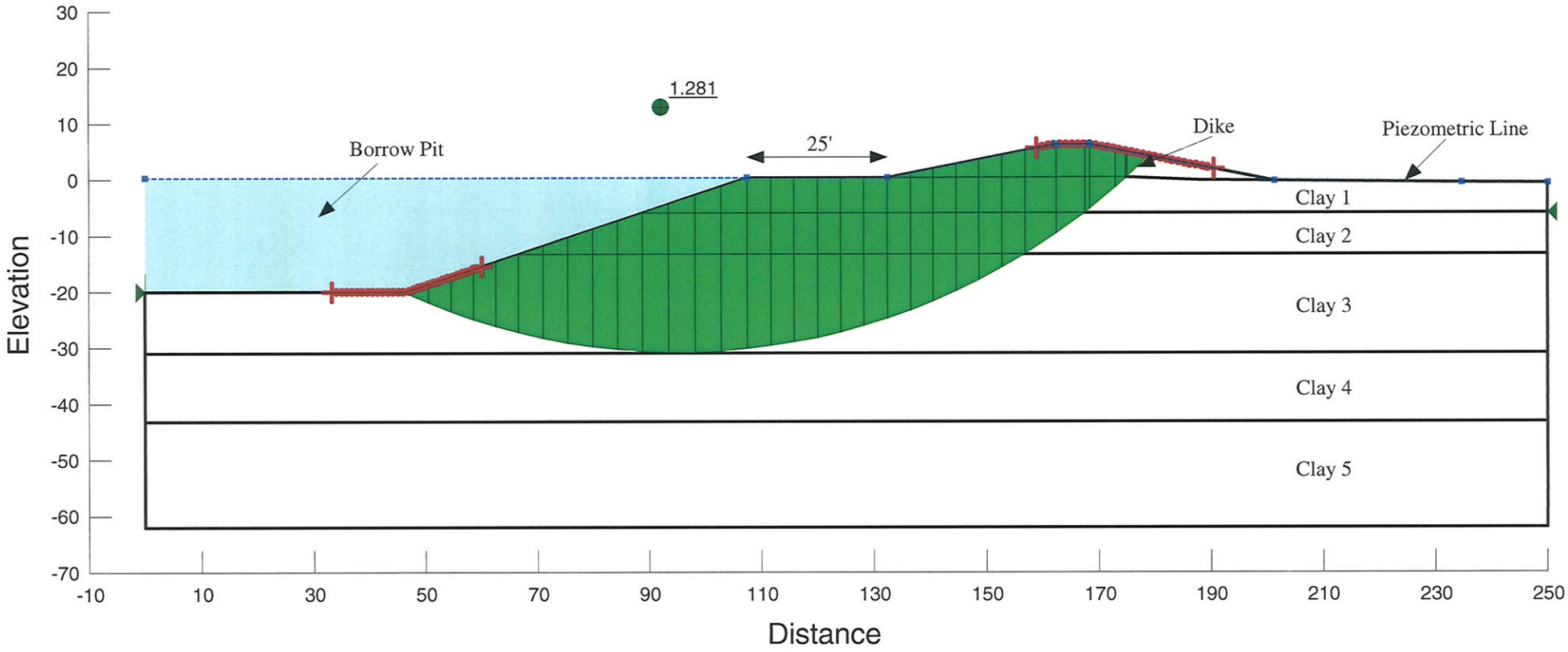


URS CORP.

Figure 72

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
BORROW PIT AT EL. -20'; DIKE Ht: 6.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °

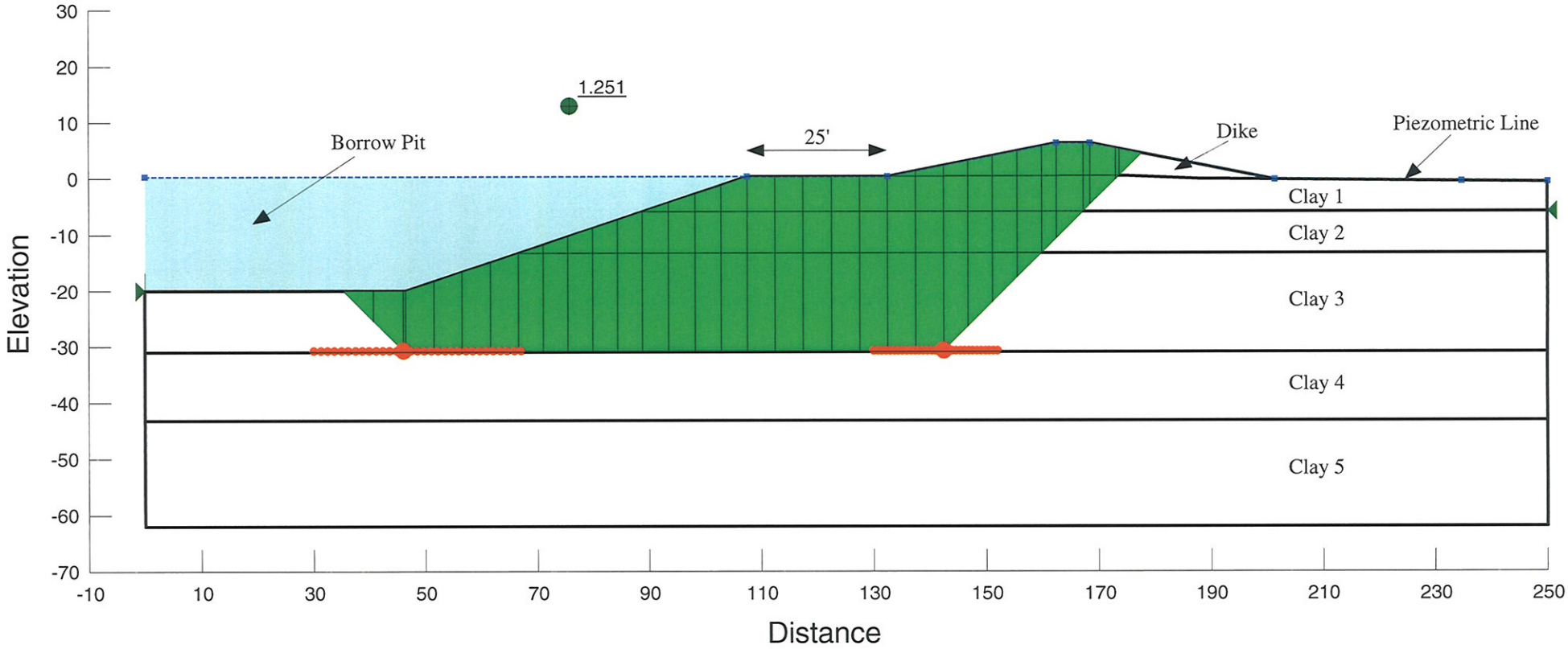


URS CORP.

Figure 73

STABILITY ANALYSIS OF DIKE AGAINST BORROW PIT
FAILURE TYPE: WEDGE
BORROW PIT AT EL. -20'; DIKE Ht: 6.0'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °

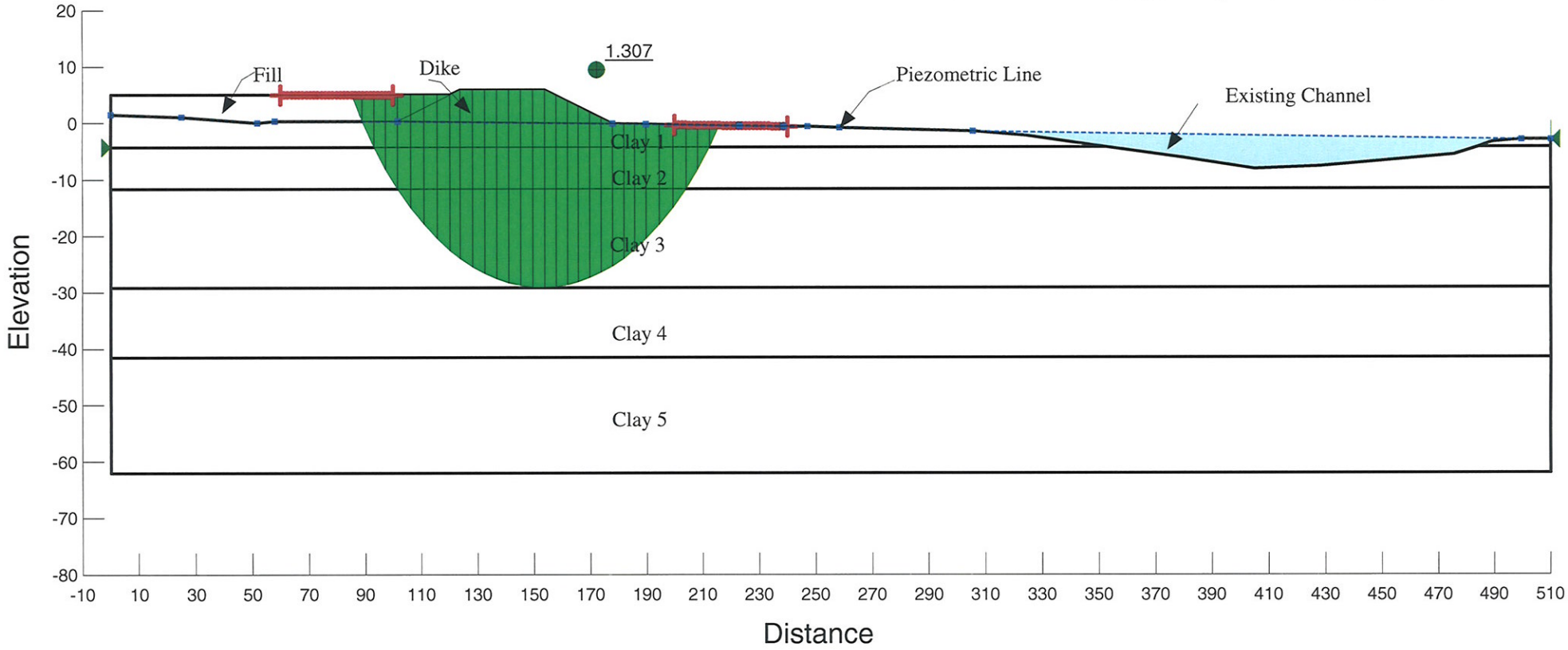


URS CORP.

Figure 74

STABILITY ANALYSIS OF RIDGE AGAINST CHANNEL
FAILURE TYPE: CIRCULAR
RIDGE Ht: 6.0'; FILL Ht: 5.0'
CROWN WIDTH: 30'

Name: Dike Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 1 Unit Weight: 71 pcf Cohesion: 75 psf Phi: 0 °
Name: Clay 2 Unit Weight: 82 pcf Cohesion: 100 psf Phi: 0 °
Name: Clay 3 Unit Weight: 100 pcf Cohesion: 115 psf Phi: 0 °
Name: Clay 4 Unit Weight: 105 pcf Cohesion: 300 psf Phi: 0 °
Name: Clay 5 Unit Weight: 105 pcf Cohesion: 350 psf Phi: 0 °
Name: Fill Unit Weight: 116 pcf Cohesion: 0 psf Phi: 30 °

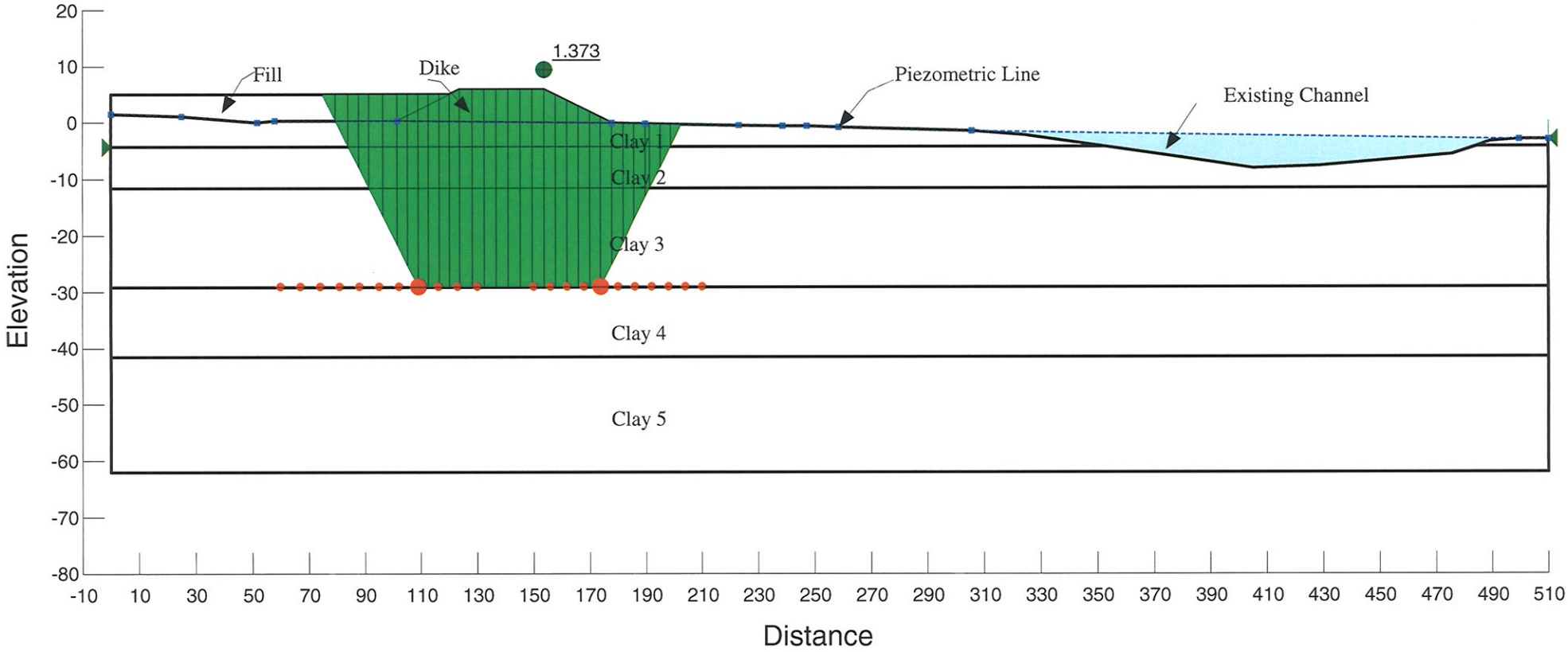


URS CORP.

Figure 75

STABILITY ANALYSIS OF RIDGE AGAINST CHANNEL
FAILURE TYPE: BLOCK or WEDGE
RIDGE Ht: 6.0'; FILL Ht: 5.0'
CROWN WIDTH: 30'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °
Name: Fill	Unit Weight: 116 pcf	Cohesion: 0 psf	Phi: 30 °

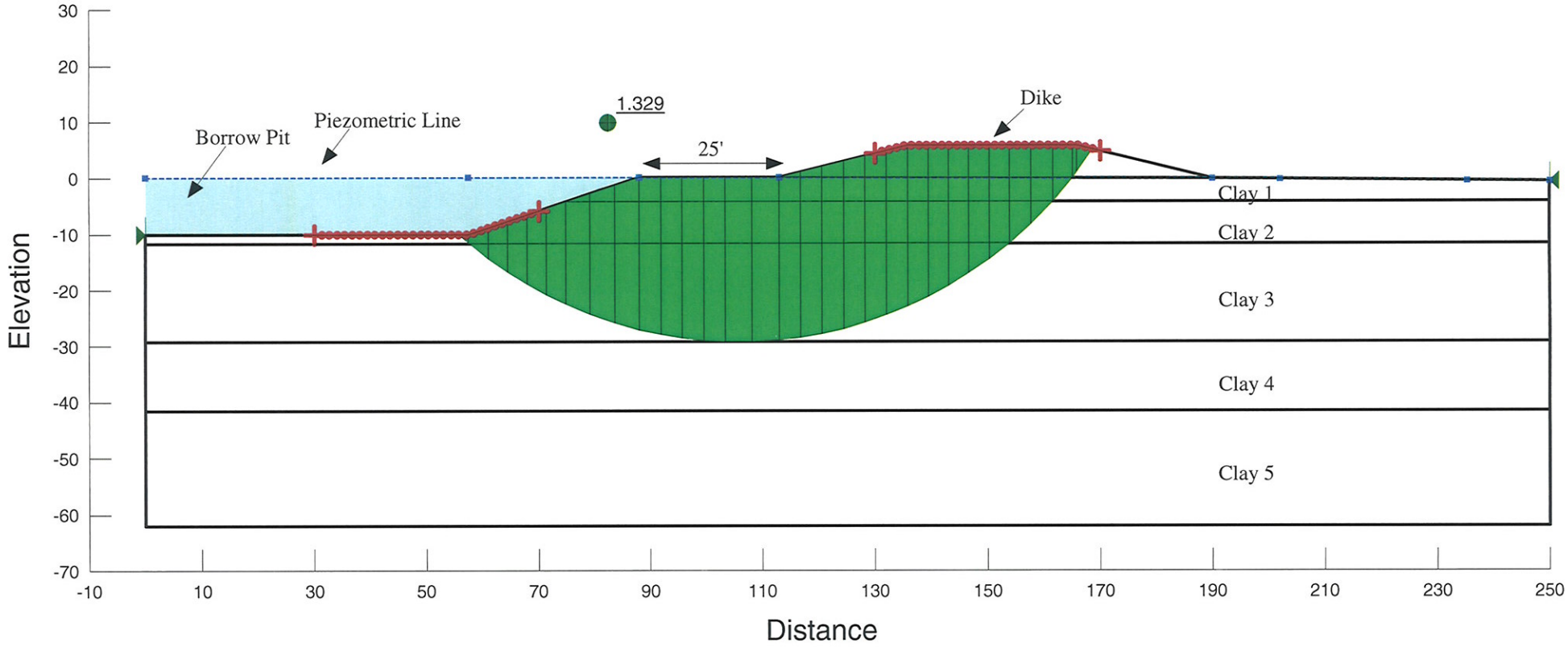


URS CORP.

Figure 76

STABILITY ANALYSIS OF RIDGE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
BORROW PIT AT EL. -10'; RIDGE Ht: 6.0'
CROWN WIDTH: 30'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

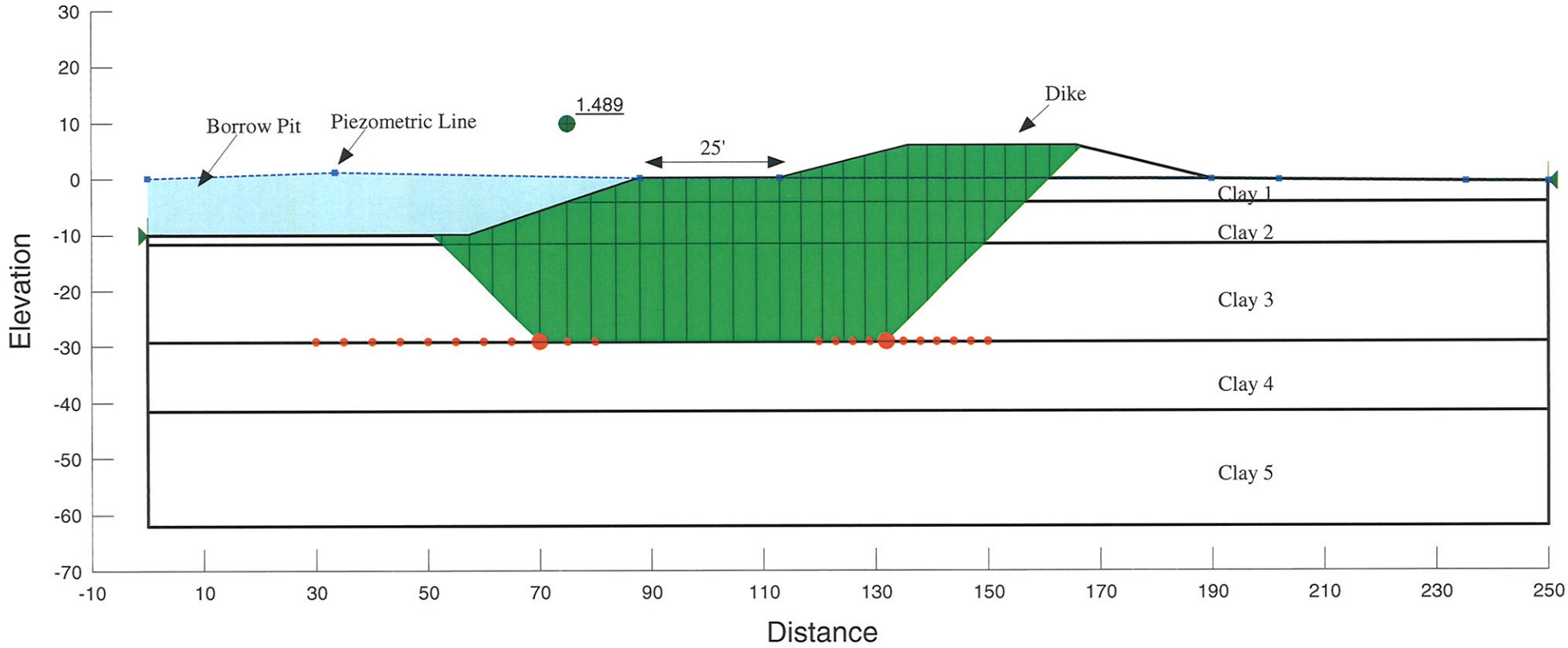


URS CORP.

Figure 77

STABILITY ANALYSIS OF RIDGE AGAINST BORROW PIT
FAILURE TYPE: BLOCK or WEDGE
BORROW PIT AT EL. -10'; RIDGE Ht: 6.0'
CROWN WIDTH: 30'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

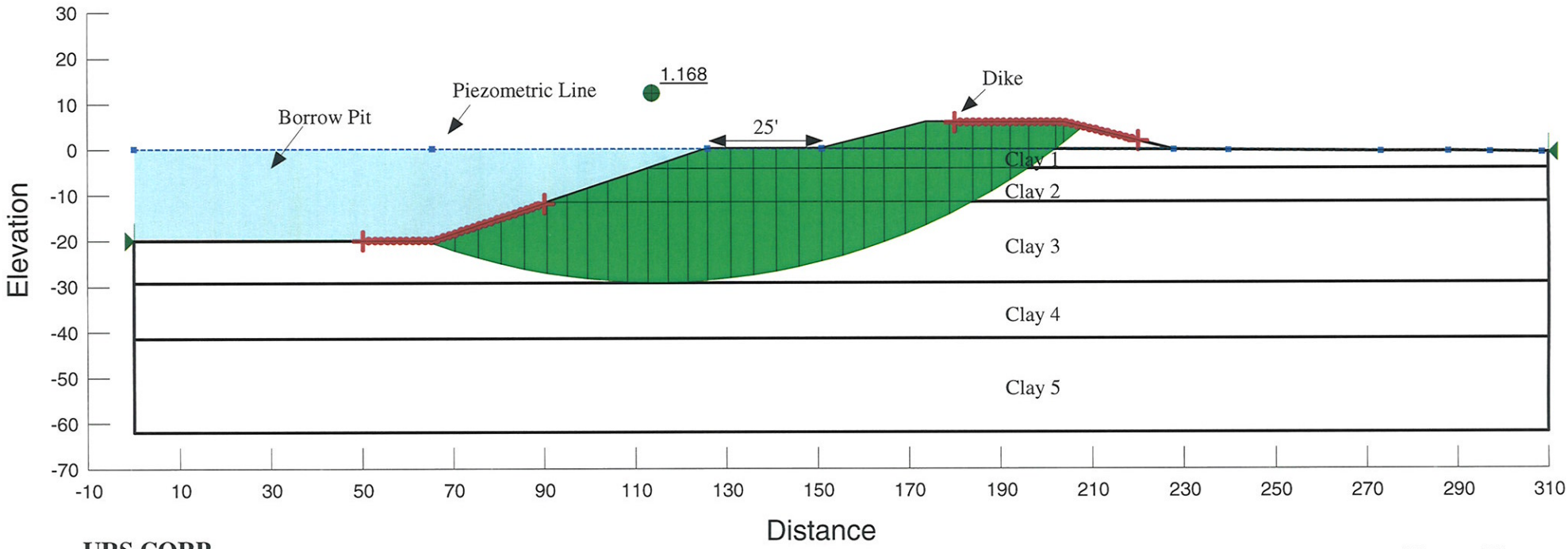


URS CORP.

Figure 78

STABILITY ANALYSIS OF RIDGE AGAINST BORROW PIT
FAILURE TYPE: CIRCULAR
BORROW PIT AT EL. -20'; RIDGE Ht: 6.0'
CROWN WIDTH: 30'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °



URS CORP.

Figure 79

STABILITY ANALYSIS OF RIDGE AGAINST BORROW PIT
FAILURE TYPE: BLOCK or WEDGE
BORROW PIT AT EL. -20'; RIDGE Ht: 6.0'
CROWN WIDTH: 30'

Name: Dike	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 1	Unit Weight: 71 pcf	Cohesion: 75 psf	Phi: 0 °
Name: Clay 2	Unit Weight: 82 pcf	Cohesion: 100 psf	Phi: 0 °
Name: Clay 3	Unit Weight: 100 pcf	Cohesion: 115 psf	Phi: 0 °
Name: Clay 4	Unit Weight: 105 pcf	Cohesion: 300 psf	Phi: 0 °
Name: Clay 5	Unit Weight: 105 pcf	Cohesion: 350 psf	Phi: 0 °

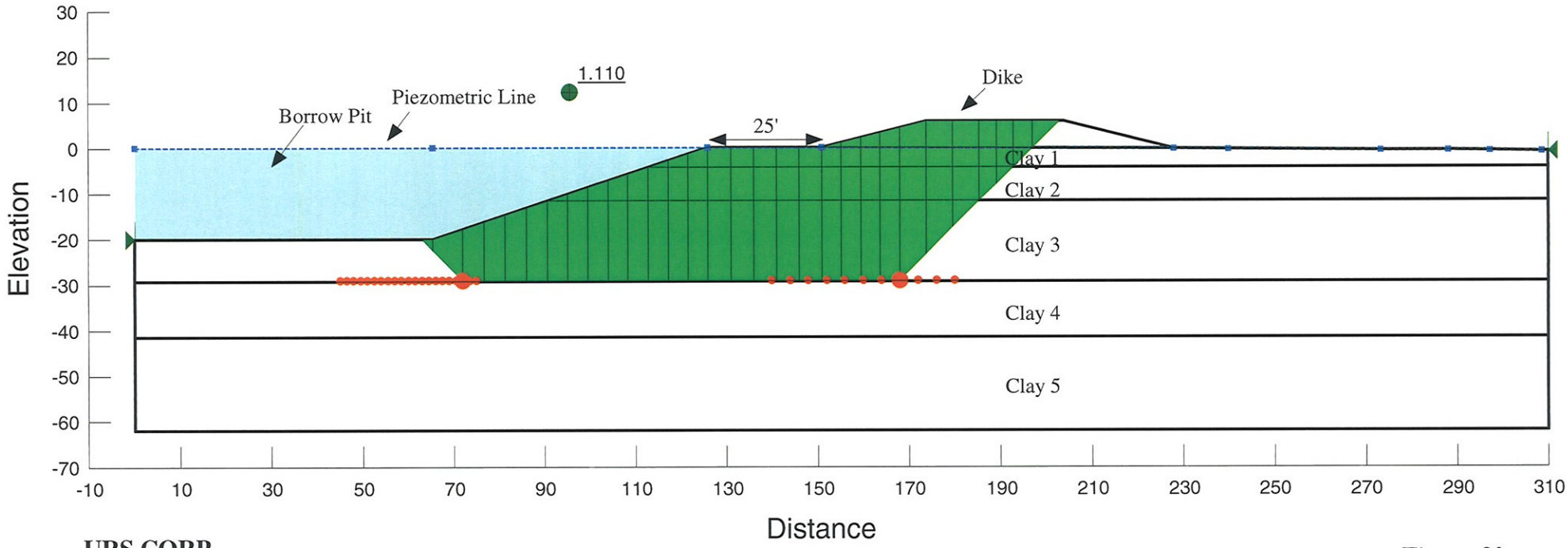


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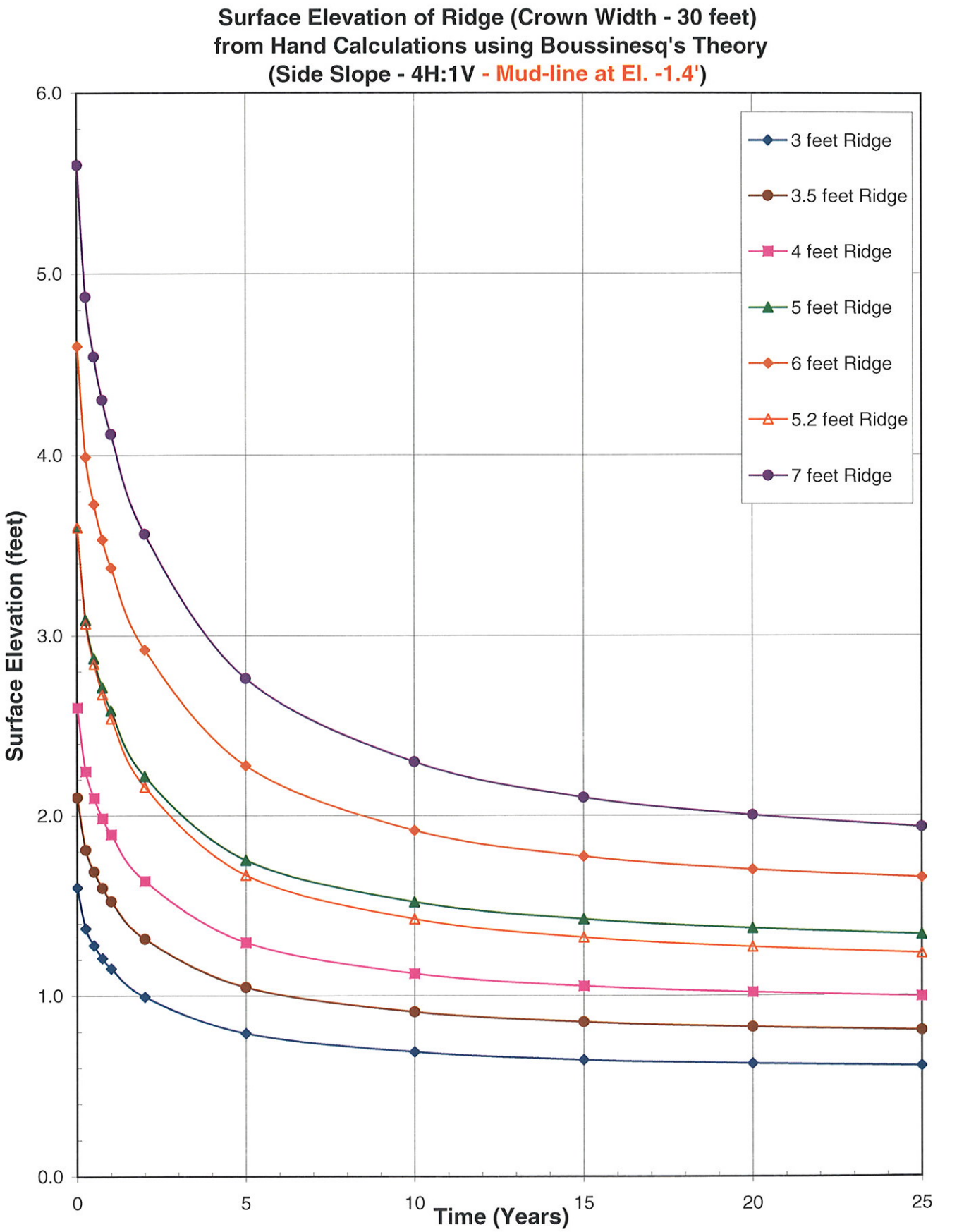
Figure 80

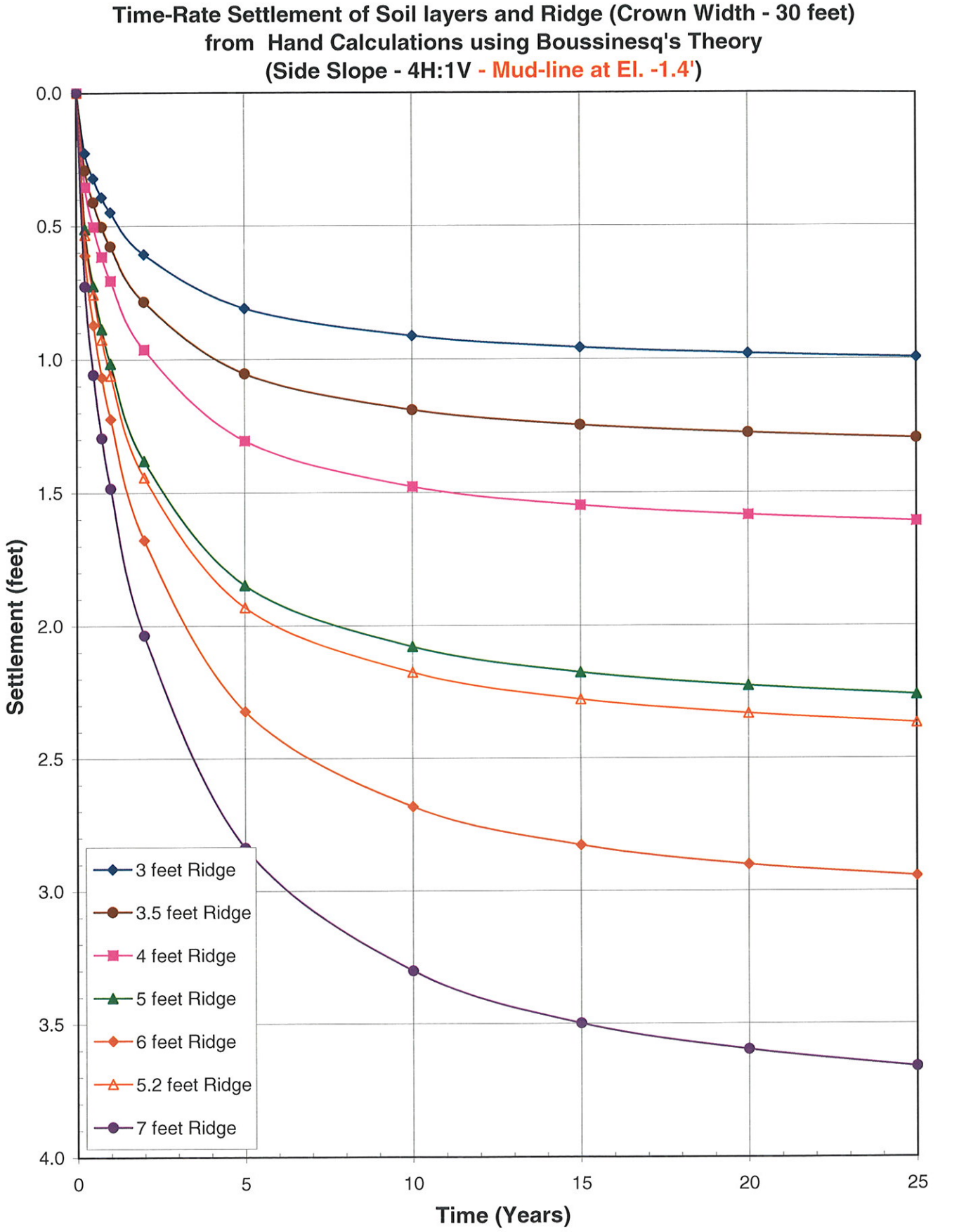
APPENDIX H

Figure No. 81



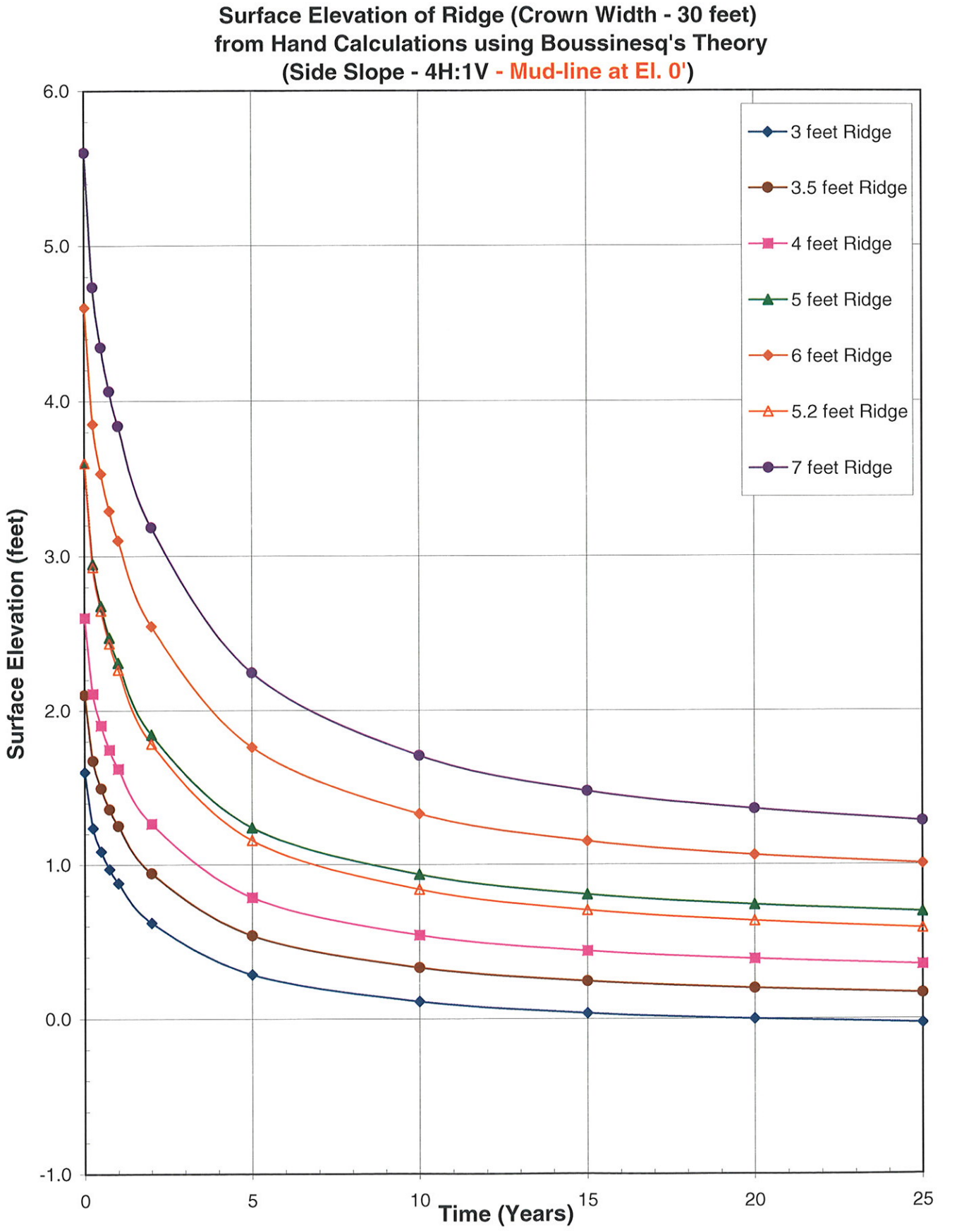
URS CORP.

Figure No. 82



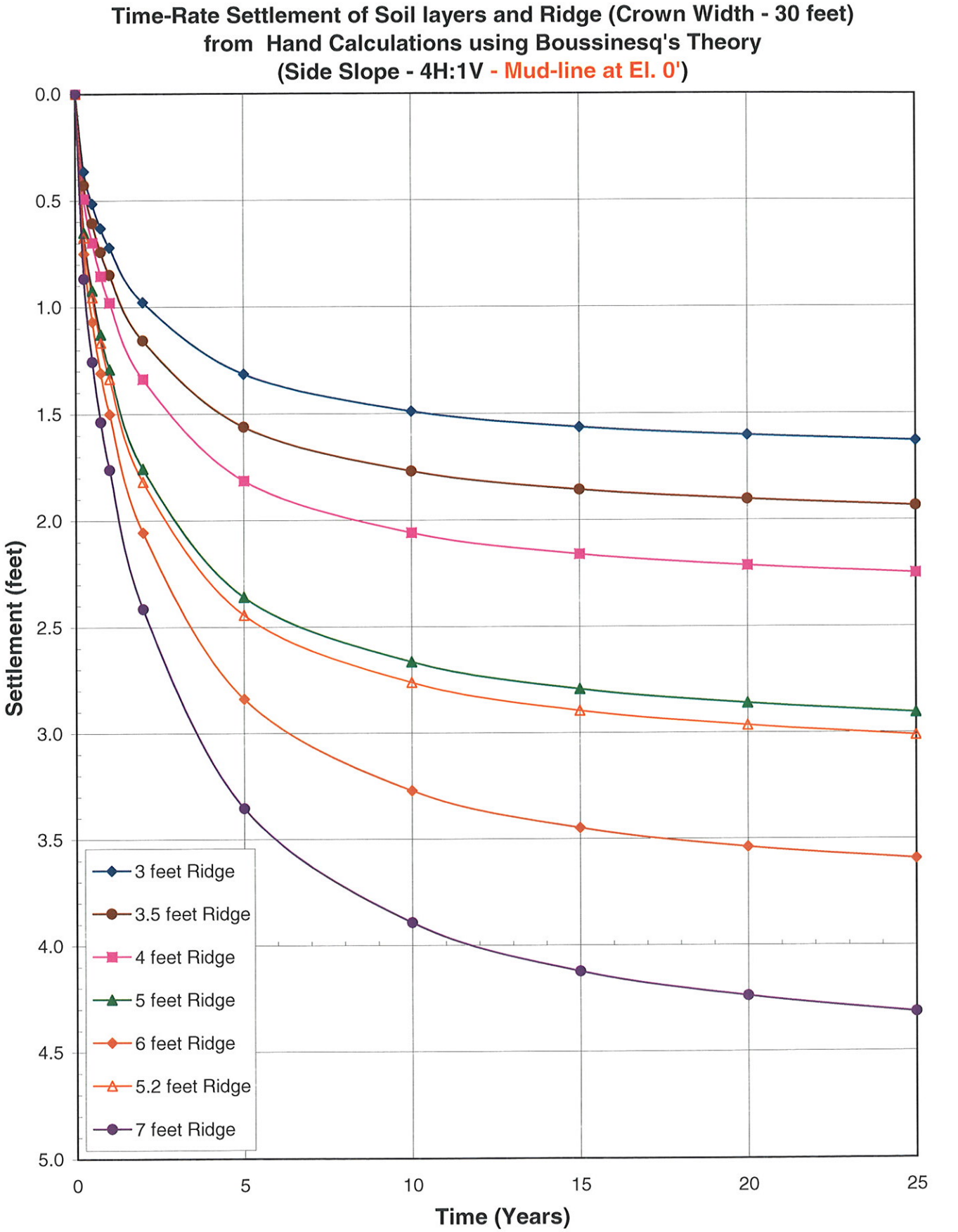
URS CORP.

Figure No. 83



URS CORP.

Figure No. 84



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APPENDIX I

URS

Job Bayou DuPont | Project No. 19228956 | Page 1 of 4

Description Bearing Capacity Calculations | Computed by Ananth T.B. | Date 6/28/09 | Sheet ___ of ___

Checked by Feng Zhu | Date 07/10/09 | Reference

* The allowable bearing capacity of the soil was computed to determine the maximum height of the fill and the dike that could be placed at the project site.

* Citing the use of the site for human activities, we assumed that a factor of safety of 1.5 would be suitable for our bearing capacity calculations.

* Based on the strength profile from Figure-4, we used a minimum strength of 75 psf for the bearing capacity of the fill and the dike.

* The fill and the dike were placed on an Organic Peat (PT) layer, hence we assumed $\phi' = 0$

(*) Finally, the 1-D Terzaghi bearing capacity equation for a strip footing was used

$$q_u' = c' N_c' + q N_q' + 0.5 \gamma B N_\gamma'$$

for $\phi' = 0$, $N_c' = 5.7$; $N_q' = 1$; $N_\gamma' = 0$

also, $q = \gamma D_f = 0$ $(\because D_f = 0)$

$\therefore$ Ultimate Capacity, $q_u = C N_c = 5.7C$

Allowable Capacity $= q_{all} = \dfrac{5.7C}{1.5}$

Bearing Capacity of fill:

$$(q_{all})_{fill} = \frac{5.7C}{1.5} = \frac{5.7 * 75}{1.5} = 285 \text{ psf}$$

$\gamma_{fill} = 116$ pcf

$$\text{Maximum height of fill} = \frac{(q_{all})_{fill}}{\text{Weight of fill}}$$

(*) We assumed the water table is 1.4 feet above the Organic Peat layer i.e. the water table is at elevation 0.0 and the Peat layer is at elevation −1.4.

$$(H_{max})_{fill} = 1.4 + \frac{[285 - (116 - 62.4) * 1.4]}{116}$$

$$(H_{max})_{fill} \approx 3.2 \text{ feet}$$

Bearing Capacity of Dike:

$$(q_{all})_{Dike} = \frac{5.7 * 75}{1.5} = 285 \text{ psf}$$

$$\gamma_{Dike} = 71 \text{ pcf}$$

$$(H_{max})_{Dike} = 1.4 + \frac{[285 - (71 - 62.4) * 1.4]}{71}$$

$$(H_{max})_{Dike} \cong 5.2 \text{ feet}$$

(*) Hence, we recommend using 3 feet of fill and 5 feet of dike such that the elevation difference between the dike and the dredged fill is atleast 1 feet.

(*) Final elevation of 5 feet dike (CW = 6 feet) after 20 years = + 1.575

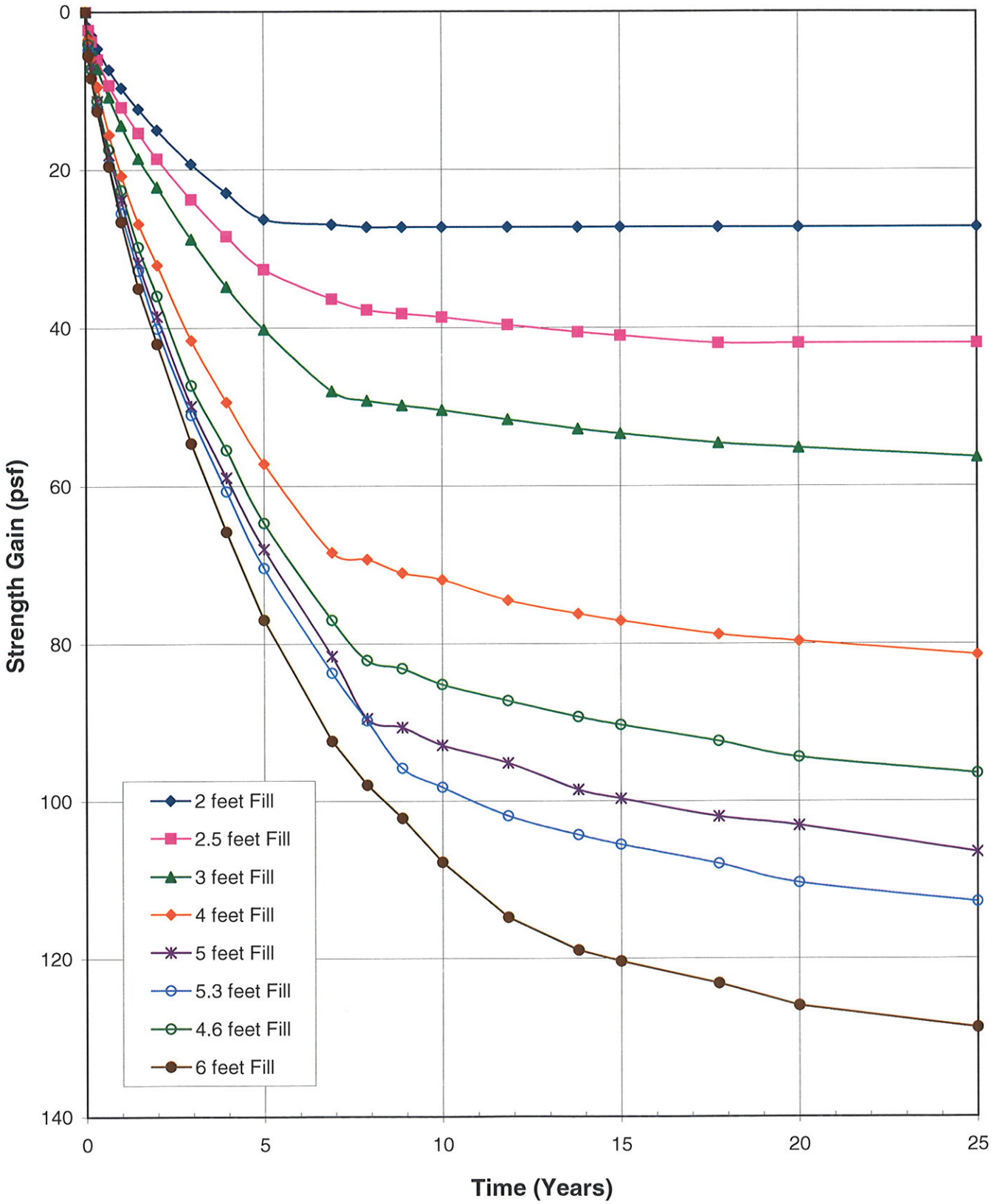
Final elevation of 3 feet fill after 20 years = - 0.502

Elevation Difference = 2.077 feet

÷ CW = Crown Width

Figure No. 85

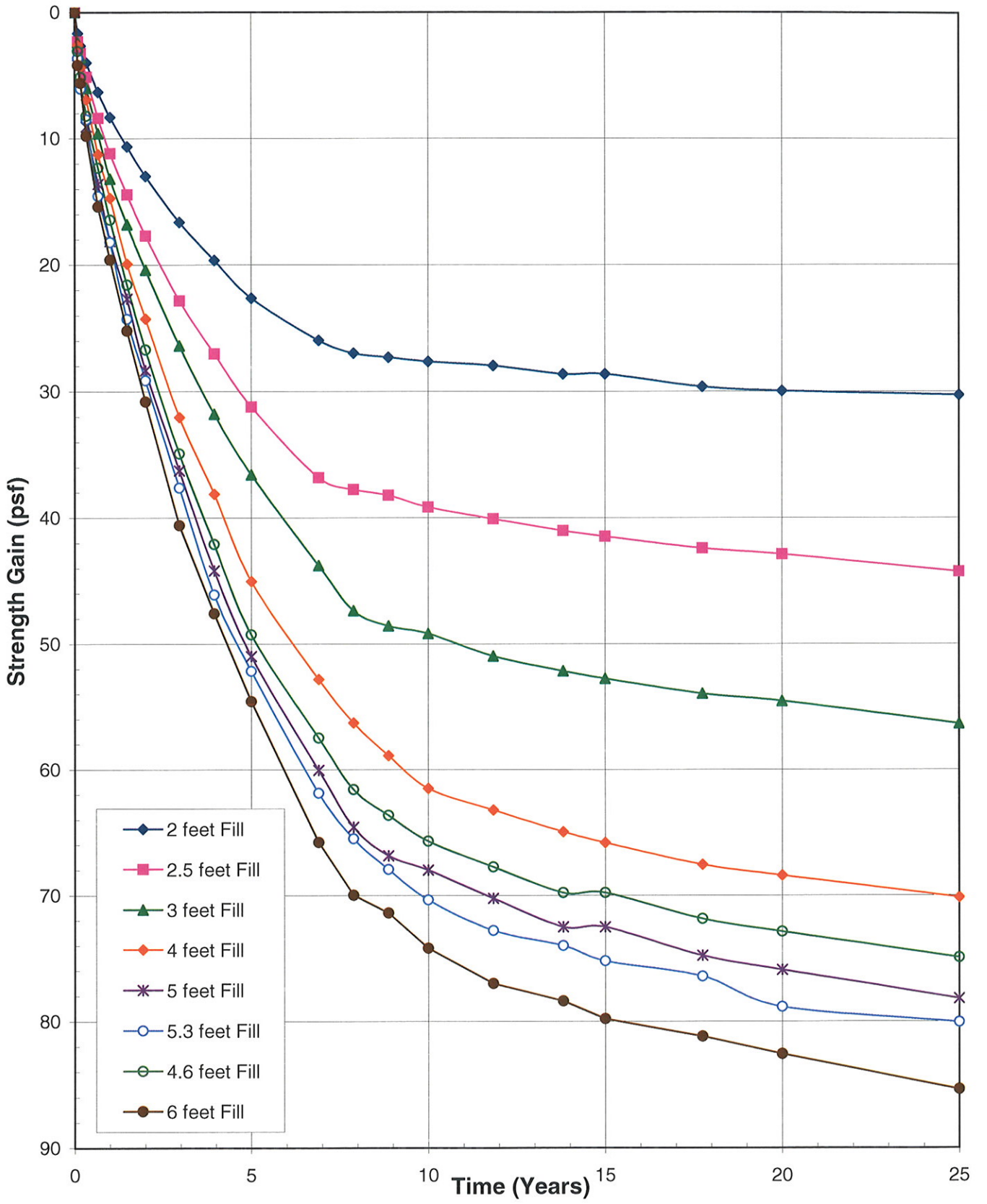
Strength Gain in Compressible Layers due to Actual Dredged Fill Height from PSDDF



URS CORP.

Figure No. 86

Strength Gain in Compressible Layers due to Equivalent Dredged Fill Height from PSDDF



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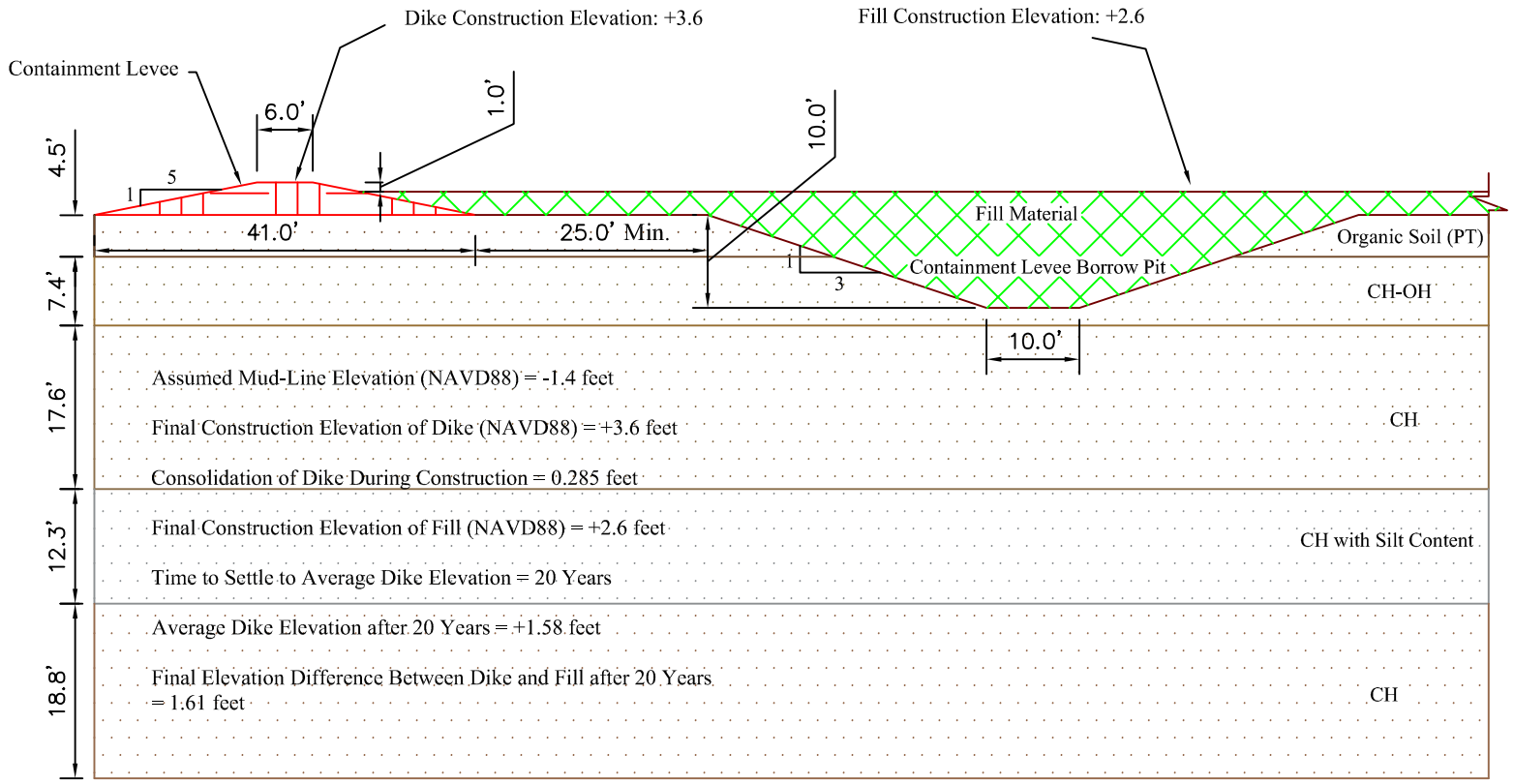


URS
7389 Florida Blvd., Suite 300
Baton Rouge, Louisiana 70806
225/922-5700

SCALE:	DRAWN BY: ABT	DATE: 07/16/09
1"=20'	CHKD. BY: IH	DATE: 07/16/09

BAYOU DUPONT MARSH CREATION
AND RIDGE RESTORATION

FINAL CONSTRUCTION ELEVATION

PROJ. NO.
19228956

FIG. NO. 87

LABORATORY RESULTS

Southern Earth Sciences, Inc.

Laboratory Test Results

Project: **Bayou DuPont** | **Technical Responsibility:** | **Quality Assurance Officer**

Client: URS

7389 Florida Blvd., Suite 300, Baton Rouge, LA 70806 | Project No.: **B09-012** | PM: S. Aviles | Date of Issue: 3/12/2009

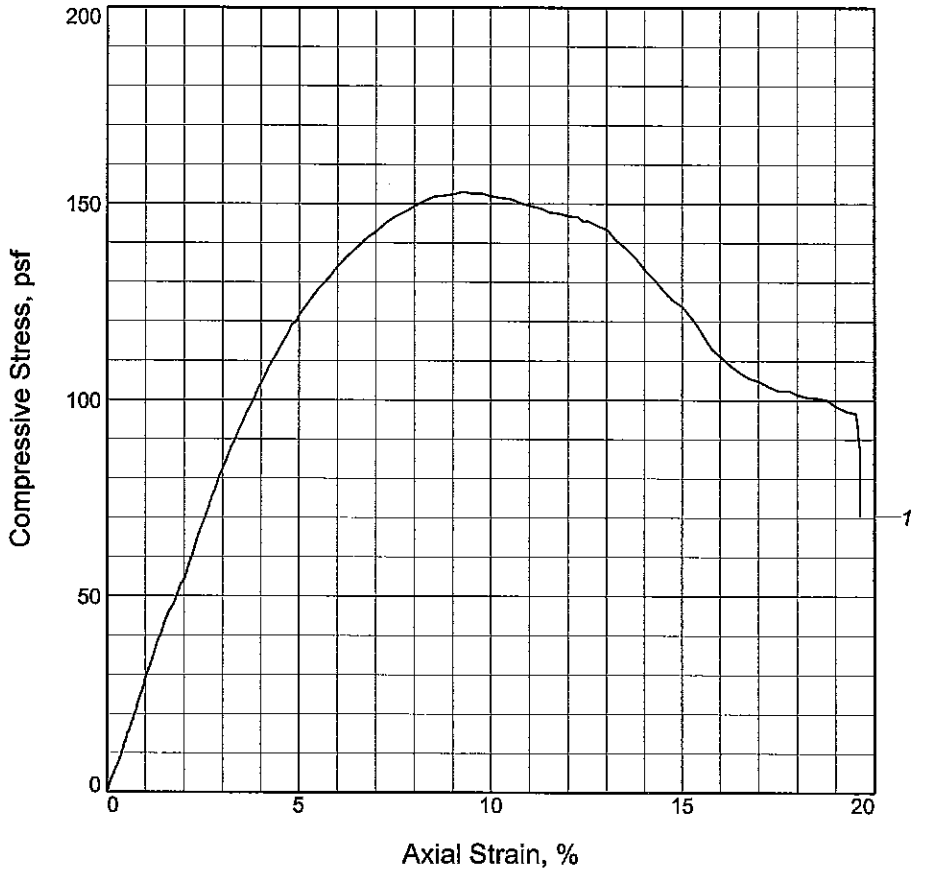
			ASTM DESIGNATION																
			D2216	D4318			D427	D2166		D2166	D2850	D422, C136 or C117					D2974	USCS	
				Atterberg Limits						Cohesion		Grain Size (% Passing)							
Boring No.	Depth (ft)	Classification	ω %	LL	PL	PI	SL	γ_{wet} pcf	γ_{dry} pcf	U psf	UU psf	Gravel	Sand	Silt	Clay	#200	Organic Content %		Confining Stress, Resistivity and Remarks
B-1	0-2	Organics with clay	607.1															(OH)	
B-1	2-4	Very Soft, Brown to Black Humus with clay	305.0	618	223	395		83.5	20.6	76.5							23.6	(OH)	Specific Gravity: 2.00 Shrink Limit- too small to test
B-1	4-6	Very Soft, CLAY with organics	230.0	202	52	150		78.6	23.8		61.3							(CH-OH)	Confining Pressure: 2.0 psi
B-1	6-8	Very Soft Gray Lean CLAY	63.8	46	26	20		118.0	72.0	145.9			0.8	57.6	41.6			(CL)	
B-1	8-10	Very Soft, Gray SILT with clay, organics and trace fine sand	54.1	43	25	18	23.4	114.6	74.3		170.1		2.1	81.6	16.3		2.4	(CL-ML)	Confining Pressure: 3.3 psi Specific Gravity: 2.71
B-1	13-15	Very Soft, Gray CLAY with silt	87.5					102.4	54.6	117.7								(CH)	
B-1	18-20	Very Soft, Gray fat CLAY	87.1	85	31	54		88.1	47.0		204.3		0.2	39.1	60.7			(CH)	Confining Pressure: 6.6 psi
B-1	23-25	Very Soft, CLAY with trace organic pockets	78.9					100.9	56.4	82.9							2.8	(CH)	
B-1	28-30	Soft, Gray fat CLAY	75.0	92	32	60		107.5	61.4		256.1		0.4	27.7	71.9			(CH)	Confining Pressure: 9.9 psi

Geotechnical Lab
11638 Sun Belt Ct. Baton Rouge, LA 70809

The results presented only relate to those samples tested

Date Samples Rec.:
Date Testing Initiated:

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	153.1			
Undrained shear strength, psf	76.5			
Failure strain, %	9.3			
Strain rate, %/min.	1.00			
Water content, %	305.0			
Wet density, pcf	83.5			
Dry density, pcf	20.6			
Saturation, %	120.6			
Void ratio	5.0566			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: VSO BR TO BK PEAT W/ CL, OH

LL = 618	**PL** = 223	**PI** = 395	**GS**= 2.00	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-4-09

Remarks:
TYPE FAILURE: VERTICAL FRACTURE

ASTM D 2166

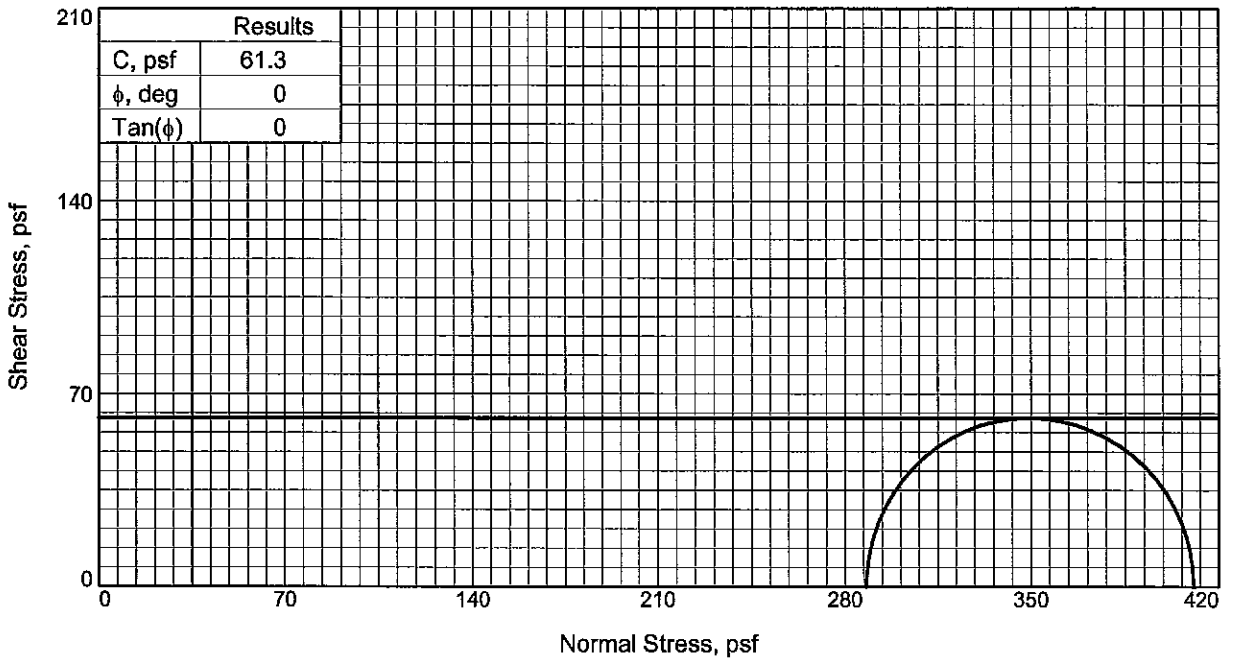
Client: URS

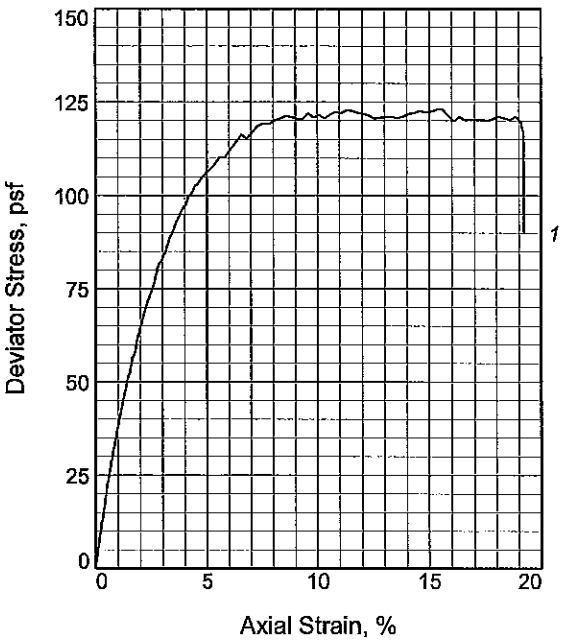
Project: BAYOU DUPONT

Source of Sample: B-1 **Depth:** 2-4
Sample Number: 2

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	230.0
	Dry Density, pcf	23.8
	Saturation, %	104.3
	Void Ratio	5.2926
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	230.0
	Dry Density, pcf	23.8
	Saturation, %	104.3
	Void Ratio	5.2926
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.000
Fail. Stress, psf		122.5
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		410.5
σ_3 Failure, psf		288.0

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO CL W/ ORGS, CH-OH

LL= 202 **PL=** 52 **PI=** 150
Assumed Specific Gravity= 2.40
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

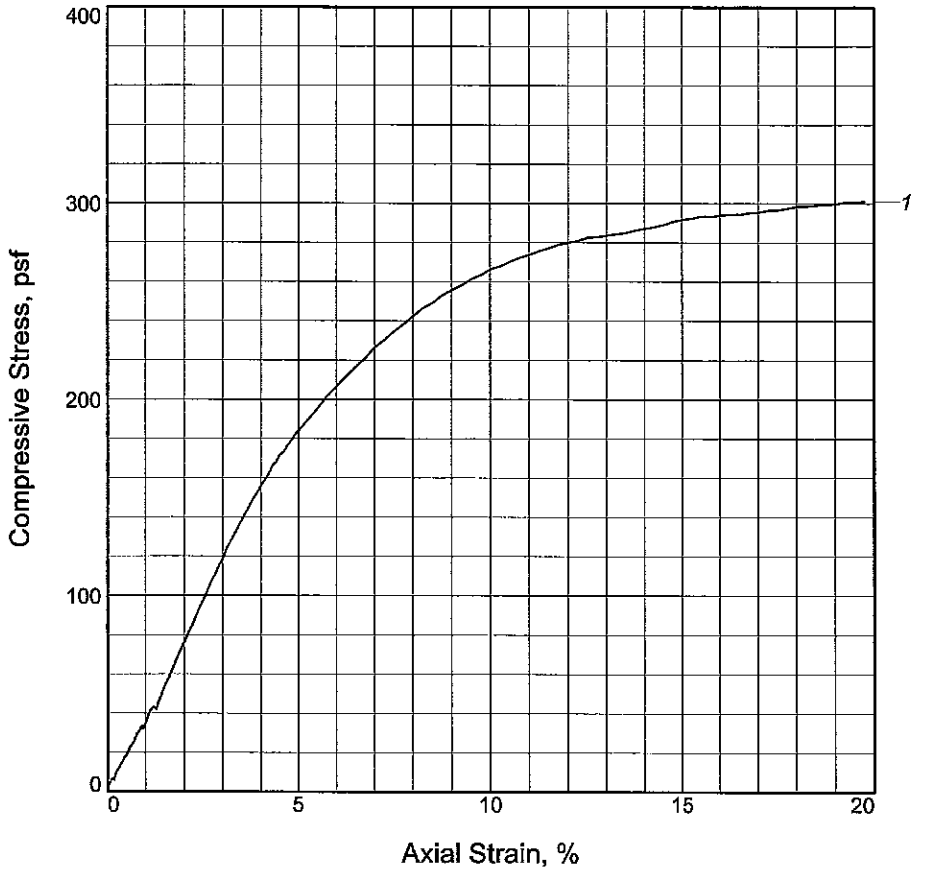
Project: BAYOU DUPONT

Source of Sample: B-1 **Depth:** 4-6
Sample Number: 3
Proj. No.: B09-012 **Date Sampled:** 3-4-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	291.8			
Undrained shear strength, psf	145.9			
Failure strain, %	15.0			
Strain rate, %/min.	1.00			
Water content, %	63.8			
Wet density, pcf	118.0			
Dry density, pcf	72.1			
Saturation, %	126.9			
Void ratio	1.3820			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: VSO G SICL, CL

LL = 46	**PL =** 26	**PI =** 20	**Assumed GS=** 2.75	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-4-09

Remarks:
TYPE FAILURE: BULGE+SMALL SHEARS

Client: URS

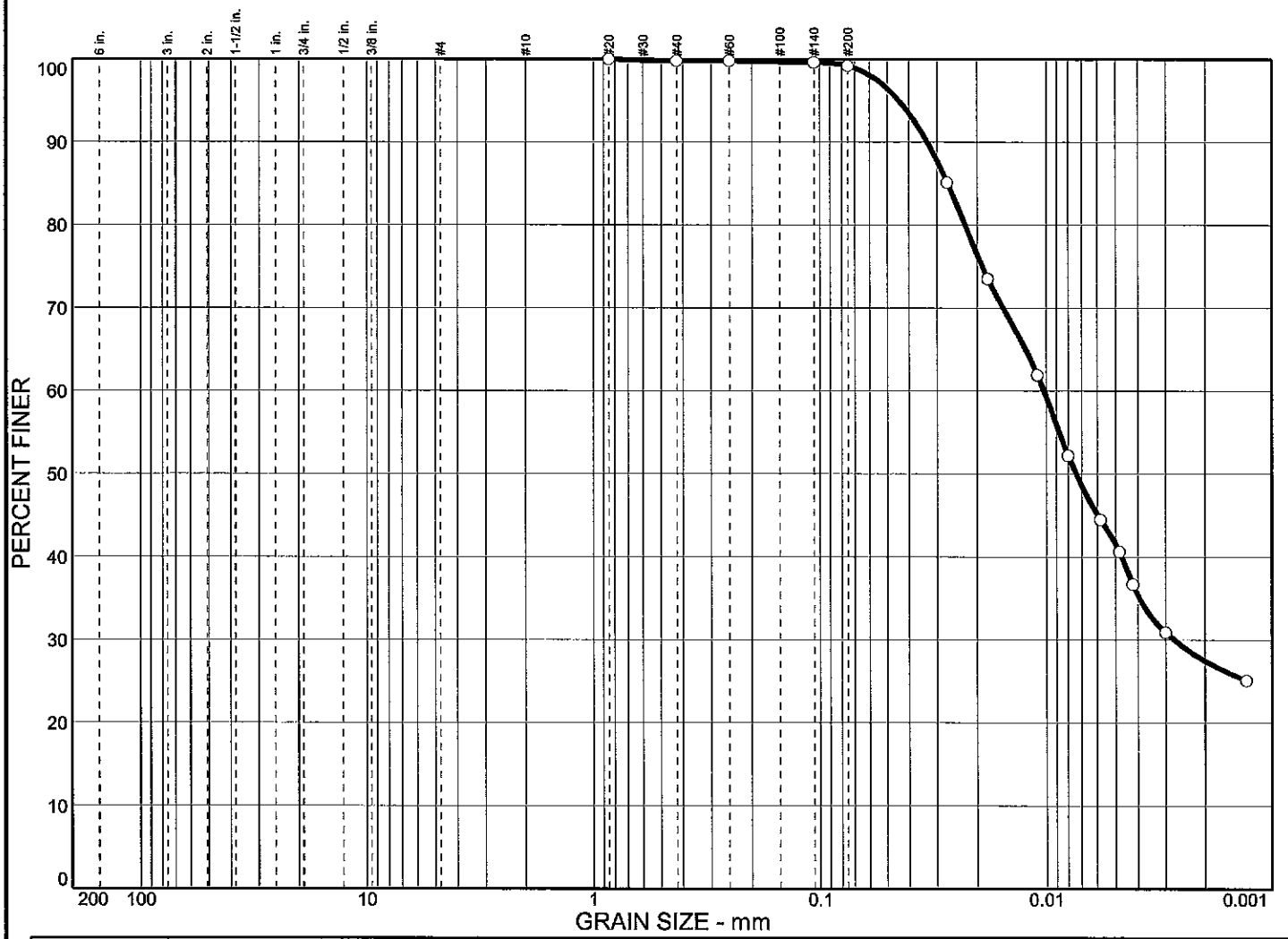
Project: BAYOU DUPONT

Source of Sample: B-1 **Depth:** 6-8
Sample Number: 4

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.8	57.6	41.6

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	46	26	0.0269	0.0102	0.0074	0.0027				

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G SICL, CL	CL	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

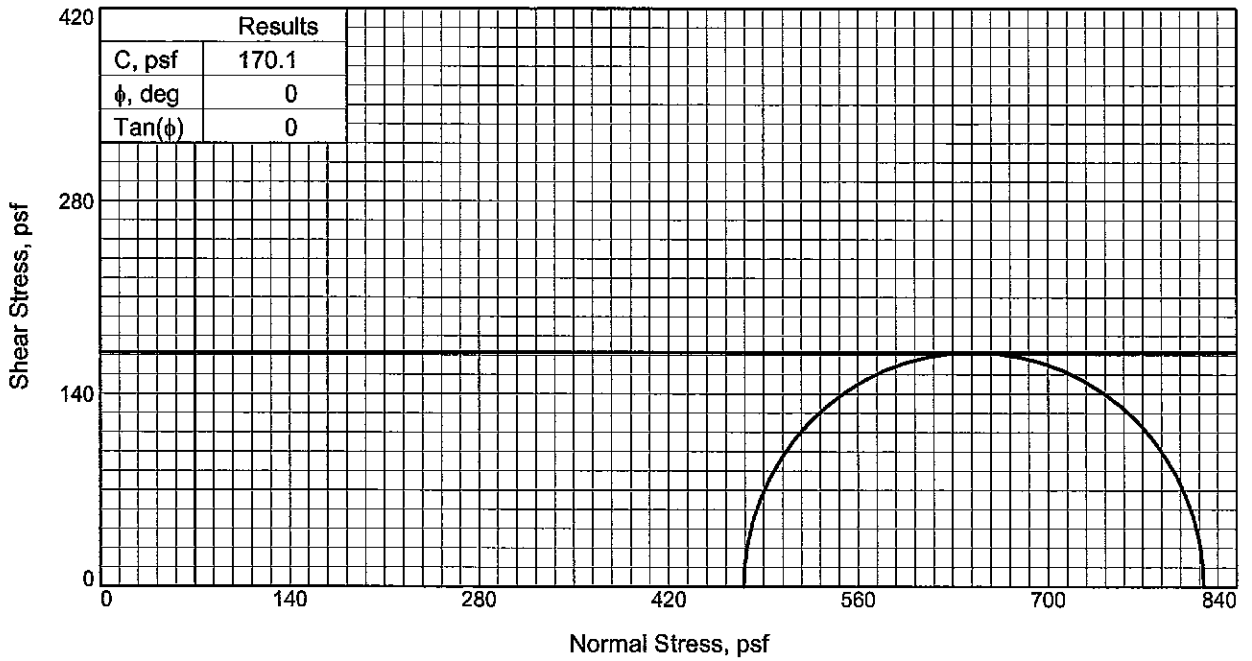
○ **Source:** B-1 **Sample No.:** 4 **Elev./Depth:** 6-8

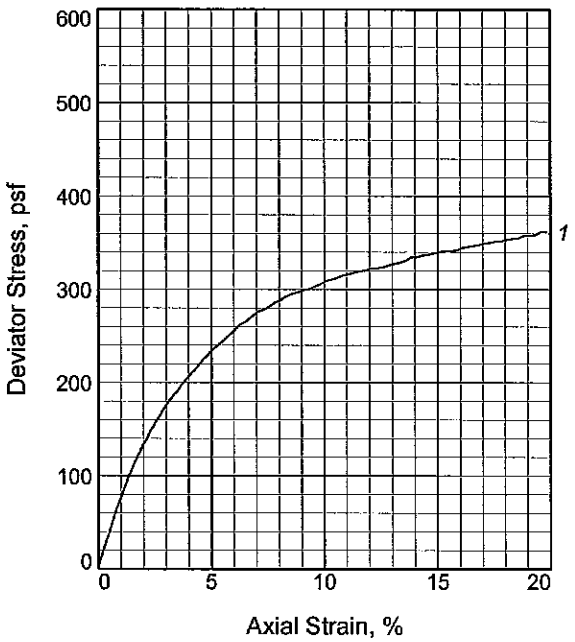
Remarks:

○ ASTM C136, D422

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	54.1
	Dry Density, pcf	74.4
	Saturation, %	115.0
	Void Ratio	1.2752
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	54.1
	Dry Density, pcf	74.4
	Saturation, %	115.0
	Void Ratio	1.2752
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		3.300
Fail. Stress, psf		340.2
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		815.4
σ_3 Failure, psf		475.2

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VLO G SI W/ CL, ORGS+TR SA, CL-ML

LL= 43 **PL=** 25 **PI=** 18

Specific Gravity= 2.71

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-1 **Depth:** 8-10

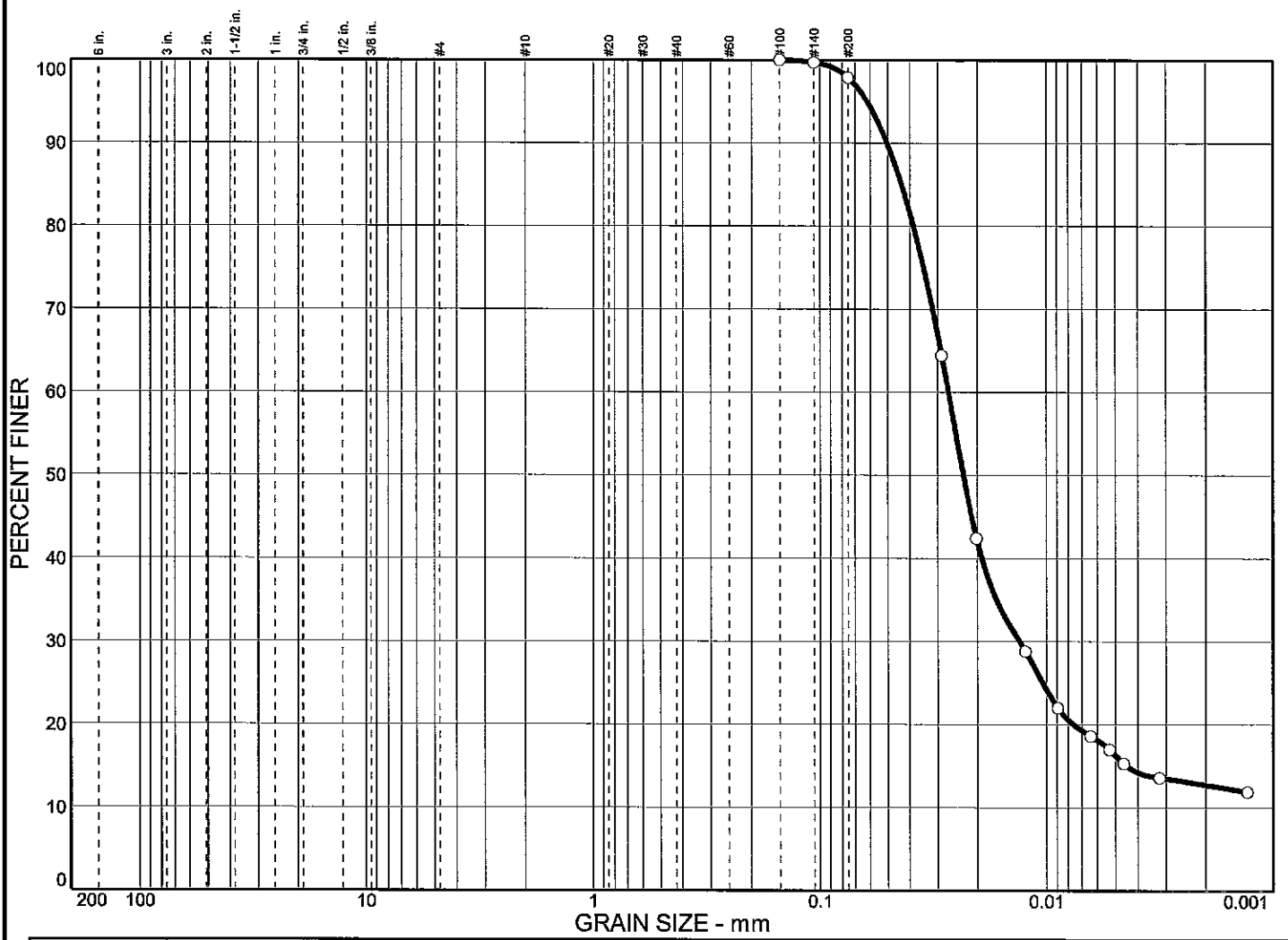
Sample Number: 5

Proj. No.: B09-012 **Date Sampled:** 3-4-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	2.1	81.6	16.3

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	43	25	0.0435	0.0269	0.0231	0.0131	0.0045			

MATERIAL DESCRIPTION	USCS	AASHTO
○ VLO G SI W/ CL, ORGS+TR SA, CL-ML	CL-ML	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-1 **Sample No.:** 5 **Elev./Depth:** 8-10

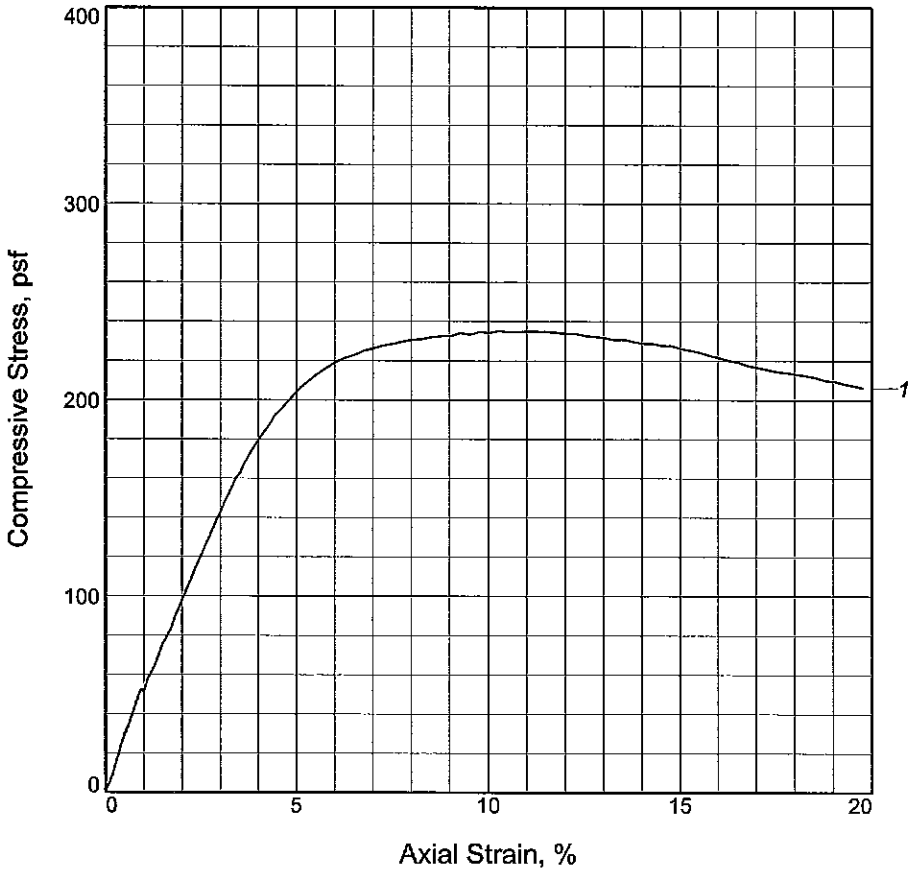
Remarks:

○ ASTM C136, D422

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	235.3			
Undrained shear strength, psf	117.7			
Failure strain, %	10.3			
Strain rate, %/min.	1.00			
Water content, %	87.5			
Wet density, pcf	102.4			
Dry density, pcf	54.6			
Saturation, %	112.2			
Void ratio	2.1447			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: VSO G CL W/ SI, CH

LL =	PL =	PI =	**Assumed GS=** 2.75	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-4-09

Remarks:
TYPE FAILURE: MULTI VERTICAL SHEAR

ASTM D 2166

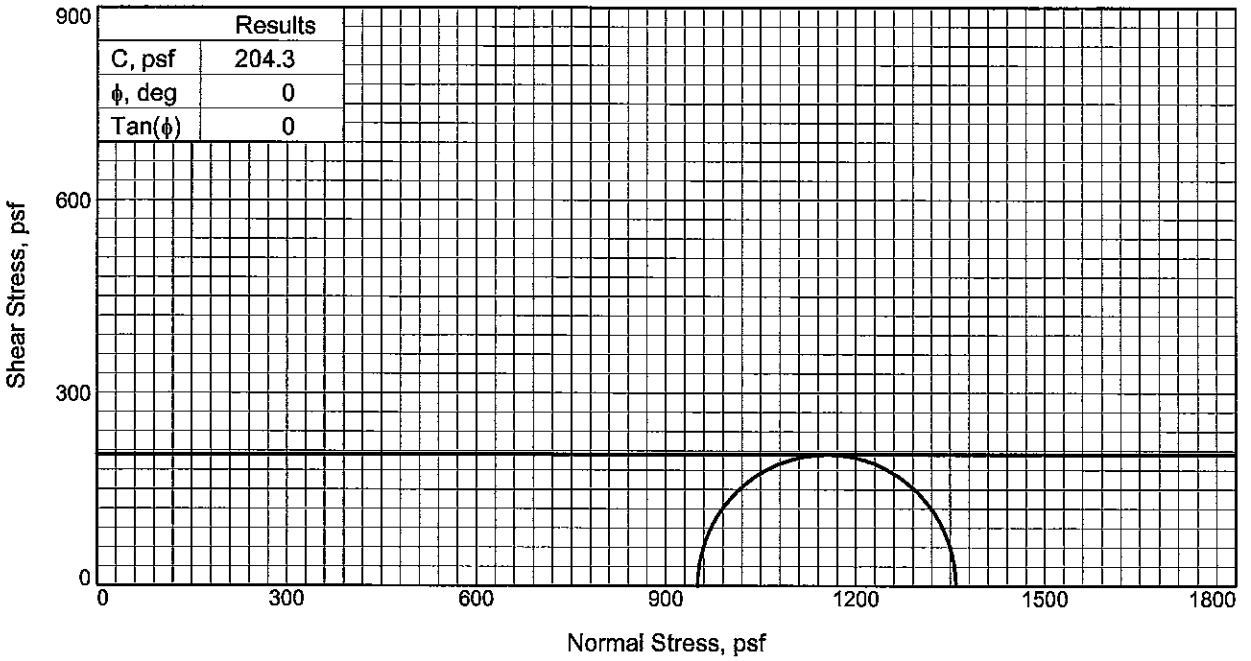
Client: URS

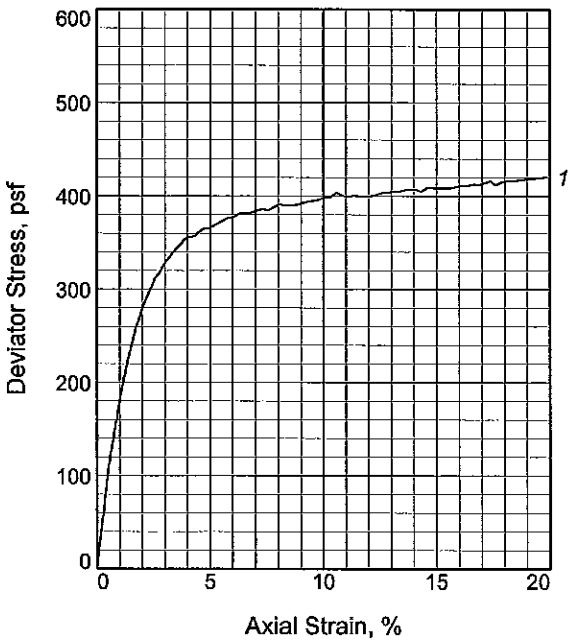
Project: BAYOU DUPONT

Source of Sample: B-1 **Depth:** 13-15
Sample Number: 6

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	87.1
	Dry Density, pcf	47.1
	Saturation, %	90.5
	Void Ratio	2.6482
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	87.1
	Dry Density, pcf	47.1
	Saturation, %	90.5
	Void Ratio	2.6482
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		6.600
Fail. Stress, psf		408.6
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1359.0
σ_3 Failure, psf		950.4

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO G CL W/ ORG PKTS+SI, CH

LL= 85 **PL=** 31 **PI=** 54
Assumed Specific Gravity= 2.75
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

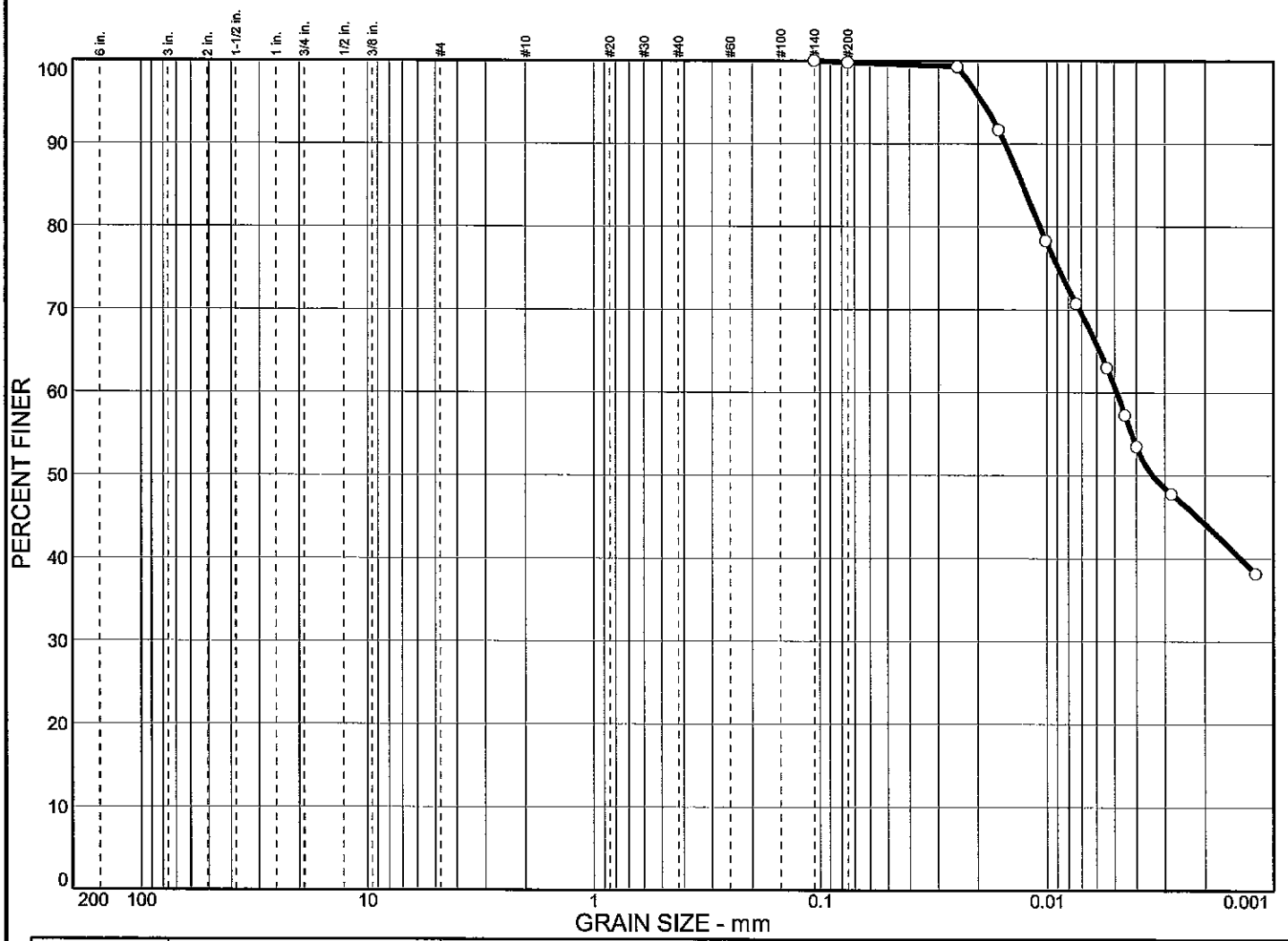
Project: BAYOU DUPONT

Source of Sample: B-1 **Depth:** 18-20
Sample Number: 7
Proj. No.: B09-012 **Date Sampled:** 3-4-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.2	39.1	60.7

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	85	31	0.0127	0.0049	0.0034					

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ ORG PKTS+SI, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-1 **Sample No.:** 7 **Elev./Depth:** 18-20

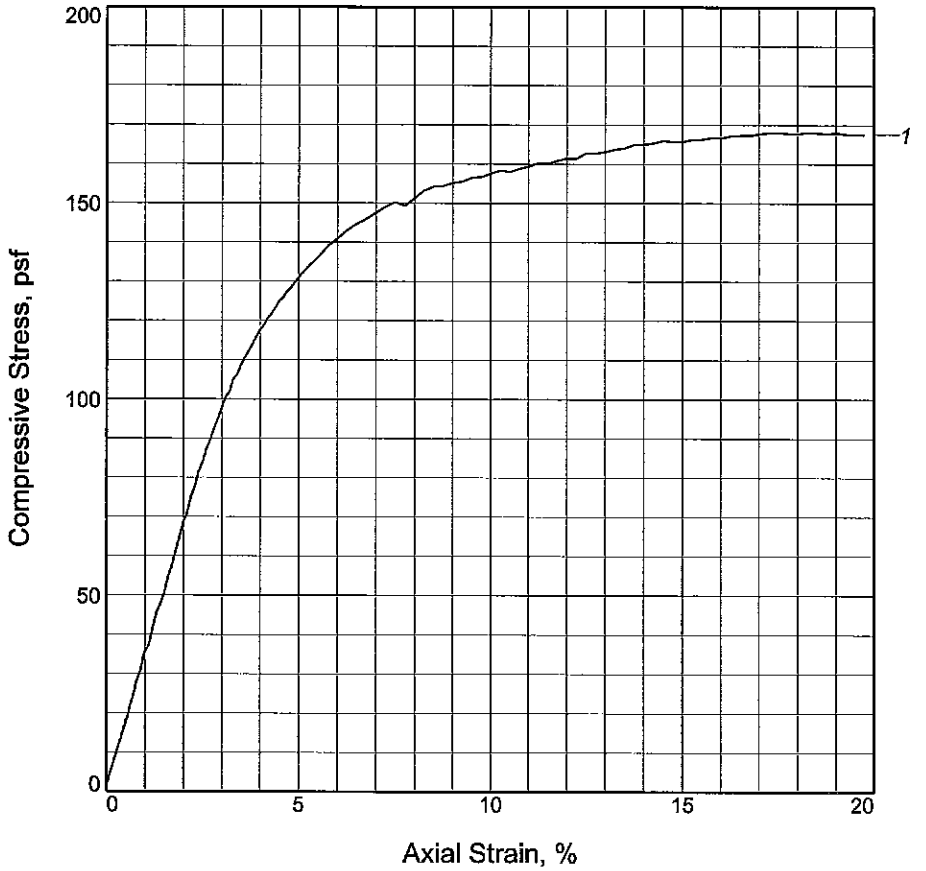
Remarks:

○ ASTM C136, D422

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	165.7			
Undrained shear strength, psf	82.9			
Failure strain, %	15.0			
Strain rate, %/min.	1.00			
Water content, %	78.9			
Wet density, pcf	100.9			
Dry density, pcf	56.4			
Saturation, %	106.1			
Void ratio	2.0442			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: VSO CL W/ TR ORG PKTS, CH

LL =	**PL =**	**PI =**	**Assumed GS=** 2.75	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-4-09

Remarks:
TYPE FAILURE: MULTI SHEAR

ASTM D 2166

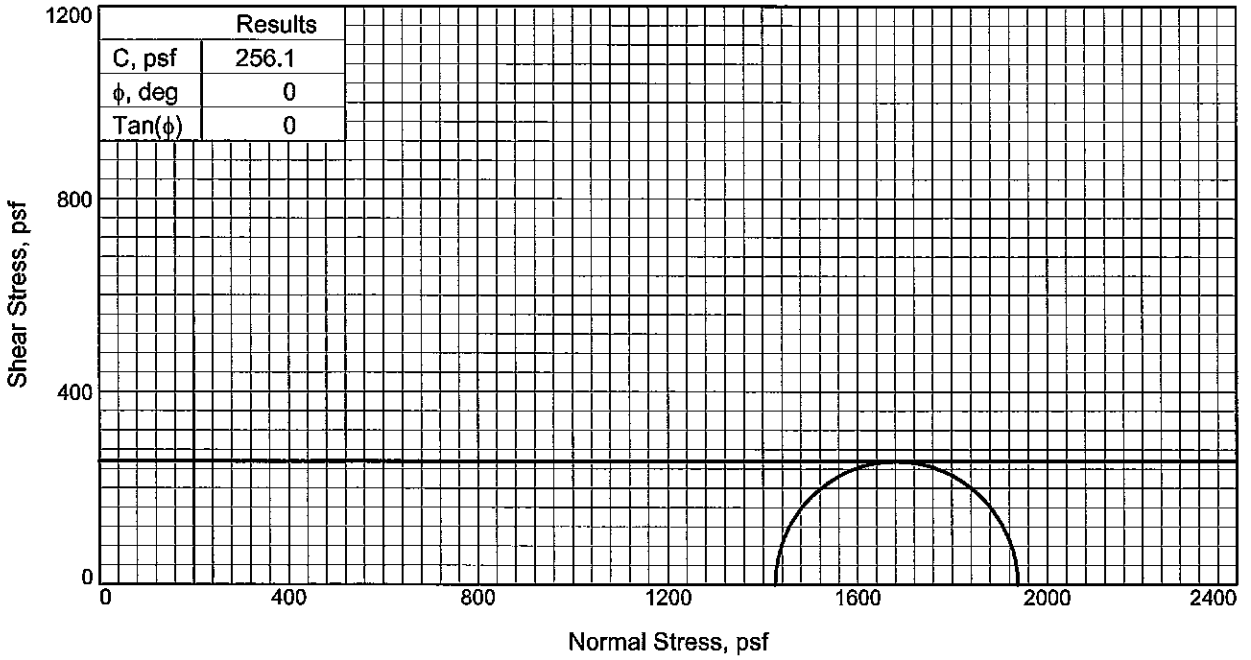
Client: URS

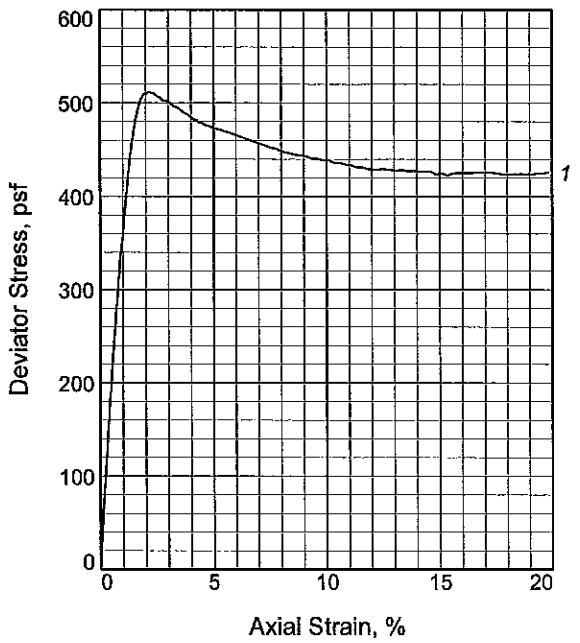
Project: BAYOU DUPONT

Source of Sample: B-1 **Depth:** 23-25
Sample Number: 8

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	75.0
	Dry Density, pcf	61.4
	Saturation, %	114.9
	Void Ratio	1.7945
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	75.0
	Dry Density, pcf	61.4
	Saturation, %	114.9
	Void Ratio	1.7945
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		9.900
Fail. Stress, psf		512.1
Strain, %		2.2
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1937.7
σ_3 Failure, psf		1425.6

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: SO G CL, CH

LL= 92 **PL=** 32 **PI=** 60

Assumed Specific Gravity= 2.75

Remarks: TYPE FAILURE: 40 DEGREE SHEAR

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-1 **Depth:** 28-30

Sample Number: 9

Proj. No.: B09-012 **Date Sampled:** 3-4-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.4	27.7	71.9

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	92	32	0.0123	0.0027	0.0016					

MATERIAL DESCRIPTION	USCS	AASHTO
○ SO G CL, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-1 **Sample No.:** 9 **Elev./Depth:** 28-30

Remarks:

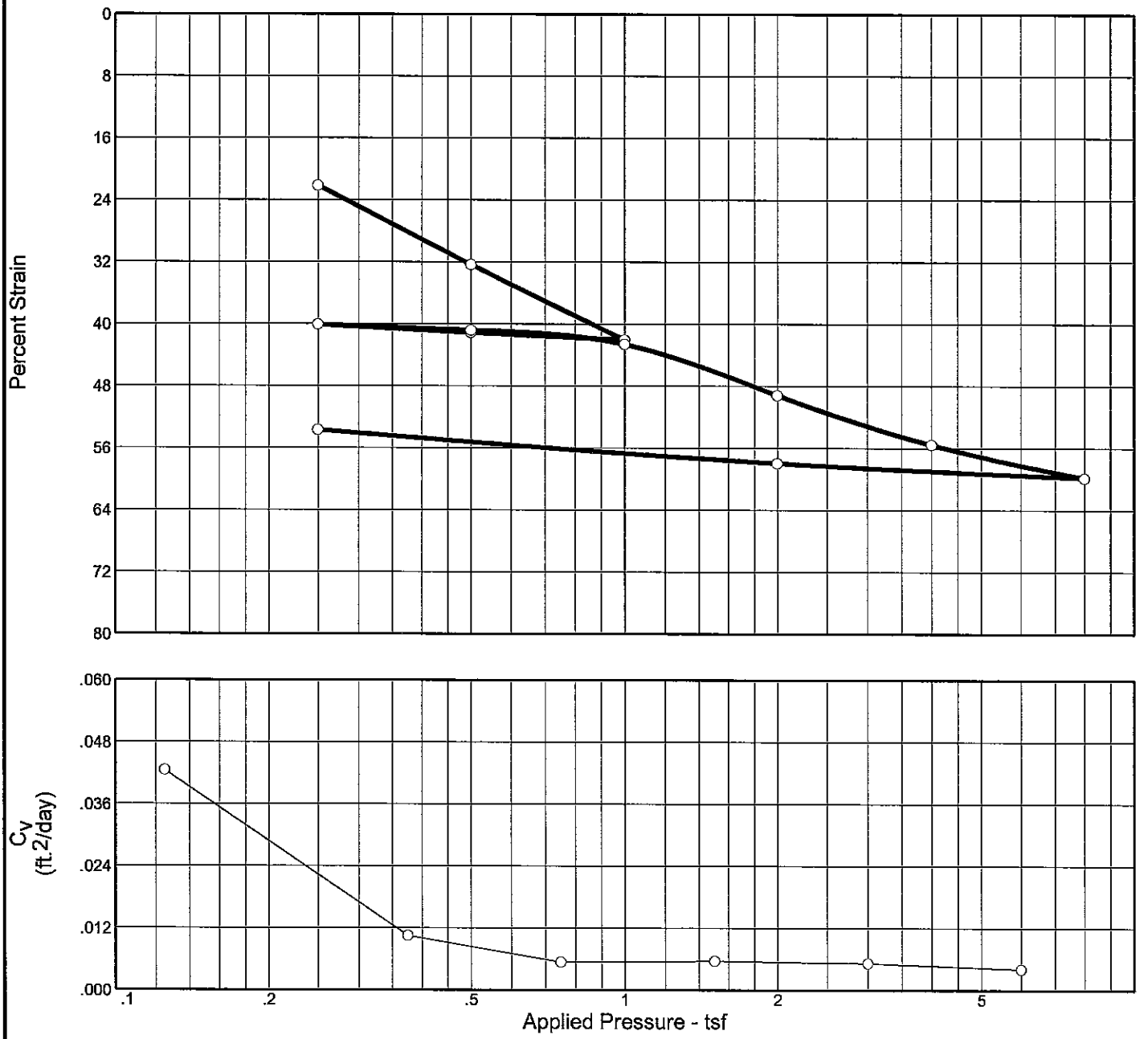
○ ASTM C136, D422

F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
100.8 %	231.7 %	22.3	202	150	2.000	(CH-OH)		4.599

MATERIAL DESCRIPTION

VSO CL W/ ORGS, CH-OH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

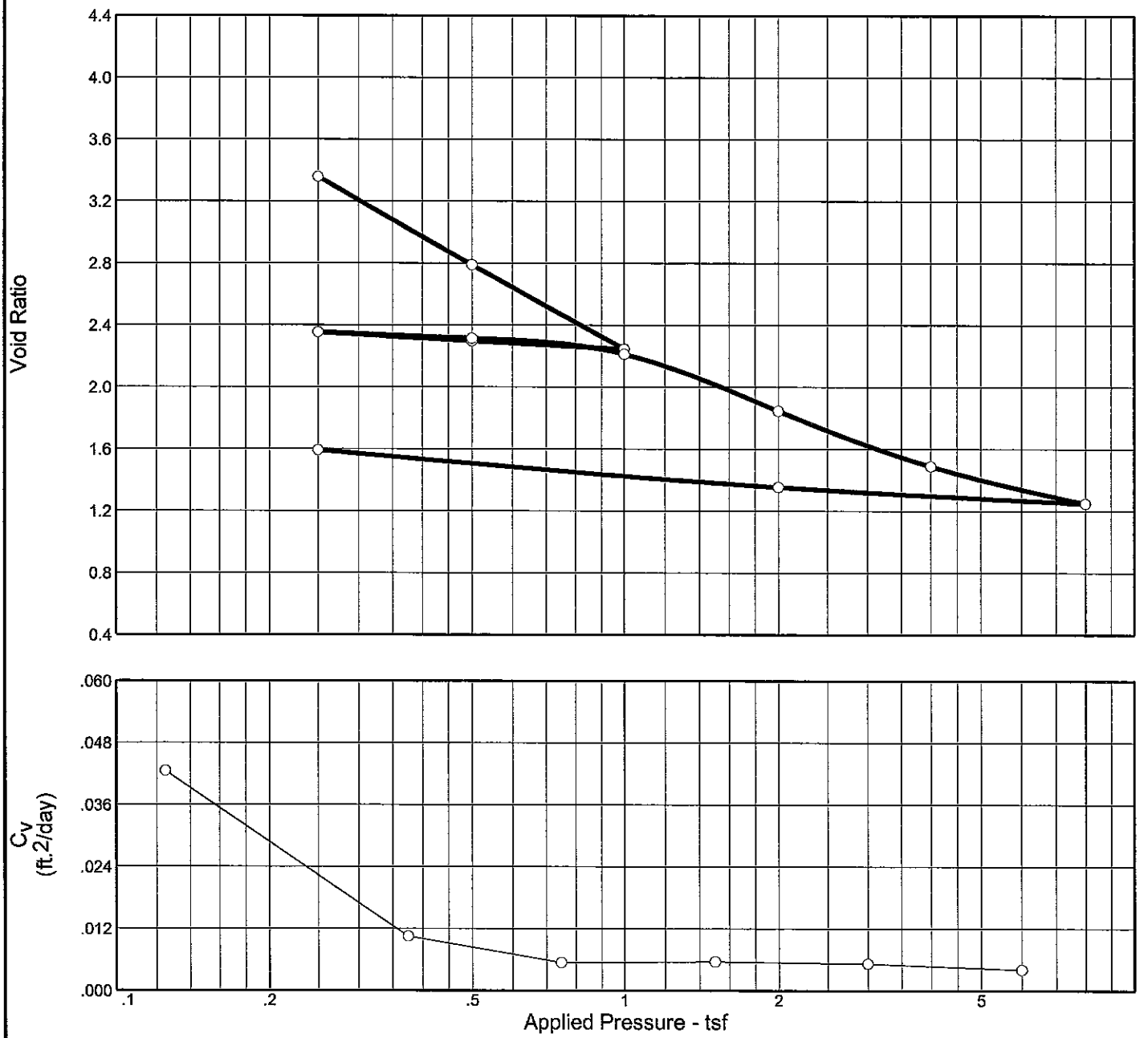
Source: B-1 **Sample No.:** 3 **Elev./Depth:** 4-6

Remarks:
ASTM D2435

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
100.8 %	231.7 %	22.3	202	150	2.000	(CH-OH)		4.599

MATERIAL DESCRIPTION

VSO CL W/ ORGS, CH-OH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-1 **Sample No.:** 3 **Elev./Depth:** 4-6

Remarks:
ASTM D2435

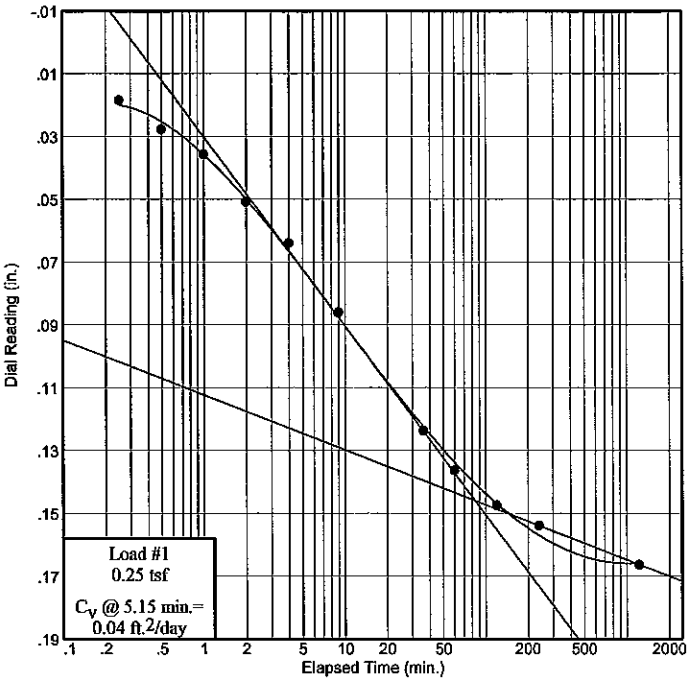
CONSOLIDATION/SWELL TEST REPORT

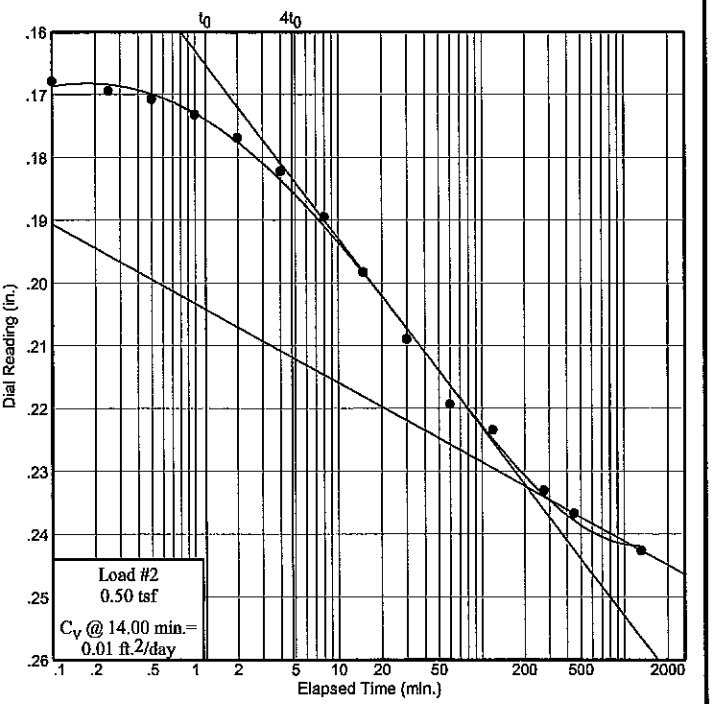
Southern Earth Sciences, Inc.

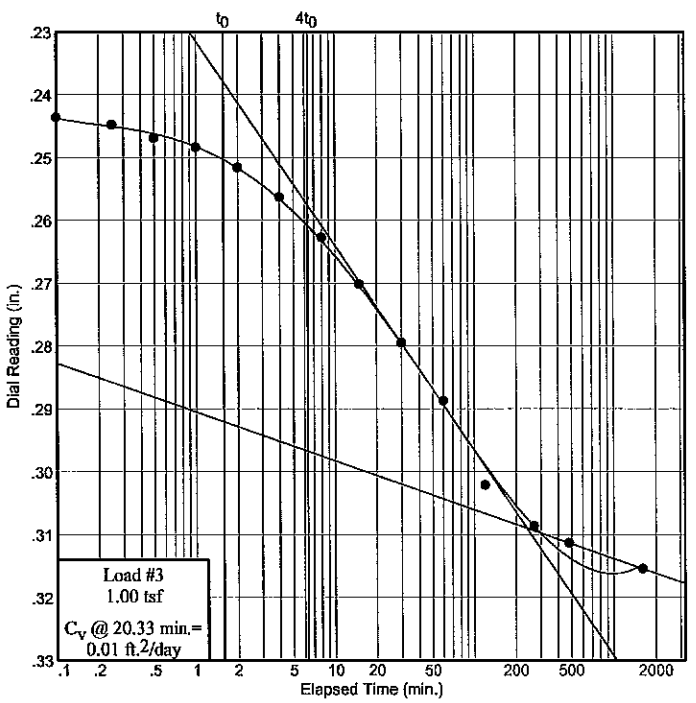
Dial Reading vs. Time

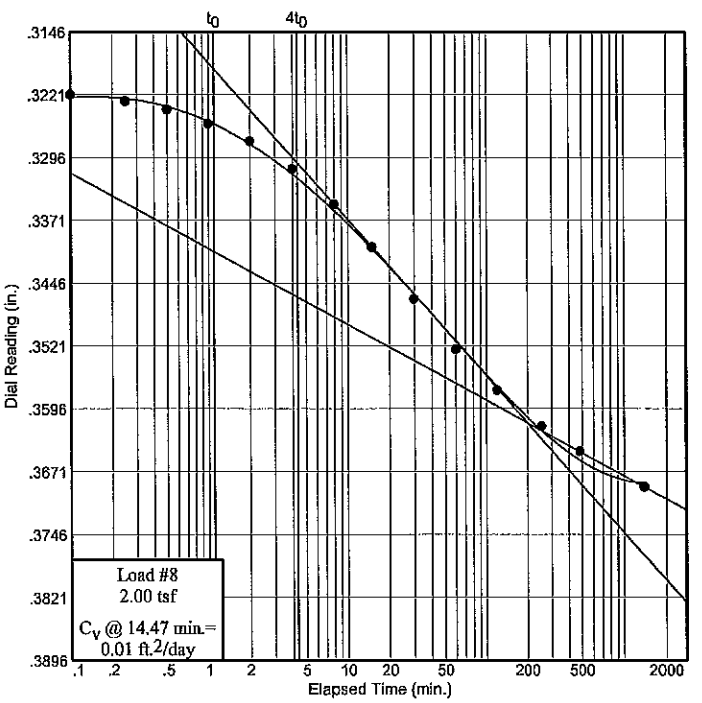
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-1 Sample No.: 3 Elev./Depth: 4-6









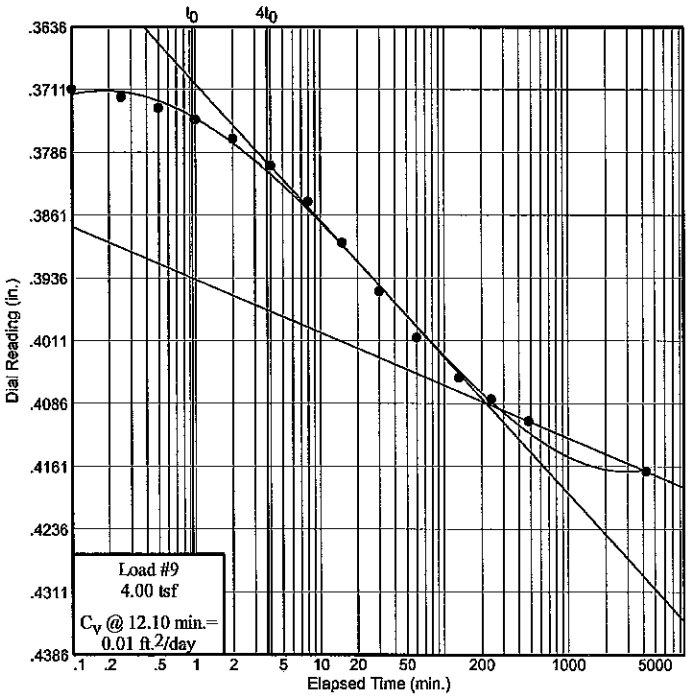
Dial Reading vs. Time

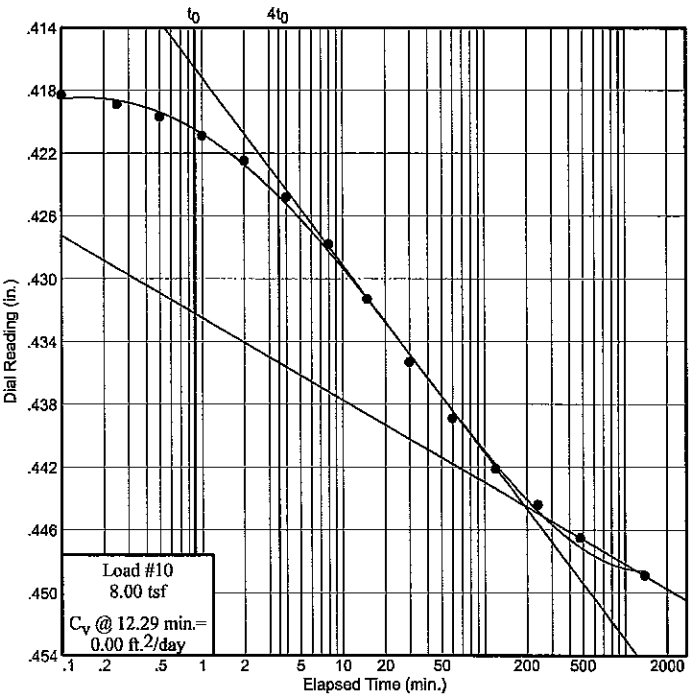
Southern Earth Sciences, Inc.

Dial Reading vs. Time

Project No.: B09-012
Project: BAYOU DUPONT

Source: B-1 Sample No.: 3 Elev./Depth: 4-6





Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-1
Sample No.: 3
Elev. or Depth: 4-6 **Sample Length(in./cm.):**
Location:
Description: VSO CL W/ ORGS, CH-OH
Liquid Limit: 202 **Plasticity Index:** 150
USCS: (CH-OH) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST		AFTER TEST	
Wet w+t =	133.27 g.	**Consolidometer #** =	1	**Wet w+t** =	37.04 g.
Dry w+t =	66.79 g.			**Dry w+t** =	21.59 g.
Tare Wt. =	38.10 g.	**Spec. Gravity** =	2.000	**Tare Wt.** =	.00 g.
Height =	.75 in.	**Height** =	.75 in.		
Diameter =	2.50 in.	**Diameter** =	2.50 in.		
Weight =	71.48 g.	**Defl. Table** =	Unit No. 1 Old 2.5in		
Moisture =	231.7 %	**Ht. Solids** =	0.1339 in.	**Moisture** =	71.6 %
Wet Den. =	74.0 pcf	**Dry Wt.** =	21.55 g.*	**Dry Wt.** =	21.59 g.
Dry Den. =	22.3 pcf	**Void Ratio** =	4.599	**Void Ratio** =	1.592
		Saturation =	100.8 %		

*** Initial dry weight used in calculations**

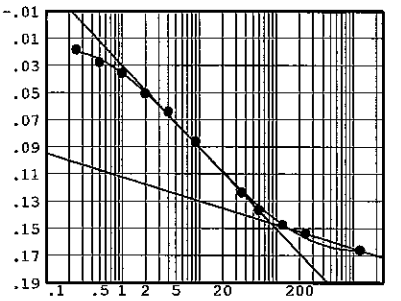
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				4.599	
0.25	0.16690	0.00060	0.04	0.023	3.358	22.2 Comprs.
0.50	0.24370	0.00110	0.01	0.022	2.788	32.3 Comprs.
1.00	0.31730	0.00190	0.01	0.015	2.245	42.1 Comprs.
0.50	0.31050	0.00210	0.03		2.297	41.1 Comprs.
0.25	0.30260	0.00180	0.00		2.354	40.1 Comprs.
0.50	0.30810	0.00200	0.05	0.002	2.314	40.8 Comprs.
1.00	0.32230	0.00250	0.05	0.008	2.212	42.6 Comprs.
2.00	0.37160	0.00270	0.01	0.021	1.845	49.2 Comprs.
4.00	0.42040	0.00370	0.01	0.017	1.488	55.6 Comprs.
8.00	0.45360	0.00470	0.00	0.016	1.248	59.9 Comprs.
2.00	0.43800	0.00320			1.353	58.0 Comprs.
0.25	0.40460	0.00180			1.592	53.7 Comprs.

C_c = 0.78 P_c = 1.02 tsf C_r = 0.24

Pressure: 0.25 tsf **TEST READINGS** **Load No. 1**

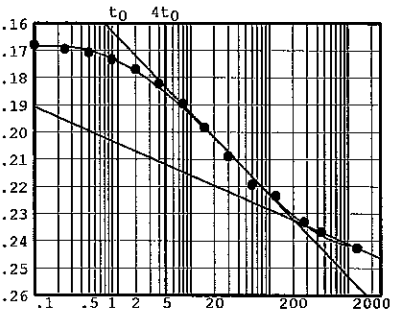
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	240.00	0.15450
2	0.25	0.01910	12	1230.00	0.16690
3	0.50	0.02830			
4	1.00	0.03630			
5	2.00	0.05140			
6	4.00	0.06460			
7	9.00	0.08660			
8	36.00	0.12430			
9	60.00	0.13690			
10	120.00	0.14800			



Void Ratio = 3.358 **Compression** = 22.2 %
D_0 = 0.00000 D_{50} = 0.07298 D_{100} = 0.14595
C_v **at 5.1 min.** = 0.04 ft.^{2}/day C_α = 0.023

Pressure: 0.50 tsf **TEST READINGS** **Load No. 2**

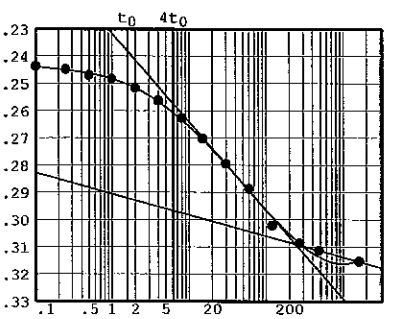
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.16690	11	60.00	0.22040
2	0.10	0.16900	12	120.00	0.22450
3	0.25	0.17050	13	275.00	0.23410
4	0.50	0.17180	14	450.00	0.23780
5	1.00	0.17430	15	1320.00	0.24370
6	2.00	0.17800			
7	4.00	0.18330			
8	8.00	0.19060			
9	15.00	0.19940			
10	30.00	0.21000			



Void Ratio = 2.788 **Compression** = 32.3 %
D_0 = 0.16259 D_{50} = 0.19753 D_{100} = 0.23247
C_v **at 14.0 min.** = 0.01 ft.^{2}/day C_α = 0.022

Pressure: 1.00 tsf **TEST READINGS** **Load No. 3**

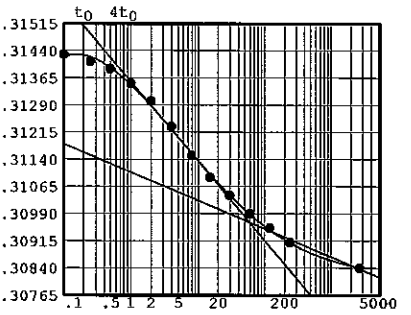
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.24370	11	60.00	0.29060
2	0.10	0.24550	12	120.00	0.30400
3	0.25	0.24670	13	270.00	0.31050
4	0.50	0.24880	14	480.00	0.31320
5	1.00	0.25030	15	1620.00	0.31730
6	2.00	0.25350			
7	4.00	0.25820			
8	8.00	0.26460			
9	15.00	0.27210			
10	30.00	0.28140			



Void Ratio = 2.245 **Compression** = 42.1 %
D_0 = 0.23982 D_{50} = 0.27439 D_{100} = 0.30895
C_v **at 20.3 min.** = 0.01 ft.^{2}/day C_α = 0.015

Pressure: 0.50 tsf **TEST READINGS** **Load No. 4**

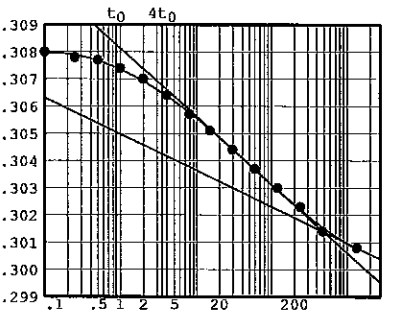
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.31730	11	60.00	0.31200
2	0.10	0.31640	12	120.00	0.31160
3	0.25	0.31620	13	240.00	0.31120
4	0.50	0.31600	14	2680.00	0.31050
5	1.00	0.31560			
6	2.00	0.31510			
7	4.00	0.31440			
8	8.00	0.31360			
9	15.00	0.31300			
10	30.00	0.31250			



Void Ratio = 2.297 **Compression** = 41.1 %
D_0 = 0.31491 D_{50} = 0.31229 D_{100} = 0.30966
C_v **at 3.8 min.** = 0.03 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 5**

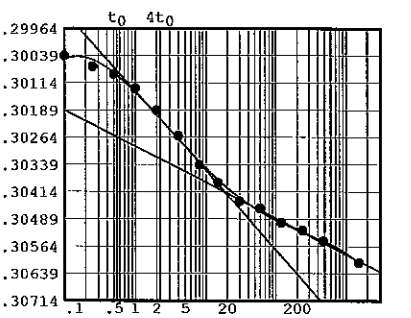
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.31050	11	60.00	0.30550
2	0.10	0.30980	12	120.00	0.30480
3	0.25	0.30960	13	240.00	0.30410
4	0.50	0.30950	14	480.00	0.30320
5	1.00	0.30920	15	1350.00	0.30260
6	2.00	0.30880			
7	4.00	0.30820			
8	8.00	0.30750			
9	15.00	0.30690			
10	30.00	0.30620			



Void Ratio = 2.354 **Compression** = 40.1 %
D_0 = 0.30836 D_{50} = 0.30487 D_{100} = 0.30139
C_v **at 19.6 min.** = 0.00 ft.^{2}/day

Pressure: 0.50 tsf **TEST READINGS** **Load No. 6**

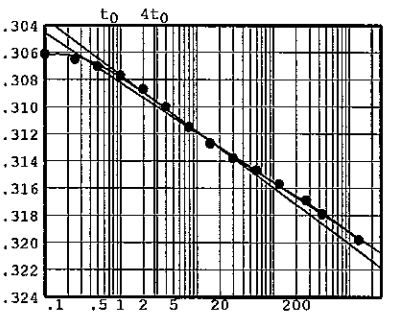
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.30260	11	60.00	0.30660
2	0.10	0.30240	12	120.00	0.30700
3	0.25	0.30270	13	240.00	0.30720
4	0.50	0.30290	14	480.00	0.30750
5	1.00	0.30330	15	1530.00	0.30810
6	2.00	0.30390			
7	4.00	0.30460			
8	8.00	0.30540			
9	15.00	0.30590			
10	30.00	0.30640			



Void Ratio = 2.314 **Compression** = 40.8 %
D_0 = 0.29974 D_{50} = 0.30194 D_{100} = 0.30415
C_v **at 1.8 min.** = 0.05 ft.^{2}/day C_α = 0.002

Pressure: 1.00 tsf **TEST READINGS** **Load No. 7**

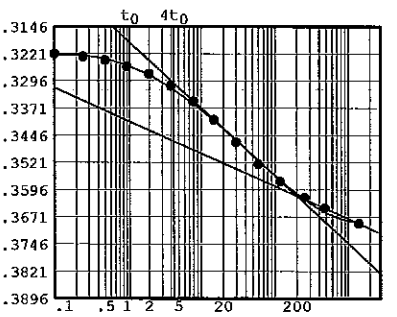
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.30810	11	60.00	0.31720
2	0.10	0.30860	12	120.00	0.31820
3	0.25	0.30900	13	270.00	0.31940
4	0.50	0.30950	14	440.00	0.32040
5	1.00	0.31020	15	1320.00	0.32230
6	2.00	0.31120			
7	4.00	0.31250			
8	8.00	0.31400			
9	15.00	0.31520			
10	30.00	0.31630			



Void Ratio = 2.212 **Compression** = 42.6 %
D_0 = 0.30509 D_{50} = 0.30876 D_{100} = 0.31243
C_v **at 1.8 min.** = 0.05 ft.^{2}/day C_α = 0.008

Pressure: 2.00 tsf **TEST READINGS** **Load No. 8**

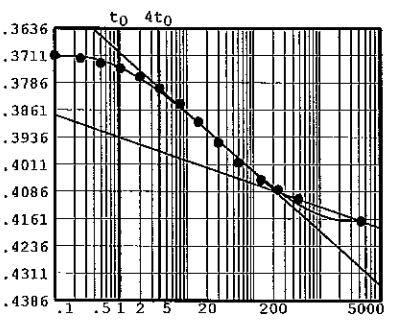
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.32230	11	60.00	0.35520
2	0.10	0.32480	12	120.00	0.36010
3	0.25	0.32560	13	254.00	0.36440
4	0.50	0.32660	14	480.00	0.36740
5	1.00	0.32830	15	1400.00	0.37160
6	2.00	0.33040			
7	4.00	0.33370			
8	8.00	0.33790			
9	15.00	0.34300			
10	30.00	0.34920			



Void Ratio = 1.845 **Compression** = 49.2 %
D_0 = 0.31912 D_{50} = 0.34019 D_{100} = 0.36126
C_v **at 14.5 min.** = 0.01 ft.^{2}/day C_α = 0.021

Pressure: 4.00 tsf **TEST READINGS** **Load No. 9**

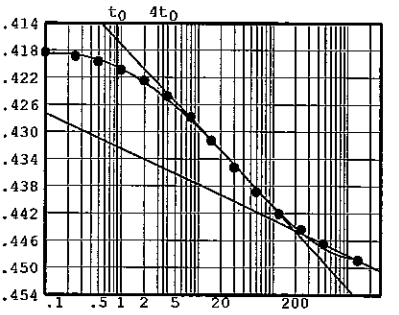
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.37160	11	60.00	0.40440
2	0.10	0.37480	12	132.00	0.40920
3	0.25	0.37570	13	240.00	0.41180
4	0.50	0.37700	14	480.00	0.41440
5	1.00	0.37840	15	4290.00	0.42040
6	2.00	0.38070			
7	4.00	0.38390			
8	8.00	0.38820			
9	15.00	0.39310			
10	30.00	0.39890			



Void Ratio = 1.488 **Compression** = 55.6 %
D_0 = 0.36779 D_{50} = 0.38817 D_{100} = 0.40854
C_v **at 12.1 min.** = 0.01 ft.^{2}/day C_α = 0.017

Pressure: 8.00 tsf **TEST READINGS** **Load No. 10**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.42040	11	60.00	0.44360
2	0.10	0.42300	12	120.00	0.44680
3	0.25	0.42360	13	240.00	0.44910
4	0.50	0.42440	14	480.00	0.45120
5	1.00	0.42560	15	1380.00	0.45360
6	2.00	0.42720			
7	4.00	0.42950			
8	8.00	0.43250			
9	15.00	0.43600			
10	30.00	0.44000			



Void Ratio = 1.248 **Compression =** 59.9 %
D_0 = 0.41617 D_{50} = 0.43029 D_{100} = 0.44441
C_v **at 12.3 min. =** 0.00 ft.^{2}/day C_α = 0.016

Southern Earth Sciences, Inc.

Laboratory Test Results

Project: **Bayou DuPont** | **Technical Responsibility:** | **Quality Assurance Officer**

Client: URS

7389 Florida Blvd., Suite 300, Baton Rouge, LA 70806 | Project No.: **B09-012** | PM: S. Aviles | Date of Issue: 3/12/2009

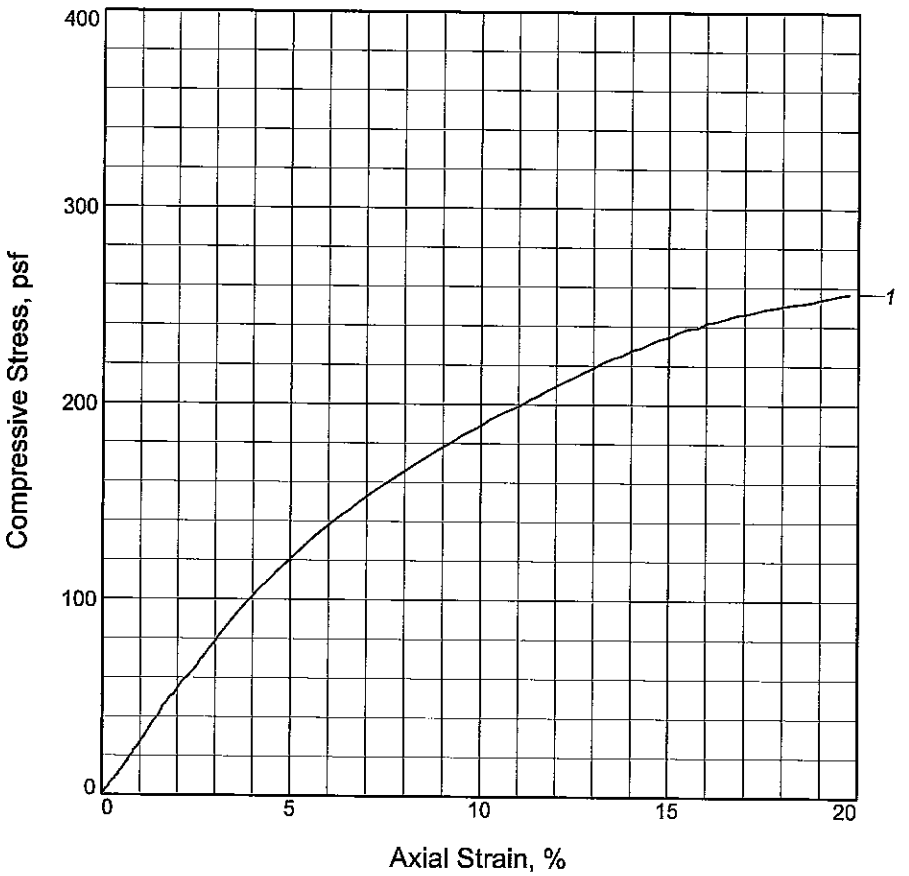
			ASTM DESIGNATION																
			D2216	D4318			D427	D2166		D2166	D2850	D422, C136 or C117					D2974	USCS	
				Atterberg Limits						Cohesion		Grain Size (% Passing)							
Boring No.	Depth (ft)	Classification	ω %	LL	PL	PI	SL	γ_{wet} pcf	γ_{dry} pcf	U psf	UU psf	Gravel	Sand	Silt	Clay	#200	Organic Content %		Confining Stress, Resistivity and Remarks
B-2	0-2	Organics with clay	915.0															(OH)	
B-2	2-4	Very Soft, Brown Organics with clay and peat	475.0	400	146	254	13.6	70.3	12.2	117.3							32.0	(OH)	Specific Gravity: 1.98
B-2	4-6	Very Soft, Gray and Black CLAY with organics and trace silt	203.7					83.2	27.4		124.5		2.5	18.5	79.0			(CH)	Confining Pressure: 2.0 psi
B-2	6-8	Very Soft, Gray CLAY with organic pockets	94.9	123	33	90		97.6	50.0	56.0								(CH)	
B-2	8-10	Very Soft, Gray CLAY with organics	88.2	97	27	70	21.3	98.7	52.4		70.8		3.5	50.7	45.8		5.2	(CH)	Confining Pressure: 3.3 psi Specific Gravity 2.786
B-2	13-15	Very Soft, Gray CLAY with organic pockets	141.4	144	40	104		88.0	36.4	67.5								(CH)	
B-2	18-20	Very Soft, Gray CLAY with silt	50.0	58	22	36		113.0	75.3		136.5		3.3	74.0	22.7			(CH)	Confining Pressure: 6.6 psi
B-2	23-25	Very Soft, Gray CLAY with silt pockets and organics	98.0					100.0	50.5	110.8							5.0	(CH)	
B-2	28-30	Very Soft, Gray CLAY with silt and organics	41.5	78	25	53		98.2	69.4		116.7		1.1	53.2	45.7			(CH)	Confining Pressure: 9.9 psi

Geotechnical Lab
11638 Sun Belt Ct. Baton Rouge, LA 70809

The results presented only relate to those samples tested

Date Samples Rec.:
Date Testing Initiated:

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	234.7			
Undrained shear strength, psf	117.3			
Failure strain, %	15.0			
Strain rate, %/min.	1.00			
Water content, %	475.0			
Wet density, pcf	70.3			
Dry density, pcf	12.2			
Saturation, %	101.4			
Void ratio	11.2481			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: VSO B ORG W/ CL+PEAT, PT

LL = 400	**PL** = 146	**PI** = 254	**Assumed GS=** 2.40	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-5-09
Remarks:
TYPE FAILURE: BULGE

ASTM D 2166

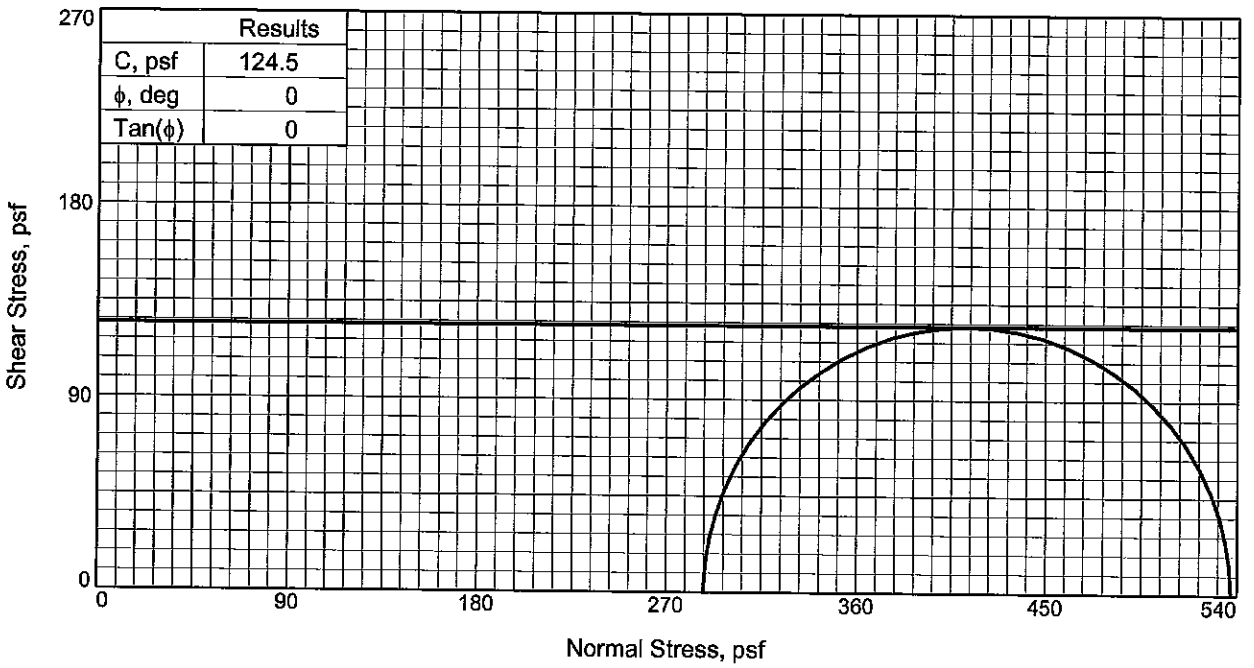
Client: URS

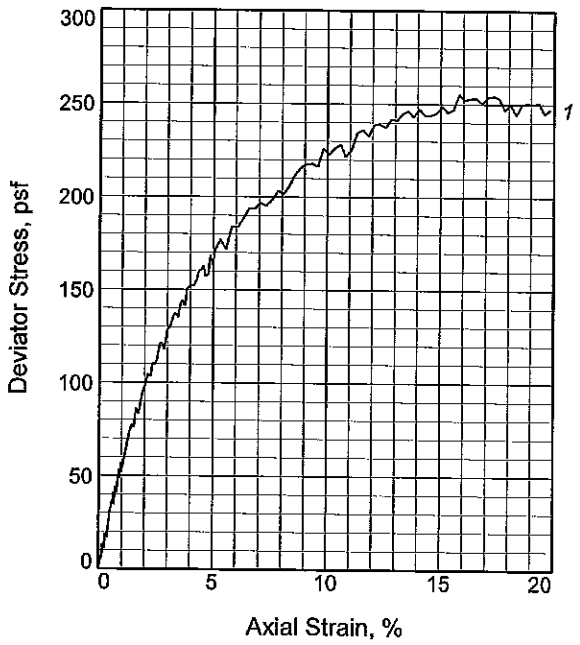
Project: BAYOU DUPONT

Source of Sample: B-2 **Depth:** 2-4
Sample Number: 2

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	203.7
	Dry Density, pcf	27.4
	Saturation, %	114.8
	Void Ratio	3.5149
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	203.7
	Dry Density, pcf	27.4
	Saturation, %	114.8
	Void Ratio	3.5149
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.000
Fail. Stress, psf		249.1
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		537.1
σ_3 Failure, psf		288.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO GR+BL CL W/ ORGS+TR SI, CH

Assumed Specific Gravity= 1.98

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-2 **Depth:** 4-6

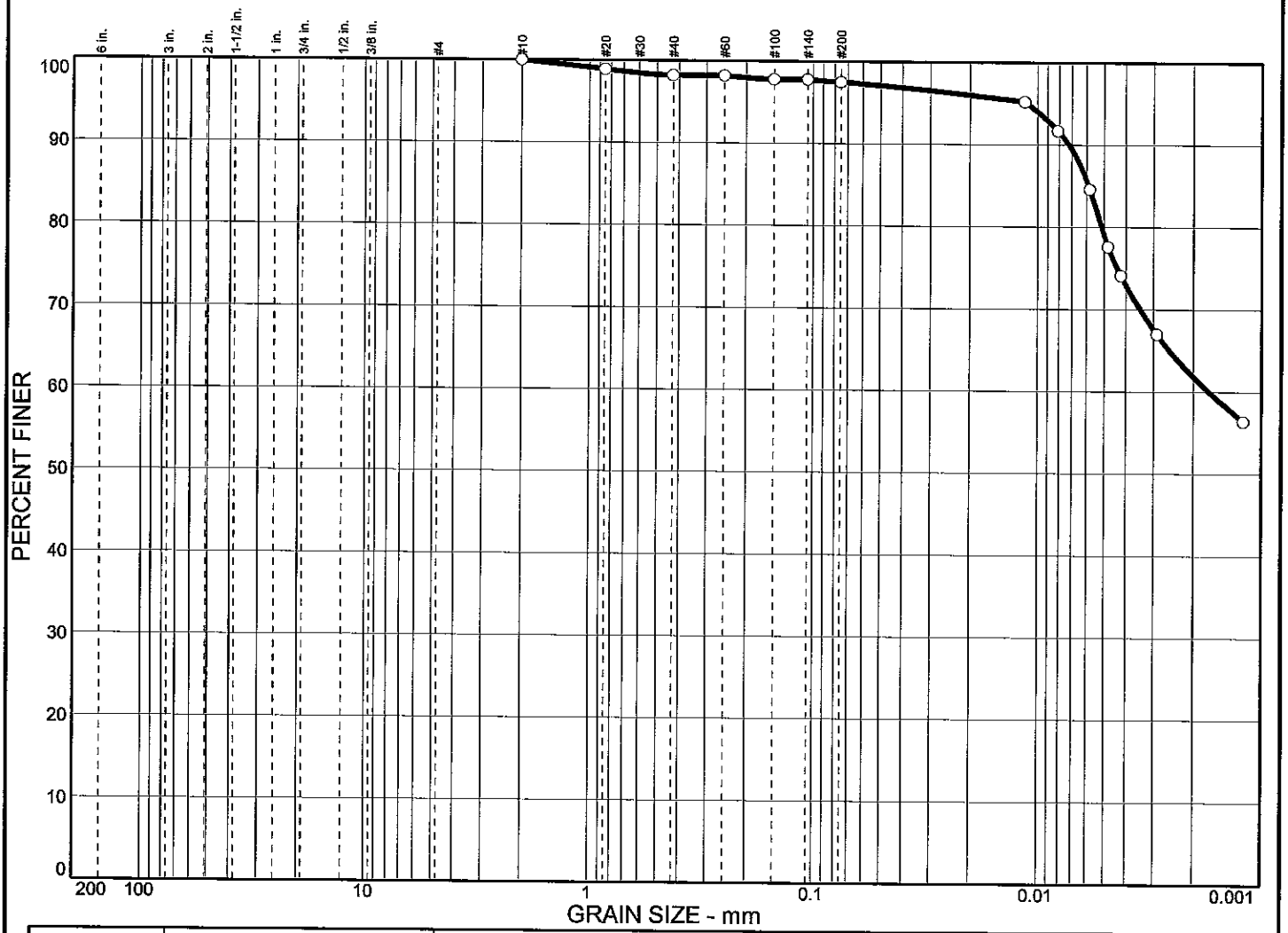
Sample Number: 3

Proj. No.: B09-012 **Date Sampled:** 3-5-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	2.5	18.5	79.0

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○			0.0059	0.0017						

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO GR+BL CL W/ ORGS+TR SI, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-2 **Sample No.:** 3 **Elev./Depth:** 4-6

Remarks:

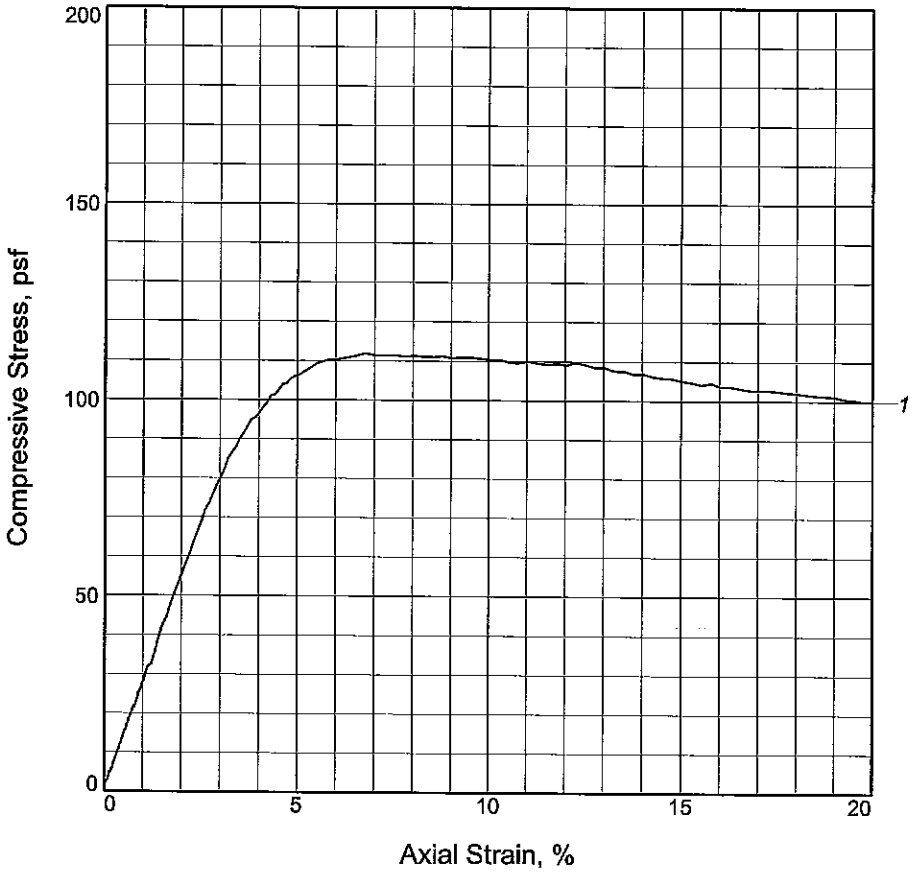
○ ASTM C136, D422

F.M.=0.02

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	111.9			
Undrained shear strength, psf	56.0			
Failure strain, %	6.8			
Strain rate, %/min.	1.00			
Water content, %	94.9			
Wet density, pcf	97.6			
Dry density, pcf	50.1			
Saturation, %	106.6			
Void ratio	2.4921			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: VSO G CL W/ ORG PKTS, CH

LL =	PL =	PI =	Assumed GS= 2.80	Type: UNDISTURBED

Project No.: B09-012
Date Sampled: 3-5-09

Remarks:
TYPE FAILURE: BULGE+PARTIAL 40 DEGREE SHEAR

ASTM D 2166

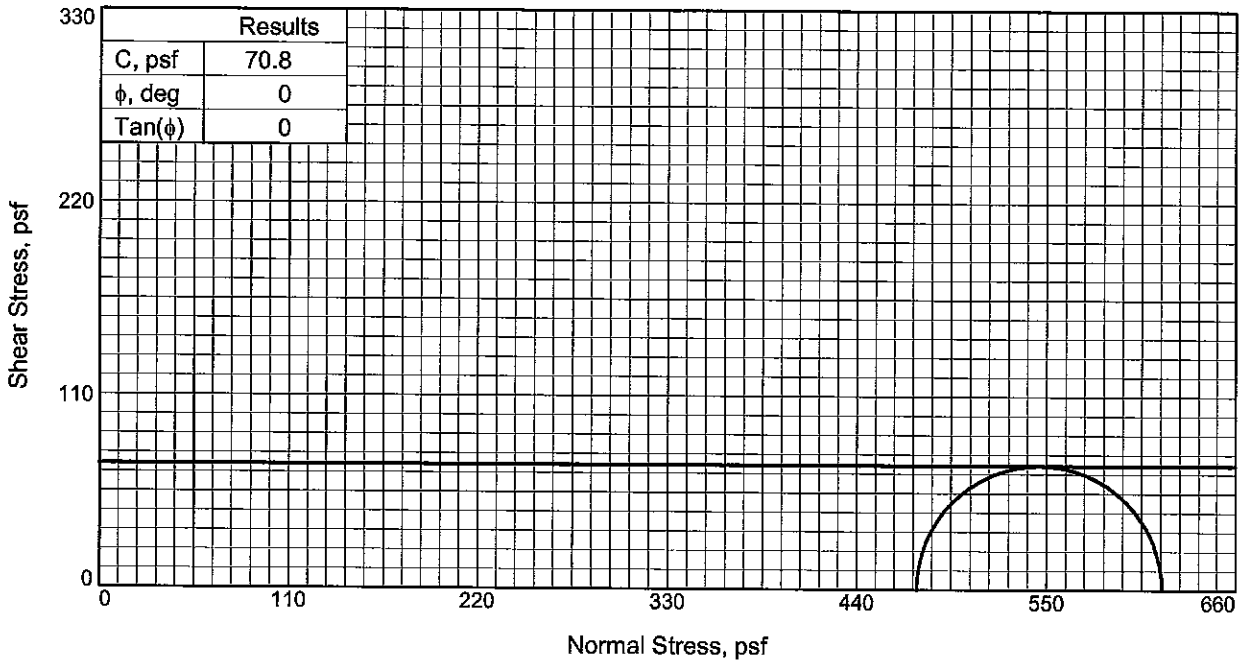
Client: URS

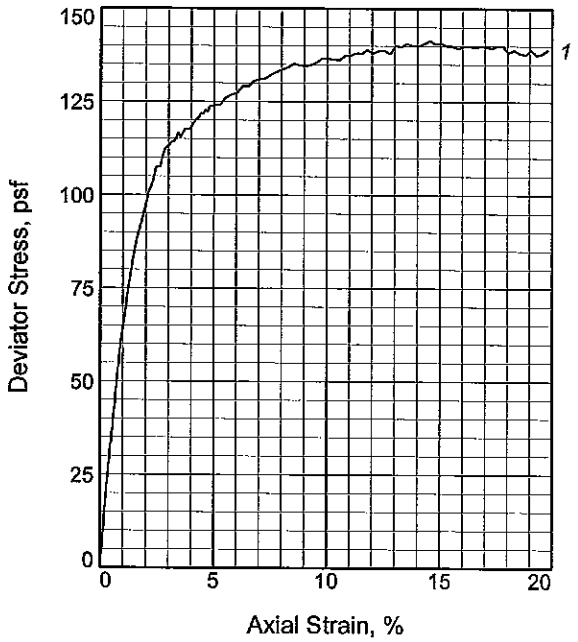
Project: BAYOU DUPONT

Source of Sample: B-2 **Depth:** 6-8
Sample Number: 4

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	88.2
	Dry Density, pcf	52.4
	Saturation, %	106.1
	Void Ratio	2.3169
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	88.2
	Dry Density, pcf	52.4
	Saturation, %	106.1
	Void Ratio	2.3169
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		3.300
Fail. Stress, psf		141.5
Strain, %		14.6
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		616.7
σ_3 Failure, psf		475.2

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO G CL W/ ORGS, CH

LL= 97 **PL=** 27 **PI=** 70
Specific Gravity= 2.786
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-2 **Depth:** 8-10
Sample Number: 5
Proj. No.: B09-012 **Date Sampled:** 3-5-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	3.5	50.7	45.8

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	97	27	0.0547	0.0128	0.0065					

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ ORGS, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-2 **Sample No.:** 5 **Elev./Depth:** 8-10

Remarks:

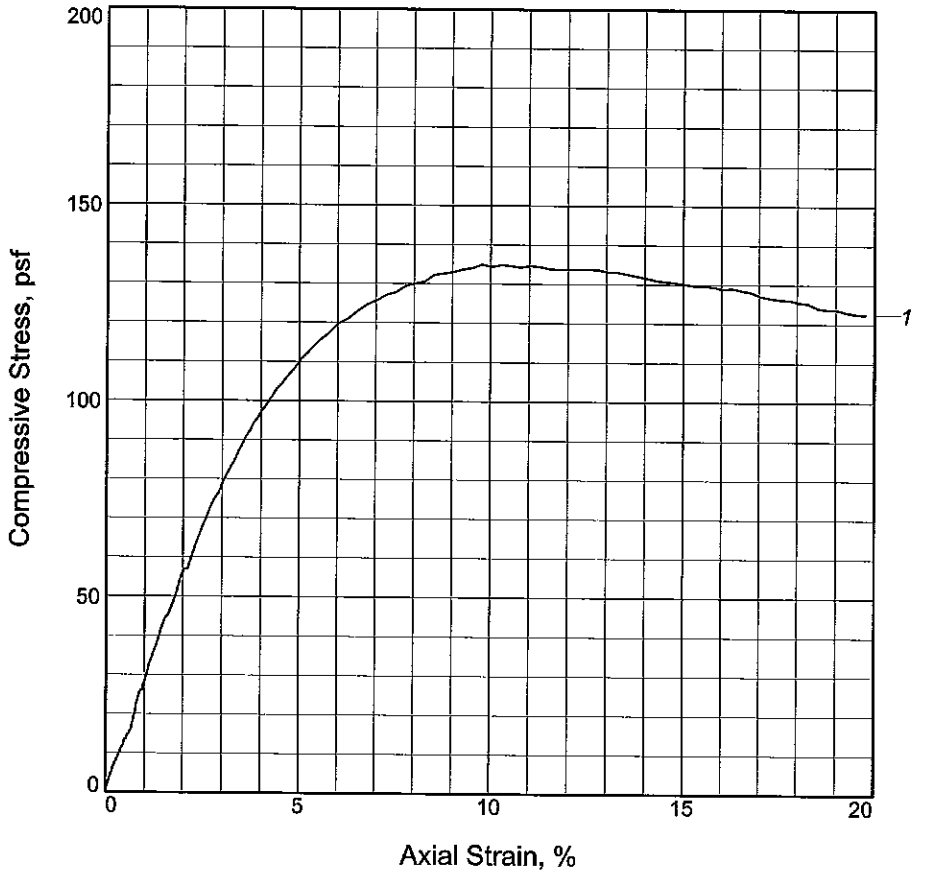
○ ASTM C136, D422

F.M.=0.02

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	135.0			
Undrained shear strength, psf	67.5			
Failure strain, %	9.8			
Strain rate, %/min.	1.00			
Water content, %	141.4			
Wet density, pcf	88.0			
Dry density, pcf	36.4			
Saturation, %	104.2			
Void ratio	3.7973			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: VSO G CL W/ ORG PKTS, CH

LL = 144	**PL** = 40	**PI** = 104	**Assumed GS=** 2.80	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-5-09

Remarks:
TYPE FAILURE: BULGE+MULTI SHEAR

ASTM D 2166

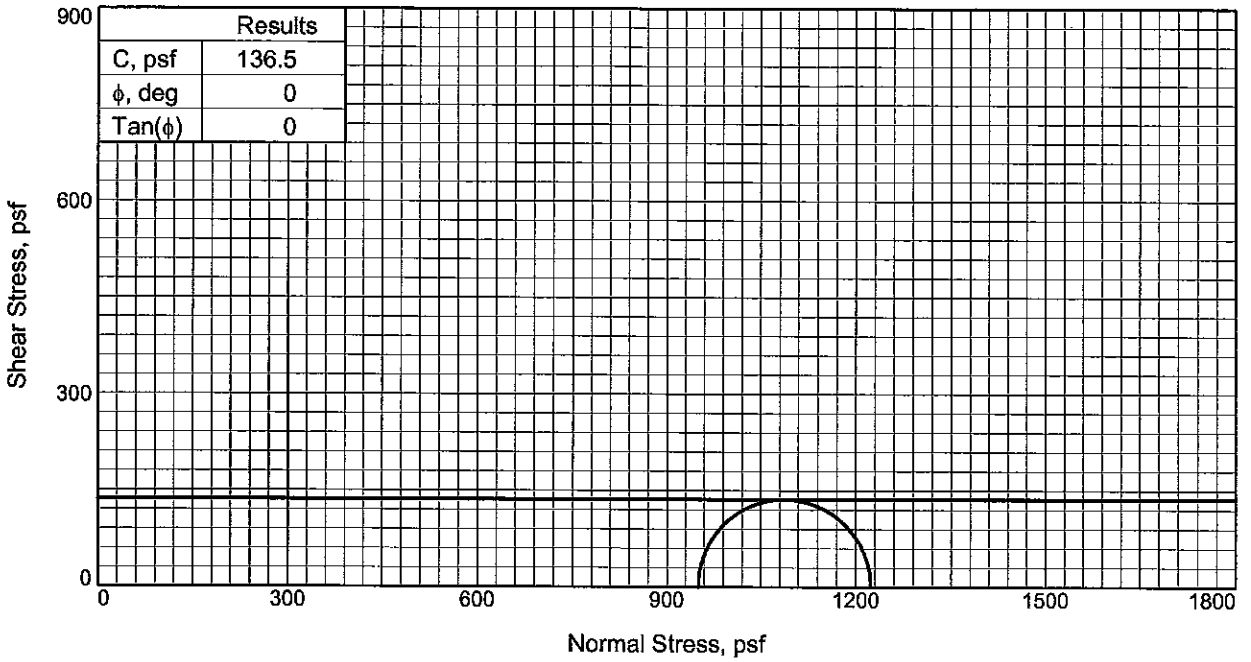
Client: URS

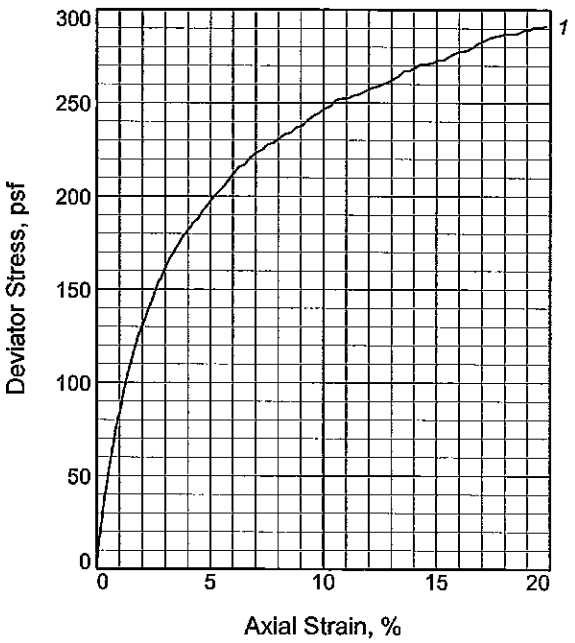
Project: BAYOU DUPONT

Source of Sample: B-2 **Depth:** 13-15
Sample Number: 6

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	50.0
	Dry Density, pcf	75.3
	Saturation, %	107.5
	Void Ratio	1.2789
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	50.0
	Dry Density, pcf	75.3
	Saturation, %	107.5
	Void Ratio	1.2789
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		6.600
Fail. Stress, psf		273.0
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1223.4
σ_3 Failure, psf		950.4

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: LO G CL W/ SI, CH

LL= 58 **PL=** 22 **PI=** 36
Assumed Specific Gravity= 2.75
Remarks: TYPE FAILURE: BULGE+SHEAR

ASTM D 2850

Client: URS

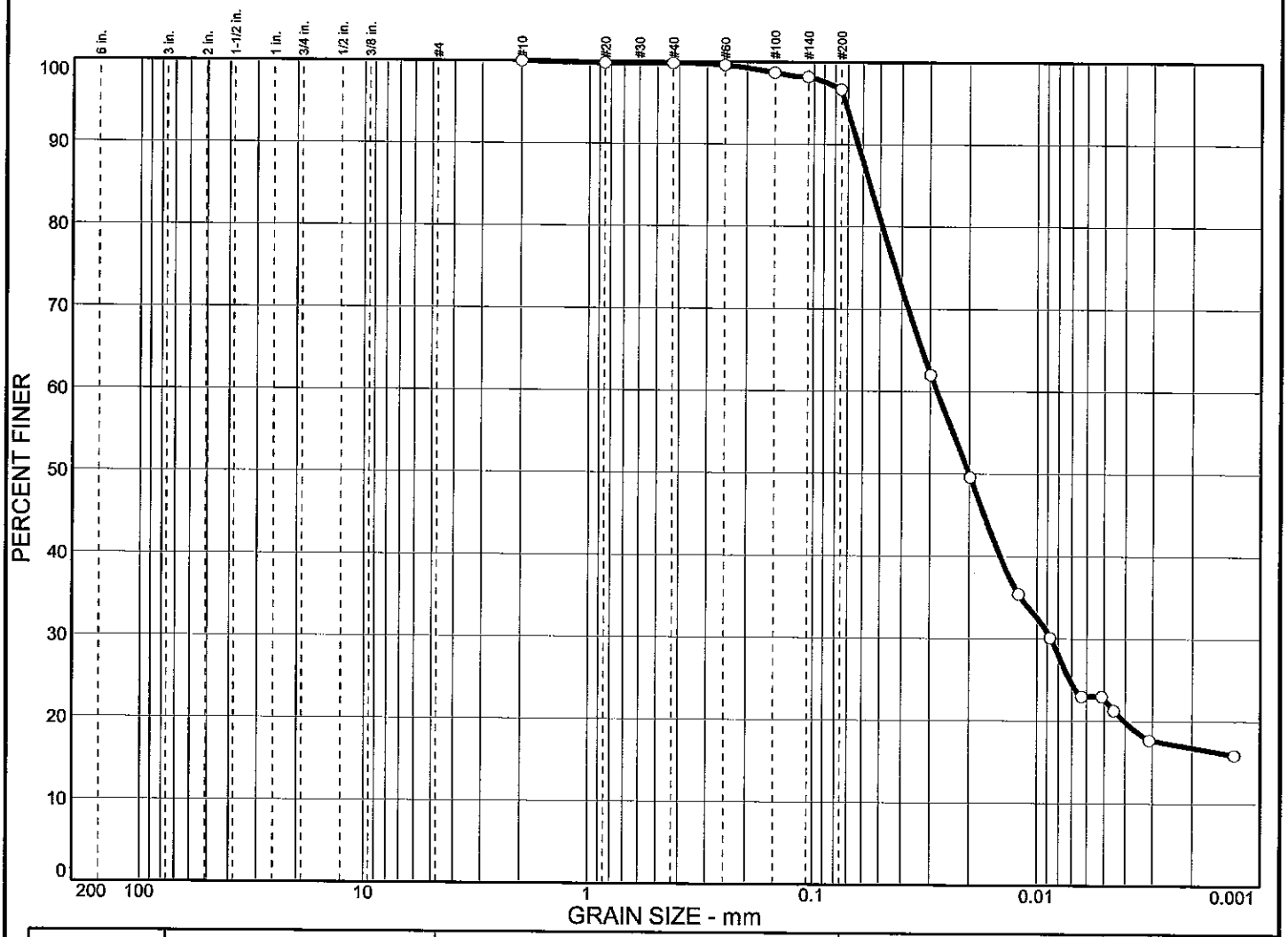
Project: BAYOU DUPONT

Source of Sample: B-2 **Depth:** 18-20
Sample Number: 7
Proj. No.: B09-012 **Date Sampled:** 3-5-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	3.3	74.0	22.7

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	58	22	0.0555	0.0279	0.0201	0.0087				

MATERIAL DESCRIPTION	USCS	AASHTO
○ LO G CL W/ SI, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-2 **Sample No.:** 7 **Elev./Depth:** 18-20

Remarks:

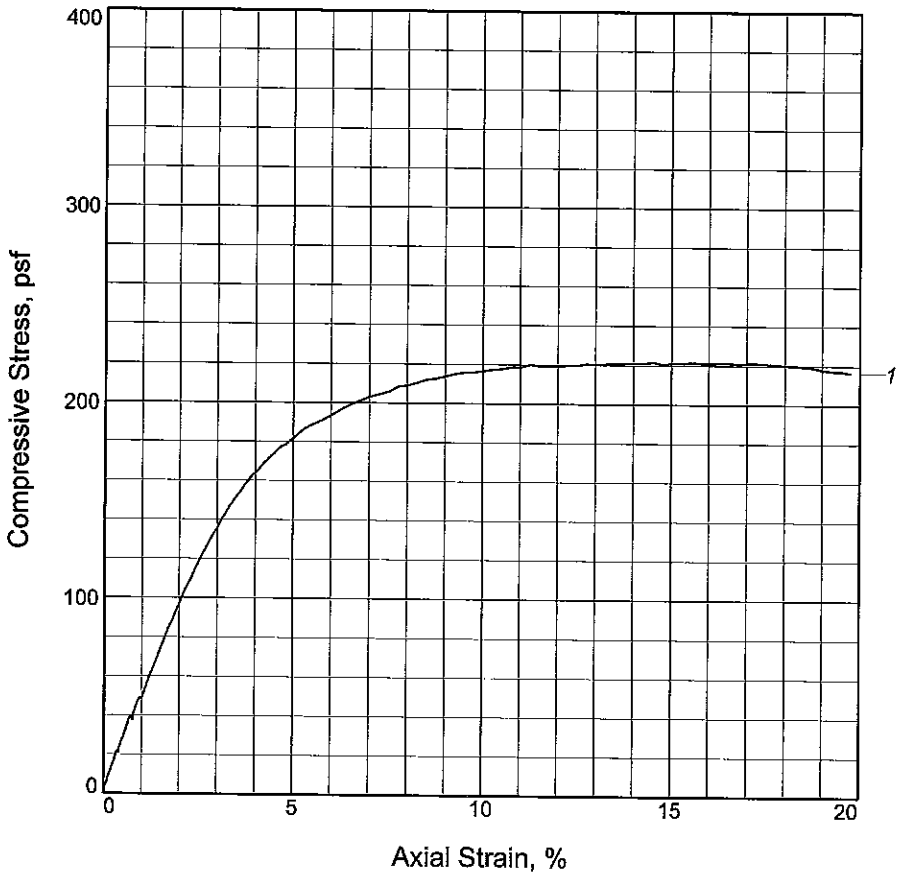
○ ASTM C136, D422

F.M.=0.01

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	221.7			
Undrained shear strength, psf	110.8			
Failure strain, %	14.5			
Strain rate, %/min.	1.00			
Water content, %	98.0			
Wet density, pcf	100.0			
Dry density, pcf	50.5			
Saturation, %	111.4			
Void ratio	2.4617			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: VSO G CL W/ SI PKTS+ORGS, CH

LL =	PL =	PI =	**Assumed GS=** 2.80	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-5-09

Remarks:
TYPE FAILURE: 40 DEGREE SHEAR

ASTM D 2166

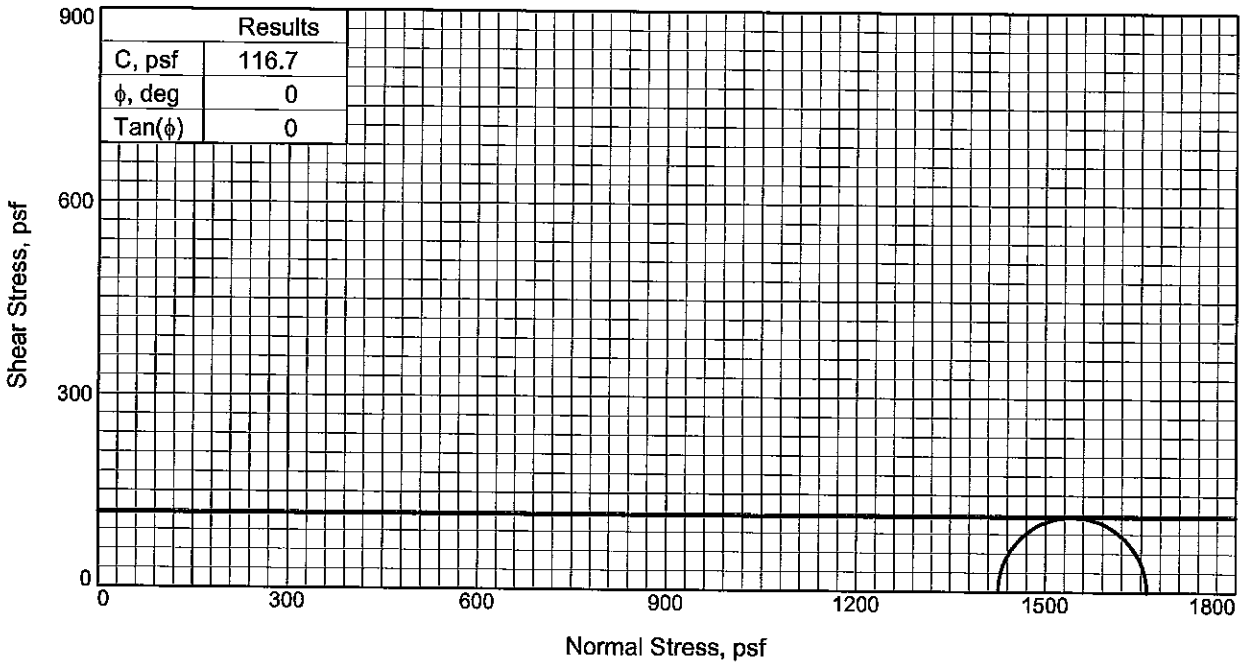
Client: URS

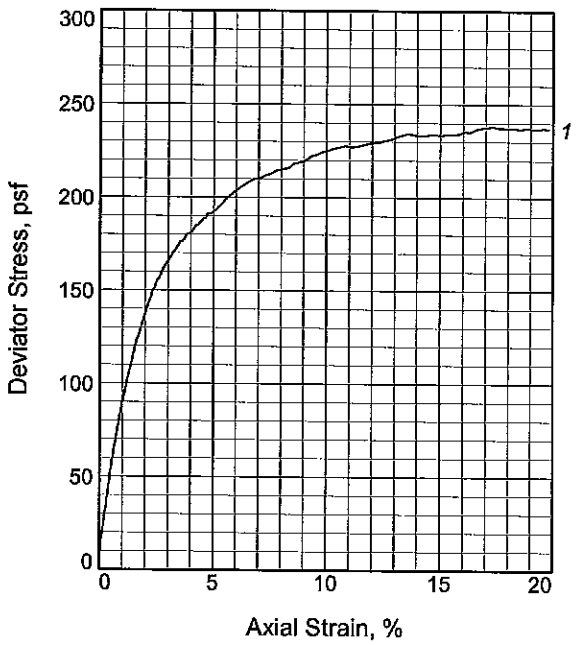
Project: BAYOU DUPONT

Source of Sample: B-2 **Depth:** 23-25
Sample Number: 8

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	41.5
	Dry Density, pcf	69.4
	Saturation, %	77.5
	Void Ratio	1.4720
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	41.5
	Dry Density, pcf	69.4
	Saturation, %	77.5
	Void Ratio	1.4720
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		9.900
Fail. Stress, psf		233.5
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1659.1
σ_3 Failure, psf		1425.6

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: SO G CL W/ SI+ORGS, CH

LL= 78 **PL=** 25 **PI=** 53
Assumed Specific Gravity= 2.75
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

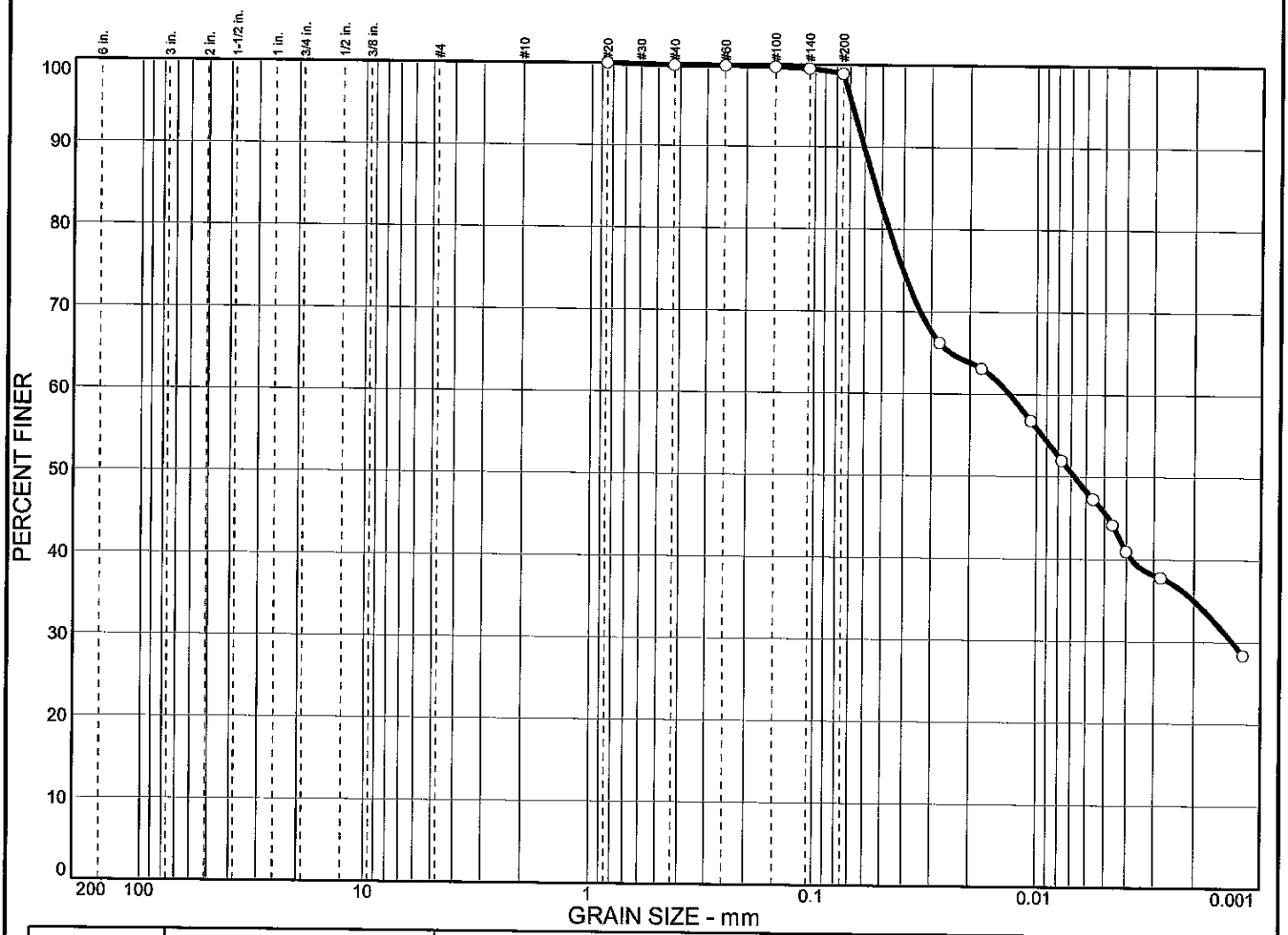
Project: BAYOU DUPONT

Source of Sample: B-2 **Depth:** 28-30
Sample Number: 9
Proj. No.: B09-012 **Date Sampled:** 3-5-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	1.1	53.2	45.7

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	78	25	0.0533	0.0132	0.0068	0.0013				

MATERIAL DESCRIPTION	USCS	AASHTO
○ SO G CL W/ SI+ORGS, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-2 **Sample No.:** 9 **Elev./Depth:** 28-30

Remarks:

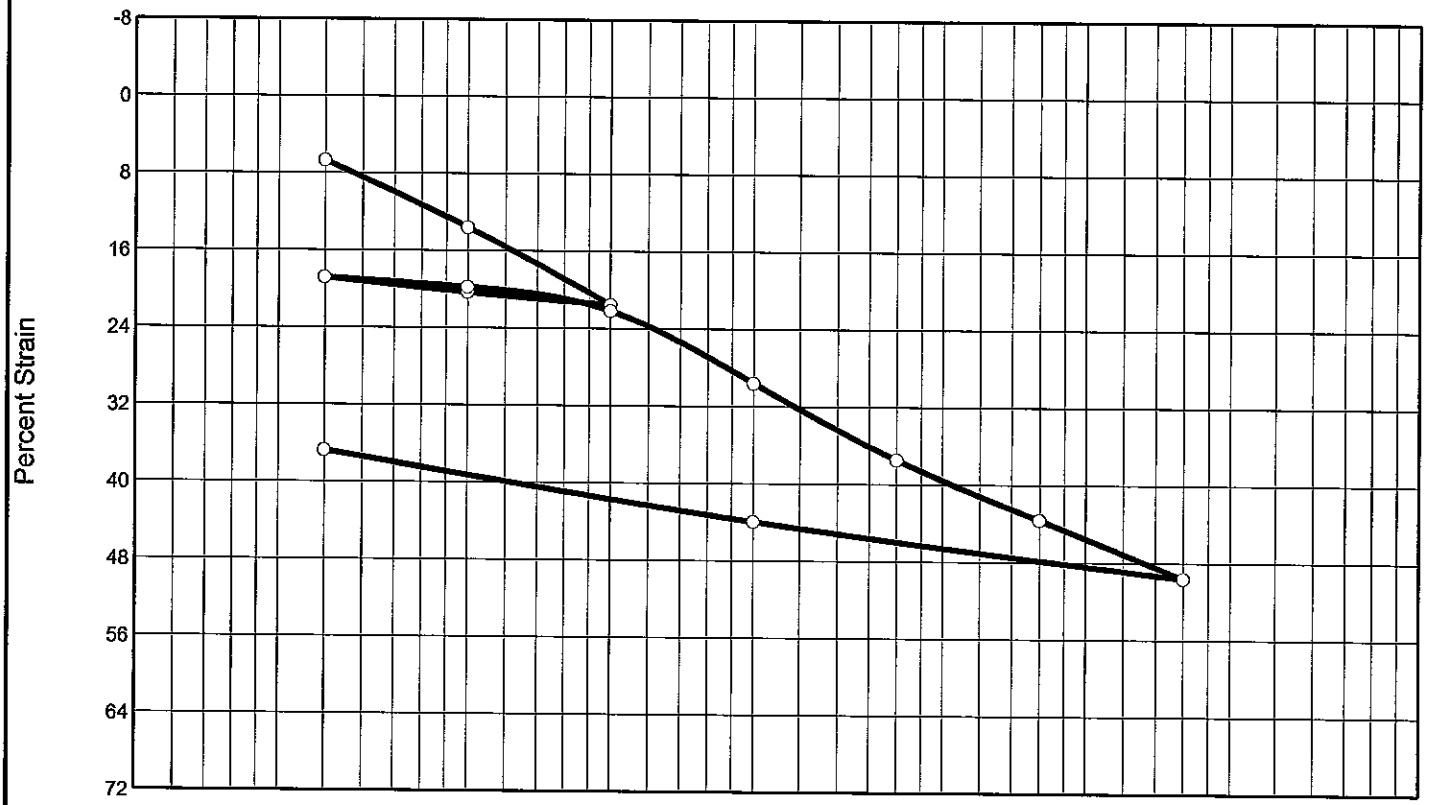
○ ASTM C136, D422

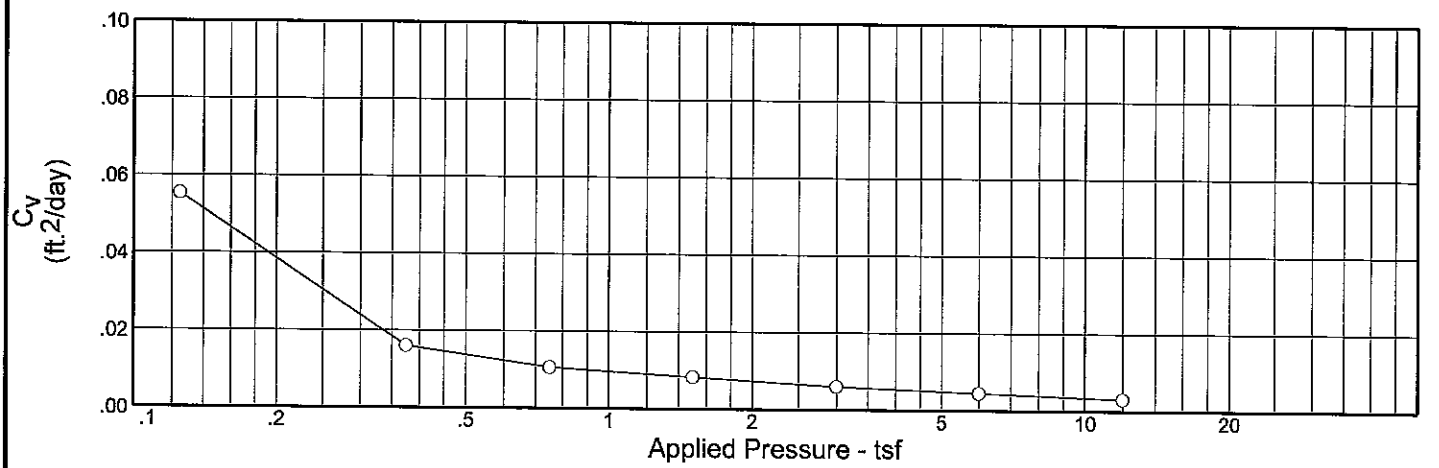
F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT





Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
92.8 %	78.4 %	51.9	144	104	2.80	(CH)		2.367

MATERIAL DESCRIPTION

VSO G CL W/ ORG PKTS, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-2 **Sample No.:** 6 **Elev./Depth:** 13-15

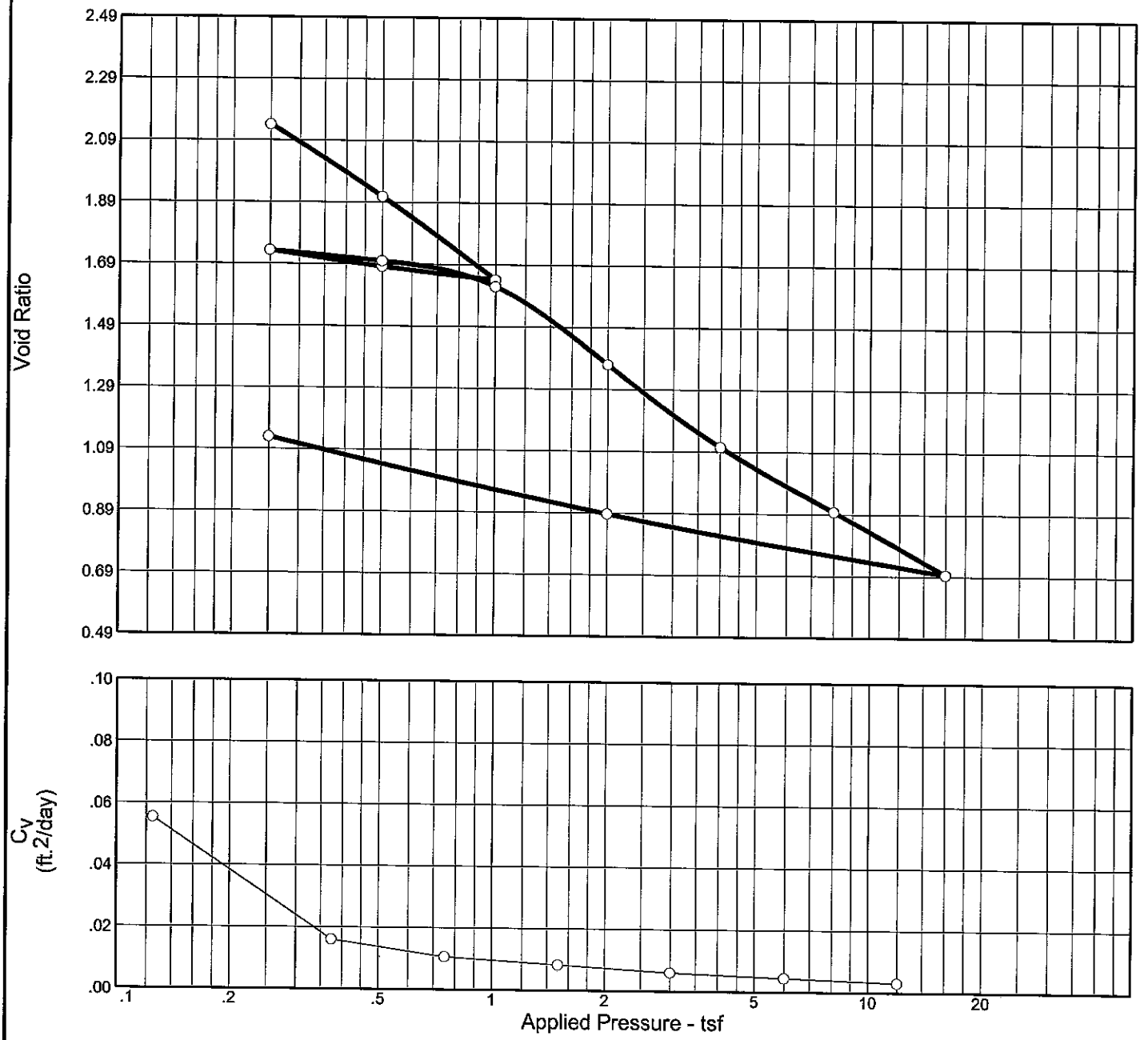
CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

Remarks:

ASTM D2435

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
92.8 %	78.4 %	51.9	144	104	2.80	(CH)		2.367

MATERIAL DESCRIPTION

VSO G CL W/ ORG PKTS, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-2 **Sample No.:** 6 **Elev./Depth:** 13-15

CONSOLIDATION/SWELL TEST REPORT

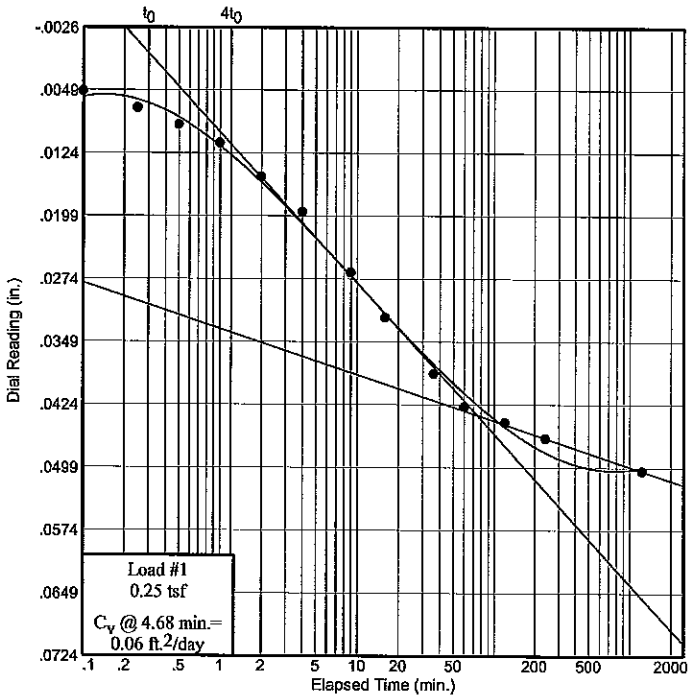
Southern Earth Sciences, Inc.

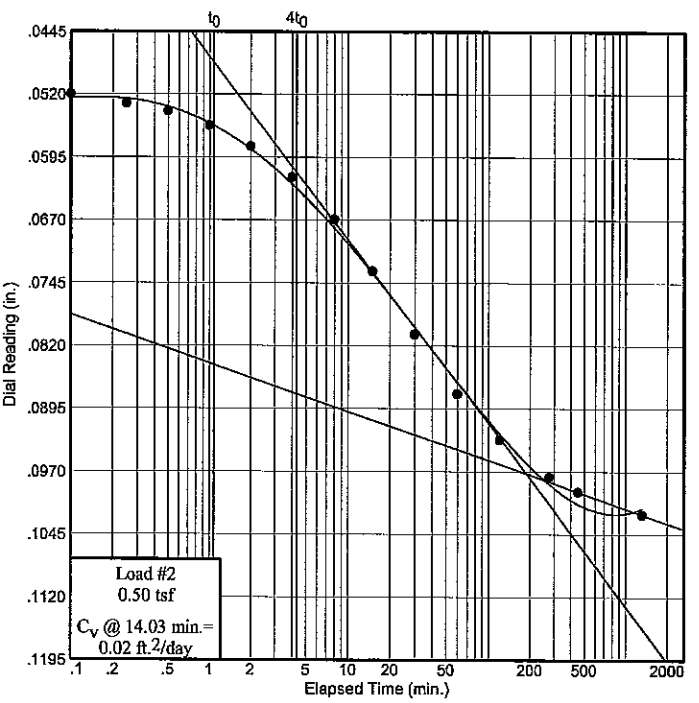
Remarks:
ASTM D2435

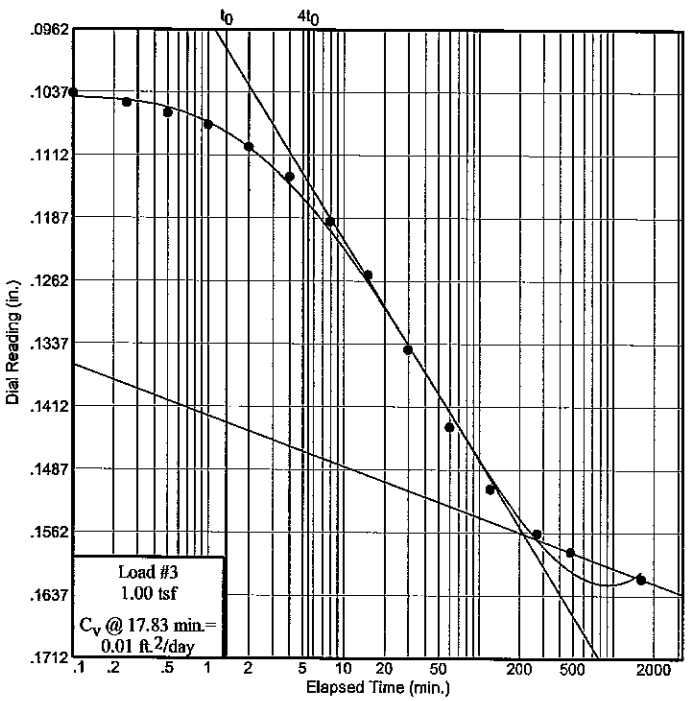
Dial Reading vs. Time

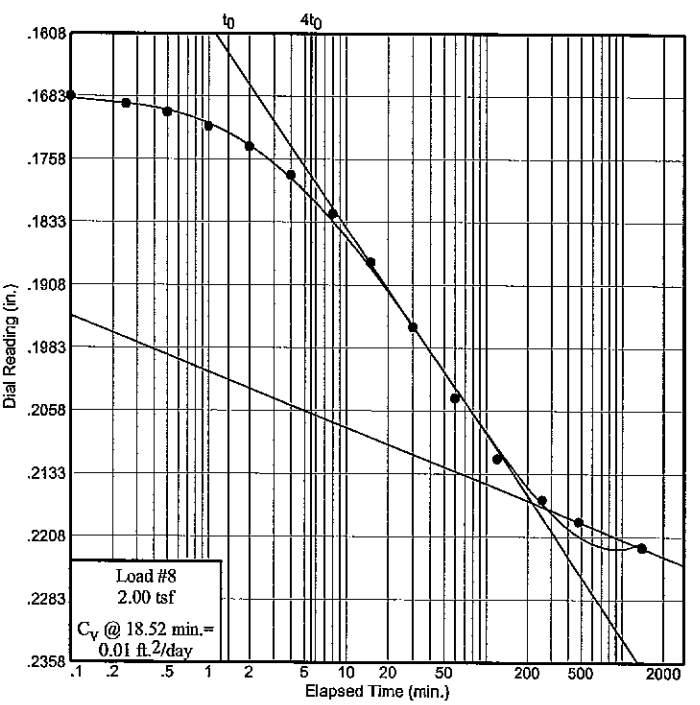
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-2 Sample No.: 6 Elev./Depth: 13-15









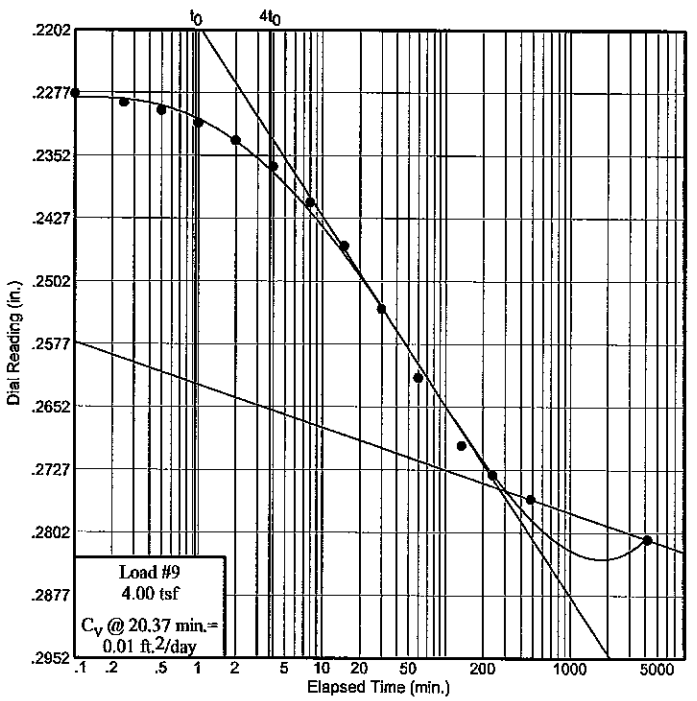
Dial Reading vs. Time

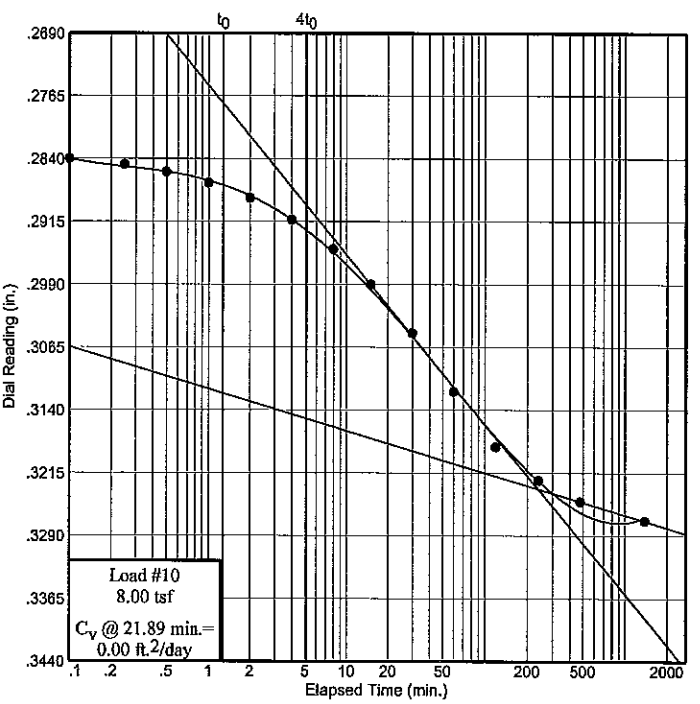
Southern Earth Sciences, Inc.

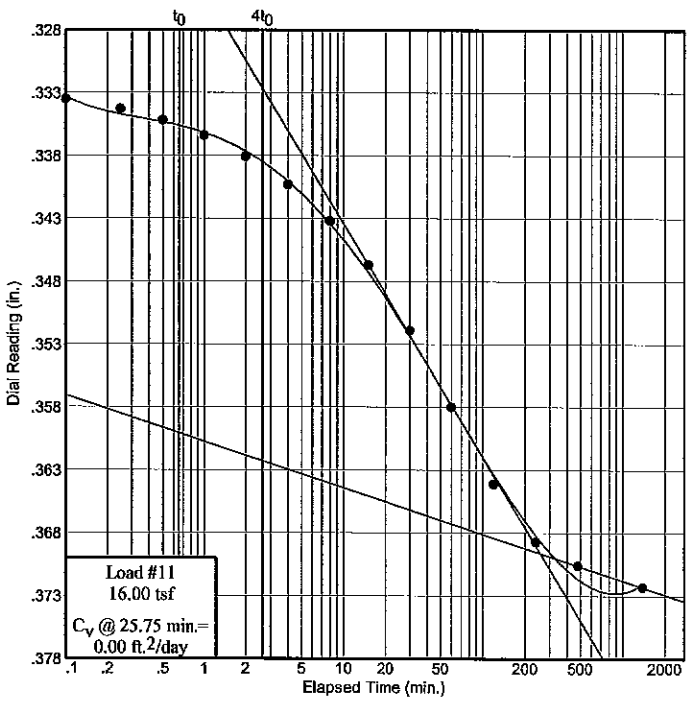
Dial Reading vs. Time

Project No.: B09-012
Project: BAYOU DUPONT

Source: B-2 Sample No.: 6 Elev./Depth: 13-15







Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-2
Sample No.: 6
Elev. or Depth: 13-15 **Sample Length(in./cm.):**
Location:
Description: VSO G CL W/ ORG PKTS, CH
Liquid Limit: 144 **Plasticity Index:** 104
USCS: (CH) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST	AFTER TEST
Wet w+t =	159.39 g.	**Consolidometer #** = 1	**Wet w+t** = 69.30 g.
Dry w+t =	106.08 g.		**Dry w+t** = 45.46 g.
Tare Wt. =	38.10 g.	**Spec. Gravity** = 2.80	**Tare Wt.** = .00 g.
Height =	.75 in.	**Height** = .75 in.	
Diameter =	2.50 in.	**Diameter** = 2.50 in.	
Weight =	89.52 g.	**Defl. Table** = Unit No. 183 Old 2.5in	
Moisture =	78.4 %	**Ht. Solids** = 0.2228 in.	**Moisture** = 52.4 %
Wet Den. =	92.6 pcf	**Dry Wt.** = 50.17 g.*	**Dry Wt.** = 45.46 g.
Dry Den. =	51.9 pcf	**Void Ratio** = 2.367	**Void Ratio** = 1.129
		Saturation = 92.8 %	

*** Initial dry weight used in calculations**

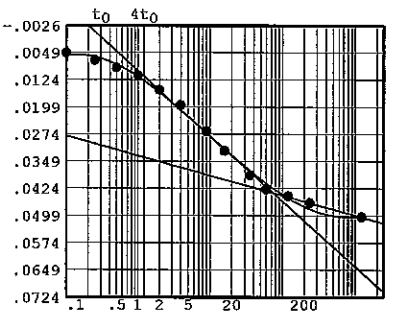
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				2.367	
0.25	0.05070	0.00040	0.06	0.007	2.141	6.7 Comprs.
0.50	0.10280	0.00070	0.02	0.008	1.908	13.6 Comprs.
1.00	0.16300	0.00130	0.01	0.009	1.641	21.6 Comprs.
0.50	0.15410	0.00160	0.04		1.682	20.3 Comprs.
0.25	0.14230	0.00120	0.01		1.733	18.8 Comprs.
0.50	0.14980	0.00130	0.05	0.001	1.700	19.8 Comprs.
1.00	0.16820	0.00170	0.03	0.005	1.619	22.2 Comprs.
2.00	0.22420	0.00210	0.01	0.011	1.370	29.6 Comprs.
4.00	0.28420	0.00320	0.01	0.010	1.105	37.5 Comprs.
8.00	0.33170	0.00450	0.00	0.011	0.898	43.6 Comprs.
16.00	0.37890	0.00660	0.00	0.009	0.696	49.6 Comprs.
2.00	0.33220	0.00250			0.887	44.0 Comprs.
0.25	0.27750	0.00180			1.129	36.8 Comprs.

C_c = 0.67 P_c = 3.89 tsf C_r = 0.19

Pressure: 0.25 tsf **TEST READINGS** **Load No. 1**

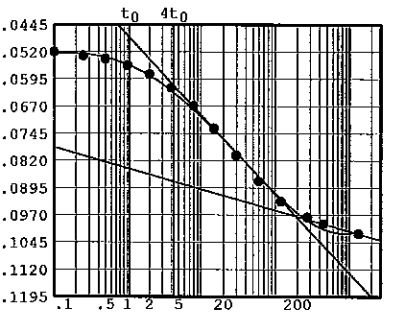
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	60.00	0.04300
2	0.10	0.00540	12	120.00	0.04490
3	0.25	0.00740	13	240.00	0.04680
4	0.50	0.00940	14	1230.00	0.05070
5	1.00	0.01160			
6	2.00	0.01560			
7	4.00	0.01980			
8	9.00	0.02700			
9	16.00	0.03240			
10	36.00	0.03910			



Void Ratio = 2.141 **Compression** = 6.7 %
D_0 = 0.00030 D_{50} = 0.02197 D_{100} = 0.04363
C_v at 4.7 min. = 0.06 ft.^{2}/day C_α = 0.007

Pressure: 0.50 tsf **TEST READINGS** **Load No. 2**

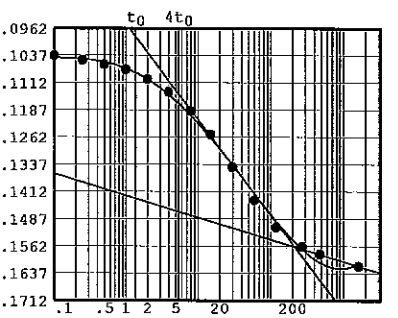
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.05070	11	60.00	0.08840
2	0.10	0.05270	12	120.00	0.09390
3	0.25	0.05380	13	275.00	0.09830
4	0.50	0.05470	14	450.00	0.10010
5	1.00	0.05640	15	1320.00	0.10280
6	2.00	0.05890			
7	4.00	0.06260			
8	8.00	0.06760			
9	15.00	0.07380			
10	30.00	0.08130			



Void Ratio = 1.908 **Compression** = 13.6 %
D_0 = 0.04820 D_{50} = 0.07271 D_{100} = 0.09722
C_v at 14.0 min. = 0.02 ft.^{2}/day C_α = 0.008

Pressure: 1.00 tsf **TEST READINGS** **Load No. 3**

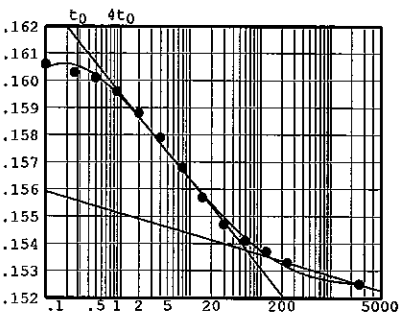
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.10280	11	60.00	0.14490
2	0.10	0.10510	12	120.00	0.15230
3	0.25	0.10630	13	270.00	0.15760
4	0.50	0.10750	14	480.00	0.15980
5	1.00	0.10890	15	1620.00	0.16300
6	2.00	0.11150			
7	4.00	0.11510			
8	8.00	0.12040			
9	15.00	0.12680			
10	30.00	0.13570			



Void Ratio = 1.641 **Compression** = 21.6 %
D_0 = 0.09993 D_{50} = 0.12816 D_{100} = 0.15639
C_v at 17.8 min. = 0.01 ft.^{2}/day C_α = 0.009

Pressure: 0.50 tsf **TEST READINGS** **Load No. 4**

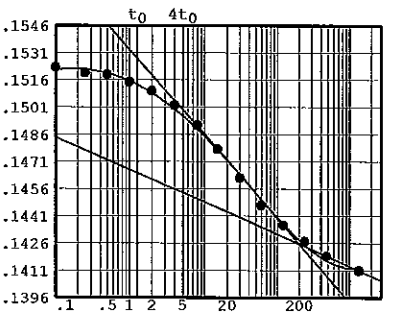
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.16300	11	60.00	0.15570
2	0.10	0.16220	12	120.00	0.15530
3	0.25	0.16190	13	240.00	0.15490
4	0.50	0.16170	14	2580.00	0.15410
5	1.00	0.16120			
6	2.00	0.16040			
7	4.00	0.15950			
8	8.00	0.15840			
9	15.00	0.15730			
10	30.00	0.15630			



Void Ratio = 1.682 **Compression =** 20.3 %
D_0 = 0.16169 **D_{50} =** 0.15772 **D_{100} =** 0.15375
C_v at 3.9 min. = 0.04 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 5**

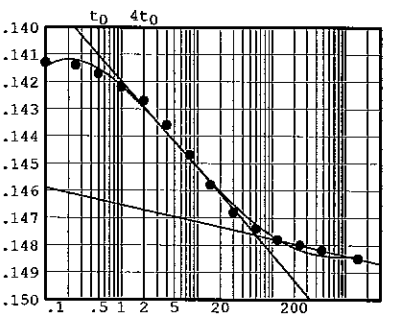
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.15410	11	60.00	0.14590
2	0.10	0.15350	12	120.00	0.14480
3	0.25	0.15320	13	240.00	0.14390
4	0.50	0.15310	14	480.00	0.14310
5	1.00	0.15270	15	1350.00	0.14230
6	2.00	0.15220			
7	4.00	0.15140			
8	8.00	0.15030			
9	15.00	0.14900			
10	30.00	0.14740			



Void Ratio = 1.733 **Compression =** 18.8 %
D_0 = 0.15306 **D_{50} =** 0.14782 **D_{100} =** 0.14258
C_v at 14.7 min. = 0.01 ft.^{2}/day

Pressure: 0.50 tsf **TEST READINGS** **Load No. 6**

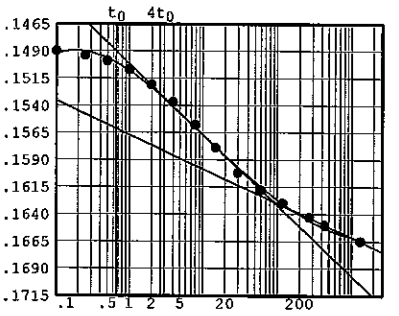
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.14230	11	60.00	0.14870
2	0.10	0.14260	12	120.00	0.14910
3	0.25	0.14270	13	240.00	0.14930
4	0.50	0.14300	14	480.00	0.14950
5	1.00	0.14350	15	1500.00	0.14980
6	2.00	0.14400			
7	4.00	0.14490			
8	8.00	0.14600			
9	15.00	0.14710			
10	30.00	0.14810			



Void Ratio = 1.700 **Compression =** 19.8 %
D_0 = 0.14008 **D_{50} =** 0.14386 **D_{100} =** 0.14763
C_v at 3.9 min. = 0.05 ft.^{2}/day **C_α =** 0.001

Pressure: 1.00 tsf **TEST READINGS** **Load No. 7**

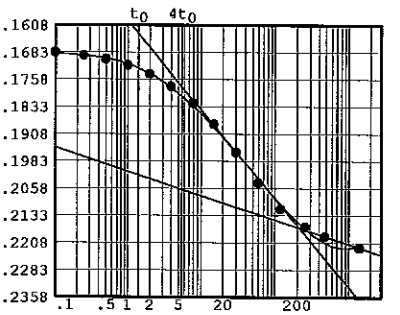
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.14980	11	60.00	0.16350
2	0.10	0.15070	12	120.00	0.16470
3	0.25	0.15110	13	270.00	0.16600
4	0.50	0.15160	14	440.00	0.16670
5	1.00	0.15240	15	1320.00	0.16820
6	2.00	0.15380			
7	4.00	0.15540			
8	8.00	0.15750			
9	15.00	0.15960			
10	30.00	0.16190			



Void Ratio = 1.619 **Compression =** 22.2 %
D_0 = 0.14708 **D_{50} =** 0.15495 **D_{100} =** 0.16281
C_v at 5.4 min. = 0.03 ft.^{2}/day **C_α =** 0.005

Pressure: 2.00 tsf **TEST READINGS** **Load No. 8**

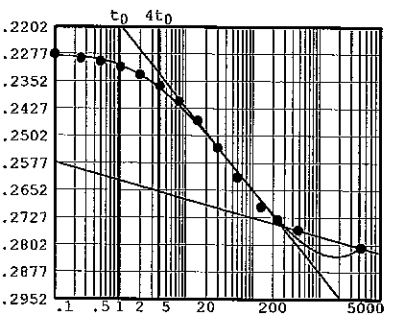
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.16820	11	60.00	0.20640
2	0.10	0.17040	12	120.00	0.21360
3	0.25	0.17130	13	256.00	0.21850
4	0.50	0.17230	14	480.00	0.22110
5	1.00	0.17400	15	1400.00	0.22420
6	2.00	0.17640			
7	4.00	0.17980			
8	8.00	0.18440			
9	15.00	0.19020			
10	30.00	0.19790			



Void Ratio = 1.370 **Compression =** 29.6 %
D_0 = 0.16491 **D_{50} =** 0.19081 **D_{100} =** 0.21670
C_v at 18.5 min. = 0.01 ft.^{2}/day **C_α =** 0.011

Pressure: 4.00 tsf **TEST READINGS** **Load No. 9**

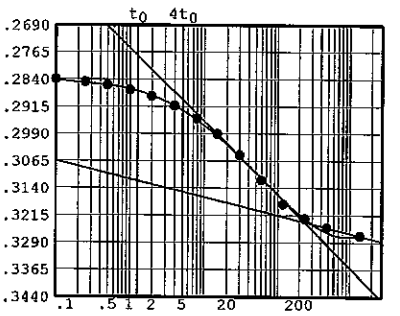
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.22420	11	60.00	0.26490
2	0.10	0.23100	12	134.00	0.27300
3	0.25	0.23210	13	240.00	0.27650
4	0.50	0.23300	14	480.00	0.27940
5	1.00	0.23450	15	4200.00	0.28420
6	2.00	0.23660			
7	4.00	0.23970			
8	8.00	0.24400			
9	15.00	0.24920			
10	30.00	0.25670			



Void Ratio = 1.105 **Compression =** 37.5 %
D_0 = 0.22451 **D_{50} =** 0.24972 **D_{100} =** 0.27493
C_v at 20.4 min. = 0.01 ft.^{2}/day **C_α =** 0.010

Pressure: 8.00 tsf **TEST READINGS** **Load No. 10**

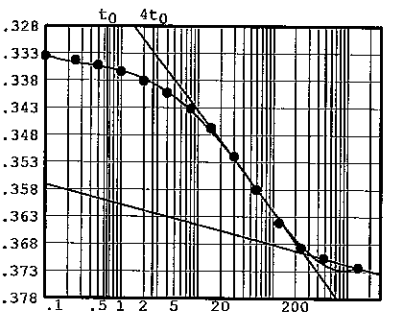
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.28420	11	60.00	0.31630
2	0.10	0.28850	12	120.00	0.32290
3	0.25	0.28920	13	240.00	0.32690
4	0.50	0.29010	14	480.00	0.32940
5	1.00	0.29140	15	1380.00	0.33170
6	2.00	0.29320			
7	4.00	0.29580			
8	8.00	0.29930			
9	15.00	0.30350			
10	30.00	0.30930			



Void Ratio = 0.898 **Compression** = 43.6 %
D_0 = 0.28174 D_{50} = 0.30256 D_{100} = 0.32338
C_v **at 21.9 min.** = 0.00 ft.^{2}/day C_α = 0.011

Pressure: 16.00 tsf **TEST READINGS** **Load No. 11**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.33170	11	60.00	0.36460
2	0.10	0.34010	12	120.00	0.37070
3	0.25	0.34090	13	240.00	0.37530
4	0.50	0.34180	14	480.00	0.37720
5	1.00	0.34300	15	1390.00	0.37890
6	2.00	0.34469			
7	4.00	0.34690			
8	8.00	0.34980			
9	15.00	0.35330			
10	30.00	0.35850			



Void Ratio = 0.696 **Compression** = 49.6 %
D_0 = 0.33273 D_{50} = 0.35117 D_{100} = 0.36961
C_v **at 25.8 min.** = 0.00 ft.^{2}/day C_α = 0.009

Southern Earth Sciences, Inc.

Laboratory Test Results

Project: **Bayou DuPont** Technical Responsibility: _____ Quality Assurance Officer

Client: URS

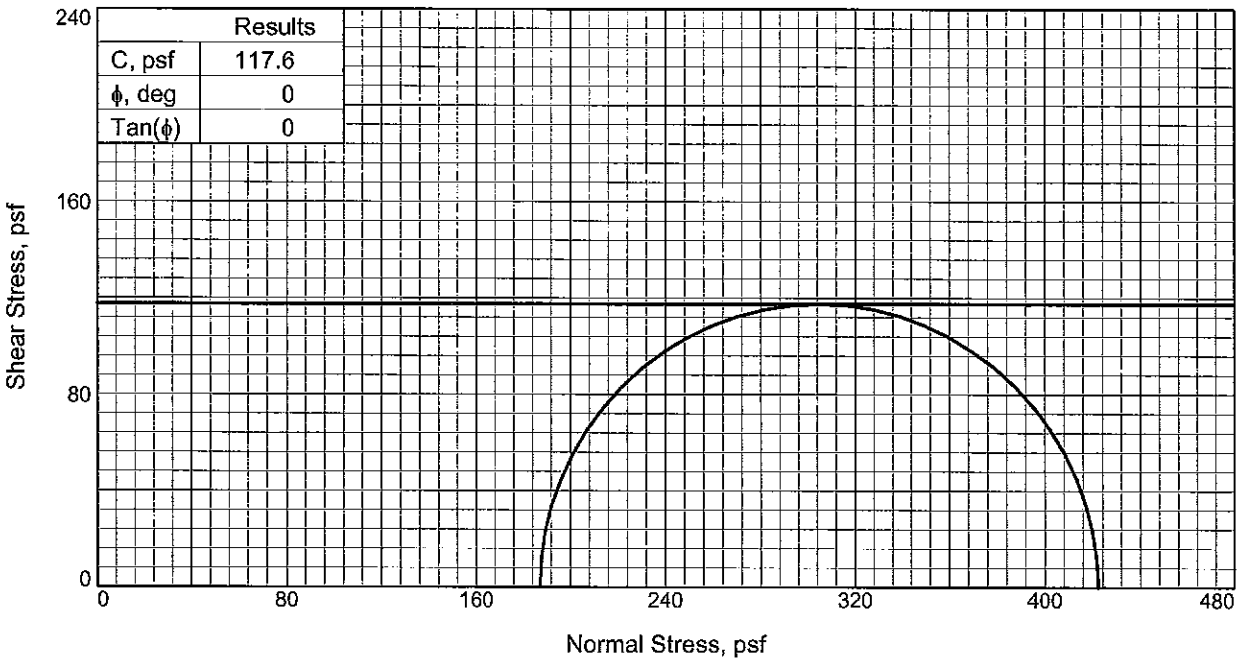
7389 Florida Blvd., Suite 300, Baton Rouge, LA 70806 Project No.: **B09-012** PM: S. Aviles Date of Issue: 3/12/2009

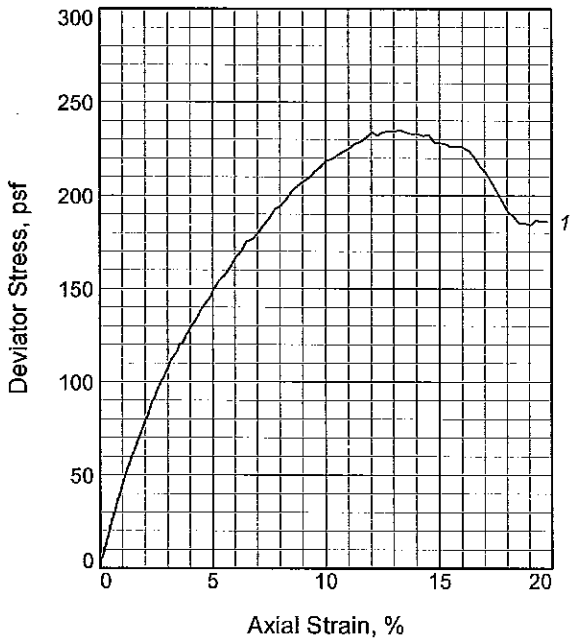
			ASTM DESIGNATION																
			D2216	D4318			D427	D2166		D2166	D2850	D422, C136 or C117					D2974	USCS	
				Atterberg Limits						Cohesion		Grain Size (% Passing)							
Boring No.	Depth (ft)	Classification	ω %	LL	PL	PI	SL	γ_{wet} pcf	γ_{dry} pcf	U psf	UU psf	Gravel	Sand	Silt	Clay	#200	Organic Content %		Confining Stress, Resistivity and Remarks
B-3	0-2	PEAT	1171.4	996	352	644											63.2	(PT)	
B-3	2-4	Very Soft, Black PEAT with clay	383.3				16.6	71.1	14.7		117.6							(CL)	Confining Pressure: 1.3 psi
B-3	4-6	Very Soft, Gray CLAY with organic pockets	171.4	141	39	102		92.5	34.1	64.0								(CL)	Specific Gravity: 2.792
B-3	6-8	Very Soft, Gray Lean CLAY with trace organics	43.0					118.2	82.6		140.5						1.5	(CL)	Confining Pressure: 2.6 psi
B-3	8-10	Very Soft, Gray Lean CLAY	46.3	45	30	15	23.0	106.0	72.5	74.1			1.2	73.7	25.1			(CL-ML)	
B-3	13-15	Very Soft, Gray CLAY with silt, shells and organics	89.7	126	22	104		98.3	51.8		75.7		2.5	55.3	42.2			(CH)	Specific Gravity: 2.778 Confining Pressure: 5.0 psi
B-3	18-20	Very Soft, Gray CLAY becoming organic peat and clay	230.3					82.6	25.0	112.4								(CH)	
B-3	23-25	VerySoft, Gray CLAY with organics	100.0	108	27	81		92.0	46.0		132.7		0.3	18.5	81.2			(CH)	Confining Pressure: 8.2 psi
B-3	28-30	Loose, Gray SILT with fine sand and trace clay	33.3	NP	NP	NP		120.8	90.6	378.5								(ML)	Shrinkage Limit- non-plastic, no shrinkage
B-3	33-35	Gray SANDY SILT with clay pockets	26.2	NP	NP	NP		130.4	103.3		5114.9		33.4	63.3	3.3			(ML)	Confining Pressure: 11.5 psi
B-3	38-40	Loose, Gray SANDY SILT with trace clay	26.5	NP	NP	NP		120.3	95.1	261.6								(ML)	

Geotechnical Lab
11638 Sun Belt Ct. Baton Rouge, LA 70809

The results presented only relate to those samples tested

Date Samples Rec.:
Date Testing Initiated:





Sample No.		1
Initial	Water Content, %	383.3
	Dry Density, pcf	14.7
	Saturation, %	100.2
	Void Ratio	9.1796
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	383.3
	Dry Density, pcf	14.7
	Saturation, %	100.2
	Void Ratio	9.1796
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		1.300
Fail. Stress, psf		235.1
Strain, %		13.3
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		422.3
σ_3 Failure, psf		187.2

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO BL PEAT W/ CL

LL= NP **PI=** NP
Assumed Specific Gravity= 2.40
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

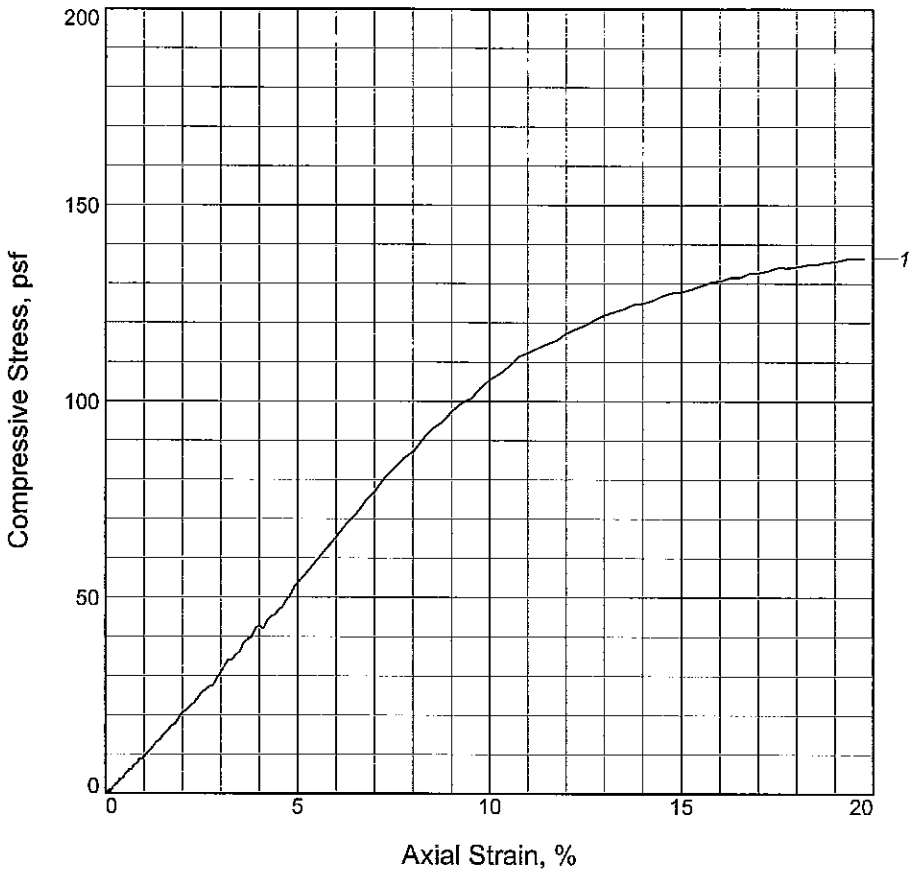
Project: BAYOU DUPONT

Source of Sample: B-3 **Depth:** 2-4
Sample Number: 2
Proj. No.: B09-012 **Date Sampled:** 3-5-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	127.9			
Undrained shear strength, psf	64.0			
Failure strain, %	15.0			
Strain rate, %/min.	1.00			
Water content, %	171.4			
Wet density, pcf	92.5			
Dry density, pcf	34.1			
Saturation, %	116.4			
Void ratio	4.1120			
Specimen diameter, in.	2.750			
Specimen height, in.	4.089			
Height/diameter ratio	1.49			

Description: VSO G CL W/ ORG PKTS, CH

LL = 141	**PL =** 39	**PI =** 102	**GS=** 2.792	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-5-09
Remarks:
TYPE FAILURE: BULGE

ASTM D 2166

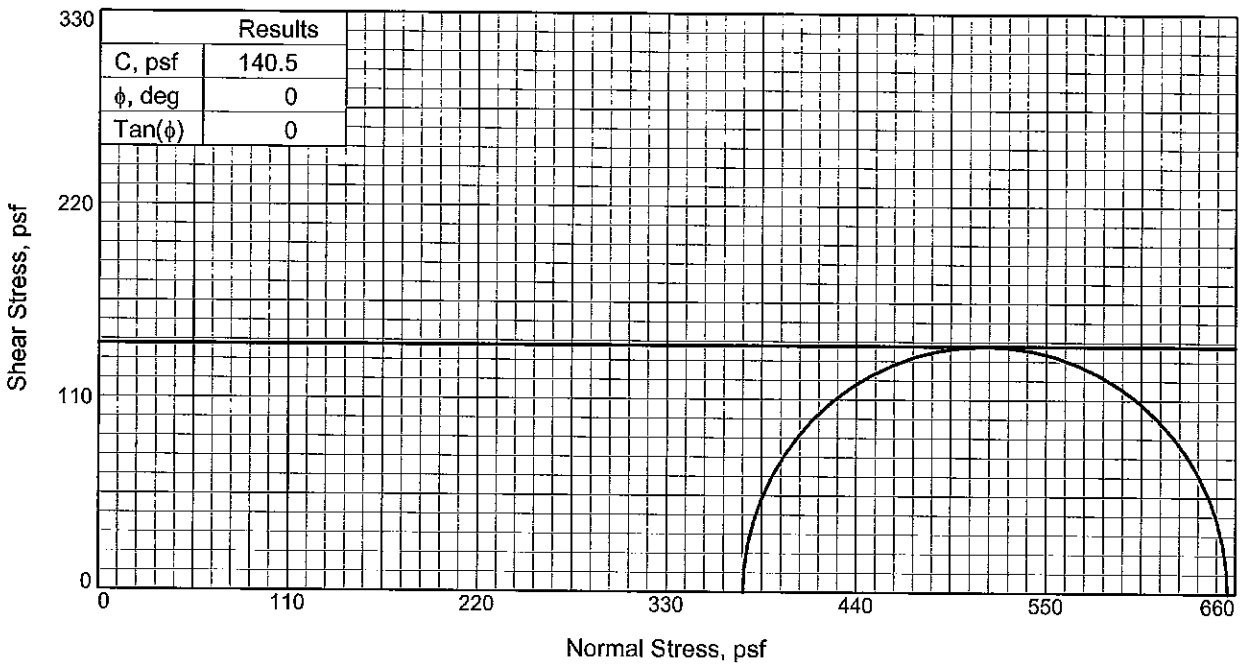
Client: URS

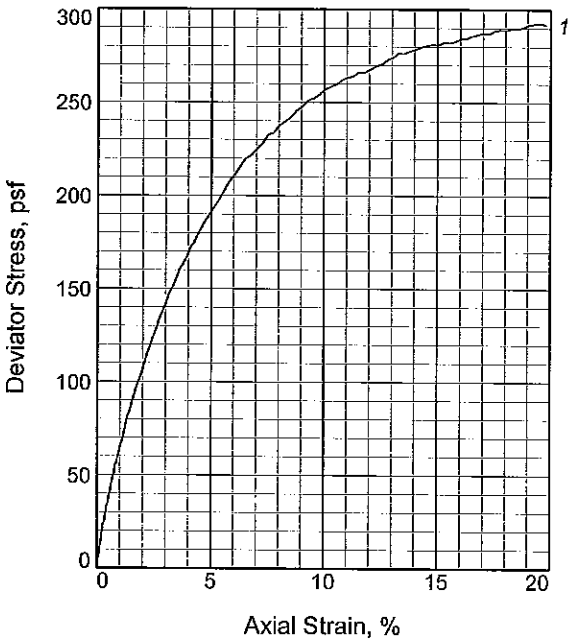
Project: BAYOU DUPONT

Source of Sample: B-3 **Depth:** 4-6
Sample Number: 3

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	43.0
	Dry Density, pcf	82.6
	Saturation, %	111.6
	Void Ratio	1.0397
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	43.0
	Dry Density, pcf	82.6
	Saturation, %	111.6
	Void Ratio	1.0397
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.600
Fail. Stress, psf		281.0
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		655.4
σ_3 Failure, psf		374.4

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G SICL W/ TR ORGS, CL

Assumed Specific Gravity= 2.70

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-3 **Depth:** 6-8

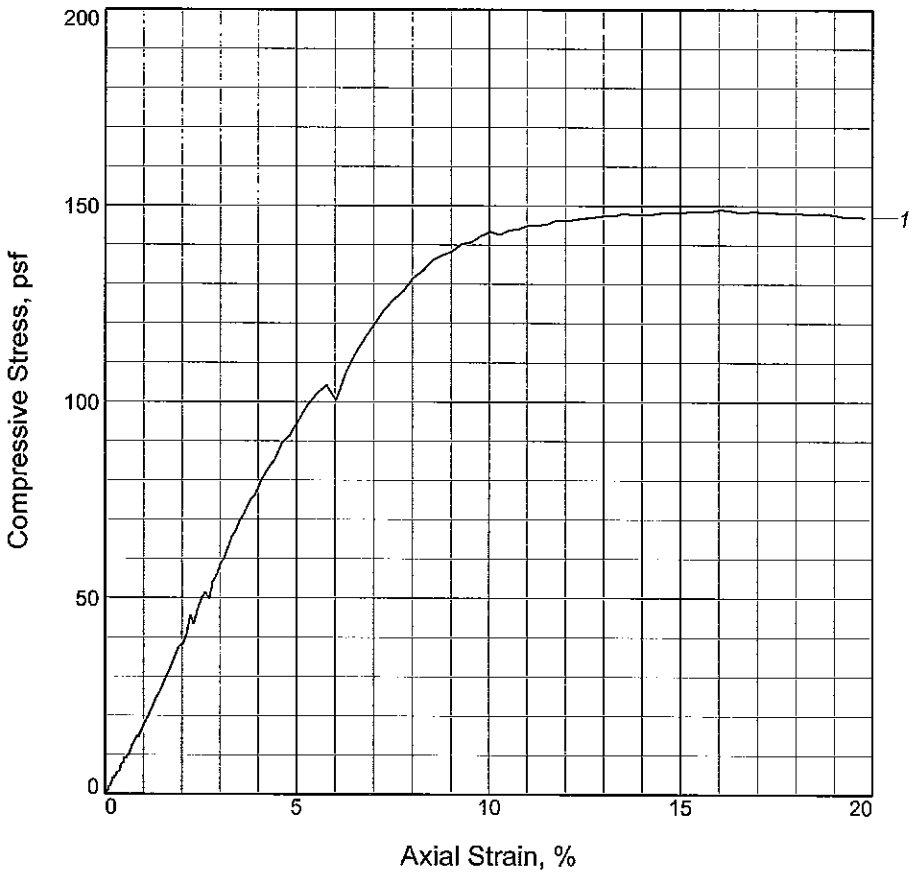
Sample Number: 4

Proj. No.: B09-012 **Date Sampled:** 3-5-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	148.2			
Undrained shear strength, psf	74.1			
Failure strain, %	15.0			
Strain rate, %/min.	1.00			
Water content, %	46.3			
Wet density, pcf	106.0			
Dry density, pcf	72.5			
Saturation, %	94.2			
Void ratio	1.3252			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: SO G SICL, CL-ML

LL = 45	**PL =** 30	**PI =** 15	**Assumed GS=** 2.70	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-5-09

Remarks:
TYPE FAILURE: BULGE+PARTIAL VERTICAL SHEAR

ASTM D 2166

Client: URS

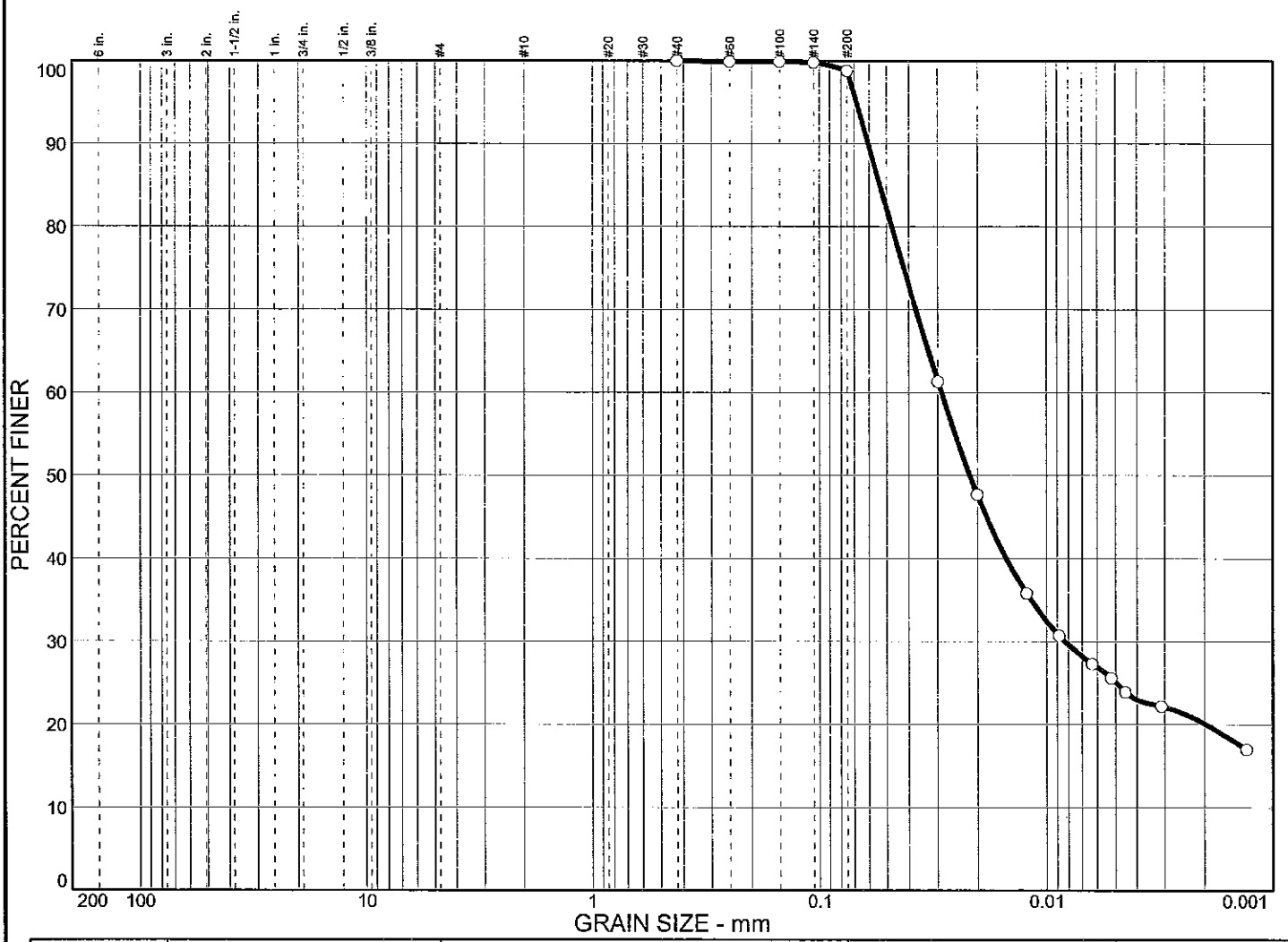
Project: BAYOU DUPONT

Source of Sample: B-3 **Depth:** 8-10
Sample Number: 5

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	1.2	73.7	25.1

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	45	30	0.0536	0.0288	0.0216	0.0083				

MATERIAL DESCRIPTION	USCS	AASHTO
○ SO G SICL, CL-ML	CL-ML	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-3 **Sample No.:** 5 **Elev./Depth:** 8-10

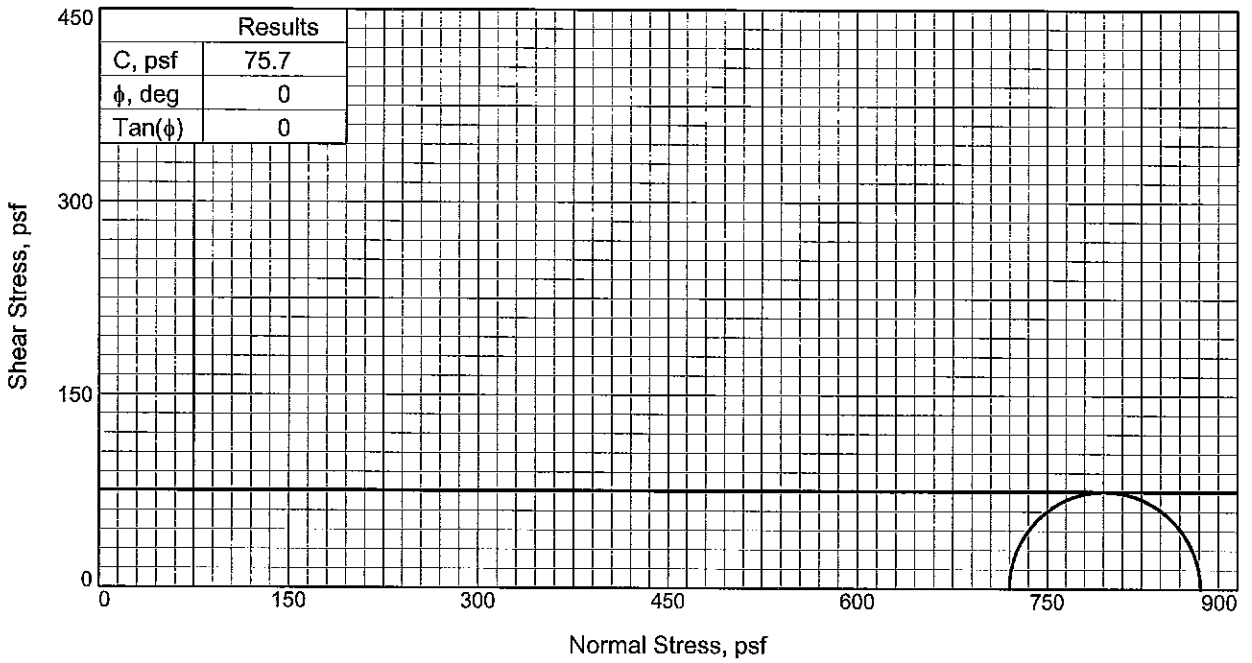
Remarks:

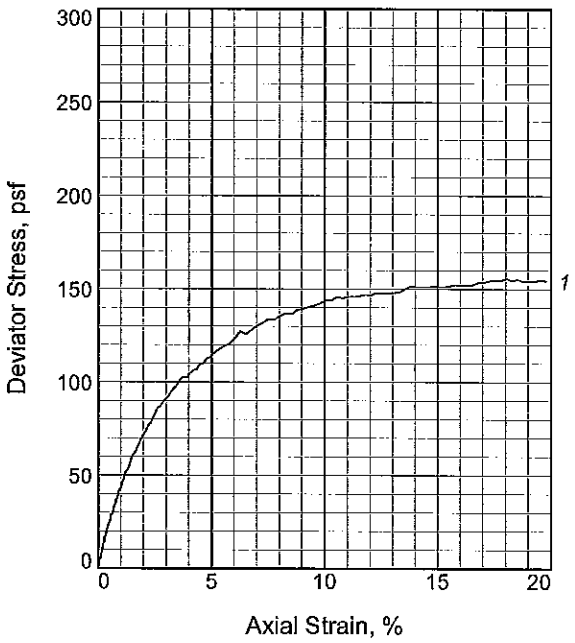
○ ASTM C136, D422

F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	89.7
	Dry Density, pcf	51.8
	Saturation, %	106.1
	Void Ratio	2.3479
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	89.7
	Dry Density, pcf	51.8
	Saturation, %	106.1
	Void Ratio	2.3479
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		5.000
Fail. Stress, psf		151.3
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		871.3
σ_3 Failure, psf		720.0

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: SO G CL W/ SI, SHELLS+ORGS, CH

LL= 126 **PL=** 22 **PI=** 104
Specific Gravity= 2.778
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

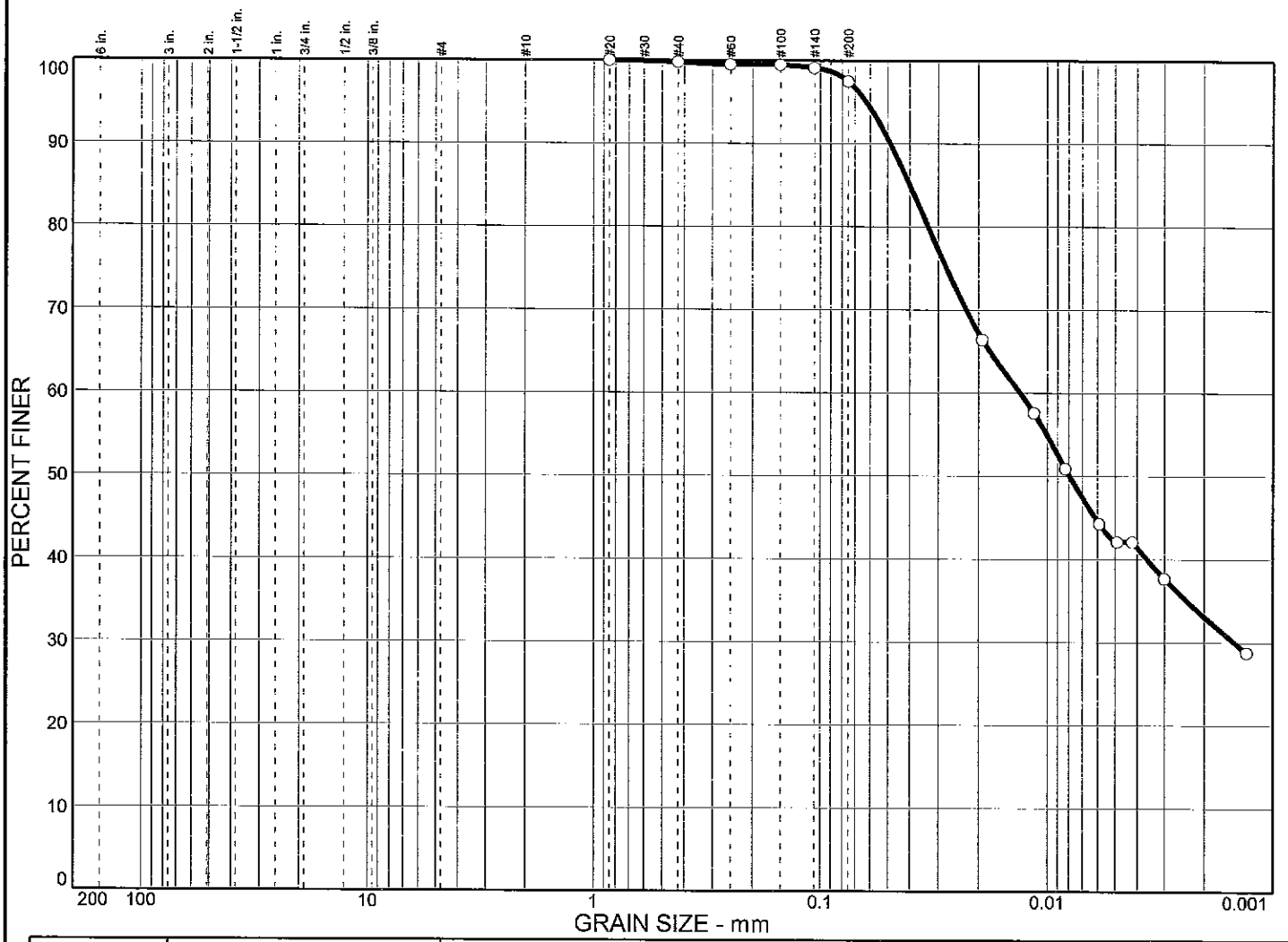
Project: BAYOU DUPONT

Source of Sample: B-3 **Depth:** 13-15
Sample Number: 6
Proj. No.: B09-012 **Date Sampled:** 3-5-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	2.5	55.3	42.2

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	126	22	0.0400	0.0131	0.0080	0.0015				

MATERIAL DESCRIPTION	USCS	AASHTO
○ SO G CL W/ SI, SHELLS+ORGS, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-3 **Sample No.:** 6 **Elev./Depth:** 13-15

Remarks:

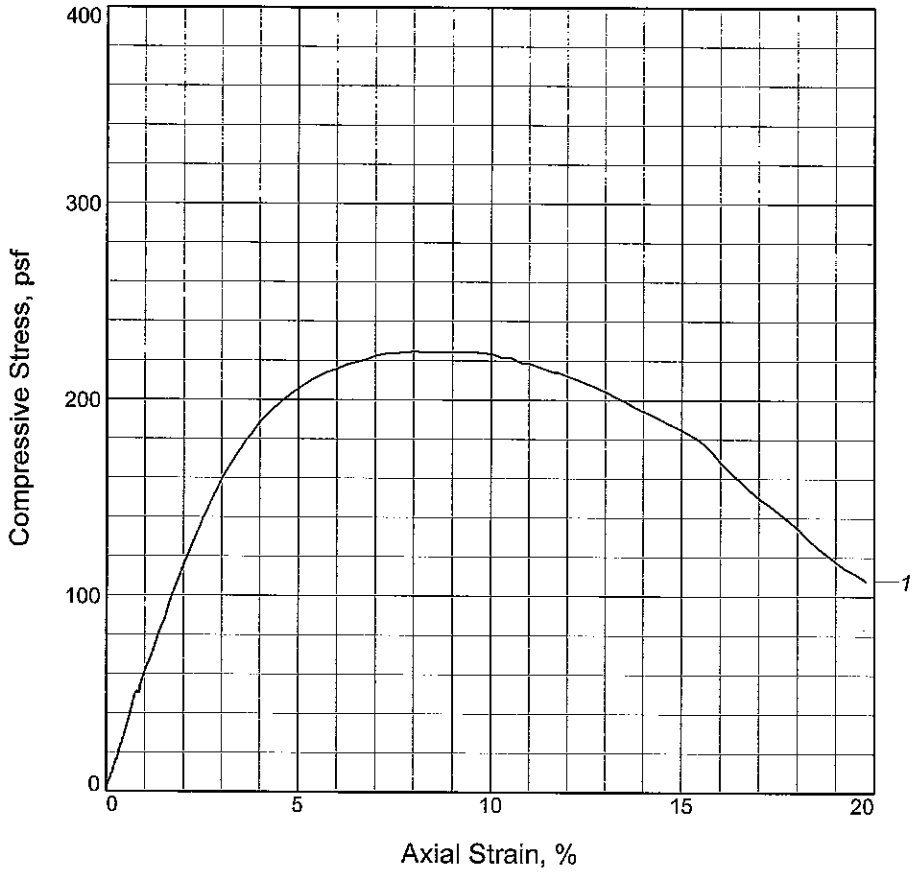
○ ASTM C136, D422

F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	224.7			
Undrained shear strength, psf	112.3			
Failure strain, %	8.0			
Strain rate, %/min.	1.00			
Water content, %	230.3			
Wet density, pcf	82.6			
Dry density, pcf	25.0			
Saturation, %	110.7			
Void ratio	4.9931			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: VSO G CL BEC ORG, PEAT+CL, OH

LL =	**PL =**	**PI =**	**Assumed GS=** 2.40	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-5-09

Remarks:
TYPE FAILURE: BULGE+MULTI FRACTURE

ASTM D 2166

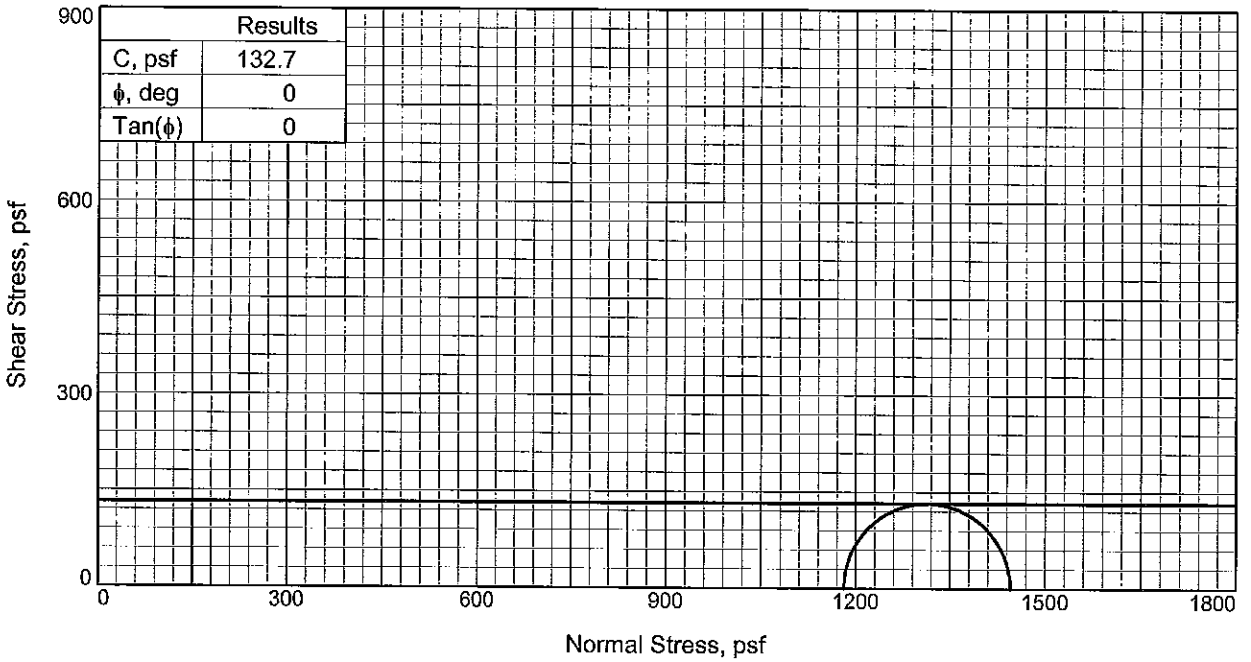
Client: URS

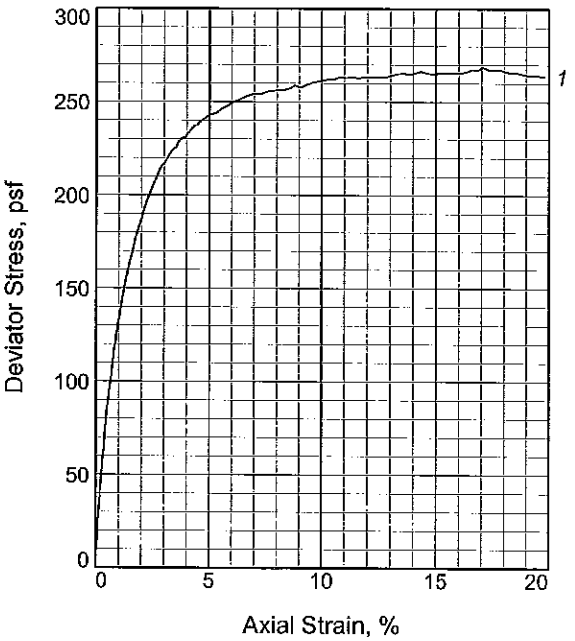
Project: BAYOU DUPONT

Source of Sample: B-3 **Depth:** 18-20
Sample Number: 7

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	100.0
	Dry Density, pcf	46.0
	Saturation, %	99.9
	Void Ratio	2.8019
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	100.0
	Dry Density, pcf	46.0
	Saturation, %	99.9
	Void Ratio	2.8019
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		8.200
Fail. Stress, psf		265.4
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1446.2
σ_3 Failure, psf		1180.8

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: SO G CL W/ ORGS, CH

LL= 108 **PL=** 27 **PI=** 81
Assumed Specific Gravity= 2.80
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

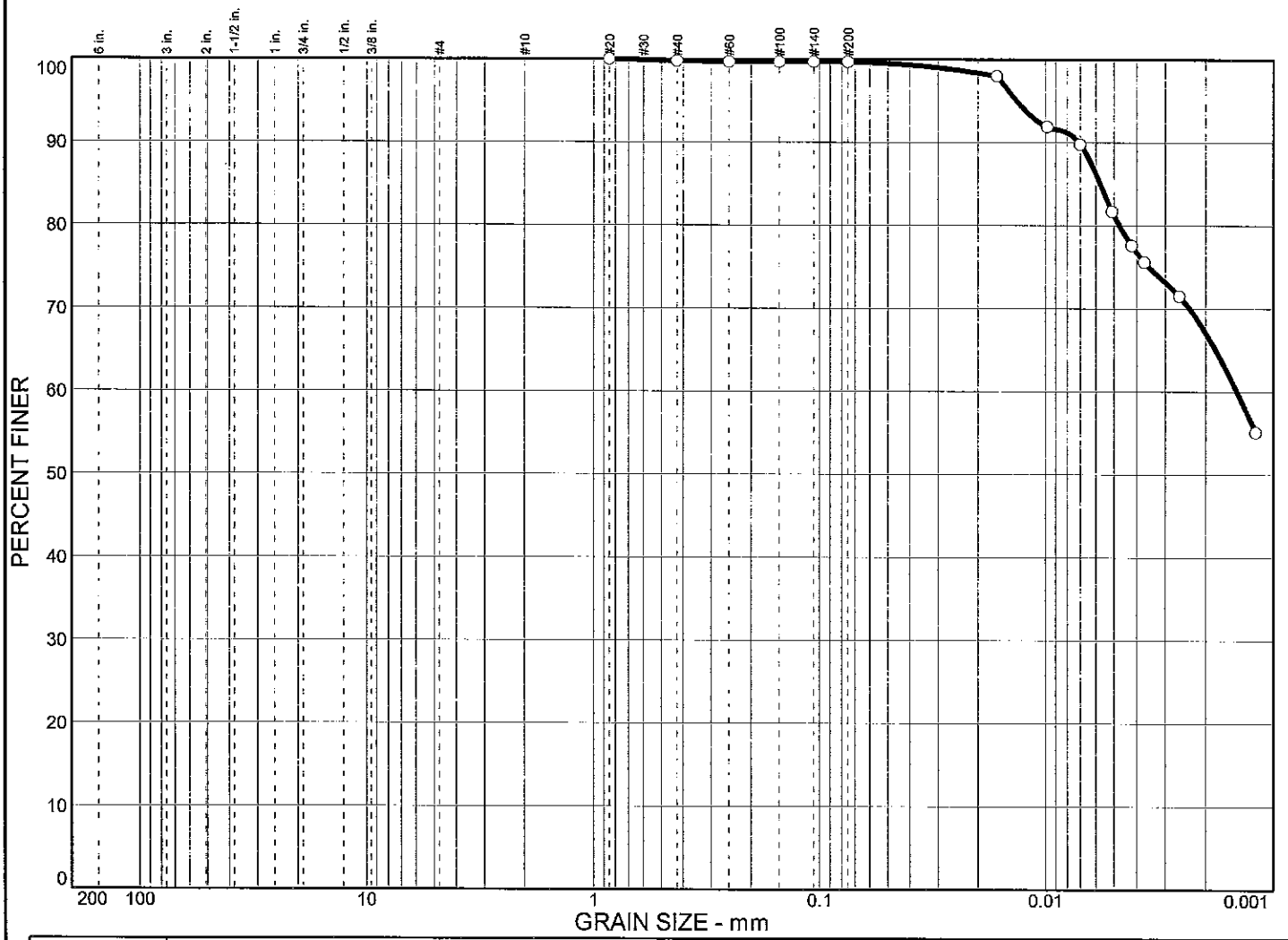
Project: BAYOU DUPONT

Source of Sample: B-3 **Depth:** 23-25
Sample Number: 8
Proj. No.: B09-012 **Date Sampled:** 3-5-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.3	18.5	81.2

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	108	27	0.0057	0.0015						

MATERIAL DESCRIPTION	USCS	AASHTO
○ SO G CL W/ ORGS, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-3 **Sample No.:** 8 **Elev./Depth:** 23-25

Remarks:

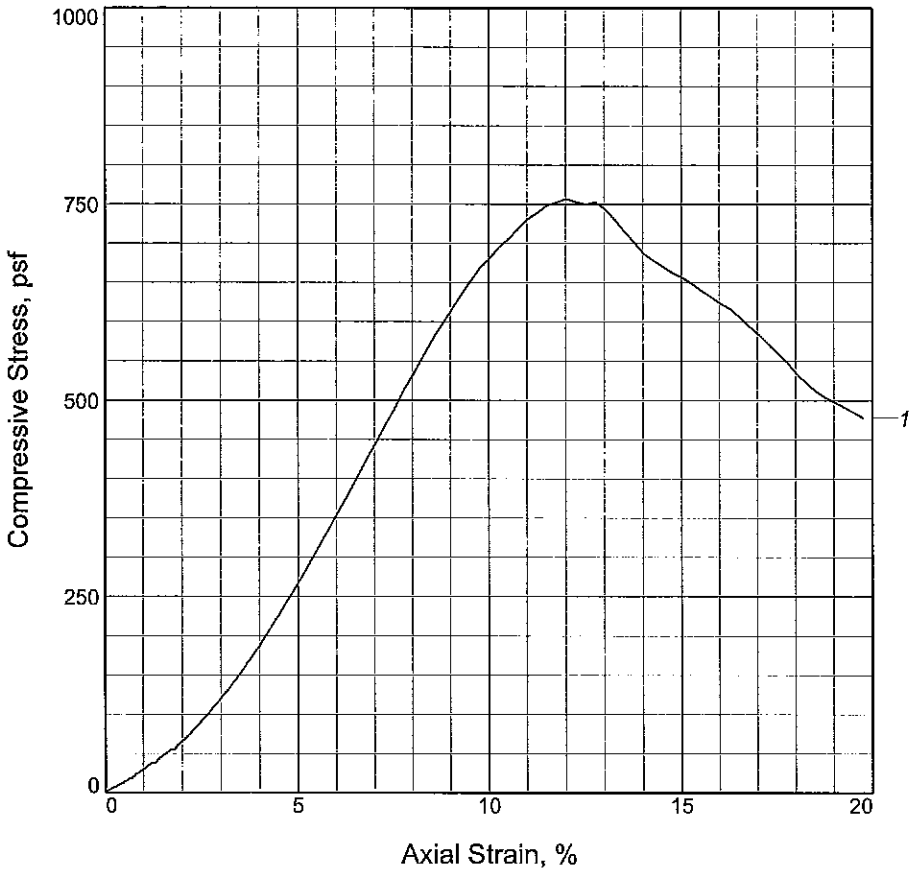
○ ASTM C136, D422

F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	756.9			
Undrained shear strength, psf	378.5			
Failure strain, %	12.0			
Strain rate, %/min.	1.00			
Water content, %	33.3			
Wet density, pcf	120.8			
Dry density, pcf	90.6			
Saturation, %	106.9			
Void ratio	0.8264			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: LO G SI W/ F SA+TR CL, ML

LL =	PL =	PI =	Assumed GS= 2.65	Type: UNDISTURBED

Project No.: B09-012
Date Sampled: 3-5-09
Remarks:
TYPE FAILURE: BULGE+MULTI SHEARS

ASTM D 2166

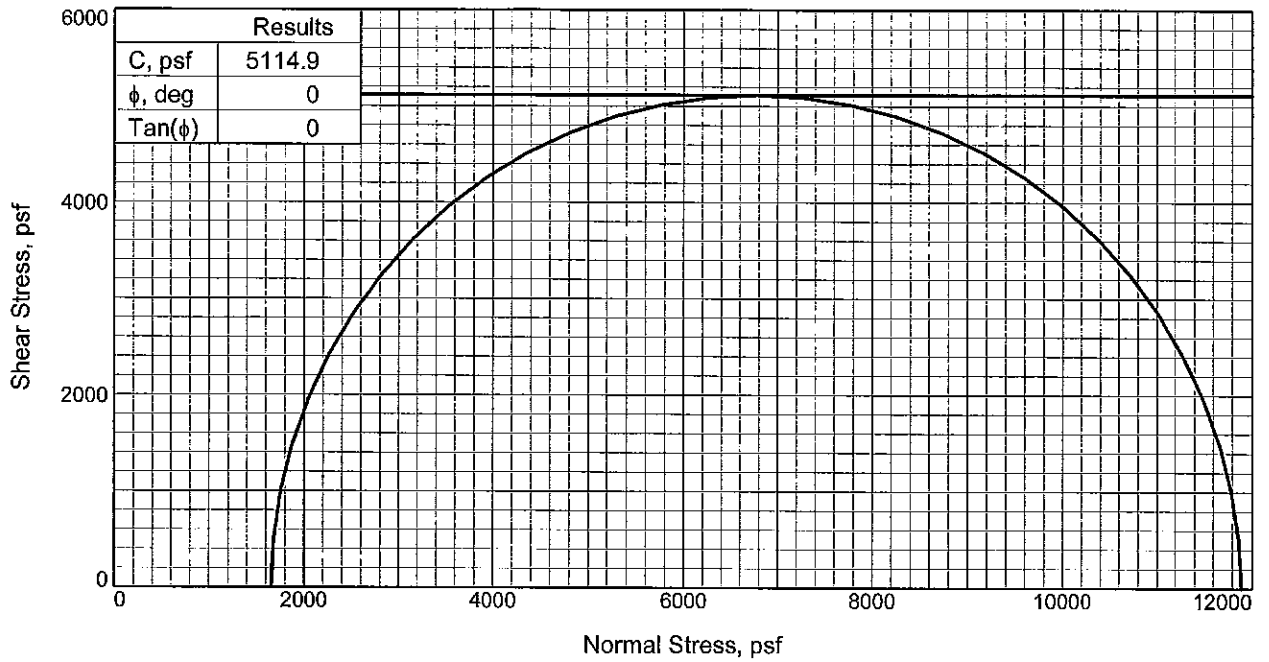
Client: URS

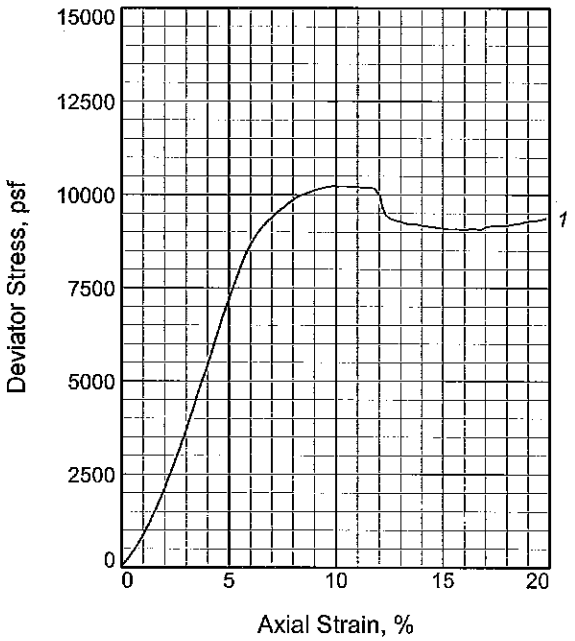
Project: BAYOU DUPONT

Source of Sample: B-3 **Depth:** 28-30
Sample Number: 9

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	26.2
	Dry Density, pcf	103.3
	Saturation, %	115.4
	Void Ratio	0.6009
	Diameter, in.	2.750
	Height, in.	5.608
At Test	Water Content, %	26.2
	Dry Density, pcf	103.3
	Saturation, %	115.4
	Void Ratio	0.6009
	Diameter, in.	2.750
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		11.500
Fail. Stress, psf		10229.8
Strain, %		9.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		11885.8
σ_3 Failure, psf		1656.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: G SASI W/ CL PKTS, ML

LL= NP **PI=** NP

Assumed Specific Gravity= 2.65

Remarks: TYPE FAILURE: BULGE+45 DEGREE SHEAR

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-3 **Depth:** 33-35

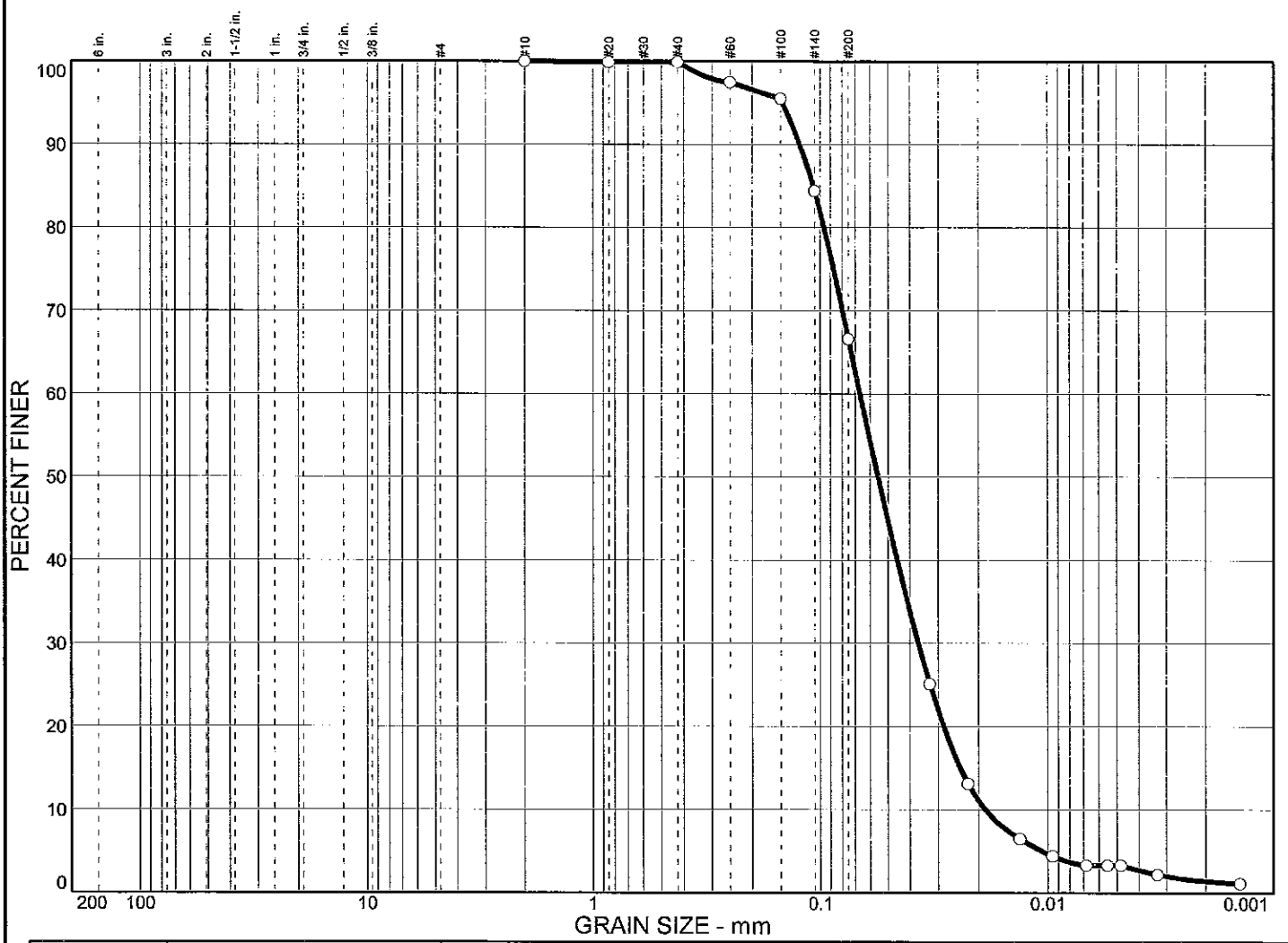
Sample Number: 10

Proj. No.: B09-012 **Date Sampled:** 3-4-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	33.4	63.3	3.3

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	NP	NP	0.108	0.0666		0.0367	0.0240	0.0187	1.08	3.56

MATERIAL DESCRIPTION	USCS	AASHTO
○ G SASI W/ CL PKTS, ML	(ML)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-3 **Sample No.:** 10 **Elev./Depth:** 33-35

Remarks:

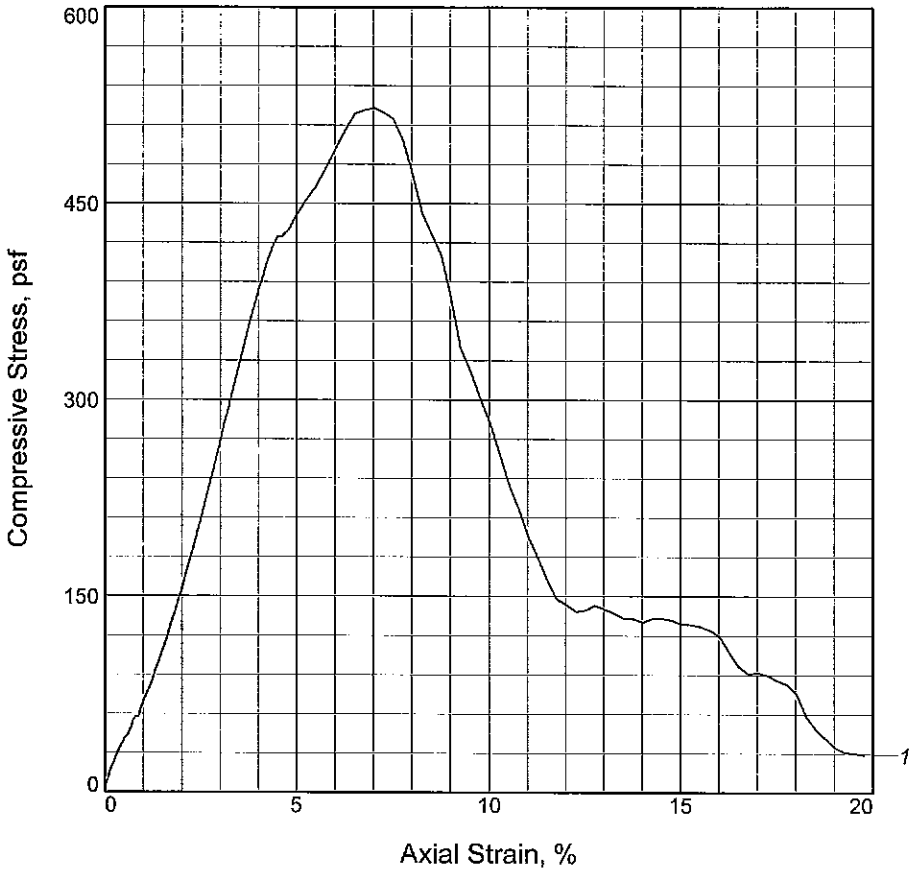
○ ASTM C136, D422

F.M.=0.05

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	523.2			
Undrained shear strength, psf	261.6			
Failure strain, %	7.0			
Strain rate, %/min.	1.00			
Water content, %	26.5			
Wet density, pcf	120.3			
Dry density, pcf	95.1			
Saturation, %	94.9			
Void ratio	0.7389			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: LO G SASI W/ TR CL, ML

LL = NP	**PL =**	**PI =** NP	**Assumed GS=** 2.65	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-5-09

Remarks:
TYPE FAILURE: VERTICAL FRACTURES

ASTM D 2166

Client: URS

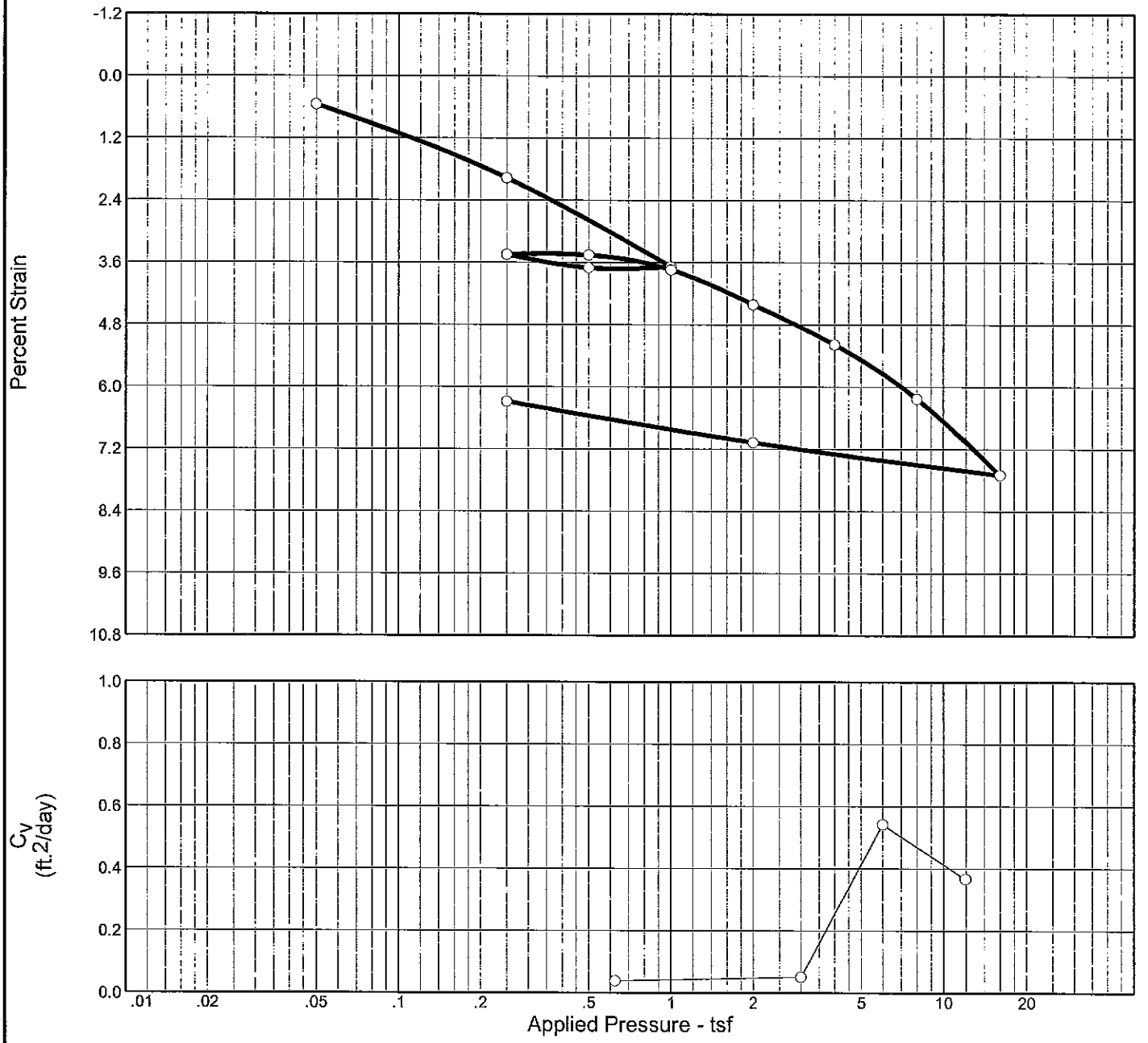
Project: BAYOU DUPONT

Source of Sample: B-3 **Depth:** 38-40
Sample Number: 11

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
96.3 %	27.0 %	94.8	NP	NP	2.65	(ML)		0.744

MATERIAL DESCRIPTION

G SASI W/ CL PKTS, ML

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

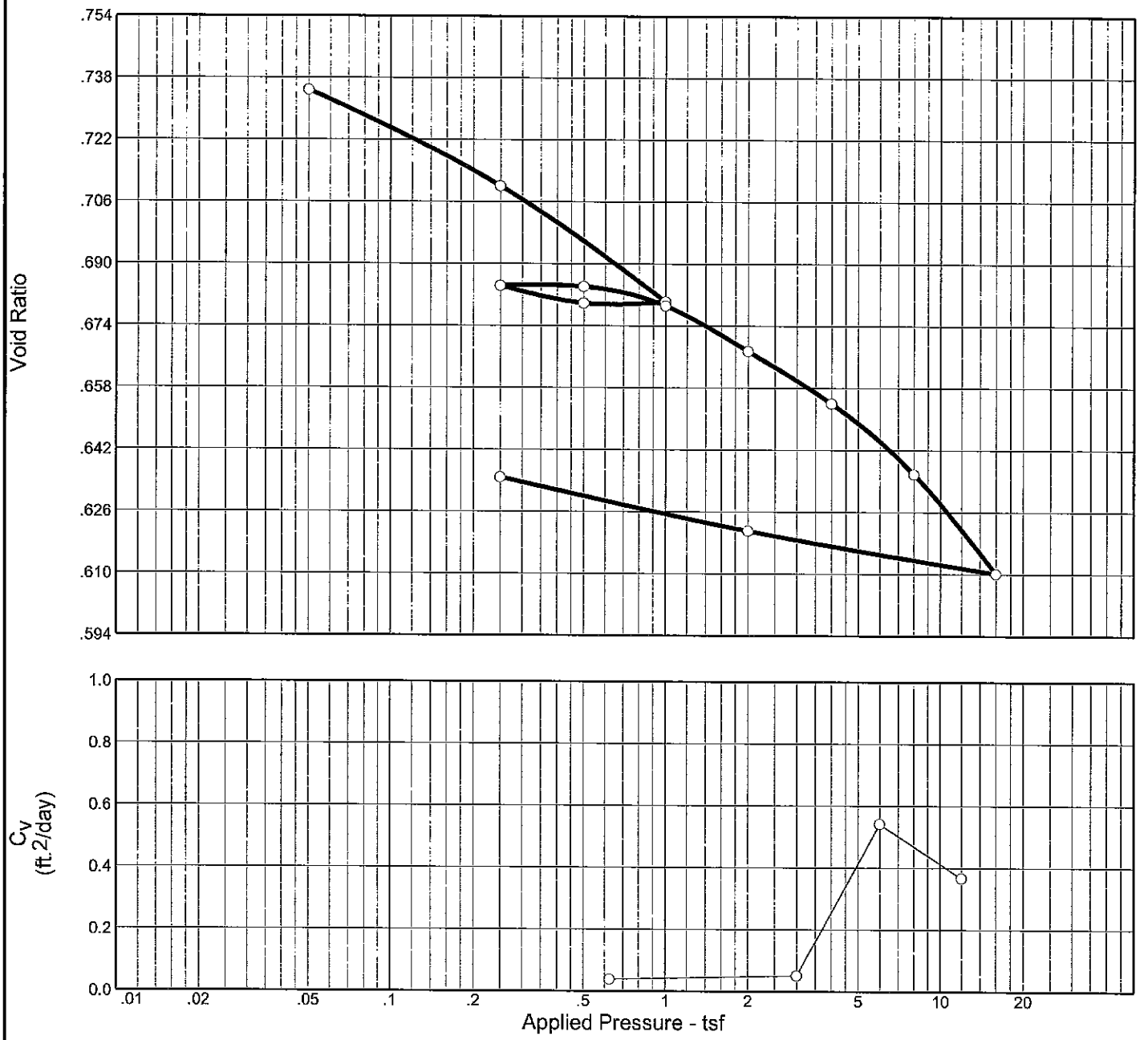
Source: B-3 **Sample No.:** 10 **Elev./Depth:** 33-35

Remarks:
ASTM D2435

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
96.3 %	27.0 %	94.8	NP	NP	2.65	(ML)		0.744

MATERIAL DESCRIPTION

G SASI W/ CL PKTS, ML

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-3 **Sample No.:** 10 **Elev./Depth:** 33-35

CONSOLIDATION/SWELL TEST REPORT

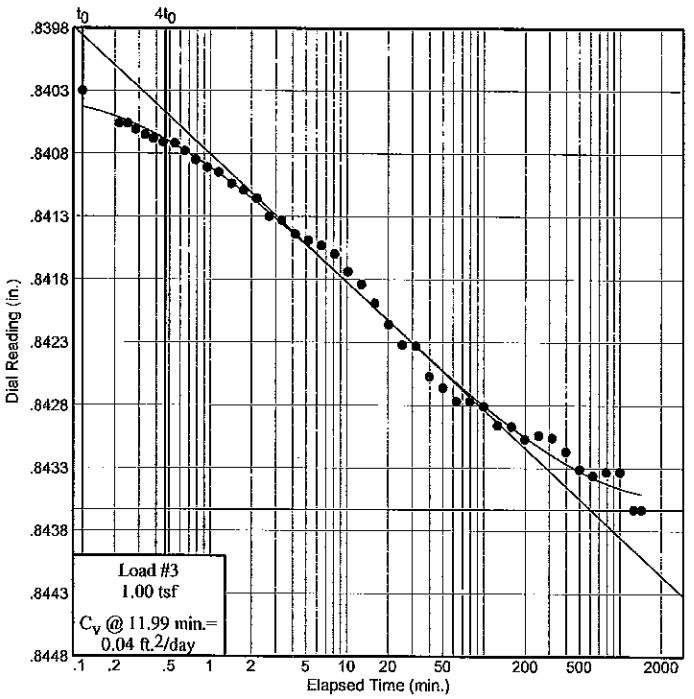
Southern Earth Sciences, Inc.

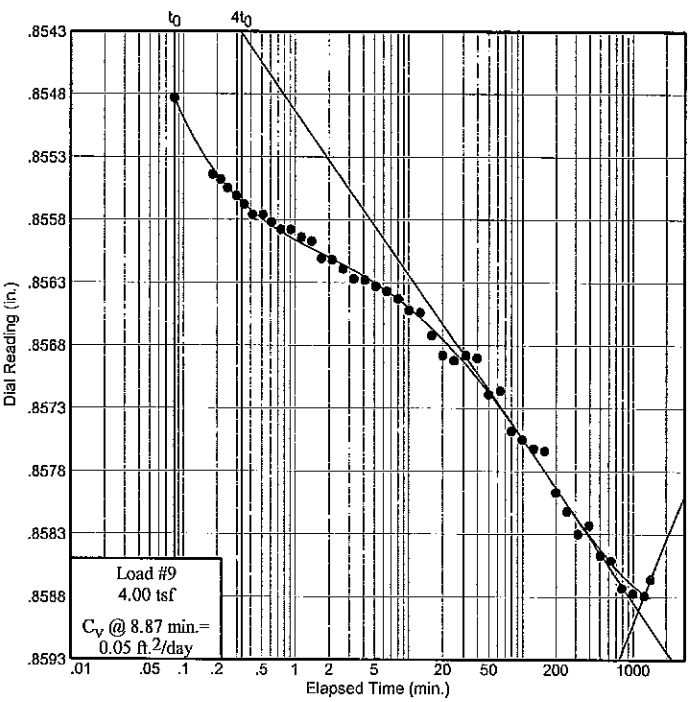
Remarks:
ASTM D2435

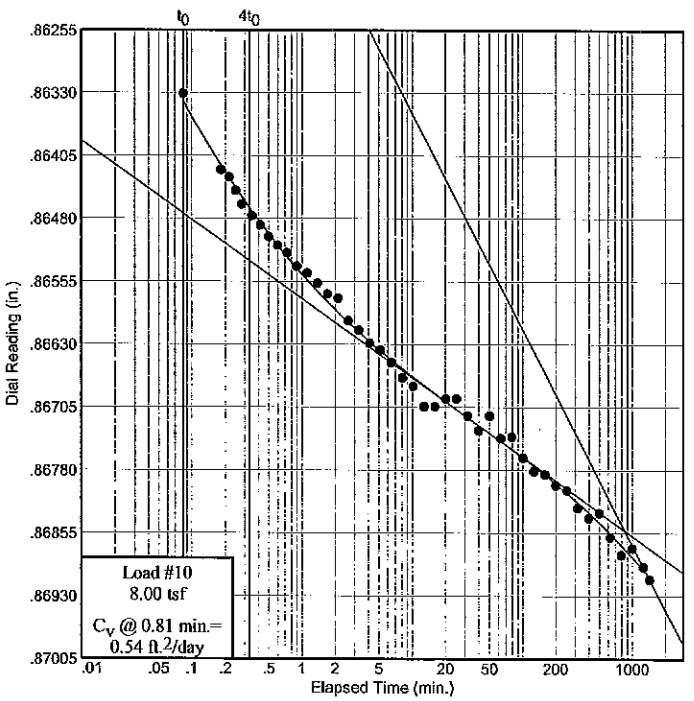
Dial Reading vs. Time

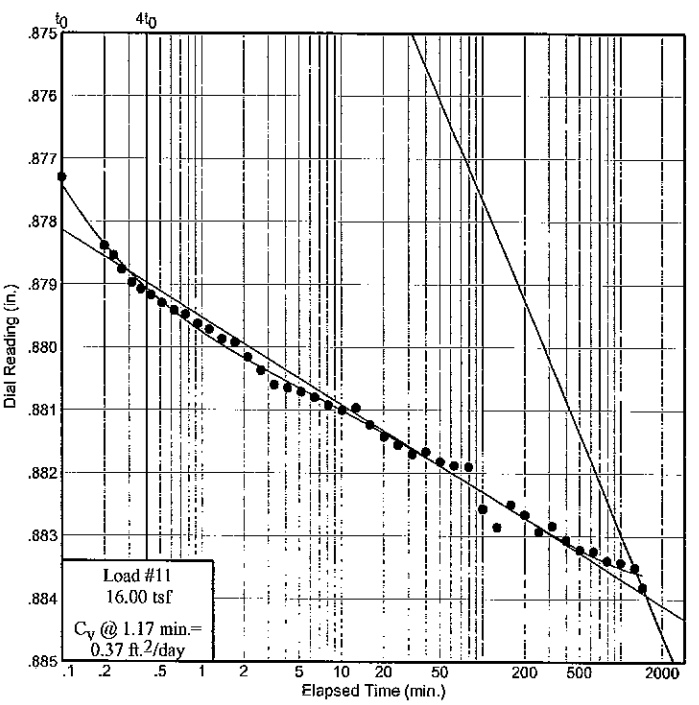
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-3 Sample No.: 10 Elev./Depth: 33-35









CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-3
Sample No.: 10
Elev. or Depth: 33-35 **Sample Length(in./cm.):**
Location:
Description: G SASI W/ CL PKTS, ML
Liquid Limit: NP **Plasticity Index:** NP
USCS: (ML) **AASHTO:** **Figure No.:** 1
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST		AFTER TEST	
Wet w+t =	207.51 g.	**Consolidometer #** =	1	**Wet w+t** =	155.49 g.
Dry w+t =	171.39 g.			**Dry w+t** =	123.31 g.
Tare Wt. =	37.82 g.	**Spec. Gravity** =	2.65	**Tare Wt.** =	.00 g.
Height =	1.00 in.	**Height** =	1.00 in.		
Diameter =	2.50 in.	**Diameter** =	2.50 in.		
Weight =	155.24 g.	**Defl. Table** =	Sigma 1 2.5in		
Moisture =	27.0 %	**Ht. Solids** =	0.5732 in.	**Moisture** =	26.1 %
Wet Den. =	120.5 pcf	**Dry Wt.** =	122.20 g.*	**Dry Wt.** =	123.31 g.
Dry Den. =	94.8 pcf	**Void Ratio** =	0.744	**Void Ratio** =	0.635
		Saturation =	96.3 %		

*** Initial dry weight used in calculations**

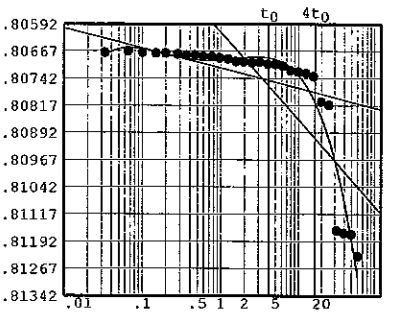
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.80680				0.744	
0.05	0.81243	0.00010		0.002	0.735	0.6 Comprs.
0.25	0.82975	0.00320		0.004	0.710	2.0 Comprs.
1.00	0.84963	0.00600	0.04	0.000	0.680	3.7 Comprs.
0.50	0.84814	0.00430		0.000	0.680	3.7 Comprs.
0.25	0.84648	0.00520			0.684	3.4 Comprs.
0.50	0.84740	0.00600		0.002	0.684	3.5 Comprs.
1.00	0.85093	0.00670	0.07	0.000	0.679	3.7 Comprs.
2.00	0.85893	0.00800		0.002	0.667	4.4 Comprs.
4.00	0.86866	0.01000	0.05		0.654	5.2 Comprs.
8.00	0.88160	0.01250	0.54	0.003	0.636	6.2 Comprs.
16.00	0.89891	0.01510	0.37	0.006	0.610	7.7 Comprs.
2.00	0.88554	0.00800	0.78		0.621	7.1 Comprs.
0.25	0.87665	0.00700	0.02		0.635	6.3 Comprs.

C_c = 0.09 P_c = 8.31 tsf C_r = 0.01

Pressure: 0.05 tsf **TEST READINGS** **Load No. 1**

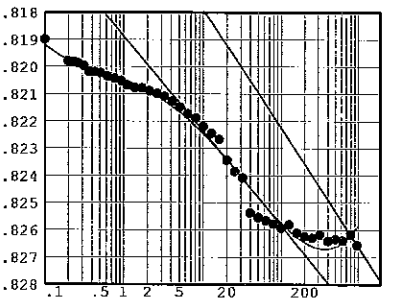
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.80680	16	2.50	0.80709
2	0.03	0.80681	17	3.15	0.80708
3	0.07	0.80677	18	3.98	0.80713
4	0.10	0.80681	19	5.02	0.80713
5	0.15	0.80683	20	6.32	0.80718
6	0.20	0.80683	21	7.95	0.80731
7	0.28	0.80686	22	10.02	0.80734
8	0.37	0.80688	23	12.62	0.80739
9	0.47	0.80688	24	15.88	0.80747
10	0.60	0.80692	25	19.98	0.80817
11	0.77	0.80693	26	25.15	0.80826
12	0.97	0.80696	27	31.67	0.81172
13	1.23	0.80699	28	39.85	0.81179
14	1.57	0.80706	29	50.17	0.81183
15	1.98	0.80707	30	60.45	0.81243



Void Ratio = 0.735 **Compression** = 0.6 %

Pressure: 0.25 tsf **TEST READINGS** **Load No. 2**

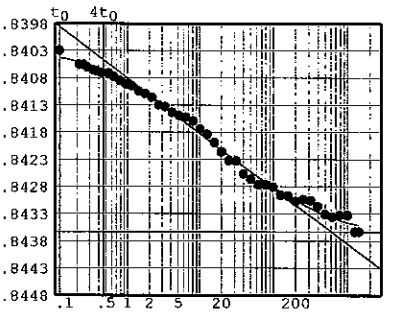
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.81243	23	10.17	0.82540
2	0.10	0.82219	24	12.77	0.82565
3	0.20	0.82299	25	16.03	0.82587
4	0.23	0.82302	26	20.13	0.82663
5	0.27	0.82307	27	25.30	0.82705
6	0.32	0.82317	28	31.82	0.82729
7	0.37	0.82337	29	40.00	0.82857
8	0.43	0.82340	30	50.32	0.82874
9	0.52	0.82343	31	63.30	0.82886
10	0.63	0.82355	32	79.63	0.82897
11	0.77	0.82363	33	100.22	0.82913
12	0.93	0.82372	34	126.10	0.82900
13	1.13	0.82388	35	158.70	0.82931
14	1.40	0.82397	36	199.75	0.82944
15	1.73	0.82399	37	251.42	0.82950
16	2.15	0.82409	38	316.45	0.82938
17	2.67	0.82419	39	398.35	0.82960
18	3.32	0.82430	40	501.42	0.82953
19	4.13	0.82447	41	631.20	0.82959
20	5.17	0.82468	42	794.57	0.82937
21	6.47	0.82493	43	971.10	0.82975
22	8.12	0.82509			



Void Ratio = 0.710 **Compression** = 2.0 %

Pressure: 1.00 tsf **TEST READINGS** **Load No. 3**

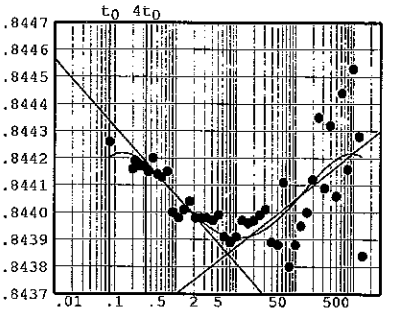
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.84307	24	12.82	0.84784
2	0.12	0.84630	25	16.08	0.84799
3	0.22	0.84656	26	20.20	0.84816
4	0.25	0.84656	27	25.37	0.84832
5	0.28	0.84661	28	31.87	0.84833
6	0.33	0.84665	29	40.07	0.84857
7	0.38	0.84668	30	50.37	0.84866
8	0.45	0.84671	31	63.35	0.84877
9	0.55	0.84672	32	79.70	0.84877
10	0.65	0.84678	33	100.27	0.84881
11	0.78	0.84685	34	126.17	0.84896
12	0.95	0.84691	35	158.77	0.84897
13	1.15	0.84695	36	199.80	0.84907
14	1.43	0.84704	37	251.47	0.84904
15	1.75	0.84709	38	316.52	0.84906
16	2.18	0.84716	39	398.40	0.84917
17	2.70	0.84730	40	501.48	0.84931
18	3.35	0.84733	41	631.27	0.84936
19	4.18	0.84744	42	794.63	0.84933
20	5.22	0.84749	43	1000.32	0.84933
21	6.52	0.84753	44	1259.25	0.84963
22	8.17	0.84760	45	1440.33	0.84963
23	10.22	0.84774			



Void Ratio = 0.680 **Compression =** 3.7 %
D_0 = 0.84017 D_{50} = 0.84190 D_{100} = 0.84363
C_v **at 12.0 min.** = 0.04 ft.^{2}/day C_α = 0.000

Pressure: 0.50 tsf | **TEST READINGS** | **Load No. 4**

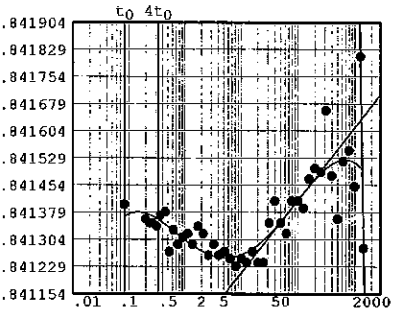
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.84960	24	12.77	0.84827
2	0.08	0.84856	25	16.03	0.84826
3	0.20	0.84846	26	20.13	0.84827
4	0.22	0.84849	27	25.32	0.84829
5	0.27	0.84847	28	31.82	0.84831
6	0.30	0.84847	29	40.02	0.84819
7	0.37	0.84845	30	50.33	0.84818
8	0.43	0.84850	31	63.32	0.84841
9	0.52	0.84844	32	79.65	0.84810
10	0.62	0.84843	33	100.23	0.84818
11	0.75	0.84845	34	126.13	0.84825
12	0.92	0.84830	35	158.72	0.84830
13	1.13	0.84828	36	199.77	0.84842
14	1.40	0.84831	37	251.43	0.84865
15	1.73	0.84834	38	316.48	0.84839
16	2.13	0.84828	39	398.35	0.84862
17	2.65	0.84828	40	501.43	0.84836
18	3.32	0.84828	41	631.22	0.84874
19	4.13	0.84827	42	794.58	0.84846
20	5.17	0.84829	43	1000.27	0.84883
21	6.47	0.84821	44	1259.20	0.84858
22	8.12	0.84819	45	1440.30	0.84814
23	10.17	0.84821			



Void Ratio = 0.680 **Compression** = 3.7 %

Pressure: 0.25 tsf **TEST READINGS** **Load No. 5**

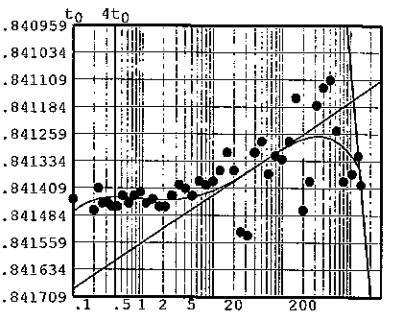
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.84814	24	12.78	0.84644
2	0.08	0.84660	25	16.05	0.84647
3	0.20	0.84656	26	20.15	0.84644
4	0.23	0.84655	27	25.32	0.84644
5	0.27	0.84655	28	31.83	0.84655
6	0.32	0.84654	29	40.02	0.84661
7	0.37	0.84657	30	50.33	0.84655
8	0.45	0.84658	31	63.32	0.84652
9	0.53	0.84647	32	79.67	0.84661
10	0.63	0.84653	33	100.23	0.84661
11	0.77	0.84649	34	126.13	0.84659
12	0.93	0.84651	35	158.73	0.84667
13	1.15	0.84652	36	199.77	0.84670
14	1.40	0.84649	37	251.43	0.84669
15	1.73	0.84654	38	316.48	0.84686
16	2.15	0.84652	39	398.37	0.84668
17	2.67	0.84646	40	501.45	0.84656
18	3.33	0.84649	41	631.22	0.84672
19	4.15	0.84646	42	794.60	0.84675
20	5.20	0.84647	43	1000.27	0.84665
21	6.50	0.84645	44	1259.20	0.84701
22	8.13	0.84643	45	1440.48	0.84648
23	10.18	0.84645			



Void Ratio = 0.684 **Compression** = 3.4 %

Pressure: 0.50 tsf **TEST READINGS** **Load No. 6**

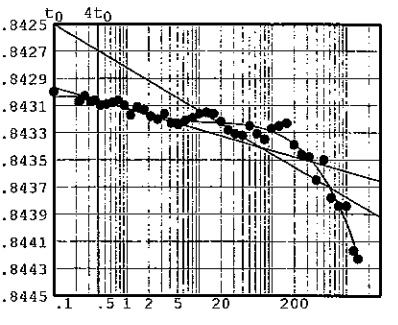
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.84650	24	12.78	0.84736
2	0.10	0.84744	25	16.05	0.84731
3	0.20	0.84747	26	20.15	0.84736
4	0.23	0.84741	27	25.32	0.84753
5	0.27	0.84745	28	31.83	0.84754
6	0.32	0.84745	29	40.02	0.84731
7	0.37	0.84746	30	50.33	0.84728
8	0.43	0.84746	31	63.32	0.84737
9	0.52	0.84743	32	79.67	0.84732
10	0.63	0.84745	33	100.23	0.84733
11	0.77	0.84743	34	126.13	0.84728
12	0.93	0.84742	35	158.73	0.84716
13	1.13	0.84745	36	199.78	0.84747
14	1.40	0.84744	37	251.45	0.84739
15	1.73	0.84746	38	316.48	0.84718
16	2.15	0.84746	39	398.37	0.84713
17	2.67	0.84743	40	501.45	0.84711
18	3.33	0.84740	41	631.23	0.84725
19	4.15	0.84741	42	794.60	0.84739
20	5.18	0.84743	43	1060.28	0.84737
21	6.48	0.84739	44	1319.22	0.84732
22	8.13	0.84740	45	1440.37	0.84740
23	10.18	0.84739			



Void Ratio = 0.684 **Compression =** 3.5 %

Pressure: 1.00 tsf	TEST READINGS	Load No. 7

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.84742	24	12.78	0.84985
2	0.10	0.84970	25	16.05	0.84986
3	0.22	0.84977	26	20.15	0.84992
4	0.23	0.84976	27	25.33	0.84998
5	0.27	0.84973	28	31.83	0.85001
6	0.32	0.84977	29	40.02	0.85002
7	0.37	0.84976	30	50.35	0.84995
8	0.43	0.84980	31	63.33	0.85001
9	0.53	0.84979	32	79.67	0.85005
10	0.63	0.84978	33	100.23	0.84997
11	0.77	0.84976	34	126.15	0.84995
12	0.93	0.84980	35	158.75	0.84993
13	1.13	0.84987	36	199.78	0.85009
14	1.40	0.84981	37	251.45	0.85016
15	1.73	0.84983	38	316.50	0.85018
16	2.15	0.84988	39	398.37	0.85035
17	2.68	0.84990	40	501.45	0.85020
18	3.33	0.84986	41	631.23	0.85048
19	4.15	0.84993	42	794.62	0.85054
20	5.18	0.84994	43	1000.28	0.85054
21	6.48	0.84991	44	1259.22	0.85087
22	8.13	0.84989	45	1440.48	0.85093
23	10.18	0.84986			



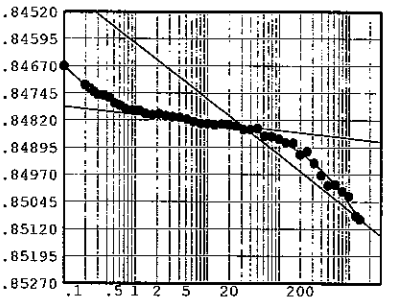
Void Ratio = 0.679 **Compression =** 3.7 %

D_0 = 0.84302 D_{50} = 0.84321 D_{100} = 0.84341

C_v **at 6.7 min.** = 0.07 ft.^{2}/day C_α = 0.000

Pressure: 2.00 tsf | TEST READINGS | Load No. 8

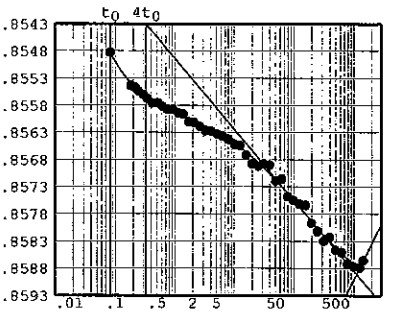
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.85093	24	12.77	0.85633
2	0.10	0.85470	25	16.03	0.85631
3	0.20	0.85522	26	20.15	0.85633
4	0.23	0.85533	27	25.32	0.85636
5	0.27	0.85542	28	31.82	0.85646
6	0.30	0.85550	29	40.02	0.85646
7	0.37	0.85552	30	50.33	0.85643
8	0.43	0.85557	31	63.32	0.85663
9	0.52	0.85573	32	79.65	0.85665
10	0.62	0.85579	33	100.23	0.85672
11	0.75	0.85590	34	126.13	0.85682
12	0.92	0.85592	35	158.73	0.85683
13	1.13	0.85593	36	199.77	0.85715
14	1.40	0.85602	37	251.43	0.85706
15	1.73	0.85606	38	316.48	0.85739
16	2.15	0.85603	39	398.37	0.85772
17	2.67	0.85608	40	501.45	0.85800
18	3.32	0.85611	41	631.22	0.85798
19	4.15	0.85613	42	794.60	0.85817
20	5.18	0.85617	43	1000.27	0.85830
21	6.48	0.85624	44	1259.20	0.85884
22	8.12	0.85630	45	1440.45	0.85893
23	10.18	0.85630			



Void Ratio = 0.667 **Compression** = 4.4 %

Pressure: 4.00 tsf **TEST READINGS** **Load No. 9**

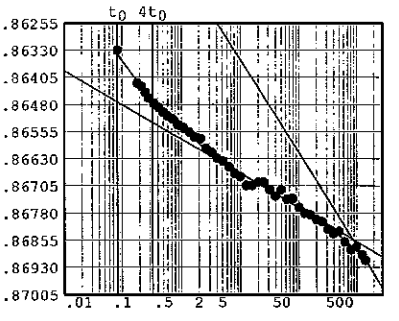
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.85888	24	12.75	0.86654
2	0.08	0.86483	25	16.02	0.86672
3	0.18	0.86544	26	20.12	0.86688
4	0.22	0.86548	27	25.28	0.86692
5	0.25	0.86555	28	31.78	0.86688
6	0.30	0.86561	29	39.98	0.86690
7	0.35	0.86568	30	50.30	0.86719
8	0.42	0.86576	31	63.28	0.86716
9	0.52	0.86576	32	79.62	0.86748
10	0.62	0.86582	33	100.20	0.86755
11	0.75	0.86588	34	126.10	0.86762
12	0.92	0.86588	35	158.68	0.86764
13	1.13	0.86594	36	199.73	0.86797
14	1.40	0.86597	37	251.40	0.86812
15	1.72	0.86611	38	316.45	0.86830
16	2.13	0.86612	39	398.32	0.86823
17	2.65	0.86619	40	501.40	0.86847
18	3.32	0.86627	41	631.18	0.86851
19	4.13	0.86628	42	794.57	0.86873
20	5.17	0.86633	43	1000.23	0.86877
21	6.47	0.86637	44	1259.17	0.86879
22	8.10	0.86643	45	1440.45	0.86866
23	10.15	0.86652			



Void Ratio = 0.654 **Compression** = 5.2 %
D_0 = 0.85401 D_{50} = 0.85646 D_{100} = 0.85890
C_v **at 8.9 min.** = 0.05 ft.^{2}/day

Pressure: 8.00 tsf | TEST READINGS | Load No. 10

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.86868	24	12.77	0.87954
2	0.08	0.87581	25	16.03	0.87954
3	0.18	0.87672	26	20.13	0.87945
4	0.22	0.87681	27	25.30	0.87945
5	0.25	0.87697	28	31.82	0.87965
6	0.28	0.87713	29	40.00	0.87983
7	0.35	0.87727	30	50.32	0.87965
8	0.42	0.87738	31	63.30	0.87992
9	0.50	0.87752	32	79.63	0.87990
10	0.60	0.87762	33	100.20	0.88015
11	0.73	0.87771	34	126.10	0.88031
12	0.90	0.87787	35	158.70	0.88035
13	1.12	0.87795	36	199.75	0.88048
14	1.38	0.87807	37	251.42	0.88054
15	1.72	0.87820	38	316.45	0.88075
16	2.13	0.87825	39	398.33	0.88087
17	2.65	0.87852	40	501.42	0.88081
18	3.30	0.87863	41	631.20	0.88110
19	4.12	0.87879	42	794.57	0.88131
20	5.15	0.87887	43	1000.25	0.88123
21	6.47	0.87902	44	1259.18	0.88145
22	8.10	0.87920	45	1440.00	0.88160
23	10.17	0.87930			



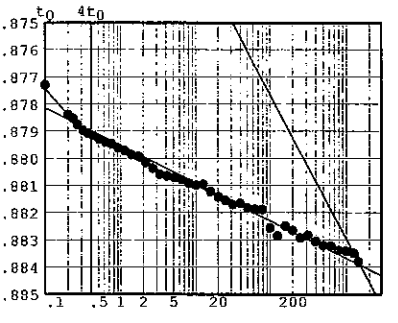
Void Ratio = 0.636 **Compression** = 6.2 %

D_0 = 0.86213 D_{50} = 0.86532 D_{100} = 0.86852

C_v **at 0.8 min.** = 0.54 ft.^{2}/day C_α = 0.003

Pressure: 16.00 tsf **TEST READINGS** **Load No. 11**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.88158	24	12.77	0.89606
2	0.10	0.89240	25	16.03	0.89633
3	0.20	0.89349	26	20.15	0.89652
4	0.23	0.89364	27	25.32	0.89665
5	0.27	0.89386	28	31.82	0.89680
6	0.32	0.89407	29	40.02	0.89676
7	0.37	0.89418	30	50.32	0.89692
8	0.43	0.89427	31	63.30	0.89698
9	0.52	0.89440	32	79.65	0.89700
10	0.63	0.89451	33	100.22	0.89767
11	0.77	0.89458	34	126.12	0.89796
12	0.93	0.89473	35	158.72	0.89760
13	1.13	0.89482	36	199.75	0.89776
14	1.40	0.89497	37	251.42	0.89803
15	1.73	0.89503	38	316.47	0.89794
16	2.15	0.89526	39	398.35	0.89816
17	2.67	0.89547	40	501.43	0.89832
18	3.32	0.89570	41	631.20	0.89834
19	4.15	0.89575	42	794.58	0.89849
20	5.18	0.89581	43	1000.25	0.89852
21	6.48	0.89590	44	1259.18	0.89860
22	8.12	0.89602	45	1440.15	0.89891
23	10.18	0.89610			



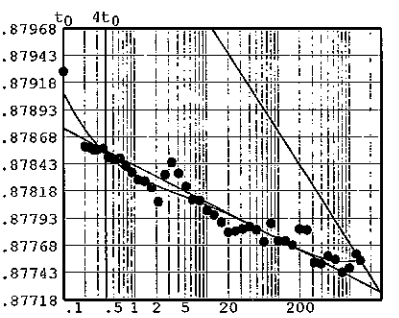
Void Ratio = 0.610 **Compression =** 7.7 %

D_0 = 0.87577 D_{50} = 0.87985 D_{100} = 0.88393

C_v **at 1.2 min.** = 0.37 ft.^{2}/day C_α = 0.006

Pressure: 2.00 tsf **TEST READINGS** **Load No. 12**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.89892	24	12.78	0.88596
2	0.10	0.88728	25	16.05	0.88589
3	0.20	0.88659	26	20.15	0.88580
4	0.23	0.88658	27	25.33	0.88581
5	0.27	0.88656	28	31.85	0.88583
6	0.30	0.88656	29	40.03	0.88585
7	0.37	0.88657	30	50.35	0.88582
8	0.43	0.88649	31	63.33	0.88571
9	0.52	0.88647	32	79.67	0.88588
10	0.63	0.88648	33	100.25	0.88572
11	0.77	0.88641	34	126.15	0.88572
12	0.93	0.88635	35	158.75	0.88568
13	1.13	0.88628	36	199.78	0.88583
14	1.40	0.88627	37	251.45	0.88582
15	1.73	0.88621	38	316.48	0.88552
16	2.15	0.88608	39	398.38	0.88551
17	2.67	0.88633	40	501.45	0.88558
18	3.33	0.88644	41	631.23	0.88555
19	4.15	0.88634	42	794.60	0.88543
20	5.18	0.88622	43	1000.28	0.88547
21	6.48	0.88610	44	1259.22	0.88560
22	8.13	0.88609	45	1440.10	0.88554
23	10.18	0.88600			



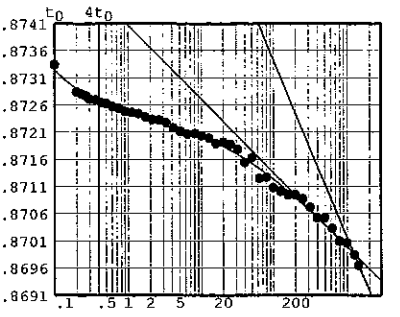
Void Ratio = 0.621 **Compression =** 7.1 %

D_0 = 0.87965 D_{50} = 0.87845 D_{100} = 0.87725

C_v **at 0.5 min.** = 0.78 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 13**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.88555	24	12.77	0.87899
2	0.10	0.88034	25	16.03	0.87889
3	0.20	0.87984	26	20.13	0.87891
4	0.23	0.87980	27	25.32	0.87887
5	0.27	0.87977	28	31.82	0.87878
6	0.30	0.87971	29	40.02	0.87854
7	0.37	0.87969	30	50.32	0.87863
8	0.43	0.87964	31	63.30	0.87825
9	0.52	0.87962	32	79.65	0.87827
10	0.62	0.87957	33	100.22	0.87808
11	0.75	0.87953	34	126.12	0.87801
12	0.92	0.87948	35	158.72	0.87794
13	1.13	0.87946	36	199.75	0.87795
14	1.40	0.87944	37	251.42	0.87787
15	1.73	0.87938	38	316.47	0.87772
16	2.15	0.87933	39	398.35	0.87752
17	2.67	0.87932	40	501.43	0.87752
18	3.32	0.87927	41	631.20	0.87733
19	4.13	0.87918	42	794.58	0.87709
20	5.17	0.87911	43	1000.25	0.87706
21	6.47	0.87906	44	1259.18	0.87684
22	8.12	0.87907	45	1440.00	0.87665
23	10.17	0.87903			



Void Ratio = 0.635 **Compression =** 6.3 %
D_0 = 0.87382 **D_{50} =** 0.87184 **D_{100} =** 0.86986
C_v at 19.7 min. = 0.02 ft.^{2}/day

Southern Earth Sciences, Inc.

Laboratory Test Results

Project: **Bayou DuPont** | **Technical Responsibility:** | **Quality Assurance Officer**

Client: URS

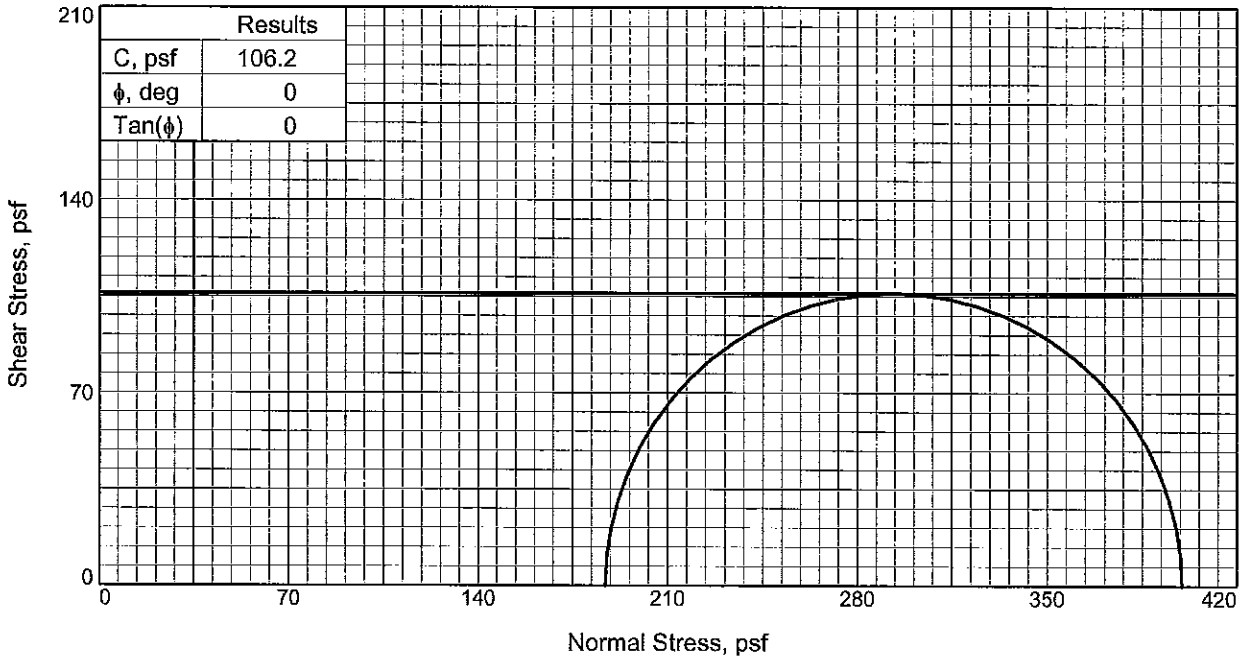
7389 Florida Blvd., Suite 300, Baton Rouge, LA 70806 | Project No.: **B09-012** | PM: S. Aviles | Date of Issue: 3/12/2009

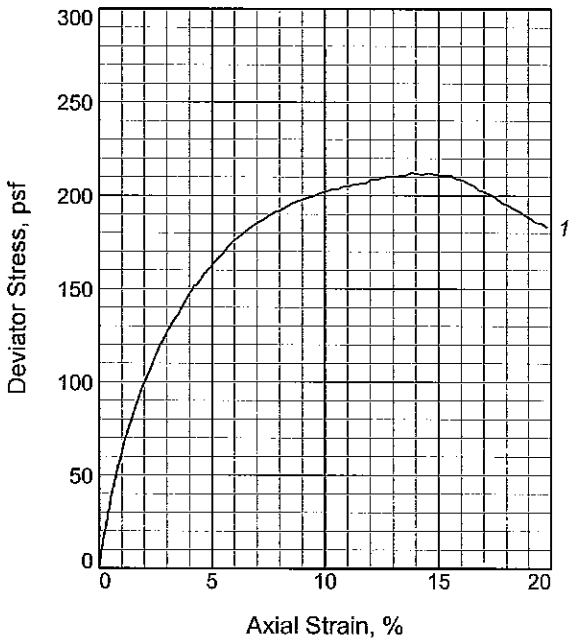
			ASTM DESIGNATION																
			D2216	D4318			D427	D2166		D2166	D2850	D422, C136 or C117					D2974	USCS	
				Atterberg Limits						Cohesion		Grain Size (% Passing)							
Boring No.	Depth (ft)	Classification	ω %	LL	PL	PI	SL	γ_{wet} pcf	γ_{dry} pcf	U psf	UU psf	Gravel	Sand	Silt	Clay	#200	Organic Content %		Confining Stress, Resistivity and Remarks
B-4	0-2	PEAT with Clay	860.0	958	531	427											64.3	(PT)	
B-4	2-4	Very Soft, Dark Gray and Gray CLAY with organic pockets	333.3	482	96	386	11.0	73.9	17.0		106.2							(OH)	Confining Pressure: 1.3 psi
B-4	4-6	Very Soft, Gray CLAY with organic pockets	80.4	122	39	83		101.7	56.4	69.6								(CH)	
B-4	6-8	Very Soft, Gray CLAY with organic pockets and trace shells	71.9	64	23	41		84.1	47.9		57.4		2.3	50.7	47.0		6.4	(CH)	Specific Gravity: 2.780 Confining Pressure: 2.6 psi
B-4	8-10	Very Soft CLAY with silt and organic pockets and shells	89.6				4.5	94.7	50.0	71.0								(CH)	
B-4	13-15	Very Soft, Gray CLAY with organics and silty clay	113.8	91	33	58		95.5	44.6		97.9		1.2	44.4	54.4			(CH)	Confining Pressure: 5.0 psi
B-4	18-20	Very Soft CLAY with silt and organic pockets	91.4					95.9	50.1	93.7							4.1	(CH)	
B-4	23-25	Very Soft, Gray CLAY with organic pockets, sandy silt and silty sand layers	97.3	101	39	62	16.4	111.7	55.0		97.5		2.7	87.2	10.1		3.7	(CH)	Specific Gravity: 2.780 Confining Pressure: 8.2 psi
B-4	28-30	Firm, Gray CLAYEY SILT	30.0					119.7	92.0	869.0								(ML)	
B-4	33-35	Firm, Gray SANDY SILT with clay	28.0	NP	NP	NP		126.7	99.0		1076.1		12.6	77.2	10.2			(ML)	Confining Pressure: 11.5 psi
B-4	38-40	Soft, Gray CLAY	62.7	63	24	39		106.9	65.7	379.1								(CH)	

Geotechnical Lab
11638 Sun Belt Ct. Baton Rouge, LA 70809

The results presented only relate to those samples tested

Date Samples Rec.:
Date Testing Initiated:





Sample No.		1
Initial	Water Content, %	333.3
	Dry Density, pcf	17.0
	Saturation, %	102.7
	Void Ratio	7.7906
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	333.3
	Dry Density, pcf	17.0
	Saturation, %	102.7
	Void Ratio	7.7906
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		1.300
Fail. Stress, psf		212.4
Strain, %		13.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		399.6
σ_3 Failure, psf		187.2

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO G ORCL W/ ORGPKTS

LL= 482 **PL=** 96 **PI=** 386
Assumed Specific Gravity= 2.40
Remarks: BULGE FAILURE
SL: 11.0

ASTM D 2850

Client: URS

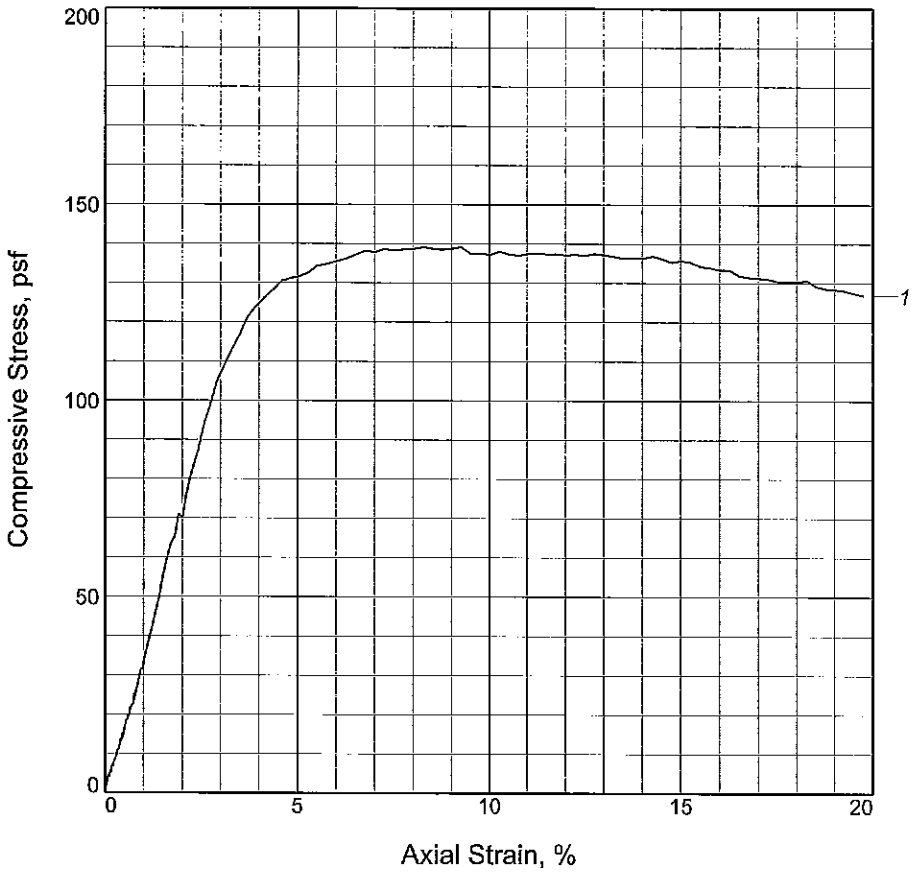
Project: BAYOU DUPONT

Source of Sample: B-4 **Depth:** 2-4
Sample Number: 2
Proj. No.: B09-012 **Date Sampled:** 3-11-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	139.2			
Undrained shear strength, psf	69.6			
Failure strain, %	8.3			
Strain rate, %/min.	1.00			
Water content, %	80.4			
Wet density, pcf	101.7			
Dry density, pcf	56.4			
Saturation, %	108.1			
Void ratio	2.0451			
Specimen diameter, in.	2.750			
Specimen height, in.	5.940			
Height/diameter ratio	2.16			

Description: VSO G C W/ ORGPKTS

LL = 122	**PL** = 39	**PI** = 83	**Assumed GS=** 2.75	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3/11/09

Remarks:
BULGE FAILURE

ASTM D 2166

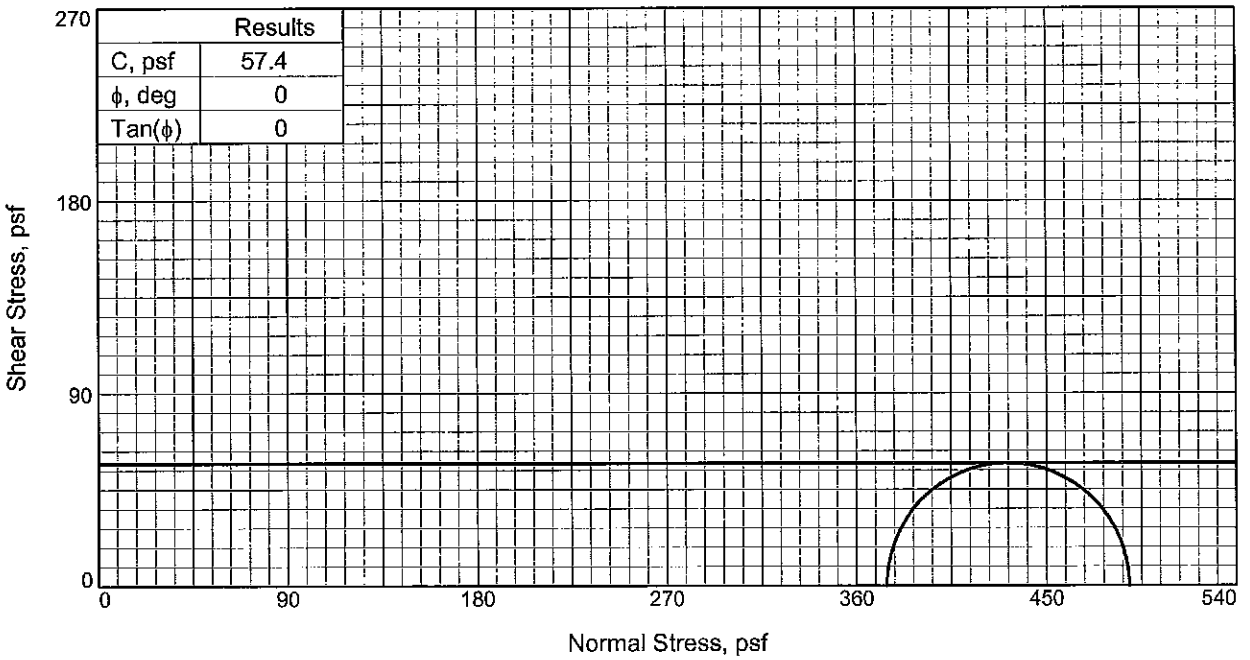
Client: URS

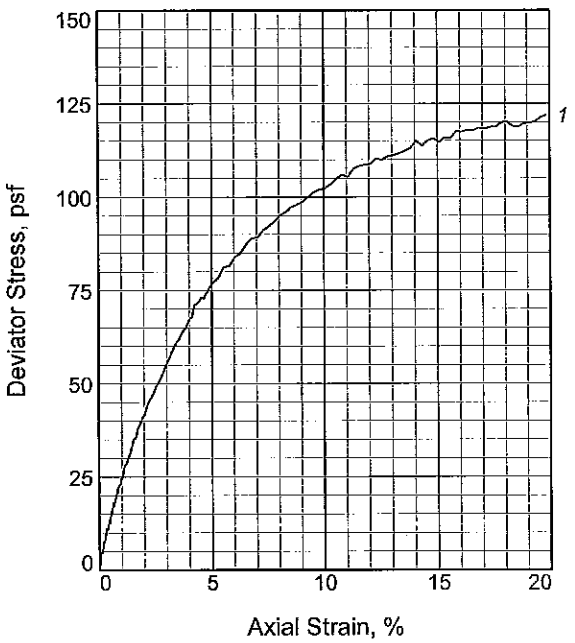
Project: BAYOU DUPONT

Source of Sample: B-4 **Depth:** 4-6
Sample Number: 3

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	71.9
	Dry Density, pcf	47.9
	Saturation, %	76.2
	Void Ratio	2.6254
	Diameter, in.	2.780
	Height, in.	5.940
At Test	Water Content, %	71.9
	Dry Density, pcf	47.9
	Saturation, %	76.2
	Void Ratio	2.6254
	Diameter, in.	2.780
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.600
Fail. Stress, psf		114.7
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		489.1
σ_3 Failure, psf		374.4

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ ORGPKTS & TRSHELLS

LL= 64 **PL=** 23 **PI=** 41

Specific Gravity= 2.78

Remarks:
BULGE FAILURE
ORGANIC CONTENT: 6.4%

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-4 **Depth:** 6-8

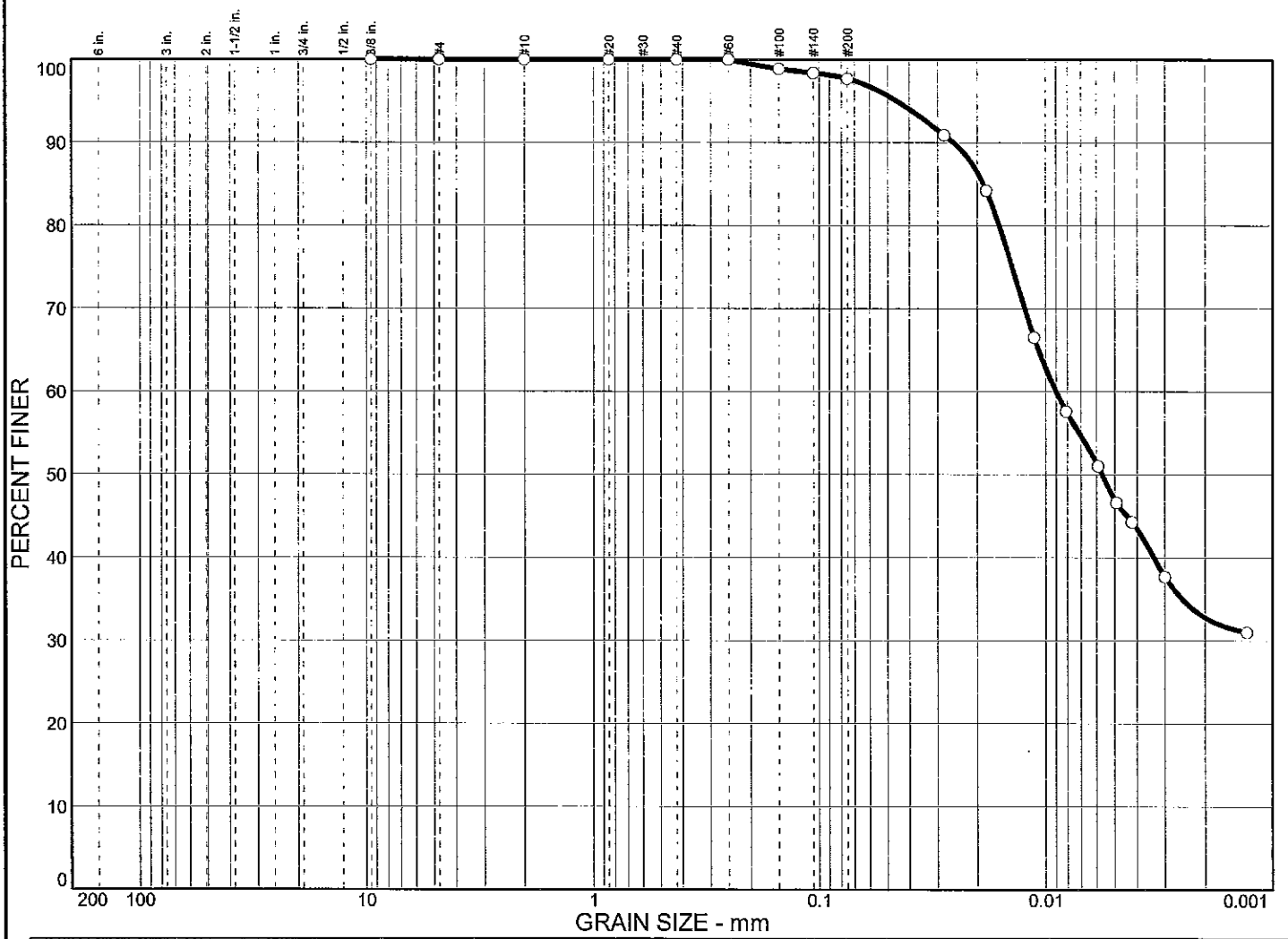
Sample Number: 4

Proj. No.: B09-012 **Date Sampled:** 3/11/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	2.3	50.7	47.0

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	64	41	0.0188	0.0090	0.0057					

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ ORGPKTS & TRSHELLS	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-4 **Sample No.:** 4 **Elev./Depth:** 6-8

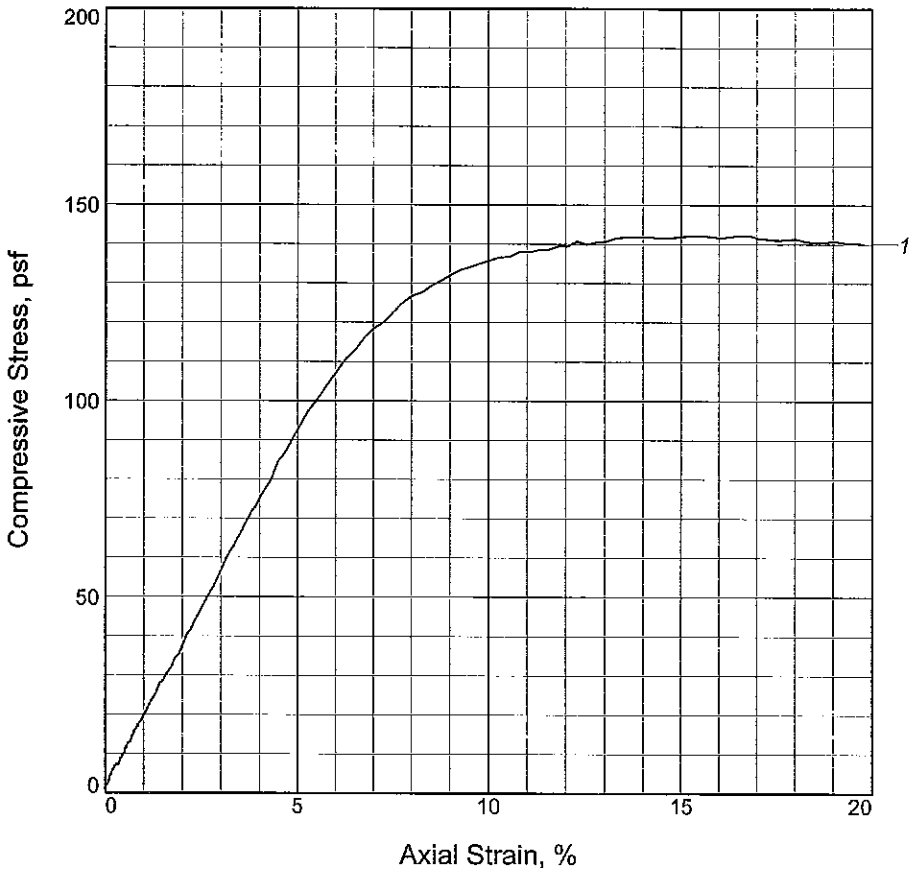
Remarks:

○ F.M.=0.01

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	142.0			
Undrained shear strength, psf	71.0			
Failure strain, %	15.0			
Strain rate, %/min.	1.00			
Water content, %	89.6			
Wet density, pcf	94.7			
Dry density, pcf	50.0			
Saturation, %	101.1			
Void ratio	2.4366			
Specimen diameter, in.	2.750			
Specimen height, in.	5.940			
Height/diameter ratio	2.16			

Description: VSO G CL W/ SIPKTS ORGPKTS & SHELLS

LL =	PL =	PI =	Assumed GS= 2.75	Type: UNDISTURBED

Project No.: B09-012
Date Sampled: 3/11/09

Remarks:
FAILURE: BULGE + MUILTISHEAR & FRACTURES
SL: 4.50

ASTM D 2166

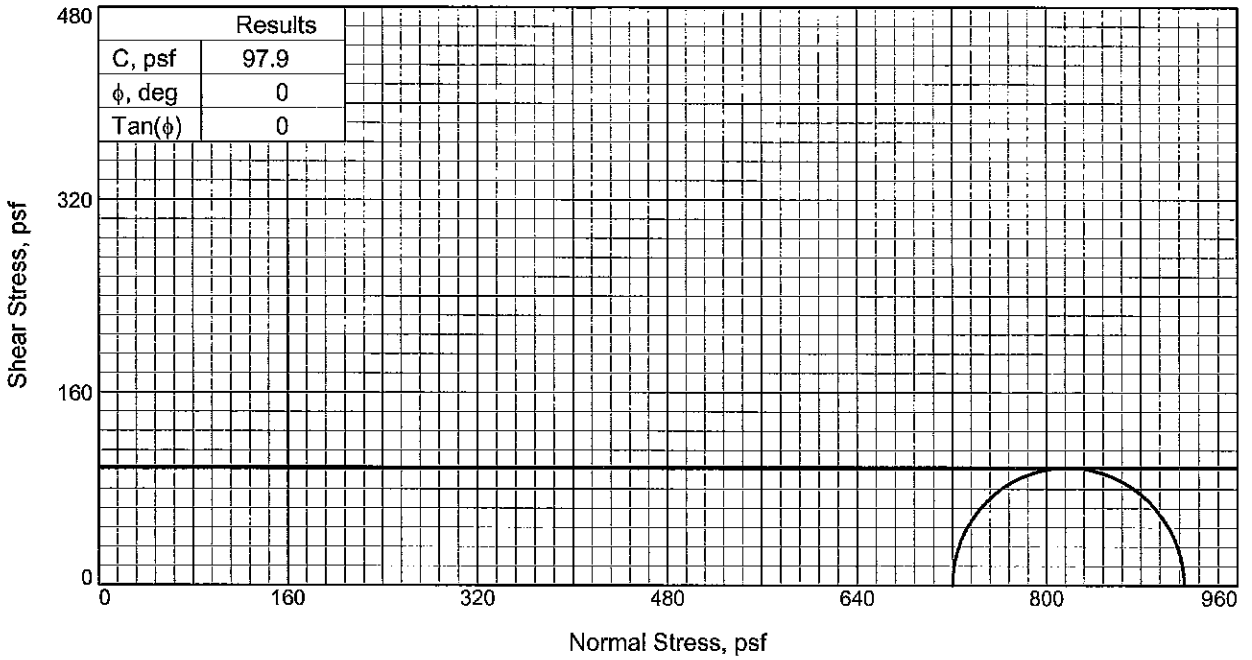
Client: URS

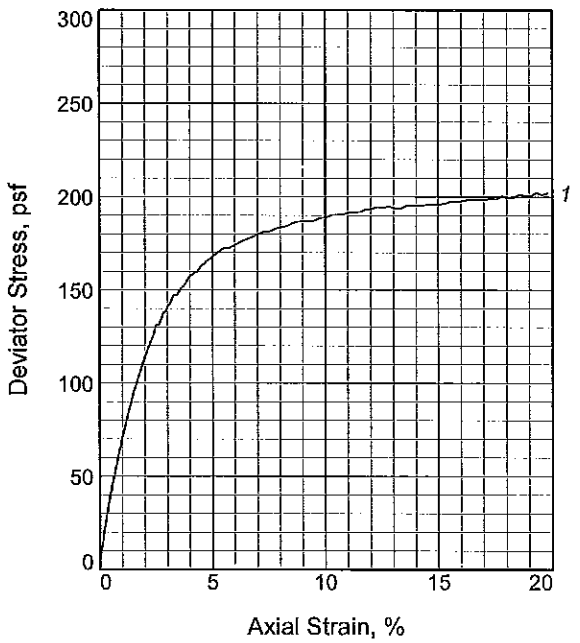
Project: BAYOU DUPONT

Source of Sample: B-4 **Depth:** 8-10
Sample Number: 5

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	113.8
	Dry Density, pcf	44.6
	Saturation, %	109.3
	Void Ratio	2.9156
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	113.8
	Dry Density, pcf	44.6
	Saturation, %	109.3
	Void Ratio	2.9156
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		5.000
Fail. Stress, psf		195.9
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		915.9
σ_3 Failure, psf		720.0

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO G CL W/ SICL & ORGS

LL= 91 **PL=** 33 **PI=** 58
Assumed Specific Gravity= 2.80
Remarks: BULGE FAILURE

ASTM D 2850

Client: URS

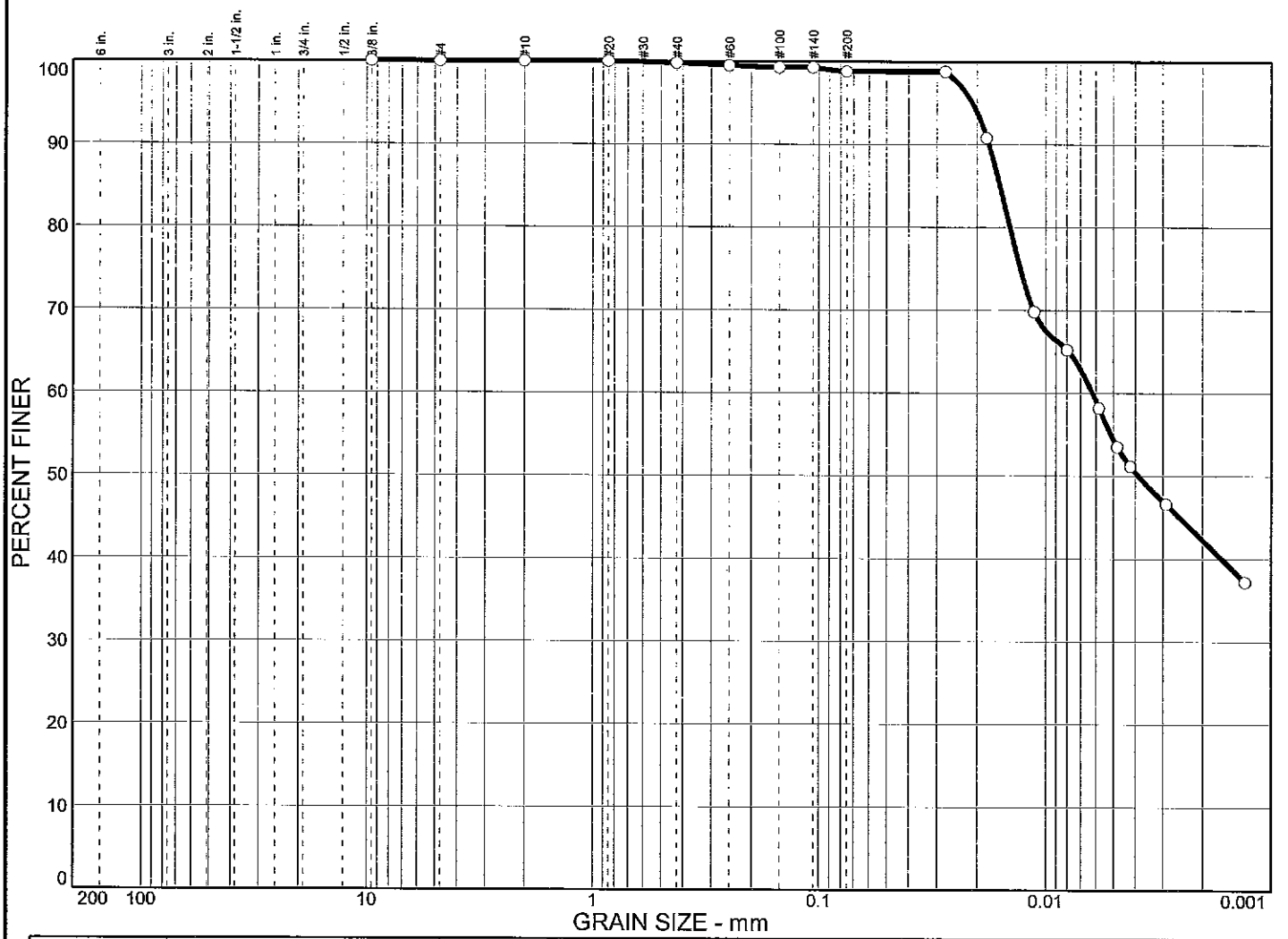
Project: BAYOU DUPONT

Source of Sample: B-4 **Depth:** 13-15
Sample Number: 6
Proj. No.: B09-012 **Date Sampled:** 3/11/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	1.2	44.4	54.4

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	91	58	0.0158	0.0062	0.0039					

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ SICL & ORGS	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-4 **Sample No.:** 6 **Elev./Depth:** 13-15

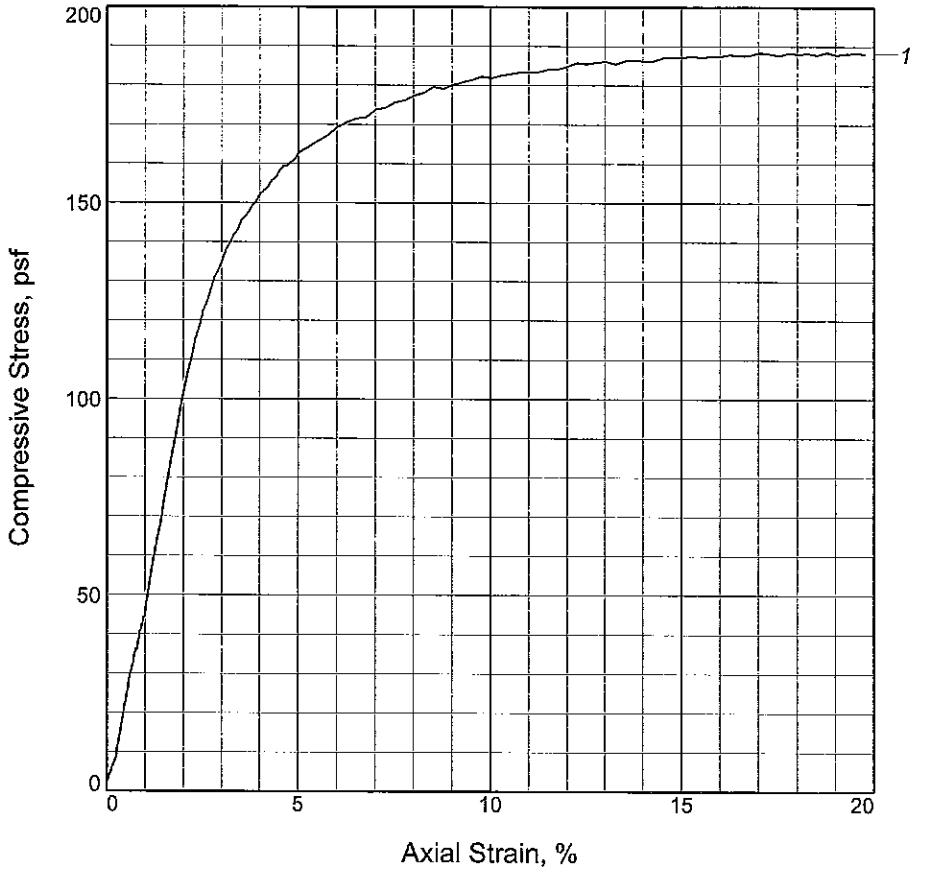
Remarks:

○ F.M.=0.01

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	187.3			
Undrained shear strength, psf	93.7			
Failure strain, %	15.0			
Strain rate, %/min.	1.00			
Water content, %	91.4			
Wet density, pcf	95.9			
Dry density, pcf	50.1			
Saturation, %	102.8			
Void ratio	2.4889			
Specimen diameter, in.	2.750			
Specimen height, in.	5.940			
Height/diameter ratio	2.16			

Description: VSO G CL W/ SI+ORG PKTS

LL = NA	**PL =**	**PI =** NA	**Assumed GS=** 2.80	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3/11/09

Remarks:
BULGE + MULTI SHEAR
ORGANIC CONTENT: 4.1%

ASTM D 2166

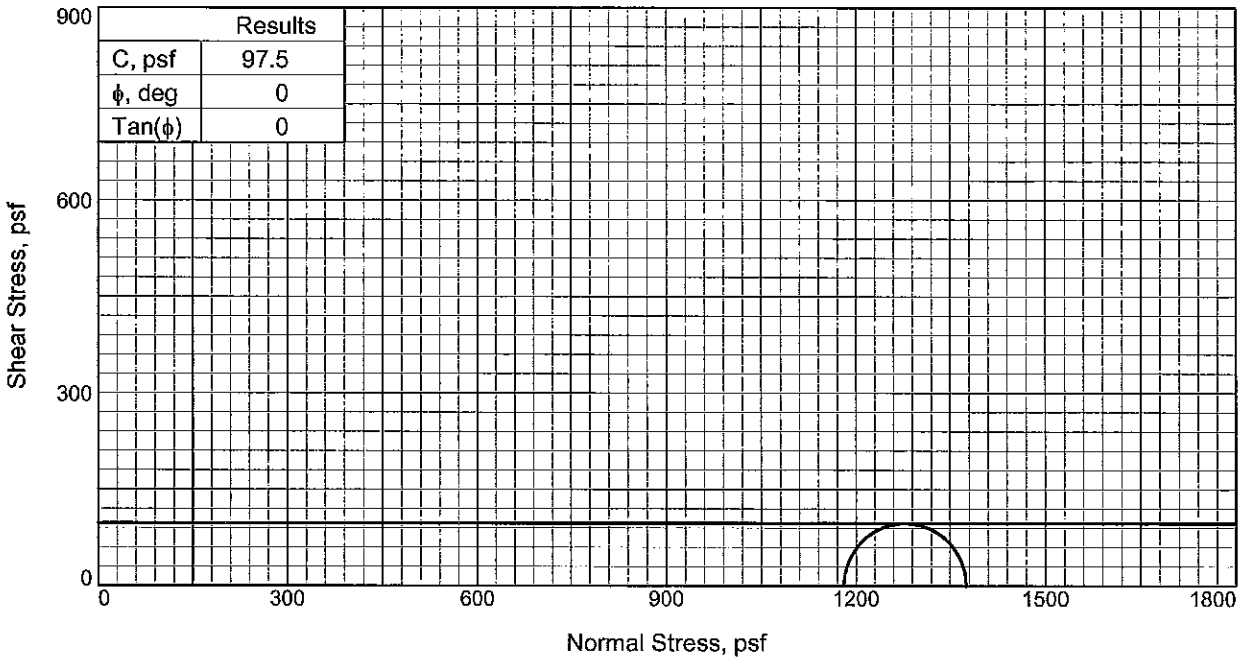
Client: URS

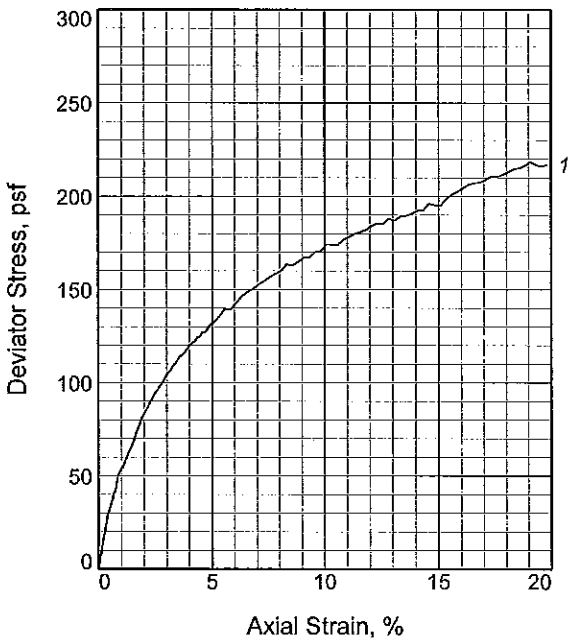
Project: BAYOU DUPONT

Source of Sample: B-4 **Depth:** 18-20
Sample Number: 7

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	97.3
	Dry Density, pcf	55.0
	Saturation, %	125.4
	Void Ratio	2.1569
	Diameter, in.	2.780
	Height, in.	4.120
At Test	Water Content, %	97.3
	Dry Density, pcf	55.0
	Saturation, %	125.4
	Void Ratio	2.1569
	Diameter, in.	2.780
	Height, in.	4.120
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		8.200
Fail. Stress, psf		194.9
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1375.7
σ_3 Failure, psf		1180.8

Type of Test:
Unconsolidated Undrained

Sample Type: undisturbed

Description: VSO G CL W/ ORG PKTS & SASI & SISA LAYS, CH

LL= 101 **PL=** 39 **PI=** 62

Specific Gravity= 2.78

Remarks: BULGE FAILURE
ORGANIC CONTENT: 3.7%

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-4 **Depth:** 23-25

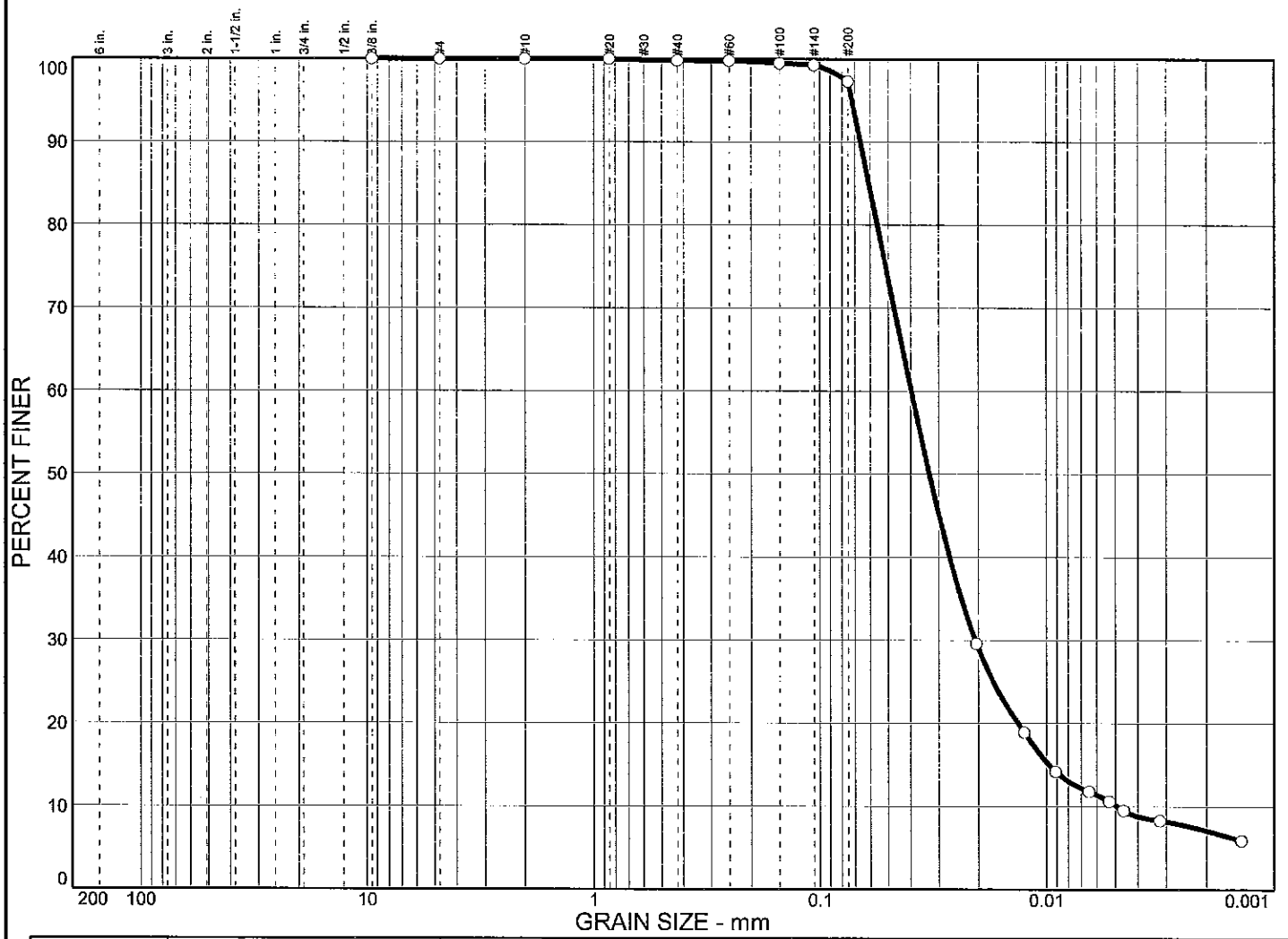
Sample Number: 8

Proj. No.: B09-012 **Date Sampled:** 3/11/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	2.7	87.2	10.1

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	101	NP	0.0608	0.0397		0.0207	0.0097	0.0049	2.19	8.08

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ ORG PKTS & SASI & SISA LAYS, CH	(CH)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-4 **Sample No.:** 8 **Elev./Depth:** 23-25

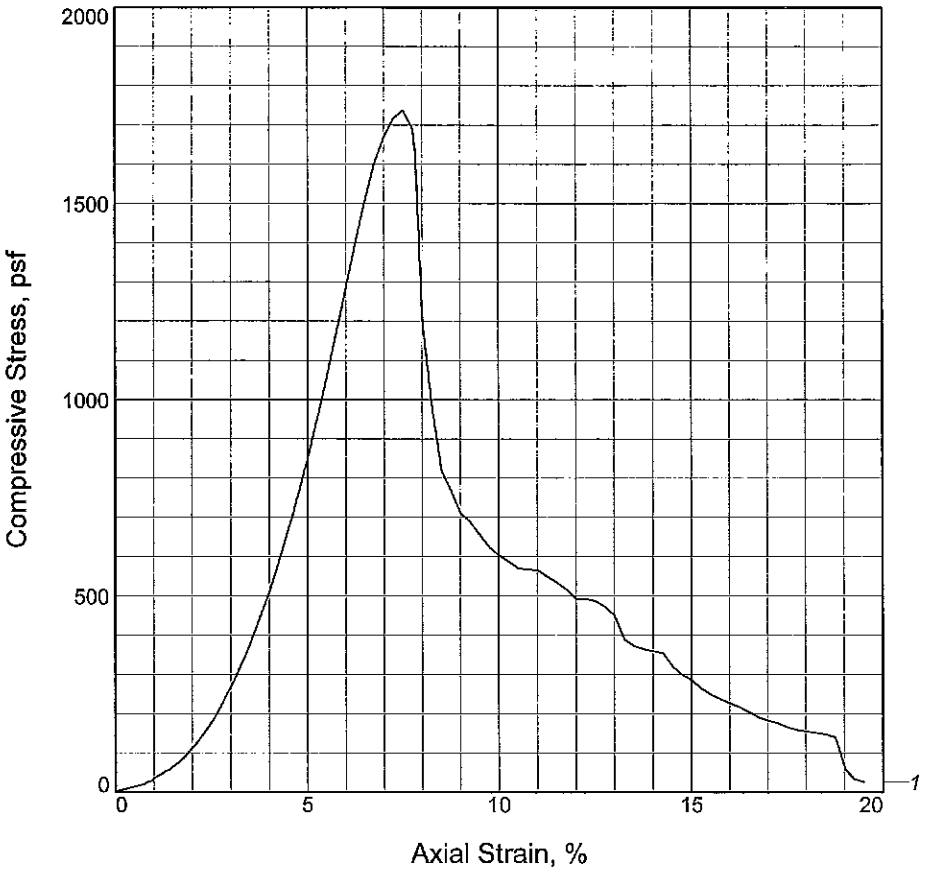
Remarks:

○ F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	1738.0			
Undrained shear strength, psf	869.0			
Failure strain, %	7.5			
Strain rate, %/min.	1.00			
Water content, %	30.0			
Wet density, pcf	119.6			
Dry density, pcf	92.0			
Saturation, %	99.7			
Void ratio	0.7976			
Specimen diameter, in.	2.750			
Specimen height, in.	5.940			
Height/diameter ratio	2.16			

Description: FM G CLSI

LL = NA	**PL =**	**PI =** NA	**Assumed GS=** 2.65	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3/11/09

Remarks:
SLUMPING UNDER OWN WEIGHT FAILURE: VERT SHEAR

ASTM D 2166

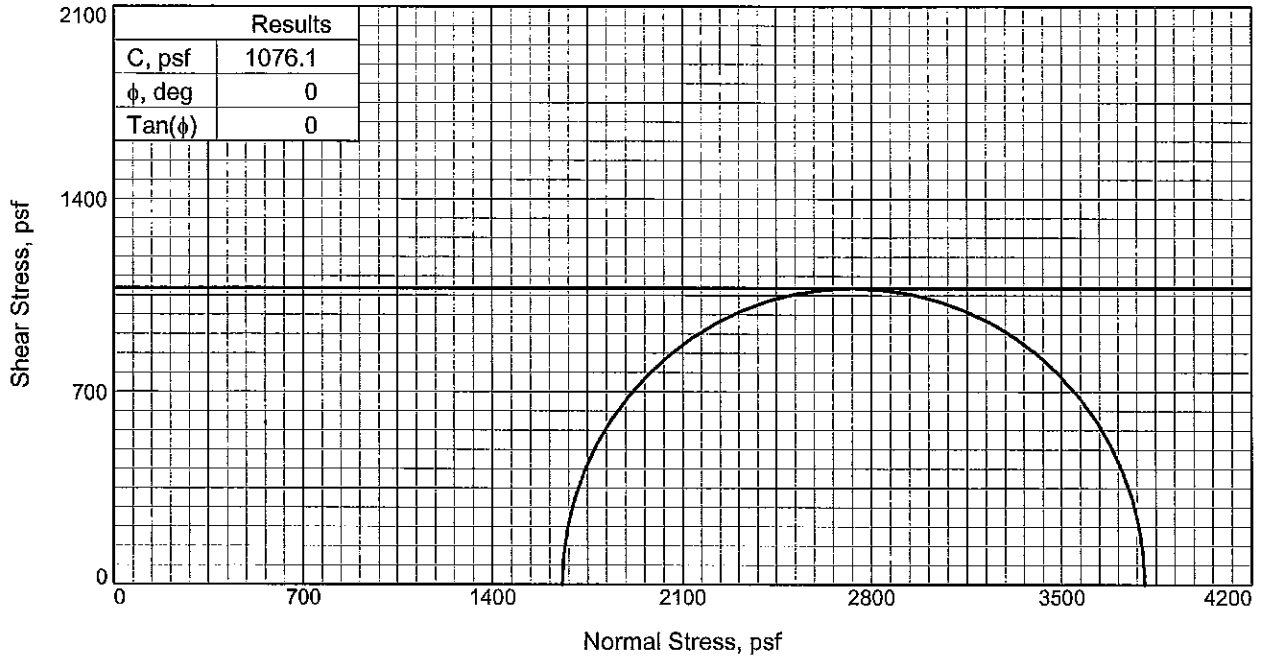
Client: URS

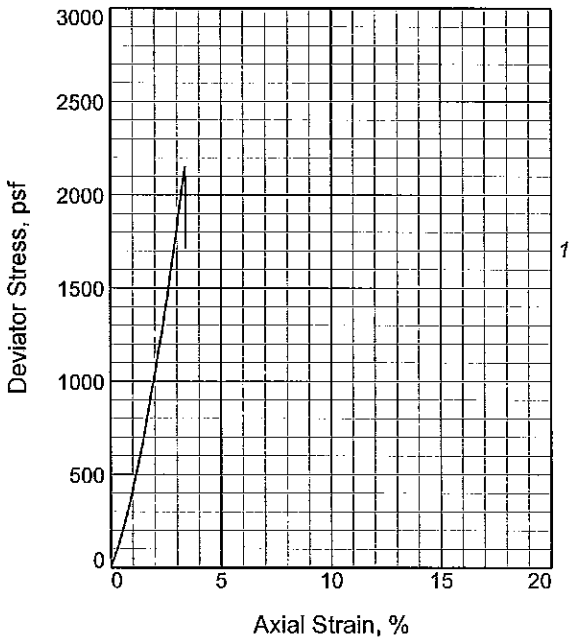
Project: BAYOU DUPONT

Source of Sample: B-4 **Depth:** 28-30
Sample Number: 9

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	28.0
	Dry Density, pcf	99.0
	Saturation, %	110.4
	Void Ratio	0.6713
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	28.0
	Dry Density, pcf	99.0
	Saturation, %	110.4
	Void Ratio	0.6713
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		11.500
Fail. Stress, psf		2152.3
Strain, %		3.4
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3808.3
σ_3 Failure, psf		1656.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: FM G SASI W/ CL

LL= NP **PI=** NP

Assumed Specific Gravity= 2.65

Remarks: SLUMPING UNDER OWN WEIGHT
FAILURE: MAXED OUT RING

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-4 **Depth:** 33-35

Sample Number: 10

Proj. No.: B09-012 **Date Sampled:** 3/11/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	12.6	77.2	10.2

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	NP	NP	0.0700	0.0465	0.0406	0.0291	0.0160	0.0049	3.73	9.50

MATERIAL DESCRIPTION	USCS	AASHTO
○ FM G SASI W/ CL		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-4 **Sample No.:** 10 **Elev./Depth:** 33-35

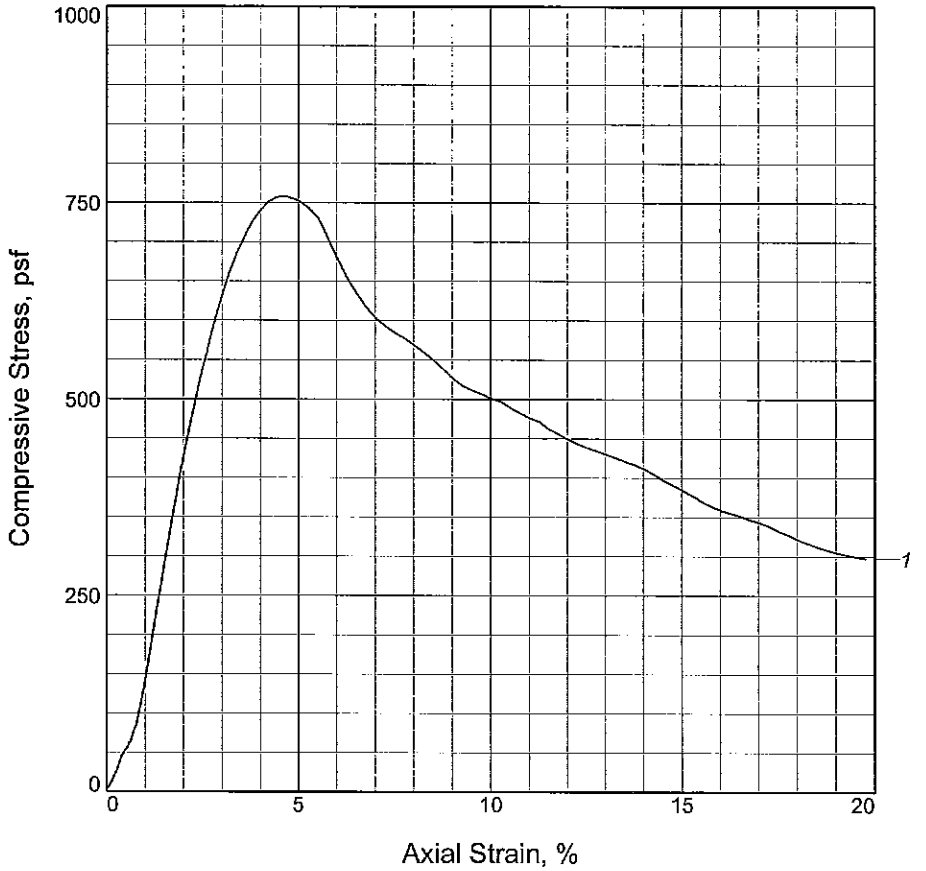
Remarks:

○ F.M.=0.05

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	758.2			
Undrained shear strength, psf	379.1			
Failure strain, %	4.7			
Strain rate, %/min.	1.00			
Water content, %	62.7			
Wet density, pcf	106.9			
Dry density, pcf	65.7			
Saturation, %	105.7			
Void ratio	1.6606			
Specimen diameter, in.	2.750			
Specimen height, in.	5.940			
Height/diameter ratio	2.16			

Description: SO G CL

LL = 63	**PL =** 24	**PI =** 39	**Assumed GS=** 2.80	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3/11/09
Remarks:
FAILURE:SLS

ASTM D 2166

Client: URS

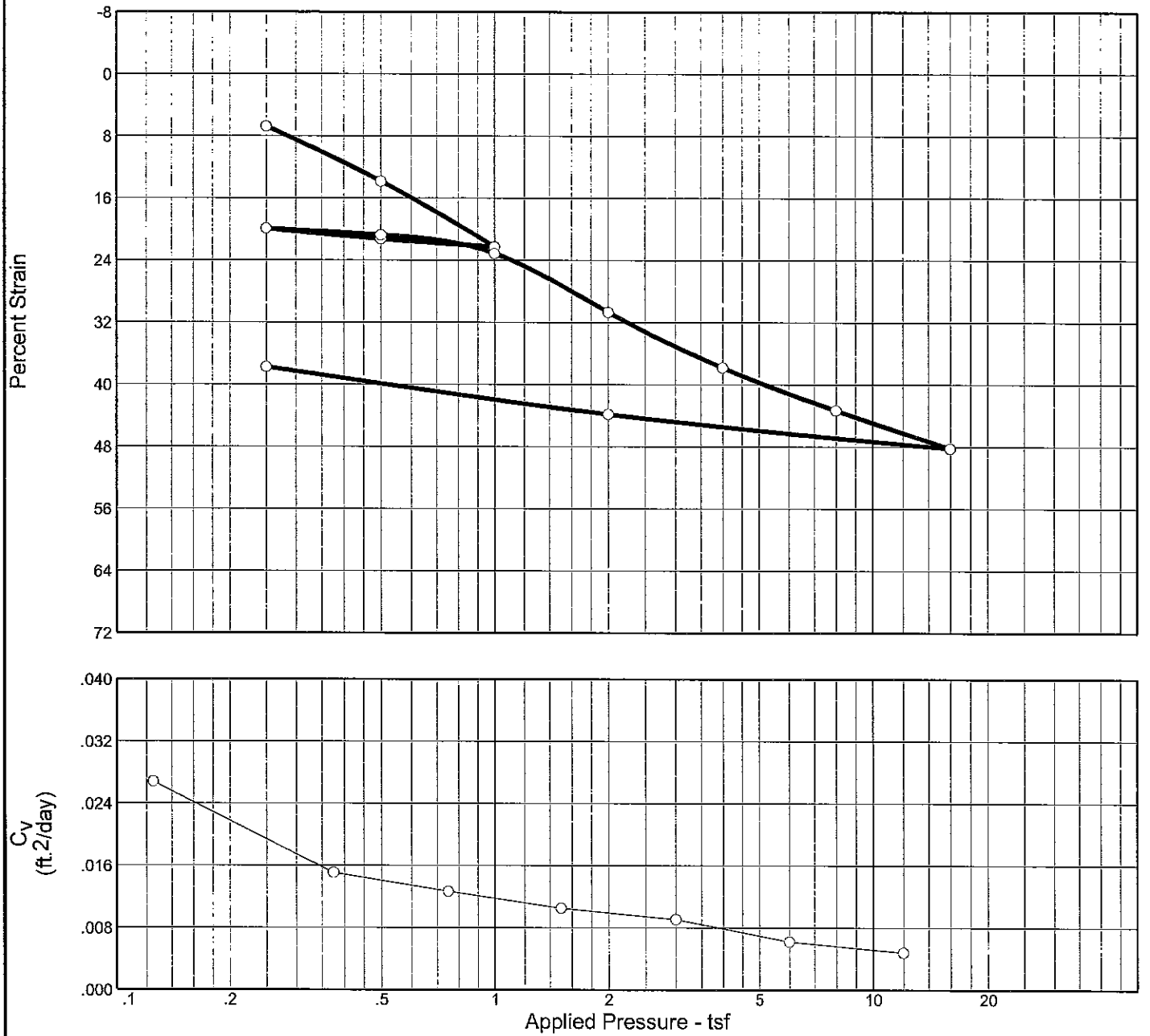
Project: BAYOU DUPONT

Source of Sample: B-4 **Depth:** 38-40
Sample Number: 11

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
96.9 %	97.1 %	45.9	101	62	2.78	(CH)		2.785

MATERIAL DESCRIPTION

VSO G CL W/ ORG PKTS & SASI & SISA LAYS, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

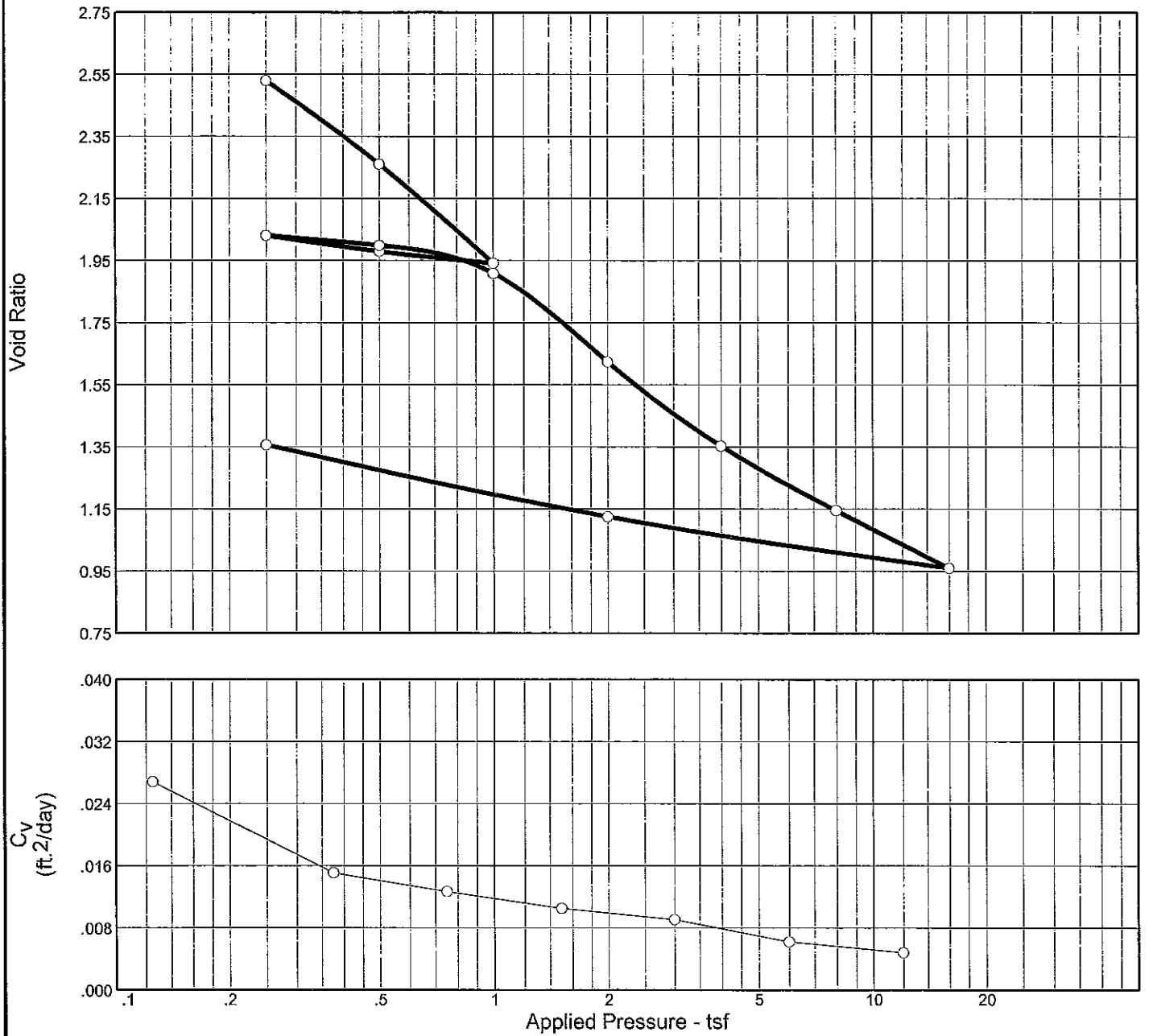
Source: B-4 **Sample No.:** 8 **Elev./Depth:** 23-25

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

Remarks:
ASTM D2435

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
96.9 %	97.1 %	45.9	101	62	2.78	(CH)		2.785

MATERIAL DESCRIPTION

VSO G CL W/ ORG PKTS & SASI & SISA LAYS, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-4 **Sample No.:** 8 **Elev./Depth:** 23-25

CONSOLIDATION/SWELL TEST REPORT

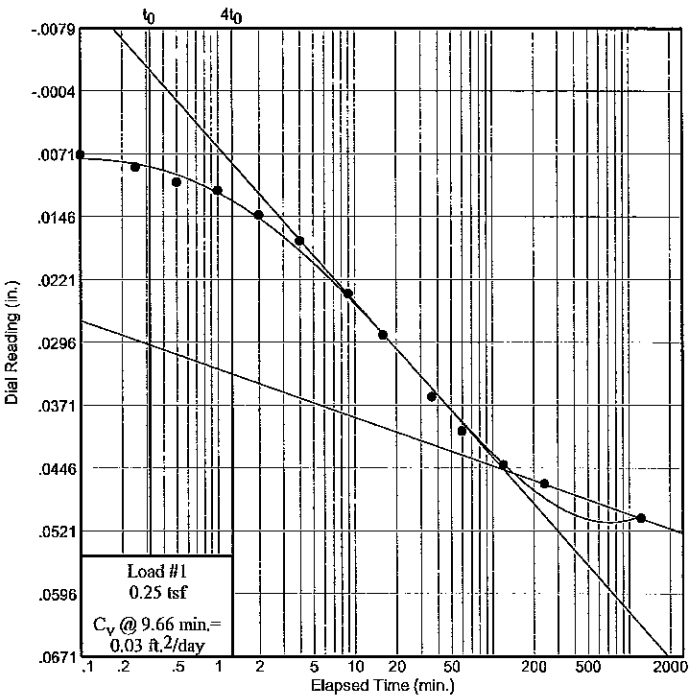
Southern Earth Sciences, Inc.

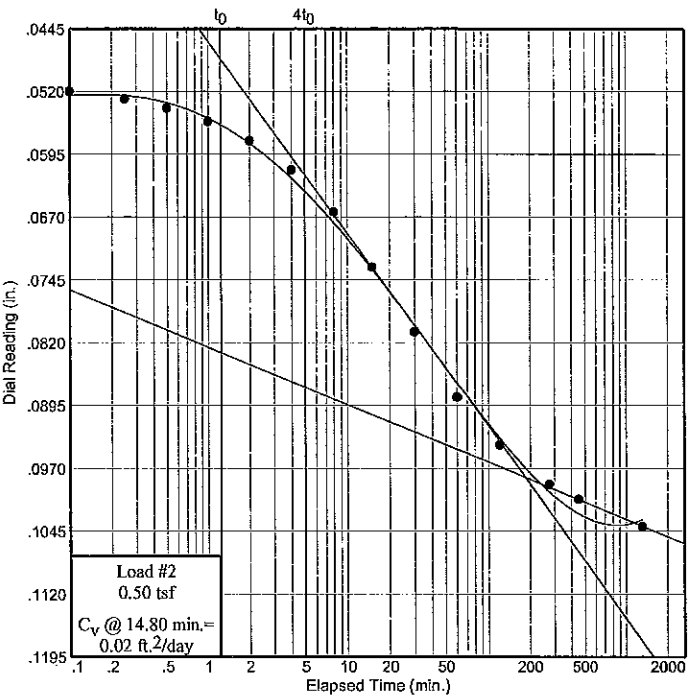
Remarks:
ASTM D2435

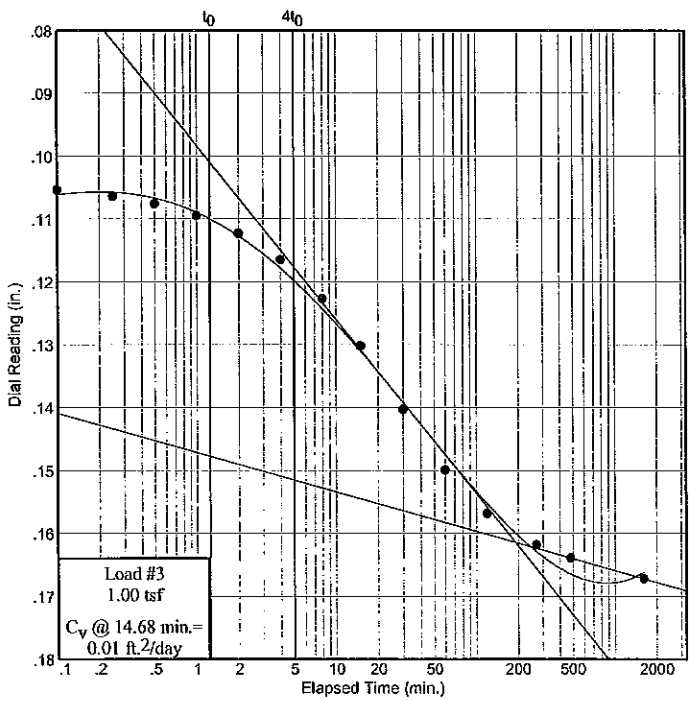
Dial Reading vs. Time

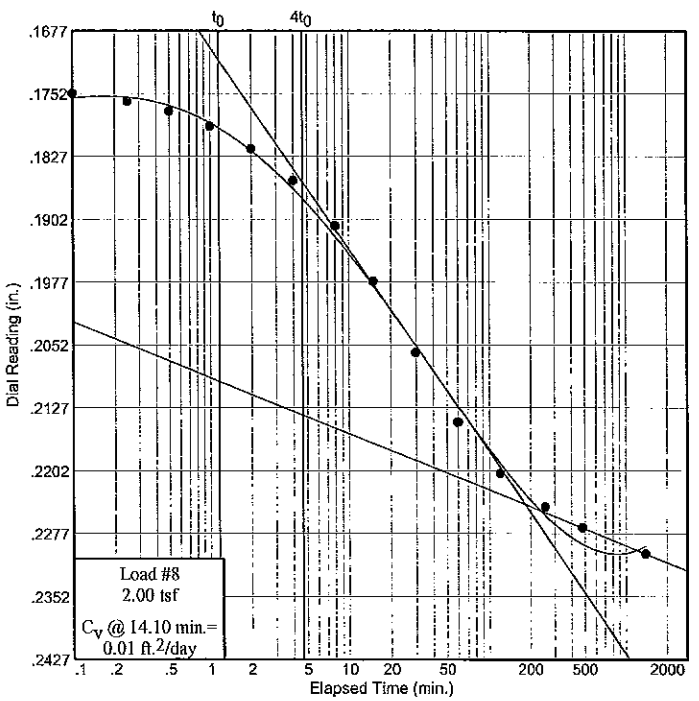
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-4 Sample No.: 8 Elev./Depth: 23-25





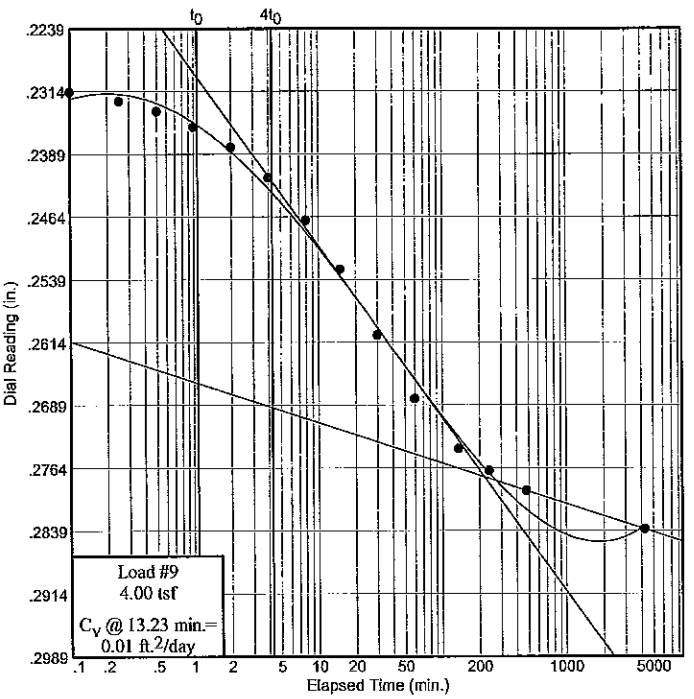


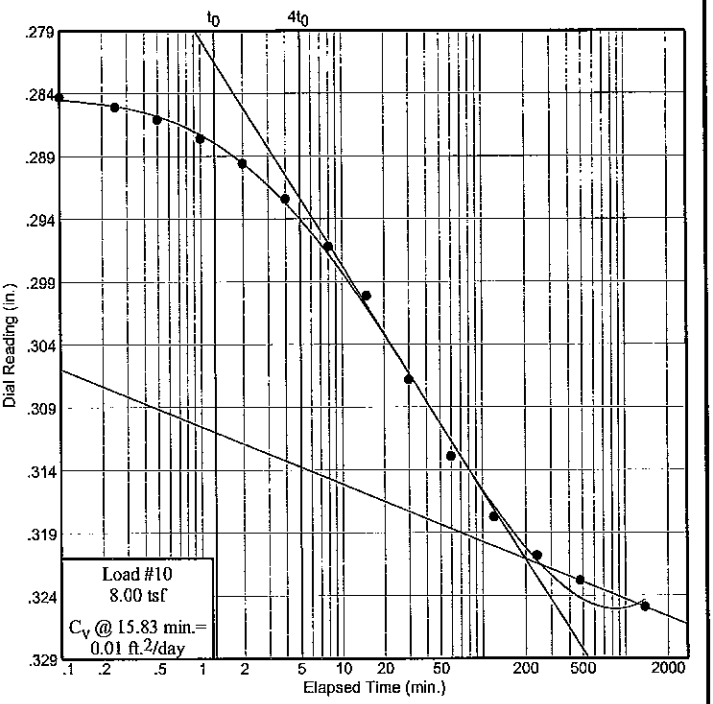


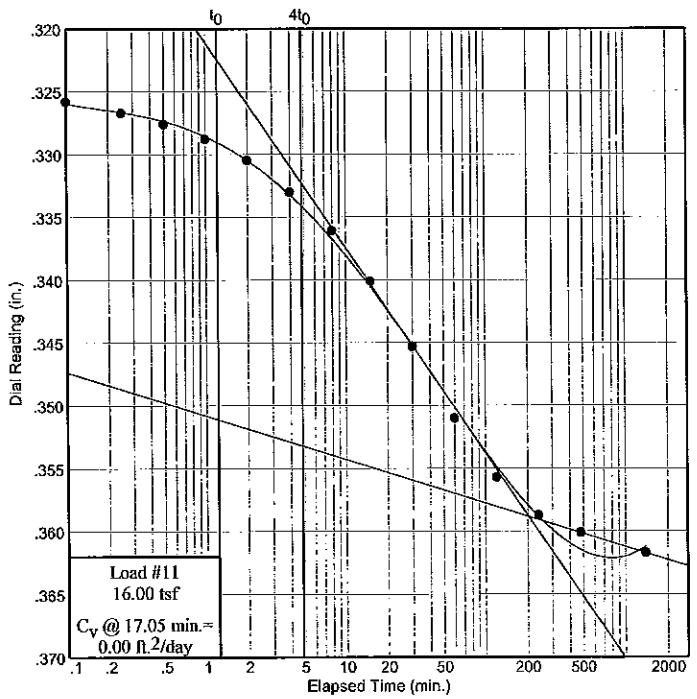
Dial Reading vs. Time

Project No.: B09-012
Project: BAYOU DUPONT

Source: B-4 Sample No.: 8 Elev./Depth: 23-25







Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-4
Sample No.: 8
Elev. or Depth: 23-25 **Sample Length(in./cm.):**
Location:
Description: VSO G CL W/ ORG PKTS & SASI & SISA LAYS, CH
Liquid Limit: 101 **Plasticity Index:** 62
USCS: (CH) **AASHTO:** **Figure No.:** 1
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST		AFTER TEST	
Wet w+t =	113.75 g.	**Consolidometer #** =	1	**Wet w+t** =	65.56 g.
Dry w+t =	76.46 g.			**Dry w+t** =	43.09 g.
Tare Wt. =	38.04 g.	**Spec. Gravity** =	2.78	**Tare Wt.** =	.00 g.
Height =	.75 in.	**Height** =	.75 in.		
Diameter =	2.50 in.	**Diameter** =	2.50 in.		
Weight =	87.33 g.	**Defl. Table** =	Unit No. 10 Old 2.5in		
Moisture =	97.1 %	**Ht. Solids** =	0.1982 in.	**Moisture** =	52.1 %
Wet Den. =	90.4 pcf	**Dry Wt.** =	44.32 g.*	**Dry Wt.** =	43.09 g.
Dry Den. =	45.9 pcf	**Void Ratio** =	2.785	**Void Ratio** =	1.356
		Saturation =	96.9 %		

*** Initial dry weight used in calculations**

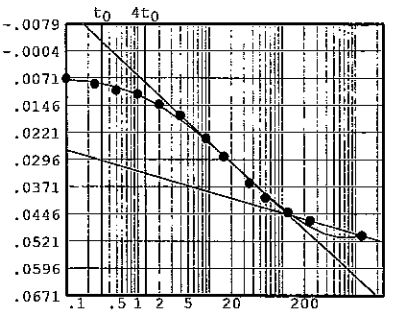
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				2.785	
0.25	0.05080	0.00020	0.03	0.008	2.529	6.7 Comprs.
0.50	0.10430	0.00040	0.02	0.010	2.260	13.9 Comprs.
1.00	0.16800	0.00080	0.01	0.010	1.941	22.3 Comprs.
0.50	0.16040	0.00080	0.08		1.979	21.3 Comprs.
0.25	0.15030	0.00080	0.02		2.030	19.9 Comprs.
0.50	0.15650	0.00080	0.07	0.001	1.999	20.8 Comprs.
1.00	0.17460	0.00100	0.03	0.006	1.909	23.1 Comprs.
2.00	0.23140	0.00130	0.01	0.012	1.623	30.7 Comprs.
4.00	0.28570	0.00200	0.01	0.009	1.353	37.8 Comprs.
8.00	0.32790	0.00300	0.01	0.010	1.145	43.3 Comprs.
16.00	0.36580	0.00410	0.00	0.008	0.959	48.2 Comprs.
2.00	0.33030	0.00150			1.125	43.8 Comprs.
0.25	0.28370	0.00060			1.356	37.7 Comprs.

C_c = 0.61 P_c = 3.11 tsf C_r = 0.20

Pressure: 0.25 tsf **TEST READINGS** **Load No. 1**

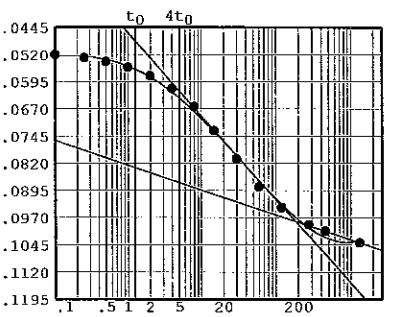
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	60.00	0.04040
2	0.10	0.00740	12	120.00	0.04440
3	0.25	0.00890	13	240.00	0.04670
4	0.50	0.01070	14	1230.00	0.05080
5	1.00	0.01170			
6	2.00	0.01460			
7	4.00	0.01770			
8	9.00	0.02400			
9	16.00	0.02890			
10	36.00	0.03630			



Void Ratio = 2.529 **Compression** = 6.7 %
D_0 = 0.00462 D_{50} = 0.02470 D_{100} = 0.04478
C_v at 9.7 min. = 0.03 ft.^{2}/day C_α = 0.008

Pressure: 0.50 tsf **TEST READINGS** **Load No. 2**

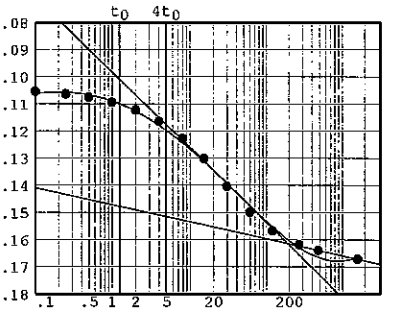
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.05080	11	60.00	0.08890
2	0.10	0.05240	12	120.00	0.09460
3	0.25	0.05330	13	275.00	0.09930
4	0.50	0.05440	14	450.00	0.10110
5	1.00	0.05600	15	1320.00	0.10430
6	2.00	0.05830			
7	4.00	0.06180			
8	8.00	0.06680			
9	15.00	0.07340			
10	30.00	0.08110			



Void Ratio = 2.260 **Compression** = 13.9 %
D_0 = 0.04809 D_{50} = 0.07307 D_{100} = 0.09805
C_v at 14.8 min. = 0.02 ft.^{2}/day C_α = 0.010

Pressure: 1.00 tsf **TEST READINGS** **Load No. 3**

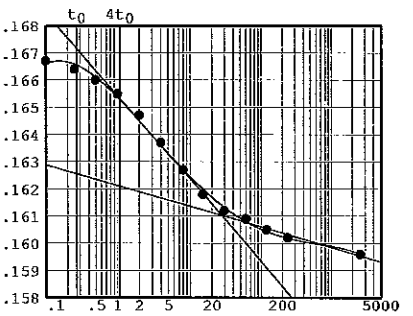
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.10430	11	60.00	0.15070
2	0.10	0.10620	12	120.00	0.15760
3	0.25	0.10720	13	270.00	0.16260
4	0.50	0.10840	14	480.00	0.16470
5	1.00	0.11030	15	1620.00	0.16800
6	2.00	0.11310			
7	4.00	0.11730			
8	8.00	0.12350			
9	15.00	0.13100			
10	30.00	0.14110			



Void Ratio = 1.941 **Compression** = 22.3 %
D_0 = 0.10018 D_{50} = 0.13079 D_{100} = 0.16140
C_v at 14.7 min. = 0.01 ft.^{2}/day C_α = 0.010

Pressure: 0.50 tsf **TEST READINGS** **Load No. 4**

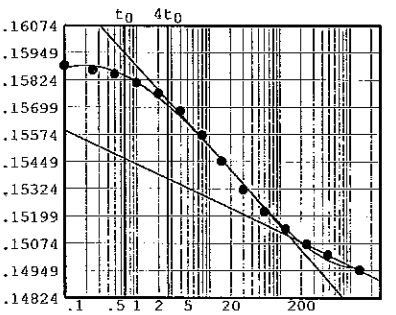
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.16800	11	60.00	0.16170
2	0.10	0.16750	12	120.00	0.16130
3	0.25	0.16720	13	240.00	0.16100
4	0.50	0.16680	14	2580.00	0.16040
5	1.00	0.16630			
6	2.00	0.16550			
7	4.00	0.16450			
8	8.00	0.16350			
9	15.00	0.16260			
10	30.00	0.16200			



Void Ratio = 1.979 **Compression** = 21.3 %
D_0 = 0.16782 D_{50} = 0.16443 D_{100} = 0.16103
C_v at 2.1 min. = 0.08 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 5**

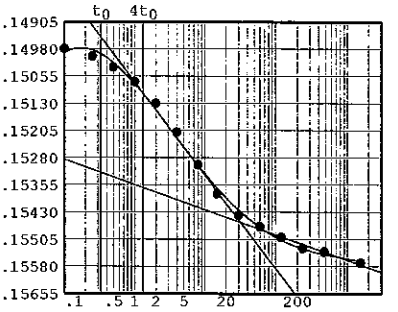
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.16040	11	60.00	0.15300
2	0.10	0.15970	12	120.00	0.15220
3	0.25	0.15950	13	240.00	0.15150
4	0.50	0.15930	14	480.00	0.15100
5	1.00	0.15890	15	1350.00	0.15030
6	2.00	0.15840			
7	4.00	0.15760			
8	8.00	0.15650			
9	15.00	0.15530			
10	30.00	0.15400			



Void Ratio = 2.030 **Compression** = 19.9 %
D_0 = 0.15983 D_{50} = 0.15544 D_{100} = 0.15105
C_v at 8.6 min. = 0.02 ft.^{2}/day

Pressure: 0.50 tsf **TEST READINGS** **Load No. 6**

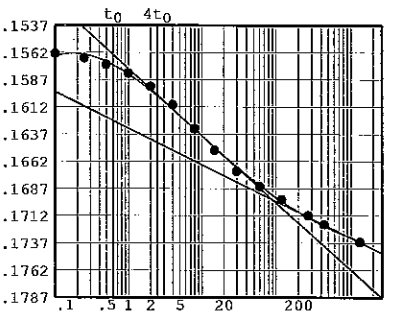
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.15030	11	60.00	0.15550
2	0.10	0.15060	12	120.00	0.15580
3	0.25	0.15080	13	240.00	0.15610
4	0.50	0.15110	14	480.00	0.15620
5	1.00	0.15150	15	1530.00	0.15650
6	2.00	0.15210			
7	4.00	0.15290			
8	8.00	0.15380			
9	15.00	0.15460			
10	30.00	0.15520			



Void Ratio = 1.999 **Compression** = 20.8 %
D_0 = 0.14882 D_{50} = 0.15171 D_{100} = 0.15459
C_v at 2.5 min. = 0.07 ft.^{2}/day C_α = 0.001

Pressure: 1.00 tsf **TEST READINGS** **Load No. 7**

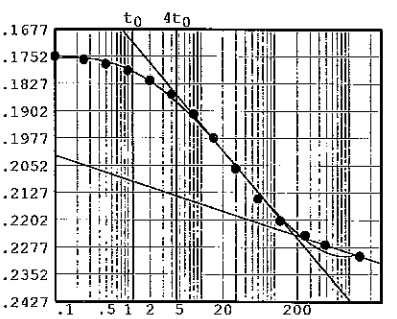
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.15650	11	60.00	0.16950
2	0.10	0.15730	12	120.00	0.17070
3	0.25	0.15770	13	270.00	0.17220
4	0.50	0.15830	14	440.00	0.17300
5	1.00	0.15910	15	1320.00	0.17460
6	2.00	0.16030			
7	4.00	0.16200			
8	8.00	0.16420			
9	15.00	0.16620			
10	30.00	0.16810			



Void Ratio = 1.909 **Compression** = 23.1 %
D_0 = 0.15446 D_{50} = 0.16206 D_{100} = 0.16966
C_v at 5.1 min. = 0.03 ft.^{2}/day C_α = 0.006

Pressure: 2.00 tsf **TEST READINGS** **Load No. 8**

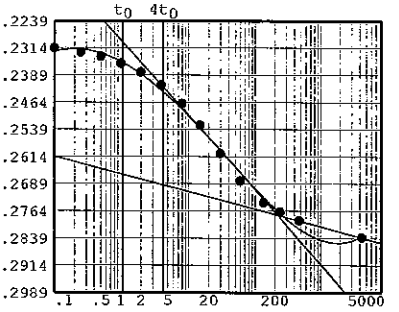
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.17460	11	60.00	0.21570
2	0.10	0.17650	12	120.00	0.22180
3	0.25	0.17740	13	257.00	0.22580
4	0.50	0.17860	14	480.00	0.22830
5	1.00	0.18040	15	1400.00	0.23140
6	2.00	0.18310			
7	4.00	0.18690			
8	8.00	0.19230			
9	15.00	0.19890			
10	30.00	0.20740			



Void Ratio = 1.623 **Compression** = 30.7 %
D_0 = 0.17090 D_{50} = 0.19756 D_{100} = 0.22421
C_v at 14.1 min. = 0.01 ft.^{2}/day C_α = 0.012

Pressure: 4.00 tsf **TEST READINGS** **Load No. 9**

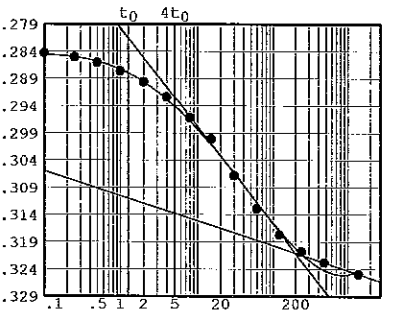
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.23140	11	60.00	0.27010
2	0.10	0.23350	12	135.00	0.27610
3	0.25	0.23460	13	240.00	0.27870
4	0.50	0.23580	14	480.00	0.28110
5	1.00	0.23770	15	4290.00	0.28570
6	2.00	0.24010			
7	4.00	0.24370			
8	8.00	0.24880			
9	15.00	0.25470			
10	30.00	0.26250			



Void Ratio = 1.353 **Compression** = 37.8 %
D_0 = 0.22736 D_{50} = 0.25241 D_{100} = 0.27746
C_v at 13.2 min. = 0.01 ft.^{2}/day C_α = 0.009

Pressure: 8.00 tsf **TEST READINGS** **Load No. 10**

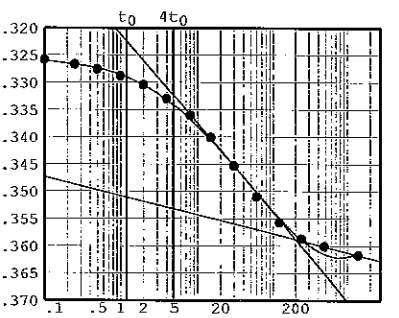
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.28570	11	60.00	0.31590
2	0.10	0.28730	12	120.00	0.32070
3	0.25	0.28810	13	240.00	0.32380
4	0.50	0.28910	14	480.00	0.32580
5	1.00	0.29060	15	1380.00	0.32790
6	2.00	0.29260			
7	4.00	0.29540			
8	8.00	0.29920			
9	15.00	0.30310			
10	30.00	0.30980			



Void Ratio = 1.145 **Compression** = 43.3 %
D_0 = 0.28189 D_{50} = 0.30146 D_{100} = 0.32104
C_v at 15.8 min. = 0.01 ft.^{2}/day C_α = 0.010

Pressure: 16.00 tsf **TEST READINGS** **Load No. 11**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.32790	11	60.00	0.35510
2	0.10	0.32990	12	120.00	0.35980
3	0.25	0.33080	13	240.00	0.36280
4	0.50	0.33170	14	480.00	0.36420
5	1.00	0.33290	15	1390.00	0.36580
6	2.00	0.33460			
7	4.00	0.33710			
8	8.00	0.34020			
9	15.00	0.34420			
10	30.00	0.34940			



Void Ratio = 0.959 **Compression** = 48.2 %
D_0 = 0.32394 D_{50} = 0.34137 D_{100} = 0.35881
C_v at 17.0 min. = 0.00 ft.^{2}/day C_α = 0.008

Southern Earth Sciences, Inc.

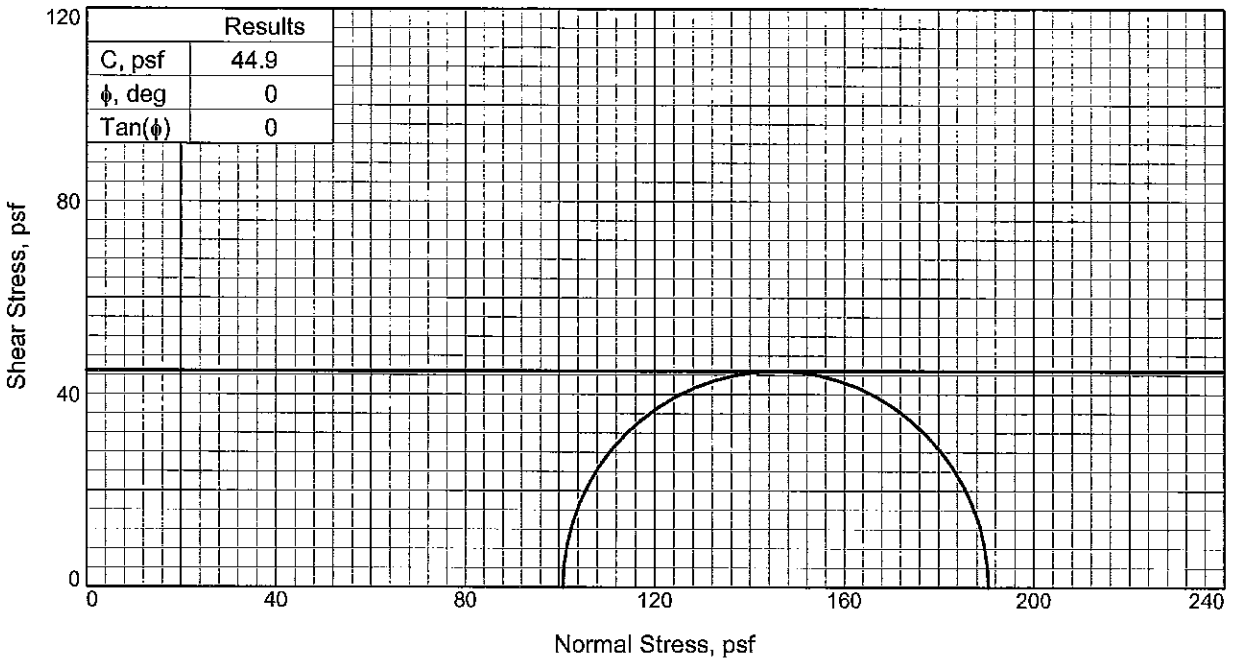
Laboratory Test Results

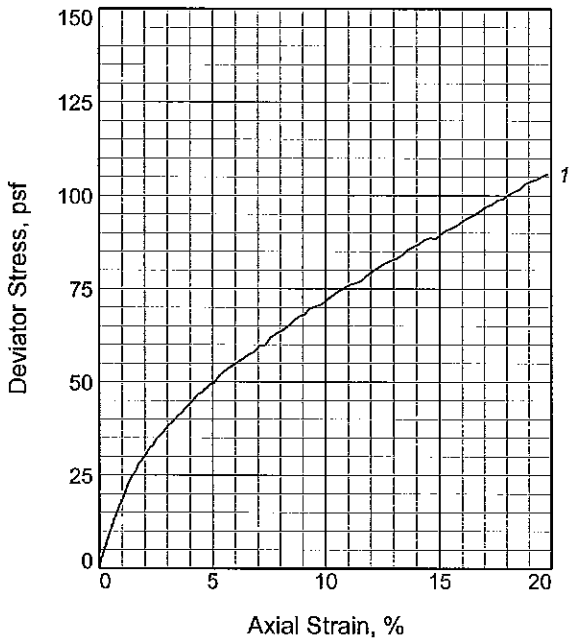
Project: **Bayou DuPont** | **Technical Responsibility:** | **Quality Assurance Officer**

Client: URS

7389 Florida Blvd., Suite 300, Baton Rouge, LA 70806 | Project No.: **B09-012** | PM: S. Aviles | Date of Issue: 3/12/2009

			ASTM DESIGNATION																
			D2216	D4318			D427	D2166		D2166	D2850	D422, C136 or C117					D2974	USCS	
				Atterberg Limits						Cohesion		Grain Size (% Passing)							
Boring No.	Depth (ft)	Classification	ω %	LL	PL	PI	SL	γ_{wet} pcf	γ_{dry} pcf	U psf	UU psf	Gravel	Sand	Silt	Clay	#200	Organic Content %		Confining Stress, Resistivity and Remarks
B-5	0-2	Very Soft PEAT	427.9					57.3	10.9		44.9							(PT)	Confining Pressure: 0.7 psi
B-5	2-4	PEAT with clay and organics	223.4	223	58	165											14.5	(PT) to (OH)	Specific Gravity: 2.399
B-5	4-6	Very Soft, PEAT with clay and organics	334.1				22.0	73.4	16.9		70.3		3.5	23.0	73.5			(PT) to (OH)	Confining Pressure: 2.0 psi
B-5	6-8	Very Soft, Gray CLAY with organic pockets	84.4	68	26	42		101.9	55.3	47.9								(CH)	
B-5	8-10	Very Soft, Gray CLAY with organic pockets and trace silt pockets	61.6					103.8	64.2									(CH)	Specific Gravity: 2.792
B-5	13-15	Very Soft, Gray Lean CLAY with organics and fine sand	117.1	78	36	42	16.0	93.9	38.7	80.0			22.0	31.3	46.7		8.6	(CH)	
B-5	18-20	Very Soft, Gray CLAY with organic pockets	138.2					94.1	39.5		65.0		8.3	32.2	59.5			(CH)	Confining Pressure: 6.6 psi
B-5	23-25	Very Soft, Gray CLAY becoming clayey silt	167.9	47	24	23	26.1	107.9	40.3	93.8							11.5	(CH)	Specific Gravity: 2.762
B-5	28-30	Very Soft, Loose Gray CLAYEY SILT with clay and sand	33.3	34	28	6		108.2	81.1		92.1							(CL-ML)	Confining Pressure: 9.9 psi
B-5	33-35	Alternating Layers Very Soft, Gray CLAY and Gray Silt with sand	46.7					105.0	71.6									(CH-CL)	
B-5	38-40	Loose, Gray SILT with clay layers	37.7	NP	NP	NP		122.4	88.9	455.9			13.3	81.0	5.7			(ML)	
B-5	43-45	Medium, Gray CLAYEY SILT with clay	31.6				15.3	124.8	94.9		604.1						1.0	(CL-ML)	Confining Pressure: 14.8 psi Specific Gravity: 2.684
B-5	48-50	Very Soft to Soft, Gray CLAY	67.9	79	35	44		103.6	61.7	237.5			0.0	22.1	77.9			(CH)	
B-5	53-55	Very Soft to Soft, Gray CLAY with silt pockets	55.9					107.1	68.7		223.7					100.0		(CH)	Confining Pressure: 18.1 psi
B-5	58-60	Soft, Gray CLAY with trace organics	52.7	67	25	42	16.3	112.5	73.7	377.1			0.0	38.9	61.1			(CH)	





Sample No.		1
Initial	Water Content, %	427.9
	Dry Density, pcf	10.9
	Saturation, %	81.5
	Void Ratio	10.4957
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	427.9
	Dry Density, pcf	10.9
	Saturation, %	81.5
	Void Ratio	10.4957
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		0.700
Fail. Stress, psf		89.7
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		190.5
σ_3 Failure, psf		100.8

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO PEAT, PT

Assumed Specific Gravity= 2.00
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

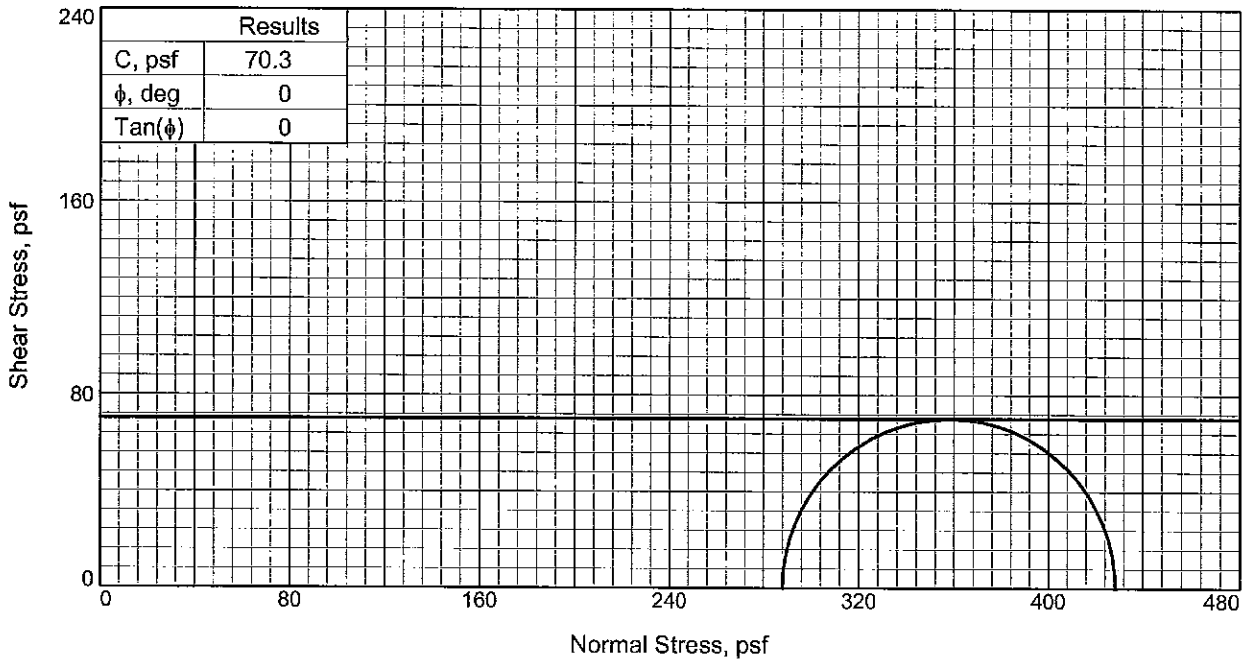
Client: URS

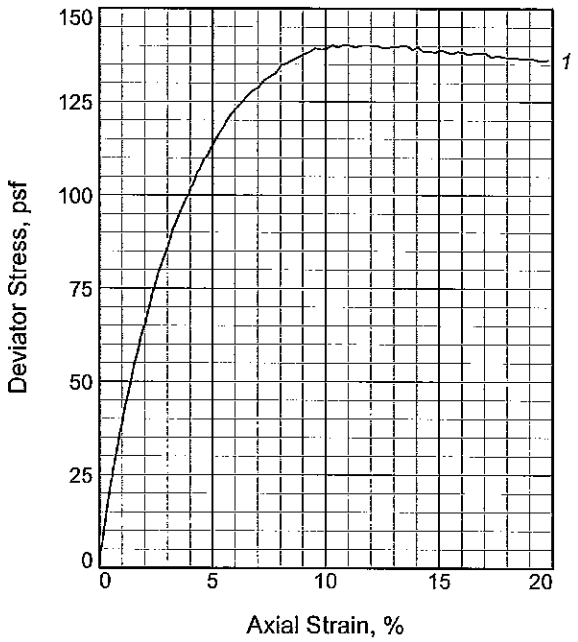
Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 0-2
Sample Number: 1
Proj. No.: B09-012 **Date Sampled:** 3-11-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	334.1
	Dry Density, pcf	16.9
	Saturation, %	102.0
	Void Ratio	7.8589
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	334.1
	Dry Density, pcf	16.9
	Saturation, %	102.0
	Void Ratio	7.8589
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.000
Fail. Stress, psf		140.5
Strain, %		10.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		428.5
σ_3 Failure, psf		288.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: PEAT W/ CL, PT TO OH

LL= NP **PI=** NP

Assumed Specific Gravity= 2.40

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 4-6

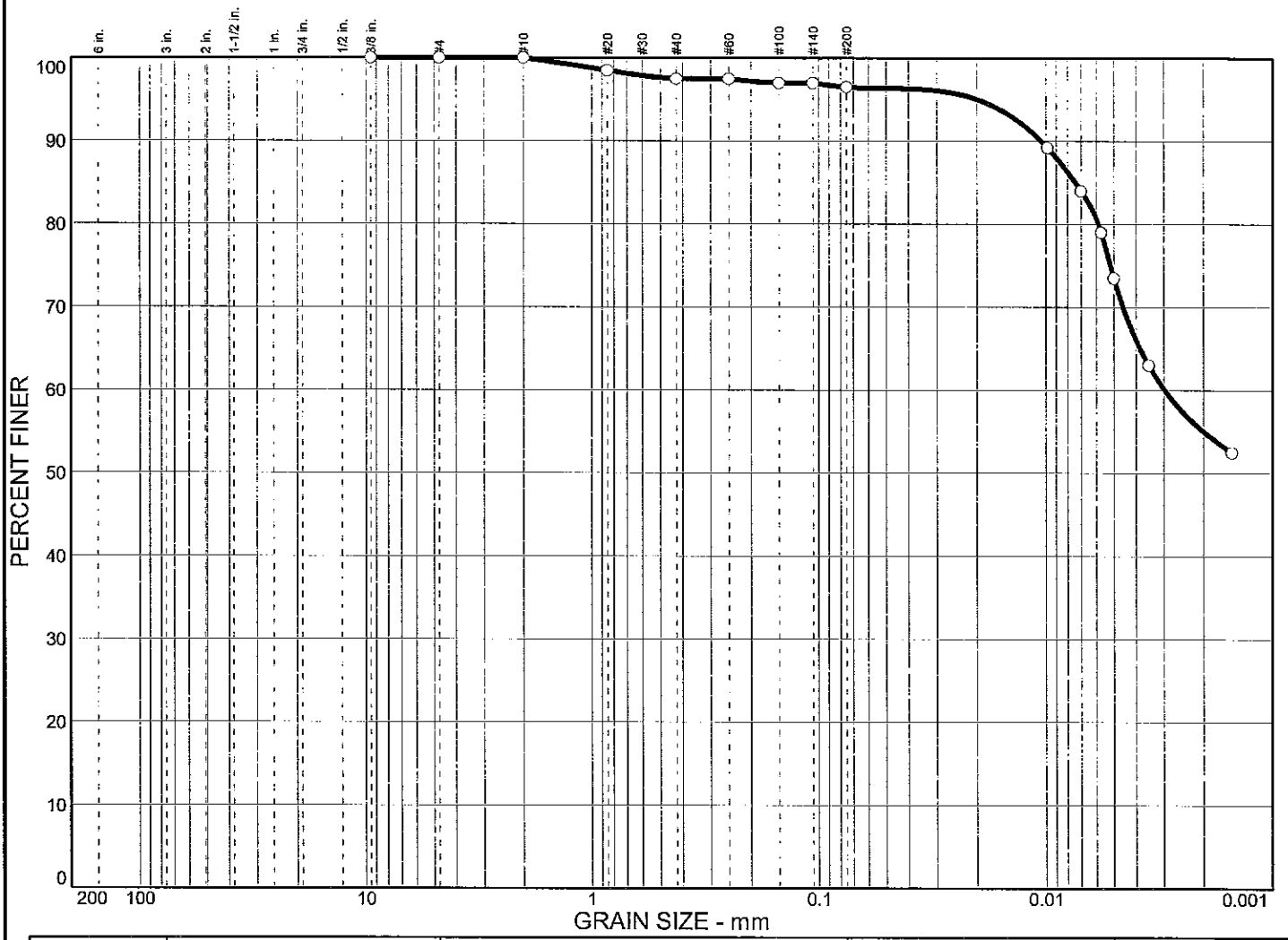
Sample Number: 3

Proj. No.: B09-012 **Date Sampled:** 3-11-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	3.5	23.0	73.5

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	NP	NP	0.0074	0.0030						

MATERIAL DESCRIPTION	USCS	AASHTO
○ PEAT W/ CL, PT TO OH	PT TO OH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-5 **Sample No.:** 3 **Elev./Depth:** 4-6

Remarks:

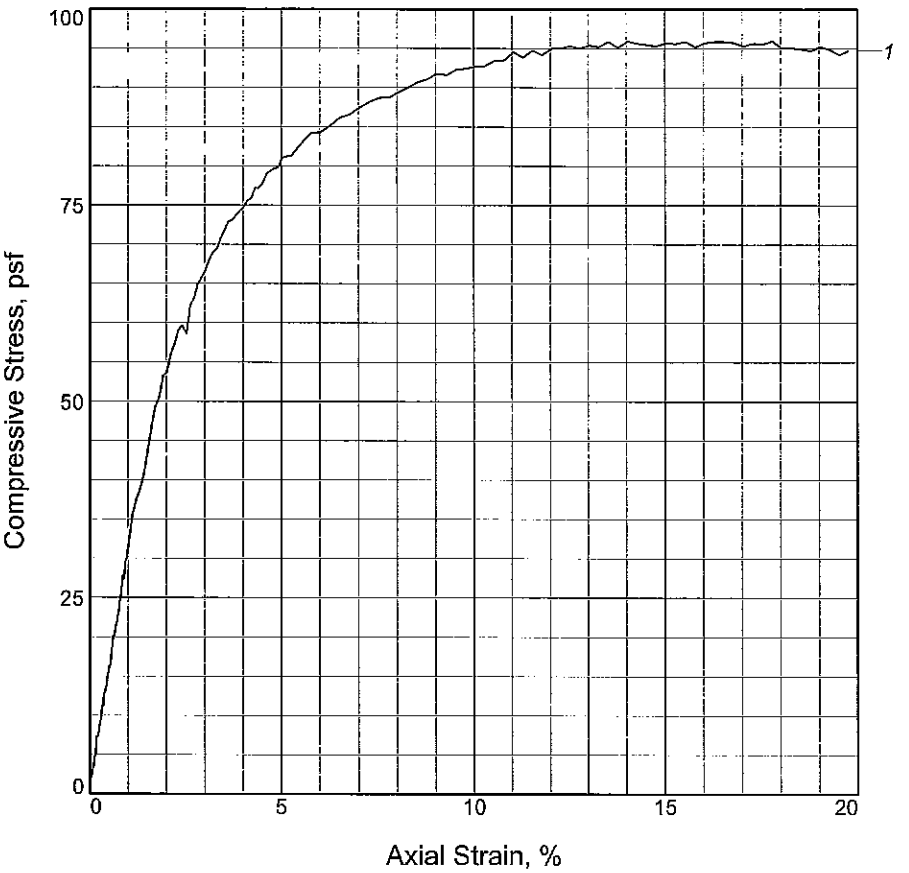
○ ASTM C136, D422

F.M.=0.03

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	95.7			
Undrained shear strength, psf	47.9			
Failure strain, %	15.0			
Strain rate, %/min.	1.00			
Water content, %	84.4			
Wet density, pcf	101.9			
Dry density, pcf	55.3			
Saturation, %	109.3			
Void ratio	2.1625			
Specimen diameter, in.	2.750			
Specimen height, in.	5.940			
Height/diameter ratio	2.16			

Description: VSO G CL W/ ORG PKTS, CH

LL = 68	**PL =** 26	**PI =** 42	**Assumed GS=** 2.80	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-11-09
Remarks:
TYPE FAILURE: BULGE

ASTM D 2166

Client: URS

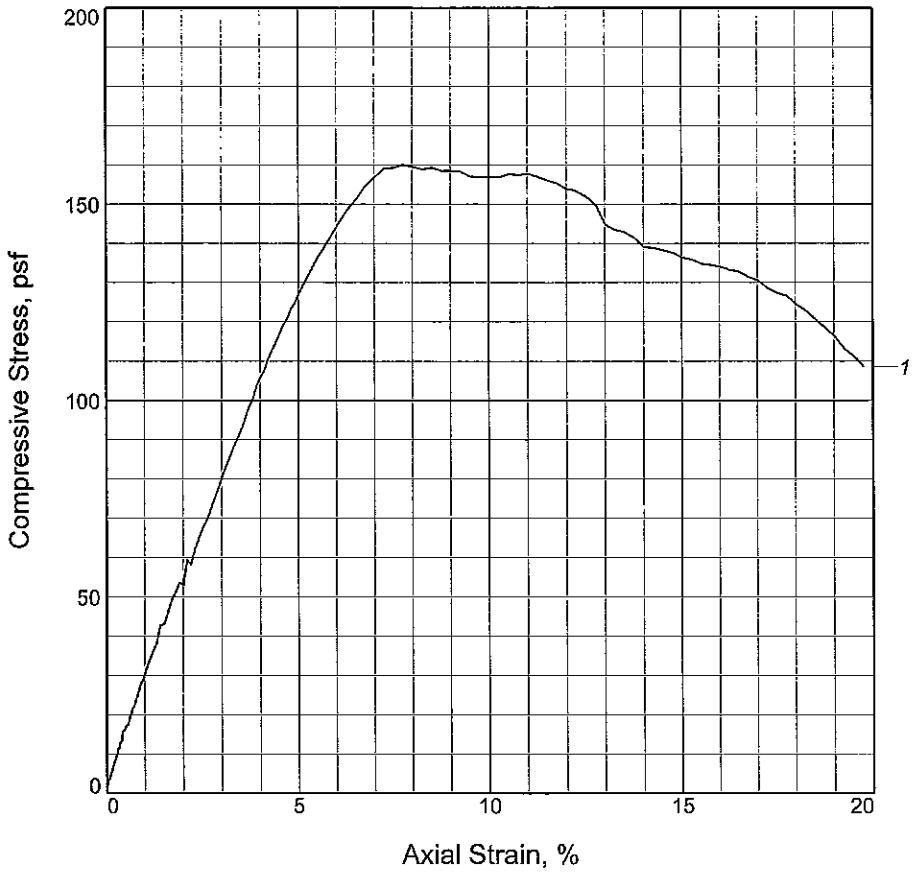
Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 6-8
Sample Number: 4

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	160.1			
Undrained shear strength, psf	80.0			
Failure strain, %	7.8			
Strain rate, %/min.	1.00			
Water content, %	117.1			
Wet density, pcf	83.9			
Dry density, pcf	38.7			
Saturation, %	93.1			
Void ratio	3.5199			
Specimen diameter, in.	2.750			
Specimen height, in.	5.608			
Height/diameter ratio	2.04			

Description: VSO G SICL W/ ORGS & FI SA, CH

LL = 78	**PL** = 36	**PI** = 42	**GS**= 2.8	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-4-09
Remarks:
TYPE FAILURE: VERTICAL FRACTURE+BULGE

ASTM D 2166

Client: URS

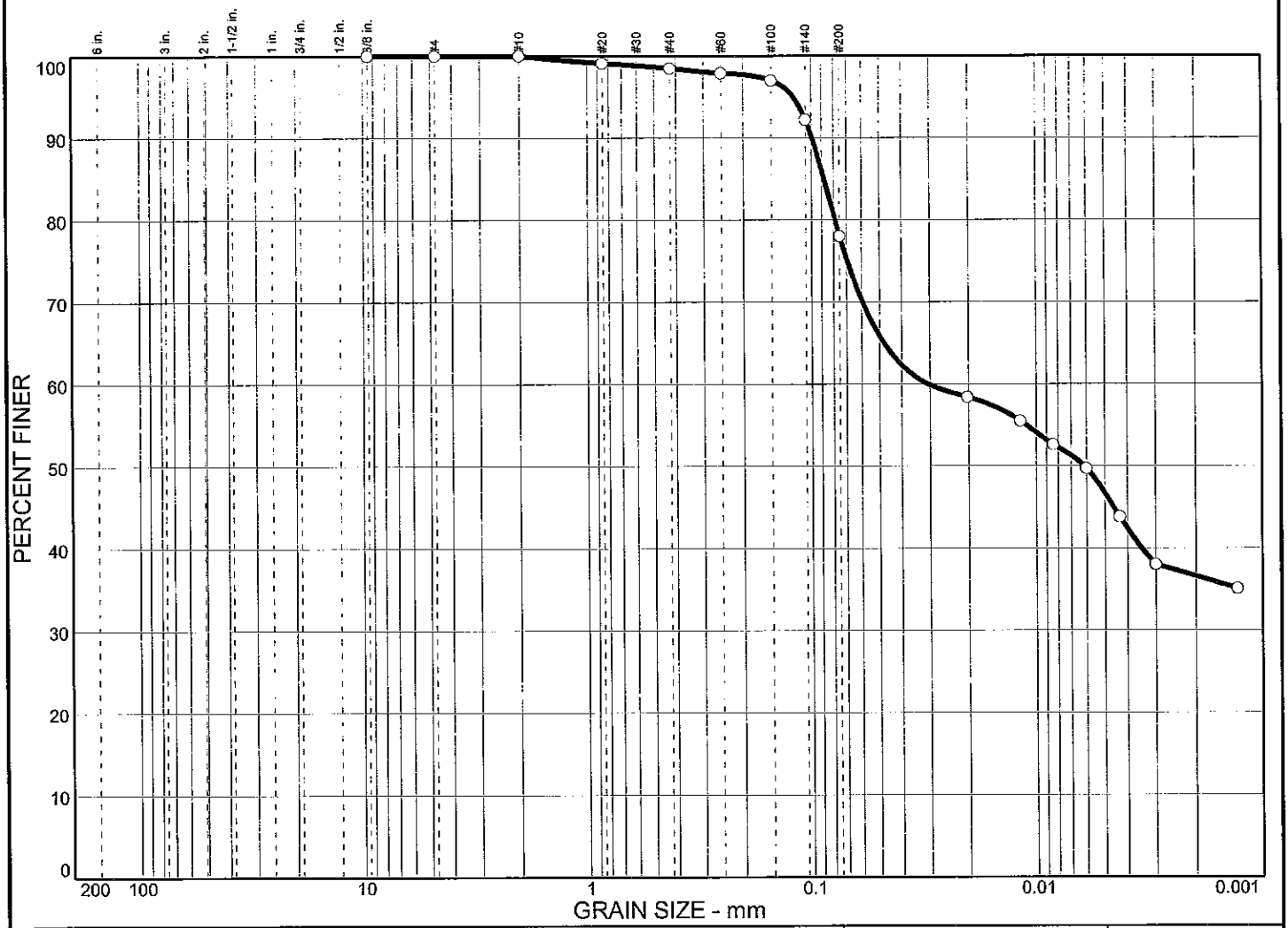
Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 13-15
Sample Number: 6

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	22.0	31.3	46.7

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	78		0.0880	0.0306						

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G SICL W/ ORGS & FI SA, CH	(CH)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-5 **Sample No.:** 6 **Elev./Depth:** 13-15

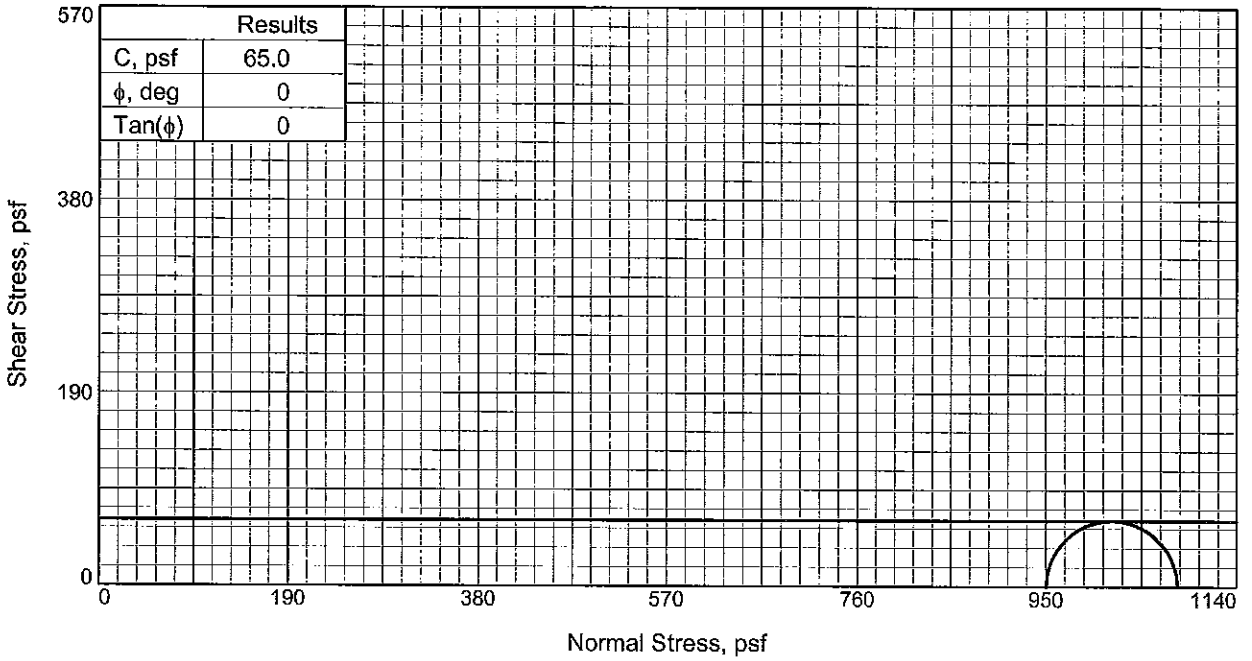
Remarks:

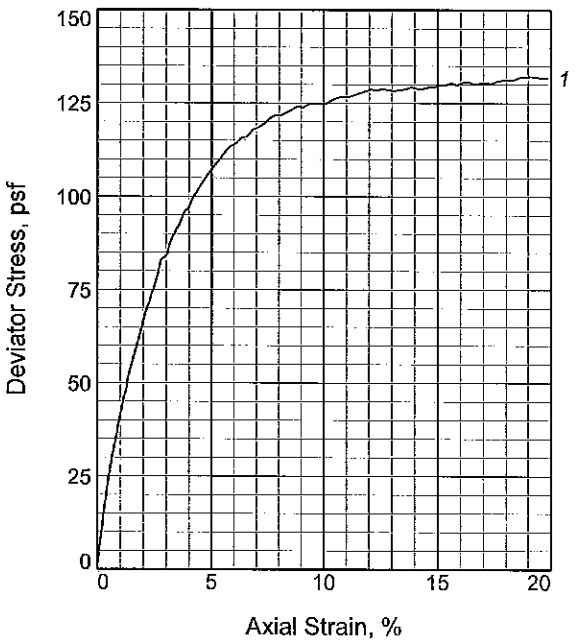
○ ASTM C136, D422

F.M.=0.03

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	138.2
	Dry Density, pcf	39.5
	Saturation, %	112.9
	Void Ratio	3.4268
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	138.2
	Dry Density, pcf	39.5
	Saturation, %	112.9
	Void Ratio	3.4268
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		6.600
Fail. Stress, psf		129.9
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1080.3
σ_3 Failure, psf		950.4

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ ORG PKTS, CH

Assumed Specific Gravity= 2.80

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 18-20

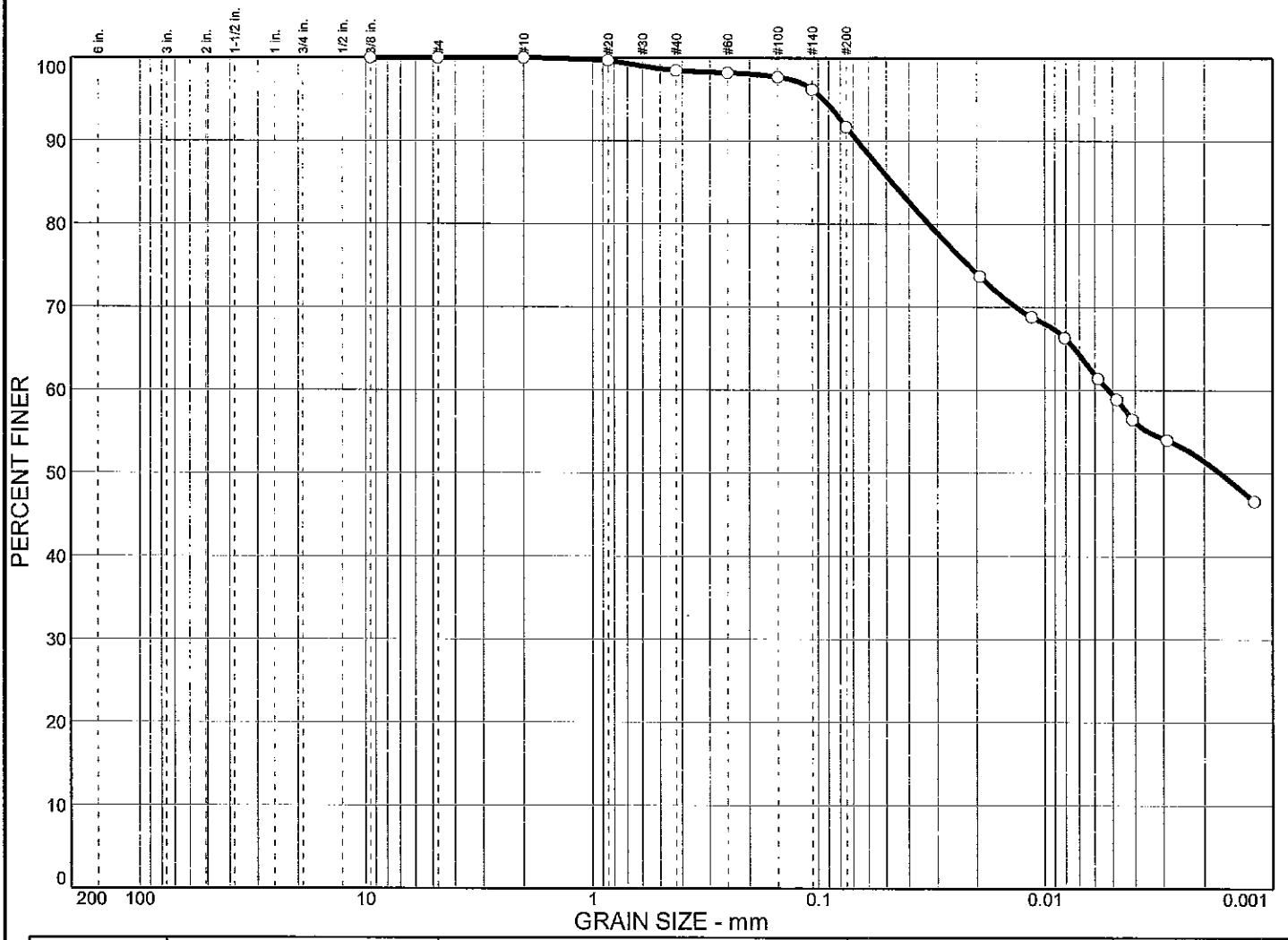
Sample Number: 7

Proj. No.: B09-012 **Date Sampled:** 3-11-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	8.3	32.2	59.5

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○			0.0473	0.0052	0.0017					

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ ORG PKTS, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-5 **Sample No.:** 7 **Elev./Depth:** 18-20

Remarks:

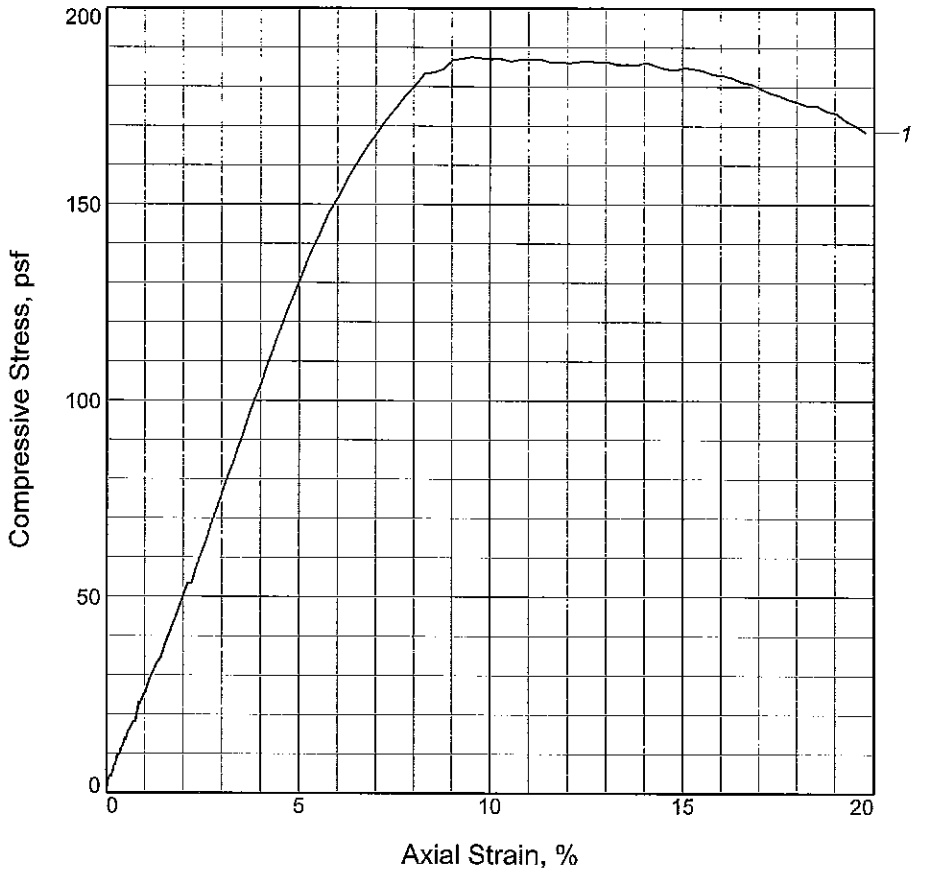
○ ASTM C136, D422

F.M.=0.02

Particle Size Distribution Report

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	187.7			
Undrained shear strength, psf	93.8			
Failure strain, %	9.5			
Strain rate, %/min.	1.00			
Water content, %	167.9			
Wet density, pcf	107.9			
Dry density, pcf	40.3			
Saturation, %	141.3			
Void ratio	3.2827			
Specimen diameter, in.	2.750			
Specimen height, in.	5.940			
Height/diameter ratio	2.16			

Description: VSO G CL BEC CLSI, CH

LL = 47	**PL** = 24	**PI** = 23	**GS=** 2.762	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-11-09

Remarks:
TYPE FAILURE: MULTI VERTICAL SHEAR

ASTM D 2166

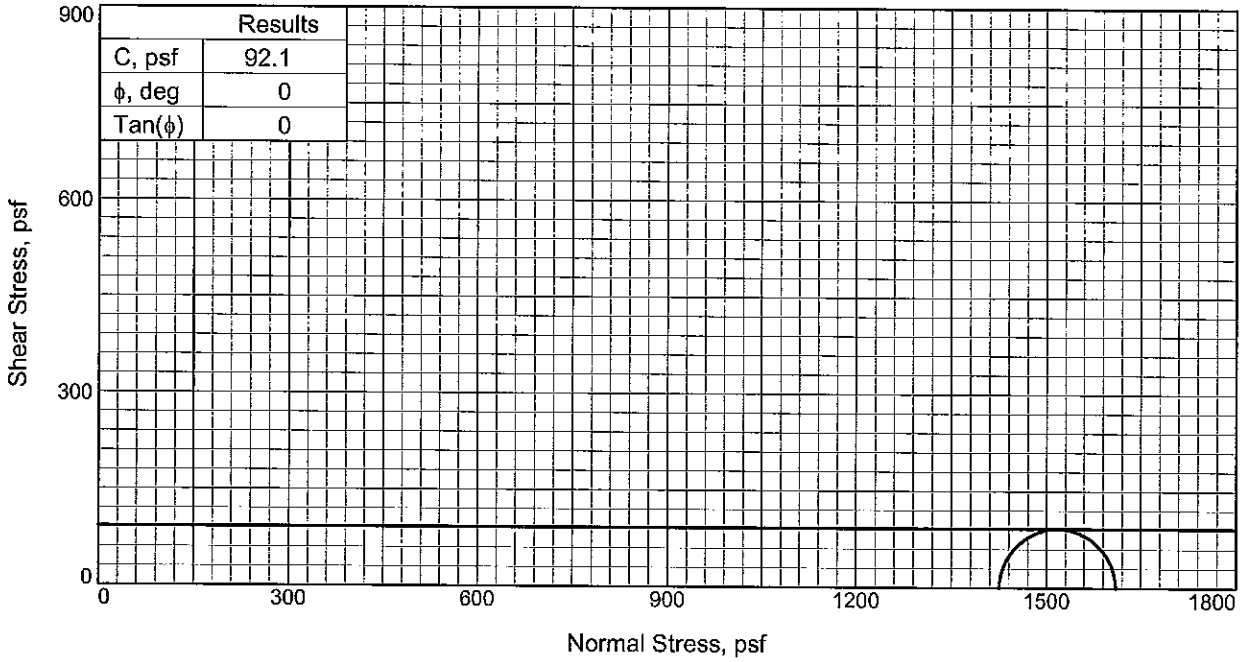
Client: URS

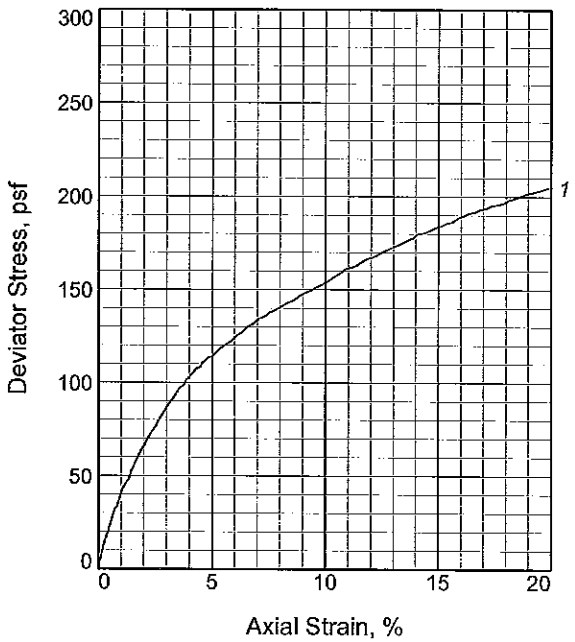
Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 23-25
Sample Number: 8

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	33.3
	Dry Density, pcf	81.1
	Saturation, %	83.6
	Void Ratio	1.0772
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	33.3
	Dry Density, pcf	81.1
	Saturation, %	83.6
	Void Ratio	1.0772
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		9.900
Fail. Stress, psf		184.2
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1609.8
σ_3 Failure, psf		1425.6

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: LO G CLSI W/ CL+SA, CL-ML

LL= 34 **PL=** 28 **PI=** 6

Assumed Specific Gravity= 2.70

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 28-30

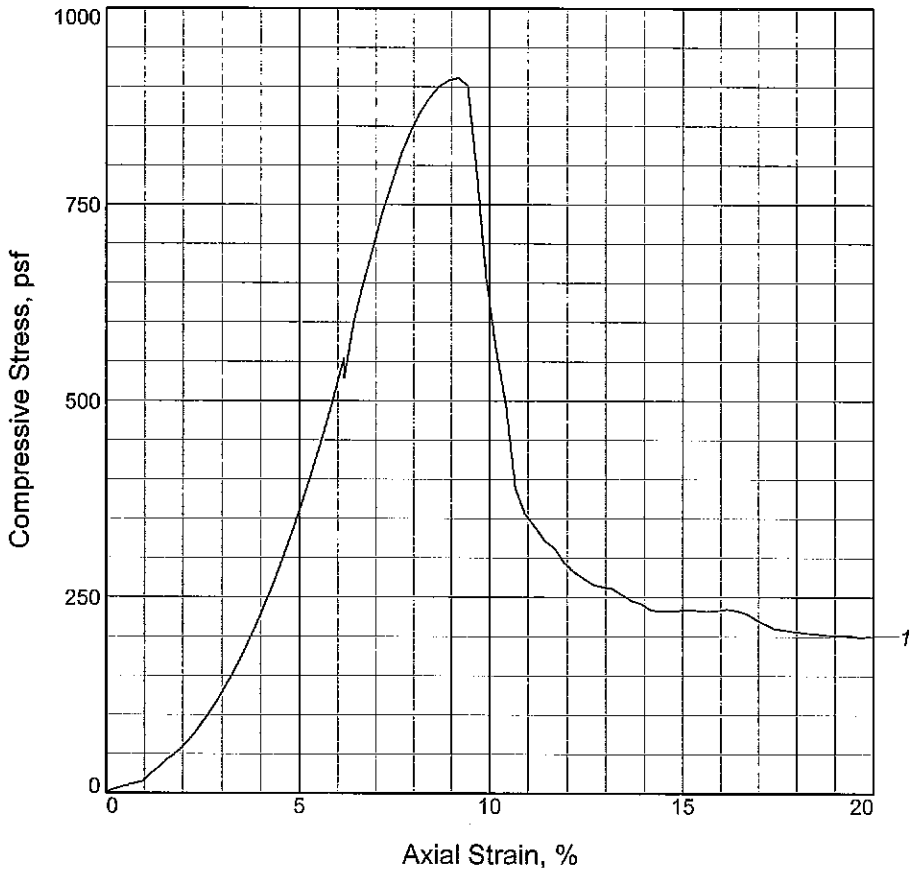
Sample Number: 9

Proj. No.: B09-012 **Date Sampled:** 3-11-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	911.8			
Undrained shear strength, psf	455.9			
Failure strain, %	9.2			
Strain rate, %/min.	1.00			
Water content, %	37.7			
Wet density, pcf	122.4			
Dry density, pcf	88.9			
Saturation, %	113.6			
Void ratio	0.8953			
Specimen diameter, in.	2.750			
Specimen height, in.	5.940			
Height/diameter ratio	2.16			

Description: LO G SI W/ CL LAYS, ML

LL = NP	**PL =**	**PI =** NP	**Assumed GS=** 2.70	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-11-09

Remarks:
TYPE FAILURE: 40 DEGREE SHEAR

ASTM D 2166

Client: URS

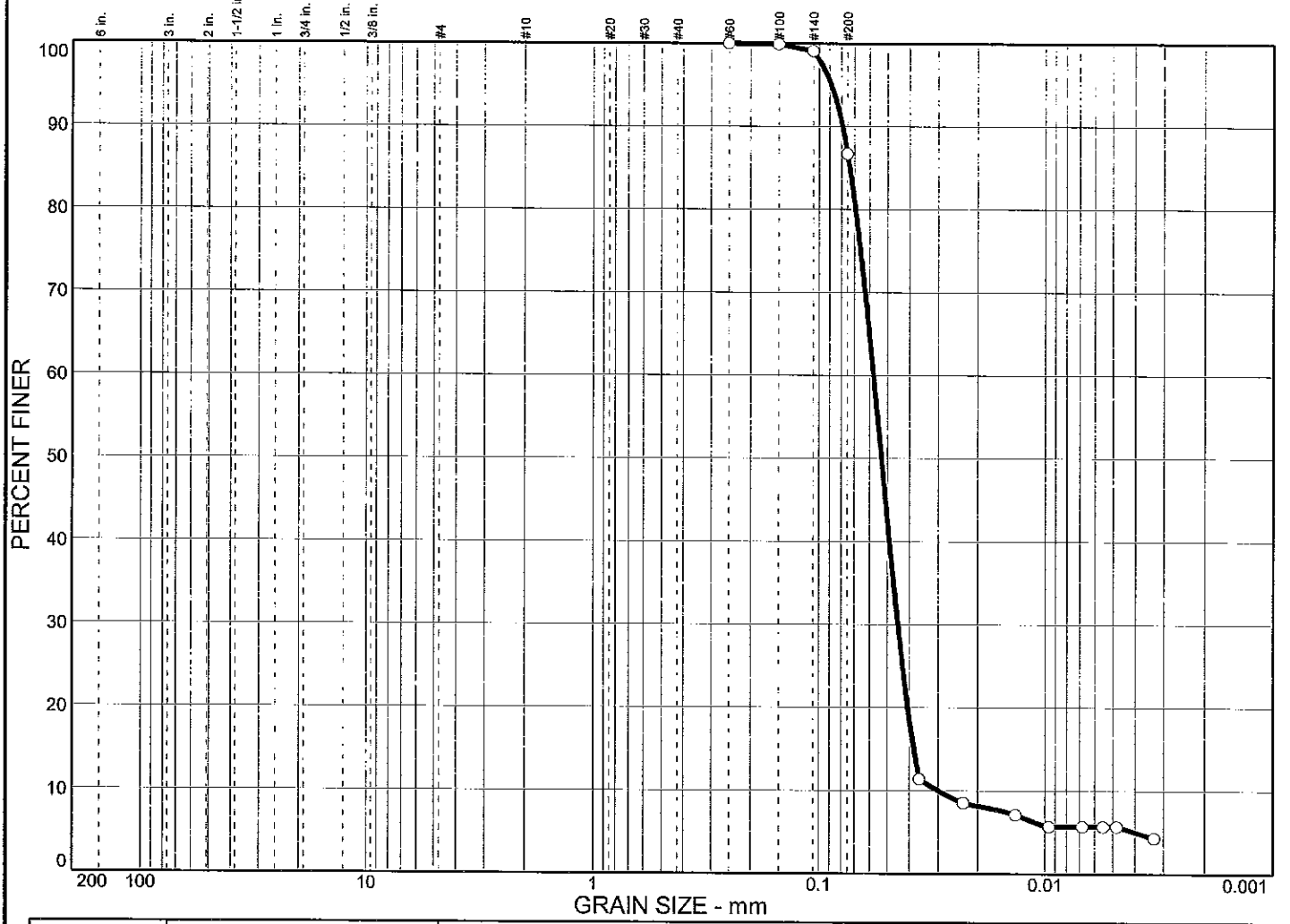
Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 38-40
Sample Number: 11

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	13.3	81.0	5.7

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	NP	NP	0.0733	0.0577	0.0532	0.0450	0.0383	0.0300	1.17	1.92

MATERIAL DESCRIPTION	USCS	AASHTO
○ LO G SI W/ CL LAYS, ML	ML	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-5 **Sample No.:** 11 **Elev./Depth:** 38-40

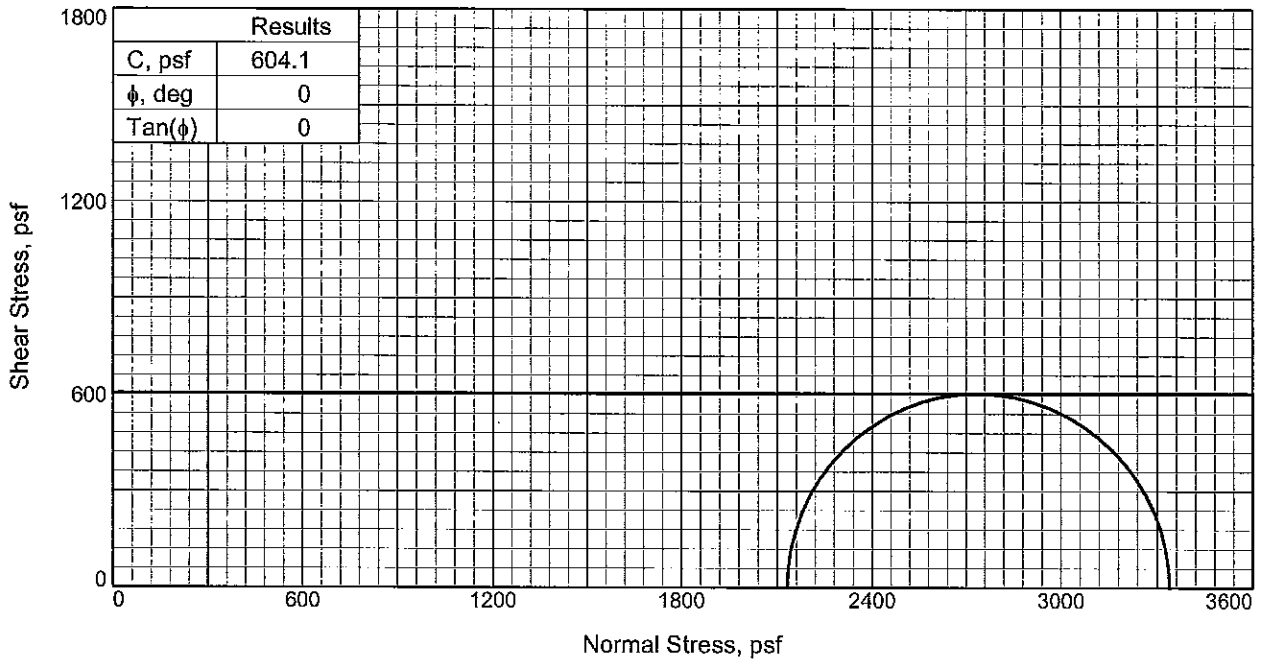
Remarks:

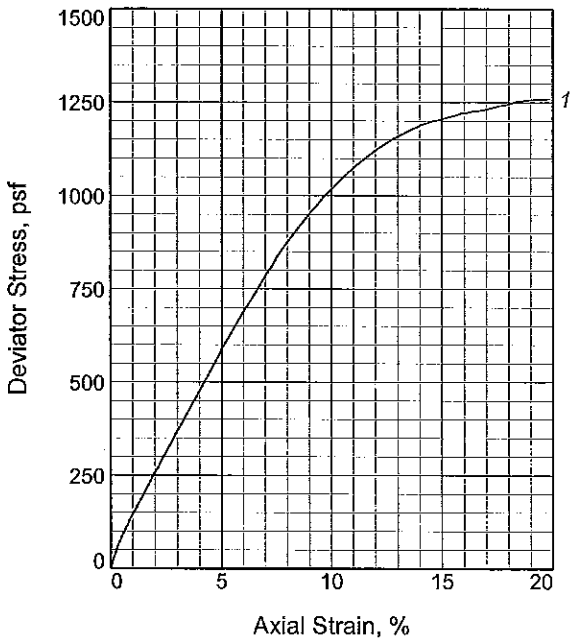
○ ASTM C136, D422

F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	31.6
	Dry Density, pcf	94.9
	Saturation, %	110.6
	Void Ratio	0.7663
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	31.6
	Dry Density, pcf	94.9
	Saturation, %	110.6
	Void Ratio	0.7663
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		14.800
Fail. Stress, psf		1208.1
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3339.3
σ_3 Failure, psf		2131.2

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: G CLSI W/ CL, CL-ML

Specific Gravity= 2.684

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 43-45

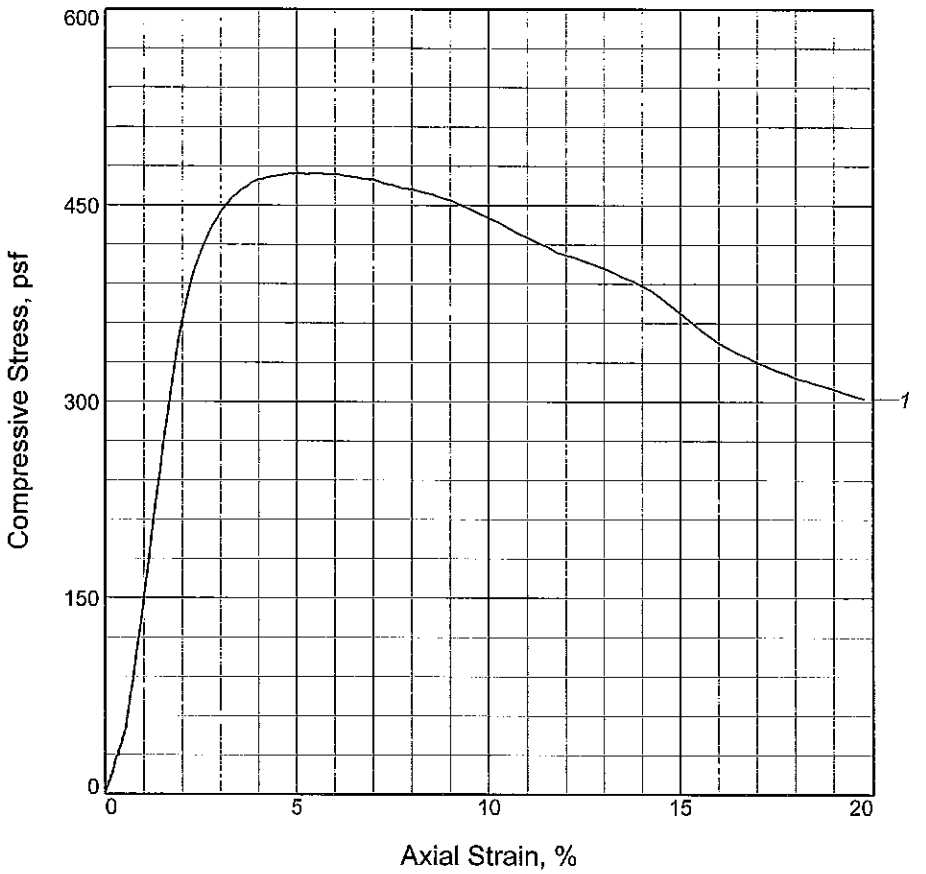
Sample Number: 12

Proj. No.: B09-012 **Date Sampled:** 3-11-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	475.0			
Undrained shear strength, psf	237.5			
Failure strain, %	5.0			
Strain rate, %/min.	1.00			
Water content, %	67.9			
Wet density, pcf	103.6			
Dry density, pcf	61.7			
Saturation, %	103.6			
Void ratio	1.8335			
Specimen diameter, in.	2.750			
Specimen height, in.	5.940			
Height/diameter ratio	2.16			

Description: VSO-SO G CL, CH

LL = 79	**PL =** 35	**PI =** 44	**Assumed GS=** 2.80	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-11-09
Remarks:
TYPE FAILURE: 45 DEGREE SHEAR

ASTM D 2166

Client: URS

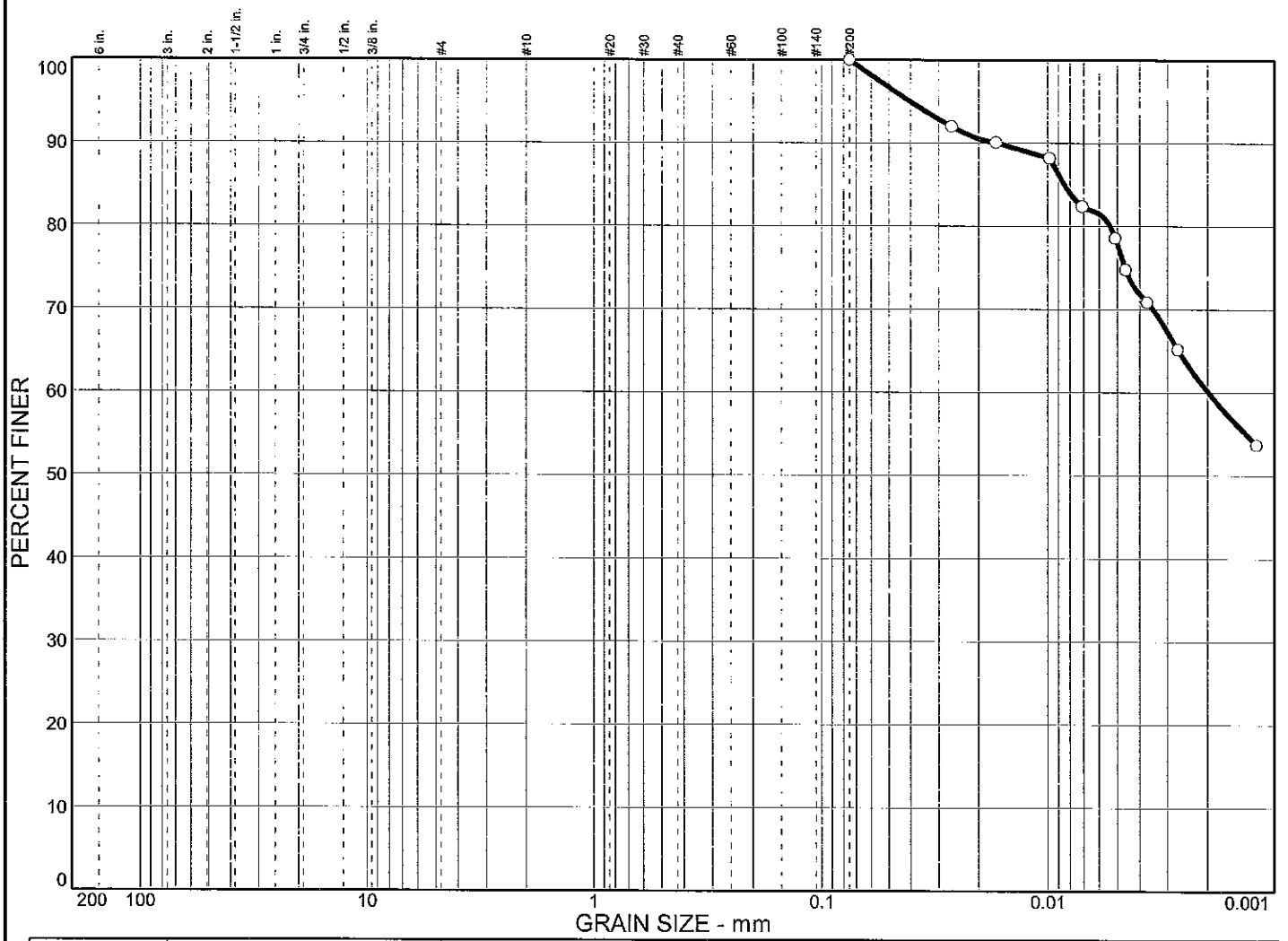
Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 48-50
Sample Number: 13

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	22.1	77.9

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	79	35	0.0085	0.0020						

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO-SO G CL, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

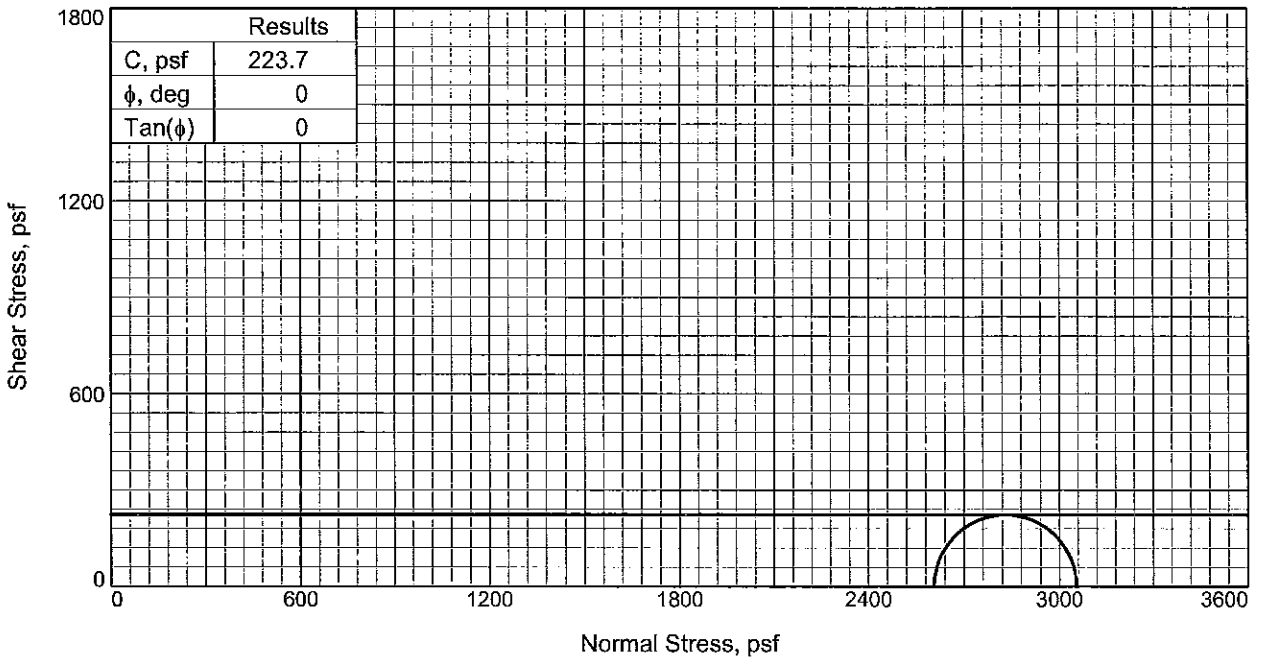
○ **Source:** B-5 **Sample No.:** 13 **Elev./Depth:** 48-50

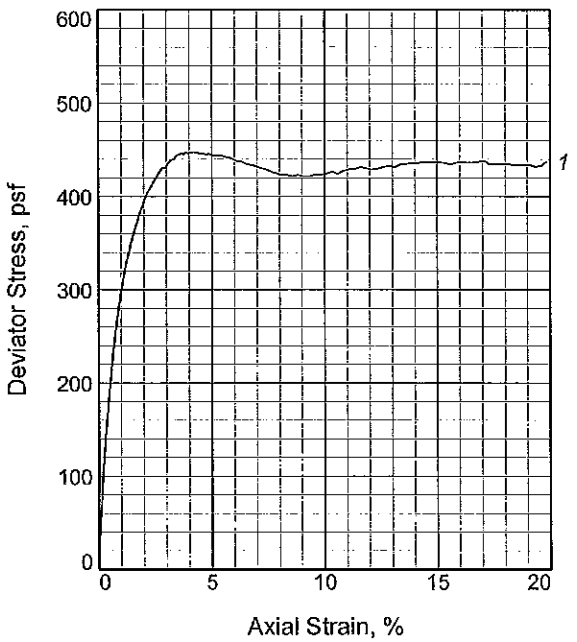
Remarks:

○ ASTM C136, D422

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	55.9
	Dry Density, pcf	68.7
	Saturation, %	101.4
	Void Ratio	1.5442
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	55.9
	Dry Density, pcf	68.7
	Saturation, %	101.4
	Void Ratio	1.5442
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		18.100
Fail. Stress, psf		447.5
Strain, %		4.3
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3053.9
σ_3 Failure, psf		2606.4

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: SO G CL W/ SI PKTS+TR ORGS, CH

Assumed Specific Gravity= 2.80

Remarks: TYPE FAILURE: 40 DEGREE SHEAR

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 53-55

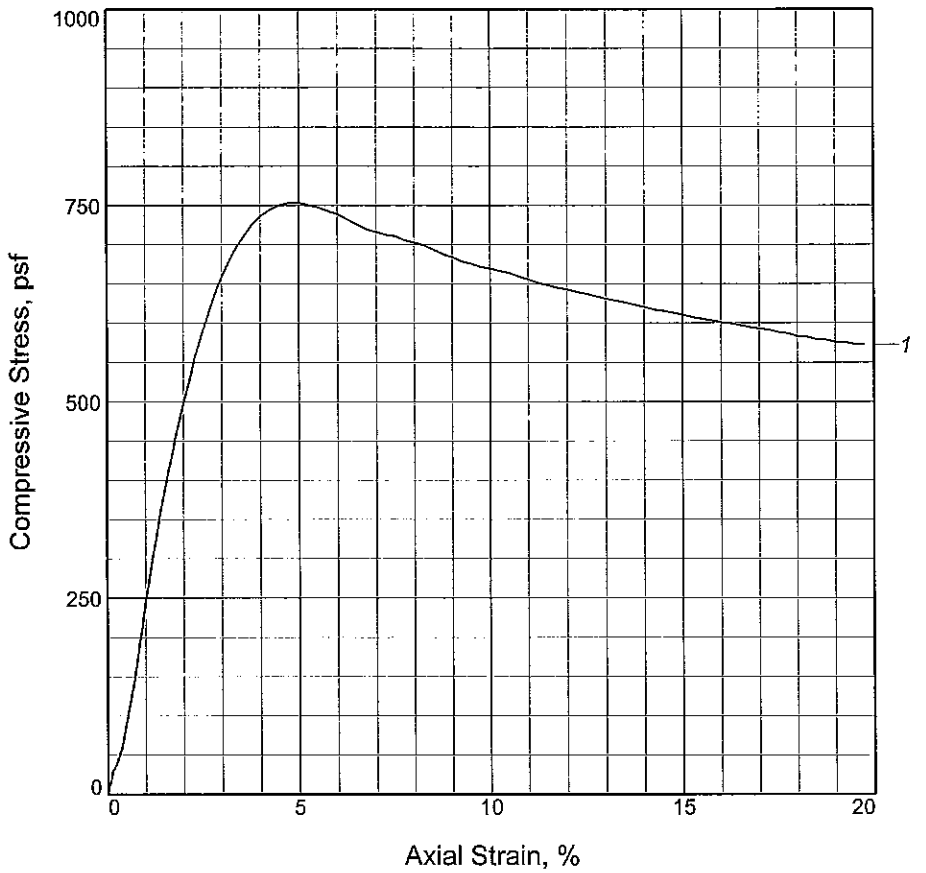
Sample Number: 14

Proj. No.: B09-012 **Date Sampled:** 3-11-09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

UNCONFINED COMPRESSION TEST



Sample No.	1			
Unconfined strength, psf	754.2			
Undrained shear strength, psf	377.1			
Failure strain, %	4.8			
Strain rate, %/min.	1.00			
Water content, %	52.7			
Wet density, pcf	112.5			
Dry density, pcf	73.7			
Saturation, %	107.6			
Void ratio	1.3730			
Specimen diameter, in.	2.750			
Specimen height, in.	5.940			
Height/diameter ratio	2.16			

Description: SO G CL W/ TR ORGS, CH

LL = 67	**PL =** 25	**PI =** 42	**Assumed GS=** 2.80	**Type:** UNDISTURBED

Project No.: B09-012
Date Sampled: 3-11-09

Remarks:
TYPE FAILURE: SLS

ASTM D 2166

Client: URS

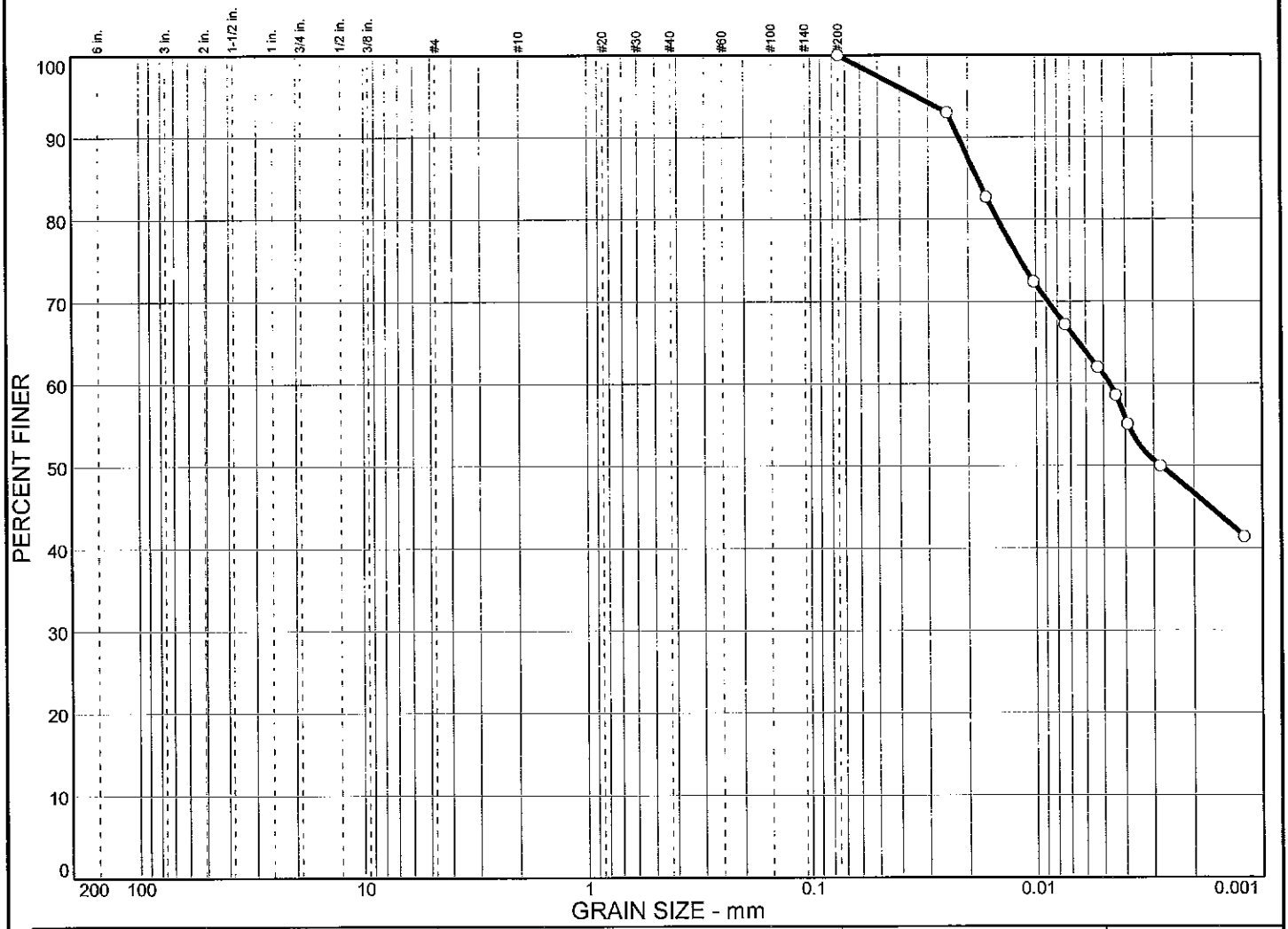
Project: BAYOU DUPONT

Source of Sample: B-5 **Depth:** 58-60
Sample Number: 15

UNCONFINED COMPRESSION TEST

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	38.9	61.1

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	67	25	0.0182	0.0047	0.0028					

MATERIAL DESCRIPTION	USCS	AASHTO
○ SO G CL W/ TR ORGS, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-5 **Sample No.:** 15 **Elev./Depth:** 58-60

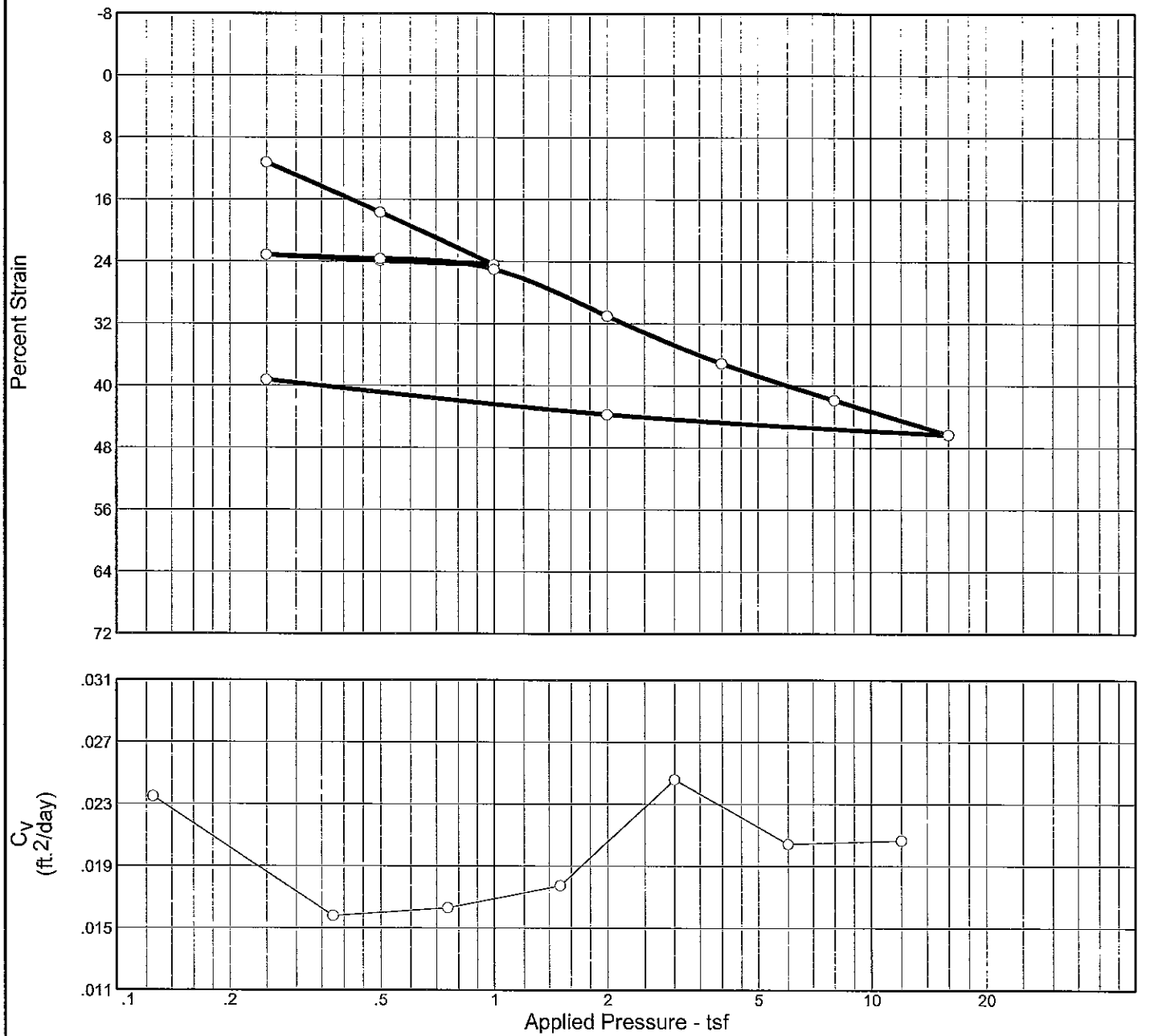
Remarks:

○ ASTM C136, D422

Particle Size Distribution Report

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
99.3 %	93.3 %	48.1	78	42	2.80	(CH)		2.633

MATERIAL DESCRIPTION

VSO G SICL W/ ORGS & FI SA, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

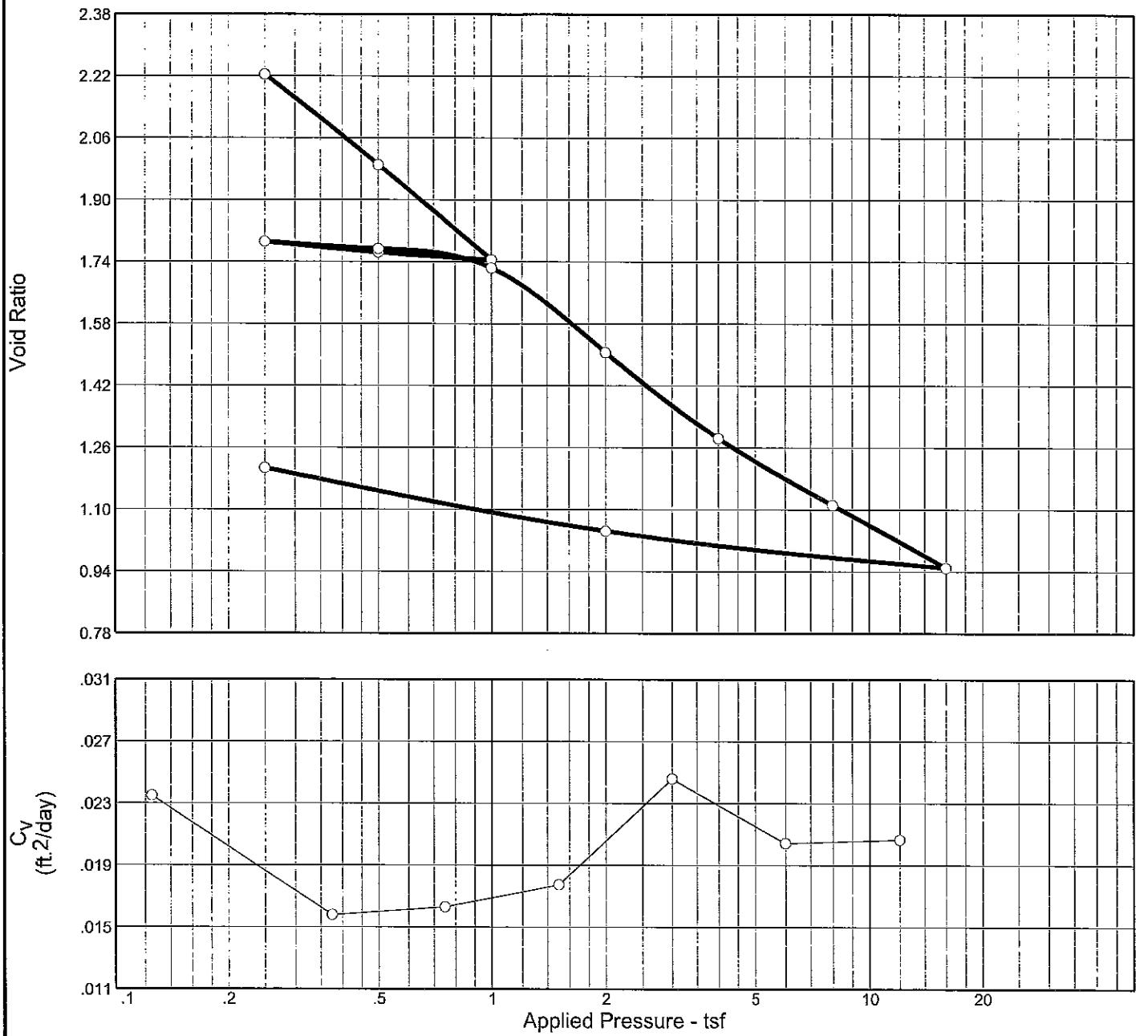
Source: B-5 **Sample No.:** 6 **Elev./Depth:** 13-15

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

Remarks:
ASTM D2435

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
99.3 %	93.3 %	48.1	78	42	2.80	(CH)		2.633

MATERIAL DESCRIPTION

VSO G SICL W/ ORGS & FI SA, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-5 **Sample No.:** 6 **Elev./Depth:** 13-15

CONSOLIDATION/SWELL TEST REPORT

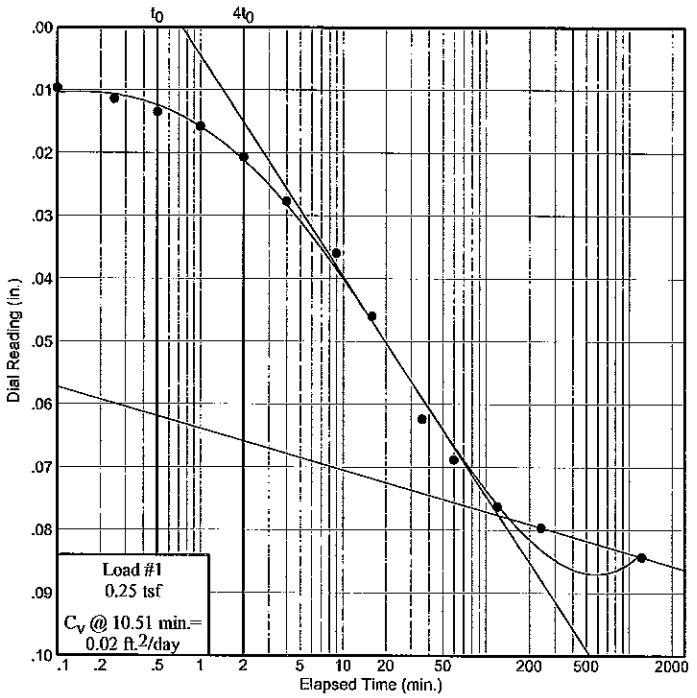
Southern Earth Sciences, Inc.

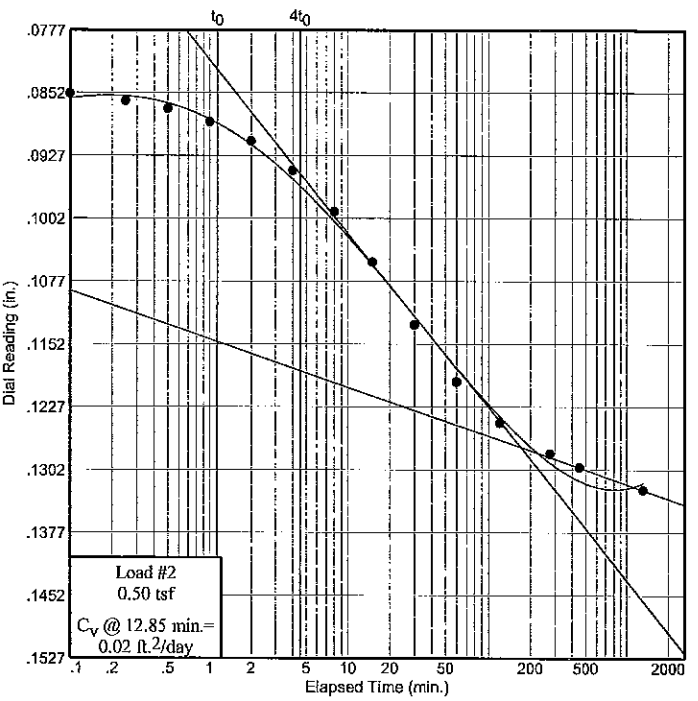
Remarks:
ASTM D2435

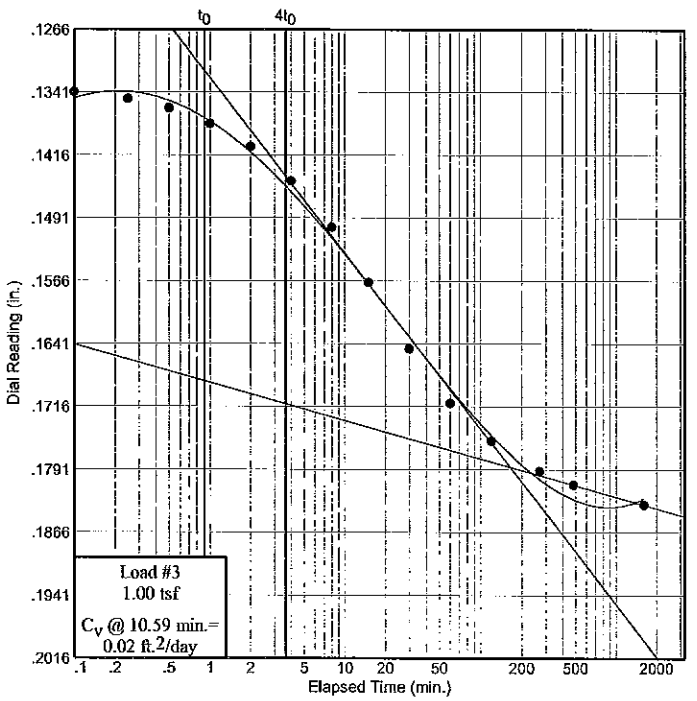
Dial Reading vs. Time

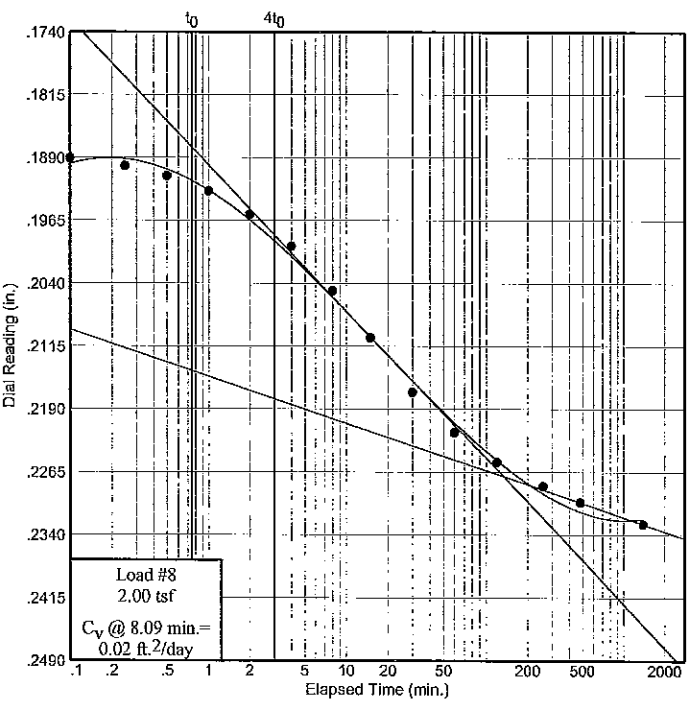
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-5 Sample No.: 6 Elev./Depth: 13-15









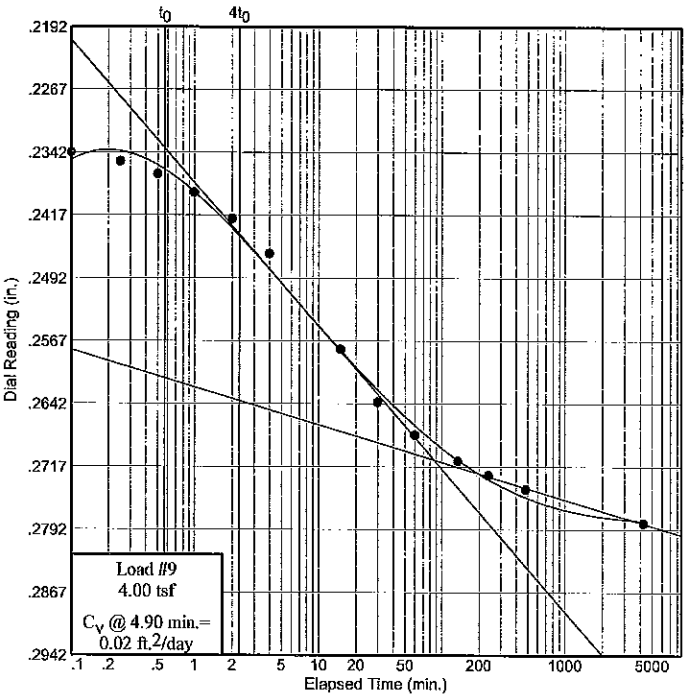
Dial Reading vs. Time

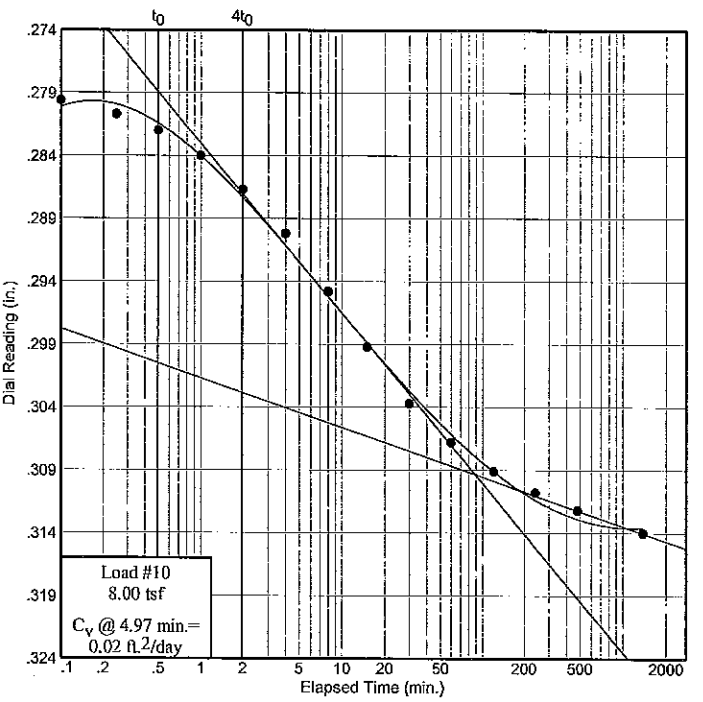
Southern Earth Sciences, Inc.

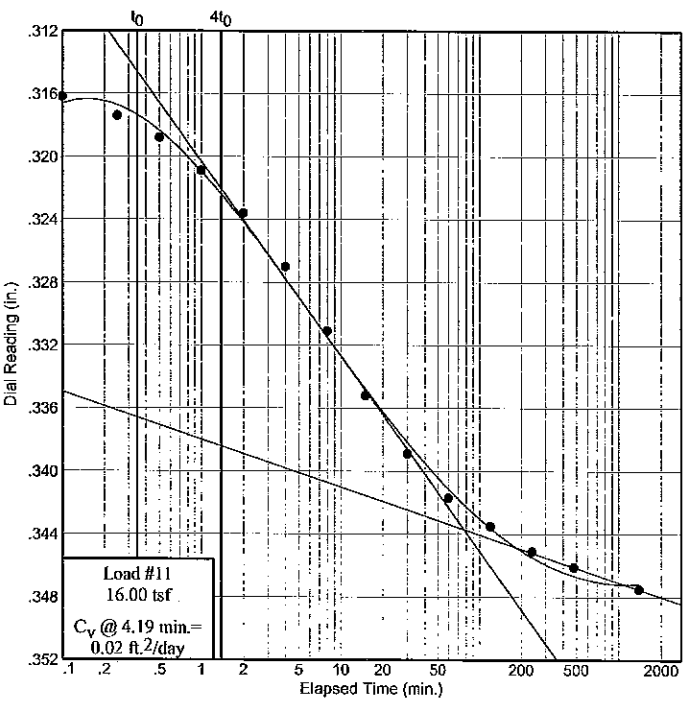
Dial Reading vs. Time

Project No.: B09-012
Project: BAYOU DUPONT

Source: B-5 Sample No.: 6 Elev./Depth: 13-15







Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-5
Sample No.: 6
Elev. or Depth: 13-15 **Sample Length(in./cm.):**
Location:
Description: VSO G SICL W/ ORGS & FI SA, CH
Liquid Limit: 78 **Plasticity Index:** 42
USCS: (CH) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST		AFTER TEST	
Wet w+t =	152.17 g.	Consolidometer # = 1		Wet w+t =	66.04 g.
Dry w+t =	108.67 g.			Dry w+t =	47.96 g.
Tare Wt. =	62.07 g.	Spec. Gravity = 2.80		Tare Wt. =	.00 g.
Height =	.75 in.	Height =	.75 in.		
Diameter =	2.50 in.	Diameter =	2.50 in.		
Weight =	89.91 g.	Defl. Table = Unit No. 9 Old 2.5in			
Moisture =	93.3 %	Ht. Solids =	0.2065 in.	Moisture =	37.7 %
Wet Den. =	93.0 pcf	Dry Wt. =	46.50 g.*	Dry Wt. =	47.96 g.
Dry Den. =	48.1 pcf	Void Ratio =	2.633	Void Ratio =	1.207
		Saturation =	99.3 %		

*** Initial dry weight used in calculations**

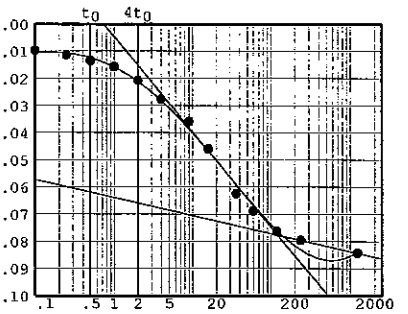
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				2.633	
0.25	0.08460	0.00030	0.02	0.009	2.224	11.2 Comprs.
0.50	0.13310	0.00050	0.02	0.009	1.990	17.7 Comprs.
1.00	0.18410	0.00080	0.02	0.007	1.745	24.4 Comprs.
0.50	0.18010	0.00080	0.11		1.764	23.9 Comprs.
0.25	0.17410	0.00050	0.03		1.792	23.1 Comprs.
0.50	0.17810	0.00070	0.12	0.001	1.773	23.7 Comprs.
1.00	0.18860	0.00090	0.11	0.004	1.724	25.0 Comprs.
2.00	0.23390	0.00120	0.02	0.010	1.506	31.0 Comprs.
4.00	0.28010	0.00170	0.02	0.009	1.284	37.1 Comprs.
8.00	0.31660	0.00260	0.02	0.008	1.112	41.9 Comprs.
16.00	0.35110	0.00360	0.02	0.007	0.950	46.3 Comprs.
2.00	0.32940	0.00150			1.044	43.7 Comprs.
0.25	0.29500	0.00060			1.207	39.3 Comprs.

C_c = 0.54 P_c = 3.58 tsf C_r = 0.11

Pressure: 0.25 tsf **TEST READINGS** **Load No. 1**

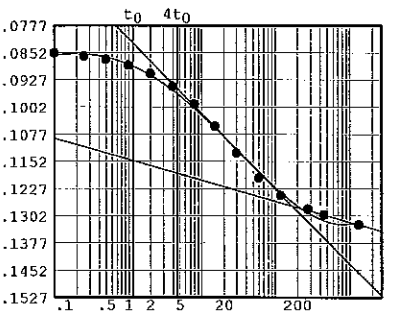
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	60.00	0.06910
2	0.10	0.01000	12	120.00	0.07660
3	0.25	0.01170	13	240.00	0.07990
4	0.50	0.01380	14	1230.00	0.08460
5	1.00	0.01610			
6	2.00	0.02100			
7	4.00	0.02800			
8	9.00	0.03630			
9	16.00	0.04630			
10	36.00	0.06270			



Void Ratio = 2.224 **Compression** = 11.2 %
D_0 = 0.00370 D_{50} = 0.04068 D_{100} = 0.07767
C_v at 10.5 min. = 0.02 ft.^{2}/day C_α = 0.009

Pressure: 0.50 tsf **TEST READINGS** **Load No. 2**

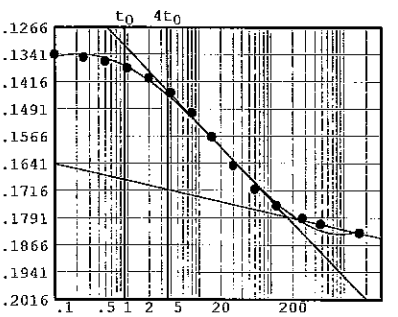
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.08460	11	60.00	0.12020
2	0.10	0.08580	12	120.00	0.12510
3	0.25	0.08670	13	275.00	0.12880
4	0.50	0.08760	14	450.00	0.13040
5	1.00	0.08920	15	1320.00	0.13310
6	2.00	0.09150			
7	4.00	0.09500			
8	8.00	0.09990			
9	15.00	0.10590			
10	30.00	0.11340			



Void Ratio = 1.990 **Compression** = 17.7 %
D_0 = 0.08132 D_{50} = 0.10439 D_{100} = 0.12746
C_v at 12.8 min. = 0.02 ft.^{2}/day C_α = 0.009

Pressure: 1.00 tsf **TEST READINGS** **Load No. 3**

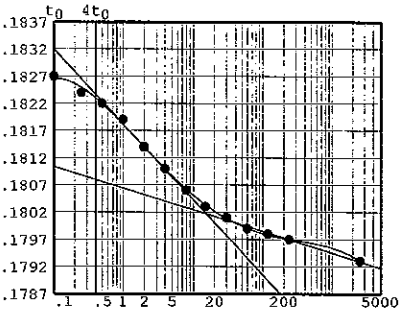
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.13310	11	60.00	0.17200
2	0.10	0.13490	12	120.00	0.17650
3	0.25	0.13570	13	270.00	0.18010
4	0.50	0.13680	14	480.00	0.18170
5	1.00	0.13870	15	1620.00	0.18410
6	2.00	0.14140			
7	4.00	0.14550			
8	8.00	0.15100			
9	15.00	0.15760			
10	30.00	0.16550			



Void Ratio = 1.745 **Compression** = 24.4 %
D_0 = 0.12904 D_{50} = 0.15392 D_{100} = 0.17880
C_v at 10.6 min. = 0.02 ft.^{2}/day C_α = 0.007

Pressure: 0.50 tsf **TEST READINGS** **Load No. 4**

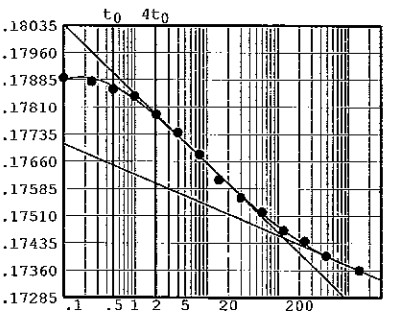
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.18410	11	60.00	0.18070
2	0.10	0.18350	12	120.00	0.18060
3	0.25	0.18320	13	240.00	0.18050
4	0.50	0.18300	14	2580.00	0.18010
5	1.00	0.18270			
6	2.00	0.18220			
7	4.00	0.18180			
8	8.00	0.18140			
9	15.00	0.18110			
10	30.00	0.18090			



Void Ratio = 1.764 **Compression** = 23.9 %
D_0 = 0.18302 D_{50} = 0.18160 D_{100} = 0.18017
C_v at 1.4 min. = 0.11 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 5**

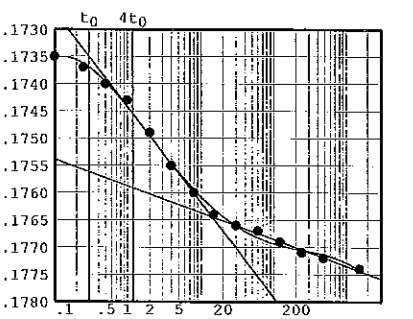
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.18010	11	60.00	0.17570
2	0.10	0.17940	12	120.00	0.17520
3	0.25	0.17930	13	240.00	0.17490
4	0.50	0.17910	14	480.00	0.17450
5	1.00	0.17890	15	1440.00	0.17410
6	2.00	0.17840			
7	4.00	0.17790			
8	8.00	0.17730			
9	15.00	0.17660			
10	30.00	0.17610			



Void Ratio = 1.792 **Compression** = 23.1 %
D_0 = 0.17952 D_{50} = 0.17701 D_{100} = 0.17450
C_v at 5.8 min. = 0.03 ft.^{2}/day

Pressure: 0.50 tsf **TEST READINGS** **Load No. 6**

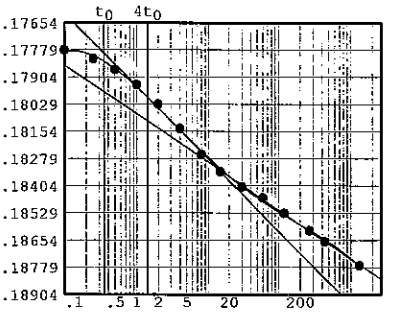
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.17410	11	60.00	0.17740
2	0.10	0.17420	12	120.00	0.17760
3	0.25	0.17440	13	240.00	0.17780
4	0.50	0.17470	14	480.00	0.17790
5	1.00	0.17500	15	1530.00	0.17810
6	2.00	0.17560			
7	4.00	0.17620			
8	8.00	0.17670			
9	15.00	0.17710			
10	30.00	0.17730			



Void Ratio = 1.773 **Compression** = 23.7 %
D_0 = 0.17283 D_{50} = 0.17463 D_{100} = 0.17644
C_v at 1.3 min. = 0.12 ft.^{2}/day C_α = 0.001

Pressure: 1.00 tsf **TEST READINGS** **Load No. 7**

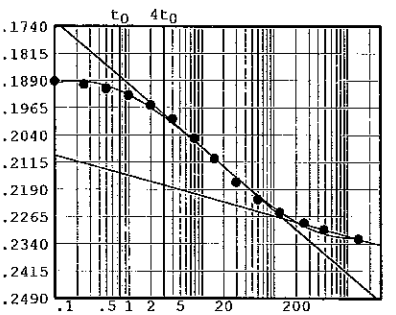
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.17810	11	60.00	0.18550
2	0.10	0.17870	12	120.00	0.18620
3	0.25	0.17910	13	270.00	0.18700
4	0.50	0.17960	14	440.00	0.18750
5	1.00	0.18030	15	1320.00	0.18860
6	2.00	0.18120			
7	4.00	0.18230			
8	8.00	0.18350			
9	15.00	0.18430			
10	30.00	0.18500			



Void Ratio = 1.724 **Compression** = 25.0 %
D_0 = 0.17667 D_{50} = 0.17995 D_{100} = 0.18324
C_v **at 1.4 min.** = 0.11 ft.^{2}/day C_α = 0.004

Pressure: 2.00 tsf **TEST READINGS** **Load No. 8**

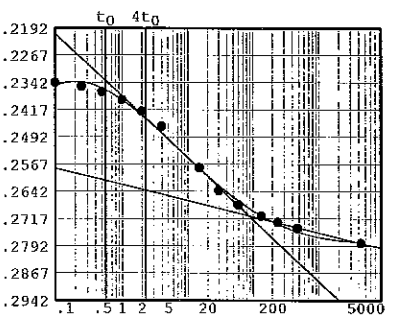
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.18860	11	60.00	0.22300
2	0.10	0.19030	12	120.00	0.22650
3	0.25	0.19120	13	258.00	0.22940
4	0.50	0.19240	14	480.00	0.23130
5	1.00	0.19420	15	1400.00	0.23390
6	2.00	0.19700			
7	4.00	0.20080			
8	8.00	0.20610			
9	15.00	0.21170			
10	30.00	0.21820			



Void Ratio = 1.506 **Compression** = 31.0 %
D_0 = 0.18456 D_{50} = 0.20578 D_{100} = 0.22701
C_v **at 8.1 min.** = 0.02 ft.^{2}/day C_α = 0.010

Pressure: 4.00 tsf **TEST READINGS** **Load No. 9**

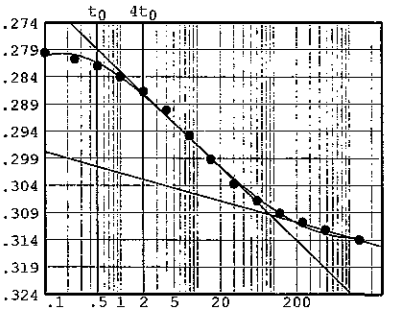
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.23390	11	135.00	0.27270
2	0.10	0.23590	12	240.00	0.27440
3	0.25	0.23700	13	480.00	0.27610
4	0.50	0.23850	14	4290.00	0.28010
5	1.00	0.24070			
6	2.00	0.24380			
7	4.00	0.24800			
8	15.00	0.25940			
9	30.00	0.26570			
10	60.00	0.26960			



Void Ratio = 1.284 **Compression** = 37.1 %
D_0 = 0.22833 D_{50} = 0.24960 D_{100} = 0.27087
C_v **at 4.9 min.** = 0.02 ft.^{2}/day C_α = 0.009

Pressure: 8.00 tsf **TEST READINGS** **Load No. 10**

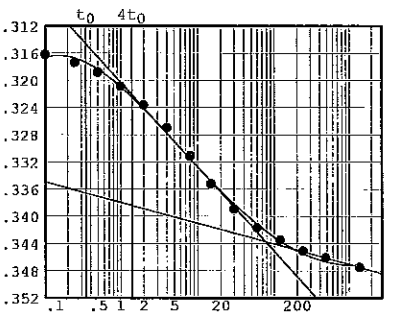
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.28010	11	60.00	0.30940
2	0.10	0.28220	12	120.00	0.31170
3	0.25	0.28330	13	240.00	0.31340
4	0.50	0.28460	14	480.00	0.31480
5	1.00	0.28660	15	1380.00	0.31660
6	2.00	0.28930			
7	4.00	0.29280			
8	8.00	0.29740			
9	15.00	0.30180			
10	30.00	0.30630			



Void Ratio = 1.112 **Compression =** 41.9 %
D_0 = 0.27550 D_{50} = 0.29241 D_{100} = 0.30932
C_v **at 5.0 min.** = 0.02 ft.^{2}/day C_α = 0.008

Pressure: 16.00 tsf **TEST READINGS** **Load No. 11**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.31660	11	60.00	0.34530
2	0.10	0.31980	12	120.00	0.34710
3	0.25	0.32100	13	240.00	0.34870
4	0.50	0.32240	14	480.00	0.34970
5	1.00	0.32450	15	1390.00	0.35110
6	2.00	0.32720			
7	4.00	0.33060			
8	8.00	0.33470			
9	15.00	0.33880			
10	30.00	0.34250			



Void Ratio = 0.950 **Compression =** 46.3 %
D_0 = 0.31231 D_{50} = 0.32801 D_{100} = 0.34370
C_v **at 4.2 min.** = 0.02 ft.^{2}/day C_α = 0.007

Southern Earth Sciences, Inc.

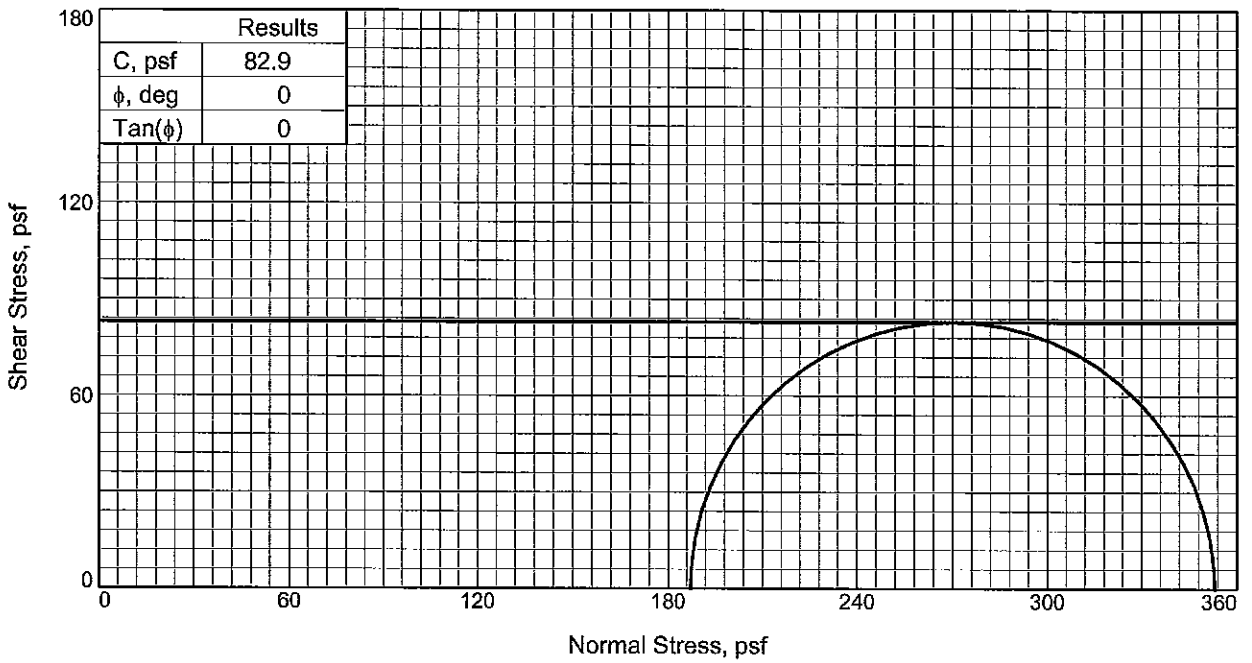
Laboratory Test Results

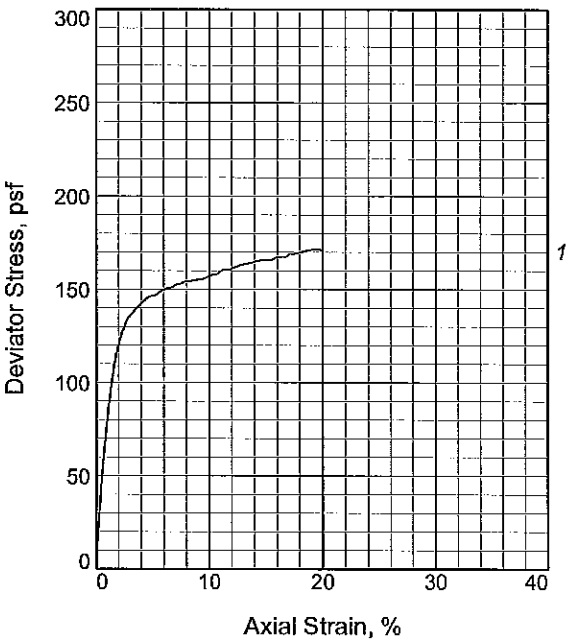
Project: **Bayou DuPont** Technical Responsibility: Quality Assurance Officer

Client: URS

7389 Florida Blvd., Suite 300, Baton Rouge, LA 70806 Project No.: **B09-012** PM: S. Aviles Date of Issue: 3/12/2009

			ASTM DESIGNATION																
			D2216	D4318			D427	D2166		D2166	D2850	D422, C136 or C117					D2974	USCS	
				Atterberg Limits						Cohesion		Grain Size (% Passing)							
Boring No.	Depth (ft)	Classification	ω %	LL	PL	PI	SL	γ_{wet} pcf	γ_{dry} pcf	U psf	UU psf	Gravel	Sand	Silt	Clay	#200	Organic Content %		Confining Stress, Resistivity and Remarks
B-6	0-2	Very Soft Peat with clay	194.0	289	144	145	26.4	66.4	22.6								8.4	(PT)	
B-6	2-4	Very Soft, Brown Organic CLAY with peat	374.2					83.2	17.5		82.9							(PT/OH/CH)	Confining Pressure: 1.3 psi
B-6	4-6	Very Soft, Gray CLAY with organic pockets	122.8	120	44	76		95.3	42.8		65.7					92.2	4.8	(CH)	Specific Gravity: 2.797 Confining Pressure: 2.0 psi
B-6	8-10	Very Soft, Gray CLAY with organic pockets	98.9	67	34	33		104.0	52.3		98.8		1.9	45.6	52.5		4.2	(CH)	Confining Pressure: 3.3 psi
B-6	13-15	Very Soft, Gray CLAY with organic pockets	123.5					98.7	44.2									(CH)	Specific Gravity: 2.798
B-6	18-20	Very Soft, Gray CLAY becoming Gray SANDY SILT with clay	104.0				20.0	96.3	47.2		99.5		0.0	30.2	69.8		4.2	(CH)	Confining Pressure: 6.6 psi
B-6	23-25	Very Soft, Gray CLAY with organics becoming Gray SILT with clay	83.1	130	40	90		115.8	63.2		163.0							(CH)	Confining Pressure: 8.2 psi
B-6	28-30	Very Soft, Gray CLAY with silt	70.6				17.0	103.9	60.9		175.6							(CH)	Specific Gravity: 2.774 Confining Pressure: 9.9 psi
B-6	33-35	Soft, Gray CLAY becoming Gray SILT with clay	45.9	83	31	52		122.0	83.6		360.8		0.0	39.1	60.9			(CH)	Confining Pressure: 11.5 psi
B-6	38-40	Soft, Gray CLAY with trace silt and organics	61.5					109.5	67.8							100.0	2.1	(CH)	
B-6	43-45	Loose, Gray SILT with trace organics, trace silt and silt lenses, with clay	49.5	55	33	22		114.2	76.4		334.6		0.0	45.3	54.7			(MH)	Confining Pressure: 14.9 psi
B-6	48-50	Medium, Gray CLAY with silt pockets	50.4					121.0	80.5		338.4							(CH)	Confining Pressure: 16.5 psi
B-6	53-55	Soft, Gray CLAY with trace silt	63.0	82	31	51	20.4	107.6	66.0		603.3		0.0	41.9	58.1			(CH)	Confining Pressure: 18.2 psi
B-6	58-60	Soft, Gray CLAY with trace silt	70.8					109.1	63.8		457.2						4.5	(CH)	Confining Pressure: 19.7 psi





Sample No.		1
Initial	Water Content, %	374.2
	Dry Density, pcf	17.5
	Saturation, %	117.1
	Void Ratio	8.7865
	Diameter, in.	2.875
	Height, in.	5.940
At Test	Water Content, %	374.2
	Dry Density, pcf	17.5
	Saturation, %	117.1
	Void Ratio	8.7865
	Diameter, in.	2.875
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		1.300
Fail. Stress, psf		165.9
Strain, %		14.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		353.1
σ_3 Failure, psf		187.2

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSo Br Org Cl w/ Pt, CH

Assumed Specific Gravity= 2.75

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

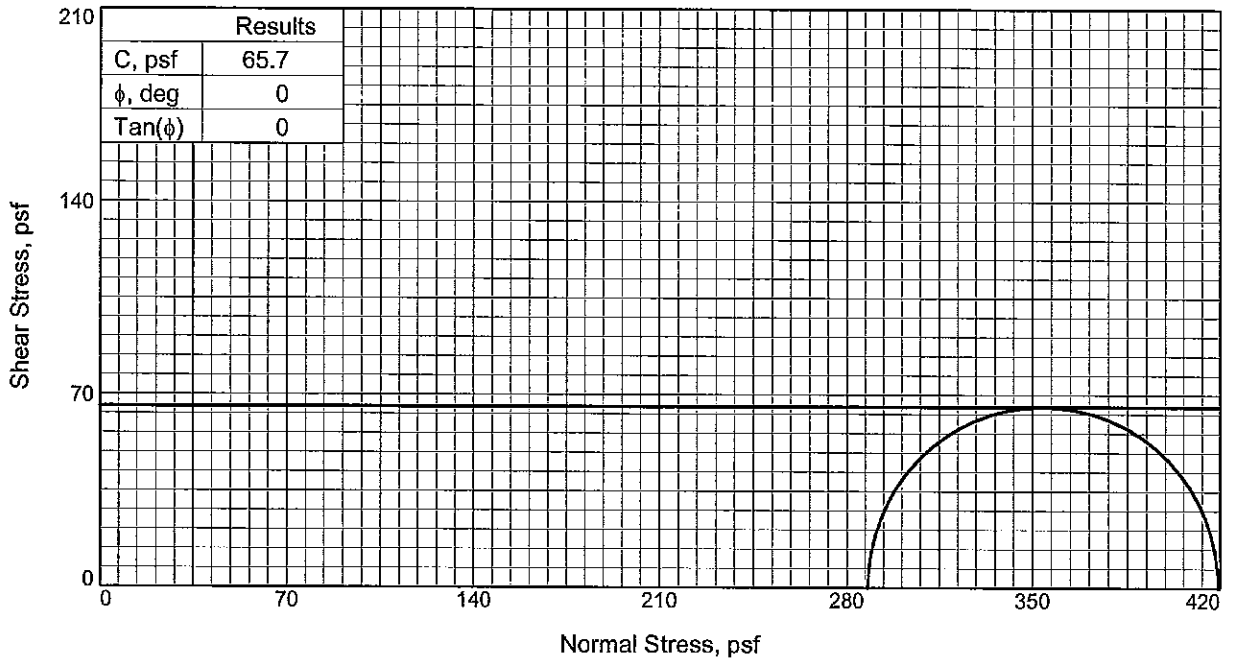
Source of Sample: B-6 **Depth:** 2-4

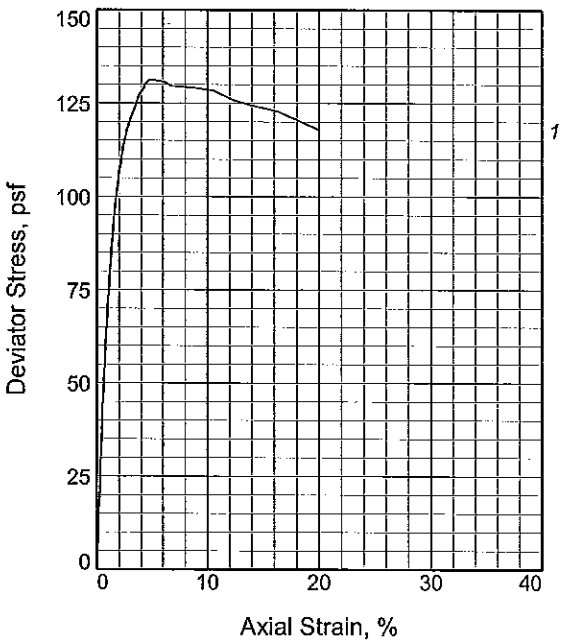
Sample Number: 2

Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	122.8
	Dry Density, pcf	42.8
	Saturation, %	111.5
	Void Ratio	3.0844
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	122.8
	Dry Density, pcf	42.8
	Saturation, %	111.5
	Void Ratio	3.0844
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.000
Fail. Stress, psf		131.4
Strain, %		4.9
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		419.4
σ_3 Failure, psf		288.0

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSo G Cl w/ Org Pkts, CH

LL= 120 **PL=** 44 **PI=** 76
Assumed Specific Gravity= 2.8
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

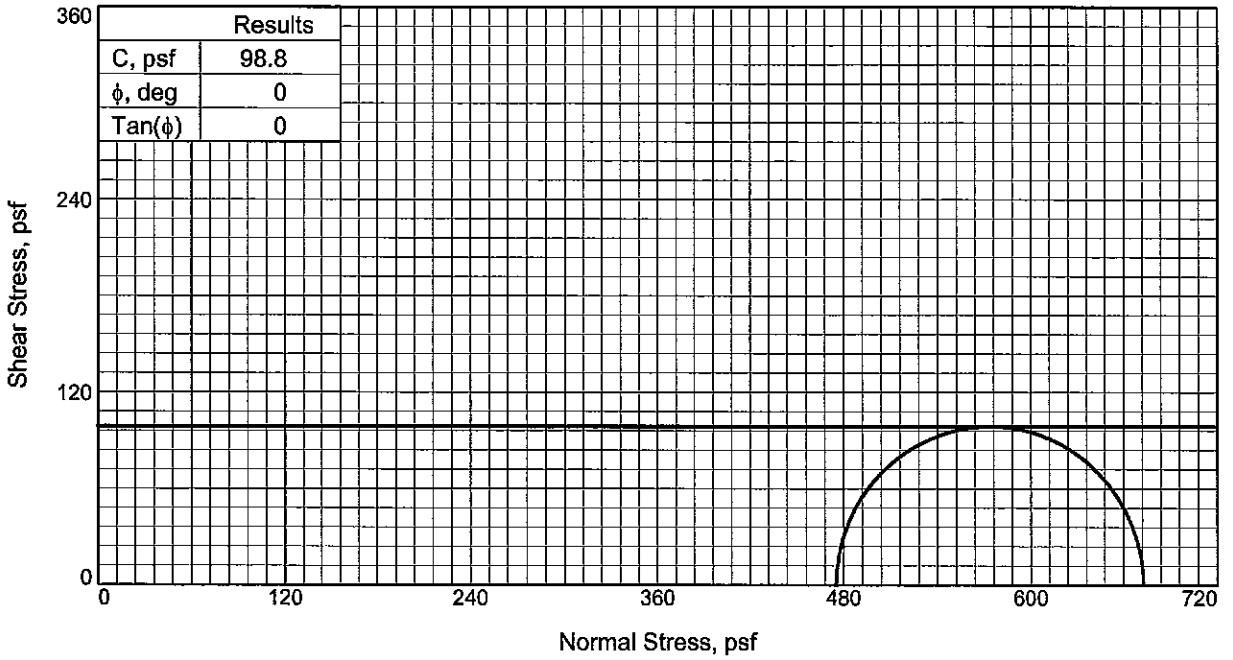
Client: URS

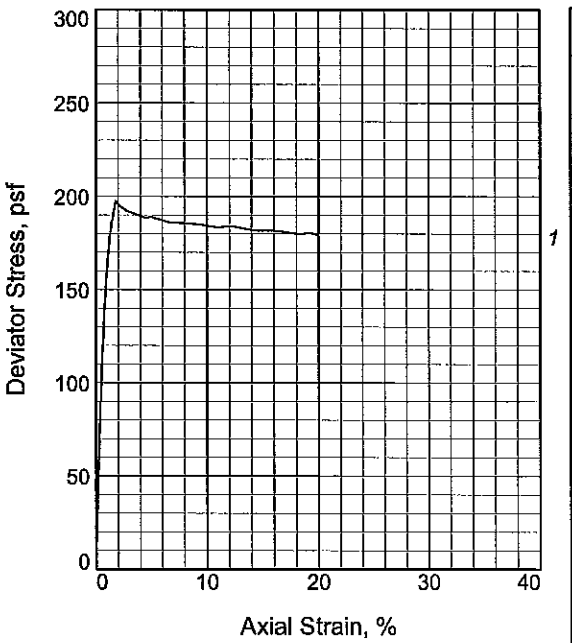
Project: BAYOU DUPONT

Source of Sample: B-6 **Depth:** 4-6
Sample Number: 3
Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	98.9
	Dry Density, pcf	52.3
	Saturation, %	118.2
	Void Ratio	2.3438
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	98.9
	Dry Density, pcf	52.3
	Saturation, %	118.2
	Void Ratio	2.3438
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		3.300
Fail. Stress, psf		197.6
Strain, %		1.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		672.8
σ_3 Failure, psf		475.2

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSo G Cl w/ Org Pkts, CH

LL= 67 **PL=** 34 **PI=** 33

Assumed Specific Gravity= 2.8

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-6 **Depth:** 8-10

Sample Number: 5

Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	1.9	45.6	52.5

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	67	34	0.0298	0.0073	0.0043					

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSo G Cl w/ Org Pkts, CH	(CH)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-6 **Sample No.:** 5 **Elev./Depth:** 8-10

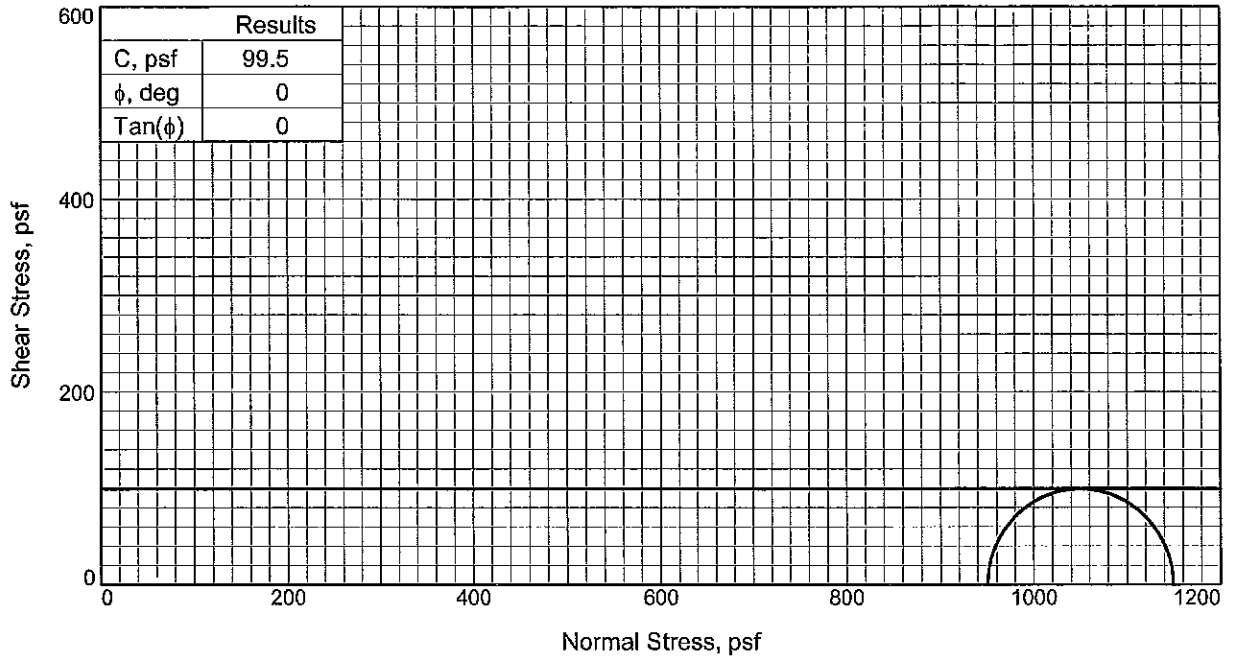
Remarks:

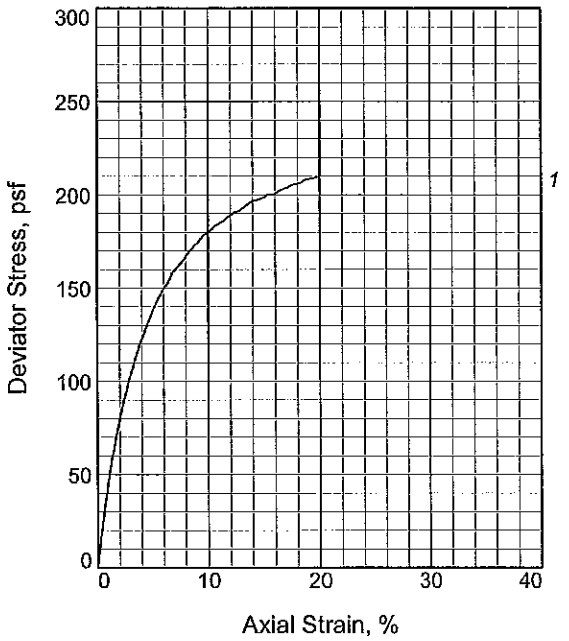
○ ASTM D422, C136

F.M.=0.01

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	104.0
	Dry Density, pcf	47.2
	Saturation, %	107.8
	Void Ratio	2.7003
	Diameter, in.	2.750
	Height, in.	4.560
At Test	Water Content, %	104.0
	Dry Density, pcf	47.2
	Saturation, %	107.8
	Void Ratio	2.7003
	Diameter, in.	2.750
	Height, in.	4.560
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		6.600
Fail. Stress, psf		199.1
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1149.5
σ_3 Failure, psf		950.4

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSo G Cl becoming G SaSi w/ Cl, CH bec. ML

Assumed Specific Gravity= 2.8

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-6 **Depth:** 18-20

Sample Number: 7

Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	30.2	69.8

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○			0.0113	0.0035	0.0015					

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSo G Cl becoming G SaSi w/ Cl, CH bec. ML	(CH)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

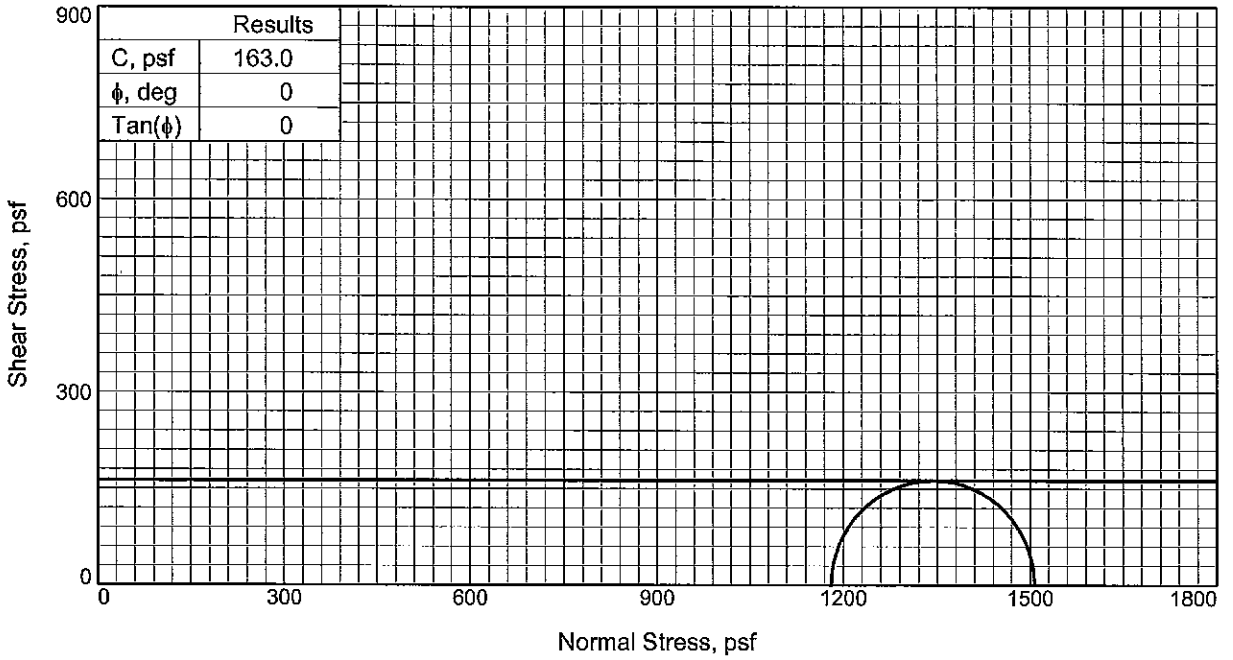
○ **Source:** B-6 **Sample No.:** 7 **Elev./Depth:** 18-20

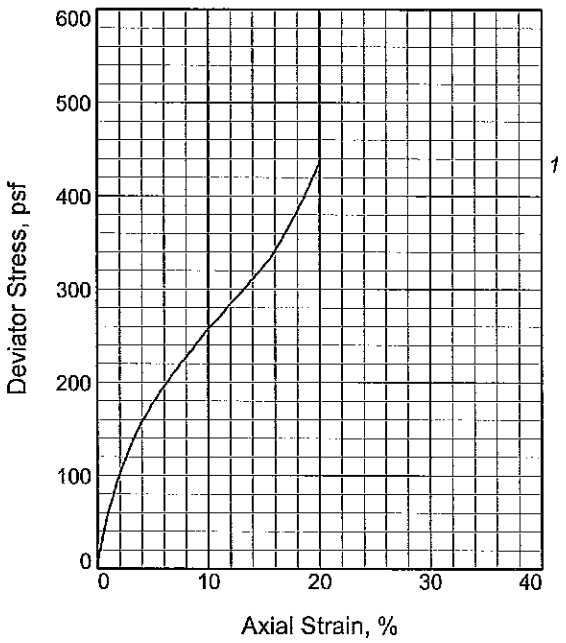
Remarks:

○ ASTM D422, C136

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	83.1
	Dry Density, pcf	63.2
	Saturation, %	133.2
	Void Ratio	1.7159
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	83.1
	Dry Density, pcf	63.2
	Saturation, %	133.2
	Void Ratio	1.7159
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		8.200
Fail. Stress, psf		325.9
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1506.7
σ_3 Failure, psf		1180.8

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSo G Cl w/ Orgs bec. G Si w/ Cl, CH

LL= 130 **PL=** 40 **PI=** 90

Assumed Specific Gravity= 2.75

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

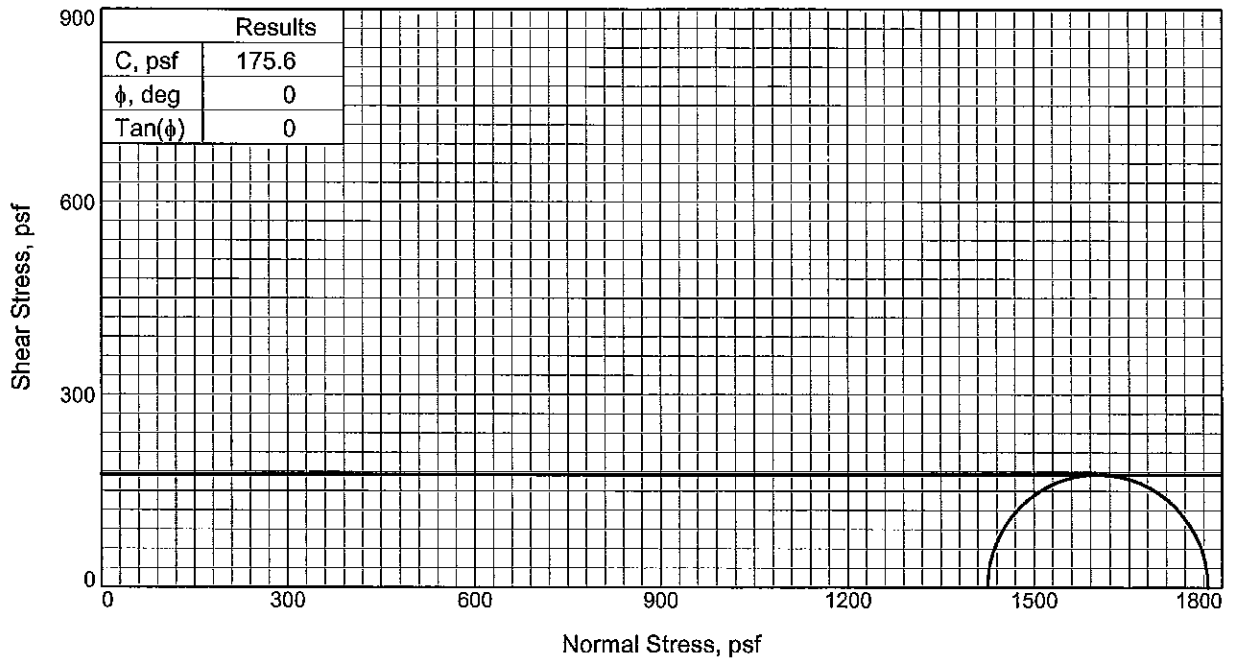
Source of Sample: B-6 **Depth:** 23-25

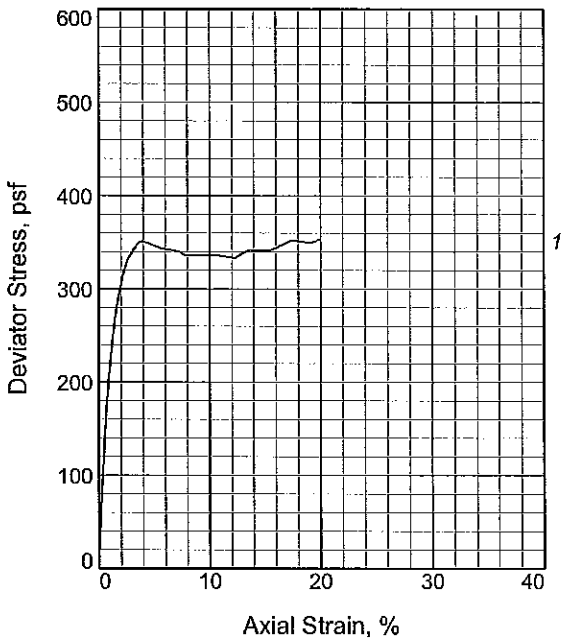
Sample Number: 8

Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	70.6
	Dry Density, pcf	60.9
	Saturation, %	106.2
	Void Ratio	1.8440
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	70.6
	Dry Density, pcf	60.9
	Saturation, %	106.2
	Void Ratio	1.8440
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		9.900
Fail. Stress, psf		351.3
Strain, %		3.9
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1776.9
σ_3 Failure, psf		1425.6

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSo G Cl w/ Si, CH

Specific Gravity= 2.774
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

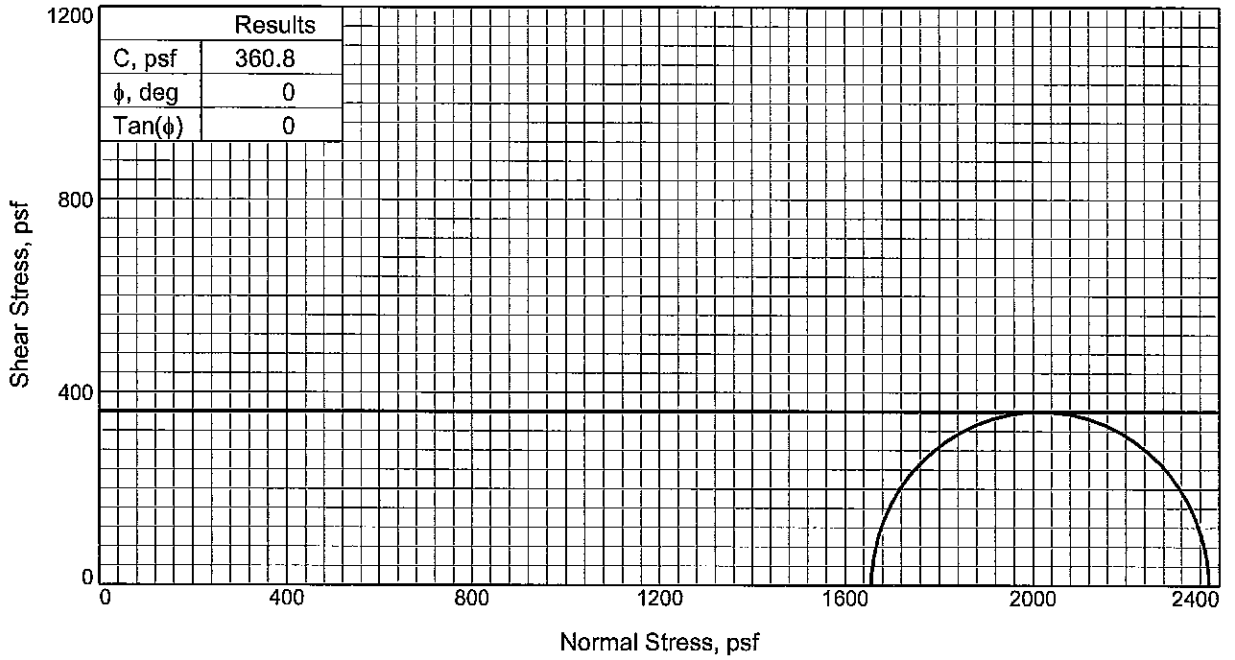
Client: URS

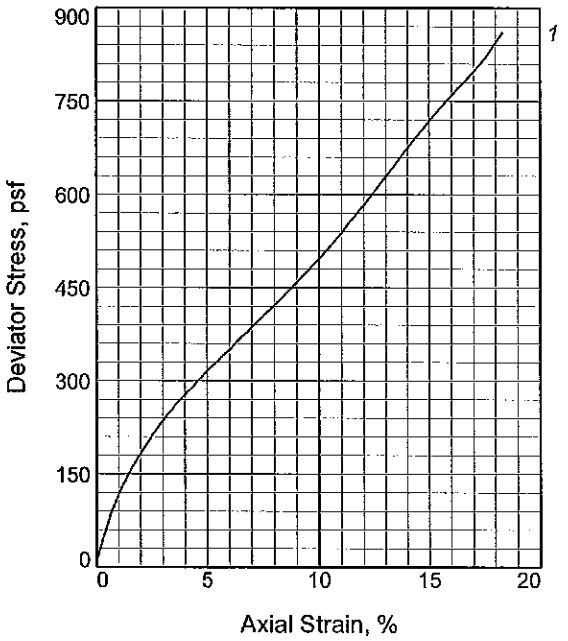
Project: BAYOU DUPONT

Source of Sample: B-6 **Depth:** 28-30
Sample Number: 9
Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	45.9
	Dry Density, pcf	83.6
	Saturation, %	119.9
	Void Ratio	1.0535
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	45.9
	Dry Density, pcf	83.6
	Saturation, %	119.9
	Void Ratio	1.0535
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		11.500
Fail. Stress, psf		721.6
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2377.6
σ_3 Failure, psf		1656.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: So G Cl bec. G Si w/ Cl, CH to ML

LL= 83 **PL=** 31 **PI=** 52

Assumed Specific Gravity= 2.75

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-6 **Depth:** 33-35

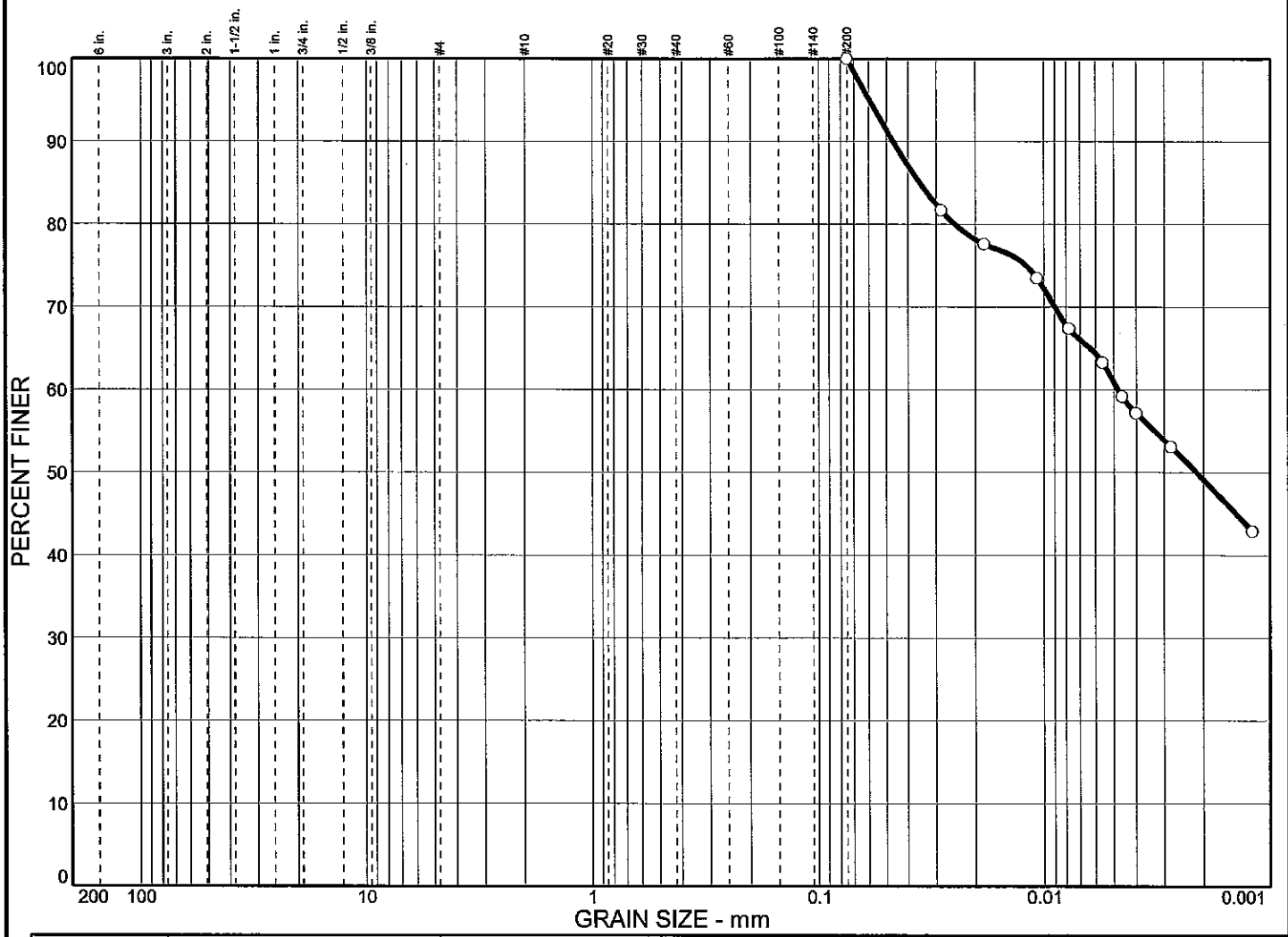
Sample Number: 10

Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	39.1	60.9

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	83	31	0.0354	0.0048	0.0021					

MATERIAL DESCRIPTION	USCS	AASHTO
○ So G Cl bec. G Si w/ Cl, CH to ML	(CH)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

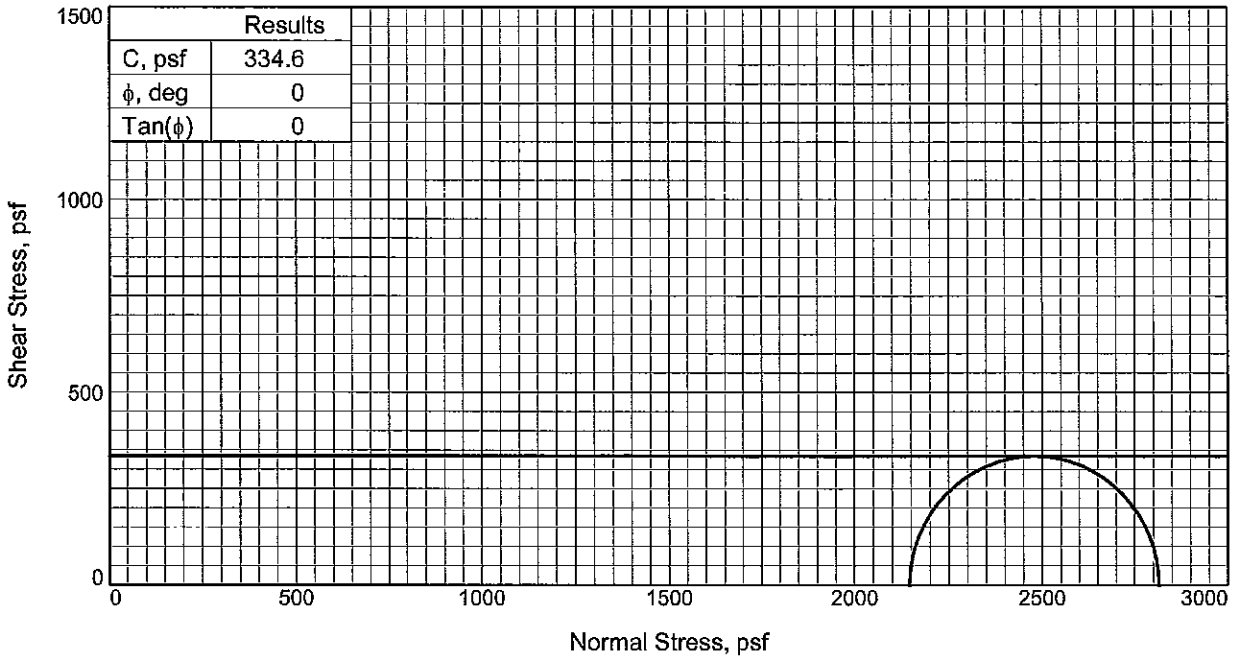
○ **Source:** B-6 **Sample No.:** 10 **Elev./Depth:** 33-35

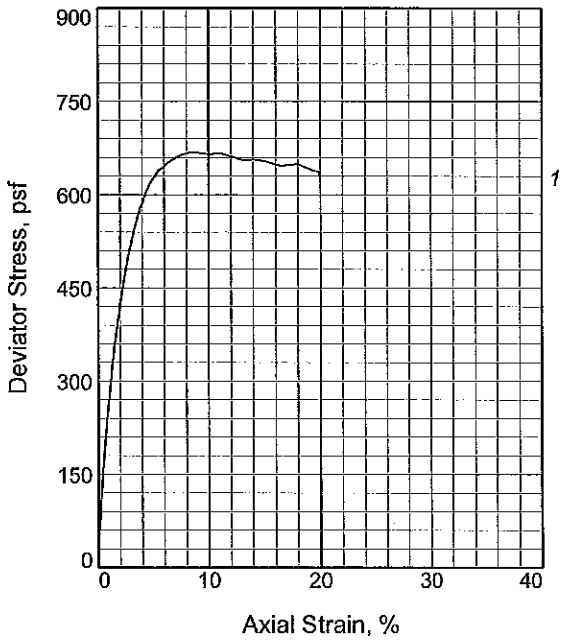
Remarks:

○ ASTM D422, C136

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	49.5
	Dry Density, pcf	76.4
	Saturation, %	109.2
	Void Ratio	1.2474
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	49.5
	Dry Density, pcf	76.4
	Saturation, %	109.2
	Void Ratio	1.2474
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		14.900
Fail. Stress, psf		669.3
Strain, %		8.6
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2814.9
σ_3 Failure, psf		2145.6

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: Lo G Si w/ Cl, Tr Orgs, Tr Si & Si Lens, MH

LL= 55 **PL=** 33 **PI=** 22

Assumed Specific Gravity= 2.75

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-6 **Depth:** 43-45

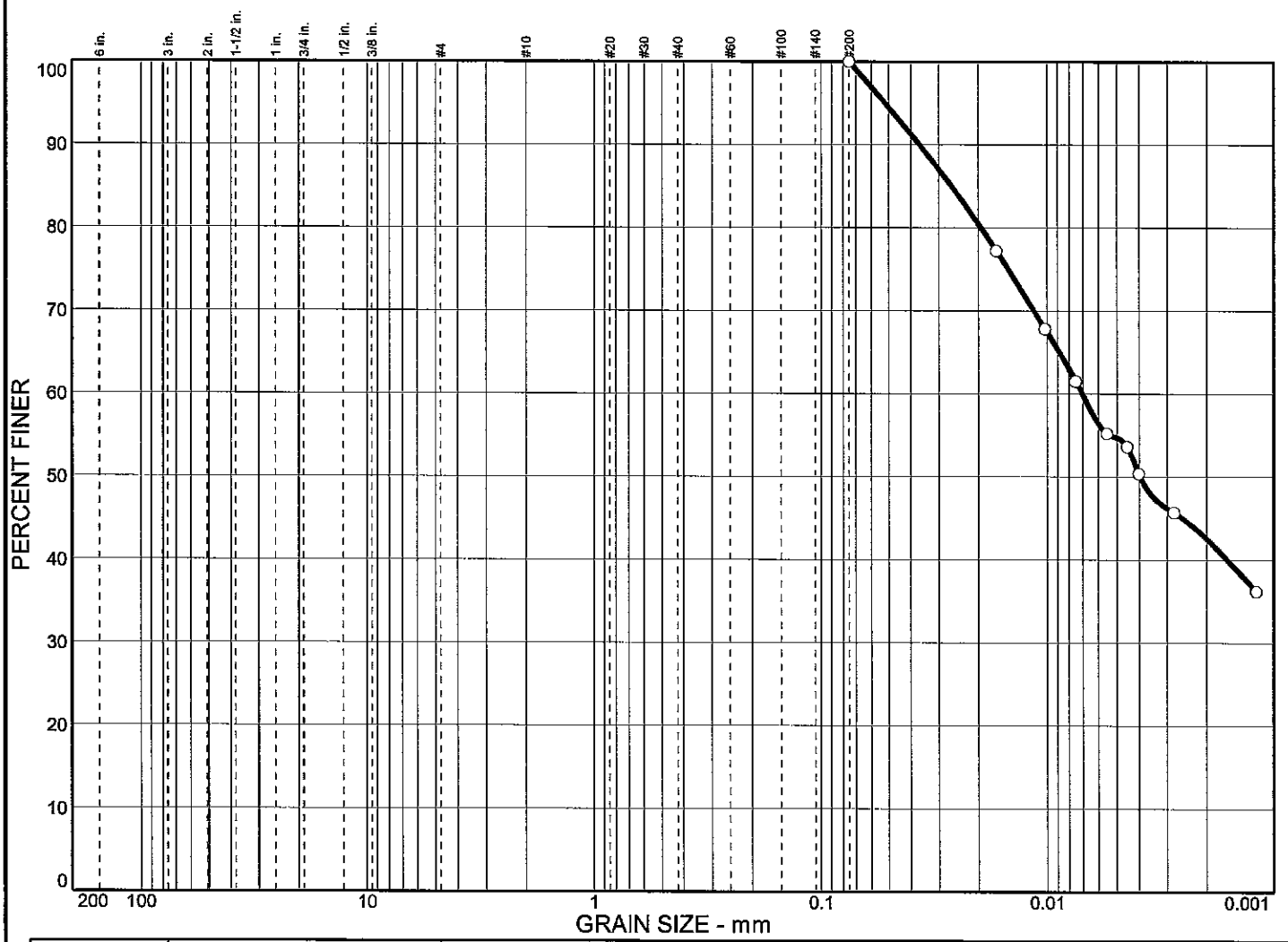
Sample Number: 12

Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	45.3	54.7

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	55	33	0.0264	0.0071	0.0039					

MATERIAL DESCRIPTION	USCS	AASHTO
○ Lo G Si w/ Cl, Tr Orgs, Tr Si & Si Lens, MH	(CH)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

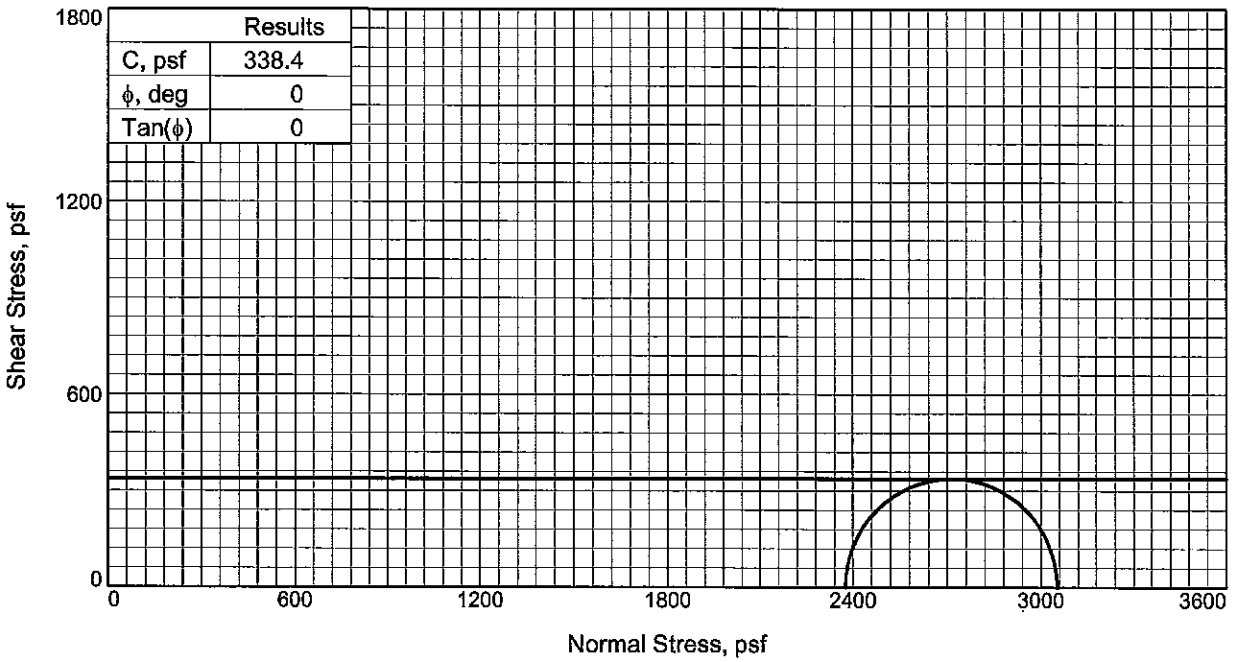
○ **Source:** B-6 **Sample No.:** 12 **Elev./Depth:** 43-45

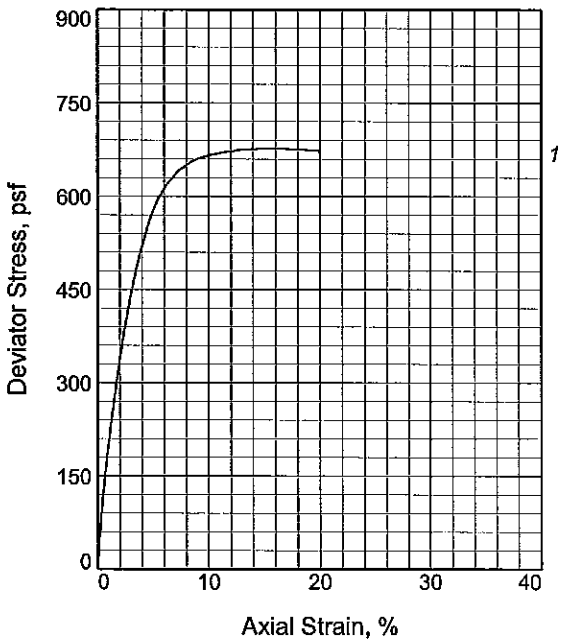
Remarks:

○ ASTM D422, C136

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	50.4
	Dry Density, pcf	80.5
	Saturation, %	122.3
	Void Ratio	1.1331
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	50.4
	Dry Density, pcf	80.5
	Saturation, %	122.3
	Void Ratio	1.1331
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		16.500
Fail. Stress, psf		676.7
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3052.7
σ_3 Failure, psf		2376.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: Med G Cl w/ Si Pkts, CH

Assumed Specific Gravity= 2.75

Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

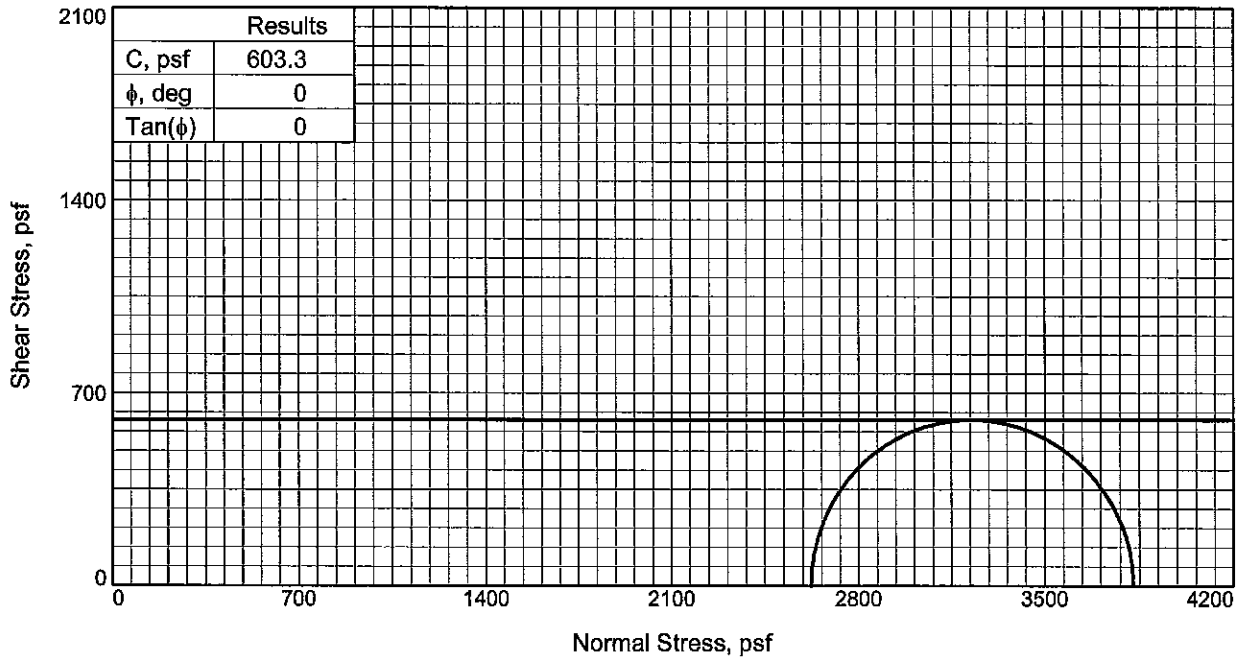
Source of Sample: B-6 **Depth:** 48-50

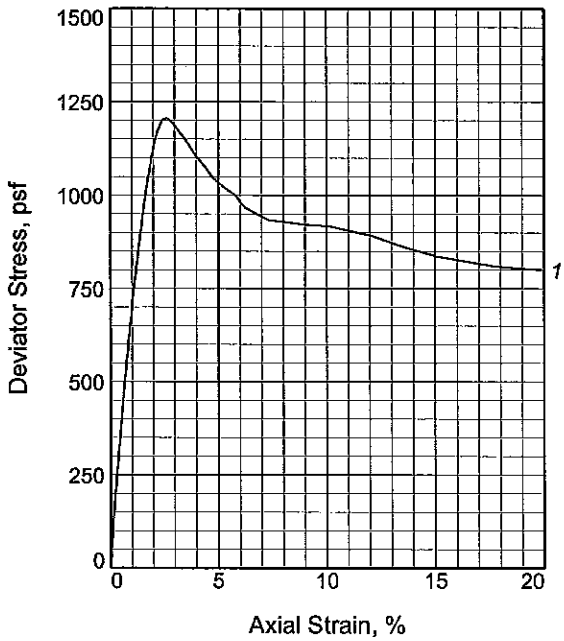
Sample Number: 13

Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	63.0
	Dry Density, pcf	66.0
	Saturation, %	108.2
	Void Ratio	1.6012
	Diameter, in.	2.750
	Height, in.	4.000
At Test	Water Content, %	63.0
	Dry Density, pcf	66.0
	Saturation, %	108.2
	Void Ratio	1.6012
	Diameter, in.	2.750
	Height, in.	4.000
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		18.200
Fail. Stress, psf		1206.6
Strain, %		2.6
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3827.4
σ_3 Failure, psf		2620.8

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: Med G Cl w/ Si Pkts, CH

LL= 82 **PL=** 31 **PI=** 51

Assumed Specific Gravity= 2.75

Remarks: 40 DEGREE SHEAR & BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-6 **Depth:** 53-55

Sample Number: 14

Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	41.9	58.1

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	82	31	0.0281	0.0059						

MATERIAL DESCRIPTION	USCS	AASHTO
○ Med G Cl w/ Si Pkts, CH	(CH)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

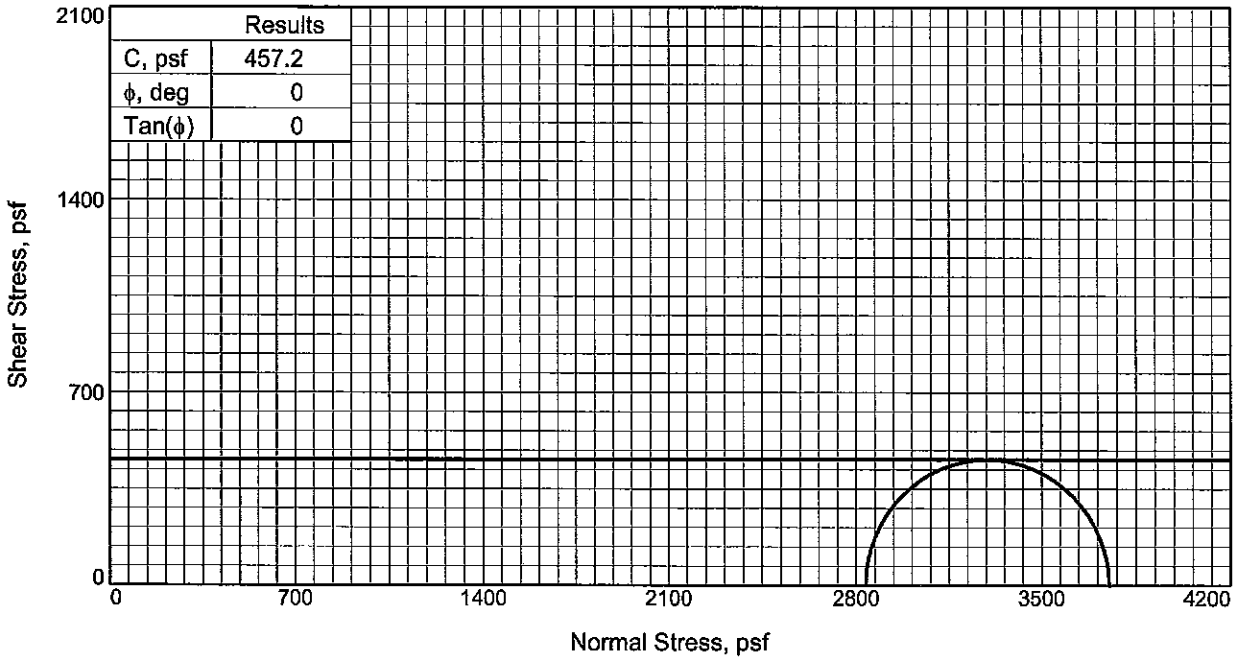
○ **Source:** B-6 **Sample No.:** 14 **Elev./Depth:** 53-55

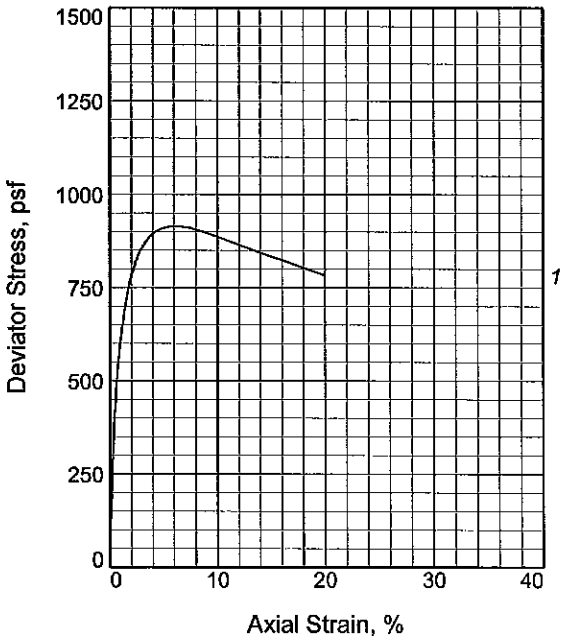
Remarks:

○ ASTM D422, C136

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	70.8
	Dry Density, pcf	63.8
	Saturation, %	115.3
	Void Ratio	1.6892
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	70.8
	Dry Density, pcf	63.8
	Saturation, %	115.3
	Void Ratio	1.6892
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		19.700
Fail. Stress, psf		914.4
Strain, %		5.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3751.2
σ_3 Failure, psf		2836.8

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: So G Cl w/ Tr Si, CH

Assumed Specific Gravity= 2.75
Remarks: TYPE FAILURE: BULGE

ASTM D 2850

Client: URS

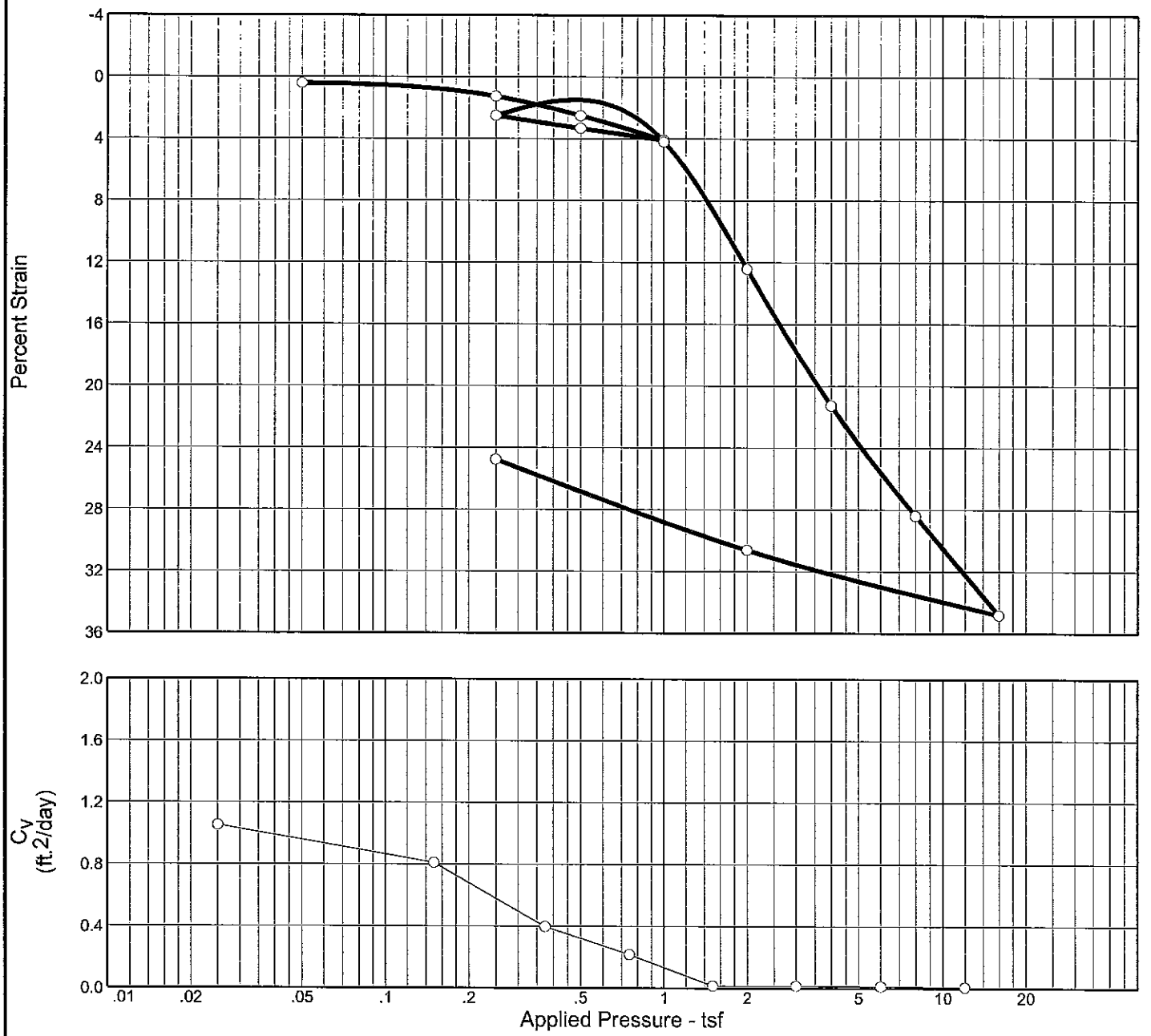
Project: BAYOU DUPONT

Source of Sample: B-6 **Depth:** 58-60
Sample Number: 15
Proj. No.: B09-012 **Date Sampled:** 3/16/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
94.4 %	50.2 %	69.7	82	51	2.75	(CH)		1.462

MATERIAL DESCRIPTION

Med G Cl w/ Si Pkts, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

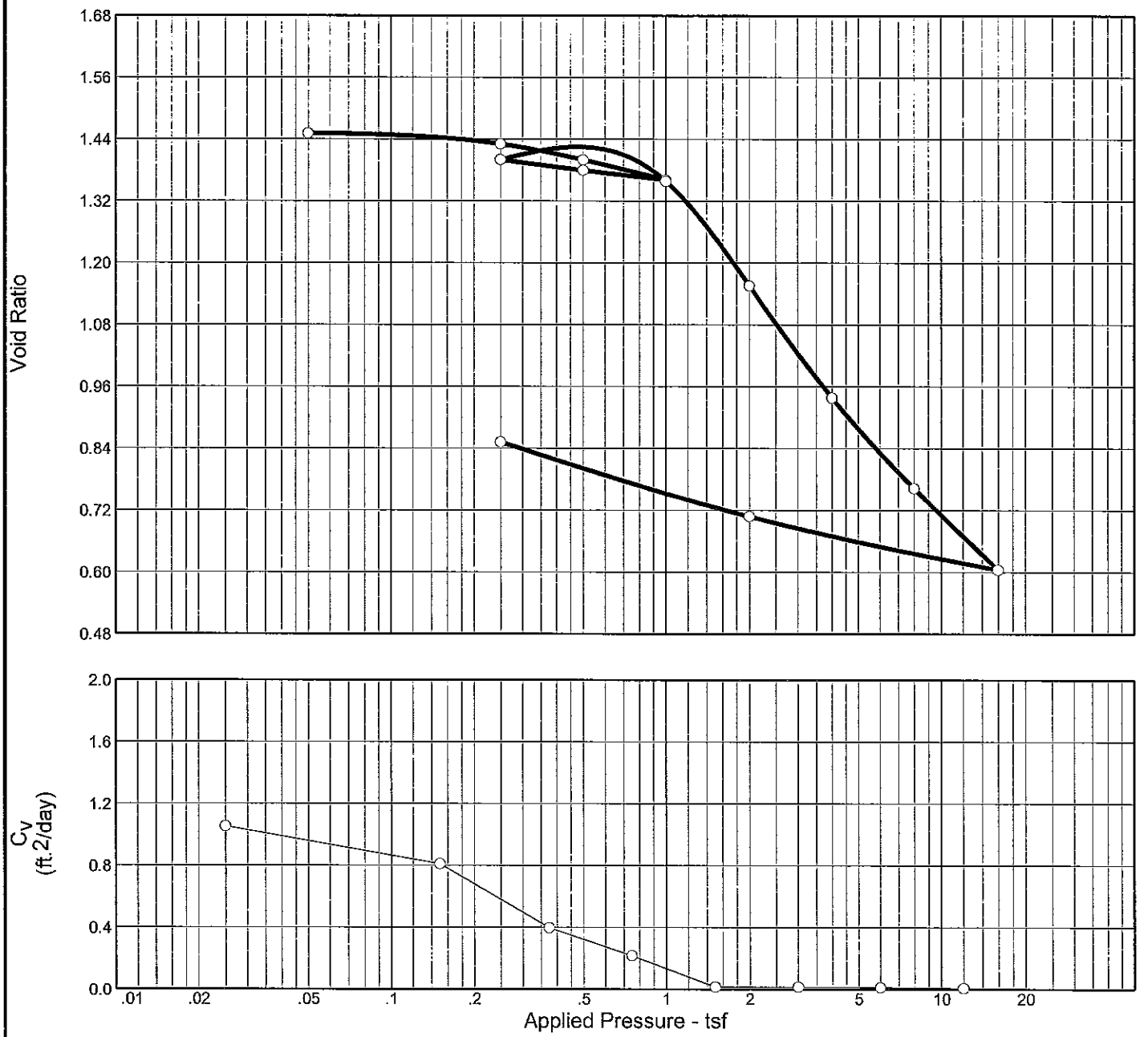
Source: B-6 **Sample No.:** 14 **Elev./Depth:** 53-55

CONSOLIDATION/SWELL TEST REPORT

Remarks:
ASTM D2435

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
94.4 %	50.2 %	69.7	82	51	2.75	(CH)		1.462

MATERIAL DESCRIPTION

Med G Cl w/ Si Pkts, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-6 **Sample No.:** 14 **Elev./Depth:** 53-55

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

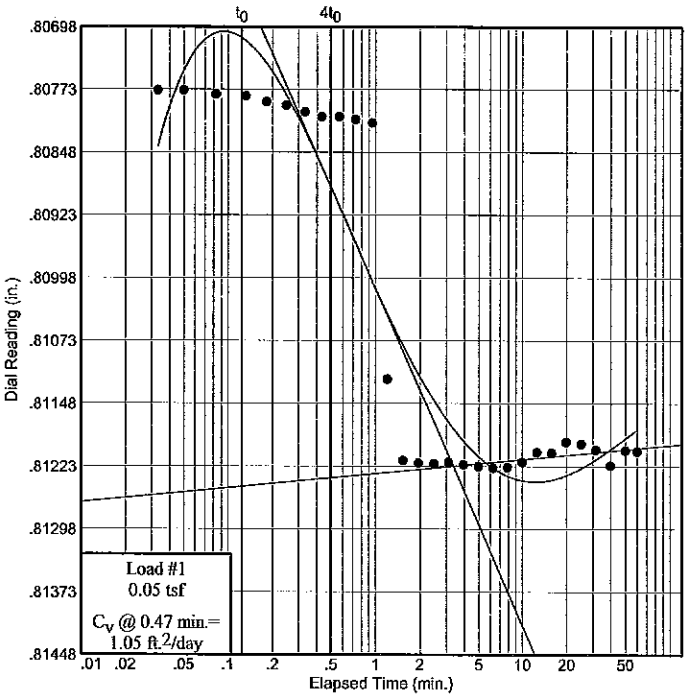
Remarks:

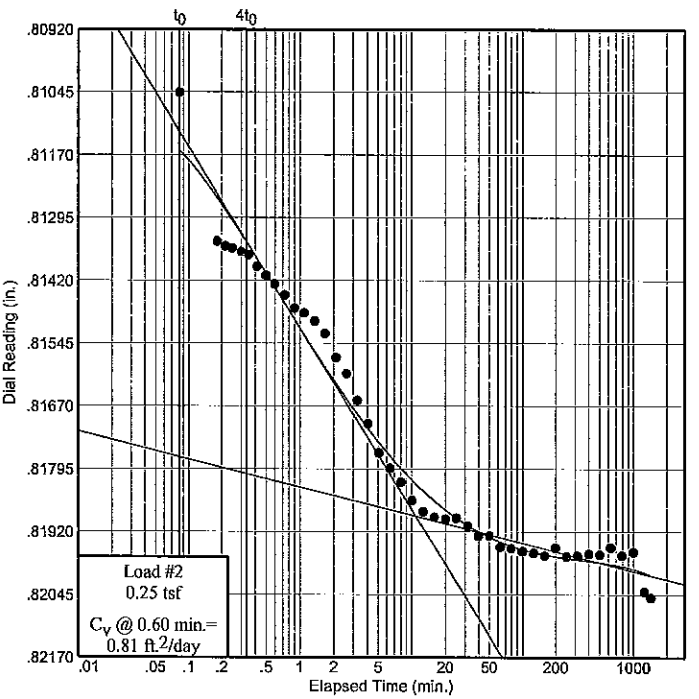
ASTM D2435

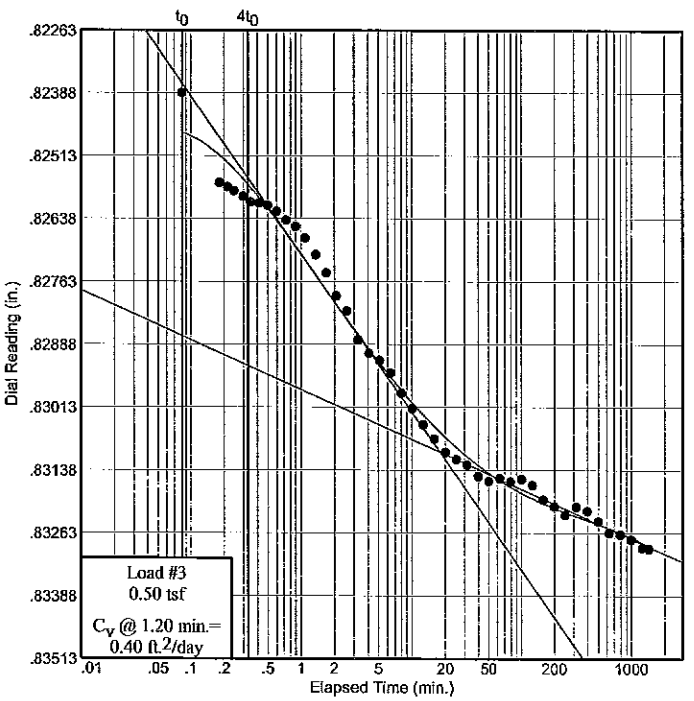
Dial Reading vs. Time

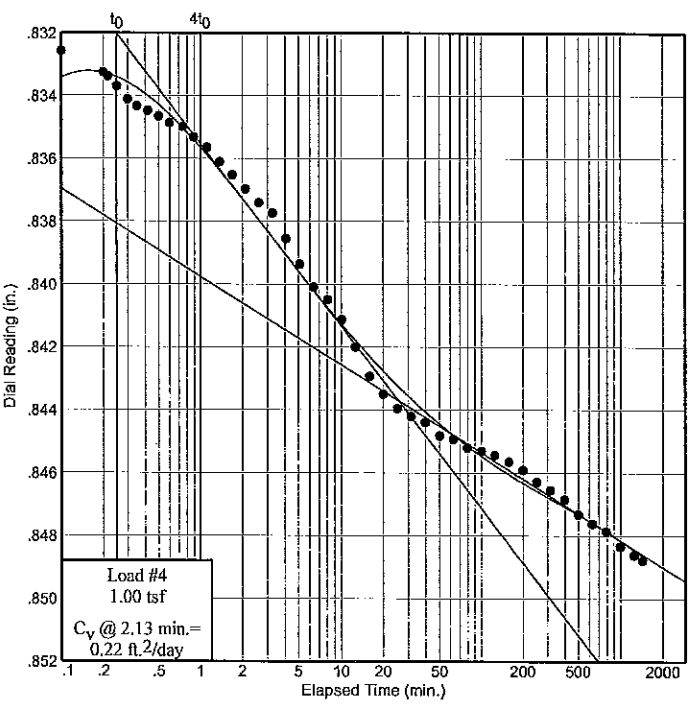
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-6 Sample No.: 14 Elev./Depth: 53-55









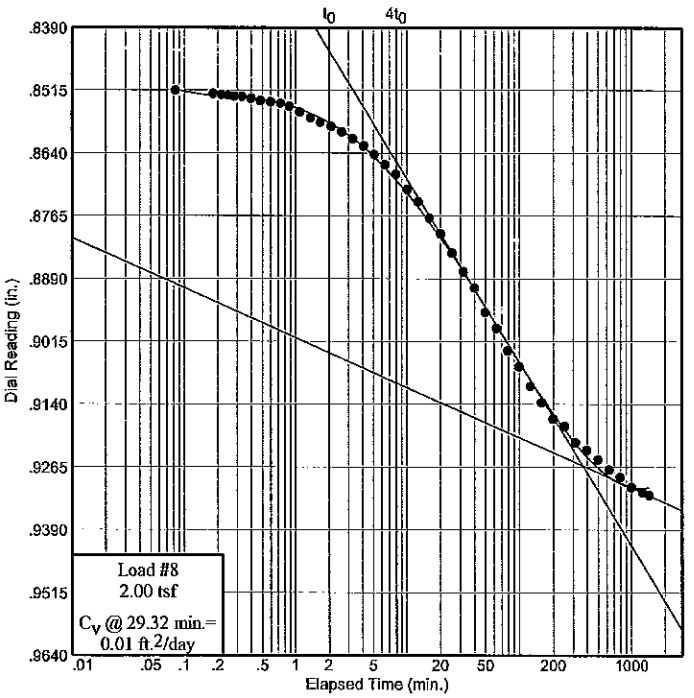
Dial Reading vs. Time

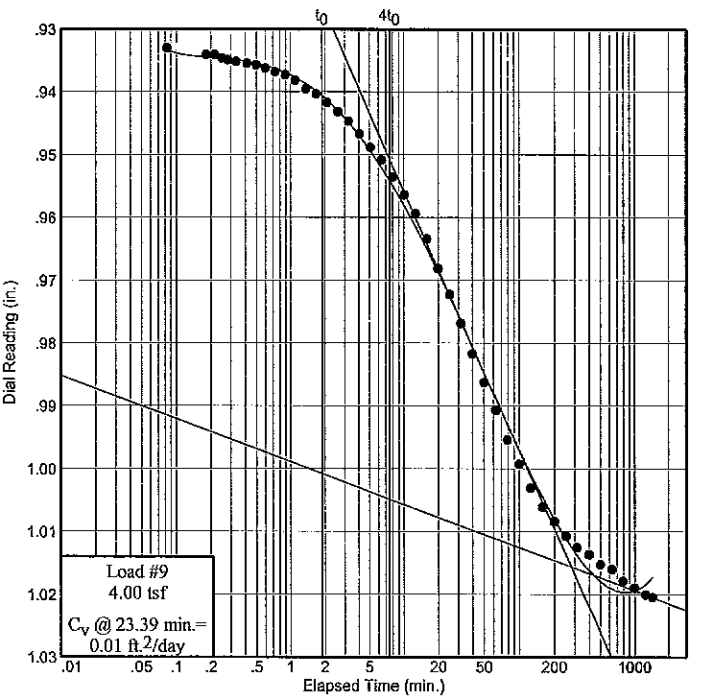
Southern Earth Sciences, Inc.

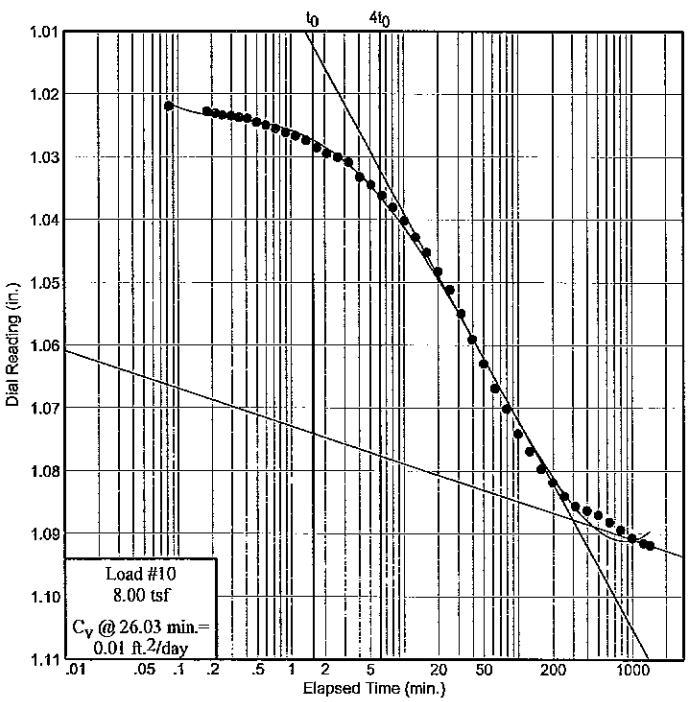
Dial Reading vs. Time

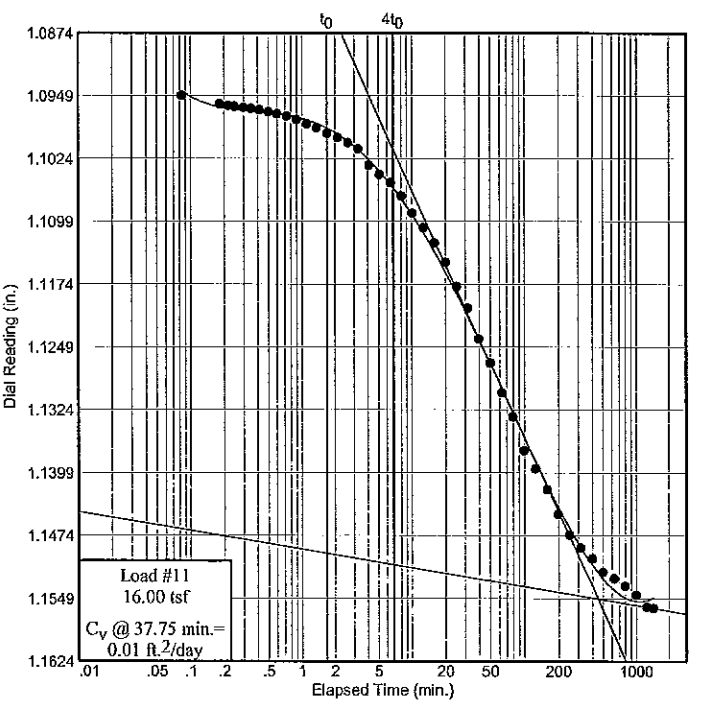
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-6 Sample No.: 14 Elev./Depth: 53-55









Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-6
Sample No.: 14
Elev. or Depth: 53-55 **Sample Length(in./cm.):**
Location:
Description: Med G Cl w/ Si Pkts, CH
Liquid Limit: 82 **Plasticity Index:** 51
USCS: (CH) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST		AFTER TEST	
Wet w+t =	116.48 g.	Consolidometer # =	1	Wet w+t =	117.68 g.
Dry w+t =	90.29 g.			Dry w+t =	84.19 g.
Tare Wt. =	38.09 g.	Spec. Gravity =	2.75	Tare Wt. =	.00 g.
Height =	1.00 in.	Height =	1.00 in.		
Diameter =	2.50 in.	Diameter =	2.50 in.		
Weight =	134.95 g.	Defl. Table =	Sigma 1 2.5in		
Moisture =	50.2 %	Ht. Solids =	0.4062 in.	Moisture =	39.8 %
Wet Den. =	104.7 pcf	Dry Wt. =	89.86 g.*	Dry Wt. =	84.19 g.
Dry Den. =	69.7 pcf	Void Ratio =	1.462	Void Ratio =	0.852
		Saturation =	94.4 %		

* Initial dry weight used in calculations

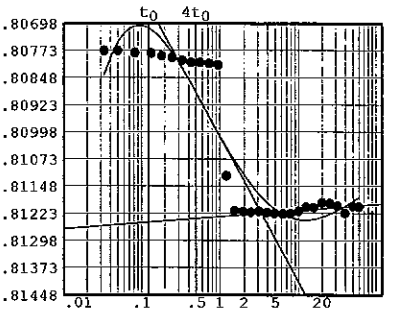
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.80783				1.462	
0.05	0.81215	0.00010	1.05		1.451	0.4 Comprs.
0.25	0.82371	0.00320	0.81	0.001	1.430	1.3 Comprs.
0.50	0.83724	0.00430	0.40	0.001	1.400	2.5 Comprs.
1.00	0.85477	0.00600	0.22	0.003	1.361	4.1 Comprs.
0.50	0.84720	0.00600	0.79		1.379	3.3 Comprs.
0.25	0.83808	0.00520	0.24		1.400	2.5 Comprs.
1.00	0.85657	0.00670	0.22	0.002	1.358	4.2 Comprs.
2.00	0.94007	0.00800	0.01	0.010	1.156	12.4 Comprs.
4.00	1.03046	0.01000	0.01	0.008	0.938	21.3 Comprs.
8.00	1.10430	0.01250	0.01	0.008	0.763	28.4 Comprs.
16.00	1.17115	0.01510	0.01	0.003	0.604	34.8 Comprs.
2.00	1.12201	0.00800	0.00		0.708	30.6 Comprs.
0.25	1.06250	0.00700	1.92		0.852	24.8 Comprs.

C_c = 0.52 P_c = 0.41 tsf C_r = 0.07

Pressure: 0.05 tsf **TEST READINGS** **Load No. 1**

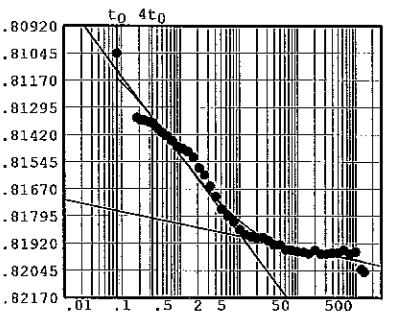
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.80783	16	2.47	0.81230
2	0.03	0.80784	17	3.12	0.81228
3	0.05	0.80784	18	3.93	0.81231
4	0.08	0.80789	19	4.97	0.81233
5	0.13	0.80791	20	6.27	0.81235
6	0.18	0.80798	21	7.90	0.81234
7	0.25	0.80802	22	9.97	0.81228
8	0.33	0.80810	23	12.55	0.81216
9	0.43	0.80816	24	15.82	0.81217
10	0.57	0.80816	25	19.92	0.81204
11	0.73	0.80819	26	25.08	0.81206
12	0.95	0.80823	27	31.58	0.81213
13	1.20	0.81129	28	39.78	0.81232
14	1.53	0.81226	29	50.08	0.81214
15	1.95	0.81229	30	60.12	0.81215



Void Ratio = 1.451 **Compression** = 0.4 %
D_0 = 0.80533 D_{50} = 0.80878 D_{100} = 0.81223
C_v at 0.5 min. = 1.05 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 2**

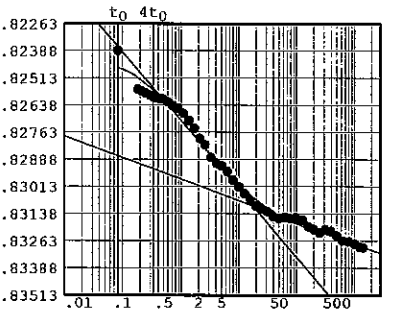
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.81217	24	12.72	0.82200
2	0.08	0.81366	25	15.97	0.82211
3	0.18	0.81662	26	20.08	0.82215
4	0.22	0.81672	27	25.25	0.82213
5	0.25	0.81676	28	31.75	0.82228
6	0.30	0.81683	29	39.93	0.82248
7	0.35	0.81689	30	50.25	0.82248
8	0.42	0.81712	31	63.23	0.82270
9	0.50	0.81730	32	79.57	0.82273
10	0.60	0.81747	33	100.13	0.82279
11	0.73	0.81769	34	126.03	0.82282
12	0.90	0.81795	35	158.63	0.82288
13	1.10	0.81805	36	199.67	0.82272
14	1.37	0.81821	37	251.33	0.82289
15	1.68	0.81846	38	316.37	0.82288
16	2.10	0.81894	39	398.25	0.82284
17	2.62	0.81926	40	501.33	0.82285
18	3.27	0.81979	41	631.10	0.82271
19	4.08	0.82025	42	794.47	0.82287
20	5.12	0.82083	43	1000.15	0.82280
21	6.43	0.82114	44	1259.07	0.82359
22	8.07	0.82141	45	1440.15	0.82371
23	10.12	0.82178			



Void Ratio = 1.430 **Compression** = 1.3 %
D_0 = 0.80979 D_{50} = 0.81434 D_{100} = 0.81889
C_v at 0.6 min. = 0.81 ft.^{2}/day C_α = 0.001

Pressure: 0.50 tsf | **TEST READINGS** | **Load No. 3**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.82372	24	12.72	0.83477
2	0.08	0.82818	25	15.97	0.83506
3	0.18	0.82996	26	20.08	0.83533
4	0.22	0.83005	27	25.25	0.83547
5	0.25	0.83013	28	31.75	0.83558
6	0.30	0.83024	29	39.95	0.83580
7	0.35	0.83035	30	50.25	0.83590
8	0.42	0.83037	31	63.23	0.83584
9	0.50	0.83042	32	79.58	0.83591
10	0.60	0.83054	33	100.15	0.83586
11	0.73	0.83071	34	126.03	0.83598
12	0.90	0.83084	35	158.63	0.83627
13	1.10	0.83107	36	199.68	0.83640
14	1.37	0.83140	37	251.35	0.83657
15	1.70	0.83176	38	316.38	0.83641
16	2.10	0.83222	39	398.27	0.83649
17	2.62	0.83252	40	501.35	0.83670
18	3.28	0.83309	41	631.12	0.83693
19	4.10	0.83336	42	794.48	0.83696
20	5.13	0.83350	43	1000.17	0.83706
21	6.43	0.83375	44	1259.10	0.83722
22	8.07	0.83415	45	1440.22	0.83724
23	10.12	0.83445			



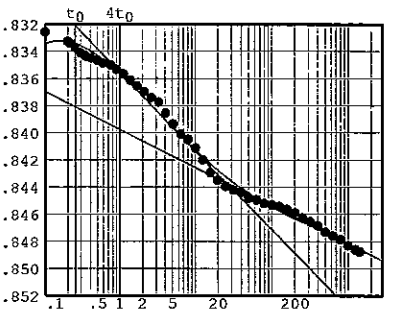
Void Ratio = 1.400 **Compression** = 2.5 %

D_0 = 0.82364 D_{50} = 0.82732 D_{100} = 0.83101

C_v **at 1.2 min.** = 0.40 ft.^{2}/day C_α = 0.001

Pressure: 1.00 tsf **TEST READINGS** **Load No. 4**

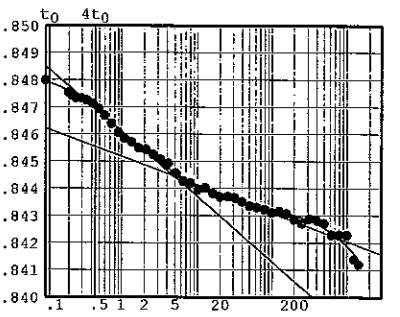
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.83726	24	12.72	0.84800
2	0.10	0.83858	25	15.98	0.84893
3	0.20	0.83926	26	20.10	0.84949
4	0.22	0.83938	27	25.27	0.84995
5	0.25	0.83970	28	31.77	0.85021
6	0.30	0.84012	29	39.97	0.85039
7	0.35	0.84034	30	50.27	0.85082
8	0.42	0.84048	31	63.25	0.85094
9	0.50	0.84066	32	79.60	0.85120
10	0.60	0.84087	33	100.17	0.85131
11	0.75	0.84099	34	126.05	0.85144
12	0.90	0.84133	35	158.65	0.85164
13	1.12	0.84166	36	199.70	0.85191
14	1.38	0.84212	37	251.37	0.85229
15	1.70	0.84254	38	316.40	0.85255
16	2.12	0.84298	39	398.28	0.85285
17	2.63	0.84341	40	501.37	0.85332
18	3.28	0.84374	41	631.13	0.85362
19	4.10	0.84455	42	794.50	0.85386
20	5.13	0.84537	43	1000.18	0.85433
21	6.43	0.84610	44	1259.12	0.85461
22	8.08	0.84650	45	1440.30	0.85477
23	10.13	0.84713			



Void Ratio = 1.361 **Compression =** 4.1 %
D_0 = 0.83117 D_{50} = 0.83743 D_{100} = 0.84370
C_v **at 2.1 min.** = 0.22 ft.^{2}/day C_α = 0.003

Pressure: 0.50 tsf **TEST READINGS** **Load No. 5**

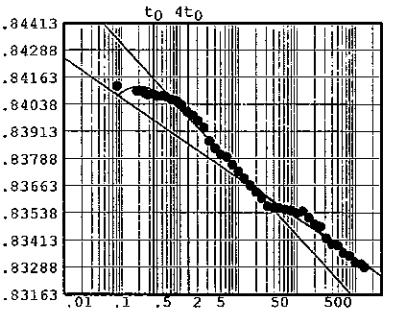
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.85476	24	12.70	0.85001
2	0.10	0.85399	25	15.97	0.84982
3	0.20	0.85354	26	20.07	0.84968
4	0.22	0.85344	27	25.23	0.84970
5	0.25	0.85334	28	31.75	0.84965
6	0.30	0.85331	29	39.93	0.84951
7	0.35	0.85324	30	50.25	0.84935
8	0.42	0.85313	31	63.23	0.84930
9	0.50	0.85293	32	79.57	0.84922
10	0.60	0.85269	33	100.13	0.84911
11	0.73	0.85238	34	126.03	0.84915
12	0.90	0.85206	35	158.63	0.84907
13	1.10	0.85183	36	199.67	0.84886
14	1.37	0.85170	37	251.33	0.84872
15	1.68	0.85148	38	316.37	0.84888
16	2.10	0.85143	39	398.25	0.84882
17	2.62	0.85124	40	501.33	0.84871
18	3.28	0.85107	41	631.10	0.84829
19	4.10	0.85091	42	794.47	0.84829
20	5.13	0.85056	43	1000.15	0.84828
21	6.43	0.85026	44	1259.07	0.84738
22	8.07	0.85019	45	1440.23	0.84720
23	10.12	0.84995			



Void Ratio = 1.379 **Compression =** 3.3 %
D_0 = 0.84886 D_{50} = 0.84667 D_{100} = 0.84447
C_v **at 0.6 min.** = 0.79 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 6**

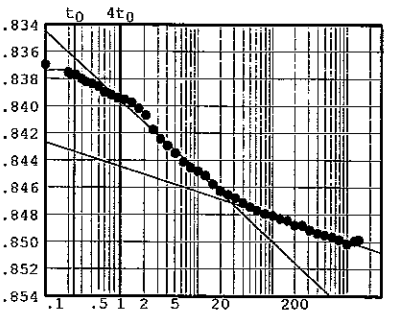
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.84725	24	12.70	0.84215
2	0.08	0.84641	25	15.97	0.84184
3	0.18	0.84619	26	20.07	0.84154
4	0.22	0.84618	27	25.23	0.84125
5	0.25	0.84610	28	31.75	0.84088
6	0.28	0.84602	29	39.93	0.84082
7	0.33	0.84604	30	50.25	0.84078
8	0.42	0.84594	31	63.22	0.84072
9	0.50	0.84595	32	79.57	0.84068
10	0.60	0.84591	33	100.13	0.84055
11	0.73	0.84580	34	126.02	0.84064
12	0.90	0.84574	35	158.62	0.84034
13	1.10	0.84555	36	199.67	0.84005
14	1.37	0.84523	37	251.32	0.83993
15	1.68	0.84506	38	316.37	0.83940
16	2.10	0.84480	39	398.25	0.83913
17	2.62	0.84450	40	501.33	0.83906
18	3.27	0.84388	41	631.10	0.83871
19	4.08	0.84355	42	794.47	0.83860
20	5.12	0.84325	43	1000.15	0.83828
21	6.42	0.84315	44	1259.07	0.83822
22	8.05	0.84278	45	1440.17	0.83808
23	10.12	0.84247			



Void Ratio = 1.400 **Compression** = 2.5 %
D_0 = 0.84230 D_{50} = 0.83939 D_{100} = 0.83647
C_v **at 1.9 min.** = 0.24 ft.^{2}/day

Pressure: 1.00 tsf | **TEST READINGS** | **Load No. 7**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.84292	24	12.70	0.85185
2	0.10	0.84367	25	15.97	0.85249
3	0.20	0.84423	26	20.07	0.85297
4	0.22	0.84439	27	25.23	0.85326
5	0.25	0.84442	28	31.75	0.85349
6	0.30	0.84471	29	39.93	0.85386
7	0.35	0.84495	30	50.25	0.85416
8	0.42	0.84507	31	63.22	0.85441
9	0.50	0.84530	32	79.57	0.85465
10	0.60	0.84570	33	100.13	0.85480
11	0.73	0.84589	34	126.03	0.85502
12	0.90	0.84611	35	158.62	0.85514
13	1.10	0.84623	36	199.67	0.85550
14	1.37	0.84645	37	251.32	0.85551
15	1.68	0.84691	38	316.37	0.85587
16	2.10	0.84739	39	398.25	0.85610
17	2.62	0.84847	40	501.33	0.85621
18	3.27	0.84915	41	631.10	0.85635
19	4.08	0.84964	42	794.47	0.85657
20	5.12	0.85018	43	1000.13	0.85687
21	6.42	0.85083	44	1259.07	0.85666
22	8.05	0.85125	45	1440.12	0.85657
23	10.12	0.85152			



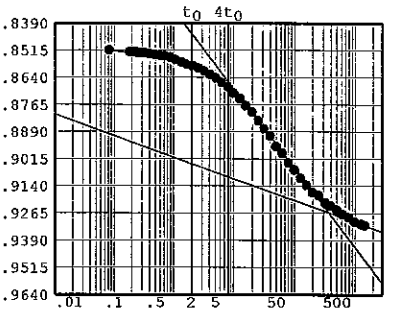
Void Ratio = 1.358 **Compression** = 4.2 %

D_0 = 0.83548 D_{50} = 0.84130 D_{100} = 0.84712

C_v **at 2.1 min.** = 0.22 ft.^{2}/day C_α = 0.002

Pressure: 2.00 tsf | **TEST READINGS** | **Load No. 8**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.85655	24	12.70	0.88167
2	0.08	0.85952	25	15.97	0.88497
3	0.18	0.86020	26	20.07	0.88804
4	0.22	0.86036	27	25.23	0.89193
5	0.25	0.86054	28	31.73	0.89560
6	0.28	0.86073	29	39.93	0.89885
7	0.33	0.86079	30	50.23	0.90371
8	0.40	0.86113	31	63.22	0.90685
9	0.48	0.86158	32	79.55	0.91130
10	0.60	0.86183	33	100.12	0.91450
11	0.73	0.86214	34	126.02	0.91842
12	0.88	0.86269	35	158.62	0.92163
13	1.10	0.86392	36	199.65	0.92492
14	1.37	0.86496	37	251.32	0.92641
15	1.68	0.86591	38	316.35	0.92959
16	2.10	0.86672	39	398.23	0.93109
17	2.62	0.86779	40	501.32	0.93304
18	3.27	0.86913	41	631.08	0.93504
19	4.08	0.87064	42	794.45	0.93651
20	5.12	0.87228	43	1000.13	0.93848
21	6.42	0.87432	44	1259.05	0.93949
22	8.05	0.87624	45	1440.18	0.94007
23	10.12	0.87922			



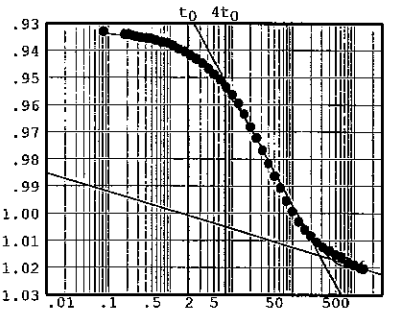
Void Ratio = 1.156 **Compression =** 12.4 %

D_0 = 0.84652 D_{50} = 0.88635 D_{100} = 0.92617

C_v **at 29.3 min.** = 0.01 ft.^{2}/day C_α = 0.010

Pressure: 4.00 tsf **TEST READINGS** **Load No. 9**

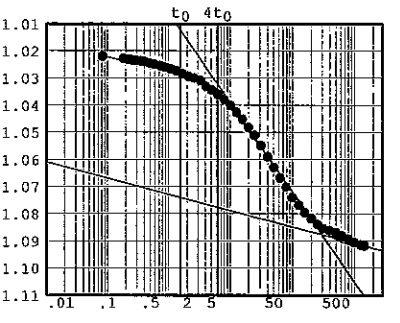
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.94007	24	12.72	0.96944
2	0.08	0.94303	25	15.97	0.97343
3	0.18	0.94407	26	20.07	0.97816
4	0.22	0.94404	27	25.23	0.98228
5	0.25	0.94463	28	31.75	0.98687
6	0.28	0.94494	29	39.93	0.99175
7	0.33	0.94520	30	50.23	0.99629
8	0.42	0.94548	31	63.22	1.00071
9	0.50	0.94576	32	79.55	1.00542
10	0.60	0.94627	33	100.12	1.00927
11	0.73	0.94684	34	126.02	1.01307
12	0.90	0.94729	35	158.62	1.01607
13	1.10	0.94816	36	199.65	1.01840
14	1.37	0.94955	37	251.32	1.02076
15	1.68	0.95032	38	316.37	1.02255
16	2.10	0.95171	39	398.25	1.02369
17	2.62	0.95315	40	501.33	1.02523
18	3.27	0.95467	41	631.10	1.02603
19	4.10	0.95667	42	794.47	1.02790
20	5.13	0.95886	43	1000.15	1.02900
21	6.42	0.96088	44	1259.07	1.03006
22	8.07	0.96357	45	1440.48	1.03046
23	10.12	0.96641			



Void Ratio = 0.938 **Compression** = 21.3 %
D_0 = 0.92701 D_{50} = 0.97130 D_{100} = 1.01559
C_v **at 23.4 min.** = 0.01 ft.^{2}/day C_α = 0.008

Pressure: 8.00 tsf | TEST READINGS | Load No. 10

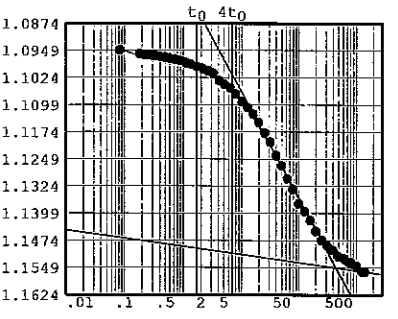
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	1.03044	24	12.72	1.05531
2	0.08	1.03450	25	15.97	1.05775
3	0.18	1.03530	26	20.08	1.06076
4	0.22	1.03560	27	25.25	1.06367
5	0.25	1.03589	28	31.75	1.06747
6	0.30	1.03604	29	39.93	1.07159
7	0.35	1.03620	30	50.25	1.07544
8	0.42	1.03644	31	63.23	1.07936
9	0.50	1.03702	32	79.57	1.08264
10	0.60	1.03750	33	100.13	1.08656
11	0.73	1.03801	34	126.03	1.08936
12	0.90	1.03863	35	158.63	1.09220
13	1.10	1.03917	36	199.67	1.09434
14	1.37	1.03990	37	251.33	1.09652
15	1.70	1.04108	38	316.37	1.09808
16	2.10	1.04196	39	398.25	1.09880
17	2.62	1.04257	40	501.33	1.09950
18	3.27	1.04337	41	631.10	1.10065
19	4.10	1.04575	42	794.48	1.10186
20	5.13	1.04699	43	1000.15	1.10319
21	6.43	1.04866	44	1259.08	1.10395
22	8.07	1.05053	45	1440.18	1.10430
23	10.12	1.05271			



Void Ratio = 0.763 **Compression** = 28.4 %
D_0 = 1.01816 D_{50} = 1.05292 D_{100} = 1.08768
C_v **at 26.0 min.** = 0.01 ft.^{2}/day C_α = 0.008

Pressure: 16.00 tsf | **TEST READINGS** | **Load No. 11**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	1.10426	24	12.72	1.12577
2	0.08	1.11001	25	15.97	1.12760
3	0.18	1.11098	26	20.08	1.12991
4	0.22	1.11120	27	25.25	1.13279
5	0.25	1.11129	28	31.75	1.13536
6	0.30	1.11143	29	39.95	1.13903
7	0.35	1.11154	30	50.25	1.14190
8	0.42	1.11172	31	63.23	1.14545
9	0.50	1.11195	32	79.57	1.14834
10	0.60	1.11218	33	100.13	1.15236
11	0.73	1.11244	34	126.03	1.15449
12	0.90	1.11286	35	158.63	1.15698
13	1.12	1.11341	36	199.67	1.15996
14	1.37	1.11383	37	251.33	1.16242
15	1.70	1.11451	38	316.38	1.16394
16	2.12	1.11502	39	398.27	1.16524
17	2.63	1.11562	40	501.35	1.16686
18	3.28	1.11637	41	631.12	1.16762
19	4.10	1.11833	42	794.48	1.16850
20	5.13	1.11939	43	1000.17	1.16958
21	6.43	1.12038	44	1259.10	1.17102
22	8.07	1.12201	45	1440.05	1.17115
23	10.12	1.12403			



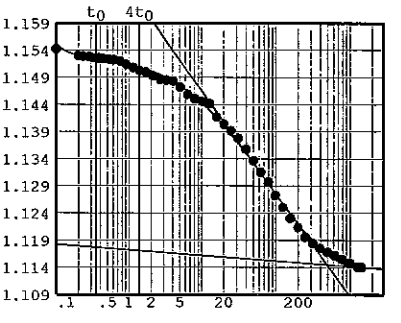
Void Ratio = 0.604 **Compression =** 34.8 %

D_0 = 1.09167 D_{50} = 1.12330 D_{100} = 1.15493

C_v **at 37.8 min. =** 0.01 ft.^{2}/day C_α = 0.003

Pressure: 2.00 tsf **TEST READINGS** **Load No. 12**

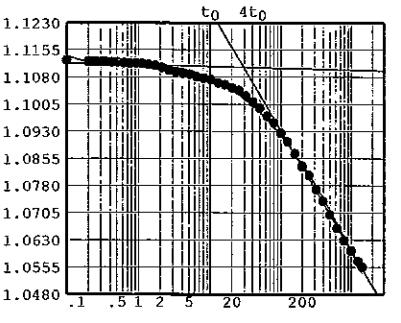
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	1.17112	24	12.78	1.15214
2	0.10	1.16217	25	16.05	1.14967
3	0.20	1.16102	26	20.17	1.14839
4	0.23	1.16087	27	25.33	1.14713
5	0.28	1.16075	28	31.83	1.14574
6	0.32	1.16062	29	40.03	1.14374
7	0.38	1.16054	30	50.33	1.14165
8	0.45	1.16042	31	63.32	1.13951
9	0.53	1.16030	32	79.67	1.13772
10	0.63	1.16017	33	100.23	1.13526
11	0.77	1.15993	34	126.13	1.13303
12	0.93	1.15929	35	158.73	1.13105
13	1.15	1.15876	36	199.78	1.12932
14	1.42	1.15821	37	251.45	1.12757
15	1.73	1.15793	38	316.50	1.12636
16	2.15	1.15721	39	398.38	1.12551
17	2.68	1.15659	40	501.47	1.12480
18	3.33	1.15647	41	631.23	1.12415
19	4.17	1.15626	42	794.62	1.12343
20	5.20	1.15517	43	1000.28	1.12277
21	6.50	1.15386	44	1259.22	1.12207
22	8.13	1.15304	45	1440.50	1.12201
23	10.20	1.15255			



Void Ratio = 0.708 **Compression** = 30.6 %
D_0 = 1.15358 D_{50} = 1.13404 D_{100} = 1.11449
C_v **at 45.4 min.** = 0.00 ft.^{2}/day

Pressure: 0.25 tsf | **TEST READINGS** | **Load No. 13**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	1.12203	24	12.78	1.11340
2	0.10	1.11962	25	16.05	1.11287
3	0.20	1.11937	26	20.17	1.11195
4	0.23	1.11935	27	25.33	1.11125
5	0.27	1.11926	28	31.83	1.10975
6	0.32	1.11926	29	40.03	1.10806
7	0.37	1.11919	30	50.35	1.10638
8	0.43	1.11911	31	63.33	1.10418
9	0.52	1.11905	32	79.67	1.10232
10	0.63	1.11888	33	100.23	1.09946
11	0.77	1.11884	34	126.13	1.09712
12	0.93	1.11882	35	158.73	1.09385
13	1.13	1.11873	36	199.78	1.09032
14	1.40	1.11848	37	251.45	1.08777
15	1.73	1.11817	38	316.48	1.08400
16	2.15	1.11756	39	398.37	1.08072
17	2.68	1.11684	40	501.45	1.07698
18	3.33	1.11632	41	631.23	1.07325
19	4.17	1.11593	42	794.60	1.06986
20	5.20	1.11573	43	1000.28	1.06701
21	6.50	1.11509	44	1259.22	1.06406
22	8.13	1.11468	45	1440.17	1.06250
23	10.20	1.11430			



Void Ratio = 0.852 **Compression =** 24.8 %
D_0 = 1.11547 D_{50} = 1.11308 D_{100} = 1.11069
C_v **at 0.1 min.** = 1.92 ft.^{2}/day

Southern Earth Sciences, Inc.

Laboratory Test Results

Project: **Bayou DuPont** Technical Responsibility: Quality Assurance Officer

Client: URS

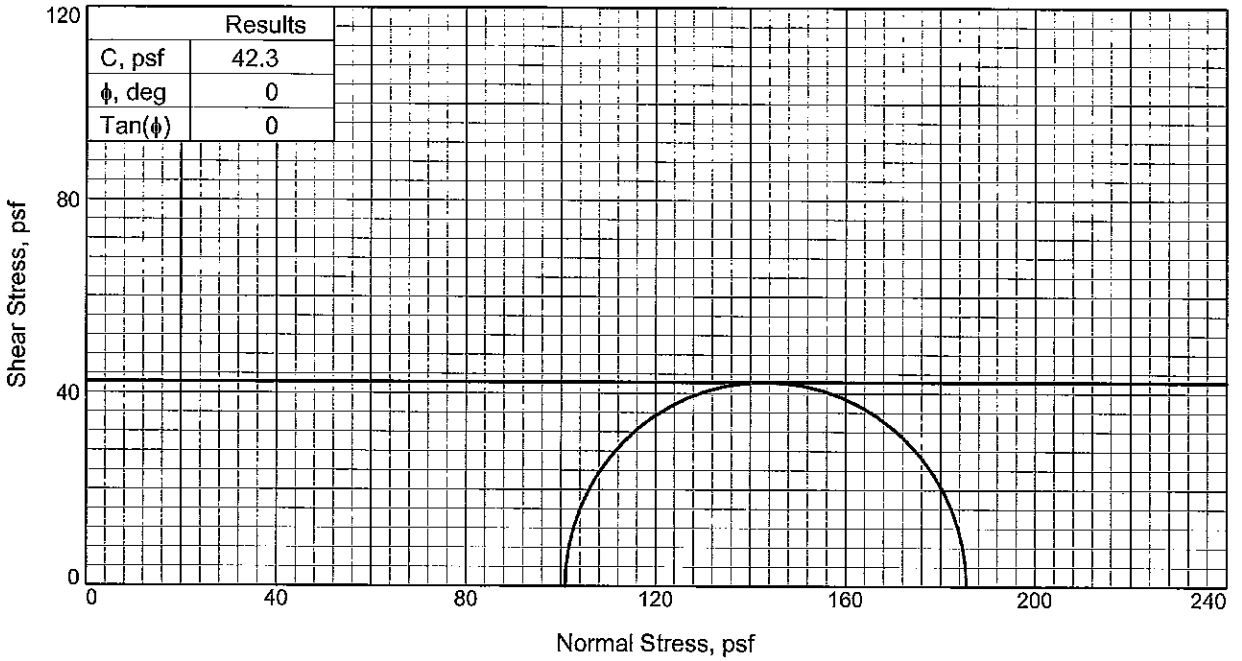
7389 Florida Blvd., Suite 300, Baton Rouge, LA 70806 Project No.: **B09-012** PM: S. Aviles Date of Issue: 3/12/2009

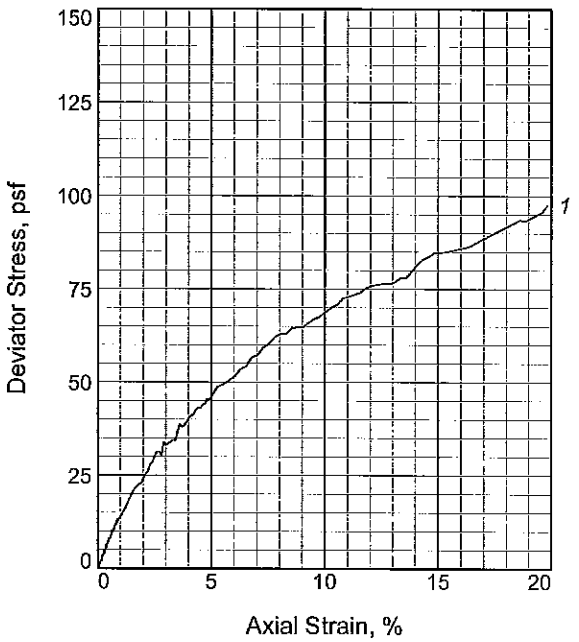
Boring No.	Depth (ft)	Classification	ASTM DESIGNATION															USCS	Confining Stress, Resistivity and Remarks
			D2216	D4318			D427	D2166		D2166	D2850	D422, C136 or C117					D2974		
				Atterberg Limits						Cohesion		Grain Size (% Passing)							
			ω %	LL	PL	PI	SL	γ_{wet} pcf	γ_{dry} pcf	U psf	UU psf	Gravel	Sand	Silt	Clay	#200	Organic Content %		
B-7	0-2	Very Soft Peat with clay pockets	955.0	925	330	595		59.5	5.6		42.3							(PT)	Confining Pressure: 0.7 psi
B-7	2-4	Very Soft Peat becoming CLAY with organics	308.8	384	100	284	20.1	73.6	18.0				0.0	21.0	79.0		20.6	(PT)	Specific Gravity: 2.400
B-7	4-6	Very Soft, Gray CLAY with organics	112.3					96.2	45.3		49.6							(CH)	Confining Pressure: 2.0 psi
B-7	6-8	Very Soft, Gray SILTY CLAY with trace organics	89.8				16.7	98.4	51.8		60.1							(CL)	Confining Pressure: 2.6 psi
B-7	8-10	Very Soft, Gray CLAY with humus and organic layers and pockets	334.0	240	62	178		79.3	18.3		95.8						24.4	(OH)	Specific Gravity: 2.811 Confining Pressure: 3.3 psi
B-7	13-15	Intermixed Gray CLAY, SILT and SANDY SILT	54.9					108.7	70.2		83.4					99.7		(CL)	Confining Pressure: 5.0 psi
B-7	18-20	Soft to Loose, Gray SILT with clay pockets and trace organics	48.1	43	21	22		122.7	82.8		287.6		3.5	74.2	22.3		1.4	(CL)	Confining Pressure: 6.6 psi
B-7	23-25	Firm, Gray CLAYEY SILT with trace sand	28.9				23.7	127.2	98.7		1058.3							(ML)	Confining Pressure: 8.3 psi
B-7	28-30	Very Soft, Gray CLAY with silt streaks and trace organics	56.3	90	30	60		110.6	70.7		173.8		0.5	56.4	43.1			(CH)	Confining Pressure: 9.9 psi
B-7	33-35	Soft, Gray CLAY becoming Gray SILT with clay	25.1					124.1	99.2		235.1							(CH)	Confining Pressure: 11.6 psi
B-7	38-40	Soft, Gray SILTY CLAY with sandy silt	47.2	35	23	12		113.9	77.4		337.2							(CL)	Confining Pressure: 13.2 psi

Geotechnical Lab
11638 Sun Belt Ct. Baton Rouge, LA 70809

The results presented only relate to those samples tested

Date Samples Rec.:
Date Testing Initiated:





Sample No.		1
Initial	Water Content, %	955.0
	Dry Density, pcf	5.6
	Saturation, %	90.4
	Void Ratio	21.1391
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	955.0
	Dry Density, pcf	5.6
	Saturation, %	90.4
	Void Ratio	21.1391
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		0.700
Fail. Stress, psf		84.7
Strain, %		14.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		185.5
σ_3 Failure, psf		100.8

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: PEAT W/ CL PKTS, PT

LL= 925 **PL=** 330 **PI=** 595
Assumed Specific Gravity= 2.00
Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

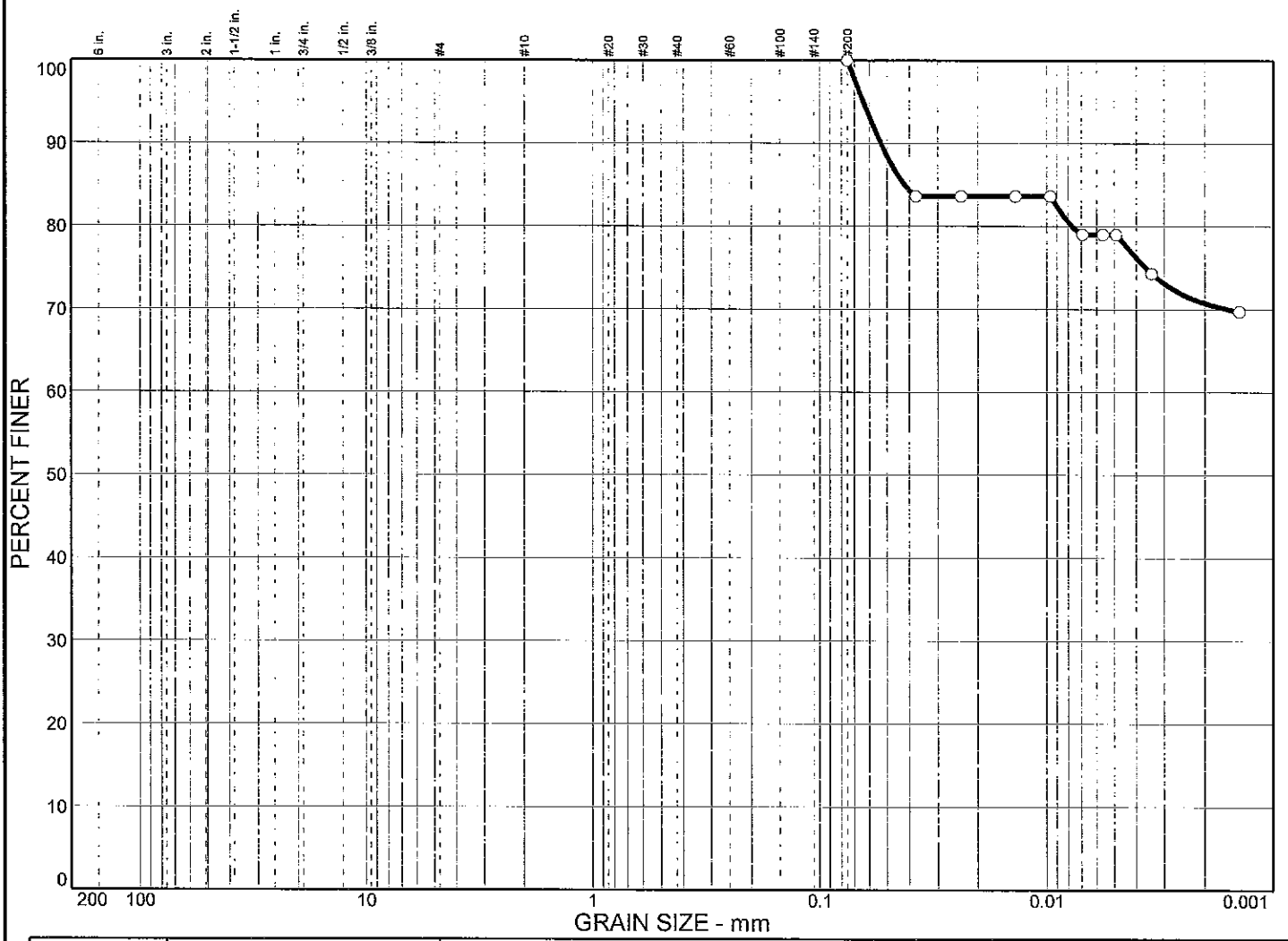
Project: BAYOU DUPONT

Source of Sample: B-7 **Depth:** 0-2
Sample Number: 1
Proj. No.: B09-012 **Date Sampled:** 3/17/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	21.0	79.0

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	384	100	0.0420							

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO PEAT BEC CL W/ ORG, PT	(PT)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

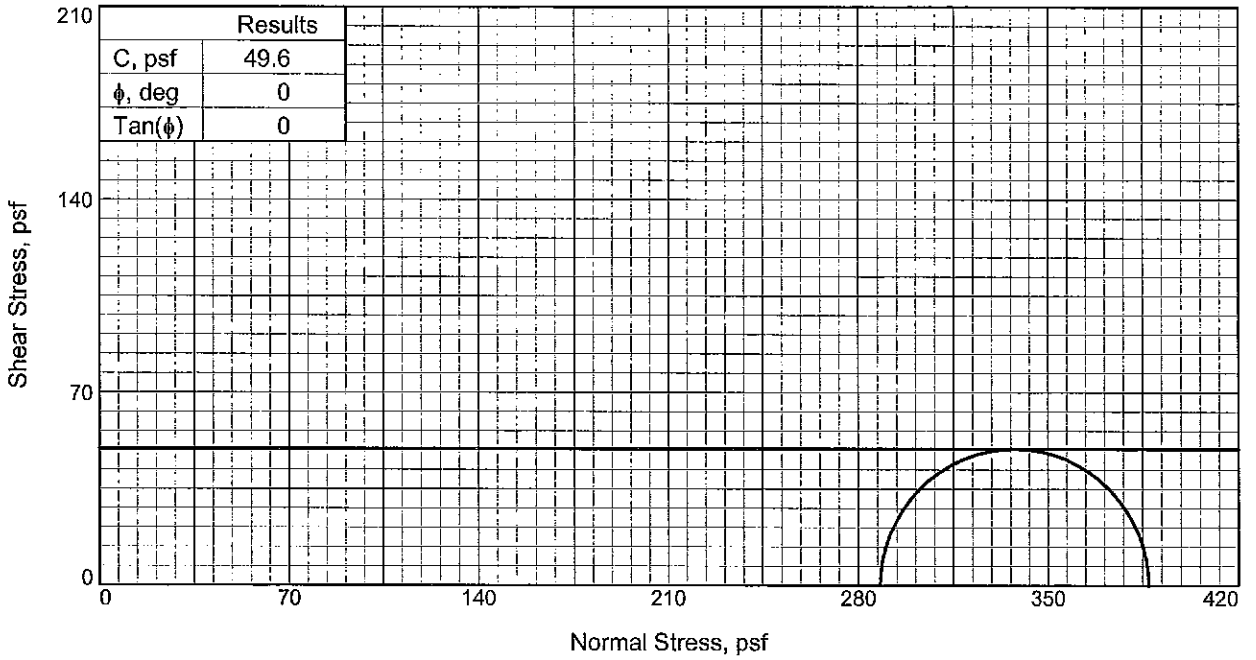
○ **Source:** B-7 **Sample No.:** 2 **Elev./Depth:** 2-4

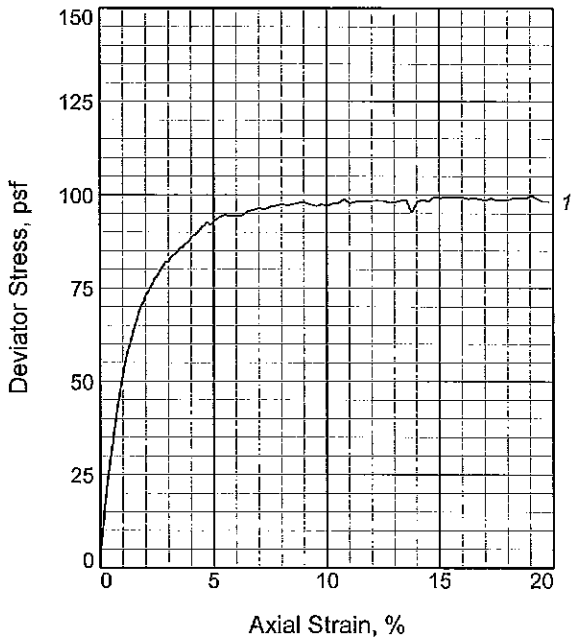
Remarks:

○ ASTM D422, C136

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	112.3
	Dry Density, pcf	45.3
	Saturation, %	110.0
	Void Ratio	2.8567
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	112.3
	Dry Density, pcf	45.3
	Saturation, %	110.0
	Void Ratio	2.8567
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.000
Fail. Stress, psf		99.2
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		387.2
σ_3 Failure, psf		288.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ ORG, CH

Assumed Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

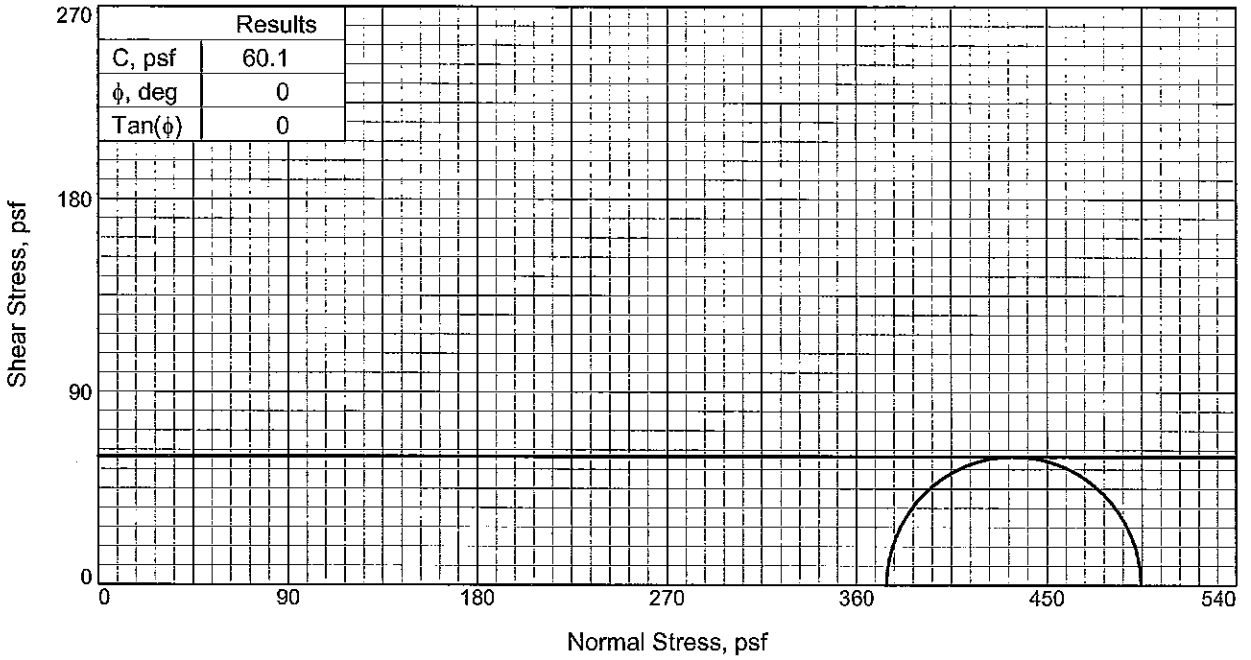
Source of Sample: B-7 **Depth:** 4-6

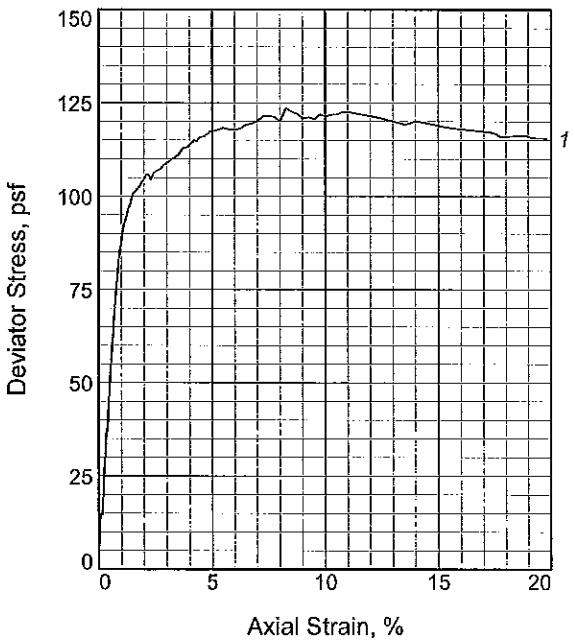
Sample Number: 3

Proj. No.: B09-012 **Date Sampled:** 3/17/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	89.8
	Dry Density, pcf	51.8
	Saturation, %	107.6
	Void Ratio	2.2518
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	89.8
	Dry Density, pcf	51.8
	Saturation, %	107.6
	Void Ratio	2.2518
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.600
Fail. Stress, psf		120.1
Strain, %		8.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		494.5
σ_3 Failure, psf		374.4

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G SICL W/ TR ORG, CL

Assumed Specific Gravity= 2.70

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

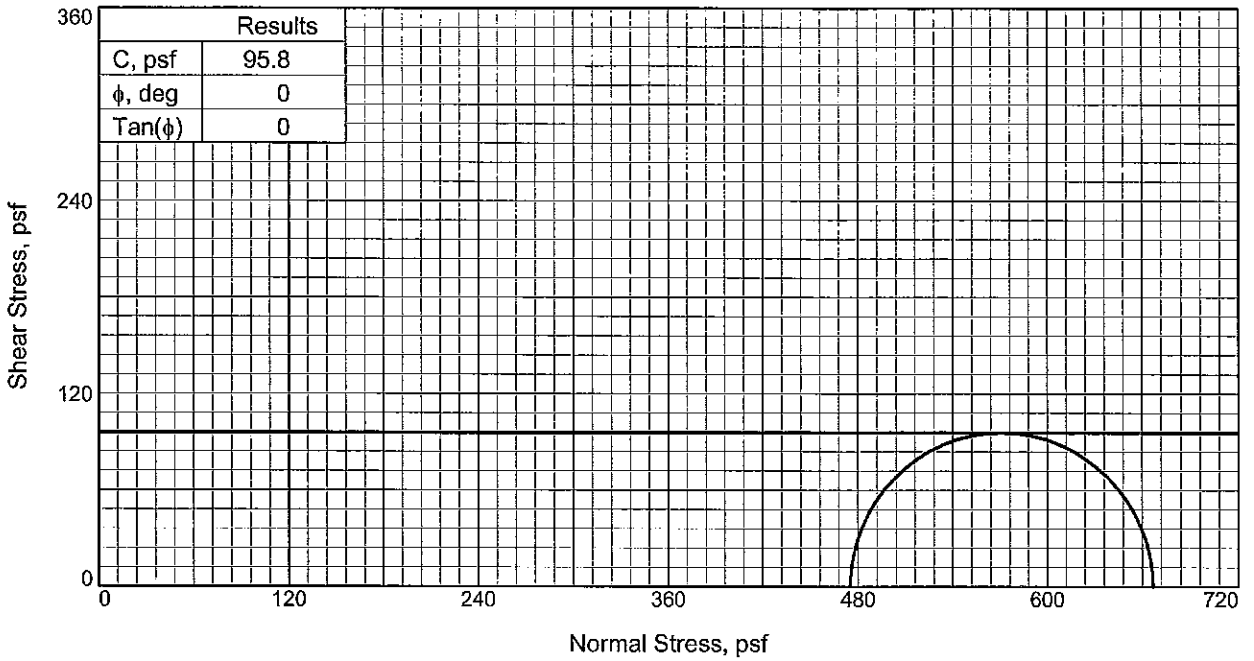
Source of Sample: B-7 **Depth:** 6-8

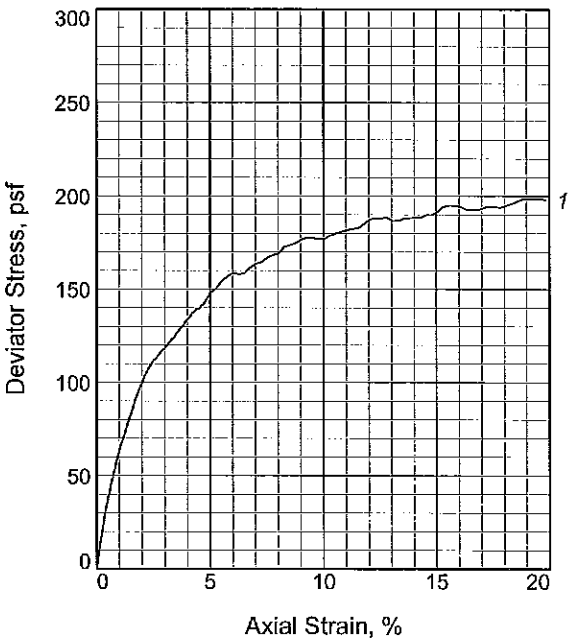
Sample Number: 4

Proj. No.: B09-012 **Date Sampled:** 3/17/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	334.0
	Dry Density, pcf	18.3
	Saturation, %	109.1
	Void Ratio	8.6105
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	334.0
	Dry Density, pcf	18.3
	Saturation, %	109.1
	Void Ratio	8.6105
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		3.300
Fail. Stress, psf		191.6
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		666.8
σ_3 Failure, psf		475.2

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ HUMUS & ORG LYRS & PKTS, OH

LL= 240 **PL=** 62 **PI=** 178

Specific Gravity= 2.811

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

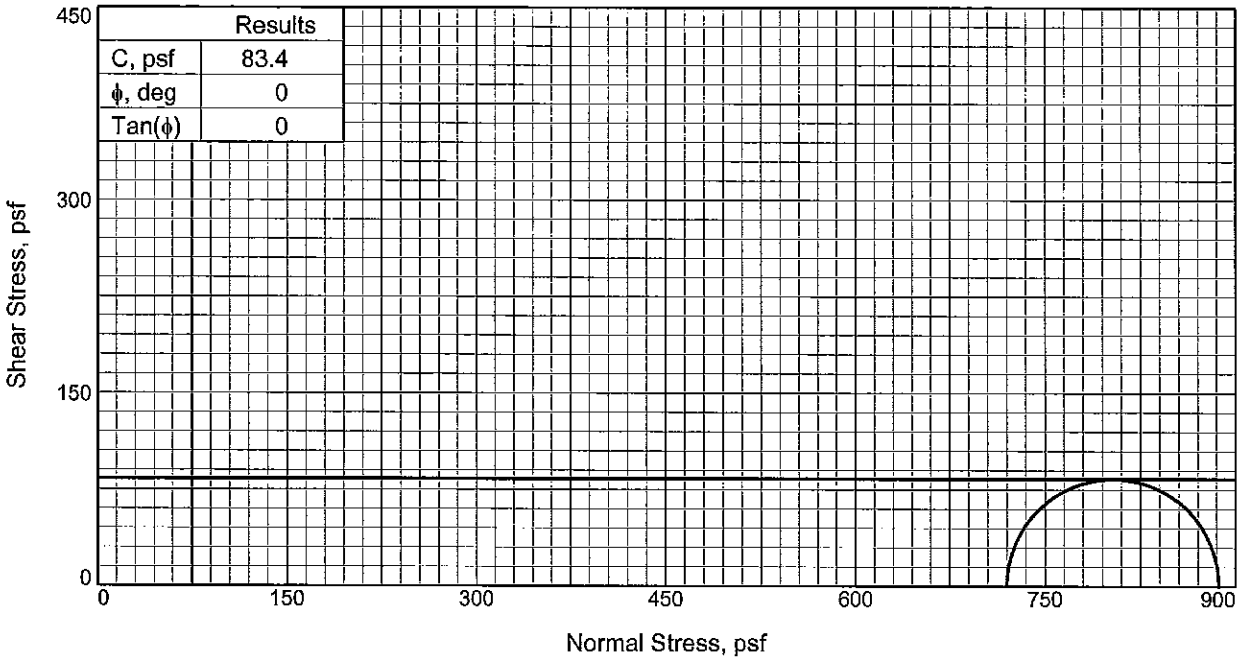
Source of Sample: B-7 **Depth:** 8-10

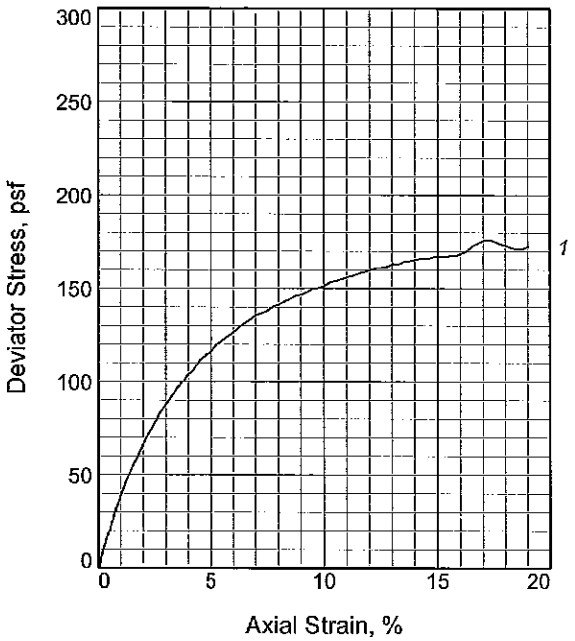
Sample Number: 5

Proj. No.: B09-012 **Date Sampled:** 3/17/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	54.9
	Dry Density, pcf	70.2
	Saturation, %	107.2
	Void Ratio	1.3571
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	54.9
	Dry Density, pcf	70.2
	Saturation, %	107.2
	Void Ratio	1.3571
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		5.000
Fail. Stress, psf		166.8
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		886.8
σ_3 Failure, psf		720.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: INT MIX G CL SI & SASI, CL TO ML

Assumed Specific Gravity= 2.65

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

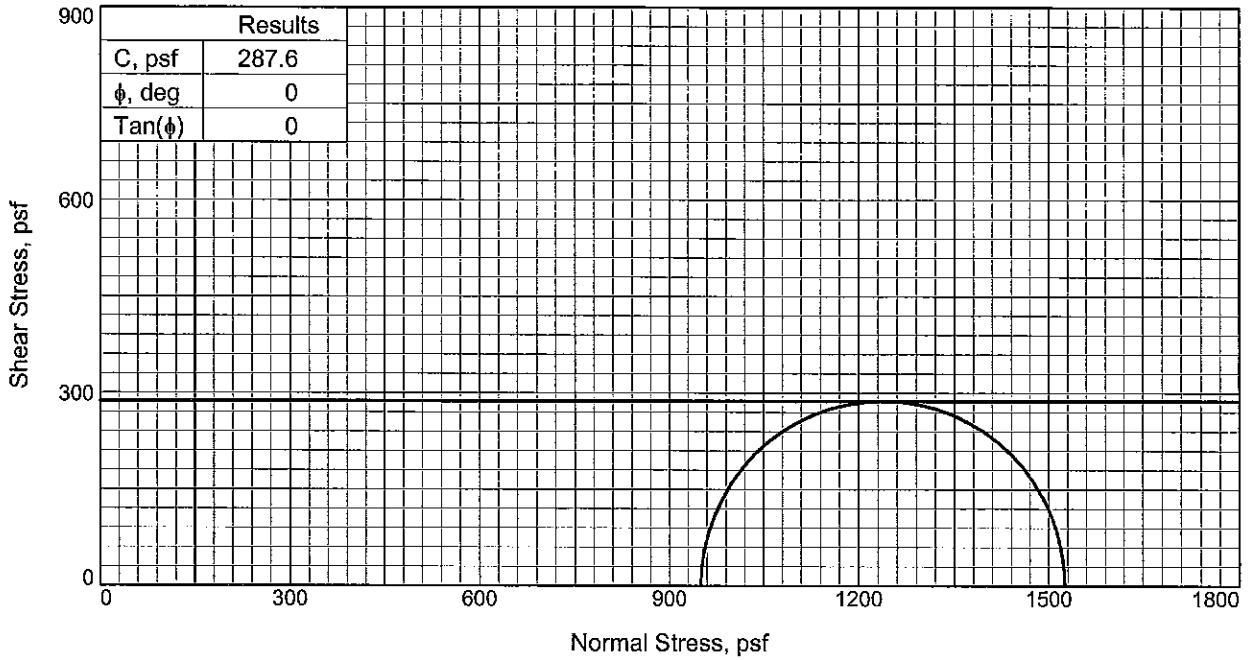
Source of Sample: B-7 **Depth:** 13-15

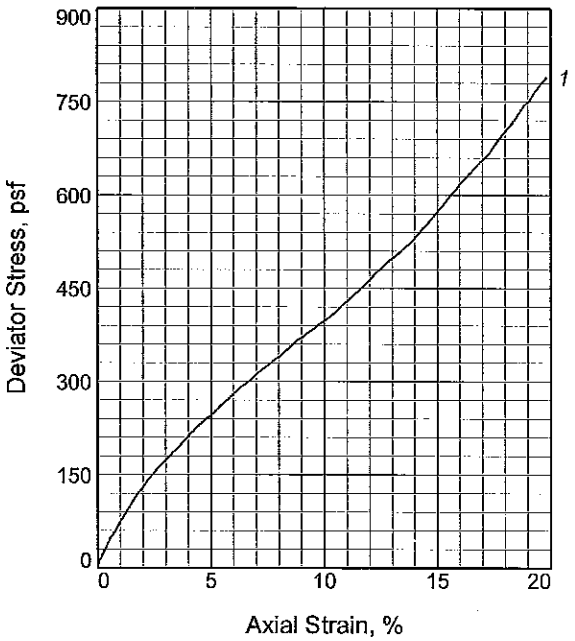
Sample Number: 6

Proj. No.: B09-012 **Date Sampled:** 3/17/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	48.1
	Dry Density, pcf	82.8
	Saturation, %	127.8
	Void Ratio	0.9969
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	48.1
	Dry Density, pcf	82.8
	Saturation, %	127.8
	Void Ratio	0.9969
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		6.600
Fail. Stress, psf		575.2
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1525.6
σ_3 Failure, psf		950.4

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTUBED

Description: SO-LO G SI W/ CL PKTS & TR ORG, CL

LL= 43 **PL=** 21 **PI=** 22

Assumed Specific Gravity= 2.65

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-7 **Depth:** 18-20

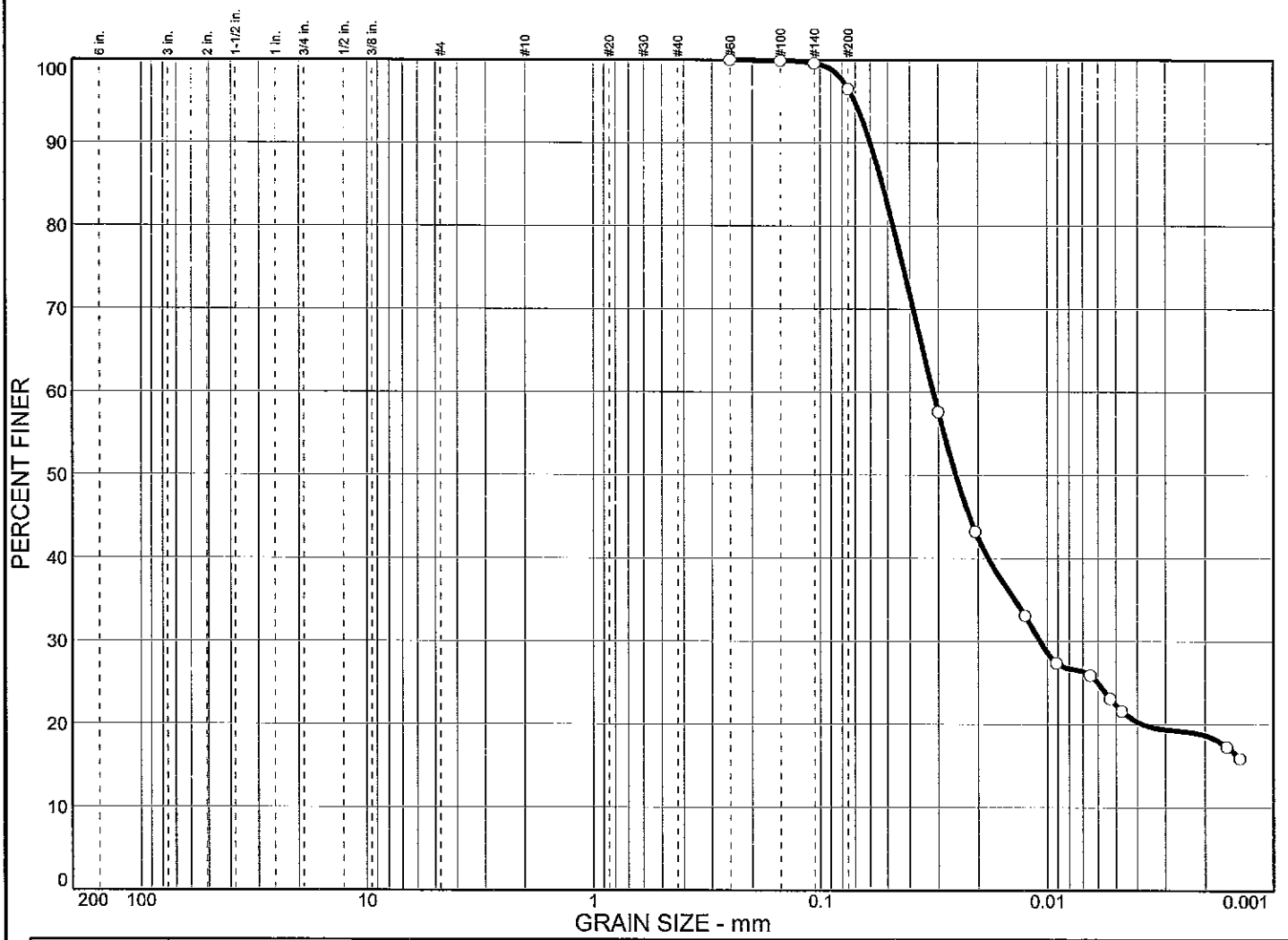
Sample Number: 7

Proj. No.: B09-012 **Date Sampled:** 3/17/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	3.5	74.2	22.3

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	43	21	0.0529	0.0316	0.0251	0.0107				

MATERIAL DESCRIPTION	USCS	AASHTO
○ SO-LO G SI W/ CL PKTS & TR ORG, CL	(CL)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-7 **Sample No.:** 7 **Elev./Depth:** 18-20

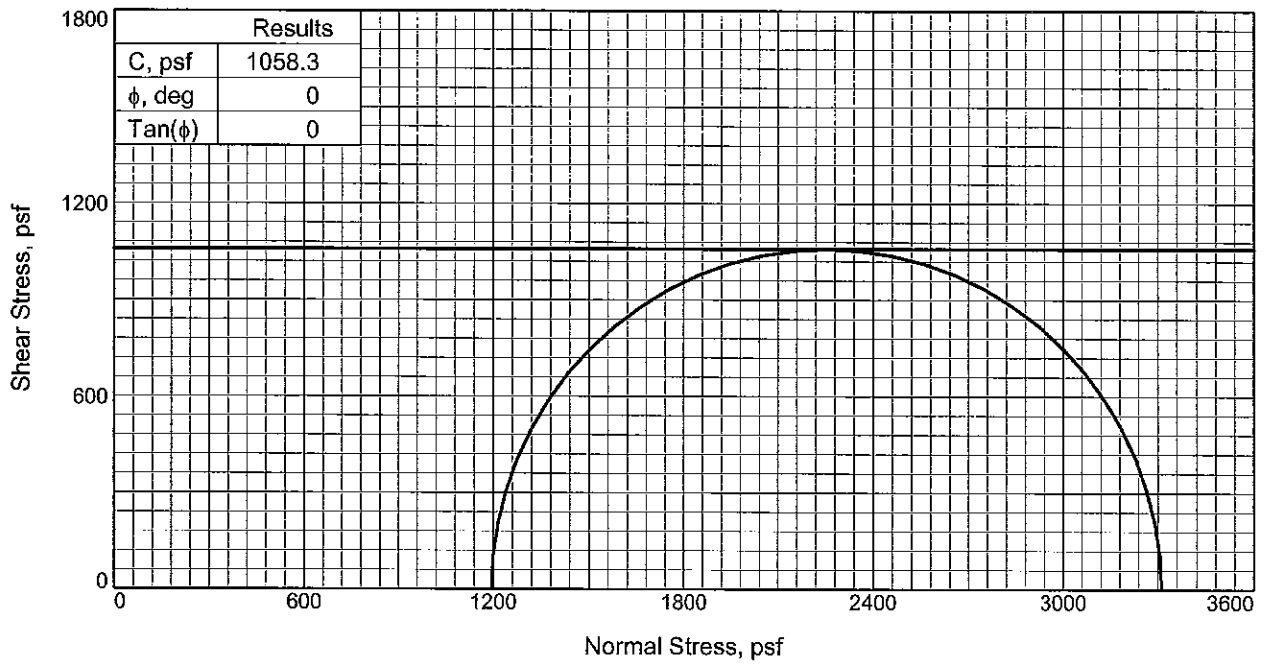
Remarks:

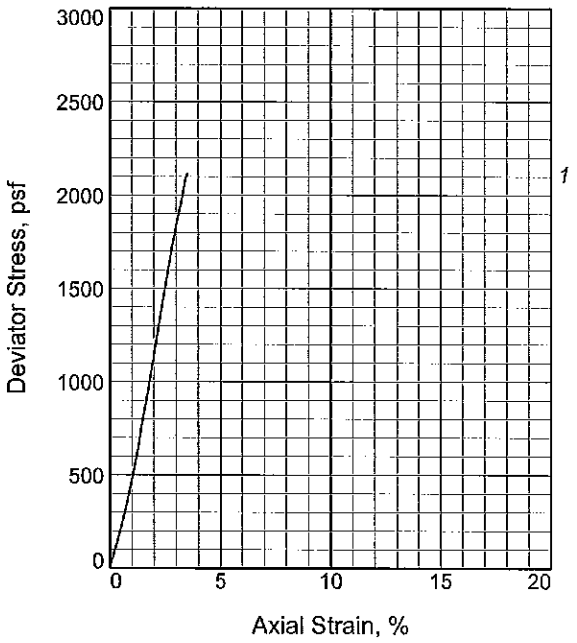
○ ASTM D422, C136

F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	28.9
	Dry Density, pcf	98.7
	Saturation, %	113.1
	Void Ratio	0.6759
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	28.9
	Dry Density, pcf	98.7
	Saturation, %	113.1
	Void Ratio	0.6759
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		8.300
Fail. Stress, psf		2116.6
Strain, %		3.5
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3311.8
σ_3 Failure, psf		1195.2

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: FM G CLSI W/ TR SA, ML

Assumed Specific Gravity= 2.65

Remarks: TYPE OF FAILURE: MAXED OUT RING

ASTM D2850

Client: URS

Project: BAYOU DUPONT

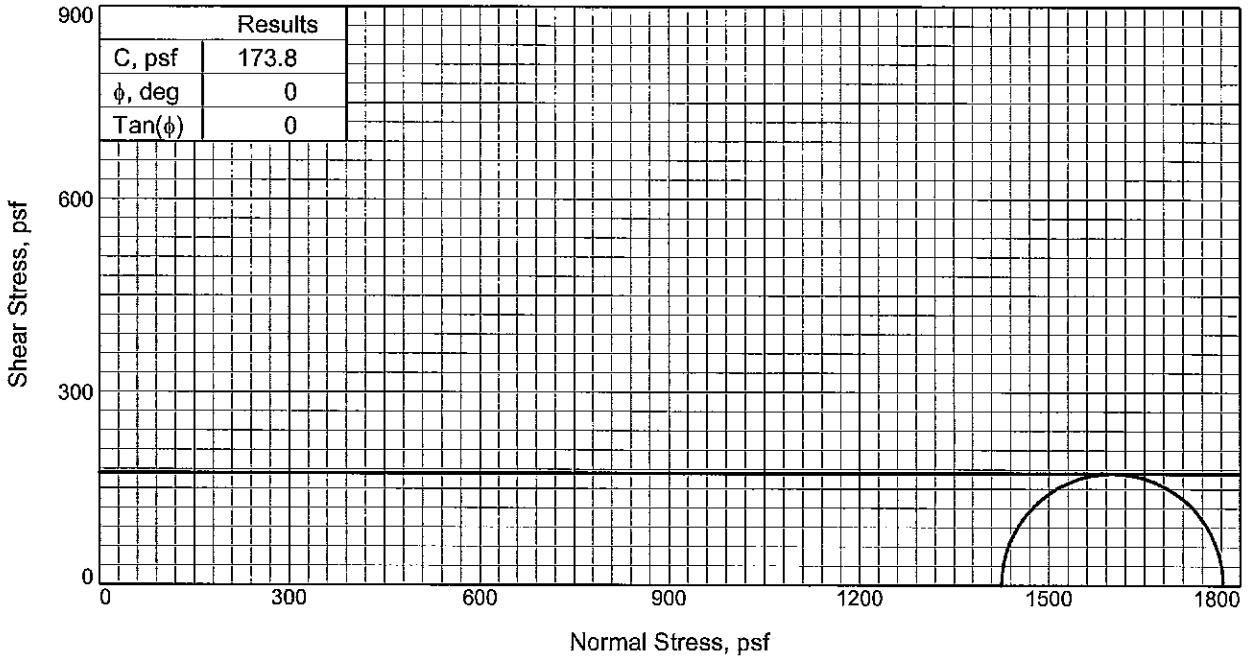
Source of Sample: B-7 **Depth:** 23-25

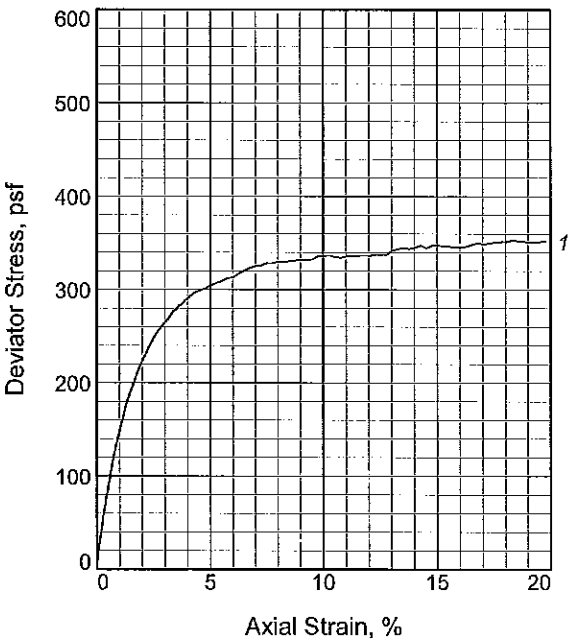
Sample Number: 8

Proj. No.: B09-012 **Date Sampled:** 3/17/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	56.3
	Dry Density, pcf	70.7
	Saturation, %	108.5
	Void Ratio	1.4274
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	56.3
	Dry Density, pcf	70.7
	Saturation, %	108.5
	Void Ratio	1.4274
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		9.900
Fail. Stress, psf		347.7
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1773.3
σ_3 Failure, psf		1425.6

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ SI STKS & TR ORG, CH

LL= 90 **PL=** 30 **PI=** 60

Assumed Specific Gravity= 2.75

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-7 **Depth:** 28-30

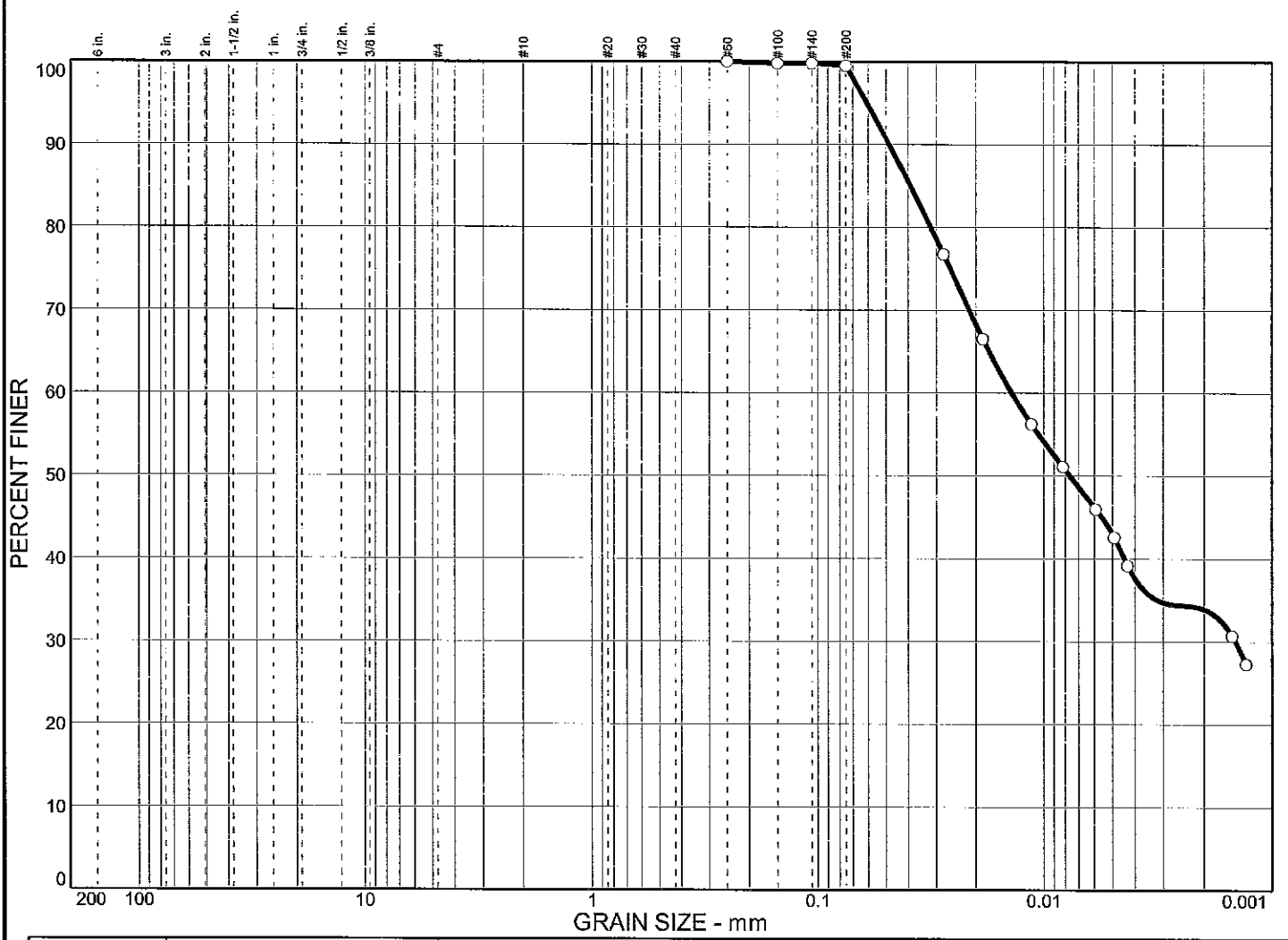
Sample Number: 9

Proj. No.: B09-012 **Date Sampled:** 3/17/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.5	56.4	43.1

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	90	30	0.0390	0.0139		0.0015				

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ SI STKS & TR ORG, CH	(CH)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-7 **Sample No.:** 9 **Elev./Depth:** 28-30

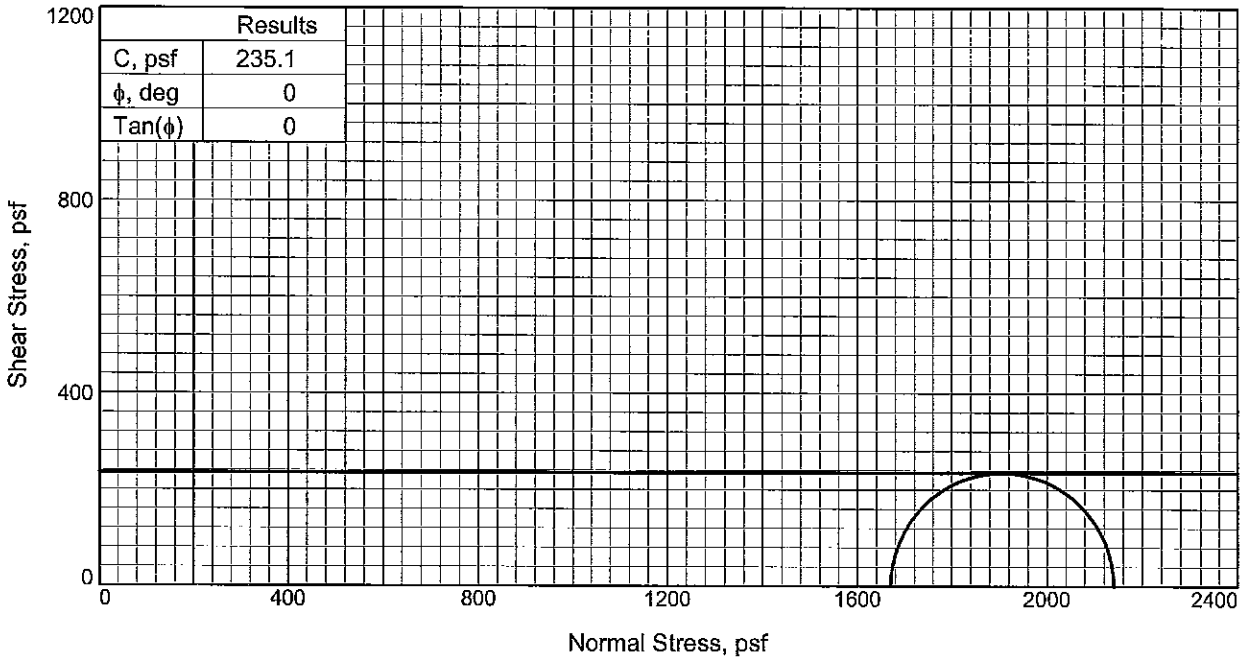
Remarks:

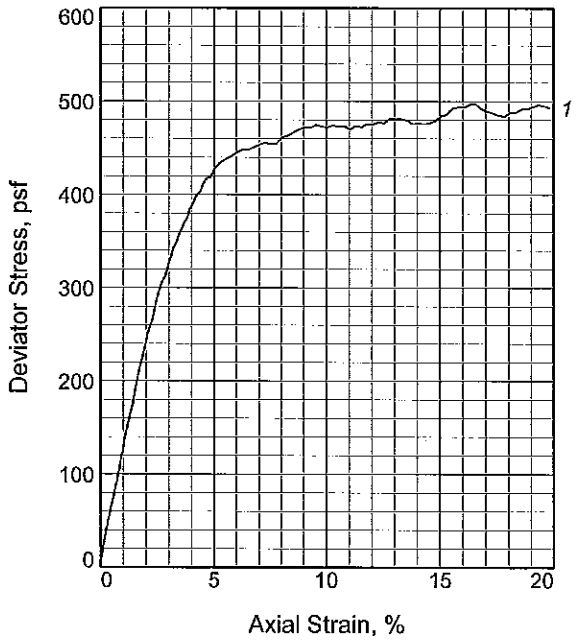
○ ASTM D422, C136

F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	25.1
	Dry Density, pcf	99.2
	Saturation, %	96.8
	Void Ratio	0.6994
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	25.1
	Dry Density, pcf	99.2
	Saturation, %	96.8
	Void Ratio	0.6994
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		11.600
Fail. Stress, psf		470.2
Strain, %		11.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2140.6
σ_3 Failure, psf		1670.4

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: SO G CL BEC G SI W/CL, CH

Assumed Specific Gravity= 2.70

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

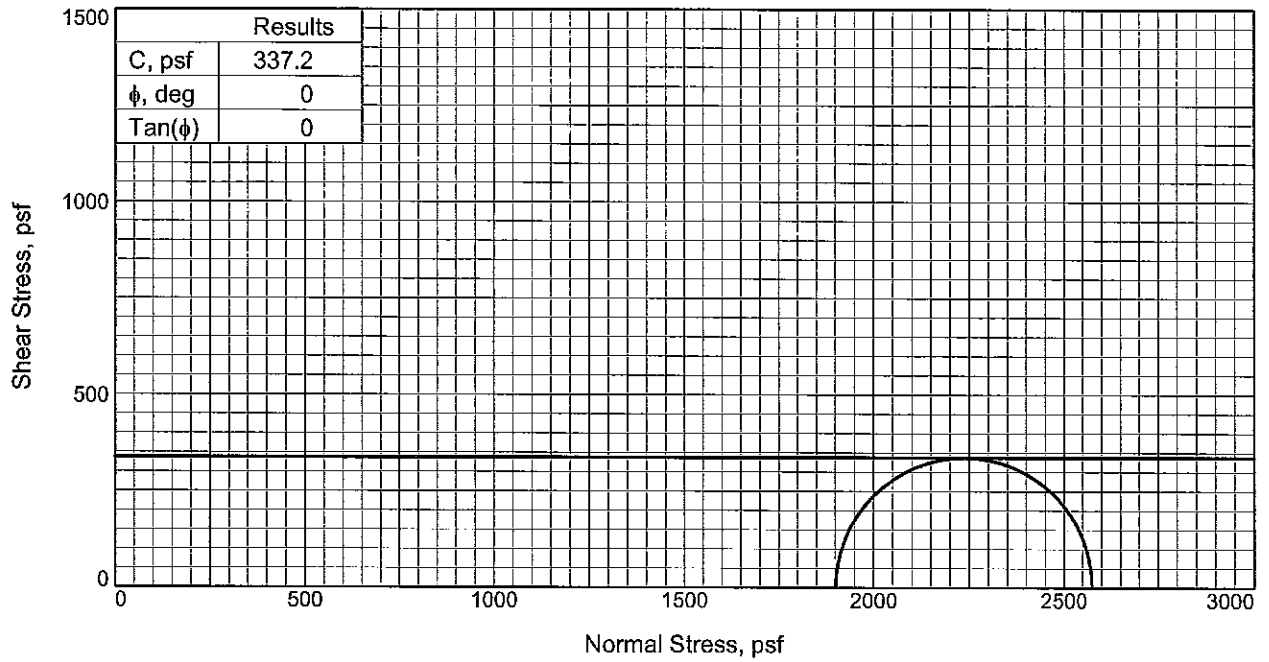
Source of Sample: B-7 **Depth:** 33-35

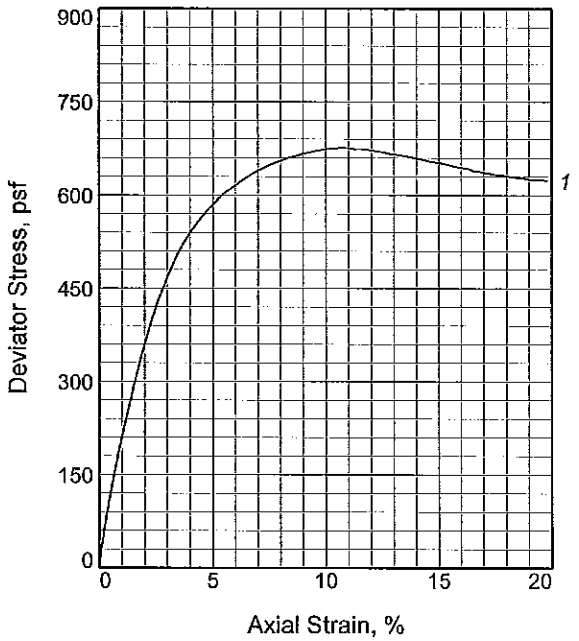
Sample Number: 10

Proj. No.: B09-012 **Date Sampled:** 3/17/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	47.2
	Dry Density, pcf	77.4
	Saturation, %	108.2
	Void Ratio	1.1777
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	47.2
	Dry Density, pcf	77.4
	Saturation, %	108.2
	Void Ratio	1.1777
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		13.200
Fail. Stress, psf		674.3
Strain, %		10.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2575.1
σ_3 Failure, psf		1900.8

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: SO G SICL W/ SASI, CL

LL= 35 **PL=** 23 **PI=** 12
Assumed Specific Gravity= 2.70
Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

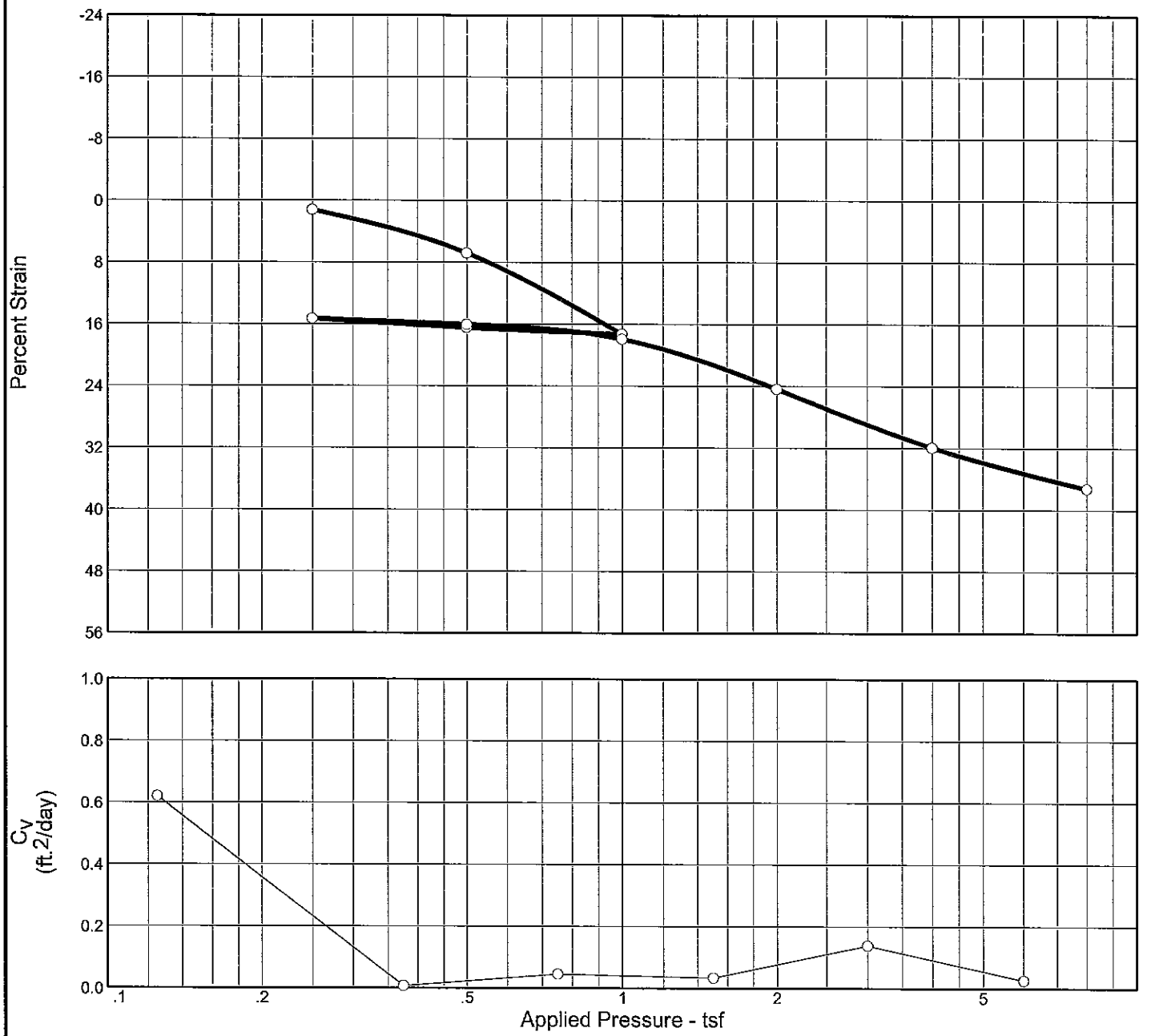
Project: BAYOU DUPONT

Source of Sample: B-7 **Depth:** 38-40
Sample Number: 11
Proj. No.: B09-012 **Date Sampled:** 3/17/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
104.6 %	88.7 %	51.5	90	60	2.75	(CH)		2.332

MATERIAL DESCRIPTION

VSO G CL W/ SI STKS & TR ORG, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

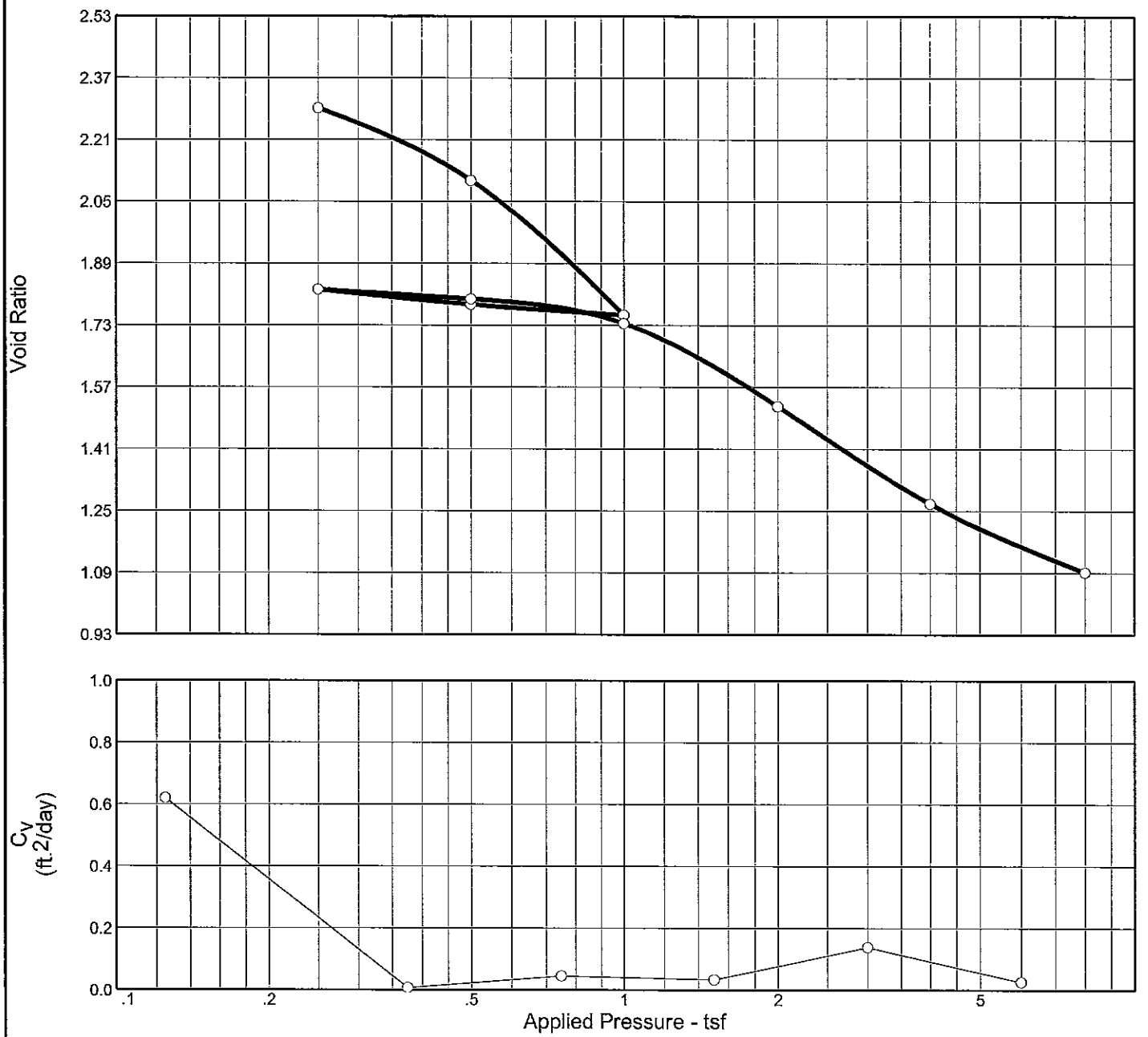
Source: B-7 **Sample No.:** 9 **Elev./Depth:** 28-30

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

Remarks:
ASTM D2435

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
104.6 %	88.7 %	51.5	90	60	2.75	(CH)		2.332

MATERIAL DESCRIPTION

VSO G CL W/ SI STKS & TR ORG, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-7 **Sample No.:** 9 **Elev./Depth:** 28-30

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

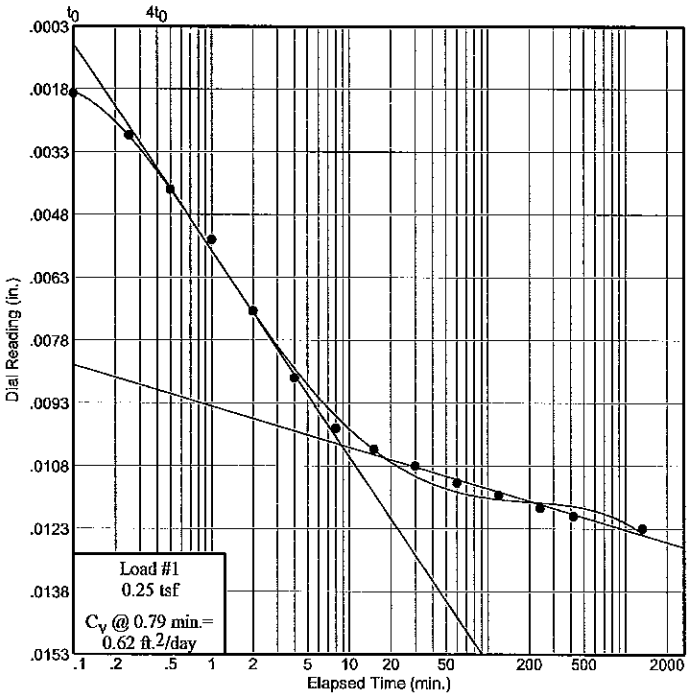
Remarks:

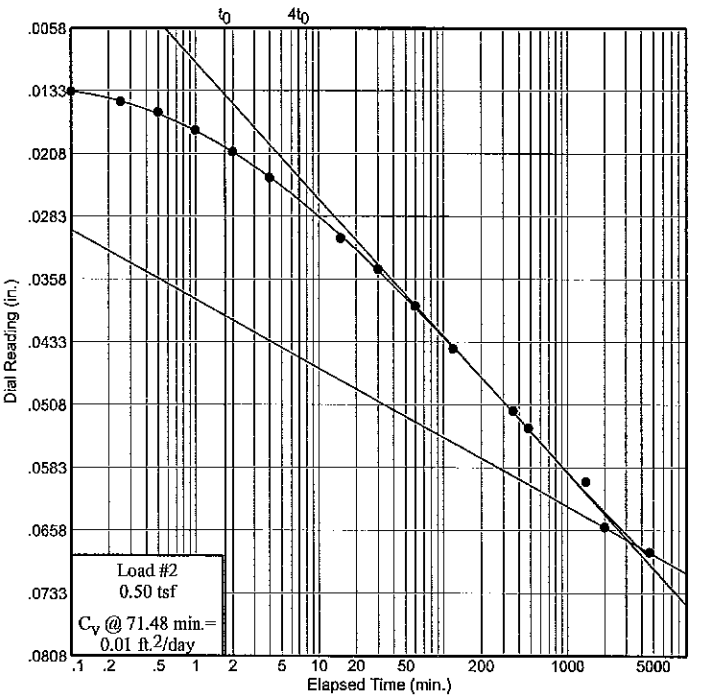
ASTM D2435

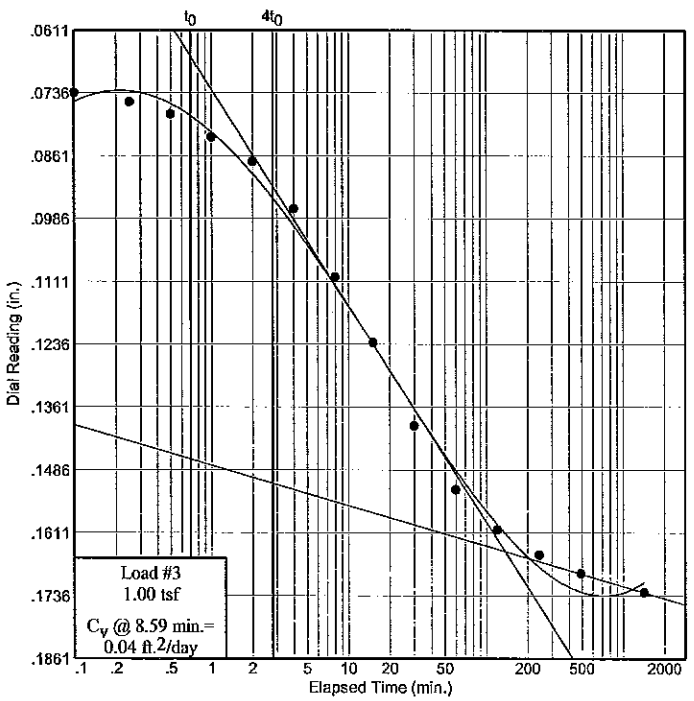
Dial Reading vs. Time

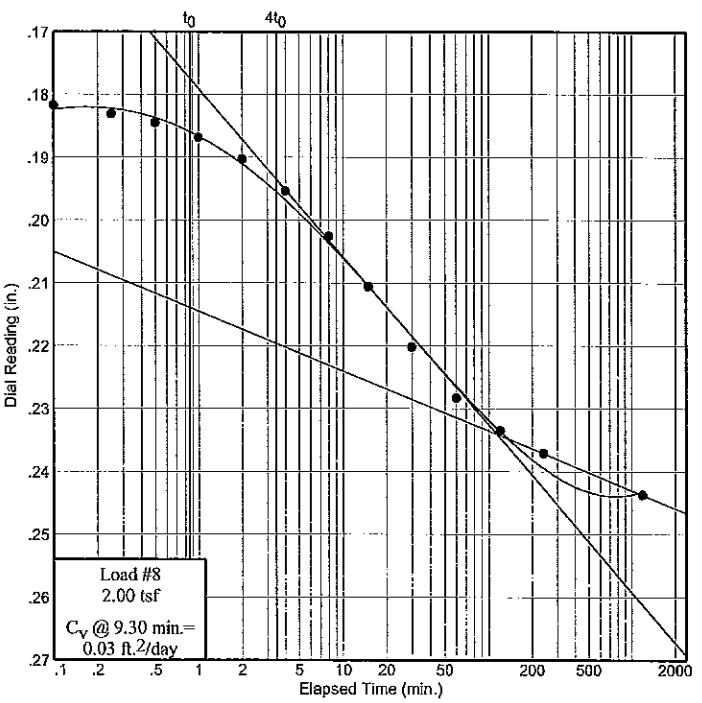
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-7 Sample No.: 9 Elev./Depth: 28-30









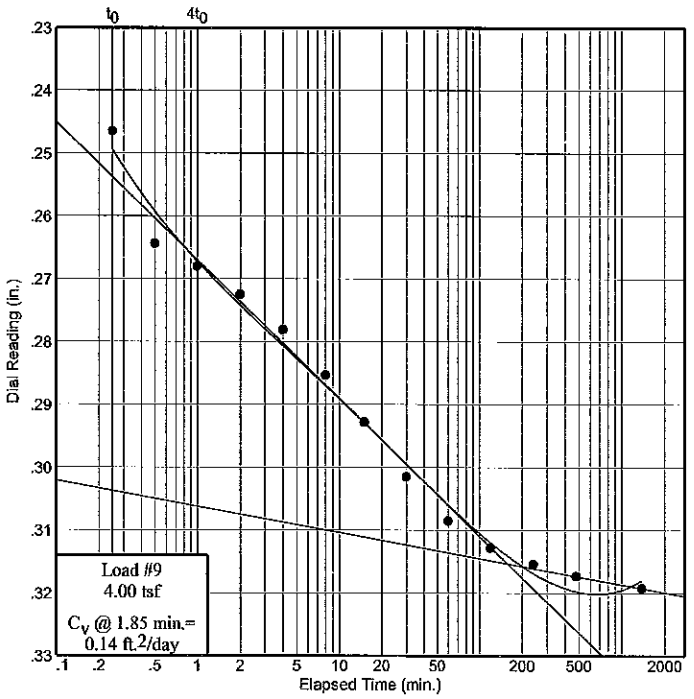
Dial Reading vs. Time

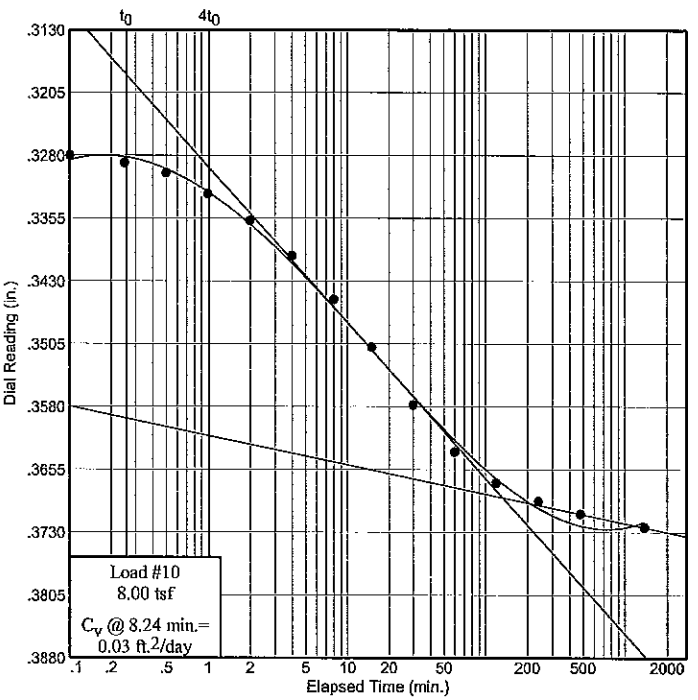
Southern Earth Sciences, Inc.

Dial Reading vs. Time

Project No.: B09-012
Project: BAYOU DUPONT

Source: B-7 Sample No.: 9 Elev./Depth: 28-30





CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-7
Sample No.: 9
Elev. or Depth: 28-30 **Sample Length(in./cm.):**
Location:
Description: VSO G CL W/ SI STKS & TR ORG, CH
Liquid Limit: 90 **Plasticity Index:** 60
USCS: (CH) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST	AFTER TEST
Wet w+t =	112.88 g.	**Consolidometer #** = 1	**Wet w+t** =
Dry w+t =	77.63 g.		**Dry w+t** =
Tare Wt. =	37.91 g.	**Spec. Gravity** = 2.75	**Tare Wt.** =
Height =	.75 in.	**Height** = 1.00 in.	
Diameter =	2.50 in.	**Diameter** = 2.50 in.	
Weight =	93.97 g.	**Defl. Table** = Unit No. 1 Old 2.5in	
Moisture =	88.7 %	**Ht. Solids** = 0.3001 in.	**Moisture** = %
Wet Den. =	97.2 pcf	**Dry Wt.** = 66.38 g.*	**Dry Wt.** = n/a
Dry Den. =	51.5 pcf	**Void Ratio** = 2.332	**Void Ratio** = 1.091
		Saturation = 104.6 %	

*** Initial dry weight used in calculations**

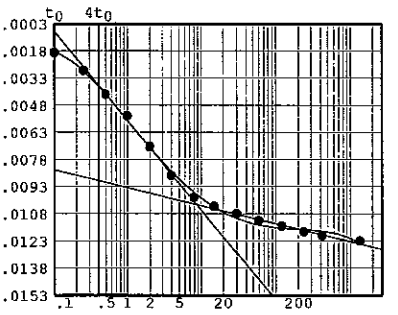
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				2.332	
0.25	0.01290	0.00060	0.62	0.001	2.291	1.2 Comprs.
0.50	0.06950	0.00110	0.01	0.008	2.104	6.8 Comprs.
1.00	0.17480	0.00190	0.04	0.009	1.756	17.3 Comprs.
0.50	0.16680	0.00210	0.15		1.784	16.5 Comprs.
0.25	0.15490	0.00180	0.05		1.822	15.3 Comprs.
0.50	0.16250	0.00200	0.16	0.001	1.798	16.0 Comprs.
1.00	0.18190	0.00250	0.14	0.004	1.735	17.9 Comprs.
2.00	0.24640	0.00270	0.03	0.012	1.520	24.4 Comprs.
4.00	0.32290	0.00370	0.14	0.005	1.269	31.9 Comprs.
8.00	0.37710	0.00470	0.03	0.005	1.091	37.2 Comprs.

C_c = 0.57 P_c = 0.00 tsf C_r = 0.15

Pressure: 0.25 tsf **TEST READINGS** **Load No. 1**

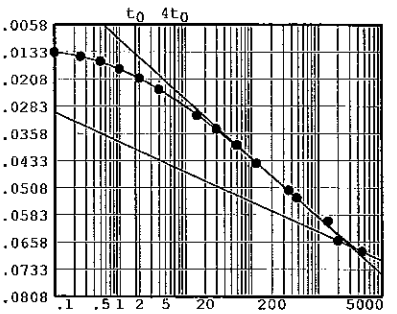
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	60.00	0.01180
2	0.10	0.00250	12	120.00	0.01210
3	0.25	0.00350	13	240.00	0.01240
4	0.50	0.00480	14	420.00	0.01260
5	1.00	0.00600	15	1333.00	0.01290
6	2.00	0.00770			
7	4.00	0.00930			
8	8.00	0.01050			
9	15.00	0.01100			
10	30.00	0.01140			



Void Ratio = 2.291 **Compression** = 1.2 %
D_0 = -0.00004 D_{50} = 0.00513 D_{100} = 0.01030
C_v at 0.8 min. = 0.62 ft.^{2}/day C_α = 0.001

Pressure: 0.50 tsf **TEST READINGS** **Load No. 2**

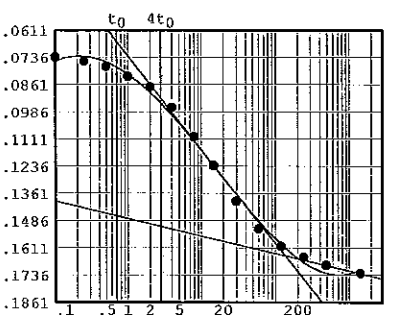
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.01290	11	120.00	0.04520
2	0.10	0.01450	12	360.00	0.05260
3	0.25	0.01570	13	480.00	0.05470
4	0.50	0.01700	14	1410.00	0.06110
5	1.00	0.01910	15	2000.00	0.06650
6	2.00	0.02170	16	4620.00	0.06950
7	4.00	0.02480			
8	15.00	0.03200			
9	30.00	0.03570			
10	60.00	0.04010			



Void Ratio = 2.104 **Compression** = 6.8 %
D_0 = 0.01378 D_{50} = 0.04038 D_{100} = 0.06699
C_v at 71.5 min. = 0.01 ft.^{2}/day C_α = 0.008

Pressure: 1.00 tsf **TEST READINGS** **Load No. 3**

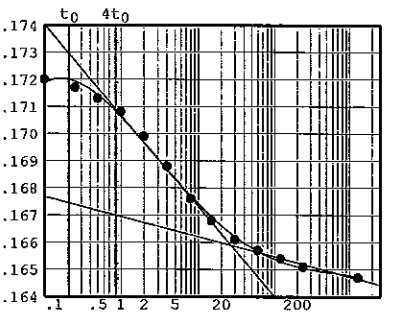
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.06950	11	60.00	0.15440
2	0.10	0.07550	12	120.00	0.16240
3	0.25	0.07730	13	242.00	0.16740
4	0.50	0.07970	14	490.00	0.17110
5	1.00	0.08430	15	1420.00	0.17480
6	2.00	0.08920			
7	4.00	0.09860			
8	8.00	0.11210			
9	15.00	0.12520			
10	30.00	0.14170			



Void Ratio = 1.756 **Compression** = 17.3 %
D_0 = 0.06175 D_{50} = 0.11325 D_{100} = 0.16475
C_v at 8.6 min. = 0.04 ft.^{2}/day C_α = 0.009

Pressure: 0.50 tsf — **TEST READINGS** — **Load No. 4**

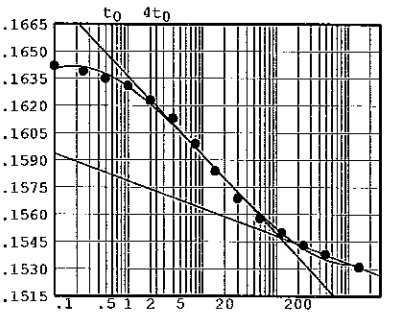
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.17480	11	60.00	0.16780
2	0.10	0.17410	12	120.00	0.16750
3	0.25	0.17380	13	240.00	0.16720
4	0.50	0.17340	14	1290.00	0.16680
5	1.00	0.17290			
6	2.00	0.17200			
7	4.00	0.17090			
8	8.00	0.16970			
9	15.00	0.16890			
10	30.00	0.16820			



Void Ratio = 1.784 **Compression** = 16.5 %
D_0 = 0.17314 D_{50} = 0.16952 D_{100} = 0.16589
C_v at 2.2 min. = 0.15 ft.^{2}/day

Pressure: 0.25 tsf — **TEST READINGS** — **Load No. 5**

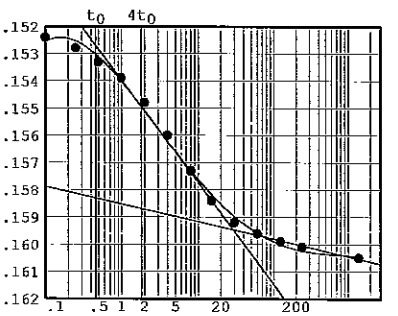
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.16680	11	60.00	0.15760
2	0.10	0.16600	12	120.00	0.15680
3	0.25	0.16570	13	240.00	0.15610
4	0.50	0.16530	14	480.00	0.15560
5	1.00	0.16490	15	1390.00	0.15490
6	2.00	0.16410			
7	4.00	0.16310			
8	8.00	0.16170			
9	15.00	0.16020			
10	30.00	0.15870			



Void Ratio = 1.822 **Compression** = 15.3 %
D_0 = 0.16539 D_{50} = 0.16007 D_{100} = 0.15476
C_v at 6.6 min. = 0.05 ft.^{2}/day

Pressure: 0.50 tsf — **TEST READINGS** — **Load No. 6**

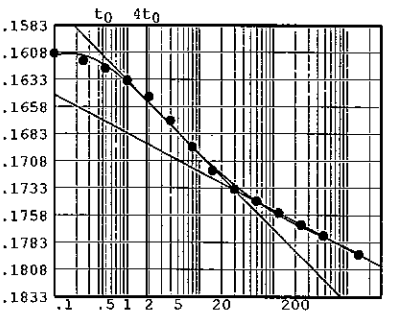
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.15490	11	60.00	0.16160
2	0.10	0.15440	12	125.00	0.16190
3	0.25	0.15480	13	240.00	0.16210
4	0.50	0.15530	14	1380.00	0.16250
5	1.00	0.15590			
6	2.00	0.15680			
7	4.00	0.15800			
8	8.00	0.15930			
9	15.00	0.16040			
10	30.00	0.16120			



Void Ratio = 1.798 **Compression** = 16.0 %
D_0 = 0.15109 D_{50} = 0.15528 D_{100} = 0.15946
C_v at 2.3 min. = 0.16 ft.^{2}/day C_α = 0.001

Pressure: 1.00 tsf **TEST READINGS** **Load No. 7**

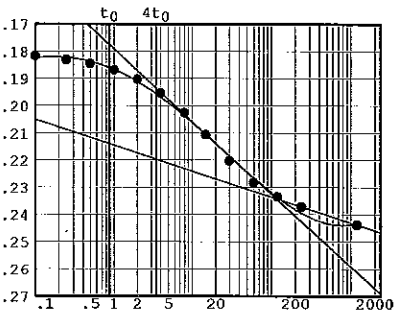
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.16250	11	60.00	0.17700
2	0.10	0.16340	12	120.00	0.17810
3	0.25	0.16410	13	240.00	0.17920
4	0.50	0.16480	14	480.00	0.18020
5	1.00	0.16590	15	1440.00	0.18190
6	2.00	0.16740			
7	4.00	0.16960			
8	8.00	0.17200			
9	15.00	0.17420			
10	30.00	0.17590			



Void Ratio = 1.735 **Compression =** 17.9 %
D_0 = 0.15856 D_{50} = 0.16602 D_{100} = 0.17348
C_v at 2.5 min. = 0.14 ft.^{2}/day C_α = 0.004

Pressure: 2.00 tsf **TEST READINGS** **Load No. 8**

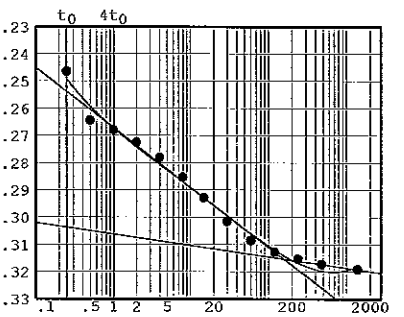
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.18190	11	60.00	0.23100
2	0.10	0.18440	12	120.00	0.23620
3	0.25	0.18580	13	240.00	0.23980
4	0.50	0.18720	14	1190.00	0.24640
5	1.00	0.18960			
6	2.00	0.19300			
7	4.00	0.19810			
8	8.00	0.20530			
9	15.00	0.21330			
10	30.00	0.22290			



Void Ratio = 1.520 **Compression =** 24.4 %
D_0 = 0.17635 D_{50} = 0.20521 D_{100} = 0.23407
C_v at 9.3 min. = 0.03 ft.^{2}/day C_α = 0.012

Pressure: 4.00 tsf **TEST READINGS** **Load No. 9**

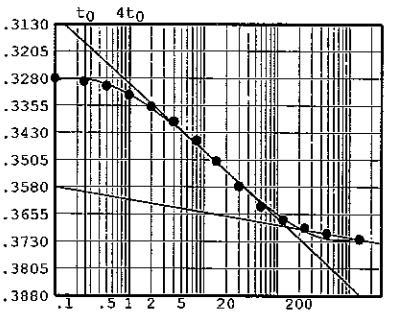
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.24640	11	120.00	0.31650
2	0.25	0.25020	12	240.00	0.31910
3	0.50	0.26810	13	480.00	0.32100
4	1.00	0.27170	14	1380.00	0.32290
5	2.00	0.27620			
6	4.00	0.28180			
7	8.00	0.28900			
8	15.00	0.29650			
9	30.00	0.30520			
10	60.00	0.31220			



Void Ratio = 1.269 **Compression =** 31.9 %
D_0 = 0.23150 D_{50} = 0.27340 D_{100} = 0.31530
C_v at 1.8 min. = 0.14 ft.^{2}/day C_α = 0.005

Pressure: 8.00 tsf | TEST READINGS | Load No. 10

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.32290	11	60.00	0.36810
2	0.10	0.33270	12	120.00	0.37180
3	0.25	0.33360	13	240.00	0.37400
4	0.50	0.33480	14	480.00	0.37550
5	1.00	0.33730	15	1380.00	0.37710
6	2.00	0.34050			
7	4.00	0.34470			
8	8.00	0.34990			
9	15.00	0.35560			
10	30.00	0.36250			



Void Ratio = 1.091 **Compression =** 37.2 %
D_0 = 0.32387 D_{50} = 0.34637 D_{100} = 0.36887
C_v **at 8.2 min.** = 0.03 ft.^{2}/day C_α = 0.005

Southern Earth Sciences, Inc.

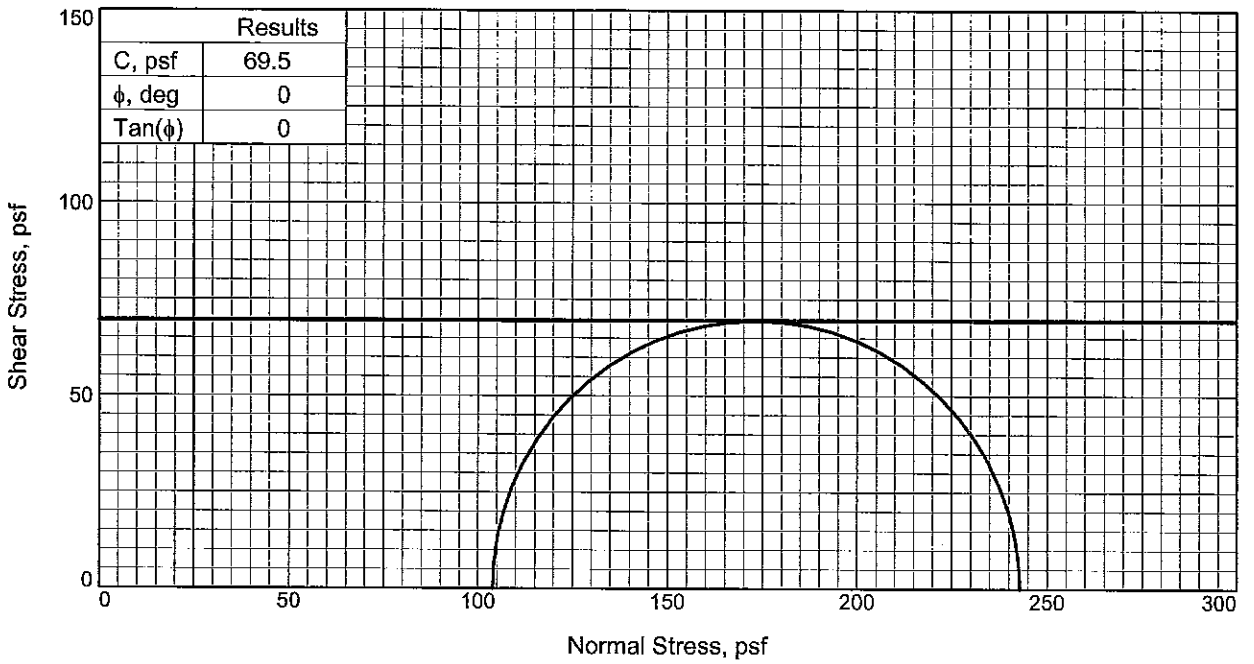
Laboratory Test Results

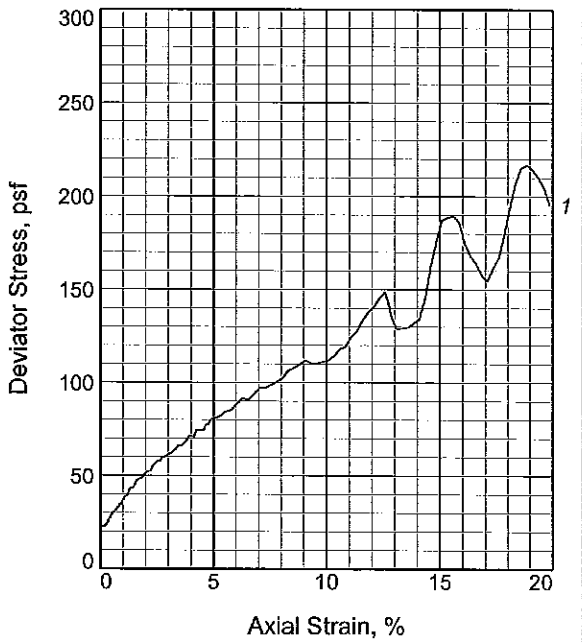
Project: **Bayou DuPont** | **Technical Responsibility:** | **Quality Assurance Officer**

Client: URS

7389 Florida Blvd., Suite 300, Baton Rouge, LA 70806 | Project No.: **B09-012** | PM: S. Aviles | Date of Issue: 3/12/2009

			ASTM DESIGNATION																
			D2216	D4318			D427	D2166		D2166	D2850	D422, C136 or C117					D2974	USCS	
				Atterberg Limits						Cohesion		Grain Size (% Passing)							
Boring No.	Depth (ft)	Classification	ω %	LL	PL	PI	SL	γ_{wet} pcf	γ_{dry} pcf	U psf	UU psf	Gravel	Sand	Silt	Clay	#200	Organic Content %		Confining Stress, Resistivity and Remarks
B-8	0-2	Very Soft PEAT	766.1					65.8	7.6		69.5						40.7	(PT)	Confining Pressure: 0.7 psi
B-8	2-4	Very Soft PEAT with clay pockets	382.5				34.9	71.0	14.7		125.2							(PT)	Confining Pressure: 1.3 psi
B-8	4-6	Very Soft, Gray CLAY with organic pockets	140.3	185	48	137		87.6	36.4		89.7		1.3	17.9	80.8			(CH-OH)	Specific Gravity: 2.80 Confining Pressure: 2.0 psi
B-8	6-8	Very Soft, Gray CLAY with organic pPockets	117.1	96	33	63		95.3	43.9		60.2						2.9	(CH)	Confining Pressure: 2.6 psi
B-8	8-10	Very Loose, Gray SILTY CLAY with clay and organic pockets	129.8	87	51	36		92.9	40.4		53.4		1.9	45.2	52.9			(MH)	Confining Pressure: 3.3 psi
B-8	13-15	Loose, Gray SILT with trace sand and silty clay pockets	50.0	NP	NP	NP		112.3	74.9		816.9		29.4	62.4	8.2			(ML)	Confining Pressure: 5.0 psi
B-8	18-20	Loose, Gray SILT with trace fine sand, trace organics and clay pockets	28.8	NP	NP	NP	20.1	123.0	95.5		976.1					87.5	0.8	(ML)	Confining Pressure: 6.6 psi
B-8	23-25	Very Soft, Gray CLAY with silt and organics	106.7	107	36	71		95.5	46.1		125.8							(CH)	Confining Pressure: 8.2 psi
B-8	28-30	Very Soft, Gray CLAY with silt pockrets Becoming Gray SILT with sandy clay	60.1					102.0	63.7		89.5						2.4	(CH)	Confining Pressure: 9.9 psi
B-8	33-35	Loose, Gray SILT with clay	62.1	34	25	9	21.9	107.3	66.2		402.2		4.4	69.1	26.5			(CL-ML)	Specific Gravity: 2.75 Confining Pressure: 11.5 psi
B-8	38-40	Intermixed Gray CLAY and SILT Trace Sand and Organics	31.9					112.4	85.2		144.9							(CL-ML)	Confining Pressure: 13.2 psi





Sample No.		1
Initial	Water Content, %	762.3
	Dry Density, pcf	7.6
	Saturation, %	98.6
	Void Ratio	17.0104
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	762.3
	Dry Density, pcf	7.6
	Saturation, %	98.6
	Void Ratio	17.0104
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		0.721
Fail. Stress, psf		139.0
Strain, %		12.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		242.9
σ_3 Failure, psf		103.9

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO PEAT

Assumed Specific Gravity= 2.2
Remarks: FAILURE: YEILD

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

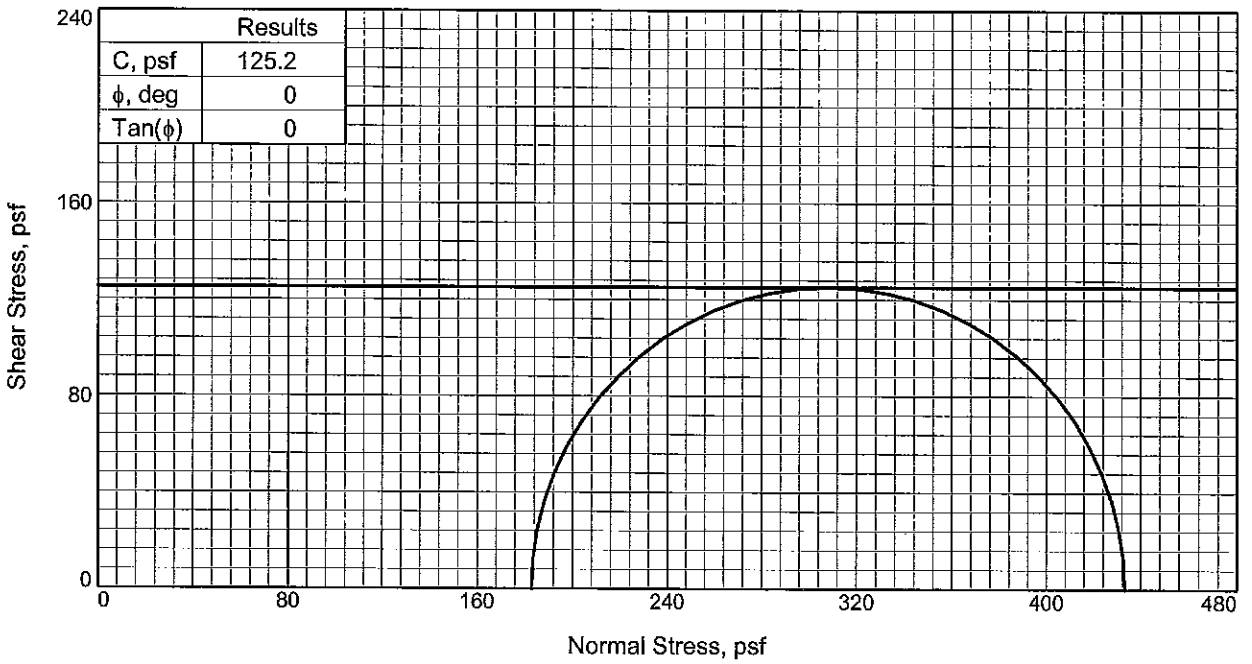
Source of Sample: B-8 **Depth:** 0-2

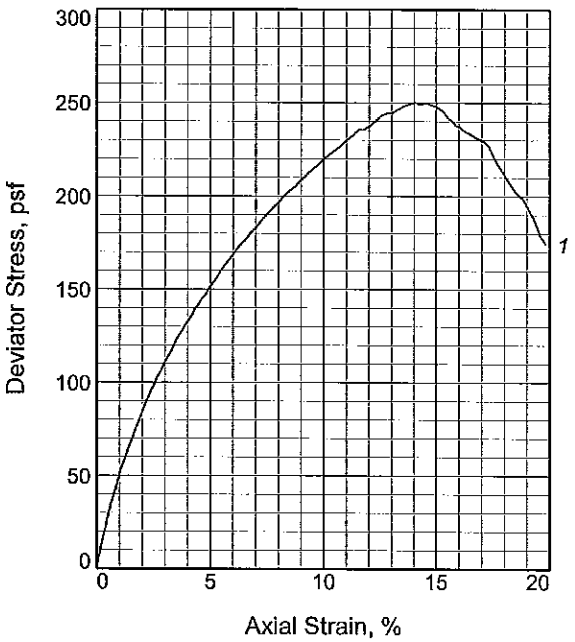
Sample Number: 1

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	382.5
	Dry Density, pcf	14.7
	Saturation, %	101.2
	Void Ratio	8.3129
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	382.5
	Dry Density, pcf	14.7
	Saturation, %	101.2
	Void Ratio	8.3129
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		1.270
Fail. Stress, psf		250.4
Strain, %		14.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		433.2
σ_3 Failure, psf		182.9

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO PEAT W/ CL PKTS

Assumed Specific Gravity= 2.20

Remarks: FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

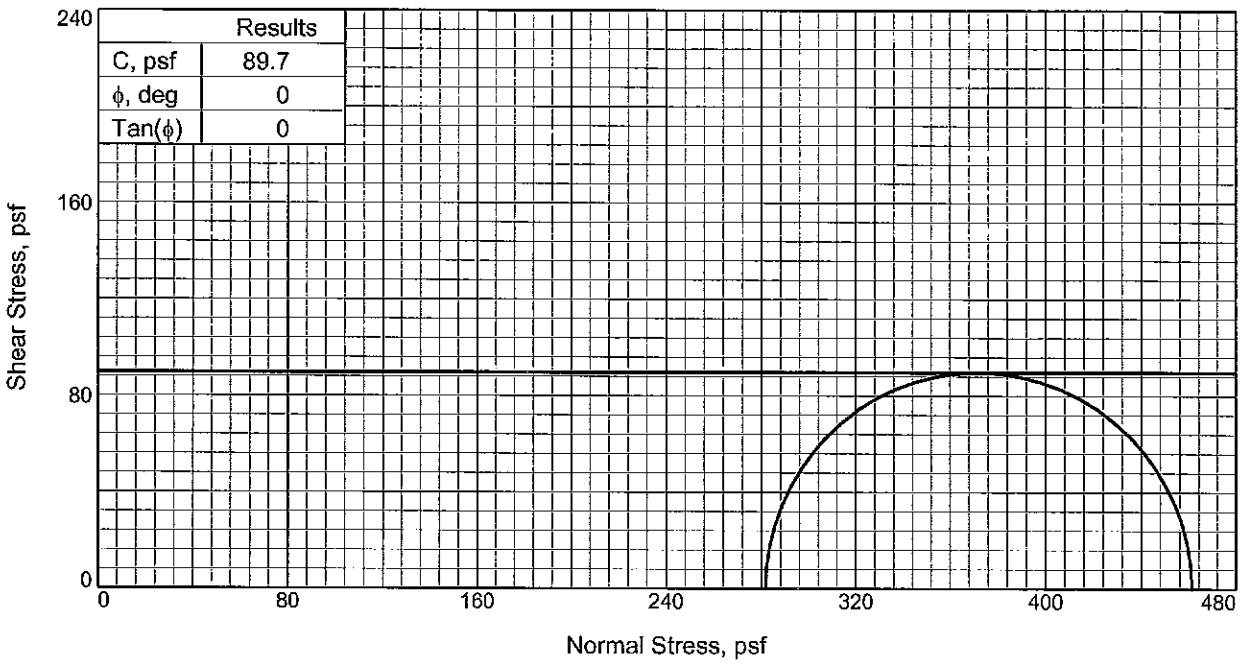
Source of Sample: B-8 **Depth:** 2-4

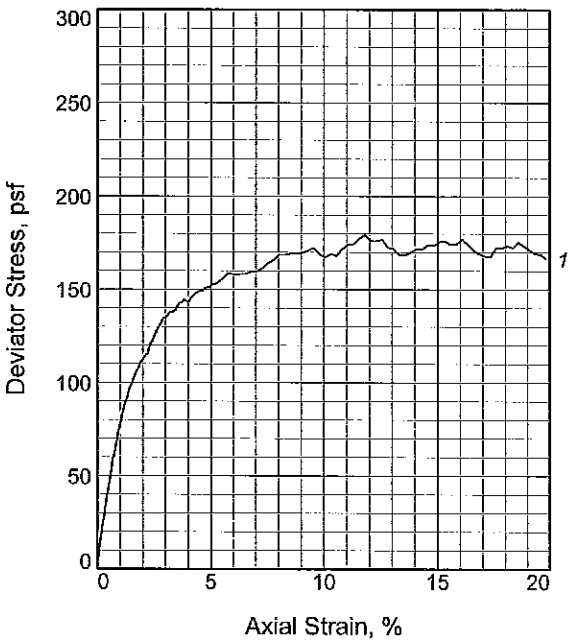
Sample Number: 2

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	140.3
	Dry Density, pcf	36.4
	Saturation, %	103.5
	Void Ratio	3.7957
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	140.3
	Dry Density, pcf	36.4
	Saturation, %	103.5
	Void Ratio	3.7957
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		1.956
Fail. Stress, psf		179.5
Strain, %		11.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		461.2
σ_3 Failure, psf		281.7

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO G CL W/ ORGPKTS

LL= 185 **PL=** 48 **PI=** 137
Specific Gravity= 2.80
Remarks: FAILURE: BULGE

ASTM D 2850

Client: URS

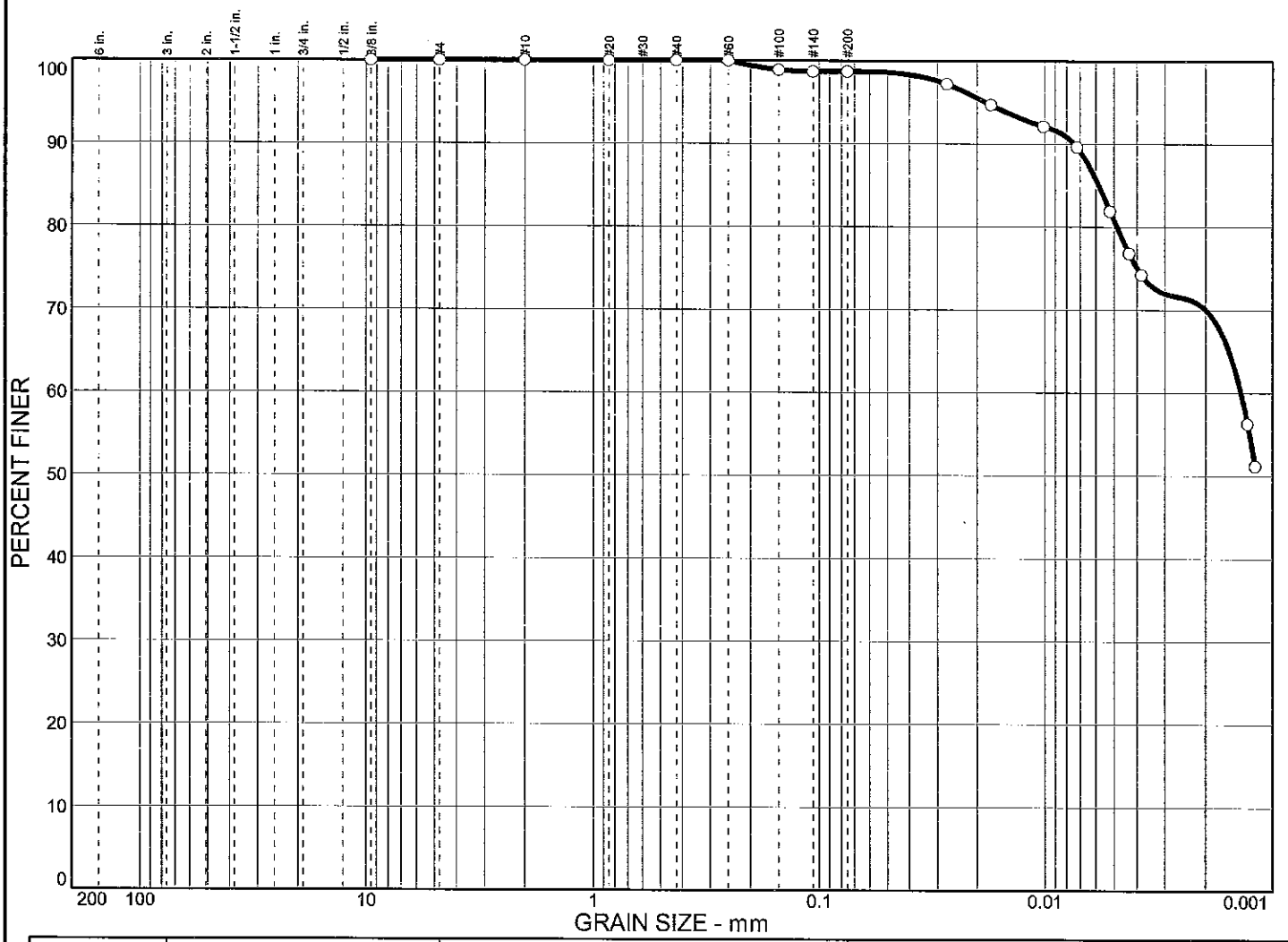
Project: BAYOU DUPONT

Source of Sample: B-8 **Depth:** 4-6
Sample Number: 3
Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	1.3	17.9	80.8

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	185	48	0.0058	0.0014						

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ ORGPKTS		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

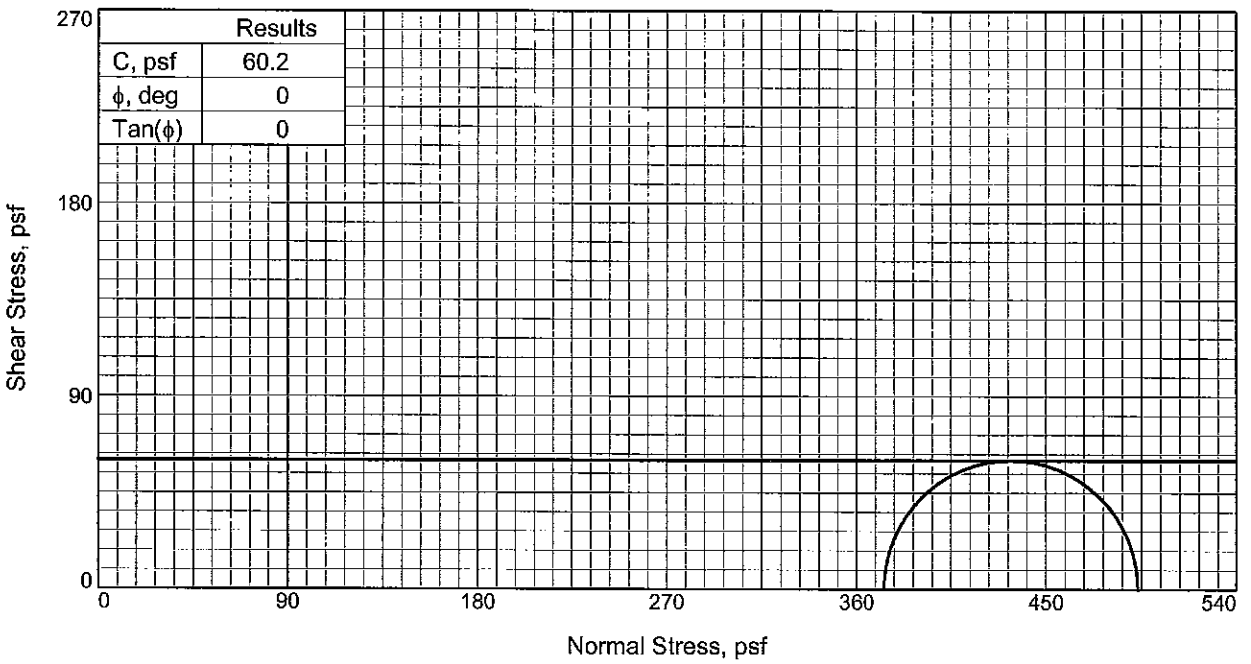
○ **Source:** B-8 **Sample No.:** 3 **Elev./Depth:** 4-6

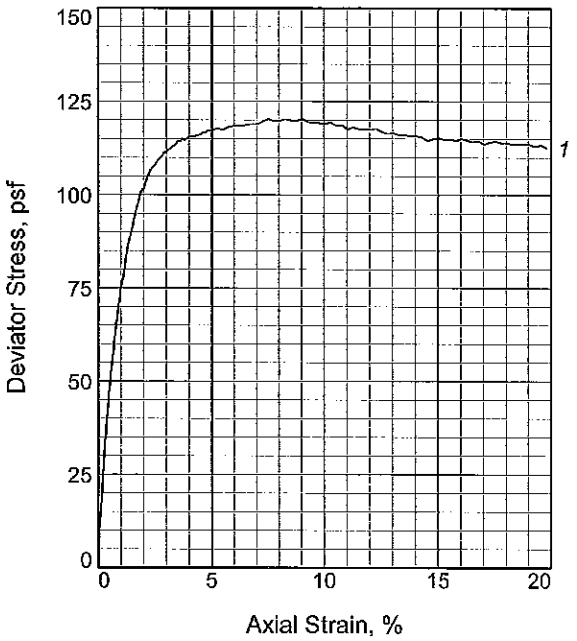
Remarks:

○ F.M.=0.01

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	117.1
	Dry Density, pcf	43.9
	Saturation, %	110.0
	Void Ratio	2.9821
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	117.1
	Dry Density, pcf	43.9
	Saturation, %	110.0
	Void Ratio	2.9821
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.590
Fail. Stress, psf		120.4
Strain, %		7.5
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		493.4
σ_3 Failure, psf		373.0

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO G CL W/ ORGPKTS

LL= 96 **PL=** 33 **PI=** 63
Assumed Specific Gravity= 2.802
Remarks: FAILURE: BULGE

ASTM D 2850

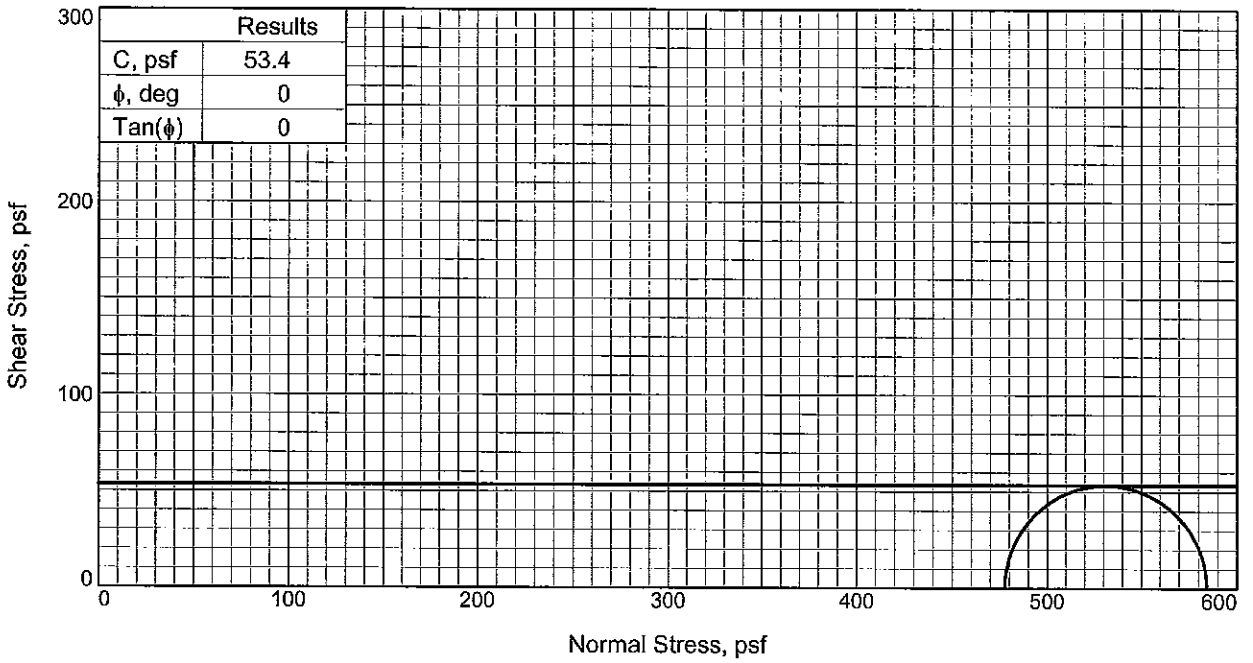
Client: URS

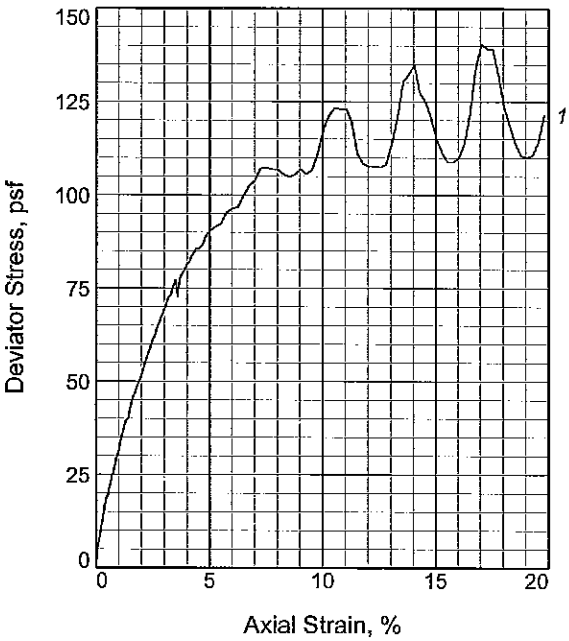
Project: BAYOU DUPONT

Source of Sample: B-8 **Depth:** 6-8
Sample Number: 4
Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	129.8
	Dry Density, pcf	40.4
	Saturation, %	109.3
	Void Ratio	3.3248
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	129.8
	Dry Density, pcf	40.4
	Saturation, %	109.3
	Void Ratio	3.3248
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		3.317
Fail. Stress, psf		106.9
Strain, %		8.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		584.5
σ_3 Failure, psf		477.6

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VLO G SICL W/ CLPKTS & ORGPKTS

LL= 96 **PL=** 60 **PI=** 36

Assumed Specific Gravity= 2.80

Remarks: FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-8 **Depth:** 8-10

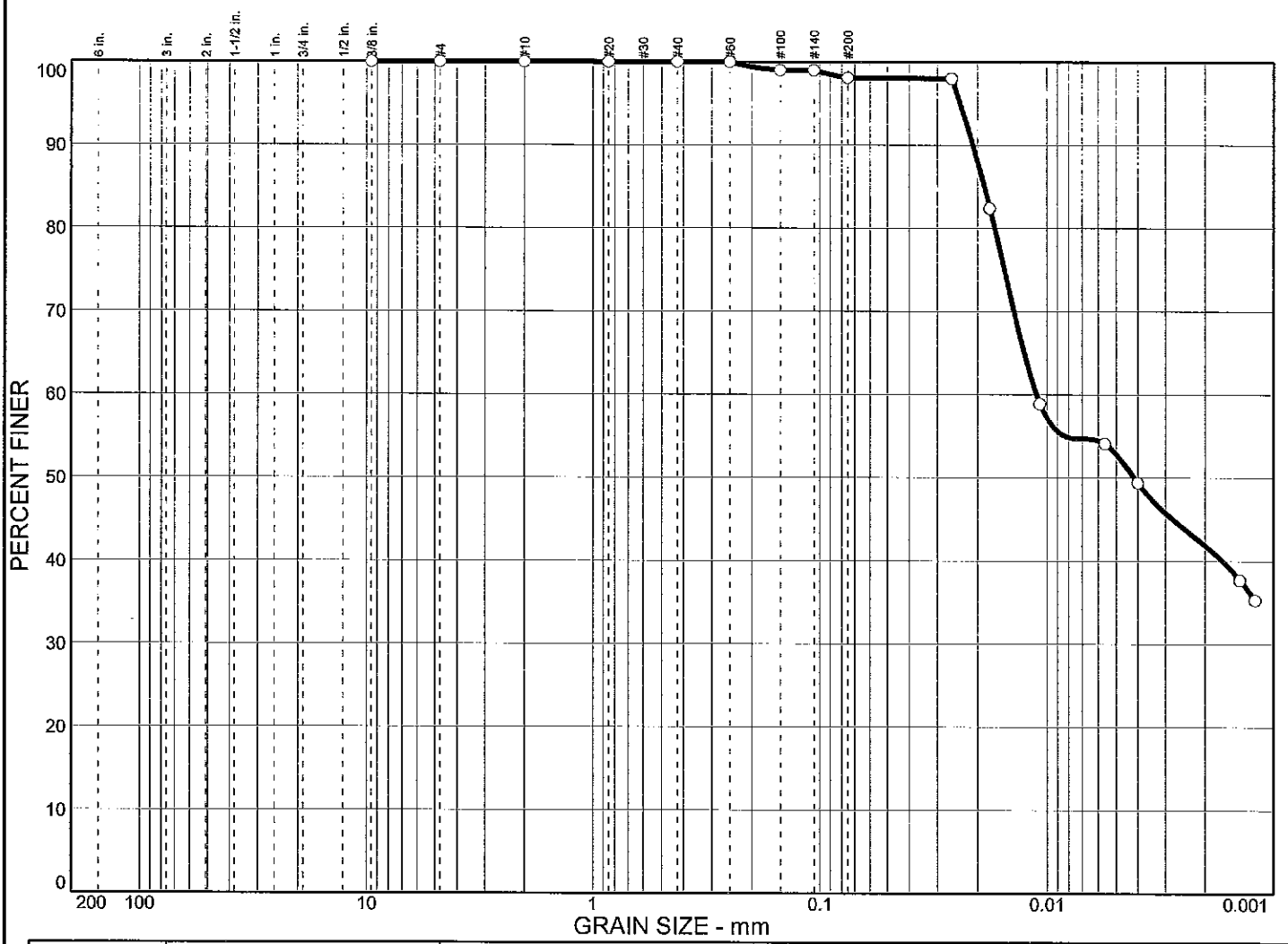
Sample Number: 5

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	1.9	45.2	52.9

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	96	51	0.0187	0.0111	0.0042					

MATERIAL DESCRIPTION	USCS	AASHTO
○ VLO G SICL W/ CLPKTS & ORGPKTS		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-8 **Sample No.:** 5 **Elev./Depth:** 8-10

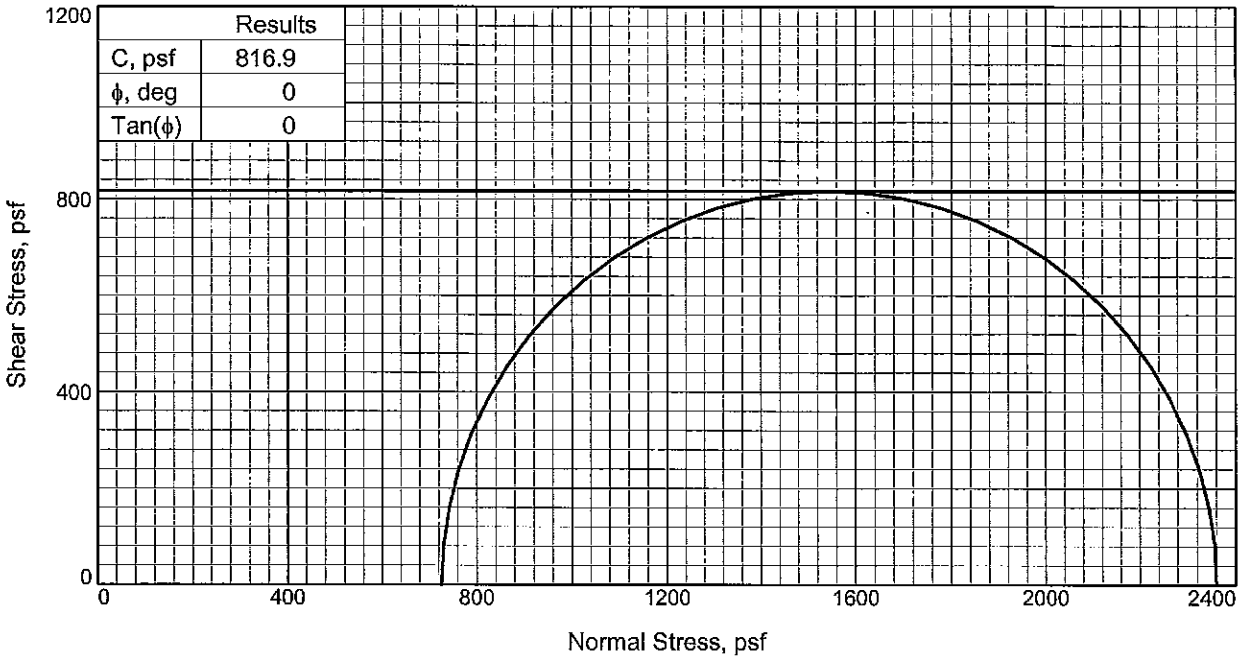
Remarks:

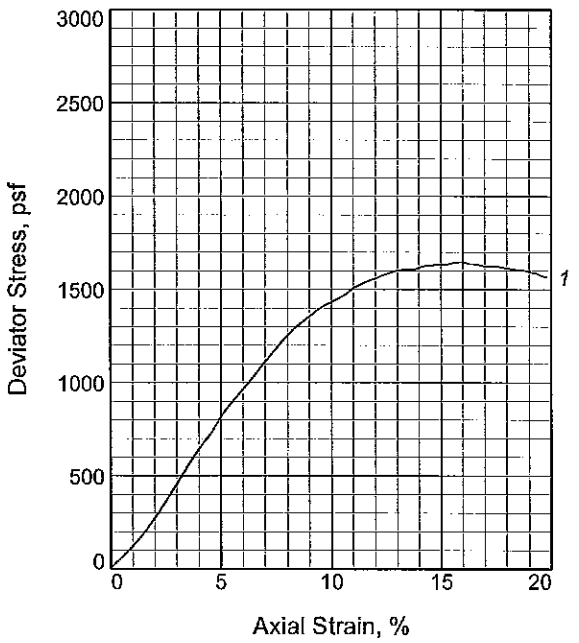
○ ASTM D422, C136

F.M.=0.01

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	50.0
	Dry Density, pcf	74.9
	Saturation, %	109.5
	Void Ratio	1.2088
	Diameter, in.	2.950
	Height, in.	5.940
At Test	Water Content, %	50.0
	Dry Density, pcf	74.9
	Saturation, %	109.5
	Void Ratio	1.2088
	Diameter, in.	2.950
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		5.045
Fail. Stress, psf		1633.8
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2360.3
σ_3 Failure, psf		726.5

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: LO G SI W/ TRSA & SICLPKTS

LL= NP **PI=** NP
Assumed Specific Gravity= 2.65
Remarks: FAILURE: BULGE
SLUMPING UNDER OWN WT.

ASTM D 2850

Client: URS

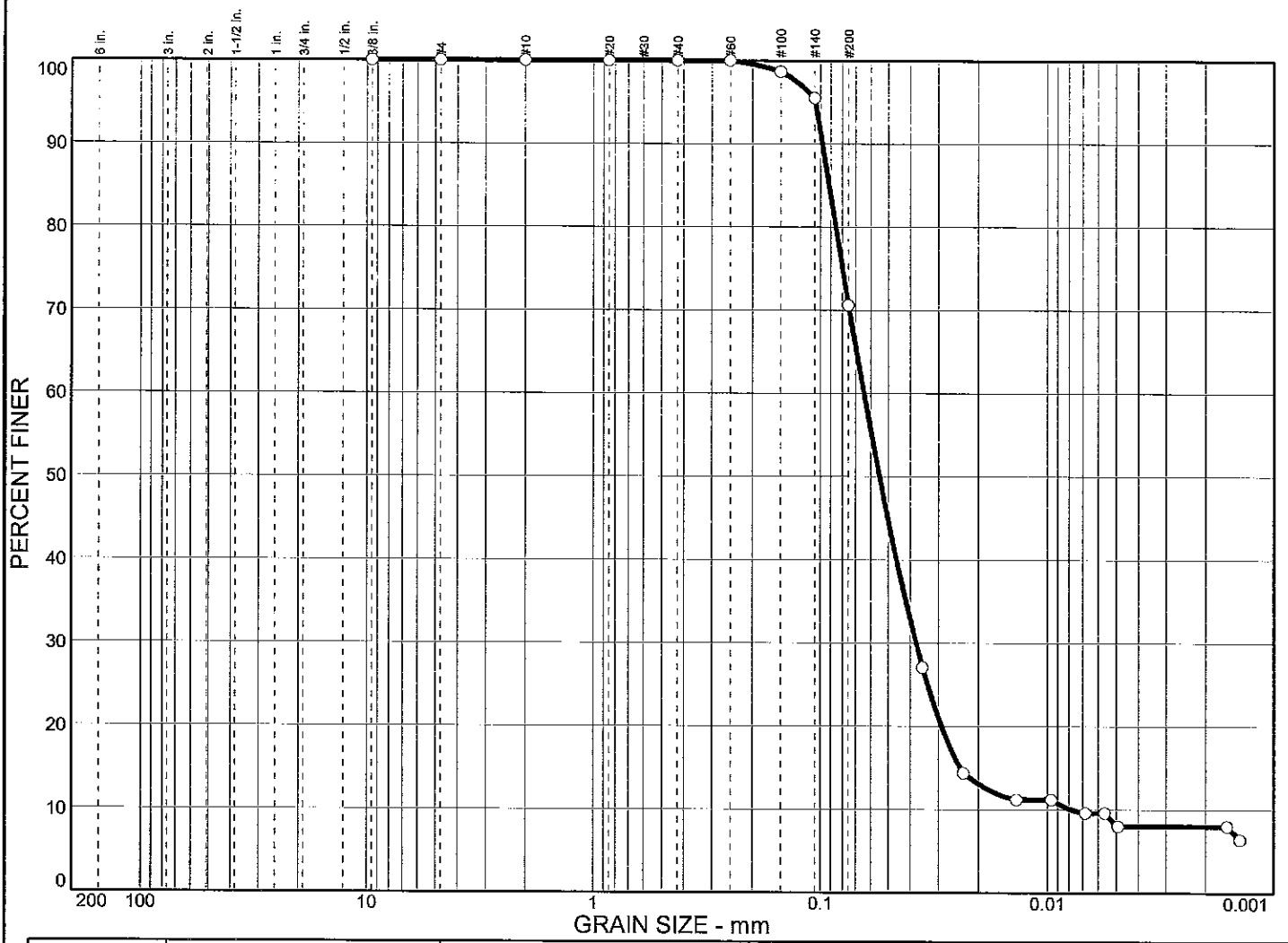
Project: BAYOU DUPONT

Source of Sample: B-8 **Depth:** 13-15
Sample Number: 6
Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	29.4	62.4	8.2

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	NP	NP	0.0917	0.0642	0.0548	0.0376	0.0240	0.0078	2.82	8.21

MATERIAL DESCRIPTION	USCS	AASHTO
○ LO G SI W/ TRSA & SICLPKTS		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-8 **Sample No.:** 6 **Elev./Depth:** 13-15

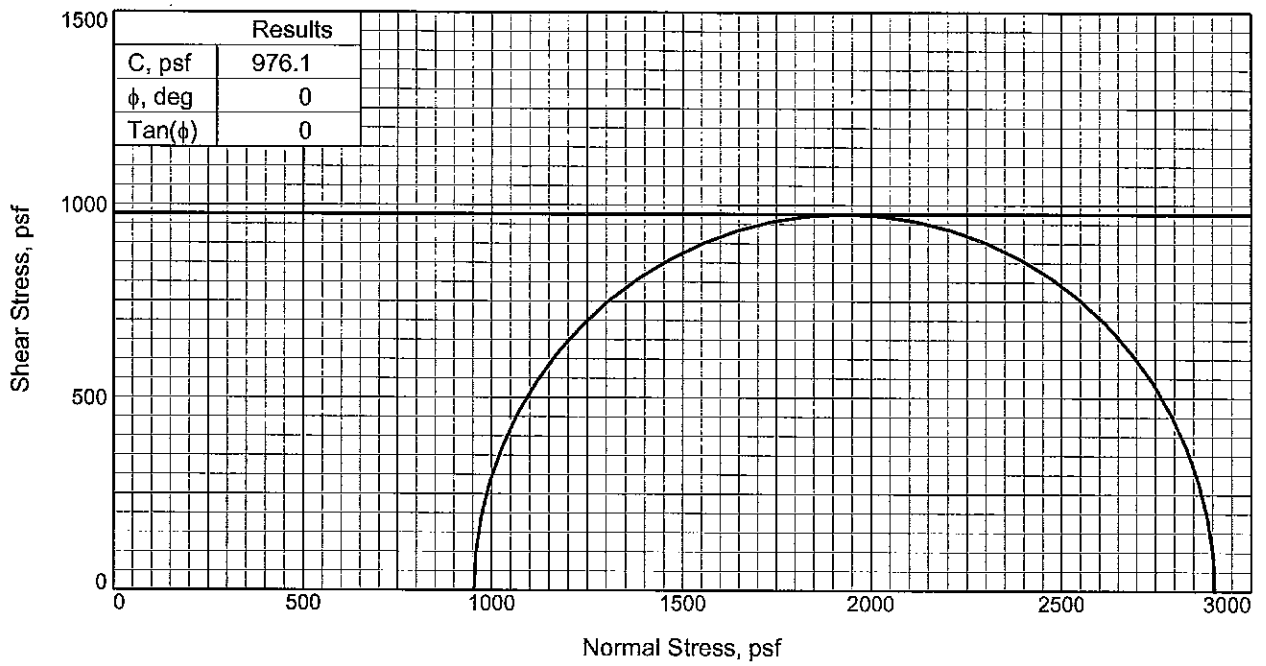
Remarks:

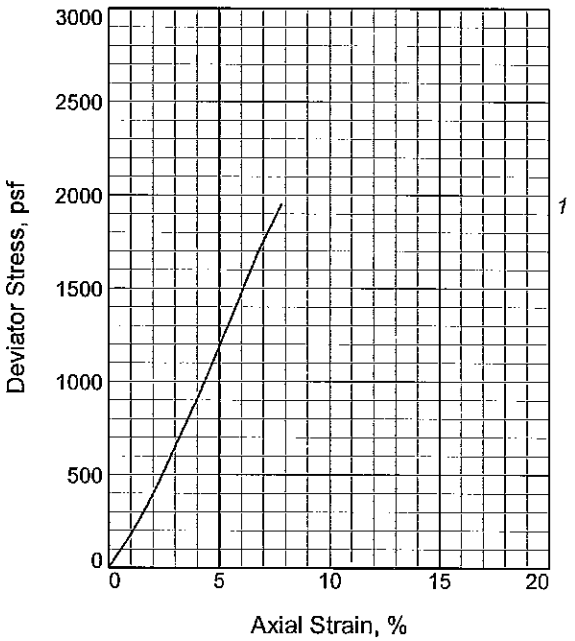
○ ASTM D422, C136

F.M.=0.01

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	28.8
	Dry Density, pcf	95.5
	Saturation, %	104.1
	Void Ratio	0.7324
	Diameter, in.	2.850
	Height, in.	4.191
At Test	Water Content, %	28.8
	Dry Density, pcf	95.5
	Saturation, %	104.1
	Void Ratio	0.7324
	Diameter, in.	2.850
	Height, in.	4.191
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		6.624
Fail. Stress, psf		1952.1
Strain, %		7.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2906.0
σ_3 Failure, psf		953.9

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: LO G SI W/ CLPKTS, TRORGS & TRFSA

PI= NP

Assumed Specific Gravity= 2.65

Remarks: FAILURE: YIELD

Client: URS

Project: BAYOU DUPONT

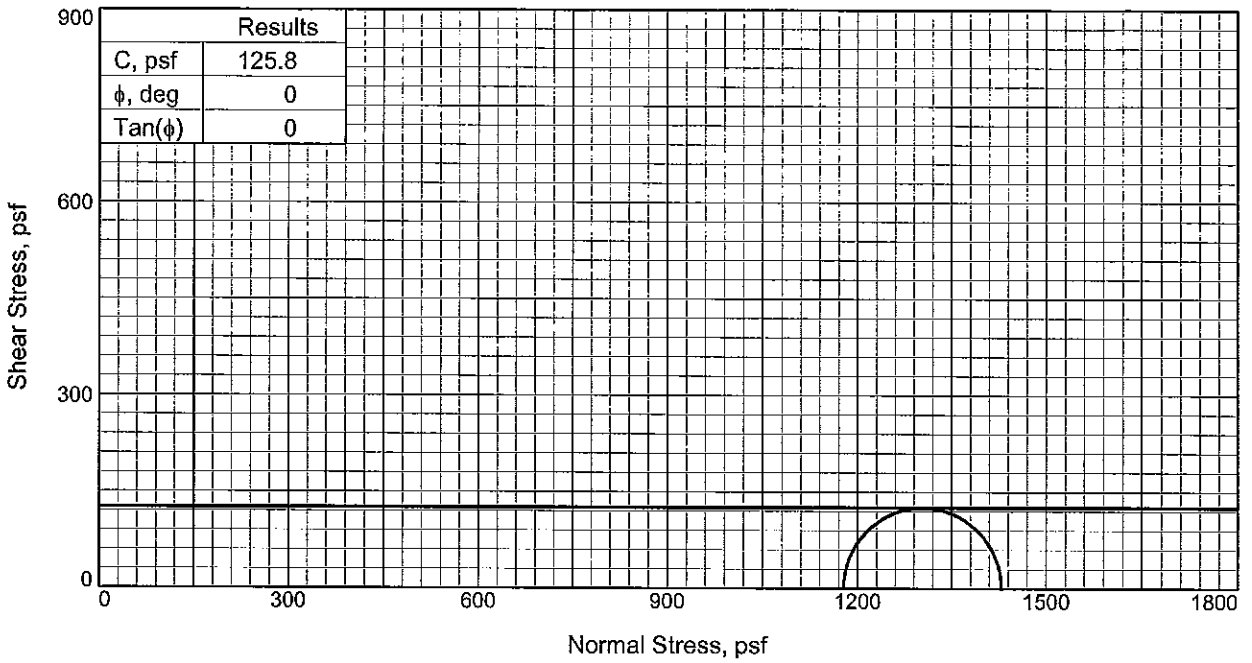
Source of Sample: B-8 **Depth:** 18-20

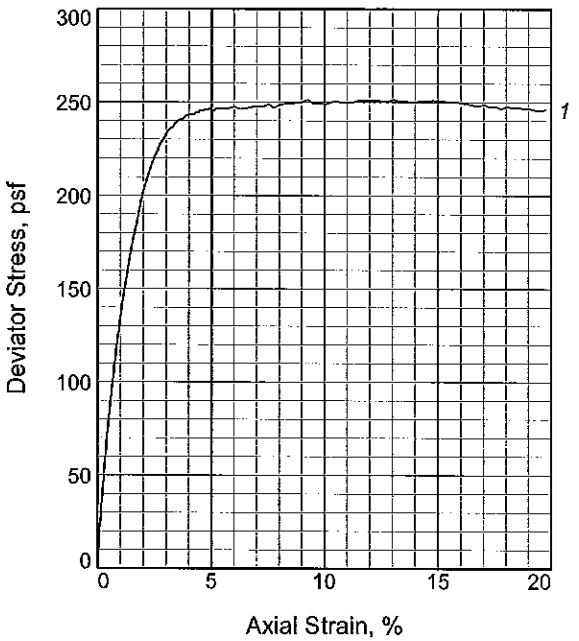
Sample Number: 7

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	106.7
	Dry Density, pcf	46.1
	Saturation, %	107.1
	Void Ratio	2.7901
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	106.7
	Dry Density, pcf	46.1
	Saturation, %	107.1
	Void Ratio	2.7901
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		8.178
Fail. Stress, psf		251.6
Strain, %		13.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1429.3
σ_3 Failure, psf		1177.6

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO G CL W/ SI& ORGS

LL= 107 **PL=** 36 **PI=** 71
Assumed Specific Gravity= 2.80
Remarks: FAILURE: BULGE

ASTM D 2850

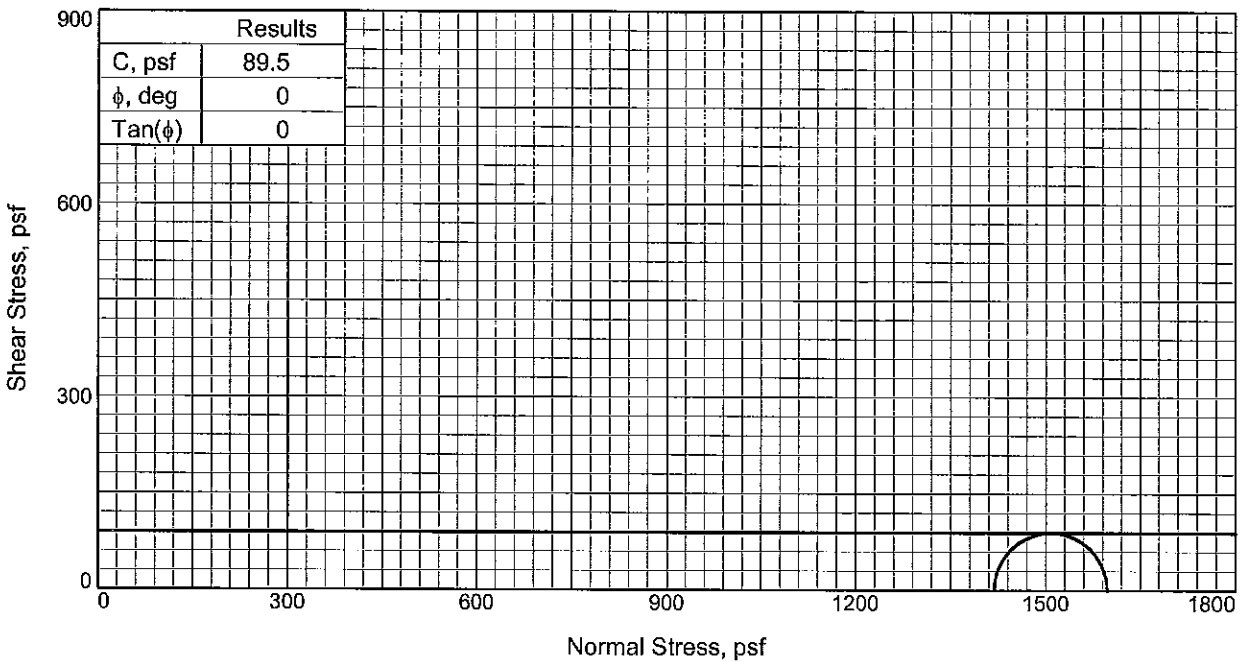
Client: URS

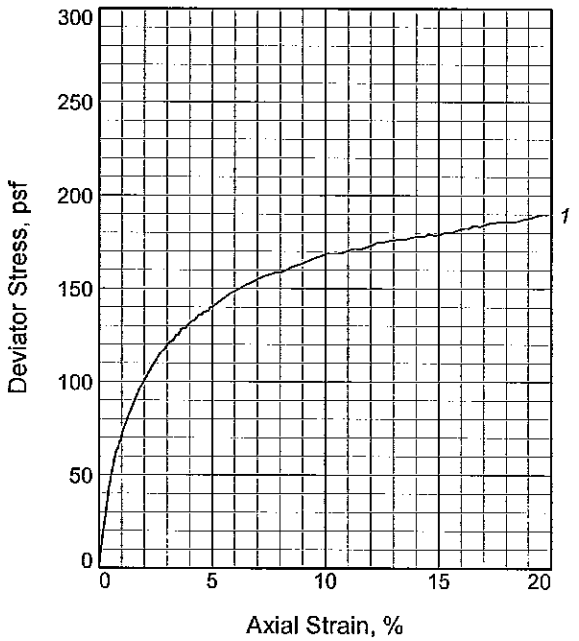
Project: BAYOU DUPONT

Source of Sample: B-8 **Depth:** 23-25
Sample Number: 8
Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	60.1
	Dry Density, pcf	63.7
	Saturation, %	98.7
	Void Ratio	1.6446
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	60.1
	Dry Density, pcf	63.7
	Saturation, %	98.7
	Void Ratio	1.6446
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		9.853
Fail. Stress, psf		179.0
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1597.8
σ_3 Failure, psf		1418.8

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ SIPKTS BEC G SI W/ CL

Assumed Specific Gravity= 2.70

Remarks: FAILURE: BULGE

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

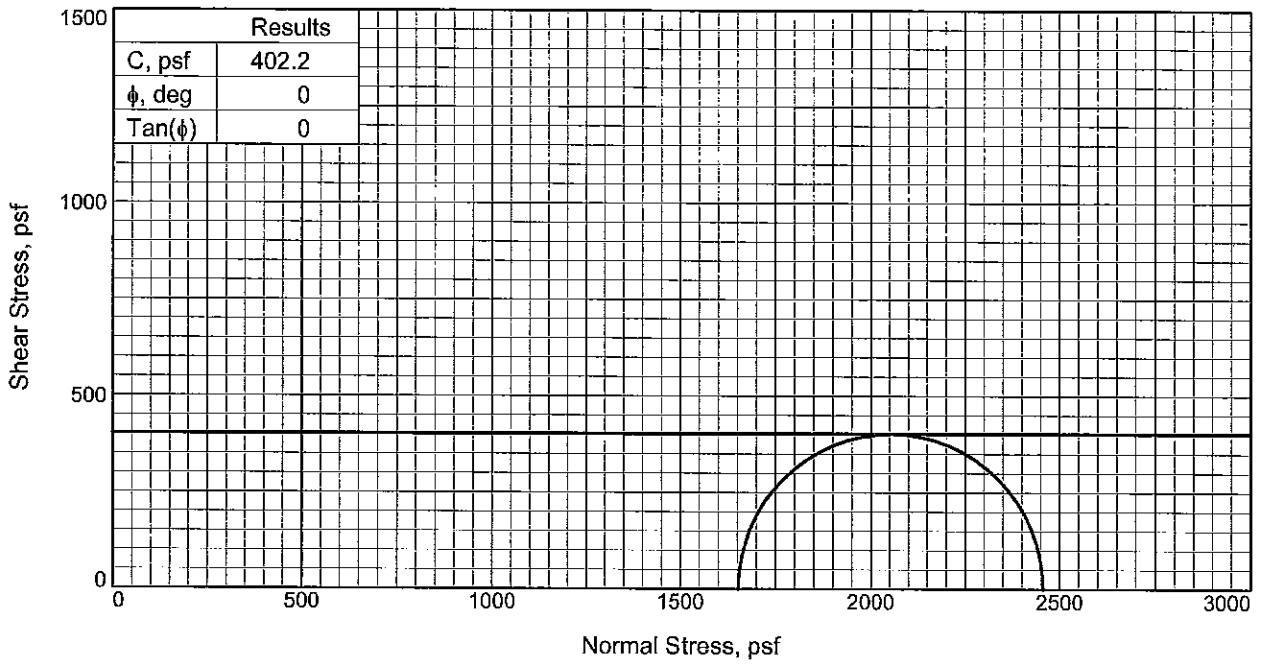
Source of Sample: B-8 **Depth:** 28-30

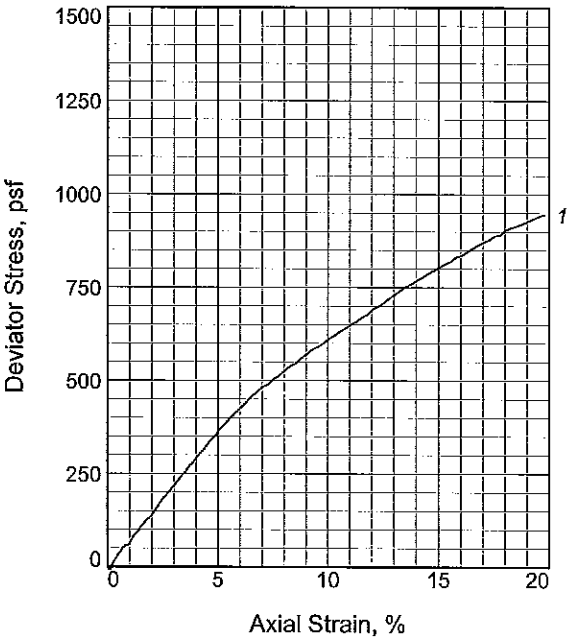
Sample Number: 9

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	62.1
	Dry Density, pcf	66.2
	Saturation, %	107.2
	Void Ratio	1.5916
	Diameter, in.	1.440
	Height, in.	2.800
At Test	Water Content, %	62.1
	Dry Density, pcf	66.2
	Saturation, %	107.2
	Void Ratio	1.5916
	Diameter, in.	1.440
	Height, in.	2.800
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		11.474
Fail. Stress, psf		804.4
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2456.7
σ_3 Failure, psf		1652.3

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: LO G SI W/ CL

LL= 34 **PL=** 25 **PI=** 9
Specific Gravity= 2.75
Remarks: FAILURE: BULGE

ASTM D 2850

Client: URS

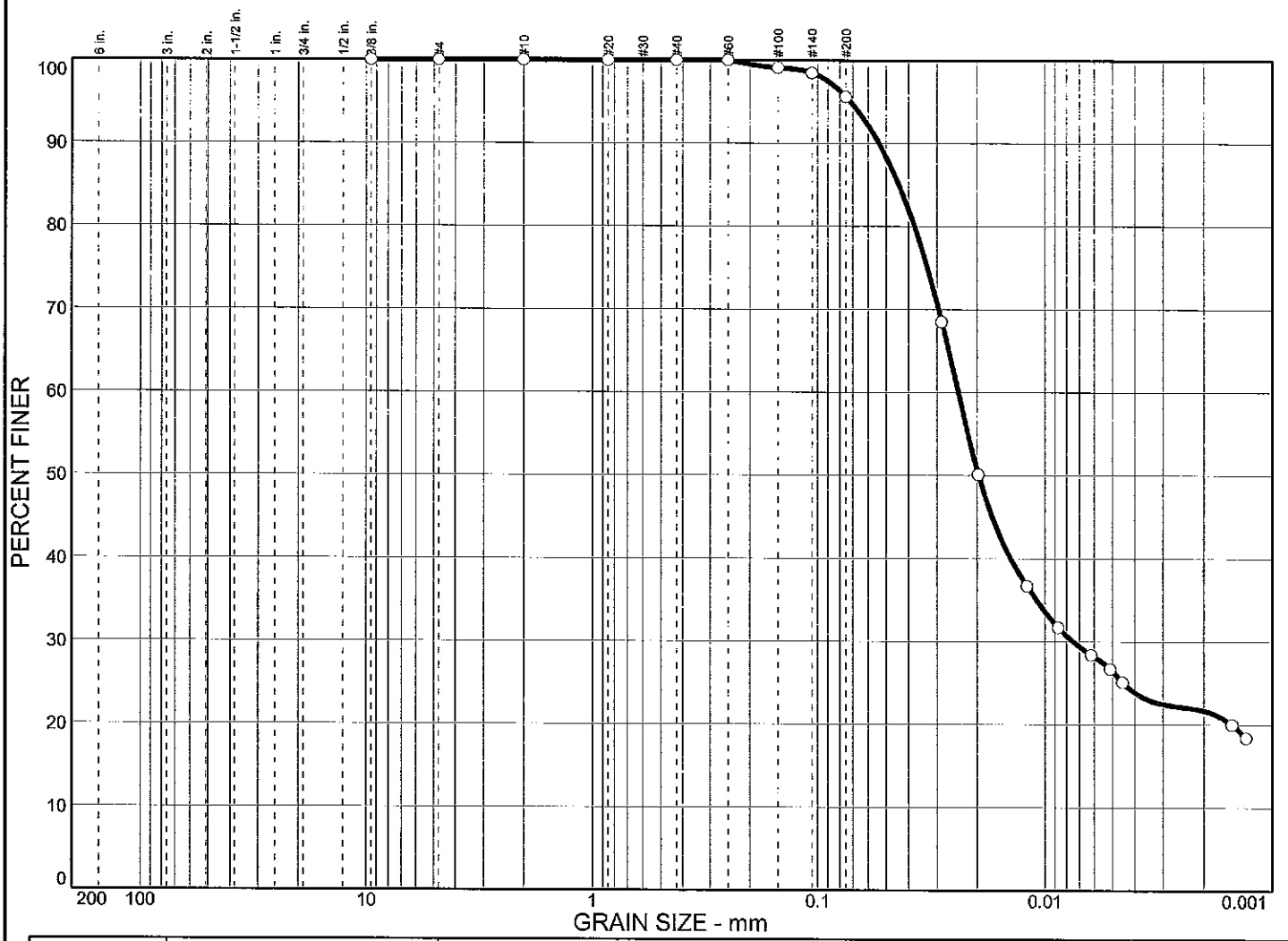
Project: BAYOU DUPONT

Source of Sample: B-8 **Depth:** 33-35
Sample Number: 10
Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	4.4	69.1	26.5

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	34	25	0.0441	0.0242	0.0197	0.0075				

MATERIAL DESCRIPTION	USCS	AASHTO
○ LO G SI W/ CL	MP	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-8 **Sample No.:** 10 **Elev./Depth:** 33-35

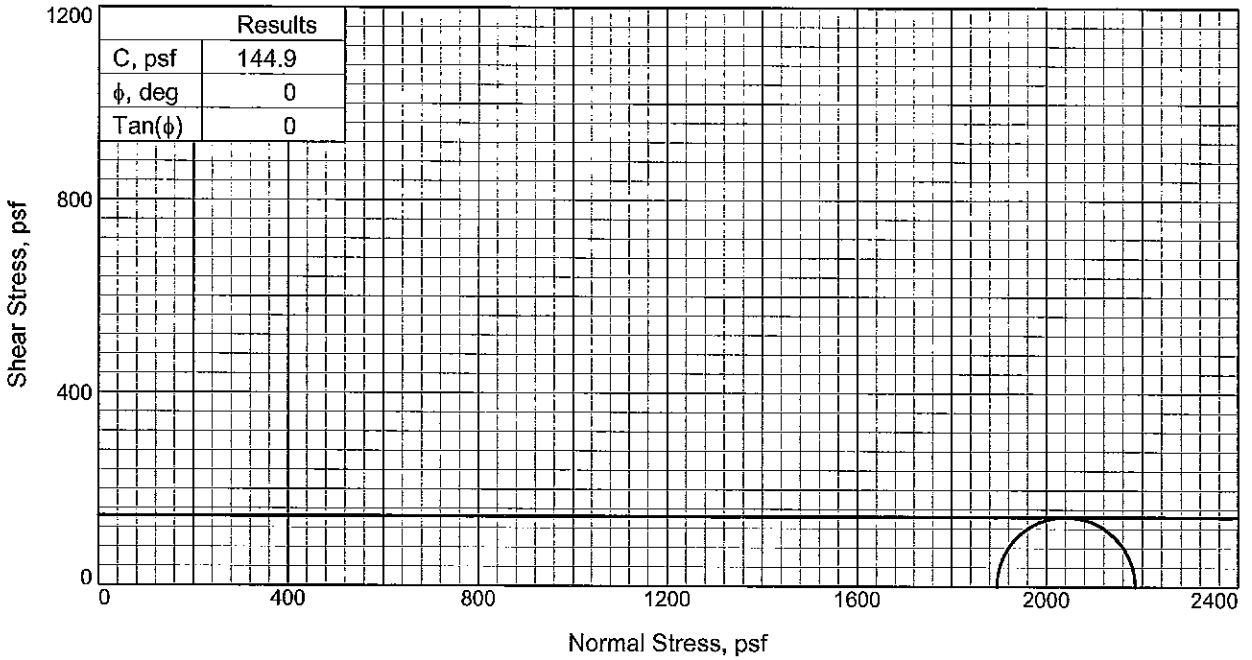
Remarks:

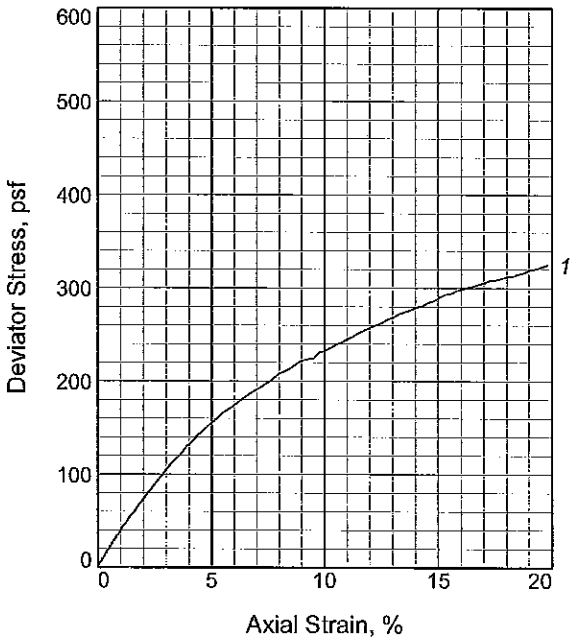
○ ASTM D422, C136

F.M.=0.01

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	31.9
	Dry Density, pcf	85.3
	Saturation, %	88.0
	Void Ratio	0.9772
	Diameter, in.	2.900
	Height, in.	5.608
At Test	Water Content, %	31.9
	Dry Density, pcf	85.3
	Saturation, %	88.0
	Void Ratio	0.9772
	Diameter, in.	2.900
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		13.165
Fail. Stress, psf		289.8
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2185.5
σ_3 Failure, psf		1895.8

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: INT MX G CL & SI W/ TRSA & ORGS

Assumed Specific Gravity= 2.70

Remarks: FAILURE: BULGE SLUMPING UNDER OWN WT.

ASTM D 2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-8 **Depth:** 38-40

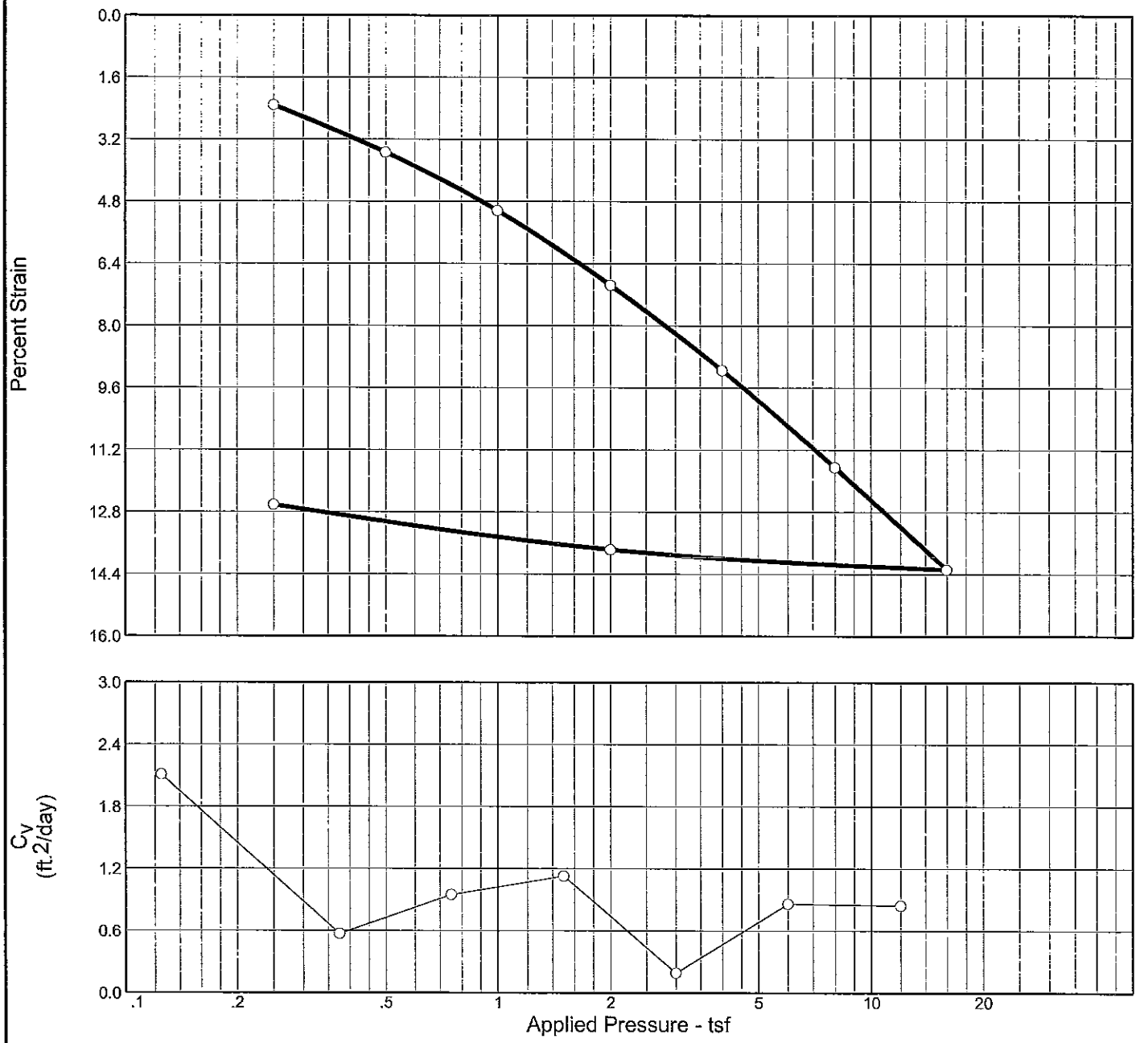
Sample Number: 11

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
95.3 %	31.5 %	89.1			2.70	(CH)		0.891

MATERIAL DESCRIPTION

VSO G CL W/ SIPKTS BEC G SI W/ CL

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

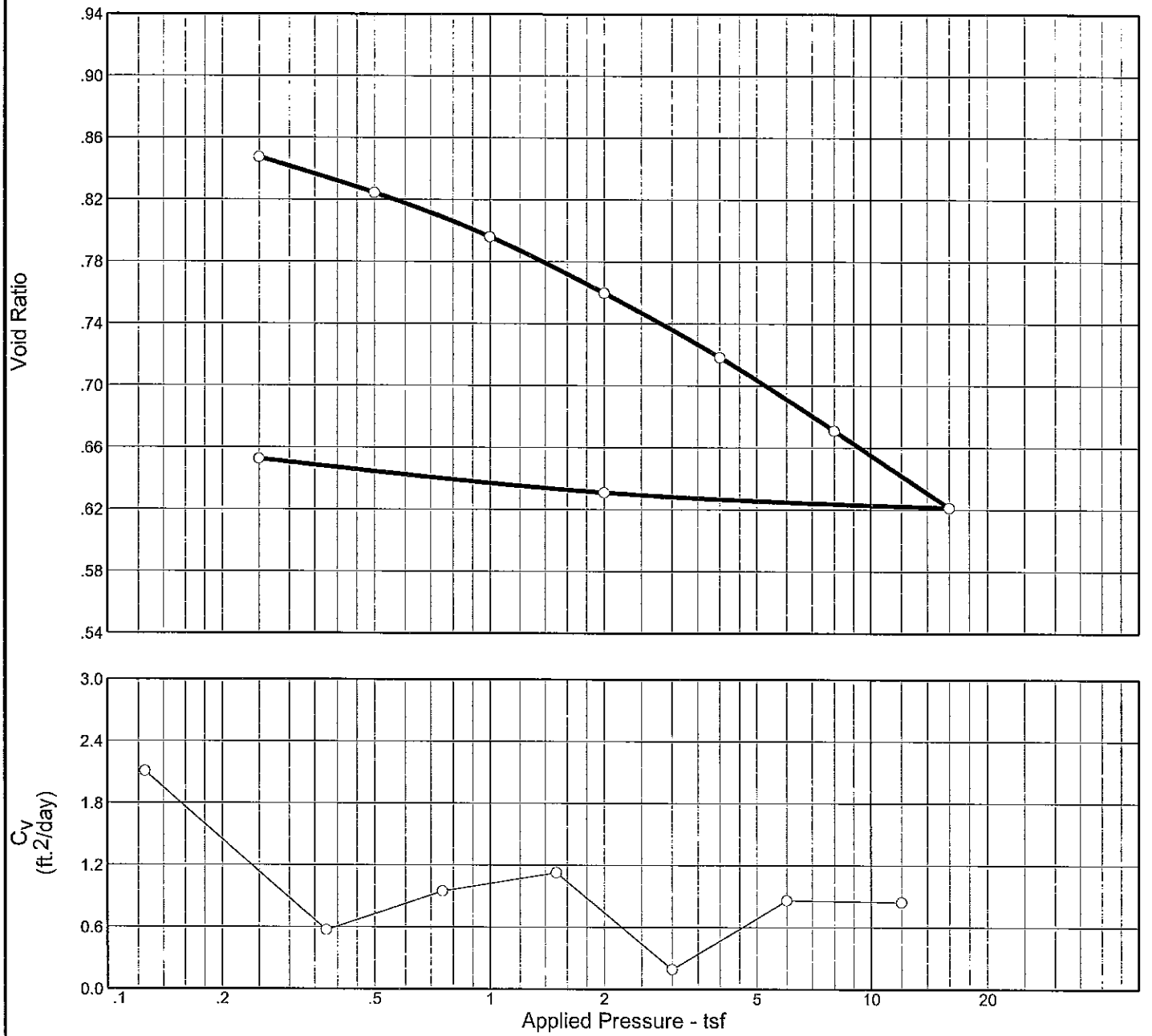
Source: B-8 **Sample No.:** 9 **Elev./Depth:** 28-30

CONSOLIDATION/SWELL TEST REPORT

Remarks:
ASTM D2435

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
95.3 %	31.5 %	89.1			2.70	(CH)		0.891

MATERIAL DESCRIPTION

VSO G CL W/ SIPKTS BEC G SI W/ CL

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-8 **Sample No.:** 9 **Elev./Depth:** 28-30

CONSOLIDATION/SWELL TEST REPORT

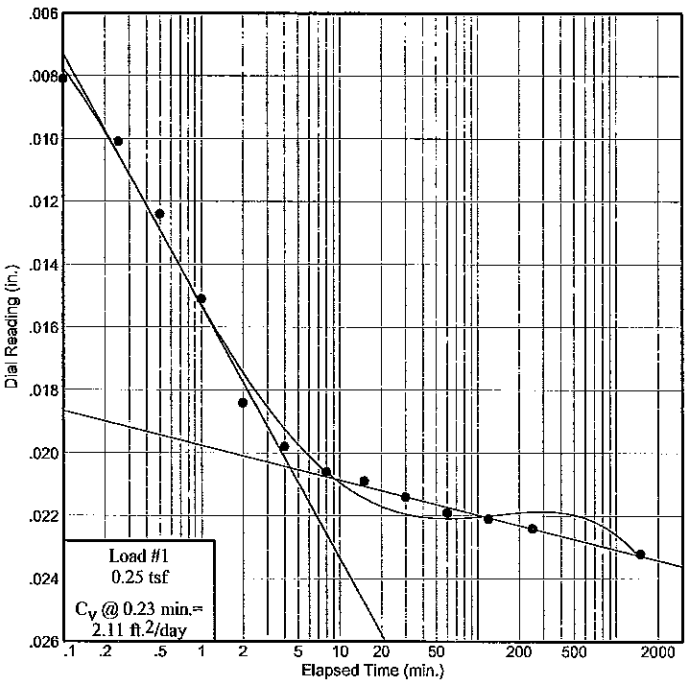
Remarks:
ASTM D2435

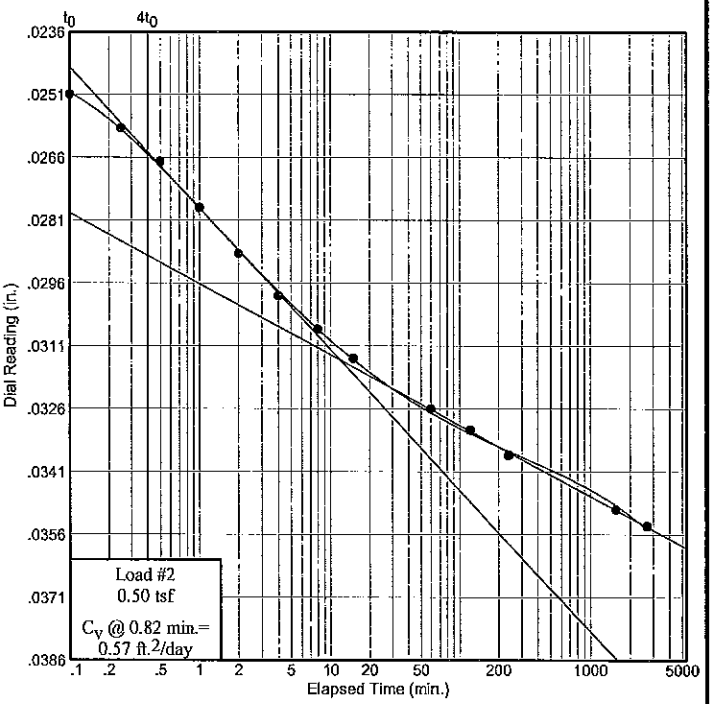
Southern Earth Sciences, Inc.

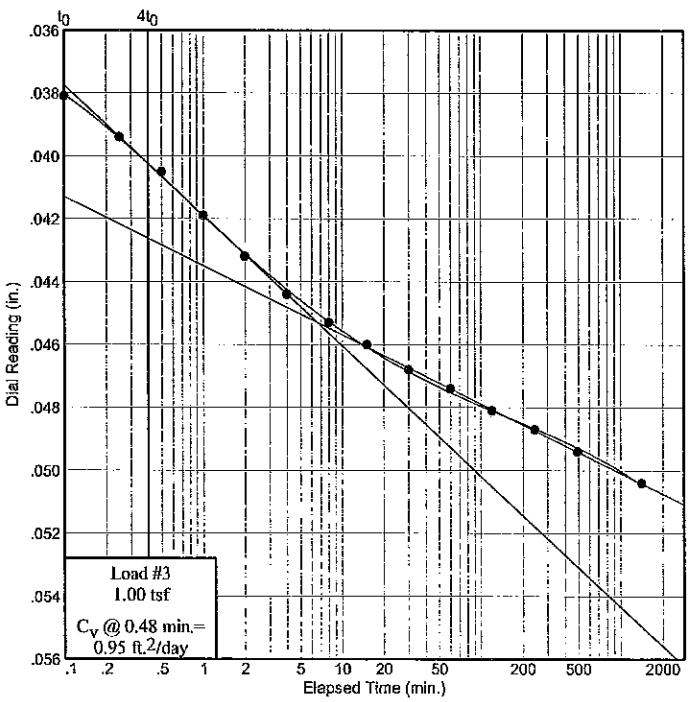
Dial Reading vs. Time

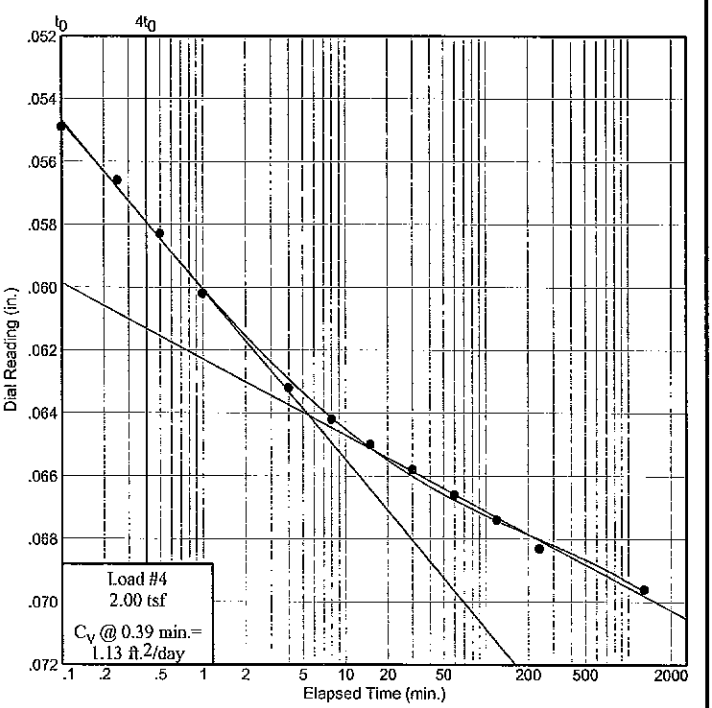
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-8 Sample No.: 9 Elev./Depth: 28-30









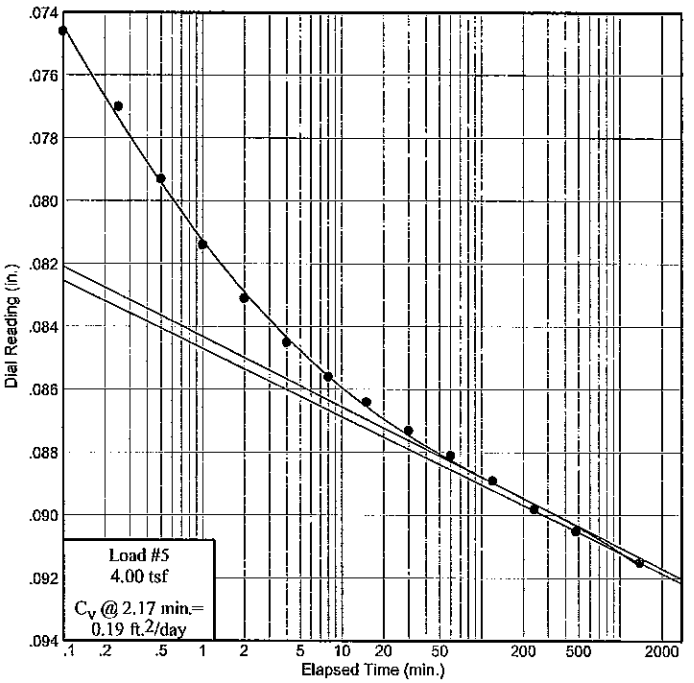
Dial Reading vs. Time

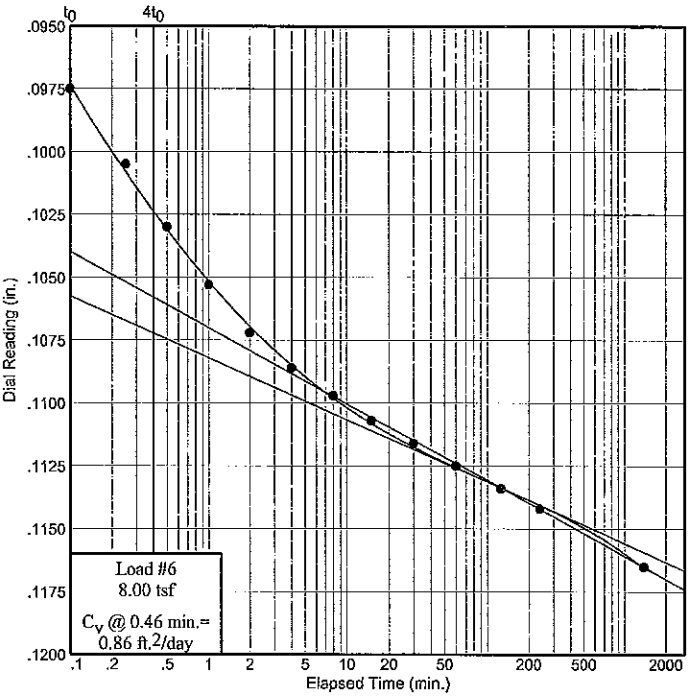
Southern Earth Sciences, Inc.

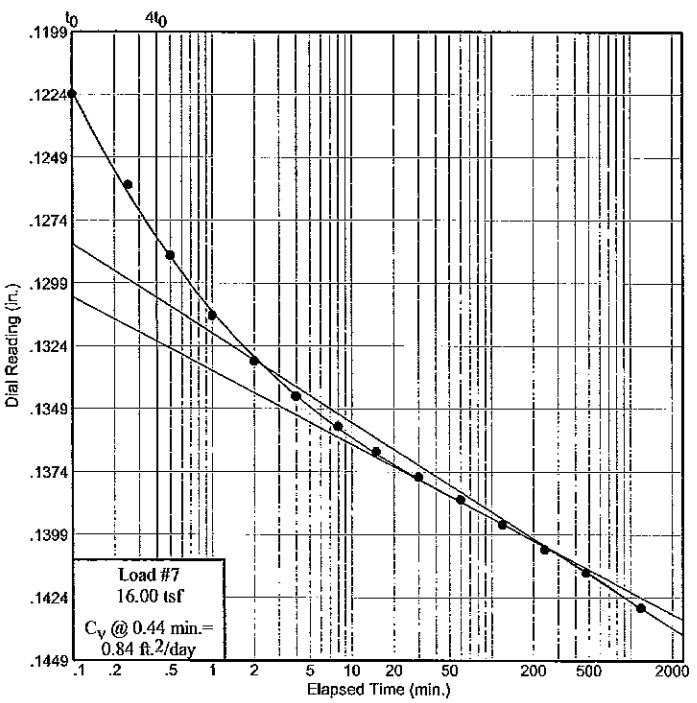
Dial Reading vs. Time

Project No.: B09-012
Project: BAYOU DUPONT

Source: B-8 Sample No.: 9 Elev./Depth: 28-30







Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-8
Sample No.: 9
Elev. or Depth: 28-30 **Sample Length(in./cm.):**
Location:
Description: VSO G CL W/ SIPKTS BEC G SI W/ CL
Liquid Limit: **Plasticity Index:**
USCS: (CH) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST		AFTER TEST	
Wet w+t	= 128.60 g.	Consolidometer #	= 1	Wet w+t	= 143.44 g.
Dry w+t	= 106.85 g.			Dry w+t	= 114.83 g.
Tare Wt.	= 37.71 g.	Spec. Gravity	= 2.70	Tare Wt.	= .00 g.
Height	= 1.00 in.	Height	= 1.00 in.		
Diameter	= 2.50 in.	Diameter	= 2.50 in.		
Weight	= 150.96 g.	Defl. Table	= Unit No. 183 Old 2.5in		
Moisture	= 31.5 %	Ht. Solids	= 0.5287 in.	Moisture	= 24.9 %
Wet Den.	= 117.2 pcf	Dry Wt.	= 114.84 g.*	Dry Wt.	= 114.83 g.
Dry Den.	= 89.1 pcf	Void Ratio	= 0.891	Void Ratio	= 0.653
		Saturation	= 95.3 %		

*** Initial dry weight used in calculations**

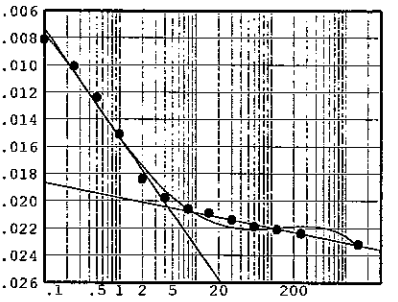
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				0.891	
0.25	0.02360	0.00040	2.11	0.001	0.847	2.3 Comprs.
0.50	0.03610	0.00070	0.57	0.002	0.824	3.5 Comprs.
1.00	0.05170	0.00130	0.95	0.002	0.796	5.0 Comprs.
2.00	0.07170	0.00210	1.13	0.003	0.760	7.0 Comprs.
4.00	0.09470	0.00320	0.19	0.002	0.718	9.1 Comprs.
8.00	0.12100	0.00450	0.86	0.003	0.671	11.6 Comprs.
16.00	0.14940	0.00660	0.84	0.004	0.621	14.3 Comprs.
2.00	0.14020	0.00250			0.631	13.8 Comprs.
0.25	0.12740	0.00120			0.653	12.6 Comprs.

C_c = 0.17 P_c = 1.66 tsf

Pressure: 0.25 tsf — **TEST READINGS** — **Load No. 1**

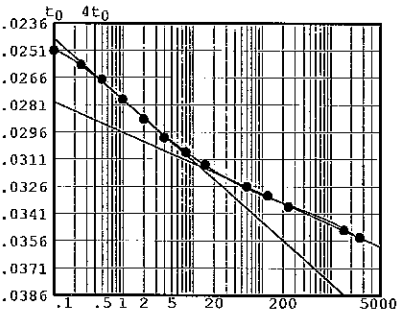
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	60.00	0.02230
2	0.10	0.00850	12	120.00	0.02250
3	0.25	0.01050	13	250.00	0.02280
4	0.50	0.01280	14	1500.00	0.02360
5	1.00	0.01550			
6	2.00	0.01880			
7	4.00	0.02020			
8	8.00	0.02100			
9	15.00	0.02130			
10	30.00	0.02180			



Void Ratio = 0.847 **Compression** = 2.3 %
D_0 = 0.00000 D_{50} = 0.01023 D_{100} = 0.02046
C_v at 0.2 min. = 2.11 ft.^{2}/day C_α = 0.001

Pressure: 0.50 tsf — **TEST READINGS** — **Load No. 2**

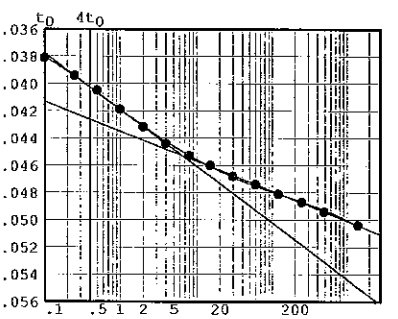
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.02360	11	120.00	0.03380
2	0.10	0.02580	12	240.00	0.03440
3	0.25	0.02660	13	1560.00	0.03570
4	0.50	0.02740	14	2700.00	0.03610
5	1.00	0.02850			
6	2.00	0.02960			
7	4.00	0.03060			
8	8.00	0.03140			
9	15.00	0.03210			
10	60.00	0.03330			



Void Ratio = 0.824 **Compression** = 3.5 %
D_0 = 0.02359 D_{50} = 0.02751 D_{100} = 0.03143
C_v at 0.8 min. = 0.57 ft.^{2}/day C_α = 0.002

Pressure: 1.00 tsf — **TEST READINGS** — **Load No. 3**

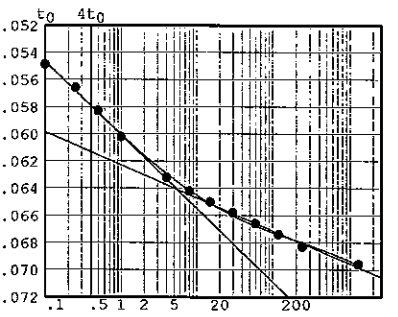
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.03610	11	60.00	0.04870
2	0.10	0.03940	12	120.00	0.04940
3	0.25	0.04070	13	244.00	0.05000
4	0.50	0.04180	14	492.00	0.05070
5	1.00	0.04320	15	1420.00	0.05170
6	2.00	0.04450			
7	4.00	0.04570			
8	8.00	0.04660			
9	15.00	0.04730			
10	30.00	0.04810			



Void Ratio = 0.796 **Compression** = 5.0 %
D_0 = 0.03584 D_{50} = 0.04056 D_{100} = 0.04528
C_v at 0.5 min. = 0.95 ft.^{2}/day C_α = 0.002

Pressure: 2.00 tsf **TEST READINGS** **Load No. 4**

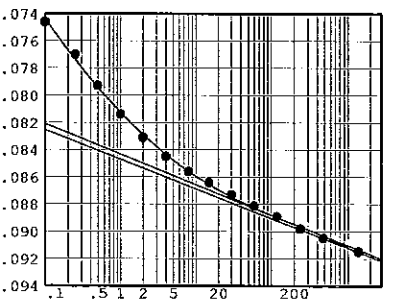
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.05170	11	120.00	0.06950
2	0.10	0.05700	12	240.00	0.07040
3	0.25	0.05870	13	1290.00	0.07170
4	0.50	0.06040			
5	1.00	0.06230			
6	4.00	0.06530			
7	8.00	0.06630			
8	15.00	0.06710			
9	30.00	0.06790			
10	60.00	0.06870			



Void Ratio = 0.760 **Compression** = 7.0 %
D_0 = 0.05161 D_{50} = 0.05784 D_{100} = 0.06407
C_v at 0.4 min. = 1.13 ft.^{2}/day C_α = 0.003

Pressure: 4.00 tsf **TEST READINGS** **Load No. 5**

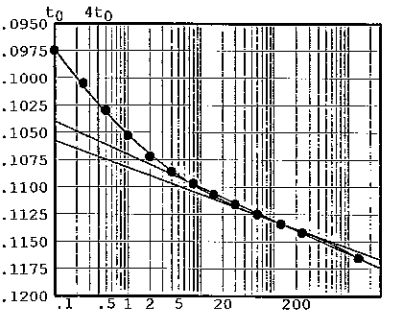
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.07170	11	60.00	0.09130
2	0.10	0.07780	12	120.00	0.09210
3	0.25	0.08020	13	240.00	0.09300
4	0.50	0.08250	14	480.00	0.09370
5	1.00	0.08460	15	1390.00	0.09470
6	2.00	0.08630			
7	4.00	0.08770			
8	8.00	0.08880			
9	15.00	0.08960			
10	30.00	0.09050			



Void Ratio = 0.718 **Compression** = 9.1 %
D_0 = 0.06960 D_{50} = 0.08307 D_{100} = 0.09655
C_v at 2.2 min. = 0.19 ft.^{2}/day C_α = 0.002

Pressure: 8.00 tsf **TEST READINGS** **Load No. 6**

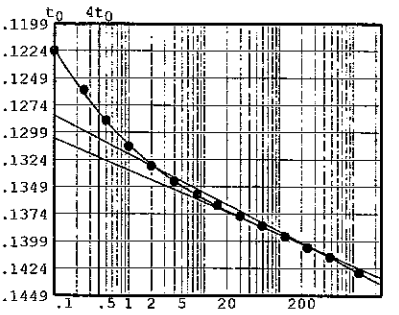
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.09470	11	60.00	0.11700
2	0.10	0.10200	12	126.00	0.11790
3	0.25	0.10500	13	240.00	0.11870
4	0.50	0.10750	14	1380.00	0.12100
5	1.00	0.10980			
6	2.00	0.11170			
7	4.00	0.11310			
8	8.00	0.11420			
9	15.00	0.11520			
10	30.00	0.11610			



Void Ratio = 0.671 **Compression** = 11.6 %
D_0 = 0.09232 D_{50} = 0.10284 D_{100} = 0.11337
C_v at 0.5 min. = 0.86 ft.^{2}/day C_α = 0.003

Pressure: 16.00 tsf | TEST READINGS | Load No. 7

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.12100	11	60.00	0.14510
2	0.10	0.12900	12	120.00	.1461.
3	0.25	0.13260	13	240.00	0.14710
4	0.50	0.13540	14	480.00	0.14800
5	1.00	0.13780	15	1190.00	0.14940
6	2.00	0.13960			
7	4.00	0.14100			
8	8.00	0.14220			
9	15.00	0.14320			
10	30.00	0.14420			



Void Ratio = 0.621 **Compression =** 14.3 %
D_0 = 0.11643 D_{50} = 0.12845 D_{100} = 0.14047
C_v **at 0.4 min.** = 0.84 ft.^{2}/day C_α = 0.004

Southern Earth Sciences, Inc.

Laboratory Test Results

Project: **Bayou DuPont** | **Technical Responsibility:** | **Quality Assurance Officer**

Client: URS

7389 Florida Blvd., Suite 300, Baton Rouge, LA 70806 | Project No.: **B09-012** | PM: S. Aviles | Date of Issue: 3/12/2009

			ASTM DESIGNATION																
			D2216	D4318			D427	D2166		D2166	D2850	D422, C136 or C117					D2974	USCS	
				Atterberg Limits						Cohesion		Grain Size (% Passing)							
Boring No.	Depth (ft)	Classification	ω %	LL	PL	PI	SL	γ_{wet} pcf	γ_{dry} pcf	U psf	UU psf	Gravel	Sand	Silt	Clay	#200	Organic Content %		Confining Stress, Resistivity and Remarks
B-9	0-2	Peat	893.5					58.2	5.9									(PT)	
B-9	2-4	Very Soft PEAT with clay and organics	255.1	257	84	173	4.9	72.1	20.3		59.6						15.1	(PT)	Confining Pressure: 1.3 psi
B-9	4-6	Very Soft, Gray CLAY with Organics	134.8					85.3	36.3		108.2		1.6	24.9	73.5			(CH)	Confining Pressure: 2.0 psi
B-9	6-8	PEAT with clay pockets and silt pockets	334.4	573	146	427	15.7	73.1	16.8		173.0							(PT)	Specific Gravity: 2.21 Confinfing Pressure: 2.6 psi
B-9	8-10	CLAY with Organics	204.6					67.1	22.0		47.6		4.8	45.5	49.7		10.5	(CL-ML)	Confining Pressure: 3.3 psi
B-9	10-12	Very Soft, Gray CLAY with trace silt and organics pockets	60.2	65	26	39	13.9	99.6	62.2		75.4							(CH)	Confining Pressure: 3.9 psi
B-9	12-14	Very Soft, Gray CLAY with trace organic pockets	58.9					114.4	72.0		148.2							(CH)	Specific Gravity: 2.78 Confinfing Pressure: 4.6 psi
B-9	14-16	Very Soft CLAY with silt and trace organics	49.3	54	28	26		120.5	80.7		134.5		1.3	70.1	28.6			(CH)	Confining Pressure: 5.3 psi
B-9	16-18	Loose, Gray SILT with clay pockets and trace fine sand	33.9					116.3	86.9		534.3					81.8		(ML)	Confining Pressure: 6.0 psi
B-9	18-20	Firm, Gray SILT with trace fine sand and clay	25.4	NP	NP	NP		119.1	94.9		2936.1		4.6	52.6	42.8		0.6	(ML)	Confining Pressure: 6.6 psi
B-9	20-22	Very Soft, Gray CLAY with silt Lenses	98.4					101.2	51.0		104.5					99.6		(CH)	Confining Pressure: 7.3 psi
B-9	22-24	Soft, Gray CLAY with silt pockets	50.9	66	27	39		101.3	67.1									(CH)	Specific Gravity: 2.80
B-9	24-26	Very Soft, Gray CLAY with silt becoming SILT with clay	79.8					104.5	58.1		111.6		1.6	40.0	58.4			(CH)	Confining Pressure: 8.5 psi
B-9	26-28	Soft, Gray CLAY with silt pockets	64.4					101.8	61.9									(CH)	
B-9	28-30	Very Soft, Gray CLAY with trace silt and trace organics	71.2	72	27	45		102.7	60.0		142.3		0.6	84.8	14.8		5.6	(CH)	Confining Pressure: 9.9 psi

Southern Earth Sciences, Inc.

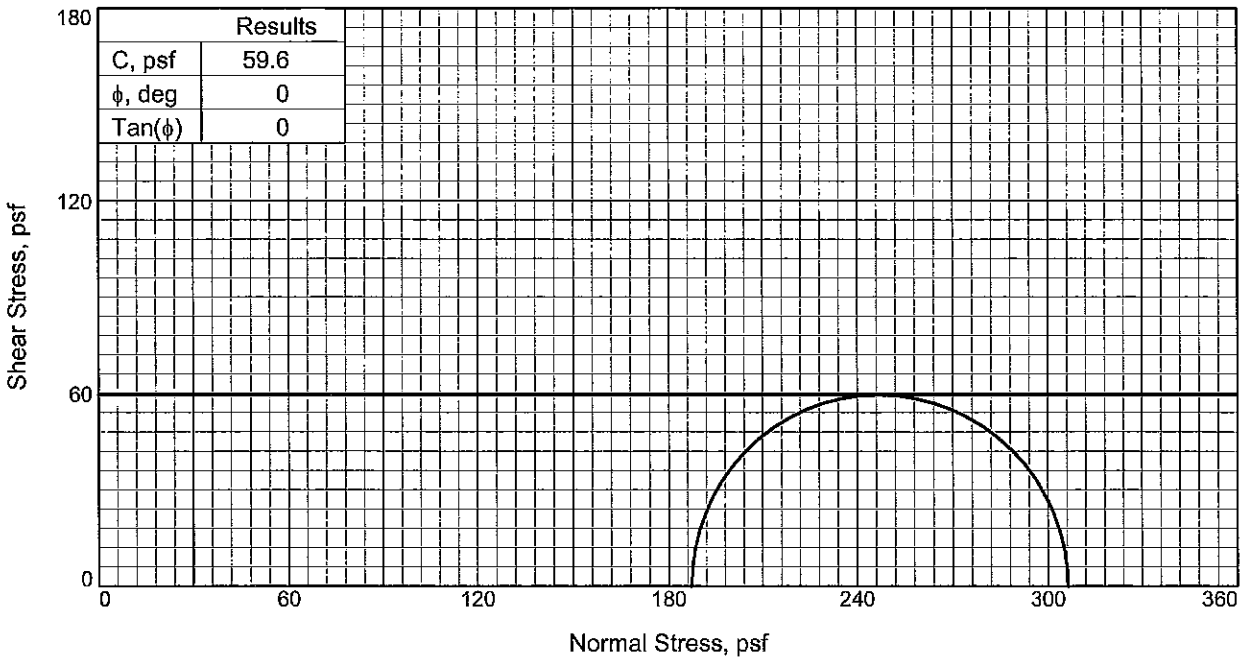
Laboratory Test Results

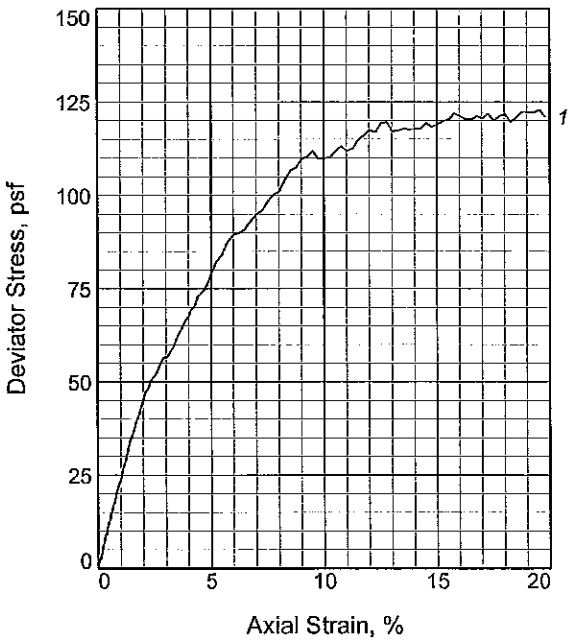
Project: **Bayou DuPont** Technical Responsibility: Quality Assurance Officer

Client: URS

7389 Florida Blvd., Suite 300, Baton Rouge, LA 70806 Project No.: **B09-012** PM: S. Aviles Date of Issue: 3/12/2009

Boring No.	Depth (ft)	Classification	ASTM DESIGNATION																USCS	Confining Stress, Resistivity and Remarks
			D2216	D4318			D427	D2166		D2166	D2850	D422, C136 or C117					D2974		
				Atterberg Limits						Cohesion		Grain Size (% Passing)					Organic Content %		
			ω %	LL	PL	PI	SL	γ_{wet} pcf	γ_{dry} pcf	U psf	UU psf	Gravel	Sand	Silt	Clay	#200			
B-9	30-32	Gray SANDY SILT with clay pockets	30.0					121.7	93.6							85.5		(ML)	
B-9	32-34	Intermixed CLAY and SANDY SILT	38.5	38	31	7	19.1	114.1	82.4		484.3							(CL-ML)	Specific Gravity: 2.65 Confining Pressure: 11.2 psi
B-9	34-36	Soft, Gray SILT with clay pockets	42.8					111.7	78.2				0.6	72.9	26.5			(ML)	
B-9	36-38	Soft, Gray CLAY with silt streaks	55.2	86	34	52		102.9	66.3		309.8							(CH)	Confining Pressure: 12.5 psi
B-9	38-40	Gray SILT with clay pockets and layers	53.1					103.8	67.8				0.0	73.3	26.7		2.8	(ML)	
B-9	40-42	Very Soft, Gray CLAY with trace silt	63.4					104.0	63.6		146.3					100.0		(CH)	Confinfing Pressure: 13.9 psi
B-9	42-44	Very Soft, Gray CLAY with silt pockets	53.8	60	26	34												(CH)	
B-9	44-46	Soft, Gray CLAY with sandy silt pockets	57.7				11.4	102.1	64.8				0.0	35.3	64.7		3.0	(CH)	
B-9	46-48	Very Soft, Gray CLAY with silt pockets	57.3	52	21	31		105.8	67.2		190.7							(CH)	Specific Gravity: 2.80 Confining Pressure: 15.9 psi
B-9	48-50	SAND CLAYEY SILT	34.3										1.4	76.3	22.3			(ML)	
B-9	50-52	Medium, Gray CLAY with silt pockets	43.0	56	26	30		108.8	76.1		458.3							(CH)	Confining Pressure: 17.2 psi
B-9	52-54	Very Soft, Gray CLAY with trace silt and trace organics																(CH)	No tests assigned to sample
B-9	54-56	Soft, Gray CLAY with silt	59.0	76	27	49		105.7	66.5		360.2		0.0	27.7	72.3			(CH)	Confining Pressure: 18.4 psi
B-9	56-58	Soft To Medium, Gray CLAY	57.9															(CH)	
B-9	58-60	Very Soft CLAY with trace silt	57.4	69	26	43		103.3	65.6		153.4		0.0	30.2	69.8		2.3	(CH)	Confining Pressure: 19.7 psi





Sample No.		1
Initial	Water Content, %	255.1
	Dry Density, pcf	20.3
	Saturation, %	95.9
	Void Ratio	6.3820
	Diameter, in.	2.675
	Height, in.	5.940
At Test	Water Content, %	255.1
	Dry Density, pcf	20.3
	Saturation, %	95.9
	Void Ratio	6.3820
	Diameter, in.	2.675
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		1.300
Fail. Stress, psf		119.1
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		306.3
σ_3 Failure, psf		187.2

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO PEAT W/ CL & ORGS, PT

LL= 257 **PL=** 84 **PI=** 173
Assumed Specific Gravity= 2.40
Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

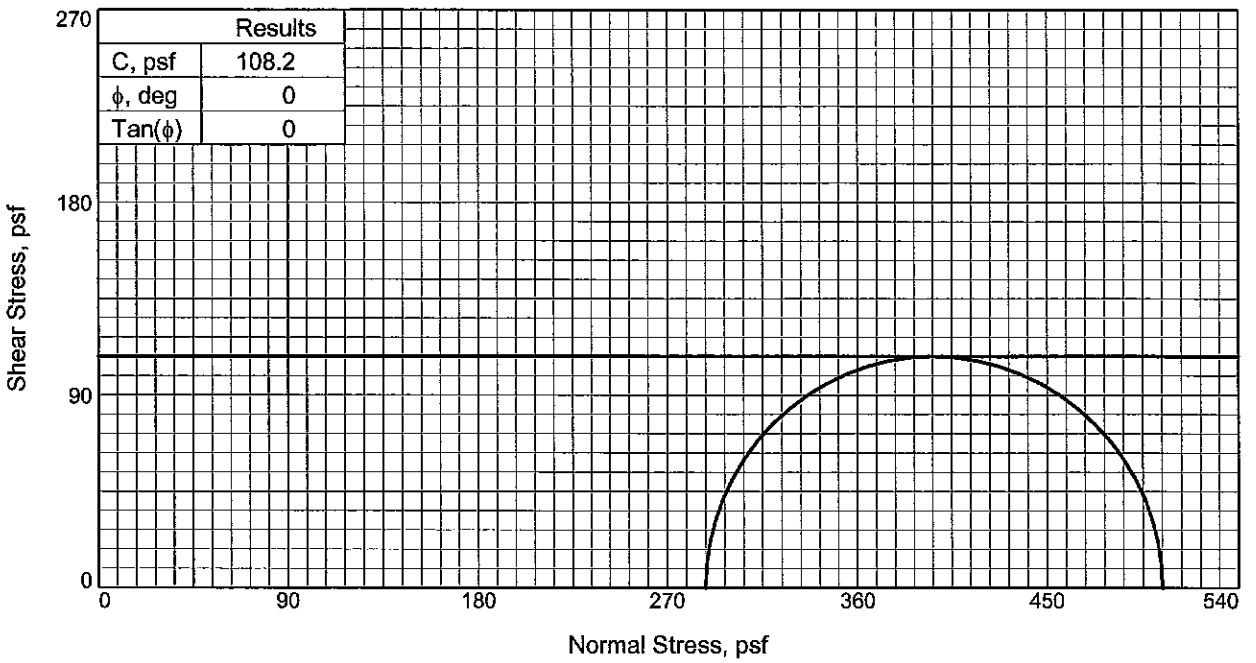
Client: URS

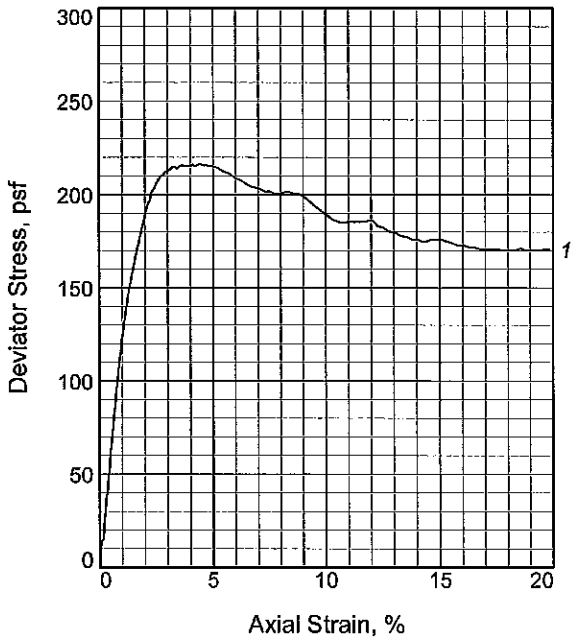
Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 2-4
Sample Number: 2
Proj. No.: B09-012 **Date Sampled:** 3/23/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	134.8
	Dry Density, pcf	36.3
	Saturation, %	99.0
	Void Ratio	3.8122
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	134.8
	Dry Density, pcf	36.3
	Saturation, %	99.0
	Void Ratio	3.8122
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.000
Fail. Stress, psf		216.3
Strain, %		4.4
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		504.3
σ_3 Failure, psf		288.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ ORGS, CH

Assumed Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 4-6

Sample Number: 3

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	1.6	24.9	73.5

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○			0.0211	0.0013						

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ ORGS, CH	CH	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-9 **Sample No.:** 3 **Elev./Depth:** 4-6

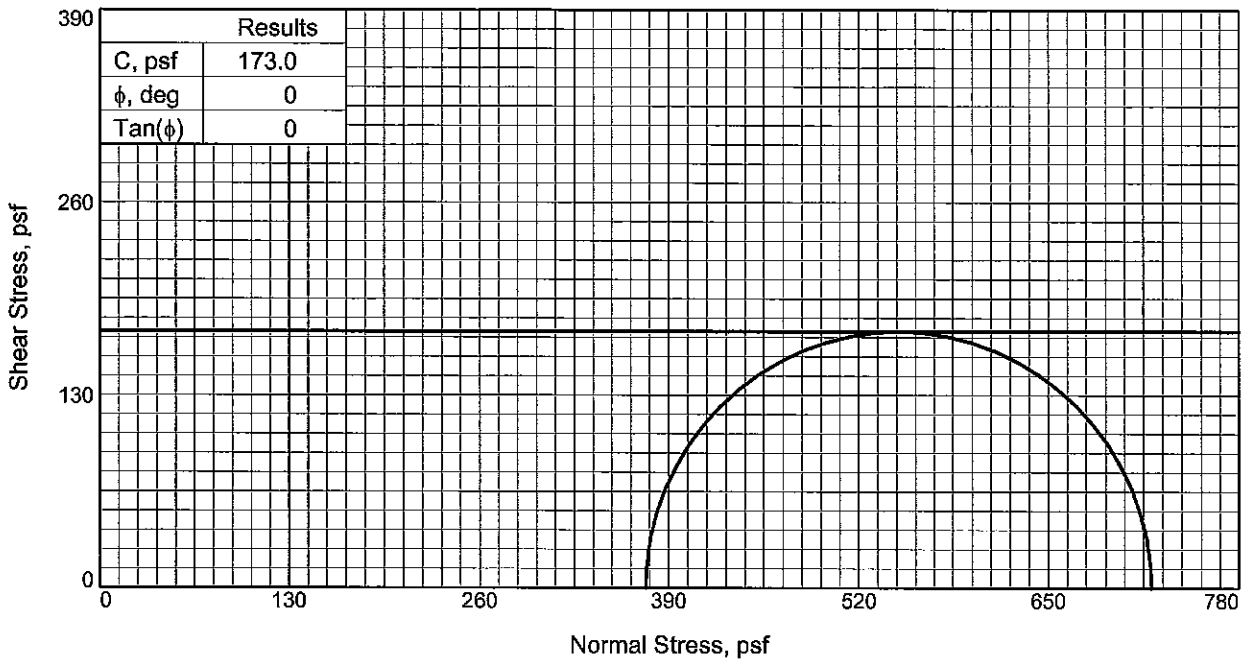
Remarks:

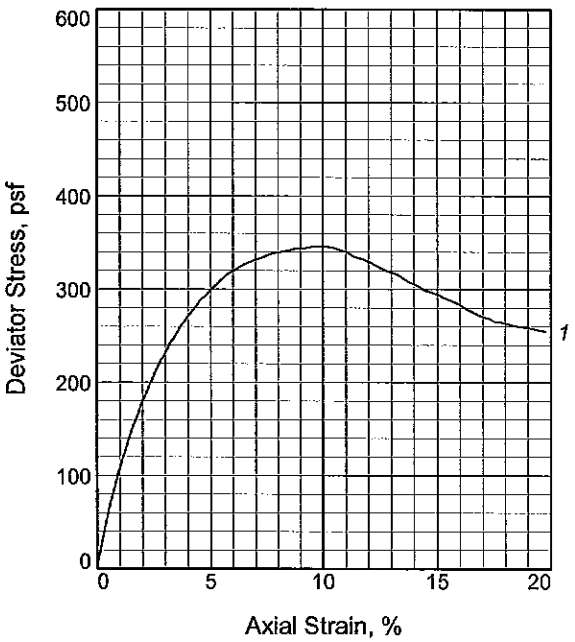
○ ASTM D422, C136

F.M.=0.01

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	334.4
	Dry Density, pcf	16.8
	Saturation, %	102.7
	Void Ratio	7.1992
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	334.4
	Dry Density, pcf	16.8
	Saturation, %	102.7
	Void Ratio	7.1992
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		2.600
Fail. Stress, psf		346.0
Strain, %		9.8
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		720.4
σ_3 Failure, psf		374.4

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: PEAT W/ CL PKTS & SI PKTS, PT

LL= 573 **PL=** 146 **PI=** 427
Specific Gravity= 2.21
Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

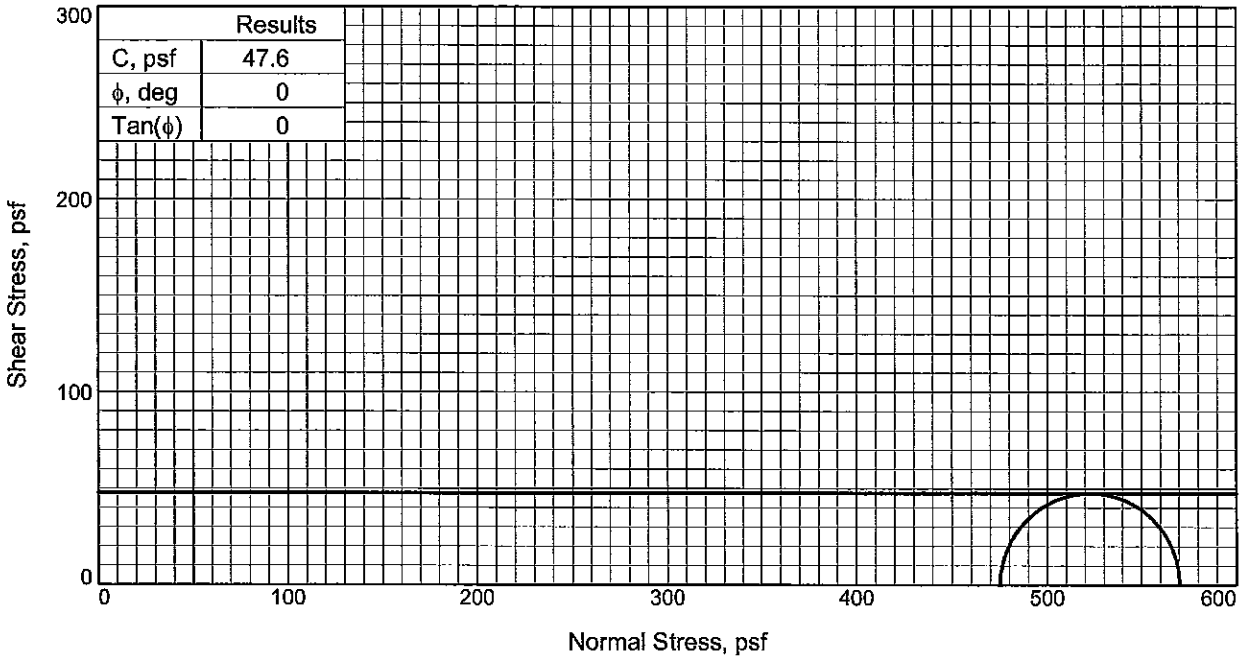
Client: URS

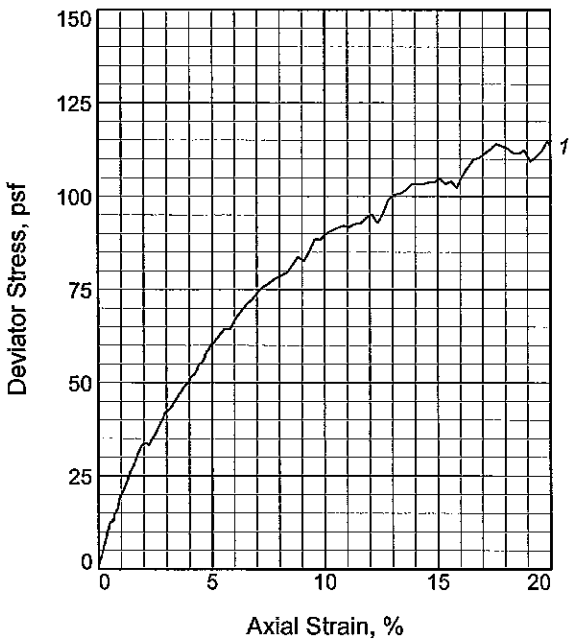
Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 6-8
Sample Number: 4
Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	204.6
	Dry Density, pcf	22.0
	Saturation, %	85.9
	Void Ratio	5.2380
	Diameter, in.	2.900
	Height, in.	5.608
At Test	Water Content, %	204.6
	Dry Density, pcf	22.0
	Saturation, %	85.9
	Void Ratio	5.2380
	Diameter, in.	2.900
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		3.300
Fail. Stress, psf		95.2
Strain, %		12.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		570.4
σ_3 Failure, psf		475.2

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: CL, CL-ML

Assumed Specific Gravity= 2.20
Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

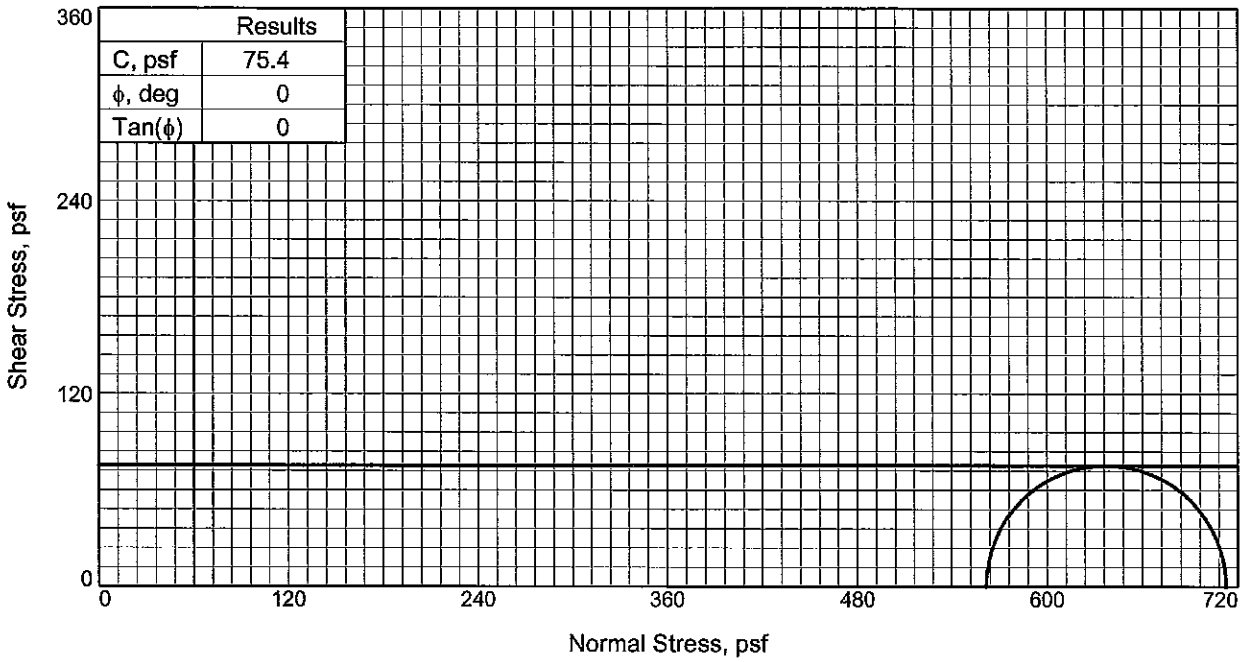
Client: URS

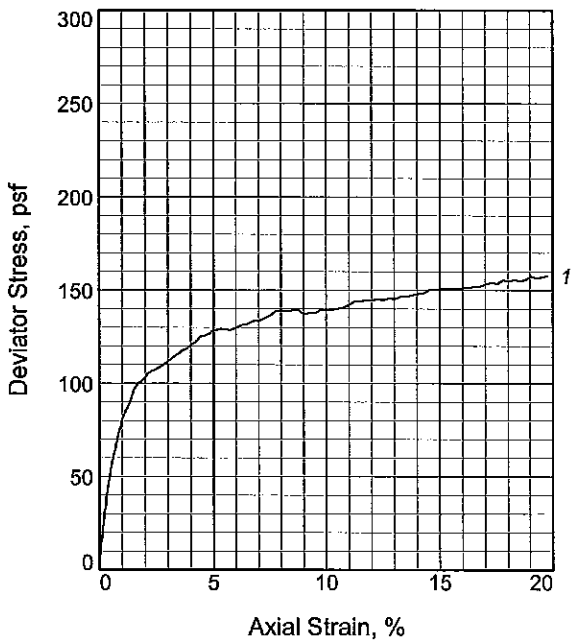
Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 8-10
Sample Number: 5
Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	60.2
	Dry Density, pcf	62.2
	Saturation, %	93.1
	Void Ratio	1.8110
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	60.2
	Dry Density, pcf	62.2
	Saturation, %	93.1
	Void Ratio	1.8110
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		3.900
Fail. Stress, psf		150.9
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		712.5
σ_3 Failure, psf		561.6

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ TR SI & ORG PKTS, CH

LL= 65 **PL=** 26 **PI=** 39

Assumed Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

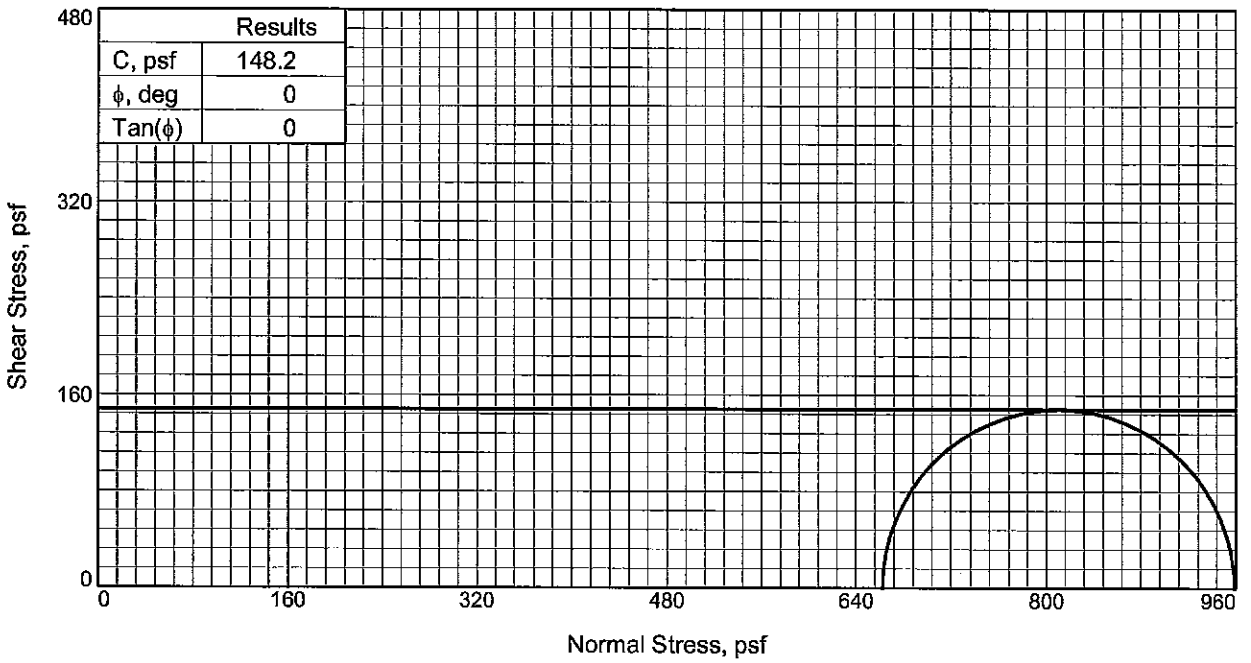
Source of Sample: B-9 **Depth:** 10-12

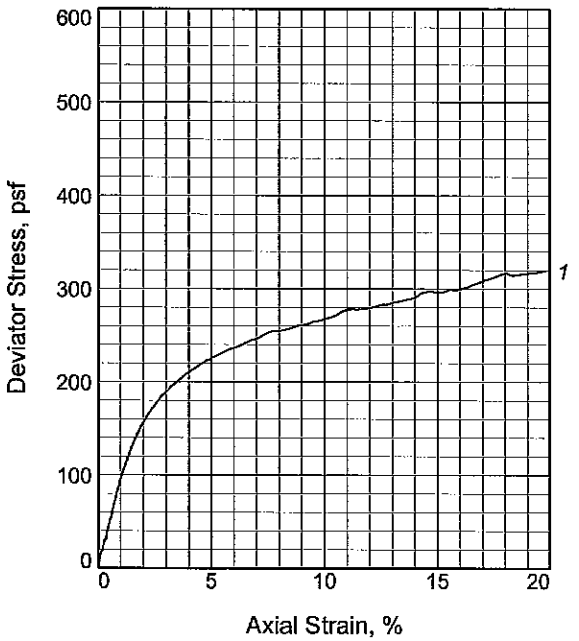
Sample Number: 6

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	58.9
	Dry Density, pcf	72.0
	Saturation, %	116.1
	Void Ratio	1.4107
	Diameter, in.	2.800
	Height, in.	5.608
At Test	Water Content, %	58.9
	Dry Density, pcf	72.0
	Saturation, %	116.1
	Void Ratio	1.4107
	Diameter, in.	2.800
	Height, in.	5.608
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		4.600
Fail. Stress, psf		296.3
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		958.7
σ_3 Failure, psf		662.4

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ TR ORG PKTS, CH

Specific Gravity= 2.78

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

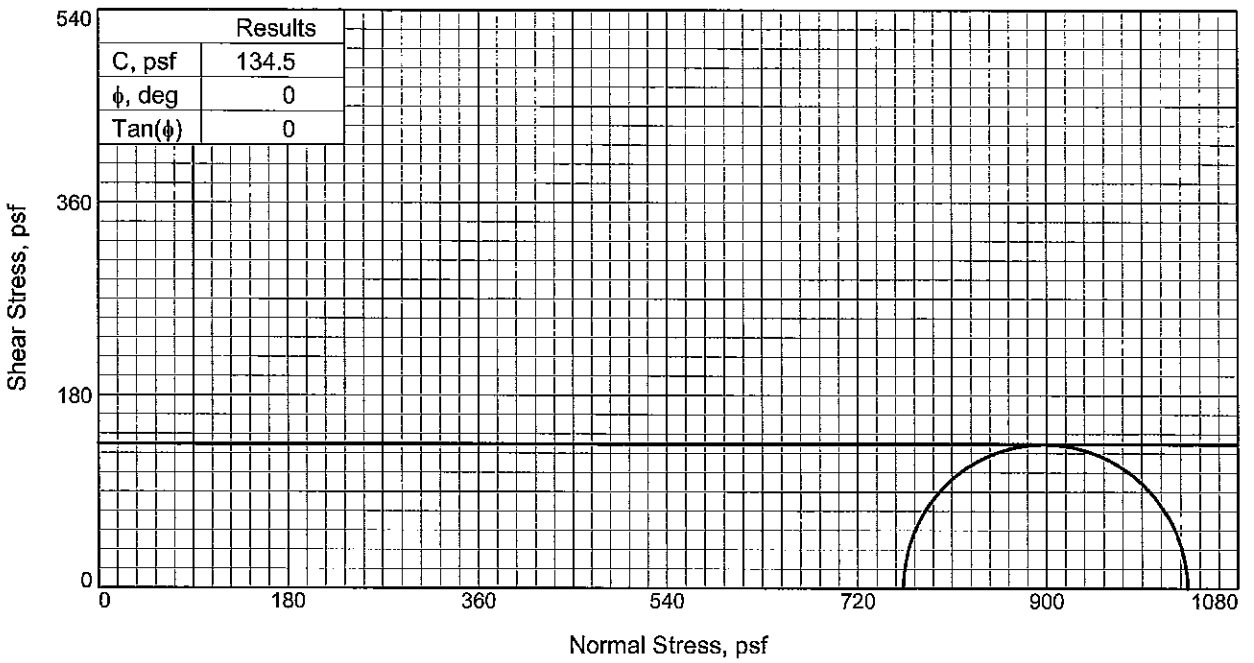
Source of Sample: B-9 **Depth:** 12-14

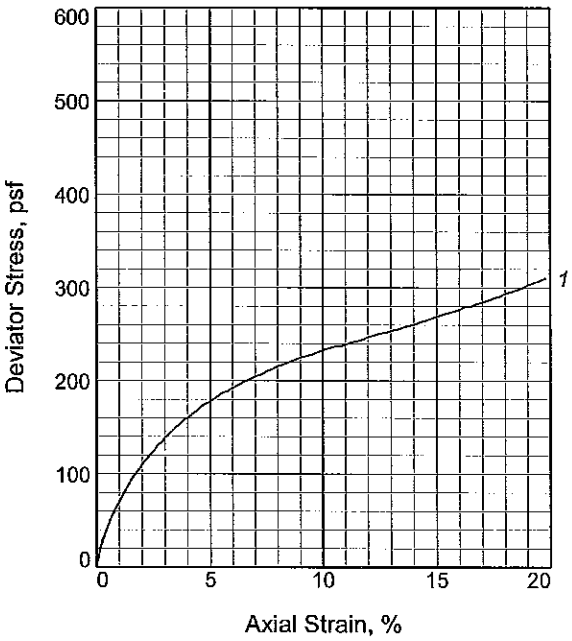
Sample Number: 7

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	49.3
	Dry Density, pcf	80.7
	Saturation, %	118.4
	Void Ratio	1.1659
	Diameter, in.	2.750
	Height, in.	5.940
At Test	Water Content, %	49.3
	Dry Density, pcf	80.7
	Saturation, %	118.4
	Void Ratio	1.1659
	Diameter, in.	2.750
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		5.300
Fail. Stress, psf		269.1
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1032.3
σ_3 Failure, psf		763.2

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ SI PKTS & TR ORGS, CH

LL= 54 **PL=** 28 **PI=** 26

Assumed Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 14-16

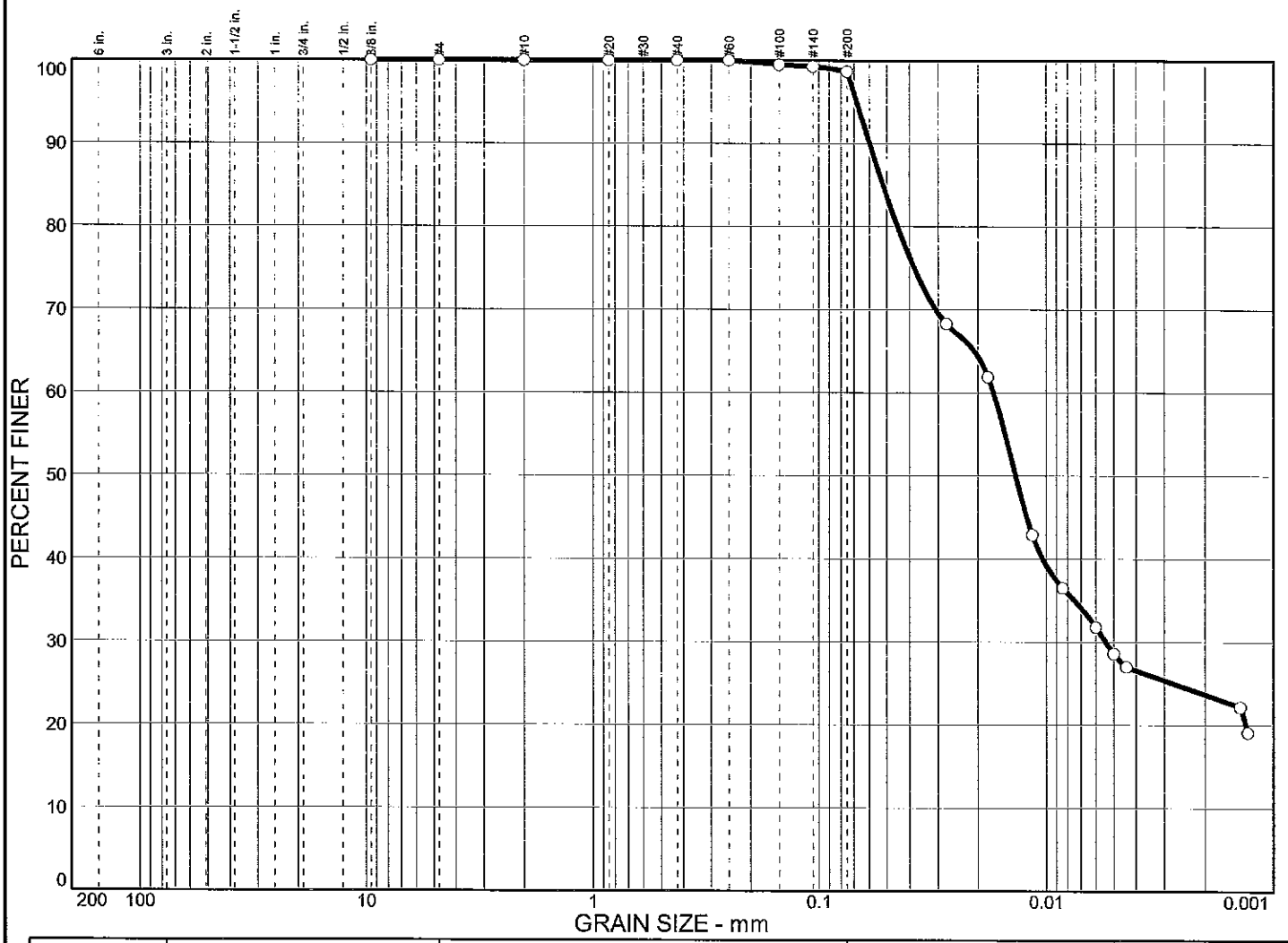
Sample Number: 8

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	1.3	70.1	28.6

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	54	28	0.0521	0.0171	0.0137	0.0054				

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ SI PKTS & TR ORGS, CH		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

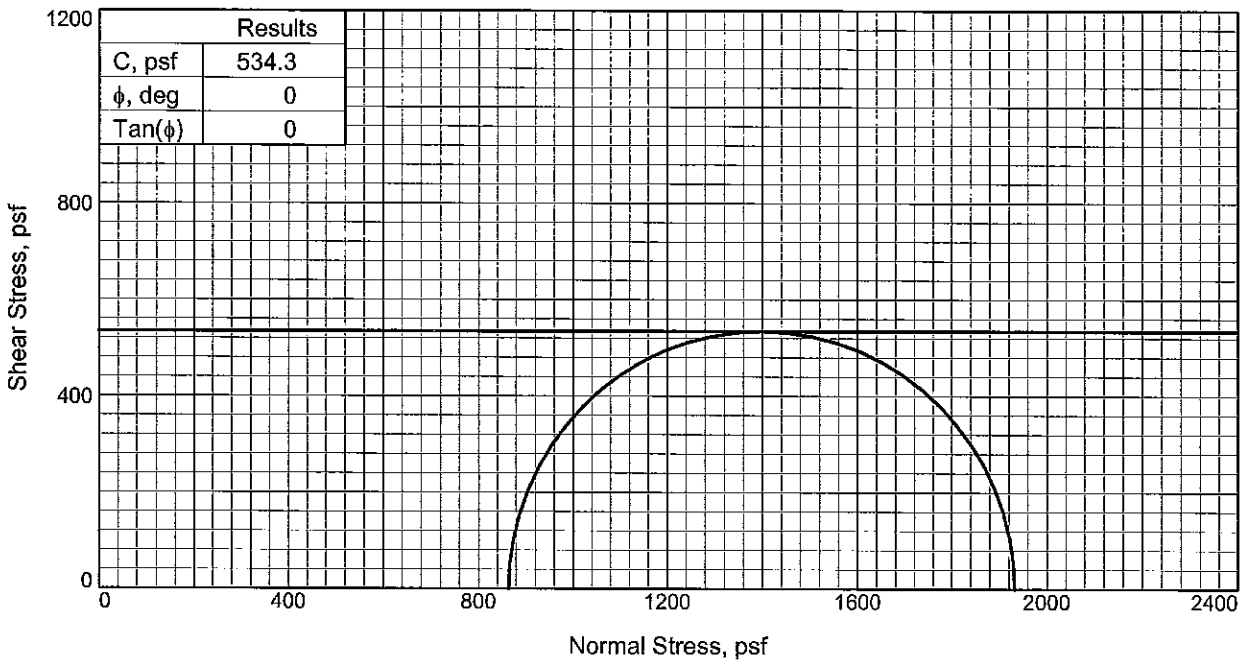
○ **Source:** B-9 **Sample No.:** 8 **Elev./Depth:** 14-16

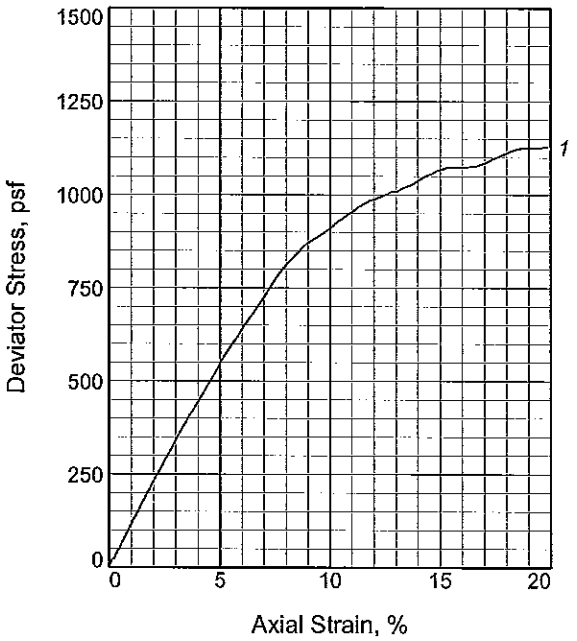
Remarks:

○ F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	33.9
	Dry Density, pcf	86.9
	Saturation, %	99.3
	Void Ratio	0.9041
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	33.9
	Dry Density, pcf	86.9
	Saturation, %	99.3
	Void Ratio	0.9041
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		6.000
Fail. Stress, psf		1068.5
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1932.5
σ_3 Failure, psf		864.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: LO G SI W/ CL PKTS & TR F SA, ML

Assumed Specific Gravity= 2.65

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

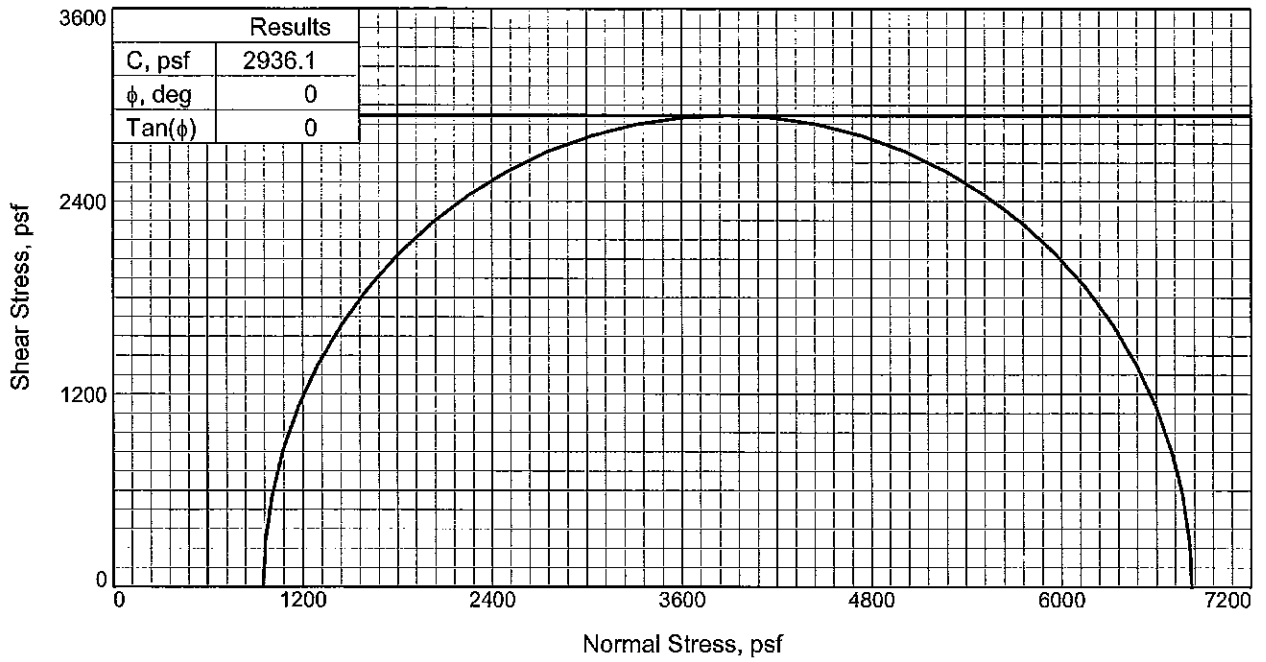
Source of Sample: B-9 **Depth:** 16-18

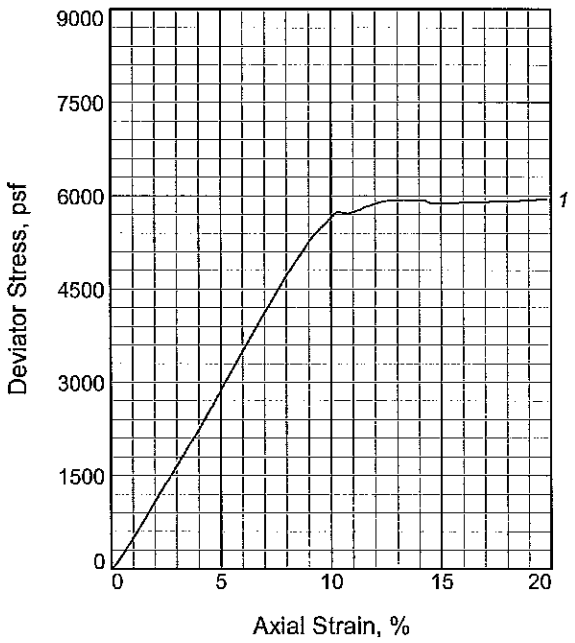
Sample Number: 9

Proj. No.: B09-012 **Date Sampled:** 3/18/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	25.4
	Dry Density, pcf	94.9
	Saturation, %	90.8
	Void Ratio	0.7426
	Diameter, in.	2.738
	Height, in.	5.940
At Test	Water Content, %	25.4
	Dry Density, pcf	94.9
	Saturation, %	90.8
	Void Ratio	0.7426
	Diameter, in.	2.738
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		6.600
Fail. Stress, psf		5872.3
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		6822.7
σ_3 Failure, psf		950.4

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: FM G SI W/ TR F SA & CL, ML

LL= NP **PI=** NP

Assumed Specific Gravity= 2.65

Remarks: TYPE OF FAILURE: BULGE & 40° SHEAR

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 18-20

Sample Number: 10

Proj. No.: B09-012 **Date Sampled:** 3/23/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	4.6	52.6	42.8

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	NP	NP	0.0565	0.0331	0.0106	0.0016				

MATERIAL DESCRIPTION	USCS	AASHTO
○ FM G SI W/ TR F SA & CL, ML	(ML)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-9 **Sample No.:** 10 **Elev./Depth:** 18-20

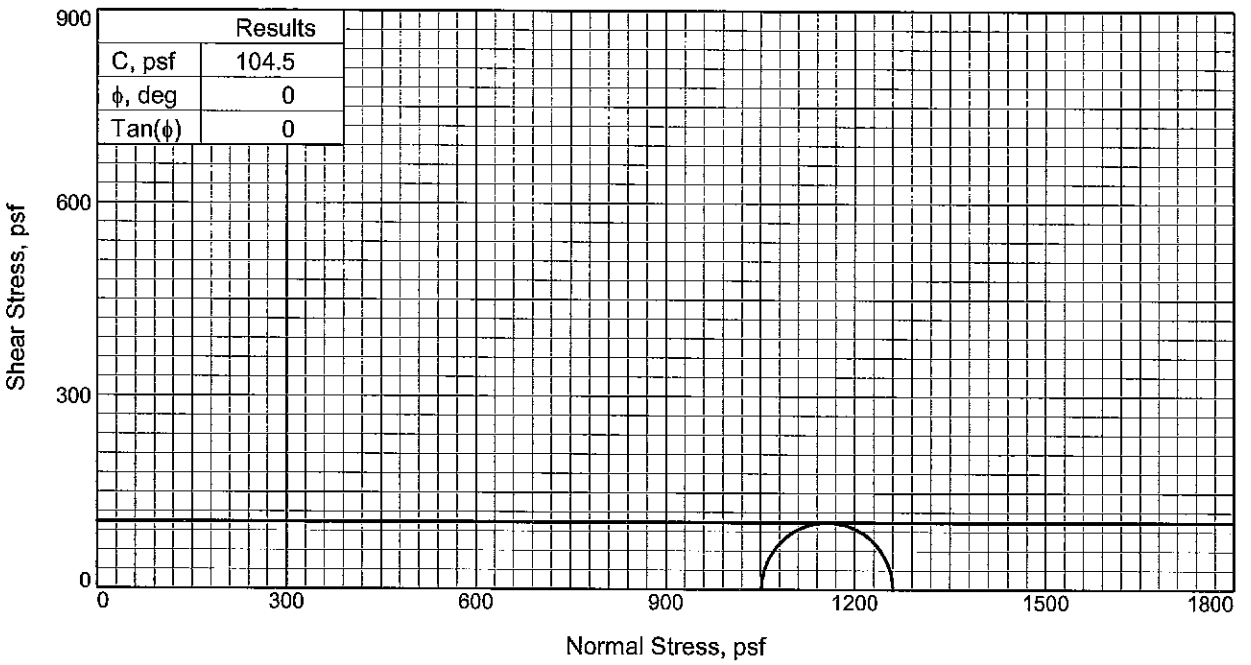
Remarks:

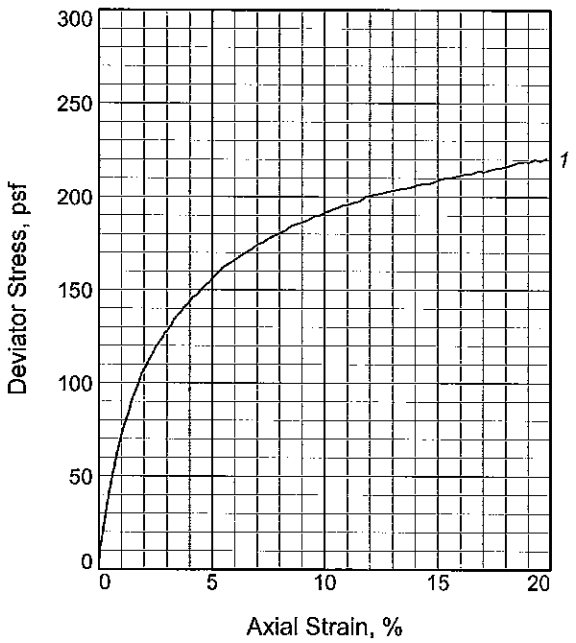
○ ASTM D422, C136

F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	98.3
	Dry Density, pcf	51.0
	Saturation, %	113.5
	Void Ratio	2.4261
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	98.3
	Dry Density, pcf	51.0
	Saturation, %	113.5
	Void Ratio	2.4261
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		7.300
Fail. Stress, psf		209.1
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1260.3
σ_3 Failure, psf		1051.2

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ SI LENS, CH

Assumed Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

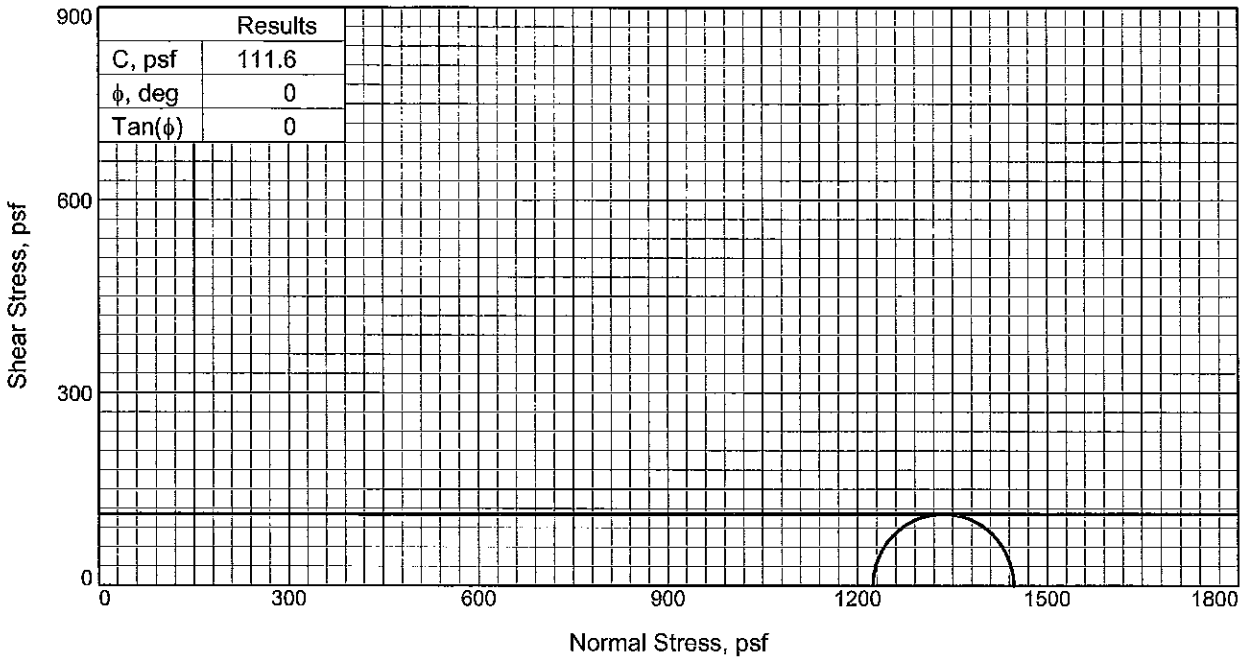
Source of Sample: B-9 **Depth:** 20-22

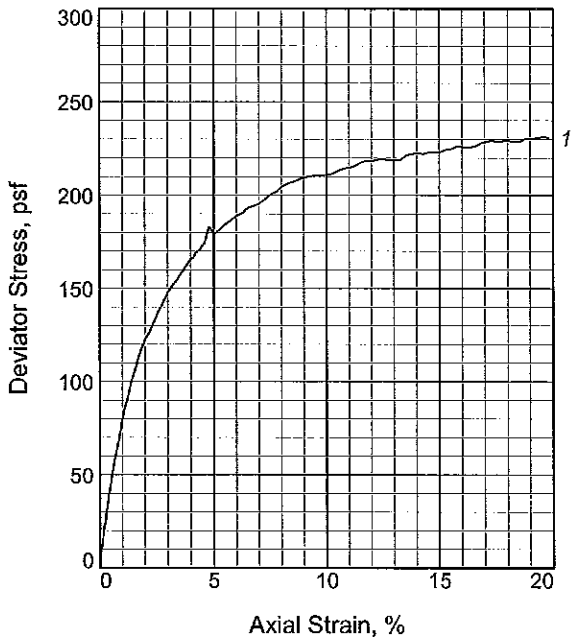
Sample Number: 11

Proj. No.: B09-012 **Date Sampled:** 3/19/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	79.8
	Dry Density, pcf	58.1
	Saturation, %	113.5
	Void Ratio	1.8988
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	79.8
	Dry Density, pcf	58.1
	Saturation, %	113.5
	Void Ratio	1.8988
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		8.500
Fail. Stress, psf		223.3
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1447.3
σ_3 Failure, psf		1224.0

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ SI BEC SI W/ CL, CH TO ML

Assumed Specific Gravity= 2.70

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 24-26

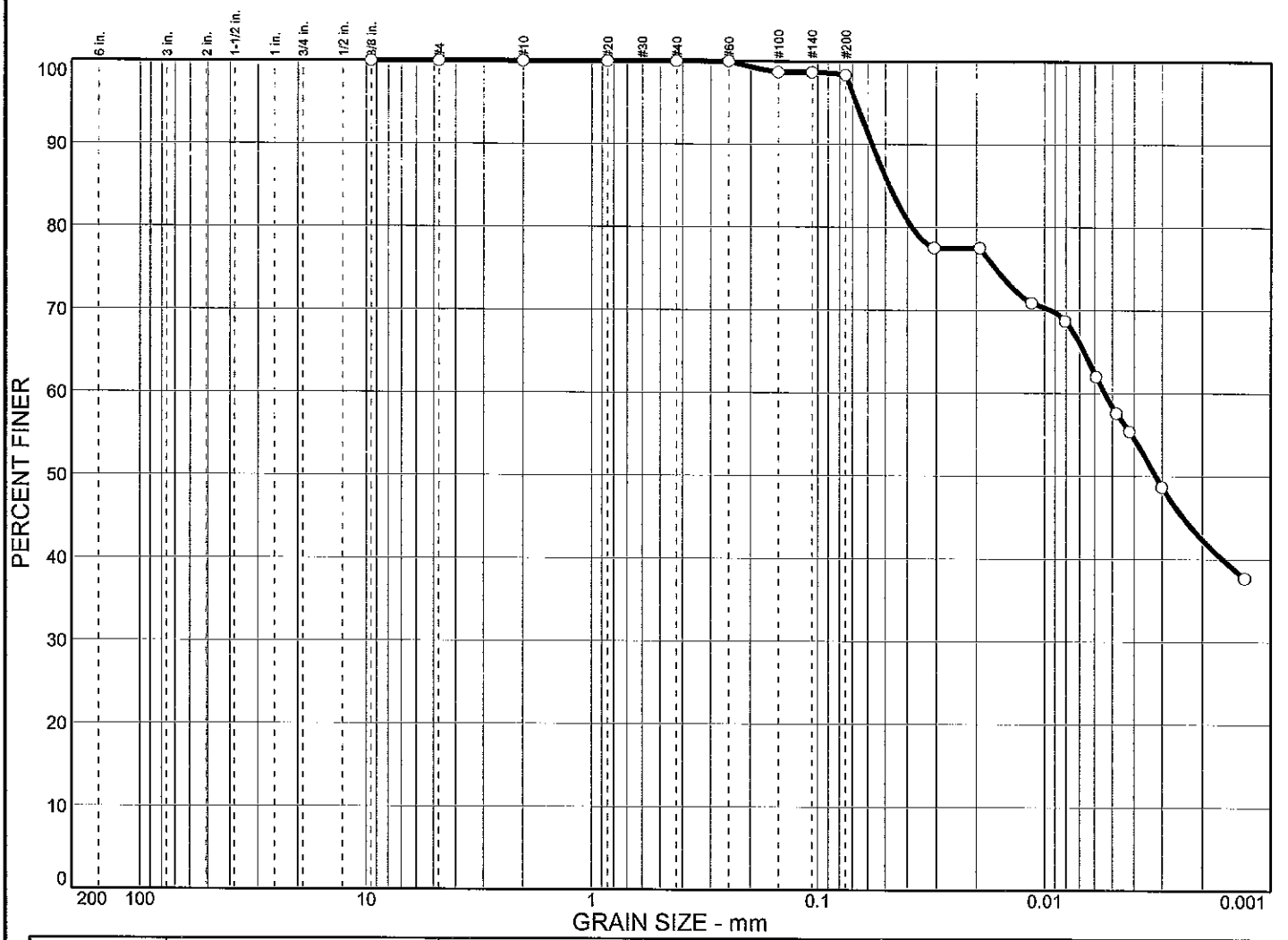
Sample Number: 13

Proj. No.: B09-012 **Date Sampled:** 3/19/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	1.6	40.0	58.4

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○			0.0481	0.0054	0.0032					

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ SI BEC SI W/ CL, CH TO ML		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

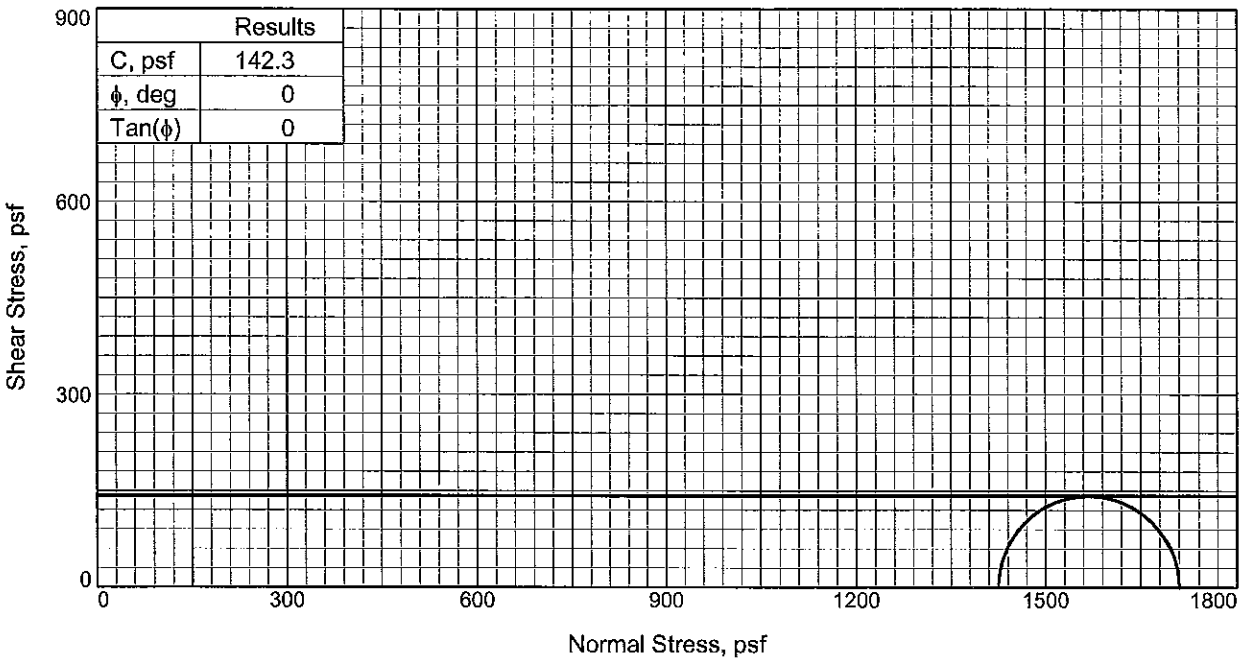
○ **Source:** B-9 **Sample No.:** 13 **Elev./Depth:** 24-26

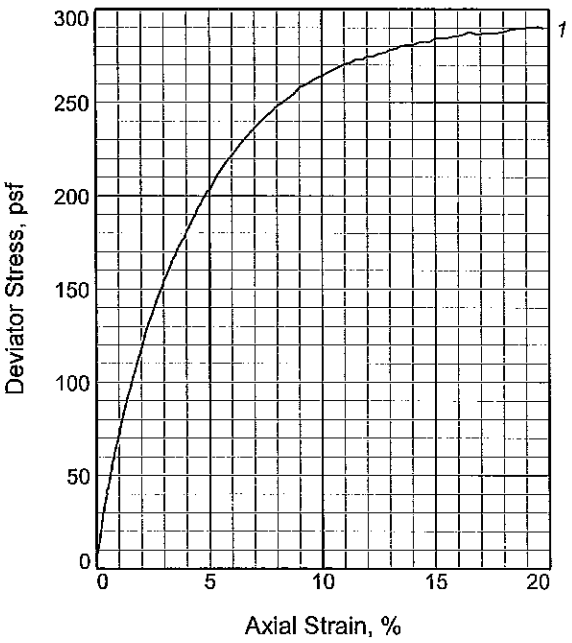
Remarks:

○ F.M.=0.01

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	71.2
	Dry Density, pcf	60.0
	Saturation, %	104.1
	Void Ratio	1.9155
	Diameter, in.	2.738
	Height, in.	5.940
At Test	Water Content, %	71.2
	Dry Density, pcf	60.0
	Saturation, %	104.1
	Void Ratio	1.9155
	Diameter, in.	2.738
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		9.900
Fail. Stress, psf		284.5
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		1710.1
σ_3 Failure, psf		1425.6

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ TR SI & TR ORGS, CH

LL= 72 **PL=** 27 **PI=** 45

Assumed Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 28-30

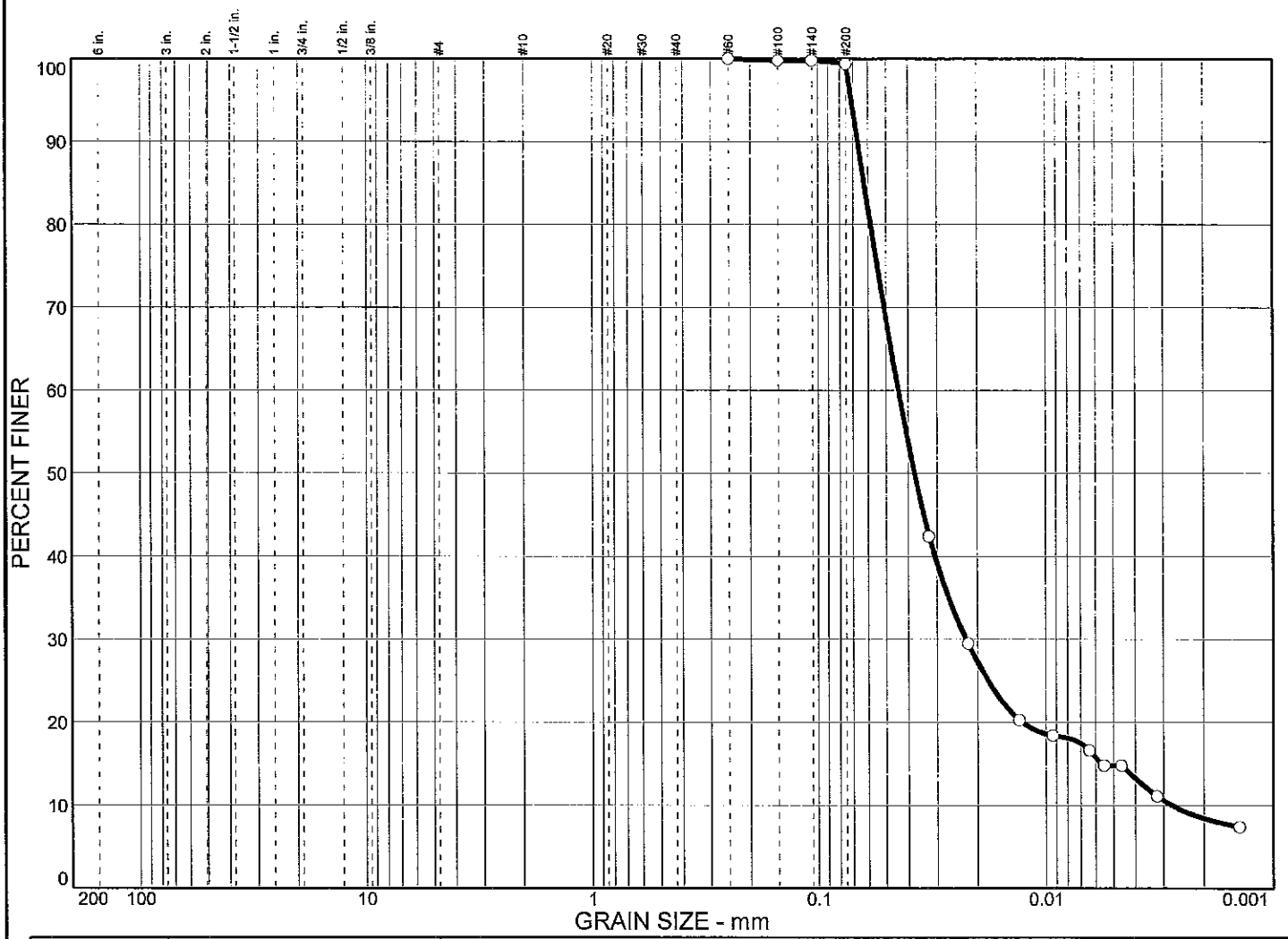
Sample Number: 15

Proj. No.: B09-012 **Date Sampled:** 3/23/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.6	84.6	14.8

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	72	27	0.0624	0.0442	0.0376	0.0224	0.0056	0.0028	4.13	16.02

MATERIAL DESCRIPTION	USCS	AASHTO
○ VSO G CL W/ TR SI & TR ORGS, CH	(CH)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-9 **Sample No.:** 15 **Elev./Depth:** 28-30

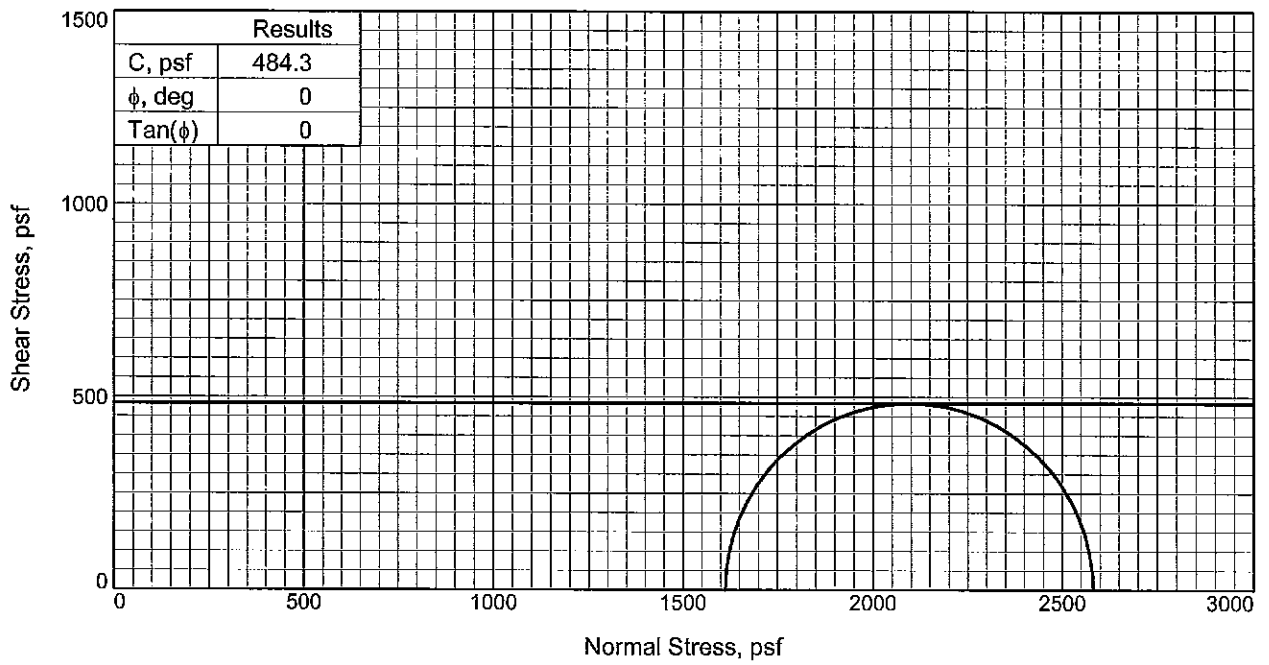
Remarks:

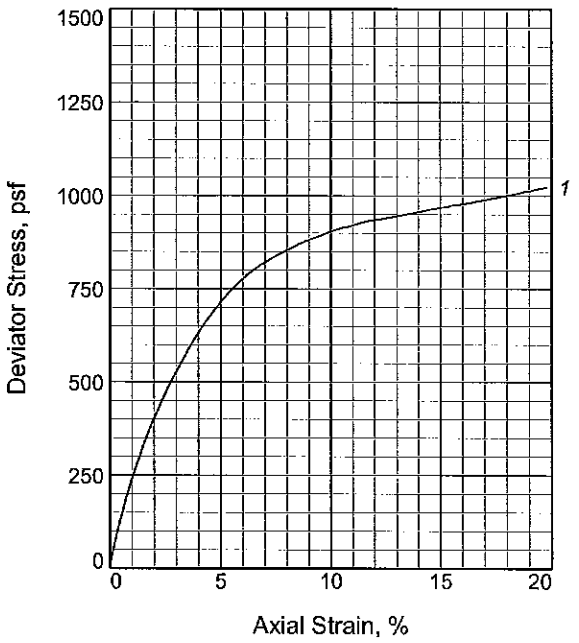
○ ASTM D422, C136

F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	38.5
	Dry Density, pcf	82.4
	Saturation, %	101.3
	Void Ratio	1.0071
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	38.5
	Dry Density, pcf	82.4
	Saturation, %	101.3
	Void Ratio	1.0071
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		11.200
Fail. Stress, psf		968.5
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2581.3
σ_3 Failure, psf		1612.8

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: INTERMIX SO G CL & G SI, CL-ML

LL= 38 **PL=** 31 **PI=** 7
Specific Gravity= 2.649
Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

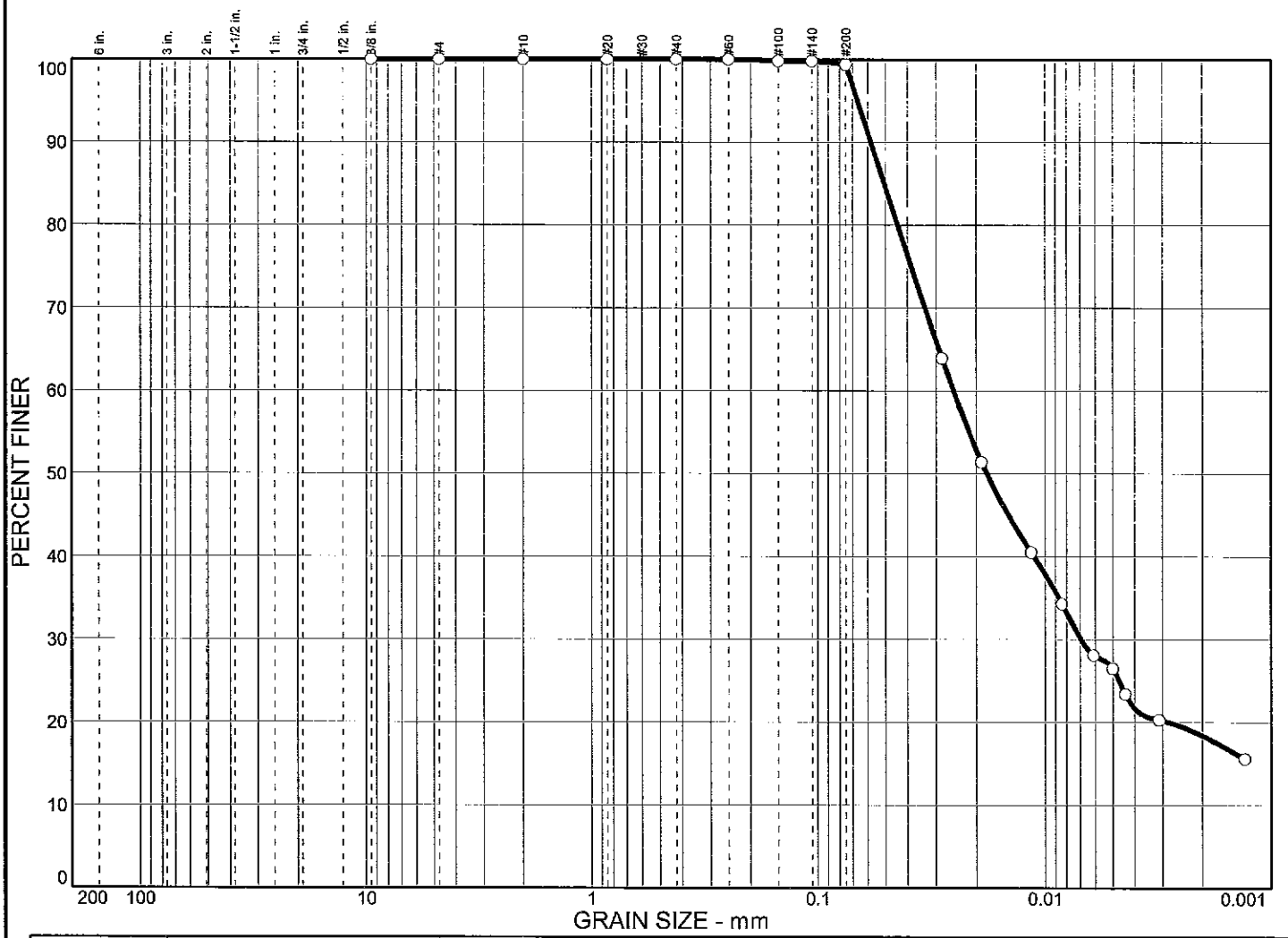
Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 32-34
Sample Number: 17
Proj. No.: B09-012 **Date Sampled:** 3/19/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.6	72.9	26.5

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○			0.0507	0.0251	0.0180	0.0069				

MATERIAL DESCRIPTION	USCS	AASHTO
○ SO G SI W/CL, ML		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

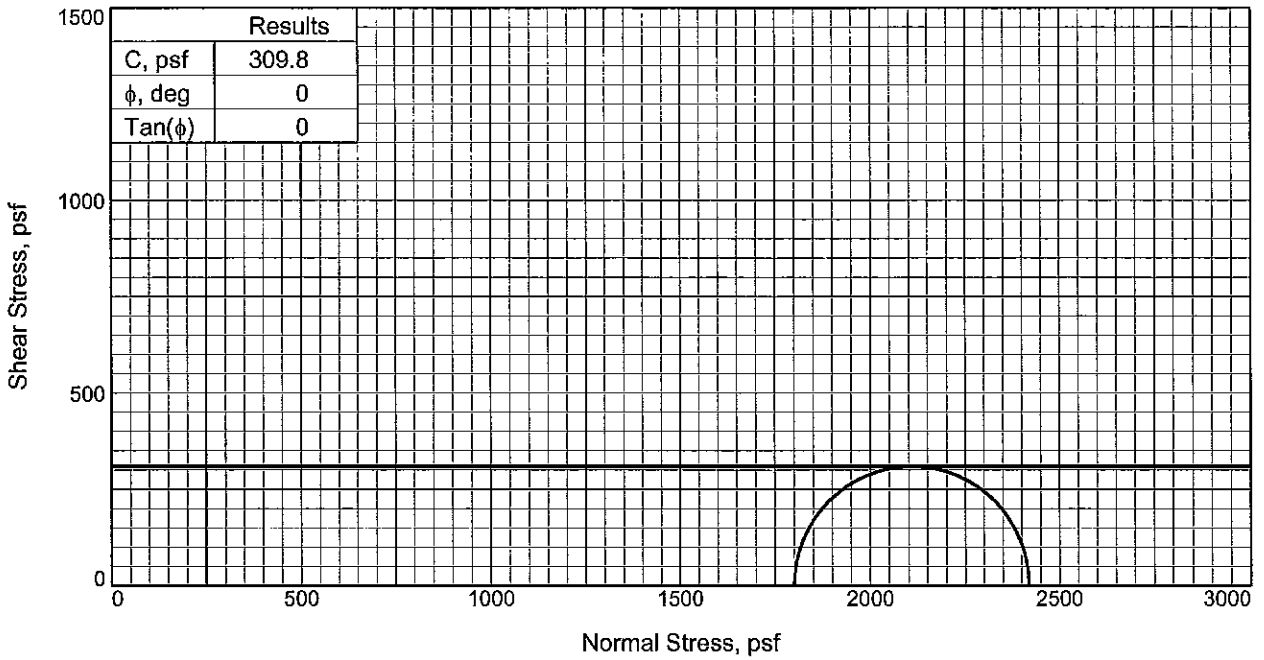
○ **Source:** B-9 **Sample No.:** 18 **Elev./Depth:** 34-36

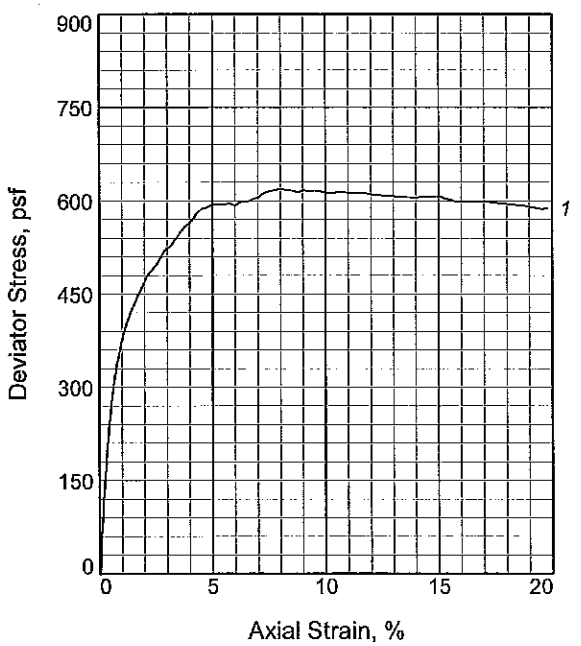
Remarks:

○ F.M.=0.00

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	55.2
	Dry Density, pcf	66.3
	Saturation, %	94.4
	Void Ratio	1.6373
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	55.2
	Dry Density, pcf	66.3
	Saturation, %	94.4
	Void Ratio	1.6373
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		12.500
Fail. Stress, psf		619.6
Strain, %		8.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2419.6
σ_3 Failure, psf		1800.0

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: SO G CL W/ SI STRKS, CH

LL= 86 **PL=** 34 **PI=** 52
Assumed Specific Gravity= 2.80
Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 36-38
Sample Number: 19
Proj. No.: B09-012 **Date Sampled:** 3/19/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	73.3	26.7

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○			0.0337	0.0136	0.0112	0.0059	0.0014			

MATERIAL DESCRIPTION	USCS	AASHTO
○ G SI W/CL, ML		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

○ **Source:** B-9 **Sample No.:** 20 **Elev./Depth:** 38-40

Remarks:

○

Particle Size Distribution Report

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	73.3	26.7

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○			0.0337	0.0136	0.0112	0.0059	0.0014			

MATERIAL DESCRIPTION	USCS	AASHTO
○ G SI W/CL, ML		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

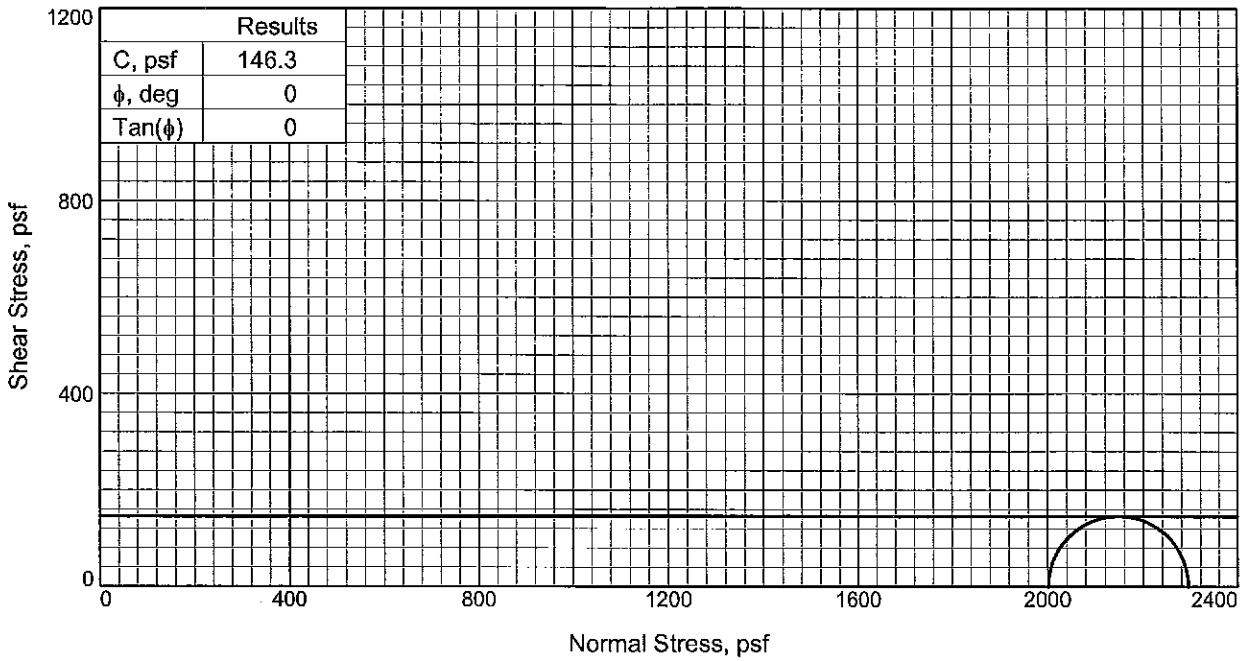
○ **Source:** B-9 **Sample No.:** 20 **Elev./Depth:** 38-40

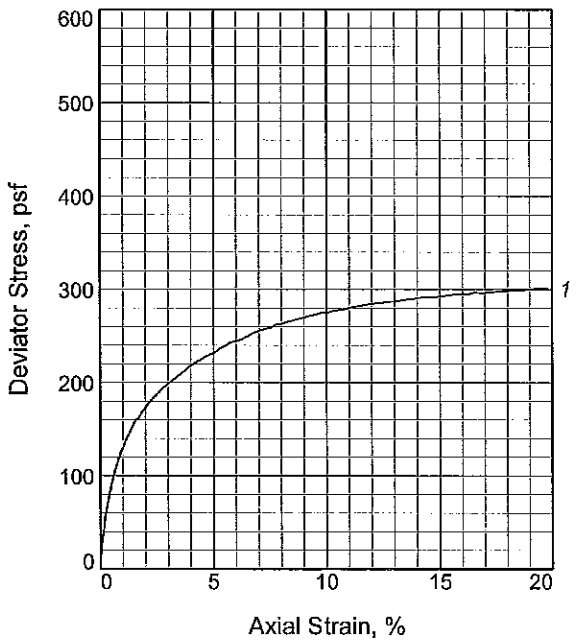
Remarks:

○

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	63.4
	Dry Density, pcf	63.6
	Saturation, %	101.6
	Void Ratio	1.7476
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	63.4
	Dry Density, pcf	63.6
	Saturation, %	101.6
	Void Ratio	1.7476
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		13.900
Fail. Stress, psf		292.7
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2294.3
σ_3 Failure, psf		2001.6

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ TR SI, CH

Assumed Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 40-42

Sample Number: 21

Proj. No.: B09-012 **Date Sampled:** 3/19/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report

	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	35.3	64.7

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○			0.0171	0.0038	0.0025					

MATERIAL DESCRIPTION	USCS	AASHTO
○ G CL W/SI PKTS		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

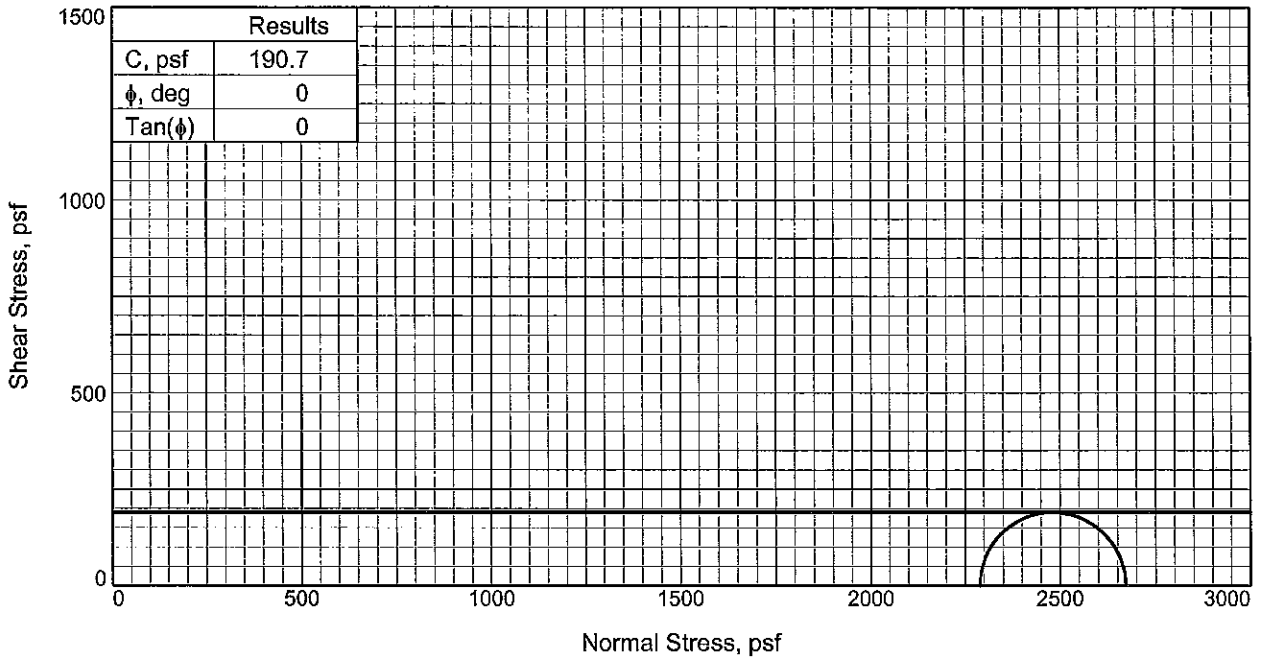
○ **Source:** B-9 **Sample No.:** 23 **Elev./Depth:** 44-46

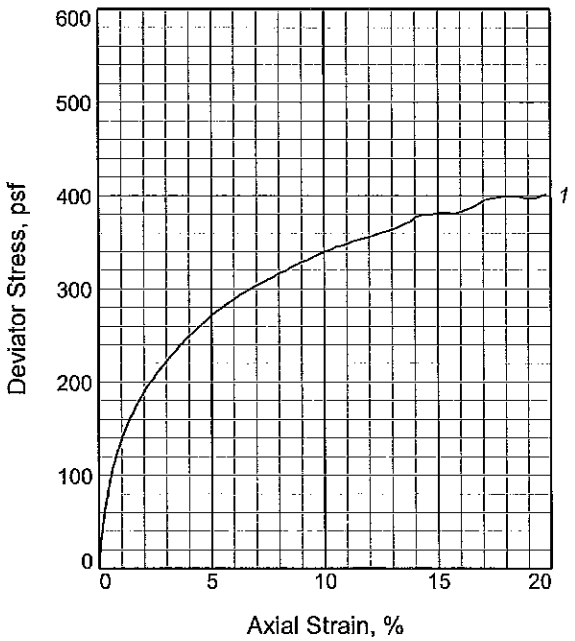
Remarks:

○

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	57.3
	Dry Density, pcf	67.2
	Saturation, %	100.3
	Void Ratio	1.6006
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	57.3
	Dry Density, pcf	67.2
	Saturation, %	100.3
	Void Ratio	1.6006
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		15.900
Fail. Stress, psf		381.4
Strain, %		15.1
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		2671.0
σ_3 Failure, psf		2289.6

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ SI PKTS, CH

LL= 52 **PL=** 21 **PI=** 31

Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 46-48

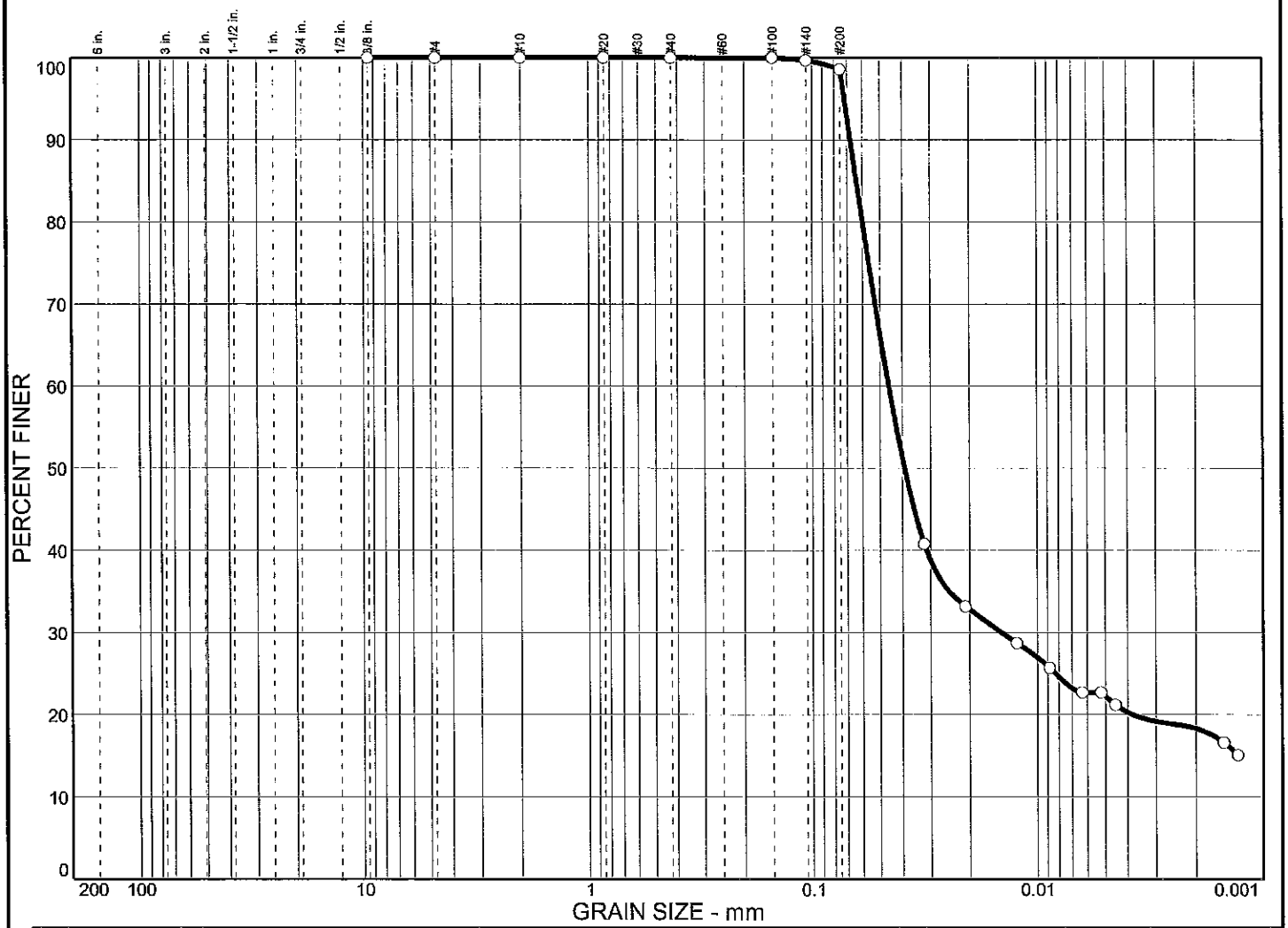
Sample Number: 24

Proj. No.: B09-012 **Date Sampled:** 3/19/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	1.4	76.3	22.3

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○			0.0636	0.0459	0.0391	0.0144				

MATERIAL DESCRIPTION	USCS	AASHTO
○ SACLSI, ML		

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

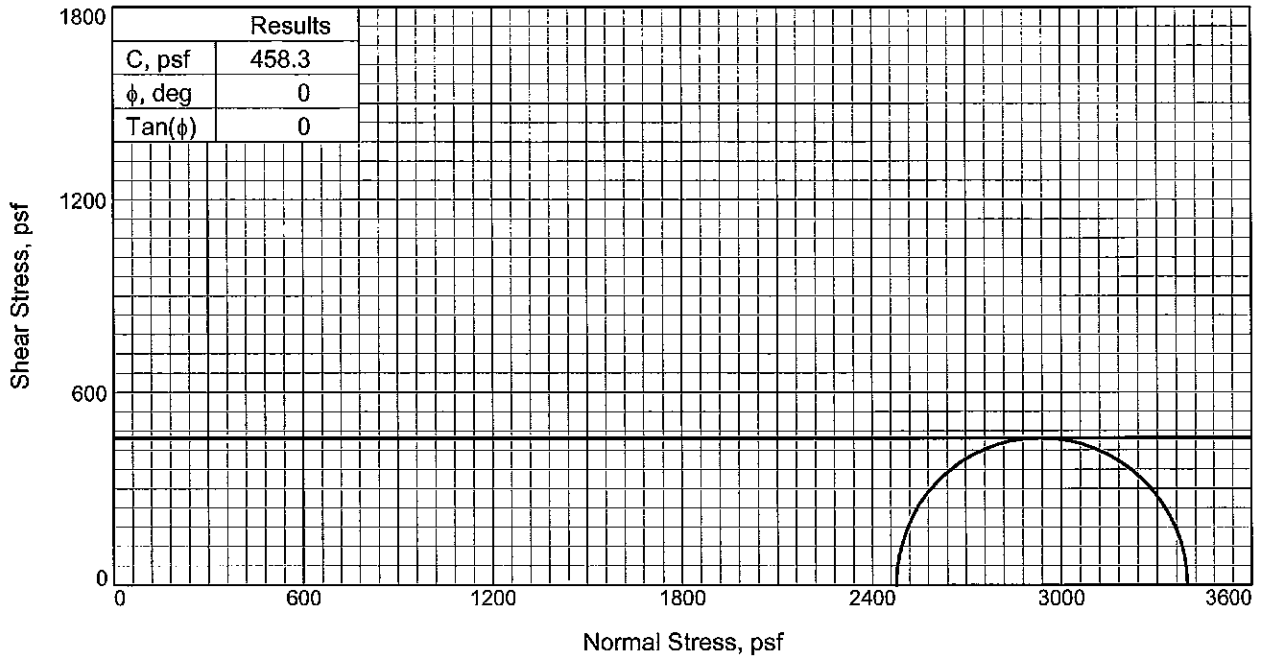
○ **Source:** B-9 **Sample No.:** 25 **Elev./Depth:** 48-50

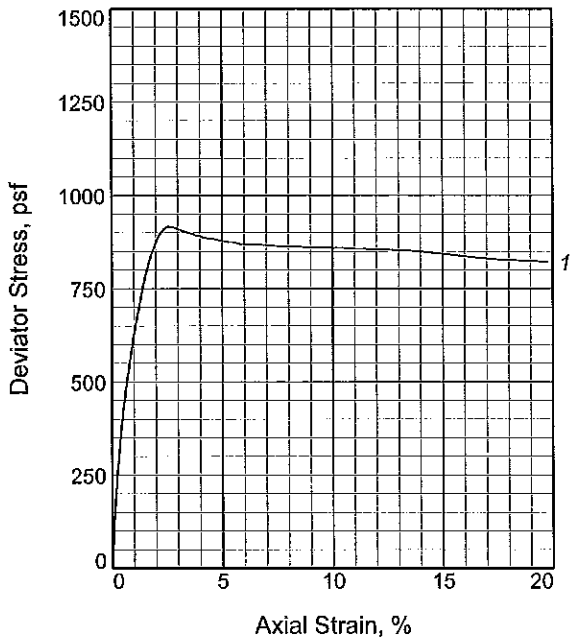
Remarks:

○

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	43.0
	Dry Density, pcf	76.1
	Saturation, %	92.8
	Void Ratio	1.2971
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	43.0
	Dry Density, pcf	76.1
	Saturation, %	92.8
	Void Ratio	1.2971
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		17.200
Fail. Stress, psf		916.7
Strain, %		2.6
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3393.5
σ_3 Failure, psf		2476.8

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: MED G CL W/ SI PKTS, CH

LL= 56 **PL=** 26 **PI=** 30

Assumed Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE & 40° SHEAR

ASTM D2850

Client: URS

Project: BAYOU DUPONT

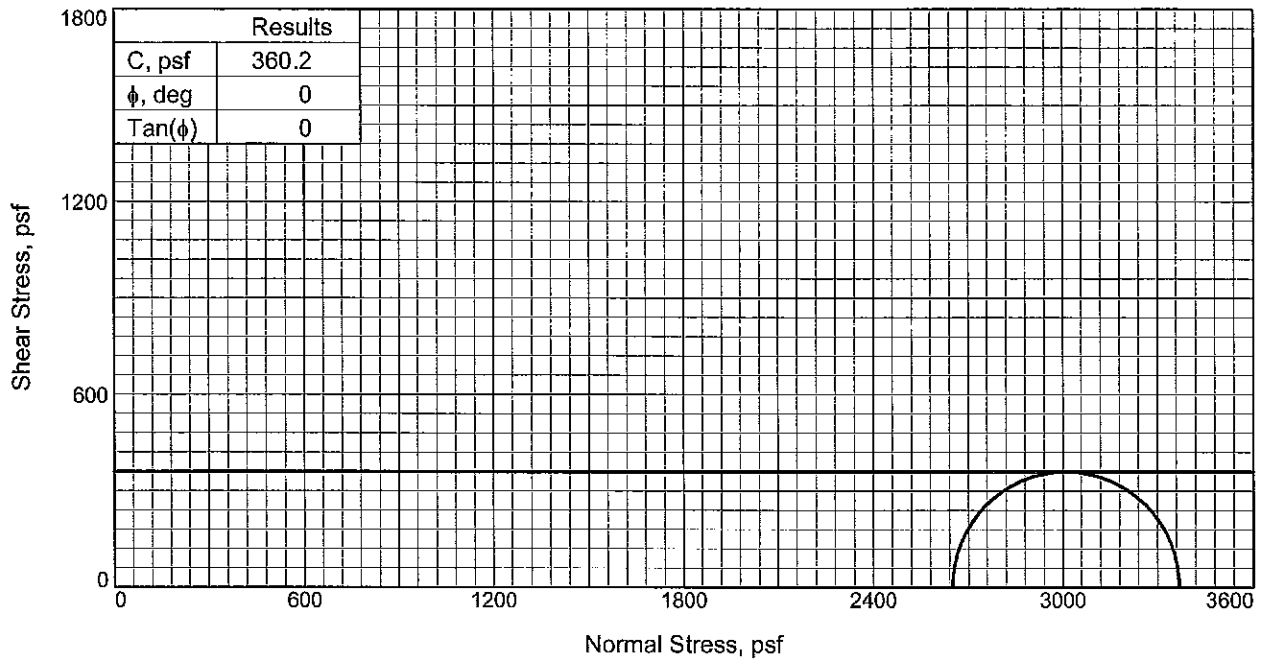
Source of Sample: B-9 **Depth:** 50-52

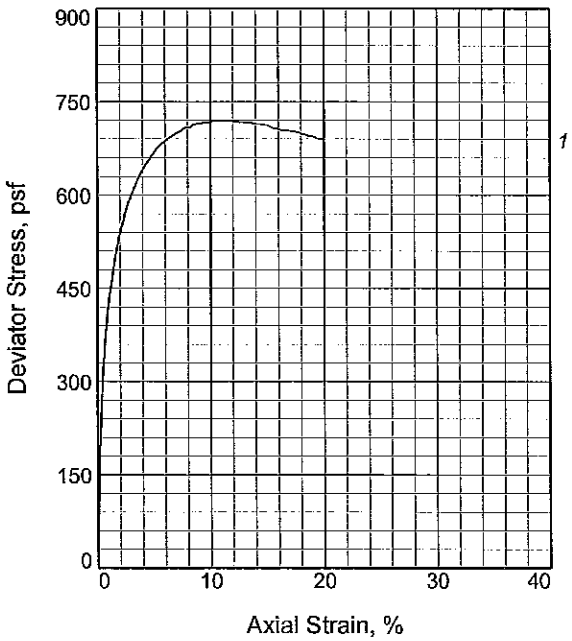
Sample Number: 26

Proj. No.: B09-012 **Date Sampled:** 3/19/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	59.0
	Dry Density, pcf	66.5
	Saturation, %	101.4
	Void Ratio	1.6296
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	59.0
	Dry Density, pcf	66.5
	Saturation, %	101.4
	Void Ratio	1.6296
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		18.400
Fail. Stress, psf		720.4
Strain, %		10.5
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3370.0
σ_3 Failure, psf		2649.6

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: SO G CL W/ SI, CH

LL= 76 **PL=** 27 **PI=** 49

Assumed Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 54-56

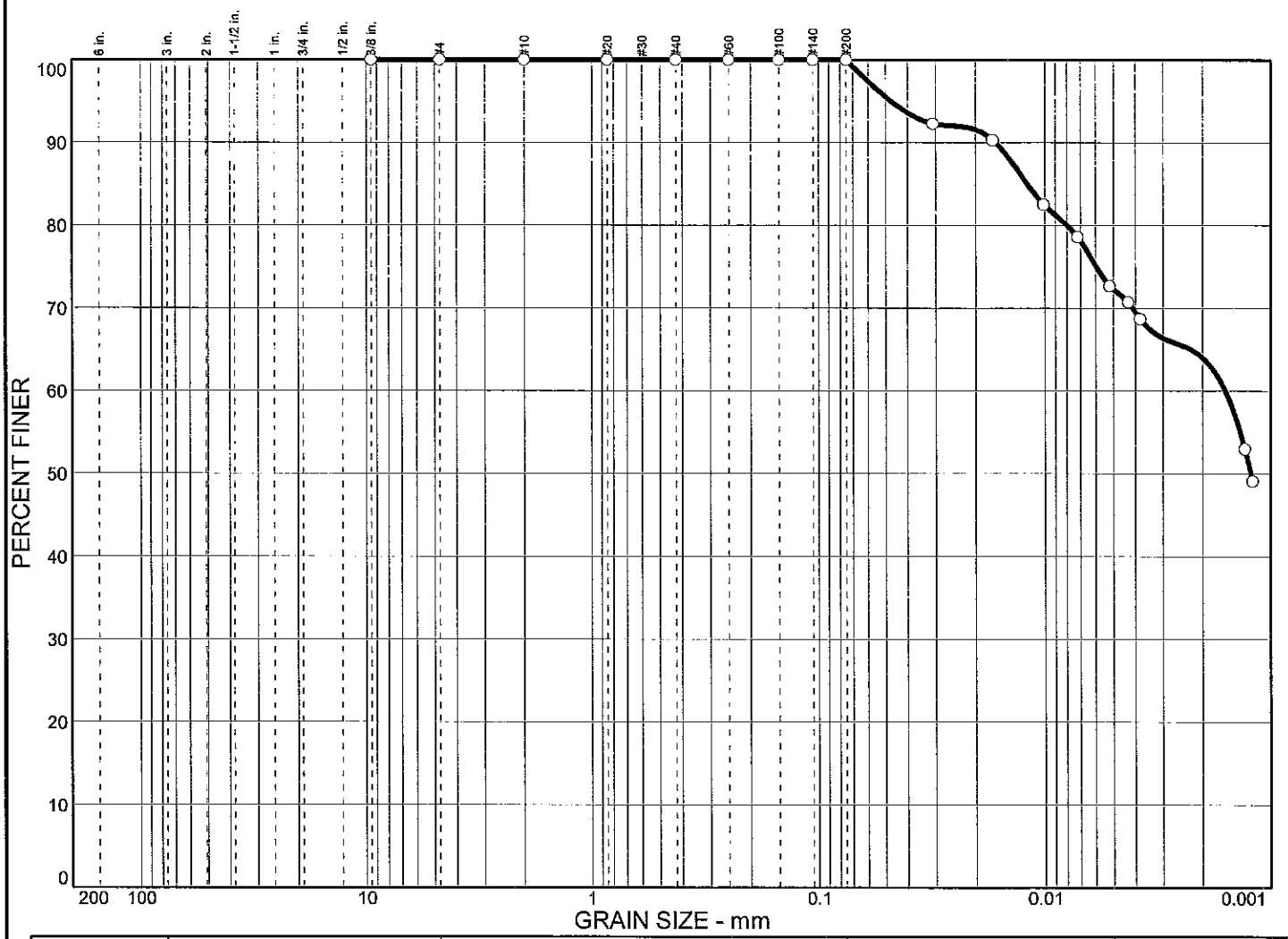
Sample Number: 28

Proj. No.: B09-012 **Date Sampled:** 3/19/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

Particle Size Distribution Report



	% COBBLES	% GRAVEL	% SAND	% SILT	% CLAY
○	0.0	0.0	0.0	27.7	72.3

	LL	PL	D_{85}	D_{60}	D_{50}	D_{30}	D_{15}	D_{10}	C_c	C_u
○	76		0.0119	0.0016						

MATERIAL DESCRIPTION	USCS	AASHTO
○ SO G CL W/ SI, CH	(CH)	

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

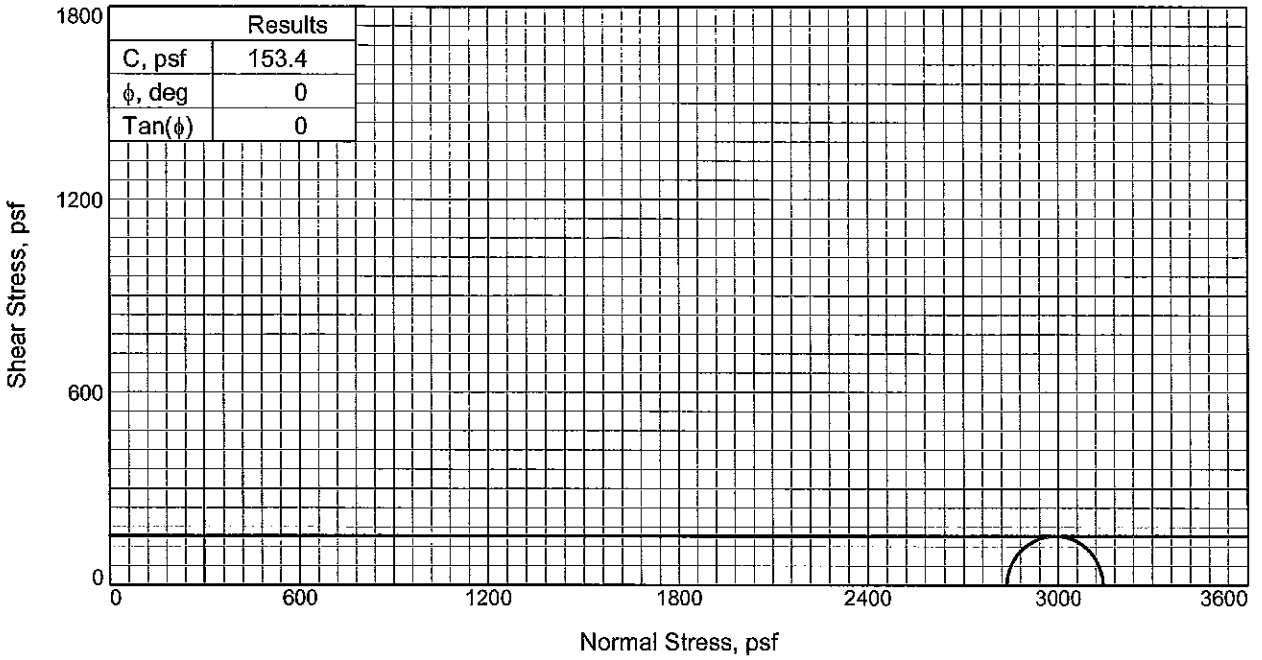
○ **Source:** B-9 **Sample No.:** 28 **Elev./Depth:** 54-56

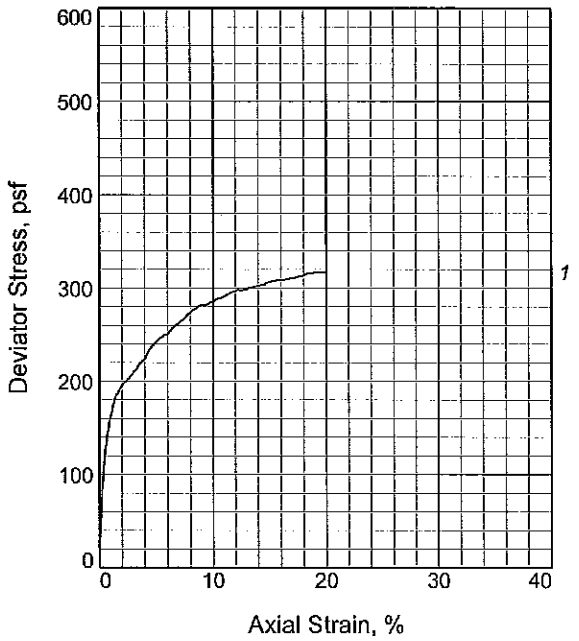
Remarks:

○

Particle Size Distribution Report

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	57.4
	Dry Density, pcf	65.6
	Saturation, %	96.6
	Void Ratio	1.6629
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	57.4
	Dry Density, pcf	65.6
	Saturation, %	96.6
	Void Ratio	1.6629
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		19.700
Fail. Stress, psf		306.7
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3143.5
σ_3 Failure, psf		2836.8

Type of Test:
Unconsolidated Undrained
Sample Type: UNDISTURBED
Description: VSO G CL W/ TR SI, CH

LL= 69 **PL=** 26 **PI=** 43
Assumed Specific Gravity= 2.80
Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

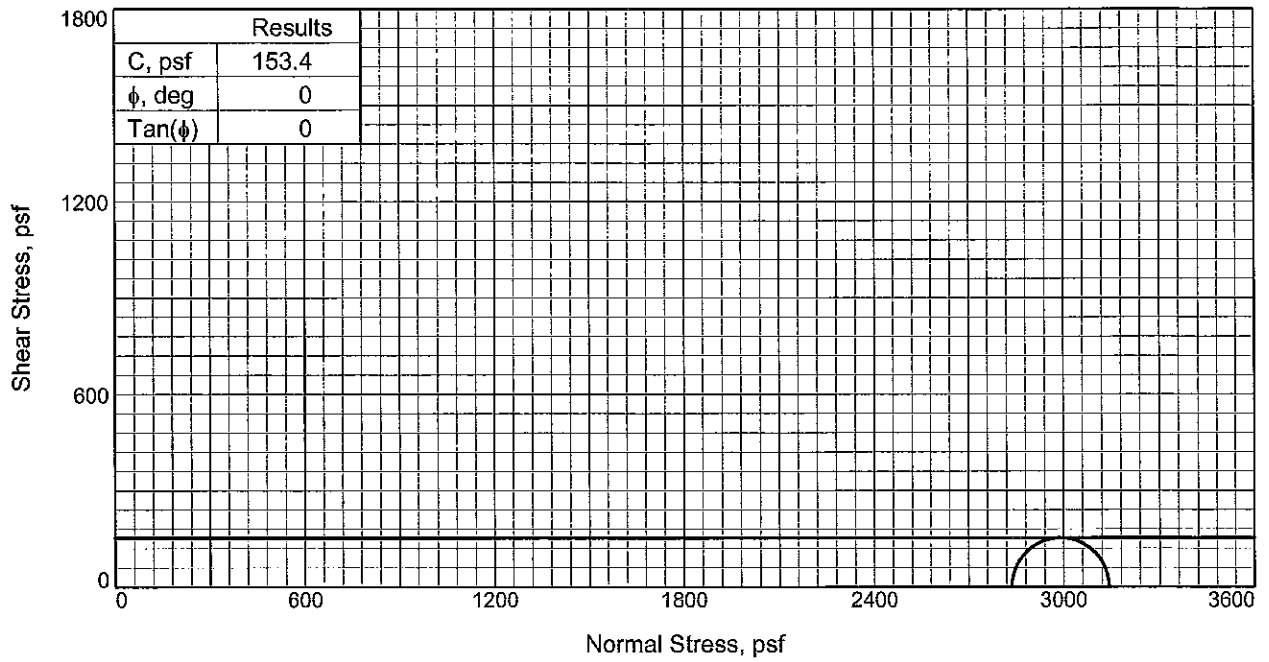
Client: URS

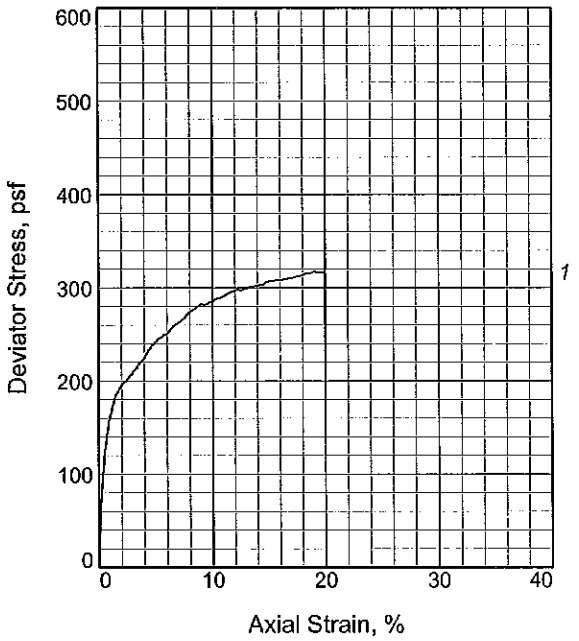
Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 58-60
Sample Number: 30
Proj. No.: B09-012 **Date Sampled:** 3/19/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.





Sample No.		1
Initial	Water Content, %	57.4
	Dry Density, pcf	65.6
	Saturation, %	96.6
	Void Ratio	1.6629
	Diameter, in.	2.850
	Height, in.	5.940
At Test	Water Content, %	57.4
	Dry Density, pcf	65.6
	Saturation, %	96.6
	Void Ratio	1.6629
	Diameter, in.	2.850
	Height, in.	5.940
Strain rate, %/min.		1.00
Back Pressure, psi		0.000
Cell Pressure, psi		19.700
Fail. Stress, psf		306.7
Strain, %		15.0
Ult. Stress, psf		
Strain, %		
σ_1 Failure, psf		3143.5
σ_3 Failure, psf		2836.8

Type of Test:
Unconsolidated Undrained

Sample Type: UNDISTURBED

Description: VSO G CL W/ TR SI, CH

LL= 69 **PL=** 26 **PI=** 43

Assumed Specific Gravity= 2.80

Remarks: TYPE OF FAILURE: BULGE

ASTM D2850

Client: URS

Project: BAYOU DUPONT

Source of Sample: B-9 **Depth:** 58-60

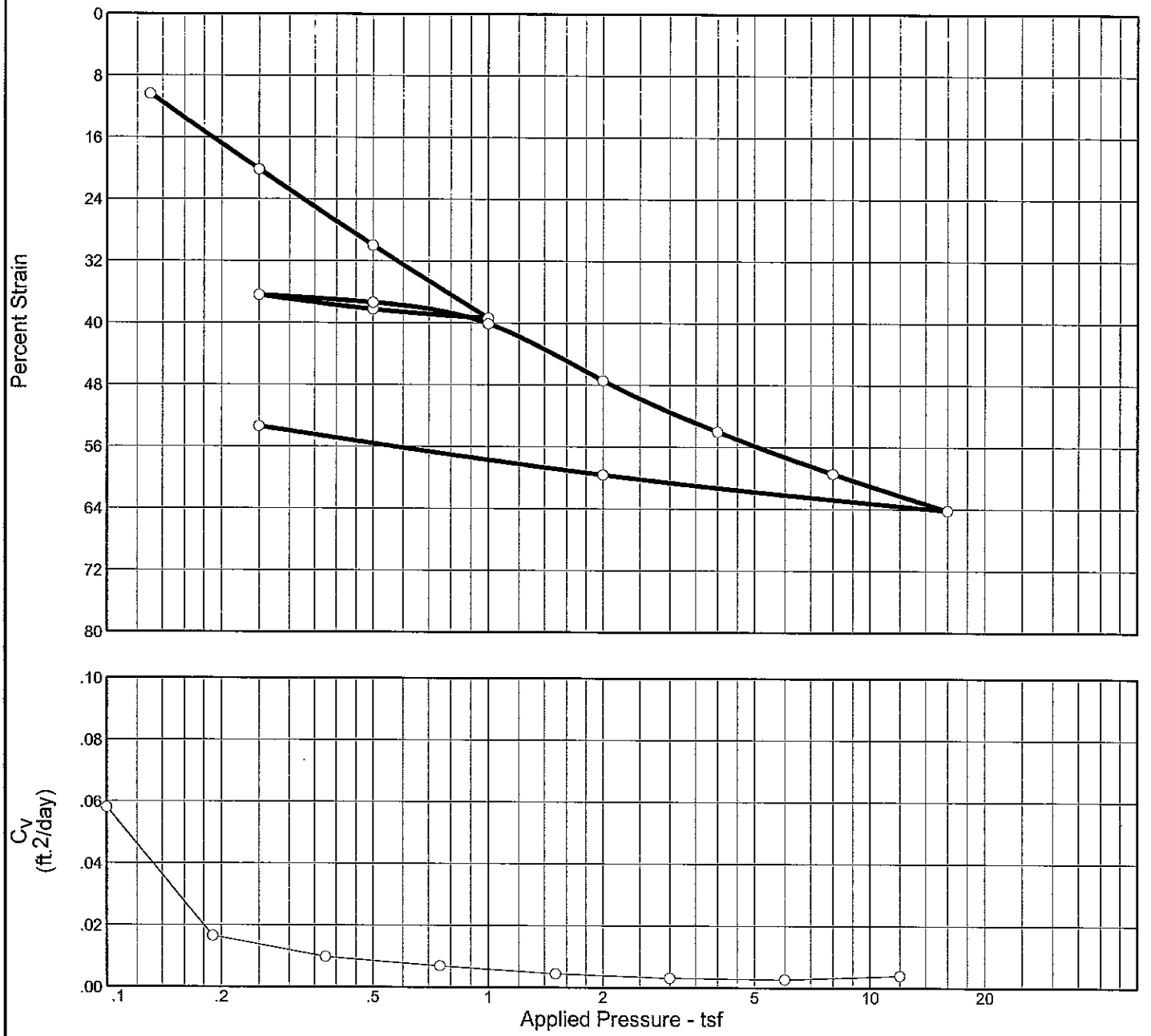
Sample Number: 30

Proj. No.: B09-012 **Date Sampled:** 3/19/09

TRIAXIAL SHEAR TEST REPORT

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
97.0 %	264.1 %	19.9	257	173	2.40	(PT)		6.534

MATERIAL DESCRIPTION

VSO PEAT W/ CL & ORGS, PT

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-9 **Sample No.:** 2 **Elev./Depth:** 2-4

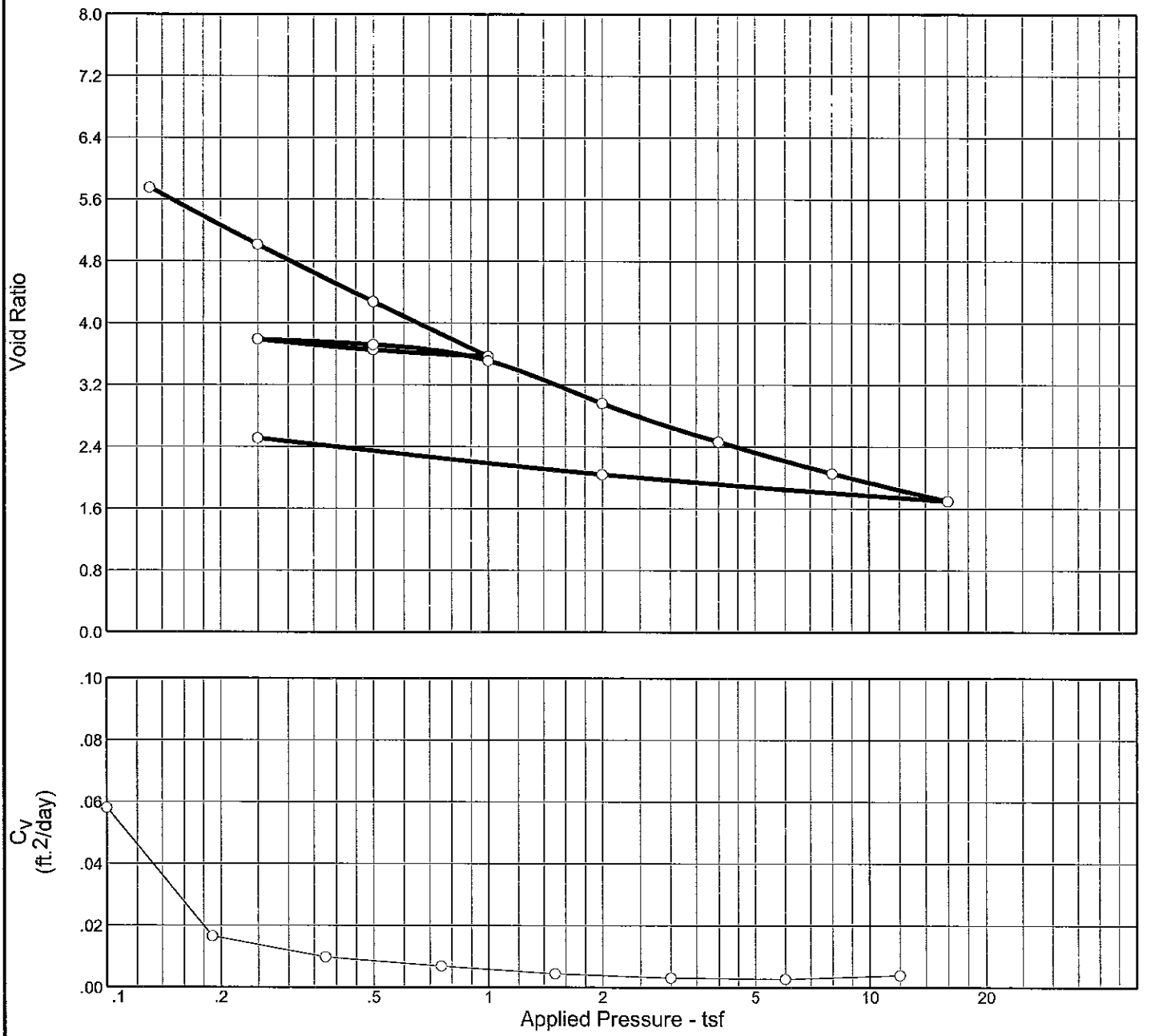
CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

Remarks:

ASTM D2435

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
97.0 %	264.1 %	19.9	257	173	2.40	(PT)		6.534

MATERIAL DESCRIPTION

VSO PEAT W/ CL & ORGS, PT

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-9 **Sample No.:** 2 **Elev./Depth:** 2-4

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

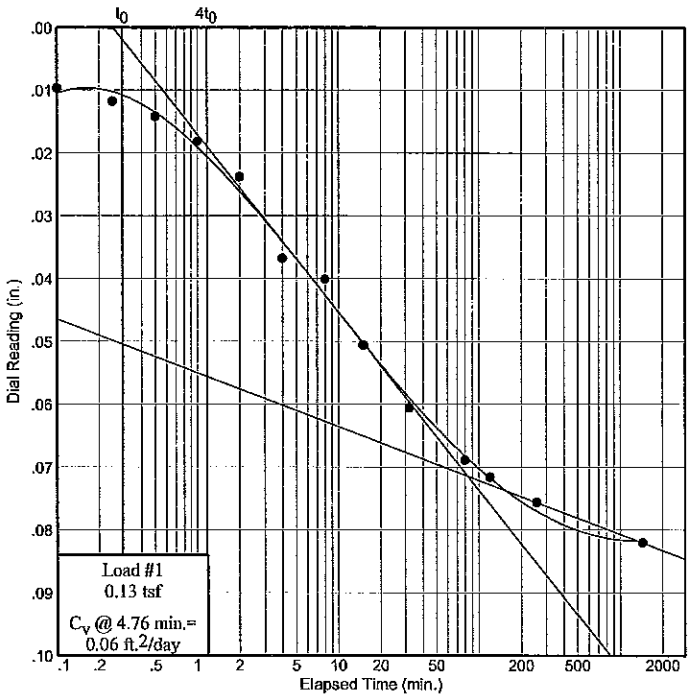
Remarks:

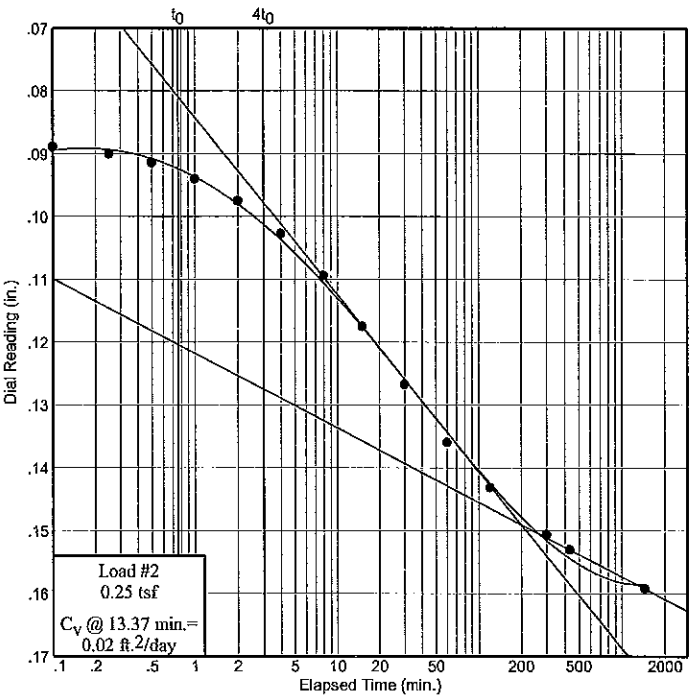
ASTM D2435

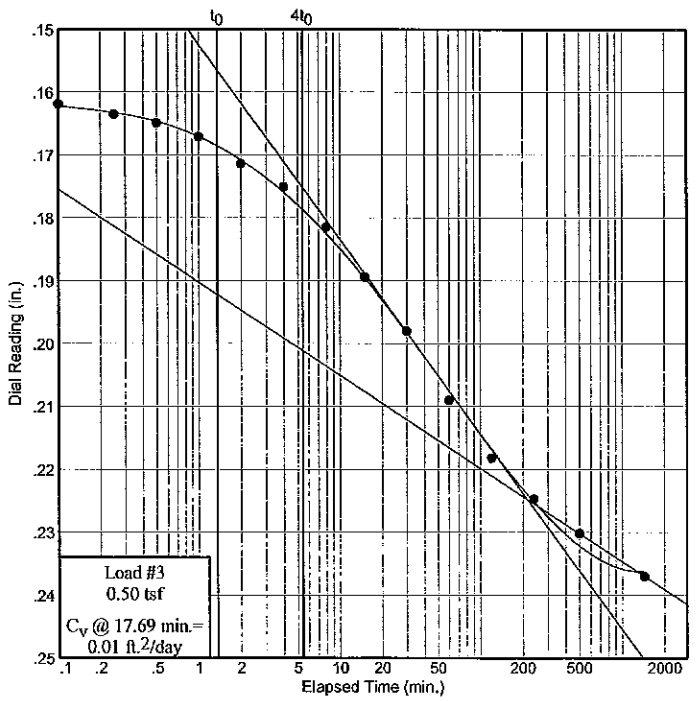
Dial Reading vs. Time

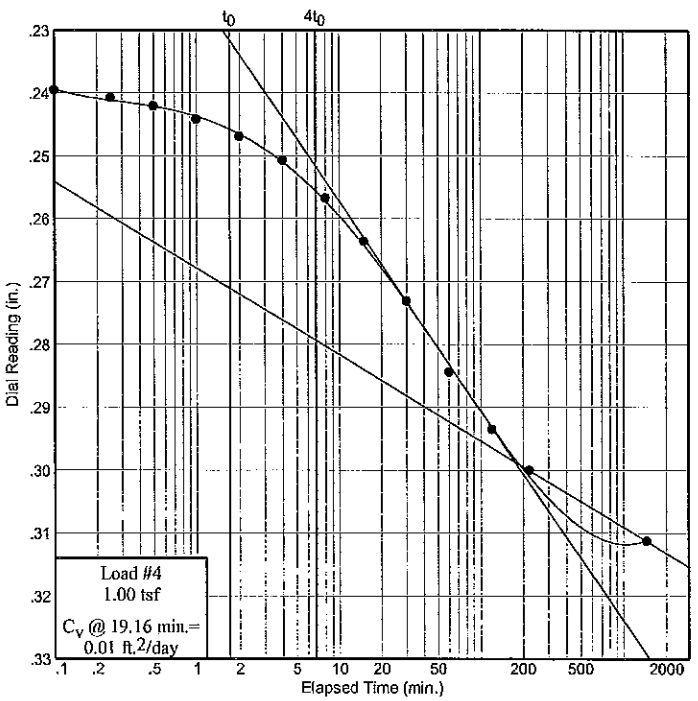
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-9 Sample No.: 2 Elev./Depth: 2-4









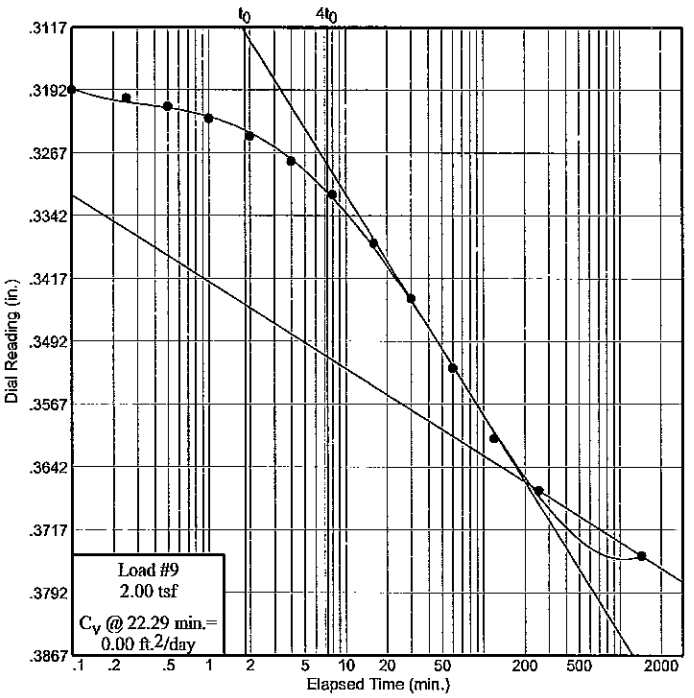
Dial Reading vs. Time

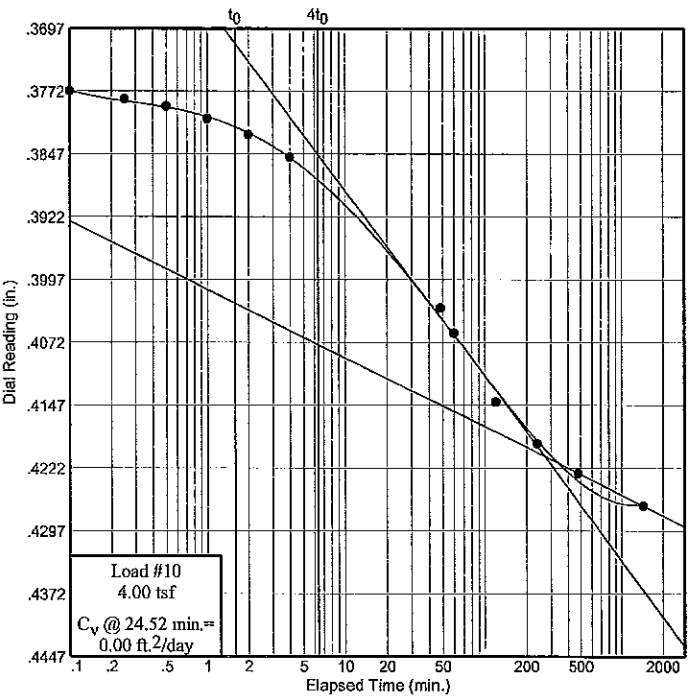
Southern Earth Sciences, Inc.

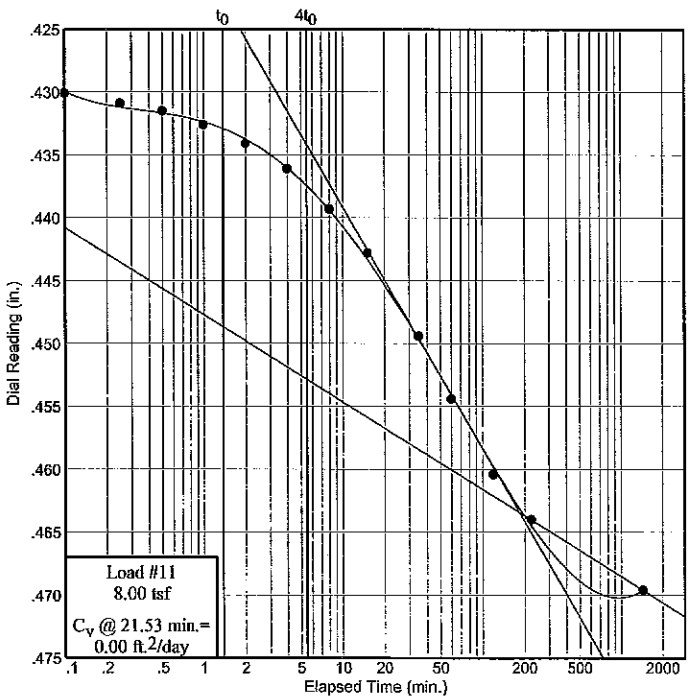
Dial Reading vs. Time

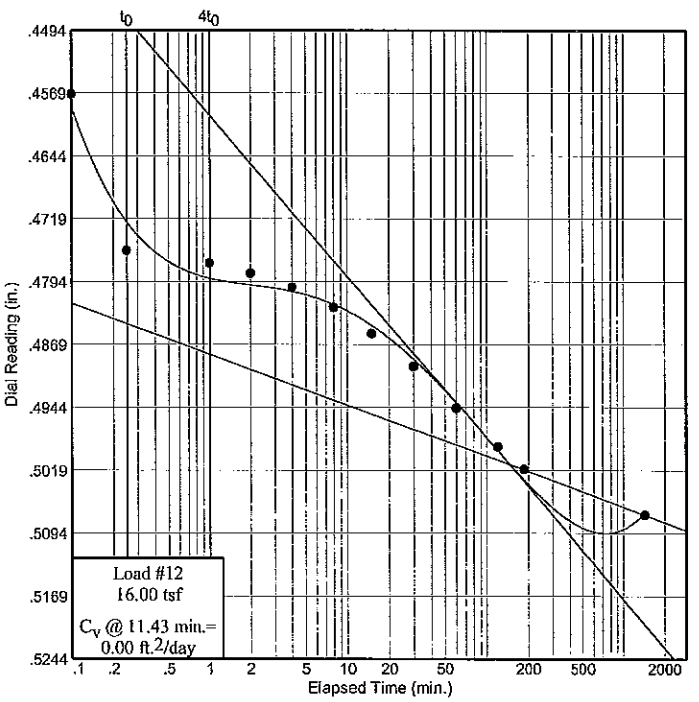
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-9 Sample No.: 2 Elev./Depth: 2-4









Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-9
Sample No.: 2
Elev. or Depth: 2-4 **Sample Length(in./cm.):**
Location:
Description: VSO PEAT W/ CL & ORGS, PT
Liquid Limit: 257 **Plasticity Index:** 173
USCS: (PT) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST	AFTER TEST
Wet w+t =	185.63 g.	**Consolidometer # =** 1	**Wet w+t =** 207.04 g.
Dry w+t =	171.08 g.		**Dry w+t =** 190.74 g.
Tare Wt. =	165.57 g.	**Spec. Gravity =** 2.40	**Tare Wt. =** 168.97 g.
Height =	.79 in.	**Height =** .79 in.	
Diameter =	2.50 in.	**Diameter =** 2.50 in.	
Weight =	73.70 g.	**Defl. Table =** Mobile Cons #2	
Moisture =	264.1 %	**Ht. Solids =** 0.1049 in.	**Moisture =** 74.9 %
Wet Den. =	72.4 pcf	**Dry Wt. =** 20.24 g.*	**Dry Wt. =** 21.77 g.
Dry Den. =	19.9 pcf	**Void Ratio =** 6.534	**Void Ratio =** 2.510
		Saturation = 97.0 %	

*** Initial dry weight used in calculations**

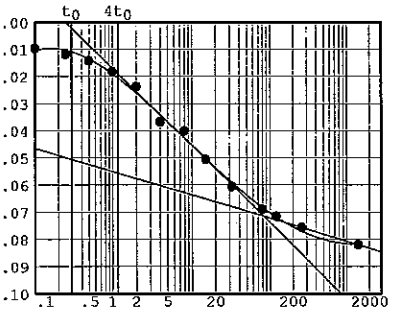
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				6.534	
0.13	0.08200	0.00000	0.06	0.011	5.752	10.4 Comprs.
0.25	0.15930	0.00010	0.02	0.017	5.016	20.2 Comprs.
0.50	0.23730	0.00030	0.01	0.023	4.274	30.0 Comprs.
1.00	0.31190	0.00070	0.01	0.025	3.566	39.4 Comprs.
0.50	0.30300	0.00070	0.02		3.651	38.3 Comprs.
0.25	0.28830	0.00050	0.01		3.789	36.4 Comprs.
0.50	0.29600	0.00070	0.02	0.002	3.718	37.4 Comprs.
1.00	0.31790	0.00100	0.02	0.010	3.512	40.1 Comprs.
2.00	0.37590	0.00110	0.00	0.022	2.960	47.4 Comprs.
4.00	0.42830	0.00160	0.00	0.020	2.465	54.0 Comprs.
8.00	0.47200	0.00240	0.00	0.019	2.056	59.4 Comprs.
16.00	0.50720	0.00000	0.00	0.019	1.697	64.2 Comprs.
2.00	0.47250	0.00140	0.00		2.041	59.6 Comprs.
0.25	0.42240	0.00050	0.00		2.510	53.4 Comprs.

C_c = 1.18 P_c = 0.38 tsf C_r = 0.46

Pressure: 0.13 tsf **TEST READINGS** **Load No. 1**

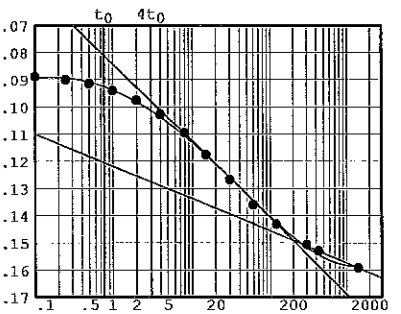
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	80.00	0.06890
2	0.10	0.00970	12	120.00	0.07160
3	0.25	0.01180	13	257.00	0.07560
4	0.50	0.01420	14	1440.00	0.08200
5	1.00	0.01820			
6	2.00	0.02380			
7	4.00	0.03680			
8	8.00	0.04010			
9	15.00	0.05060			
10	32.00	0.06060			



Void Ratio = 5.752 **Compression** = 10.4 %
D_0 = 0.00102 D_{50} = 0.03622 D_{100} = 0.07143
C_v **at 4.8 min.** = 0.06 ft.^{2}/day C_α = 0.011

Pressure: 0.25 tsf **TEST READINGS** **Load No. 2**

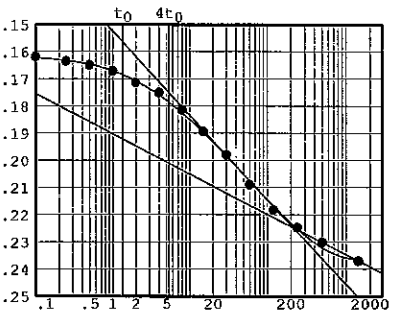
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.08200	11	60.00	0.13600
2	0.10	0.08900	12	120.00	0.14320
3	0.25	0.09010	13	300.00	0.15070
4	0.50	0.09150	14	432.00	0.15310
5	1.00	0.09410	15	1440.00	0.15930
6	2.00	0.09760			
7	4.00	0.10280			
8	8.00	0.10950			
9	15.00	0.11760			
10	30.00	0.12680			



Void Ratio = 5.016 **Compression** = 20.2 %
D_0 = 0.08342 D_{50} = 0.11622 D_{100} = 0.14901
C_v **at 13.4 min.** = 0.02 ft.^{2}/day C_α = 0.017

Pressure: 0.50 tsf **TEST READINGS** **Load No. 3**

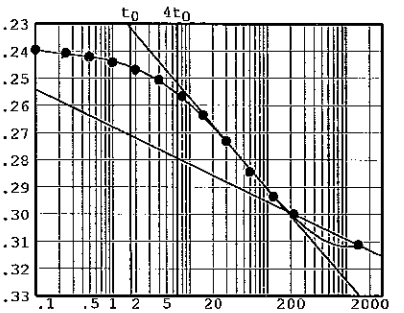
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.15930	11	60.00	0.20930
2	0.10	0.16220	12	120.00	0.21850
3	0.25	0.16380	13	240.00	0.22500
4	0.50	0.16520	14	500.00	0.23050
5	1.00	0.16740	15	1440.00	0.23730
6	2.00	0.17170			
7	4.00	0.17540			
8	8.00	0.18180			
9	15.00	0.18970			
10	30.00	0.19830			



Void Ratio = 4.274 **Compression =** 30.0 %
D_0 = 0.15836 **D_{50} =** 0.19157 **D_{100} =** 0.22478
C_v at 17.7 min. = 0.01 ft.^{2}/day **C_α =** 0.023

Pressure: 1.00 tsf **TEST READINGS** **Load No. 4**

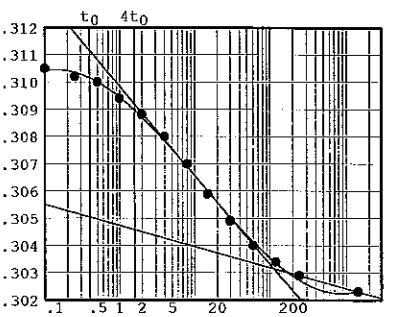
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.23730	11	60.00	0.28510
2	0.10	0.24020	12	120.00	0.29420
3	0.25	0.24140	13	220.00	0.30070
4	0.50	0.24280	14	1440.00	0.31190
5	1.00	0.24490			
6	2.00	0.24760			
7	4.00	0.25140			
8	8.00	0.25740			
9	15.00	0.26430			
10	30.00	0.27380			



Void Ratio = 3.566 **Compression =** 39.4 %
D_0 = 0.23590 **D_{50} =** 0.26726 **D_{100} =** 0.29861
C_v at 19.2 min. = 0.01 ft.^{2}/day **C_α =** 0.025

Pressure: 0.50 tsf **TEST READINGS** **Load No. 5**

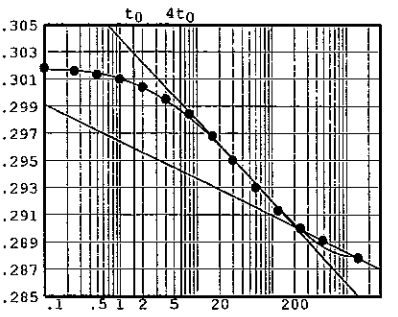
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.31190	11	60.00	0.30470
2	0.10	0.31120	12	120.00	0.30410
3	0.25	0.31090	13	240.00	0.30360
4	0.50	0.31070	14	1440.00	0.30300
5	1.00	0.31010			
6	2.00	0.30950			
7	4.00	0.30870			
8	8.00	0.30770			
9	15.00	0.30660			
10	30.00	0.30560			



Void Ratio = 3.651 **Compression =** 38.3 %
D_0 = 0.31133 **D_{50} =** 0.30724 **D_{100} =** 0.30315
C_v at 6.2 min. = 0.02 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 6**

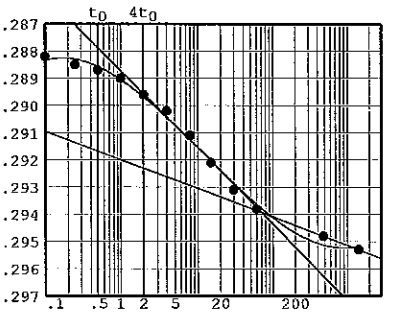
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.30300	11	60.00	0.29350
2	0.10	0.30230	12	120.00	0.29180
3	0.25	0.30210	13	240.00	0.29050
4	0.50	0.30180	14	480.00	0.28960
5	1.00	0.30150	15	1440.00	0.28830
6	2.00	0.30090			
7	4.00	0.30000			
8	8.00	0.29890			
9	16.00	0.29730			
10	30.00	0.29550			



Void Ratio = 3.789 **Compression =** 36.4 %
D_0 = 0.30265 D_{50} = 0.29638 D_{100} = 0.29011
C_v **at 18.0 min. =** 0.01 ft.^{2}/day

Pressure: 0.50 tsf **TEST READINGS** **Load No. 7**

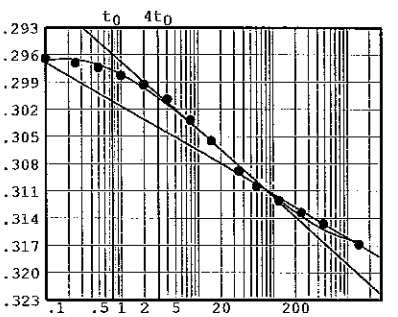
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.28830	11	60.00	0.29450
2	0.10	0.28890	12	480.00	0.29550
3	0.25	0.28920	13	1443.00	0.29600
4	0.50	0.28940			
5	1.00	0.28970			
6	2.00	0.29030			
7	4.00	0.29090			
8	8.00	0.29180			
9	15.00	0.29280			
10	30.00	0.29380			



Void Ratio = 3.718 **Compression =** 37.4 %
D_0 = 0.28744 D_{50} = 0.29069 D_{100} = 0.29393
C_v **at 4.9 min.** = 0.02 ft.^{2}/day C_α = 0.002

Pressure: 1.00 tsf **TEST READINGS** **Load No. 8**

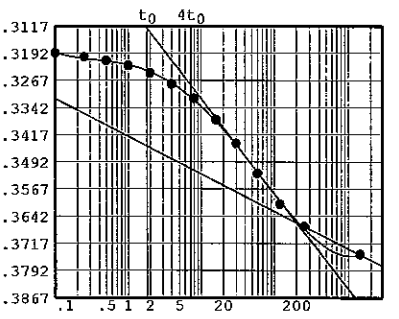
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.29600	11	60.00	0.31150
2	0.10	0.29740	12	120.00	0.31310
3	0.25	0.29790	13	240.00	0.31440
4	0.50	0.29840	14	480.00	0.31560
5	1.00	0.29930	15	1440.00	0.31790
6	2.00	0.30030			
7	4.00	0.30190			
8	8.00	0.30420			
9	15.00	0.30650			
10	35.00	0.30980			



Void Ratio = 3.512 **Compression =** 40.1 %
D_0 = 0.29464 D_{50} = 0.30270 D_{100} = 0.31077
C_v **at 6.1 min.** = 0.02 ft.^{2}/day C_α = 0.010

Pressure: 2.00 tsf **TEST READINGS** **Load No. 9**

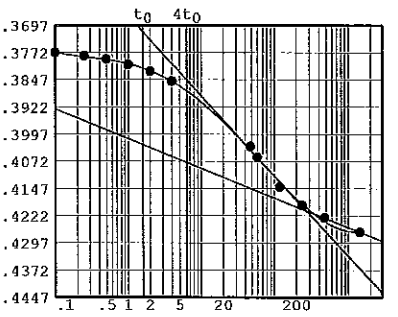
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.31790	11	60.00	0.35350
2	0.10	0.32030	12	120.00	0.36190
3	0.25	0.32130	13	254.00	0.36810
4	0.50	0.32230	14	1440.00	0.37590
5	1.00	0.32370			
6	2.00	0.32580			
7	4.00	0.32880			
8	8.00	0.33280			
9	16.00	0.33860			
10	30.00	0.34520			



Void Ratio = 2.960 **Compression** = 47.4 %
D_0 = 0.31655 D_{50} = 0.34126 D_{100} = 0.36598
C_v **at 22.3 min.** = 0.00 ft.^{2}/day C_α = 0.022

Pressure: 4.00 tsf **TEST READINGS** **Load No. 10**

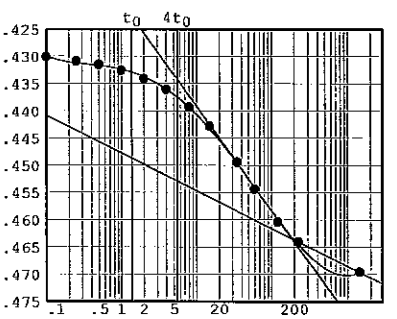
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.37590	11	240.00	0.42090
2	0.10	0.37880	12	480.00	0.42440
3	0.25	0.37970	13	1440.00	0.42830
4	0.50	0.38060			
5	1.00	0.38210			
6	2.00	0.38400			
7	4.00	0.38670			
8	48.00	0.40470			
9	60.00	0.40770			
10	120.00	0.41590			



Void Ratio = 2.465 **Compression** = 54.0 %
D_0 = 0.37514 D_{50} = 0.39797 D_{100} = 0.42079
C_v **at 24.5 min.** = 0.00 ft.^{2}/day C_α = 0.020

Pressure: 8.00 tsf **TEST READINGS** **Load No. 11**

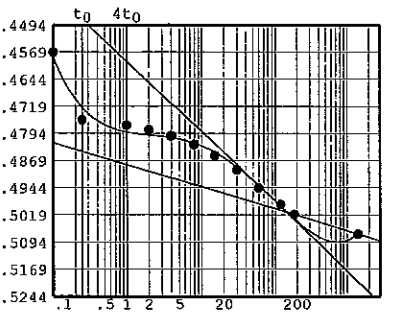
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.42830	11	60.00	0.45680
2	0.10	0.43250	12	120.00	0.46280
3	0.25	0.43330	13	224.00	0.46640
4	0.50	0.43390	14	1440.00	0.47200
5	1.00	0.43500			
6	2.00	0.43650			
7	4.00	0.43850			
8	8.00	0.44170			
9	15.00	0.44520			
10	35.00	0.45180			



Void Ratio = 2.056 **Compression** = 59.4 %
D_0 = 0.42836 D_{50} = 0.44588 D_{100} = 0.46340
C_v **at 21.5 min.** = 0.00 ft.^{2}/day C_α = 0.019

Pressure: 16.00 tsf **TEST READINGS** **Load No. 12**

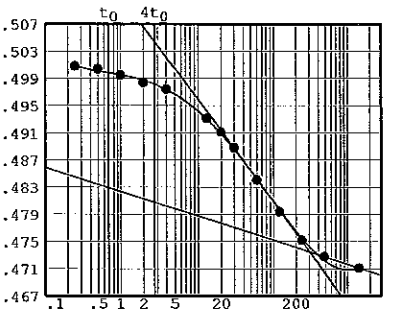
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.47200	11	120.00	0.49910
2	0.10	0.45700	12	185.00	0.50180
3	0.25	0.47570	13	1440.00	0.50720
4	1.00	0.47720			
5	2.00	0.47840			
6	4.00	0.48010			
7	8.00	0.48250			
8	15.00	0.48560			
9	30.00	0.48950			
10	60.00	0.49450			



Void Ratio = 1.697 **Compression** = 64.2 %
D_0 = 0.46557 D_{50} = 0.48337 D_{100} = 0.50117
C_v **at 11.4 min.** = 0.00 ft.^{2}/day C_α = 0.019

Pressure: 2.00 tsf **TEST READINGS** **Load No. 13**

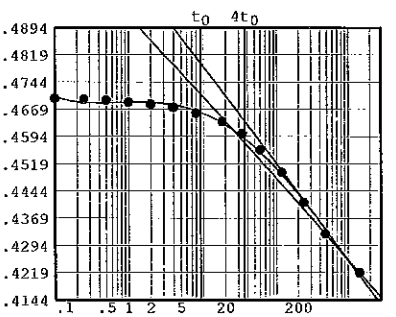
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.50720	11	120.00	0.48080
2	0.25	0.50220	12	240.00	0.47660
3	0.50	0.50180	13	480.00	0.47420
4	1.00	0.50090	14	1440.00	0.47250
5	2.00	0.49980			
6	4.00	0.49880			
7	13.00	0.49450			
8	20.00	0.49250			
9	30.00	0.49020			
10	60.00	0.48550			



Void Ratio = 2.041 **Compression** = 59.6 %
D_0 = 0.50152 D_{50} = 0.48751 D_{100} = 0.47349
C_v **at 35.9 min.** = 0.00 ft.^{2}/day

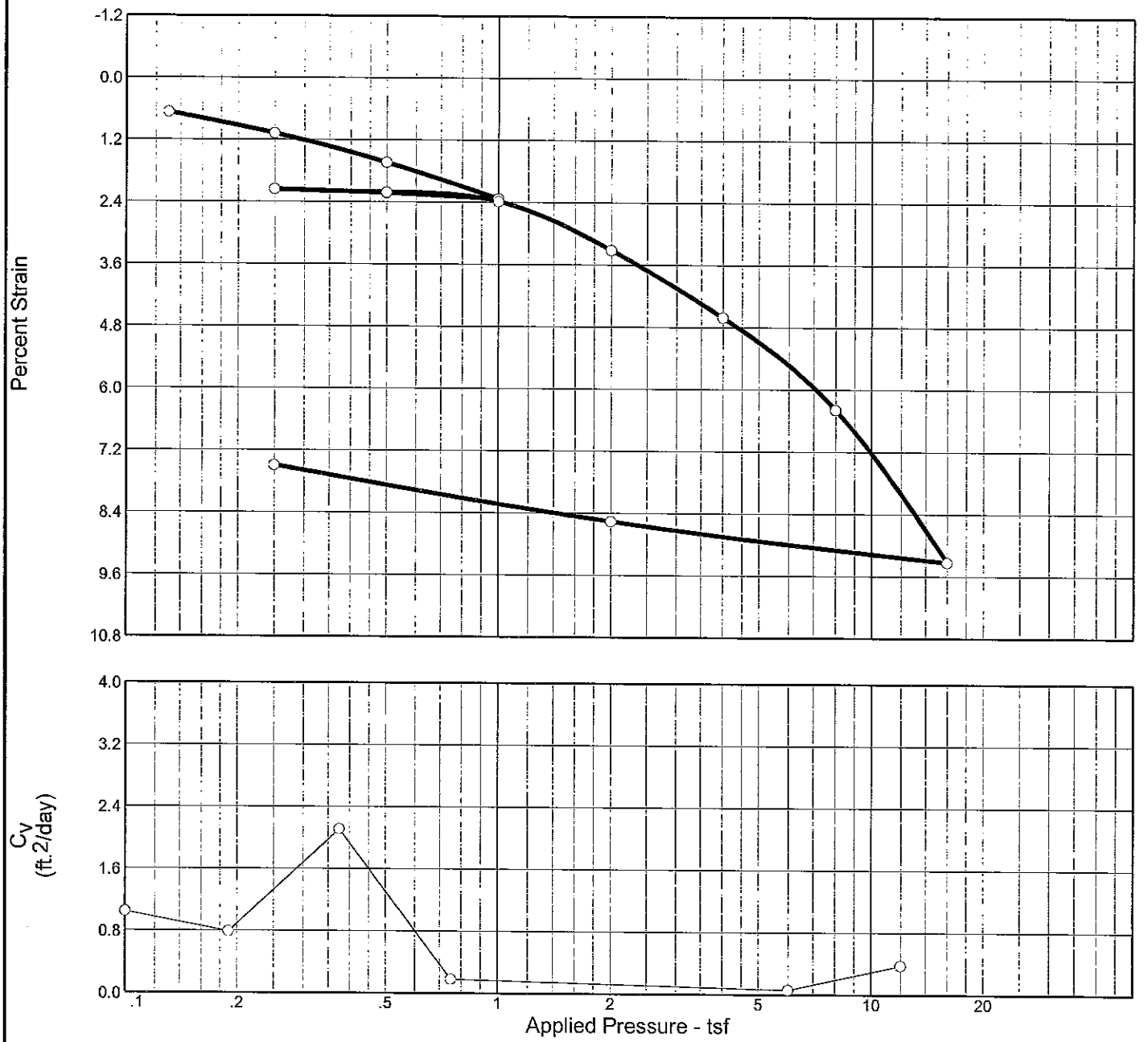
Pressure: 0.25 tsf **TEST READINGS** **Load No. 14**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.47250	11	60.00	0.45620
2	0.10	0.47040	12	120.00	0.45000
3	0.25	0.47010	13	240.00	0.44170
4	0.50	0.46980	14	480.00	0.43310
5	1.00	0.46930	15	1440.00	0.42240
6	2.00	0.46880			
7	4.00	0.46790			
8	8.00	0.46630			
9	18.00	0.46400			
10	34.00	0.46070			



Void Ratio = 2.510 **Compression** = 53.4 %
D_0 = 0.47331 D_{50} = 0.44954 D_{100} = 0.42576
C_v **at 111.8 min.** = 0.00 ft.^{2}/day

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
100.5 %	30.8 %	91.4	NP	NP	2.65	(ML)		0.811

MATERIAL DESCRIPTION

FM G SI W/ TR F SA & CL, ML

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

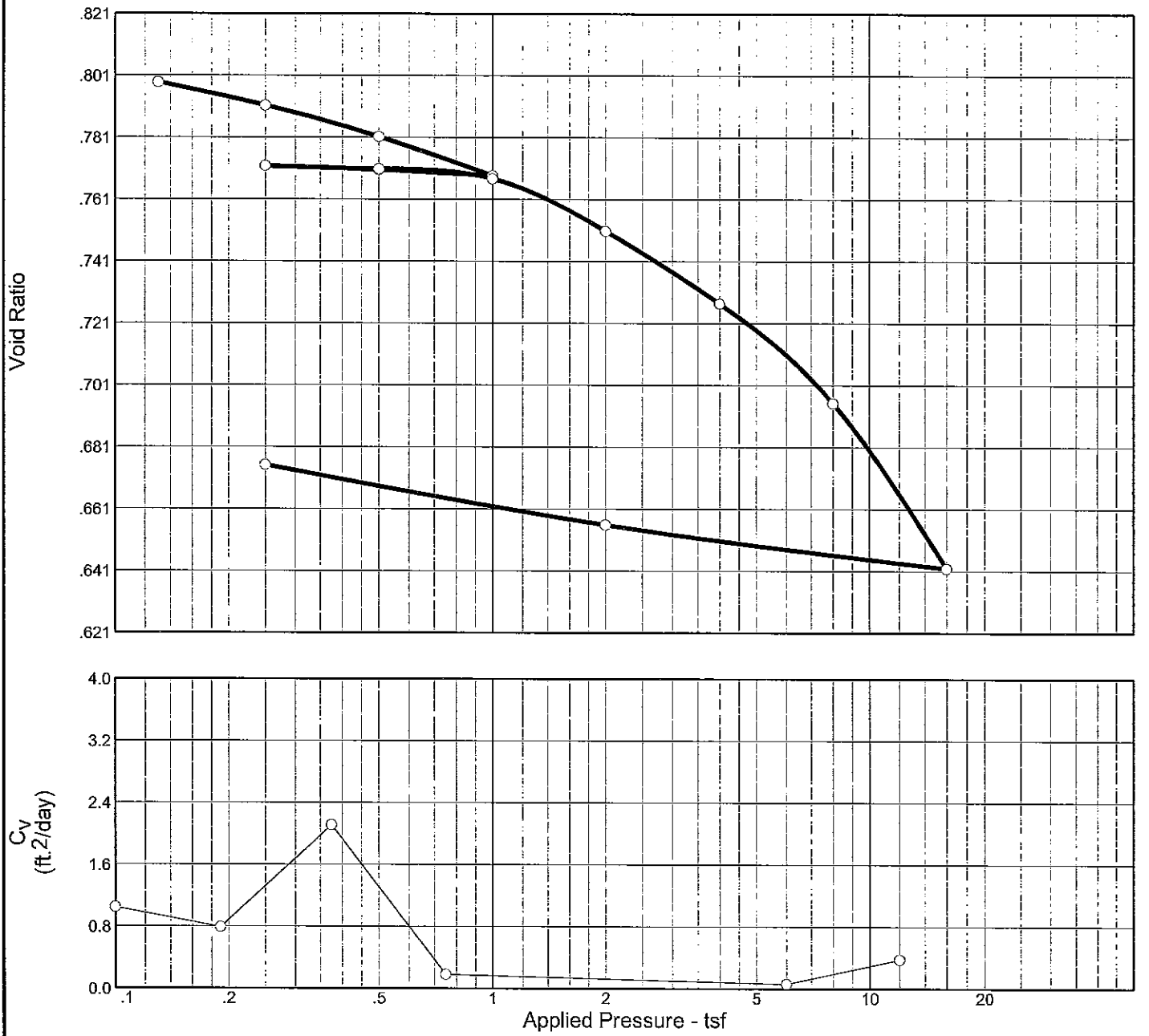
Source: B-9 **Sample No.:** 10 **Elev./Depth:** 18-20

CONSOLIDATION/SWELL TEST REPORT

Remarks:
ASTM D2435

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
100.5 %	30.8 %	91.4	NP	NP	2.65	(ML)		0.811

MATERIAL DESCRIPTION

FM G SI W/ TR F SA & CL, ML

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-9 **Sample No.:** 10 **Elev./Depth:** 18-20

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

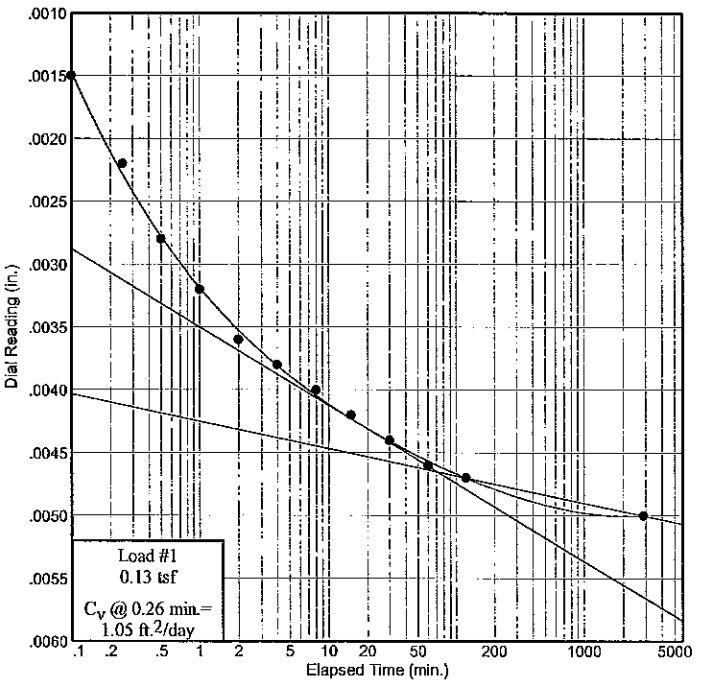
Remarks:

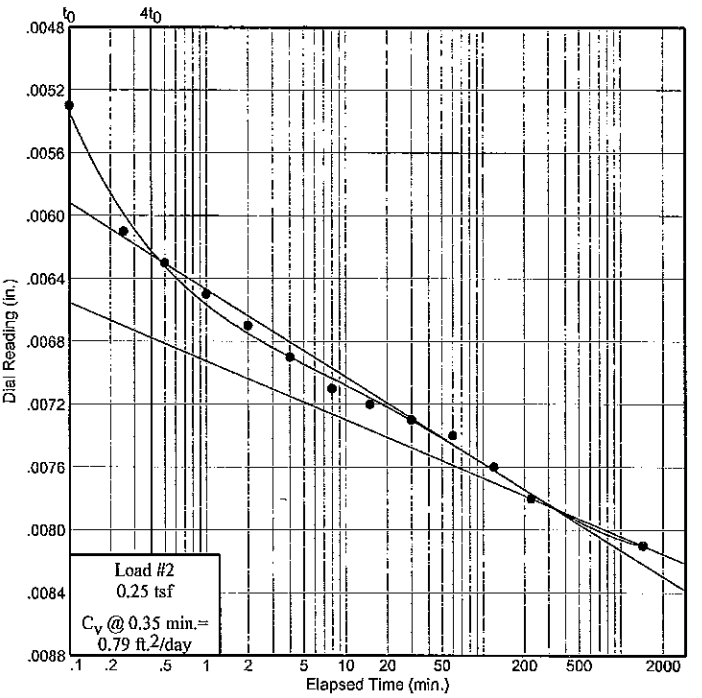
ASTM D2435

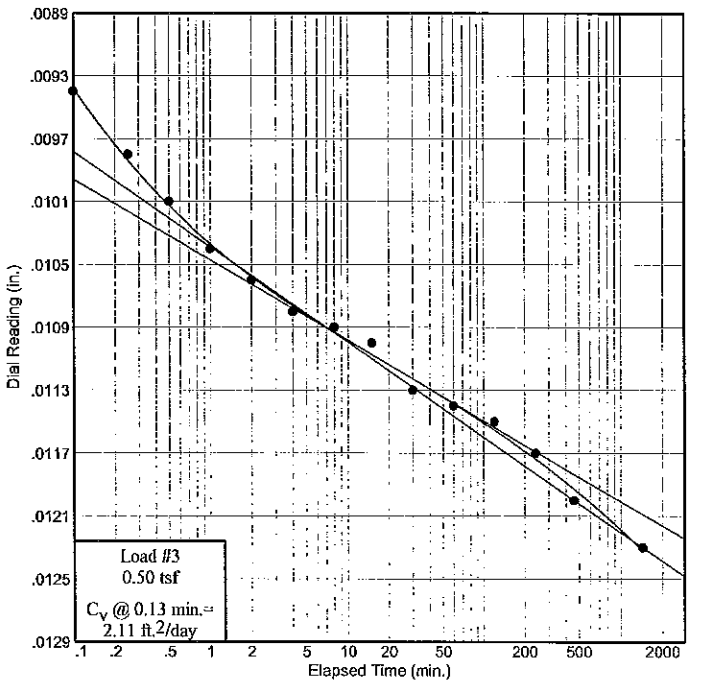
Dial Reading vs. Time

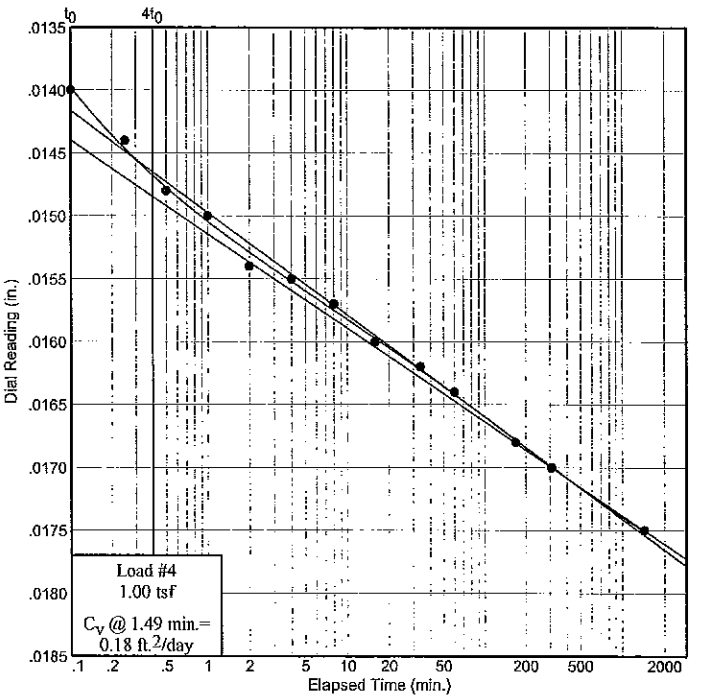
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-9 Sample No.: 10 Elev./Depth: 18-20









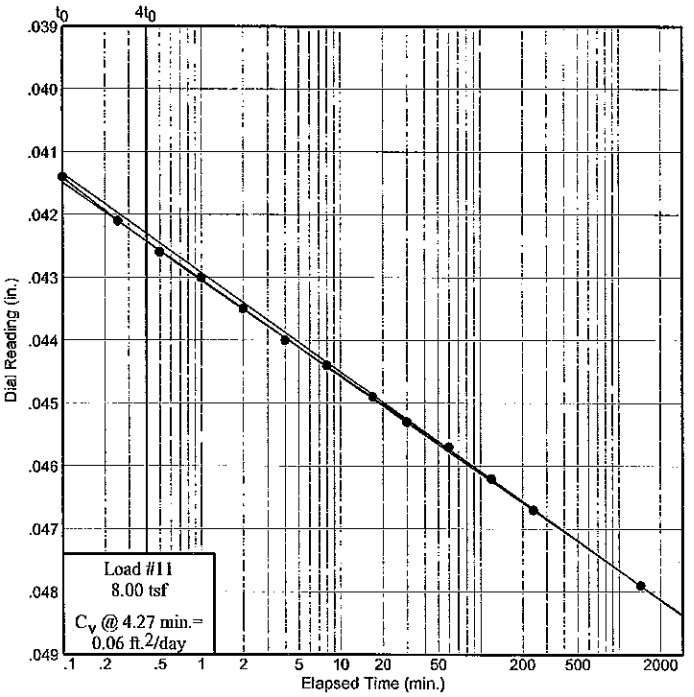
Dial Reading vs. Time

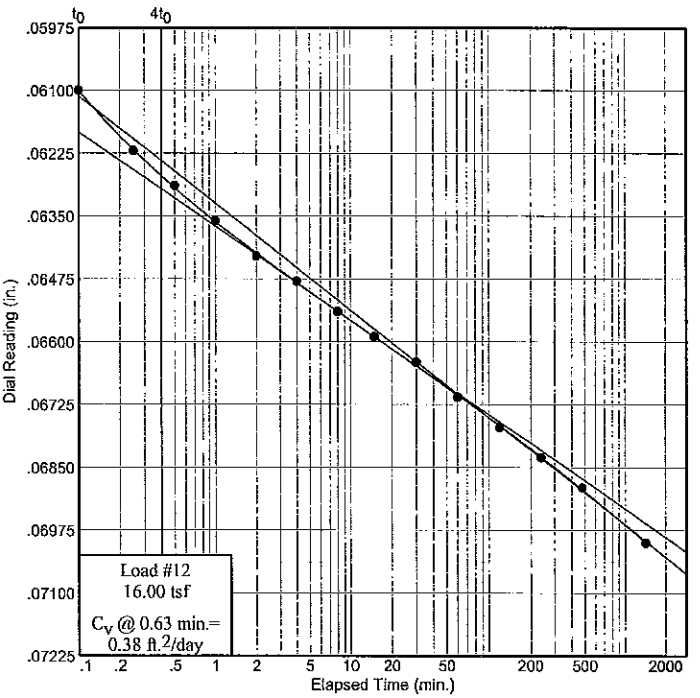
Southern Earth Sciences, Inc.

Dial Reading vs. Time

Project No.: B09-012
Project: BAYOU DUPONT

Source: B-9 Sample No.: 10 Elev./Depth: 18-20





Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-9
Sample No.: 10
Elev. or Depth: 18-20 **Sample Length(in./cm.):**
Location:
Description: FM G SI W/ TR F SA & CL, ML
Liquid Limit: NP **Plasticity Index:** NP
USCS: (ML) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST	AFTER TEST
Wet w+t =	190.95 g.	Consolidometer # = 1	Wet w+t =
Dry w+t =	182.28 g.		Dry w+t =
Tare Wt. =	154.09 g.	Spec. Gravity = 2.65	Tare Wt. =
Height =	.75 in.	Height = .75 in.	
Diameter =	2.50 in.	Diameter = 2.50 in.	
Weight =	115.44 g.	Defl. Table = Mobile Cons #2	
Moisture =	30.8 %	Ht. Solids = 0.4142 in.	Moisture = %
Wet Den. =	119.5 pcf	Dry Wt. = 88.29 g.*	Dry Wt. = n/a
Dry Den. =	91.4 pcf	Void Ratio = 0.811	Void Ratio = 0.675
		Saturation = 100.5 %	

*** Initial dry weight used in calculations**

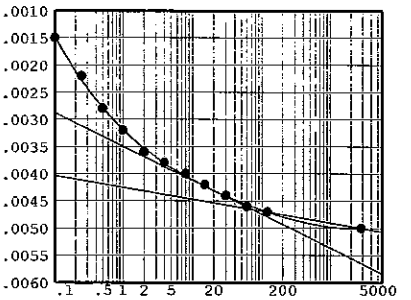
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				0.811	
0.13	0.00500	0.00000	1.05	0.000	0.799	0.7 Comprs.
0.25	0.00820	0.00010	0.79	0.000	0.791	1.1 Comprs.
0.50	0.01260	0.00030	2.11	0.001	0.781	1.6 Comprs.
1.00	0.01820	0.00070	0.18	0.001	0.769	2.3 Comprs.
0.50	0.01740	0.00070	0.80	0.000	0.771	2.2 Comprs.
0.25	0.01670	0.00050	2.24	0.000	0.772	2.2 Comprs.
0.50	0.01730	0.00070	1.05	0.000	0.771	2.2 Comprs.
1.00	0.01890	0.00100	2.51	0.000	0.768	2.4 Comprs.
2.00	0.02600	0.00110		0.001	0.751	3.3 Comprs.
4.00	0.03620	0.00160		0.002	0.727	4.6 Comprs.
8.00	0.05030	0.00240	0.06	0.002	0.695	6.4 Comprs.
16.00	0.07000	0.00000	0.38	0.003	0.642	9.3 Comprs.
2.00	0.06560	0.00140	0.60	0.000	0.656	8.6 Comprs.
0.25	0.05670	0.00050	0.47	0.000	0.675	7.5 Comprs.

C_c = 0.18 P_c = 8.38 tsf C_r = 0.01

Pressure: 0.13 tsf — **TEST READINGS** — **Load No. 1**

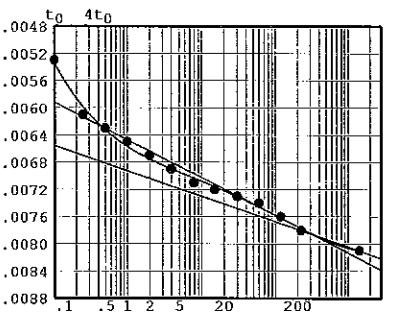
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	60.00	0.00460
2	0.10	0.00150	12	120.00	0.00470
3	0.25	0.00220	13	2880.00	0.00500
4	0.50	0.00280			
5	1.00	0.00320			
6	2.00	0.00360			
7	4.00	0.00380			
8	8.00	0.00400			
9	15.00	0.00420			
10	30.00	0.00440			



Void Ratio = 0.799 **Compression** = 0.7 %
D_0 = 0.00000 D_{50} = 0.00233 D_{100} = 0.00465
C_v **at 0.3 min.** = 1.05 ft.^{2}/day C_α = 0.000

Pressure: 0.25 tsf — **TEST READINGS** — **Load No. 2**

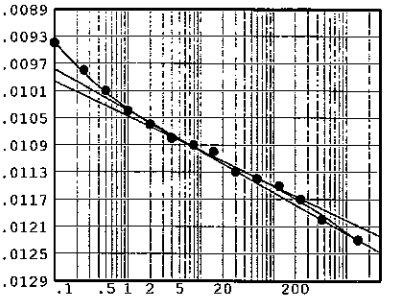
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00500	11	60.00	0.00750
2	0.10	0.00540	12	120.00	0.00770
3	0.25	0.00620	13	225.00	0.00790
4	0.50	0.00640	14	1440.00	0.00820
5	1.00	0.00660			
6	2.00	0.00680			
7	4.00	0.00700			
8	8.00	0.00720			
9	15.00	0.00730			
10	30.00	0.00740			



Void Ratio = 0.791 **Compression** = 1.1 %
D_0 = 0.00445 D_{50} = 0.00616 D_{100} = 0.00786
C_v **at 0.3 min.** = 0.79 ft.^{2}/day C_α = 0.000

Pressure: 0.50 tsf **TEST READINGS** **Load No. 3**

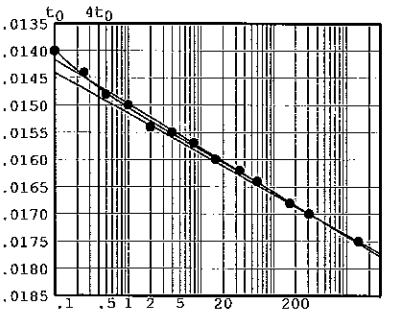
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00820	11	60.00	0.01170
2	0.10	0.00970	12	120.00	0.01180
3	0.25	0.01010	13	240.00	0.01200
4	0.50	0.01040	14	460.00	0.01230
5	1.00	0.01070	15	1440.00	0.01260
6	2.00	0.01090			
7	4.00	0.01110			
8	8.00	0.01120			
9	15.00	0.01130			
10	30.00	0.01160			



Void Ratio = 0.781 **Compression** = 1.6 %
D_0 = 0.00810 D_{50} = 0.00951 D_{100} = 0.01093
C_v at 0.1 min. = 2.11 ft.^{2}/day C_α = 0.001

Pressure: 1.00 tsf **TEST READINGS** **Load No. 4**

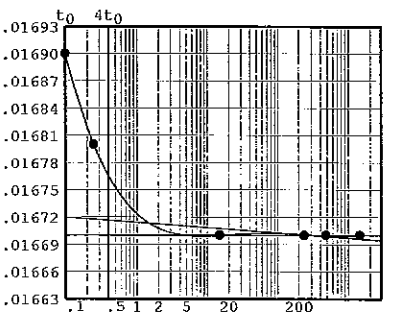
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.01260	11	60.00	0.01710
2	0.10	0.01470	12	168.00	0.01750
3	0.25	0.01510	13	308.00	0.01770
4	0.50	0.01550	14	1440.00	0.01820
5	1.00	0.01570			
6	2.00	0.01610			
7	4.00	0.01620			
8	8.00	0.01640			
9	16.00	0.01670			
10	34.00	0.01690			



Void Ratio = 0.769 **Compression** = 2.3 %
D_0 = 0.01327 D_{50} = 0.01519 D_{100} = 0.01710
C_v at 1.5 min. = 0.18 ft.^{2}/day C_α = 0.001

Pressure: 0.50 tsf **TEST READINGS** **Load No. 5**

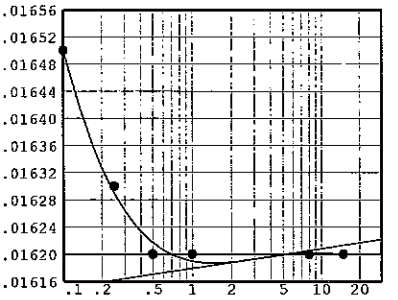
No.	Elapsed Time	Dial Reading
1	0.00	0.01820
2	0.10	0.01760
3	0.25	0.01750
4	15.00	0.01740
5	240.00	0.01740
6	480.00	0.01740
7	1440.00	0.01740



Void Ratio = 0.771 **Compression** = 2.2 %
D_0 = 0.01703 D_{50} = 0.01687 D_{100} = 0.01670
C_v at 0.3 min. = 0.80 ft.^{2}/day C_α = 0.000

Pressure: 0.25 tsf **TEST READINGS** **Load No. 6**

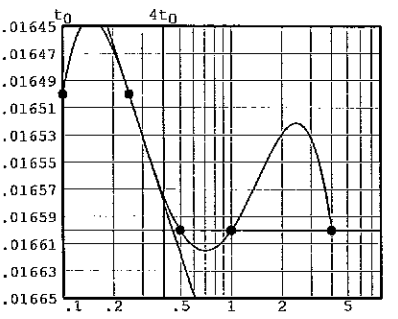
No.	Elapsed Time	Dial Reading
1	0.00	0.01740
2	0.10	0.01700
3	0.25	0.01680
4	0.50	0.01670
5	1.00	0.01670
6	8.00	0.01670
7	15.00	0.01670



Void Ratio = 0.772 **Compression** = 2.2 %
D_0 = 0.01670 D_{50} = 0.01645 D_{100} = 0.01620
C_v **at 0.1 min.** = 2.24 ft.^{2}/day C_α = 0.000

Pressure: 0.50 tsf **TEST READINGS** **Load No. 7**

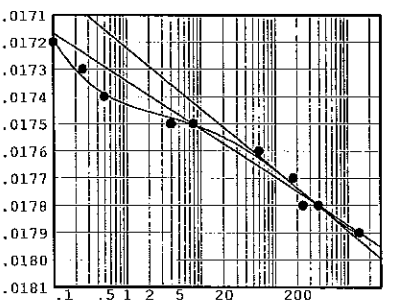
No.	Elapsed Time	Dial Reading
1	0.00	0.01670
2	0.10	0.01720
3	0.25	0.01720
4	0.50	0.01730
5	1.00	0.01730
6	4.00	0.01730



Void Ratio = 0.771 **Compression** = 2.2 %
D_0 = 0.01642 D_{50} = 0.01651 D_{100} = 0.01660
C_v **at 0.3 min.** = 1.05 ft.^{2}/day C_α = 0.000

Pressure: 1.00 tsf **TEST READINGS** **Load No. 8**

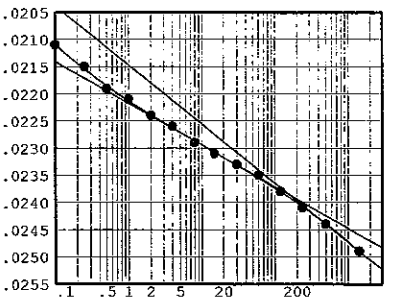
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.01730	11	1440.00	0.01890
2	0.10	0.01820			
3	0.25	0.01830			
4	0.50	0.01840			
5	4.00	0.01850			
6	8.00	0.01850			
7	60.00	0.01860			
8	177.00	0.01870			
9	240.00	0.01880			
10	390.00	0.01880			



Void Ratio = 0.768 **Compression** = 2.4 %
D_0 = 0.01660 D_{50} = 0.01720 D_{100} = 0.01780
C_v **at 0.1 min.** = 2.51 ft.^{2}/day C_α = 0.000

Pressure: 2.00 tsf — **TEST READINGS** — **Load No. 9**

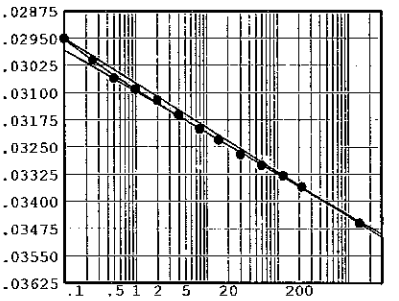
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.01890	11	60.00	0.02460
2	0.10	0.02220	12	120.00	0.02490
3	0.25	0.02260	13	240.00	0.02520
4	0.50	0.02300	14	500.00	0.02550
5	1.00	0.02320	15	1440.00	0.02600
6	2.00	0.02350			
7	4.00	0.02370			
8	8.00	0.02400			
9	15.00	0.02420			
10	30.00	0.02440			



Void Ratio = 0.751 **Compression =** 3.3 %

Pressure: 4.00 tsf — **TEST READINGS** — **Load No. 10**

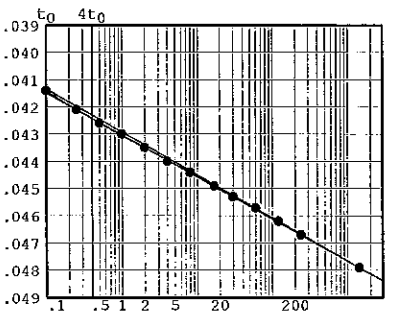
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.02600	11	60.00	0.03460
2	0.10	0.03110	12	120.00	0.03490
3	0.25	0.03170	13	220.00	0.03520
4	0.50	0.03220	14	1440.00	0.03620
5	1.00	0.03250			
6	2.00	0.03280			
7	4.00	0.03320			
8	8.00	0.03360			
9	15.00	0.03390			
10	30.00	0.03430			



Void Ratio = 0.727 **Compression =** 4.6 %

Pressure: 8.00 tsf — **TEST READINGS** — **Load No. 11**

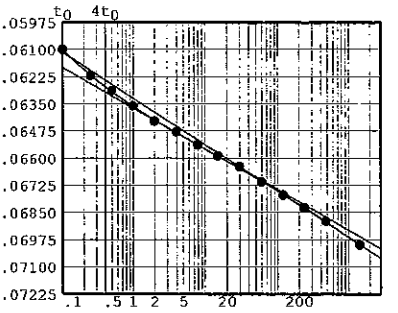
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.03620	11	60.00	0.04810
2	0.10	0.04380	12	120.00	0.04860
3	0.25	0.04450	13	240.00	0.04910
4	0.50	0.04500	14	1440.00	0.05030
5	1.00	0.04540			
6	2.00	0.04590			
7	4.00	0.04640			
8	8.00	0.04680			
9	17.00	0.04730			
10	30.00	0.04770			



Void Ratio = 0.695 **Compression =** 6.4 %
D_0 = 0.04038 D_{50} = 0.04400 D_{100} = 0.04762
C_v at 4.3 min. = 0.06 ft.^{2}/day C_α = 0.002

Pressure: 16.00 tsf **TEST READINGS** **Load No. 12**

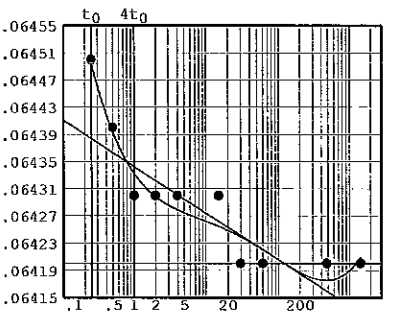
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.05030	11	60.00	0.06710
2	0.10	0.06100	12	120.00	0.06770
3	0.25	0.06220	13	240.00	0.06830
4	0.50	0.06290	14	480.00	0.06890
5	1.00	0.06360	15	1440.00	0.07000
6	2.00	0.06430			
7	4.00	0.06480			
8	8.00	0.06540			
9	15.00	0.06590			
10	30.00	0.06640			



Void Ratio = 0.642 **Compression** = 9.3 %
D_0 = 0.05930 D_{50} = 0.06317 D_{100} = 0.06703
C_v at 0.6 min. = 0.38 ft.^{2}/day C_α = 0.003

Pressure: 2.00 tsf **TEST READINGS** **Load No. 13**

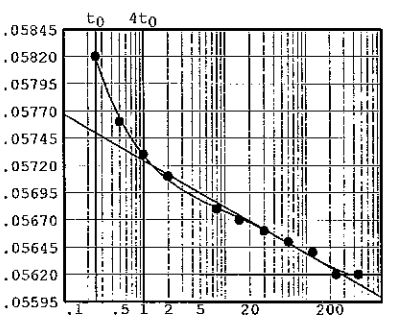
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.07000	11	1440.00	0.06560
2	0.25	0.06590			
3	0.50	0.06580			
4	1.00	0.06570			
5	2.00	0.06570			
6	4.00	0.06570			
7	15.00	0.06570			
8	30.00	0.06560			
9	60.00	0.06560			
10	480.00	0.06560			



Void Ratio = 0.656 **Compression** = 8.6 %
D_0 = 0.06466 D_{50} = 0.06443 D_{100} = 0.06420
C_v at 0.4 min. = 0.60 ft.^{2}/day C_α = 0.000

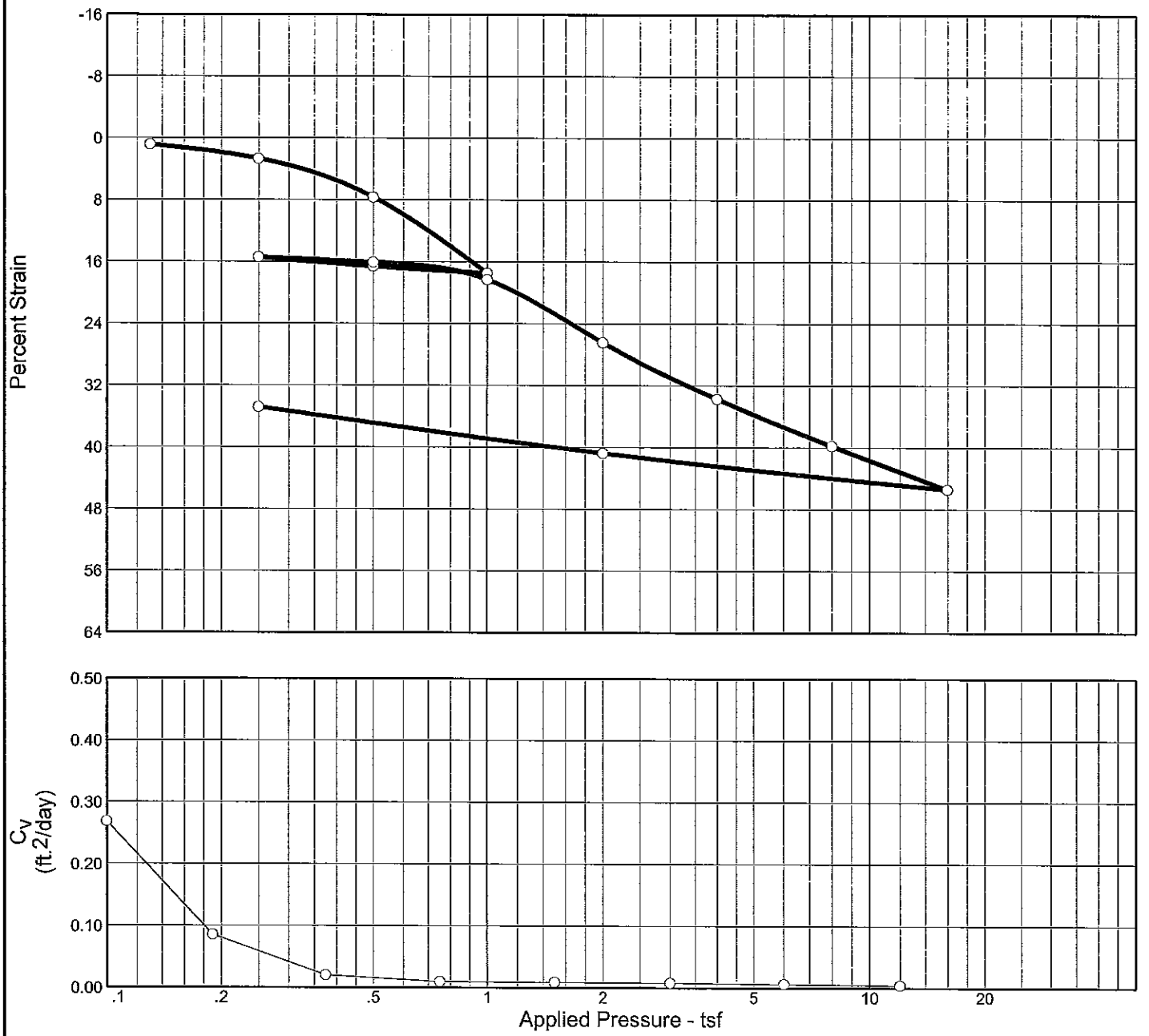
Pressure: 0.25 tsf **TEST READINGS** **Load No. 14**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.06560	11	240.00	0.05670
2	0.25	0.05870	12	450.00	0.05670
3	0.50	0.05810			
4	1.00	0.05780			
5	2.00	0.05760			
6	8.00	0.05730			
7	15.00	0.05720			
8	30.00	0.05710			
9	60.00	0.05700			
10	120.00	0.05690			



Void Ratio = 0.675 **Compression** = 7.5 %
D_0 = 0.05908 D_{50} = 0.05764 D_{100} = 0.05620
C_v at 0.5 min. = 0.47 ft.^{2}/day C_α = 0.000

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
99.2 %	73.6 %	55.8	72	45	2.65	(CH)		1.964

MATERIAL DESCRIPTION

VSO G CL W/ TR SI & TR ORGS, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

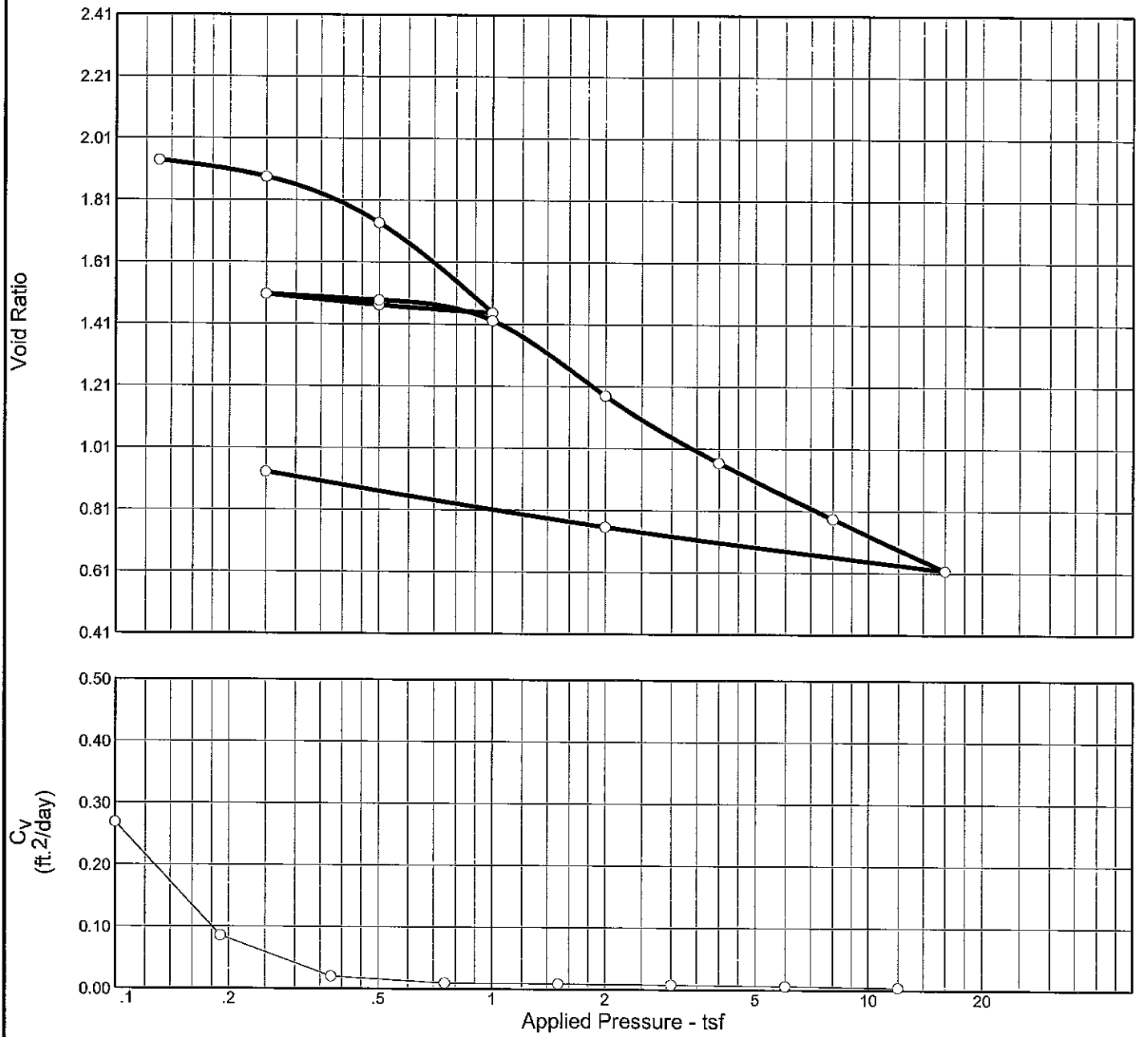
Source: B-9 **Sample No.:** 15 **Elev./Depth:** 28-30

Remarks:
ASTM D2435

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
99.2 %	73.6 %	55.8	72	45	2.65	(CH)		1.964

MATERIAL DESCRIPTION

VSO G CL W/ TR SI & TR ORGS, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-9 **Sample No.:** 15 **Elev./Depth:** 28-30

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

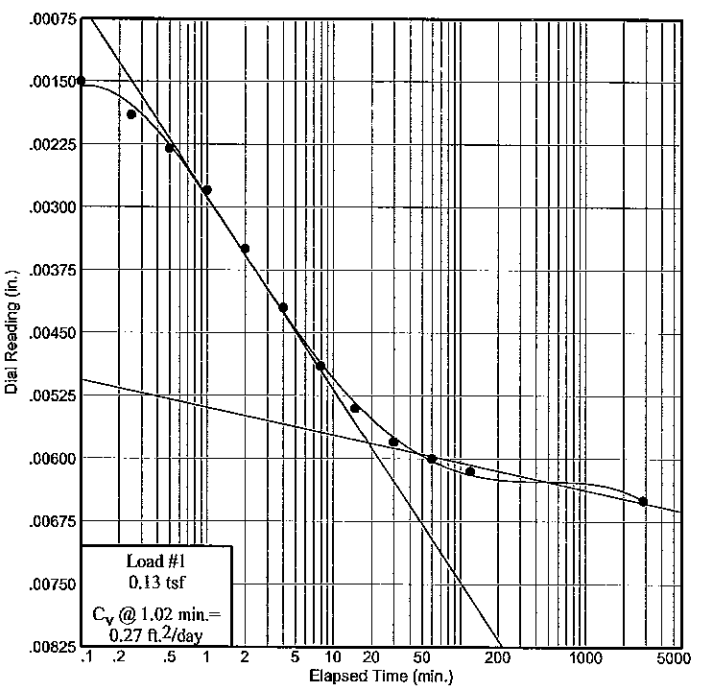
Remarks:

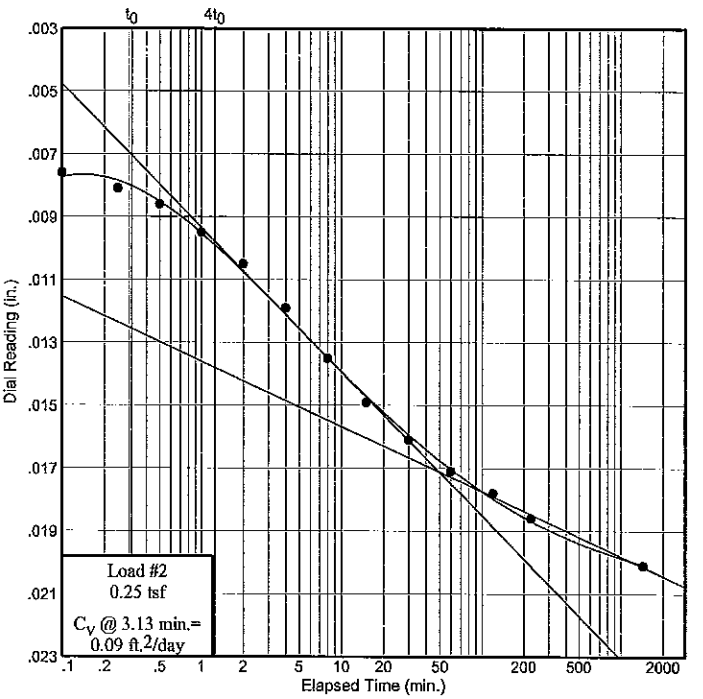
ASTM D2435

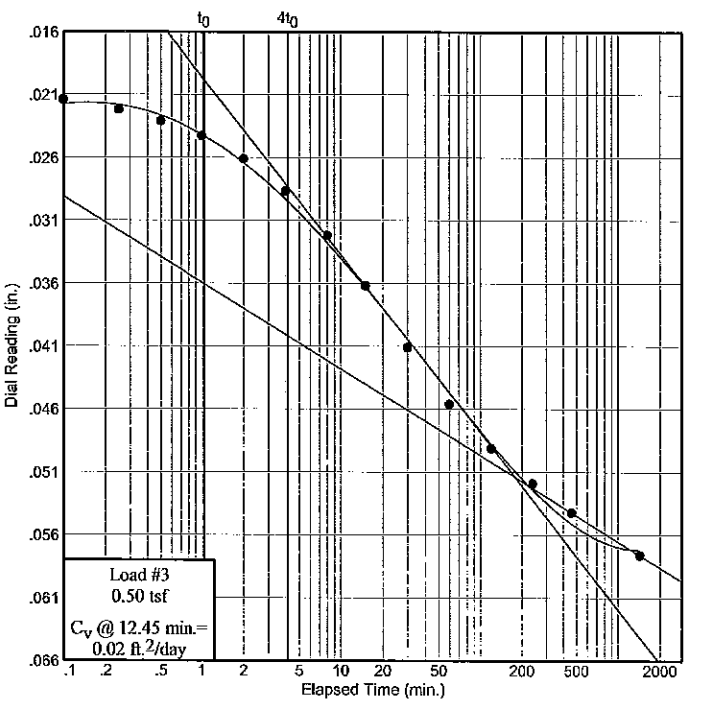
Dial Reading vs. Time

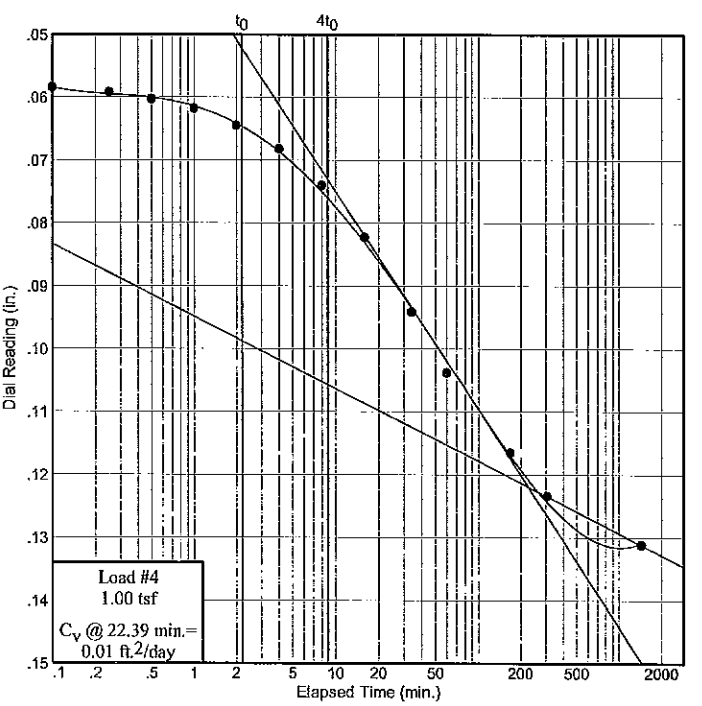
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-9 Sample No.: 15 Elev./Depth: 28-30









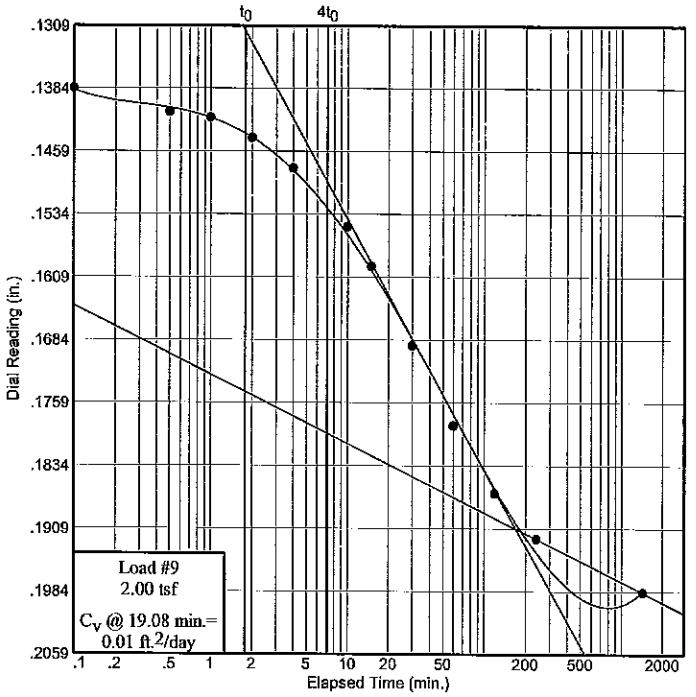
Dial Reading vs. Time

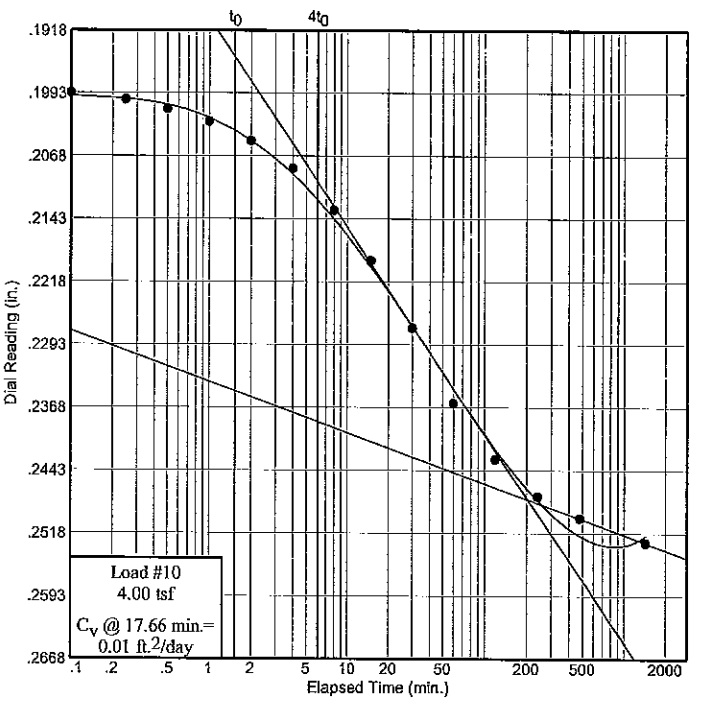
Southern Earth Sciences, Inc.

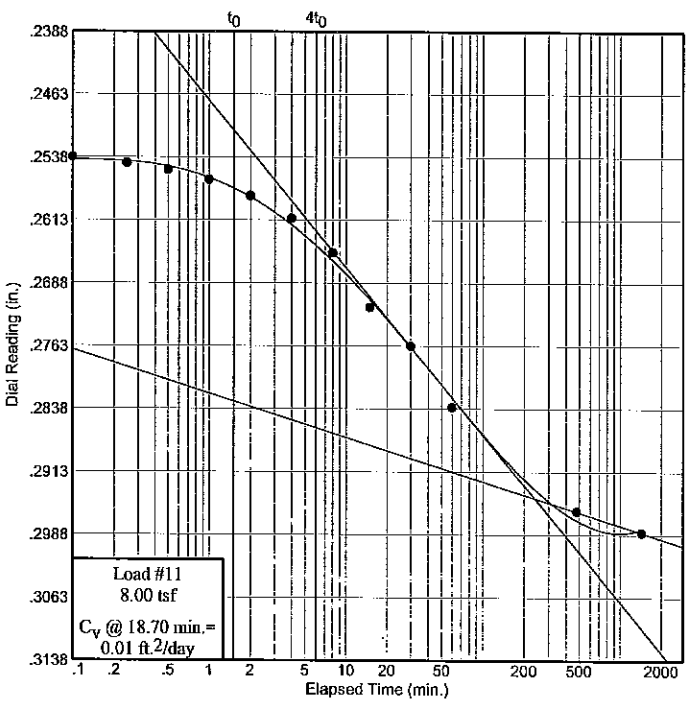
Dial Reading vs. Time

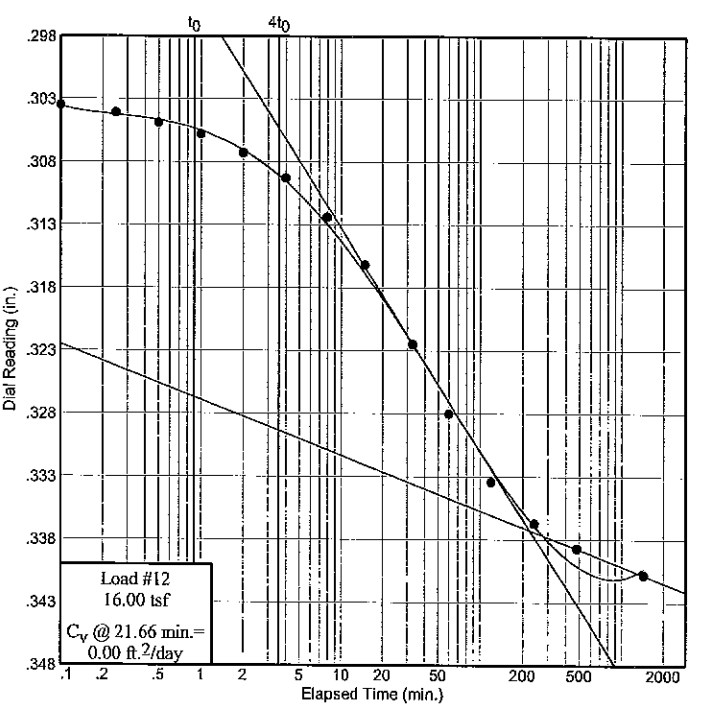
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-9 Sample No.: 15 Elev./Depth: 28-30









Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-9
Sample No.: 15
Elev. or Depth: 28-30 **Sample Length(in./cm.):**
Location:
Description: VSO G CL W/ TR SI & TR ORGS, CH
Liquid Limit: 72 **Plasticity Index:** 45
USCS: (CH) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST	AFTER TEST
Wet w+t =	173.35 g.	Consolidometer # = 1	Wet w+t =
Dry w+t =	165.45 g.		Dry w+t =
Tare Wt. =	154.71 g.	Spec. Gravity = 2.65	Tare Wt. =
Height =	.75 in.	Height = .75 in.	
Diameter =	2.50 in.	Diameter = 2.50 in.	
Weight =	93.61 g.	Defl. Table = Mobile Cons #1	
Moisture =	73.6 %	Ht. Solids = 0.2530 in.	Moisture = %
Wet Den. =	96.9 pcf	Dry Wt. = 53.94 g.*	Dry Wt. = n/a
Dry Den. =	55.8 pcf	Void Ratio = 1.964	Void Ratio = 0.932
		Saturation = 99.2 %	

*** Initial dry weight used in calculations**

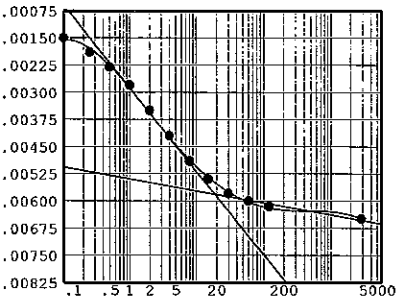
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				1.964	
0.13	0.00650	0.00000	0.27	0.000	1.938	0.9 Comprs.
0.25	0.02030	0.00020	0.09	0.003	1.885	2.7 Comprs.
0.50	0.05810	0.00050	0.02	0.009	1.736	7.7 Comprs.
1.00	0.13210	0.00100	0.01	0.017	1.446	17.5 Comprs.
0.50	0.12550	0.00080	0.07		1.471	16.6 Comprs.
0.25	0.11630	0.00050	0.02		1.506	15.4 Comprs.
0.50	0.12150	0.00080	0.06	0.001	1.487	16.1 Comprs.
1.00	0.13860	0.00120	0.04	0.005	1.421	18.3 Comprs.
2.00	0.20000	0.00150	0.01	0.013	1.180	26.5 Comprs.
4.00	0.25510	0.00220	0.01	0.011	0.965	33.7 Comprs.
8.00	0.30150	0.00300	0.01	0.011	0.784	39.8 Comprs.
16.00	0.34080	0.00000	0.00	0.010	0.617	45.4 Comprs.
2.00	0.30740	0.00170	0.00		0.756	40.8 Comprs.
0.25	0.26170	0.00050	0.00		0.932	34.8 Comprs.

C_c = 0.55 P_c = 0.01 tsf C_r = 0.14

Pressure: 0.13 tsf — **TEST READINGS** — **Load No. 1**

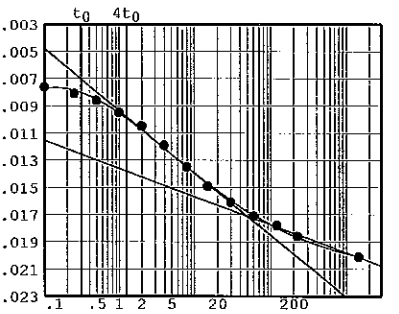
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	60.00	0.00600
2	0.10	0.00150	12	120.00	0.00615
3	0.25	0.00190	13	2880.00	0.00650
4	0.50	0.00230			
5	1.00	0.00280			
6	2.00	0.00350			
7	4.00	0.00420			
8	8.00	0.00490			
9	15.00	0.00540			
10	30.00	0.00580			



Void Ratio = 1.938 **Compression** = 0.9 %
D_0 = 0.00000 D_{50} = 0.00290 D_{100} = 0.00581
C_v **at 1.0 min.** = 0.27 ft.^{2}/day C_α = 0.000

Pressure: 0.25 tsf — **TEST READINGS** — **Load No. 2**

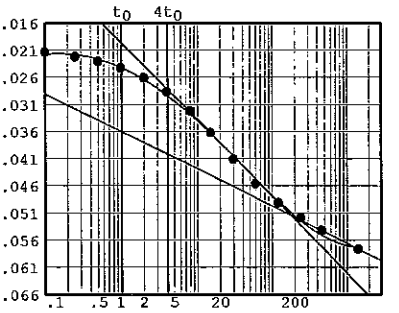
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00650	11	60.00	0.01730
2	0.10	0.00780	12	120.00	0.01800
3	0.25	0.00830	13	225.00	0.01880
4	0.50	0.00880	14	1440.00	0.02030
5	1.00	0.00970			
6	2.00	0.01070			
7	4.00	0.01210			
8	8.00	0.01370			
9	15.00	0.01510			
10	30.00	0.01630			



Void Ratio = 1.885 **Compression** = 2.7 %
D_0 = 0.00613 D_{50} = 0.01162 D_{100} = 0.01710
C_v **at 3.1 min.** = 0.09 ft.^{2}/day C_α = 0.003

Pressure: 0.50 tsf **TEST READINGS** **Load No. 3**

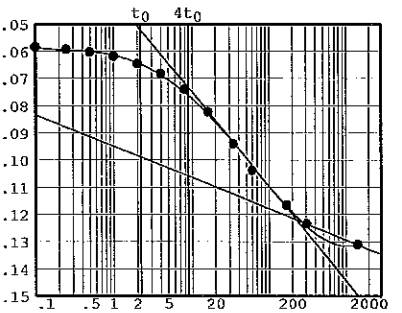
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.02030	11	60.00	0.04610
2	0.10	0.02190	12	120.00	0.04960
3	0.25	0.02270	13	240.00	0.05240
4	0.50	0.02360	14	460.00	0.05470
5	1.00	0.02480	15	1440.00	0.05810
6	2.00	0.02660			
7	4.00	0.02920			
8	8.00	0.03270			
9	15.00	0.03670			
10	30.00	0.04160			



Void Ratio = 1.736 **Compression =** 7.7 %
D_0 = 0.01907 **D_{50} =** 0.03522 **D_{100} =** 0.05137
C_v at 12.5 min. = 0.02 ft.^{2}/day **C_α =** 0.009

Pressure: 1.00 tsf **TEST READINGS** **Load No. 4**

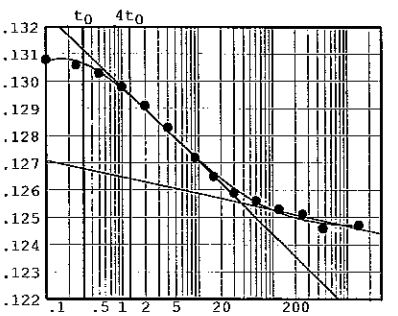
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.05810	11	60.00	0.10480
2	0.10	0.05940	12	168.00	0.11750
3	0.25	0.06020	13	308.00	0.12440
4	0.50	0.06130	14	1440.00	0.13210
5	1.00	0.06280			
6	2.00	0.06550			
7	4.00	0.06920			
8	8.00	0.07500			
9	16.00	0.08330			
10	34.00	0.09510			



Void Ratio = 1.446 **Compression =** 17.5 %
D_0 = 0.05327 **D_{50} =** 0.08755 **D_{100} =** 0.12184
C_v at 22.4 min. = 0.01 ft.^{2}/day **C_α =** 0.017

Pressure: 0.50 tsf **TEST READINGS** **Load No. 5**

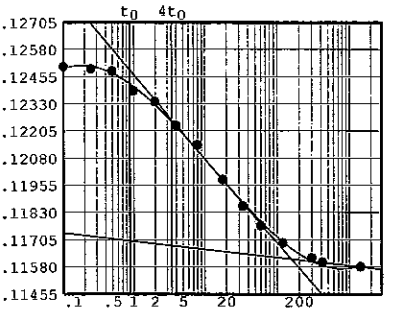
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.13210	11	60.00	0.12640
2	0.10	0.13160	12	120.00	0.12610
3	0.25	0.13140	13	251.00	0.12590
4	0.50	0.13110	14	465.00	0.12540
5	1.00	0.13060	15	1440.00	0.12550
6	2.00	0.12990			
7	4.00	0.12910			
8	9.00	0.12800			
9	16.00	0.12730			
10	30.00	0.12670			



Void Ratio = 1.471 **Compression =** 16.6 %
D_0 = 0.13181 **D_{50} =** 0.12867 **D_{100} =** 0.12553
C_v at 2.6 min. = 0.07 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 6**

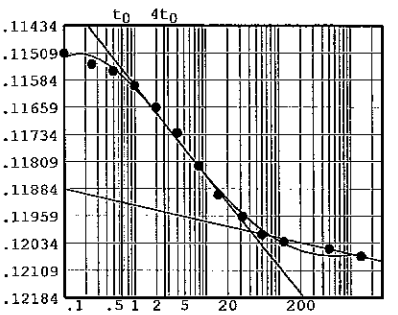
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.12550	11	60.00	0.11820
2	0.10	0.12550	12	120.00	0.11740
3	0.25	0.12540	13	300.00	0.11670
4	0.50	0.12530	14	420.00	0.11650
5	1.00	0.12440	15	1440.00	0.11630
6	2.00	0.12390			
7	4.00	0.12280			
8	8.00	0.12190			
9	18.00	0.12030			
10	34.00	0.11910			



Void Ratio = 1.506 **Compression** = 15.4 %
D_0 = 0.12601 D_{50} = 0.12108 D_{100} = 0.11616
C_v at 8.4 min. = 0.02 ft.^{2}/day

Pressure: 0.50 tsf **TEST READINGS** **Load No. 7**

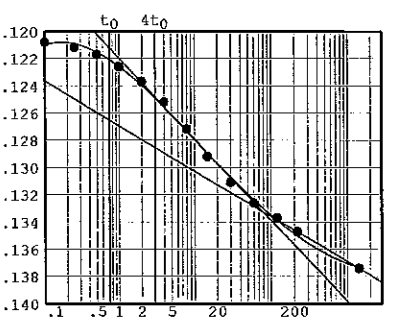
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.11630	11	60.00	0.12090
2	0.10	0.11590	12	120.00	0.12110
3	0.25	0.11620	13	500.00	0.12130
4	0.50	0.11640	14	1400.00	0.12150
5	1.00	0.11680			
6	2.00	0.11740			
7	4.00	0.11810			
8	8.00	0.11900			
9	15.00	0.11980			
10	32.00	0.12040			



Void Ratio = 1.487 **Compression** = 16.1 %
D_0 = 0.11438 D_{50} = 0.11720 D_{100} = 0.12002
C_v at 3.1 min. = 0.06 ft.^{2}/day C_α = 0.001

Pressure: 1.00 tsf **TEST READINGS** **Load No. 8**

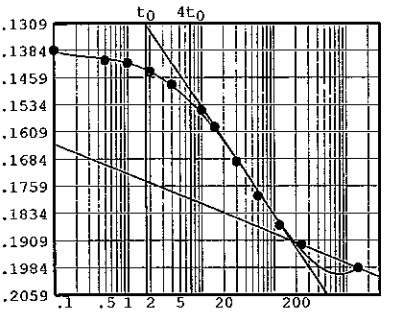
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.12150	11	60.00	0.13380
2	0.10	0.12200	12	120.00	0.13490
3	0.25	0.12240	13	220.00	0.13590
4	0.50	0.12290	14	1440.00	0.13860
5	1.00	0.12380			
6	2.00	0.12490			
7	4.00	0.12640			
8	8.00	0.12840			
9	15.00	0.13040			
10	30.00	0.13230			



Void Ratio = 1.421 **Compression** = 18.3 %
D_0 = 0.11928 D_{50} = 0.12625 D_{100} = 0.13322
C_v at 5.2 min. = 0.04 ft.^{2}/day C_α = 0.005

Pressure: 2.00 tsf **TEST READINGS** **Load No. 9**

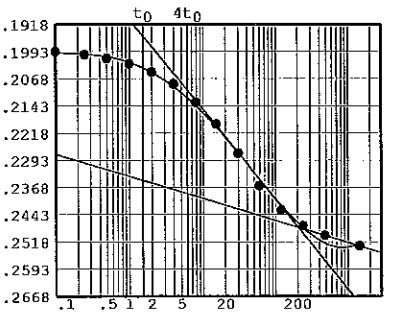
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.13860	11	120.00	0.18820
2	0.10	0.13990	12	240.00	0.19360
3	0.50	0.14270	13	1440.00	0.20000
4	1.00	0.14340			
5	2.00	0.14580			
6	4.00	0.14940			
7	10.00	0.15640			
8	15.00	0.16110			
9	30.00	0.17060			
10	60.00	0.18010			



Void Ratio = 1.180 **Compression** = 26.5 %
D_0 = 0.13484 D_{50} = 0.16286 D_{100} = 0.19088
C_v at 19.1 min. = 0.01 ft.^{2}/day C_α = 0.013

Pressure: 4.00 tsf **TEST READINGS** **Load No. 10**

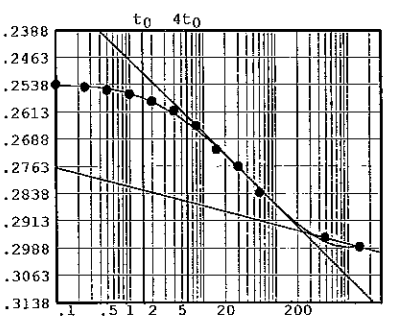
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.20000	11	60.00	0.23850
2	0.10	0.20150	12	120.00	0.24520
3	0.25	0.20230	13	240.00	0.24960
4	0.50	0.20340	14	480.00	0.25220
5	1.00	0.20490	15	1440.00	0.25510
6	2.00	0.20720			
7	4.00	0.21050			
8	8.00	0.21550			
9	15.00	0.22150			
10	30.00	0.22950			



Void Ratio = 0.965 **Compression** = 33.7 %
D_0 = 0.19548 D_{50} = 0.22161 D_{100} = 0.24774
C_v at 17.7 min. = 0.01 ft.^{2}/day C_α = 0.011

Pressure: 8.00 tsf **TEST READINGS** **Load No. 11**

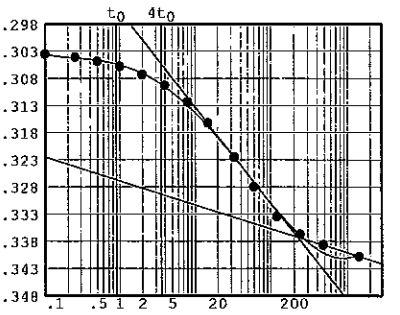
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.25510	11	60.00	0.28660
2	0.10	0.25680	12	480.00	0.29900
3	0.25	0.25750	13	1440.00	0.30150
4	0.50	0.25830			
5	1.00	0.25950			
6	2.00	0.26140			
7	4.00	0.26410			
8	8.00	0.26820			
9	15.00	0.27470			
10	30.00	0.27930			



Void Ratio = 0.784 **Compression** = 39.8 %
D_0 = 0.25069 D_{50} = 0.27255 D_{100} = 0.29440
C_v at 18.7 min. = 0.01 ft.^{2}/day C_α = 0.011

Pressure: 16.00 tsf **TEST READINGS** **Load No. 12**

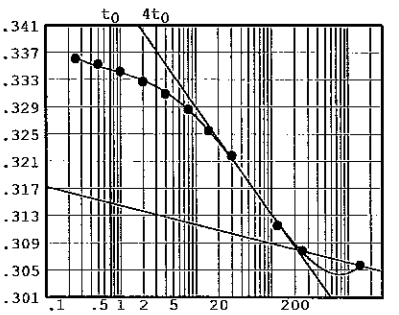
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.30150	11	60.00	0.32800
2	0.10	0.30350	12	120.00	0.33340
3	0.25	0.30410	13	240.00	0.33670
4	0.50	0.30490	14	480.00	0.33870
5	1.00	0.30580	15	1440.00	0.34080
6	2.00	0.30730			
7	4.00	0.30930			
8	8.00	0.31240			
9	15.00	0.31620			
10	33.00	0.32250			



Void Ratio = 0.617 **Compression** = 45.4 %
D_0 = 0.30157 D_{50} = 0.31940 D_{100} = 0.33724
C_v at 21.7 min. = 0.00 ft.^{2}/day C_α = 0.010

Pressure: 2.00 tsf **TEST READINGS** **Load No. 13**

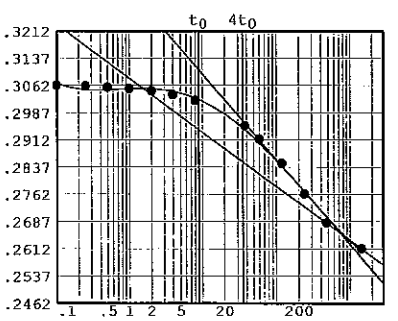
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.34080	11	253.00	0.30950
2	0.25	0.33780	12	1440.00	0.30740
3	0.50	0.33700			
4	1.00	0.33590			
5	2.00	0.33440			
6	4.00	0.33260			
7	8.00	0.33030			
8	15.00	0.32720			
9	30.00	0.32350			
10	120.00	0.31320			



Void Ratio = 0.756 **Compression** = 40.8 %
D_0 = 0.33694 D_{50} = 0.32248 D_{100} = 0.30801
C_v at 25.0 min. = 0.00 ft.^{2}/day

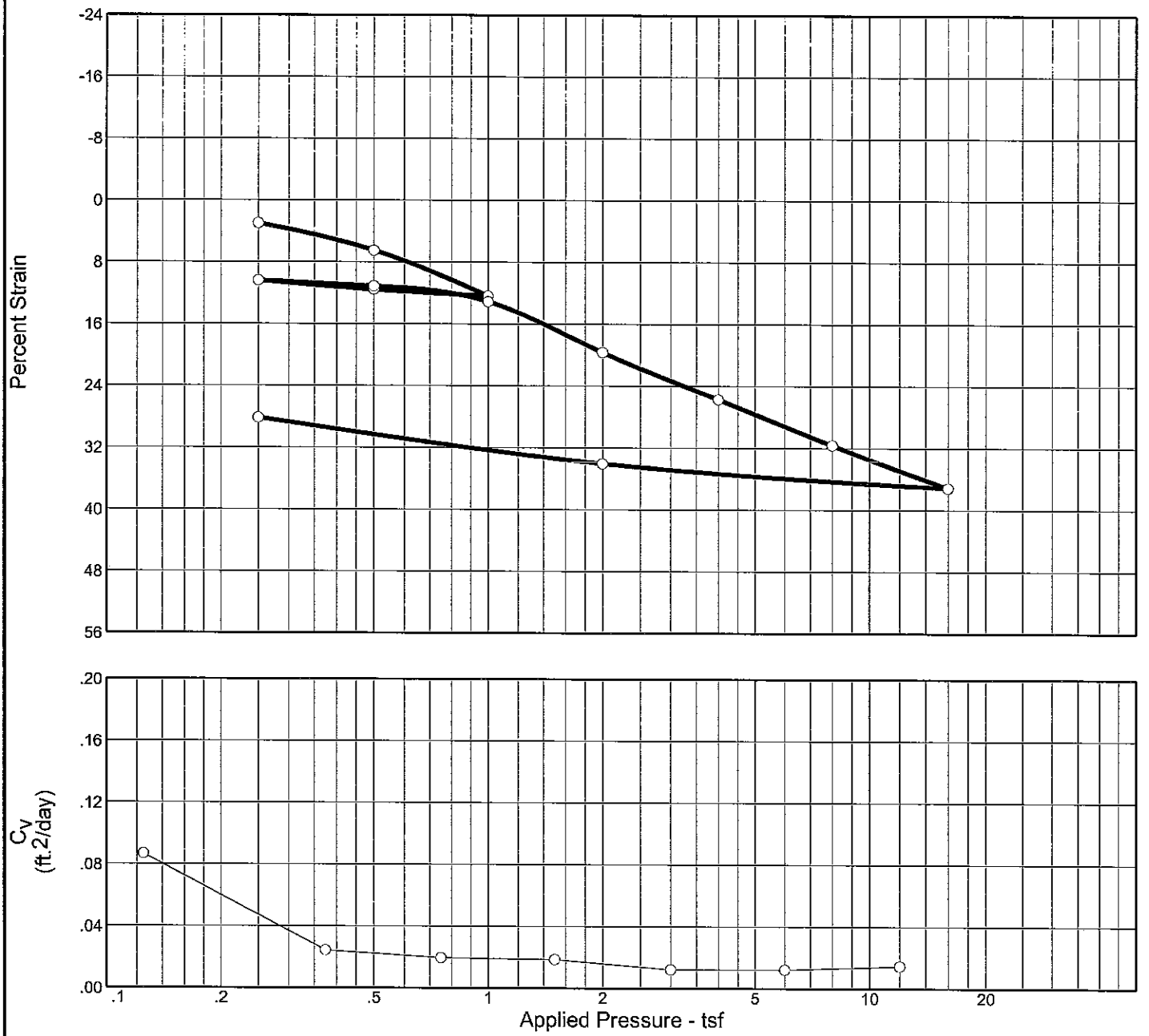
Pressure: 0.25 tsf **TEST READINGS** **Load No. 14**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.30740	11	120.00	0.28520
2	0.10	0.30670	12	240.00	0.27680
3	0.25	0.30650	13	480.00	0.26880
4	0.50	0.30620	14	1440.00	0.26170
5	1.00	0.30580			
6	2.00	0.30520			
7	4.00	0.30410			
8	8.00	0.30250			
9	38.00	0.29550			
10	60.00	0.29190			



Void Ratio = 0.932 **Compression** = 34.8 %
D_0 = 0.31015 D_{50} = 0.28787 D_{100} = 0.26558
C_v at 79.1 min. = 0.00 ft.^{2}/day

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
93.6 %	54.1 %	66.7	86	52	2.80	(CH)		1.620

MATERIAL DESCRIPTION

SO G CL W/ SI STRKS, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

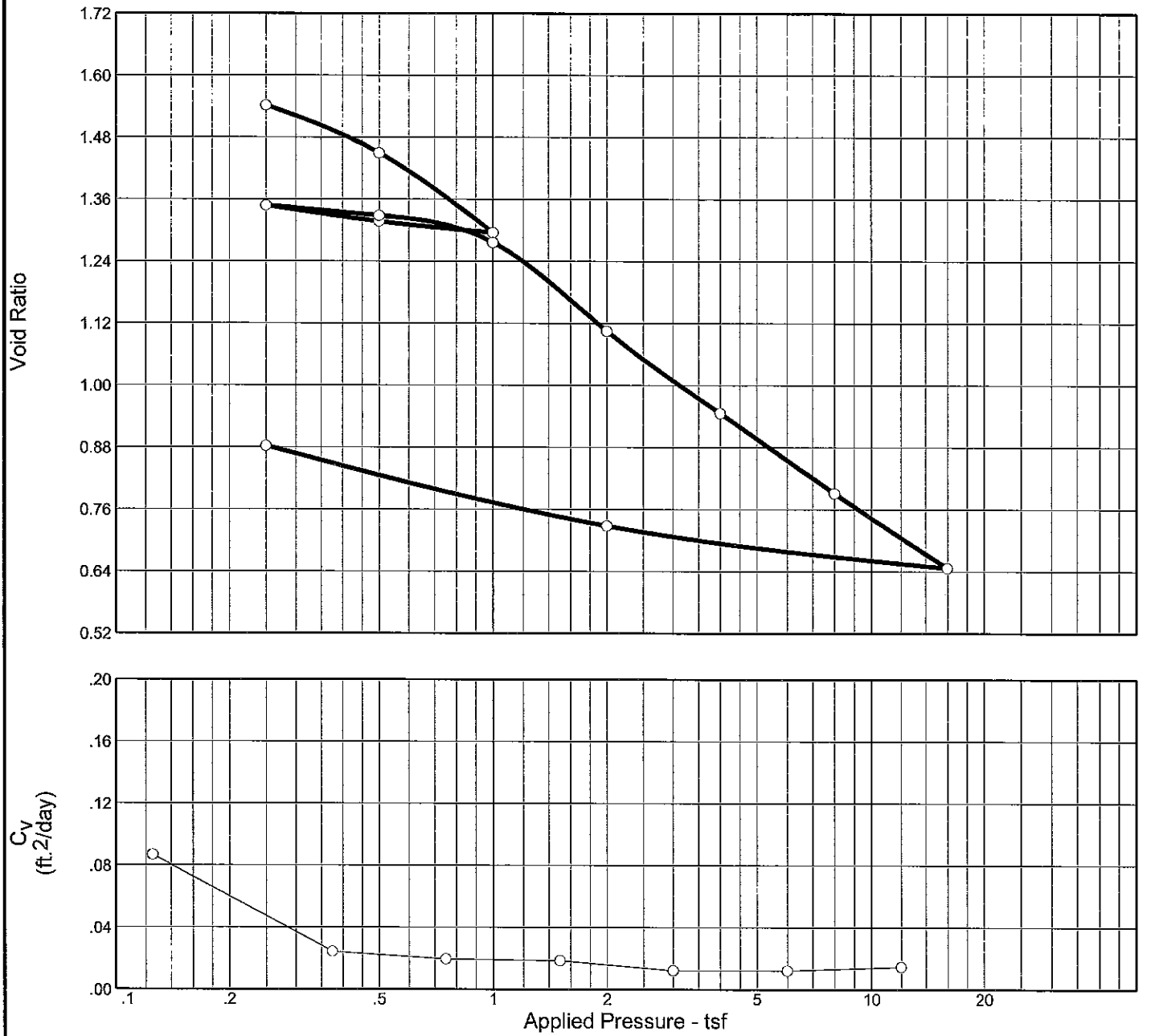
Source: B-9 **Sample No.:** 19 **Elev./Depth:** 36-38

CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

Remarks:
ASTM D2435

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
93.6 %	54.1 %	66.7	86	52	2.80	(CH)		1.620

MATERIAL DESCRIPTION

SO G CL W/ SI STRKS, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-9 **Sample No.:** 19 **Elev./Depth:** 36-38

Remarks:
ASTM D2435

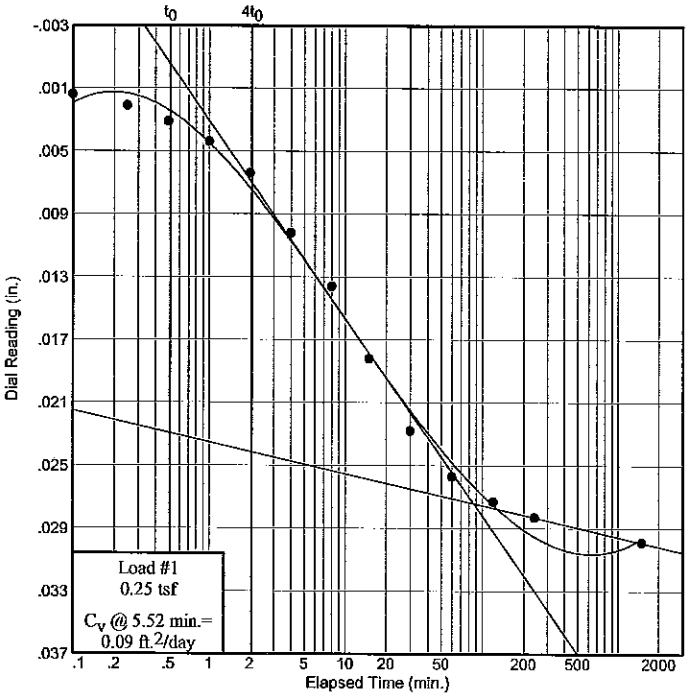
CONSOLIDATION/SWELL TEST REPORT

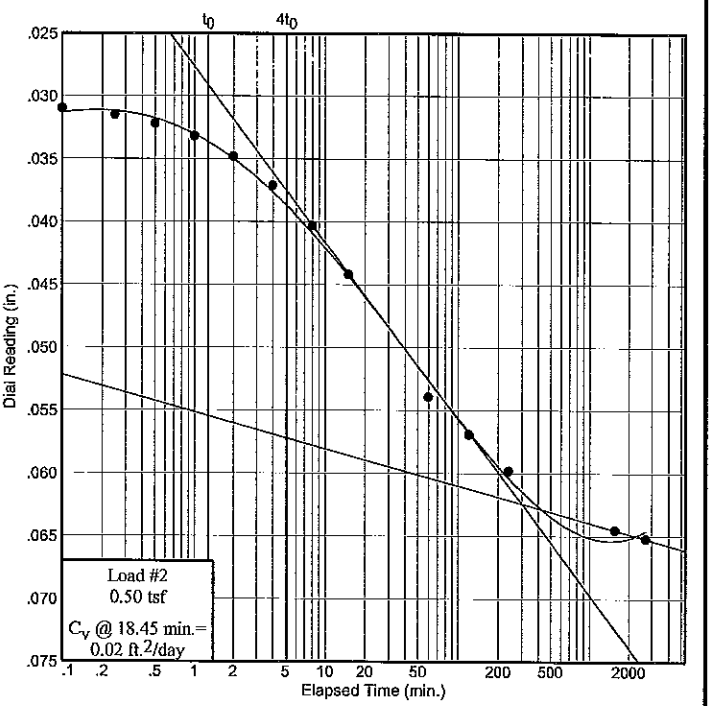
Southern Earth Sciences, Inc.

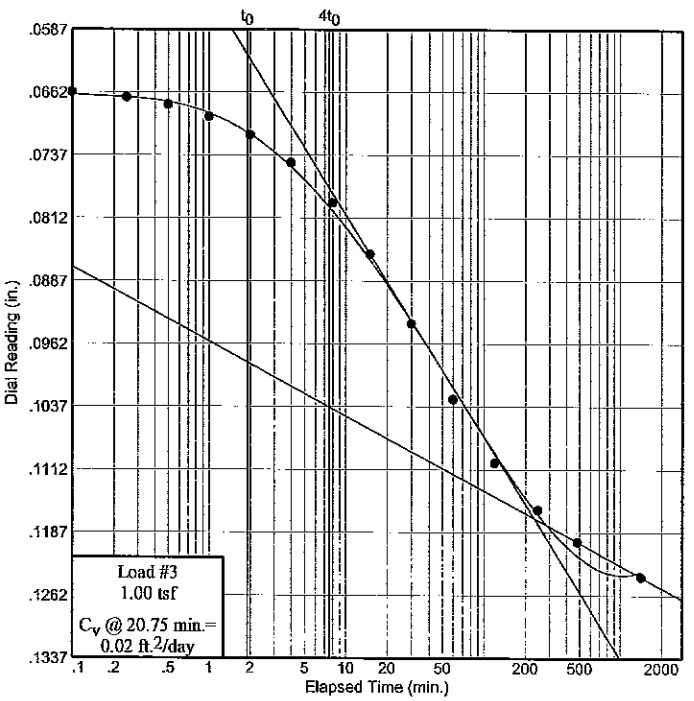
Dial Reading vs. Time

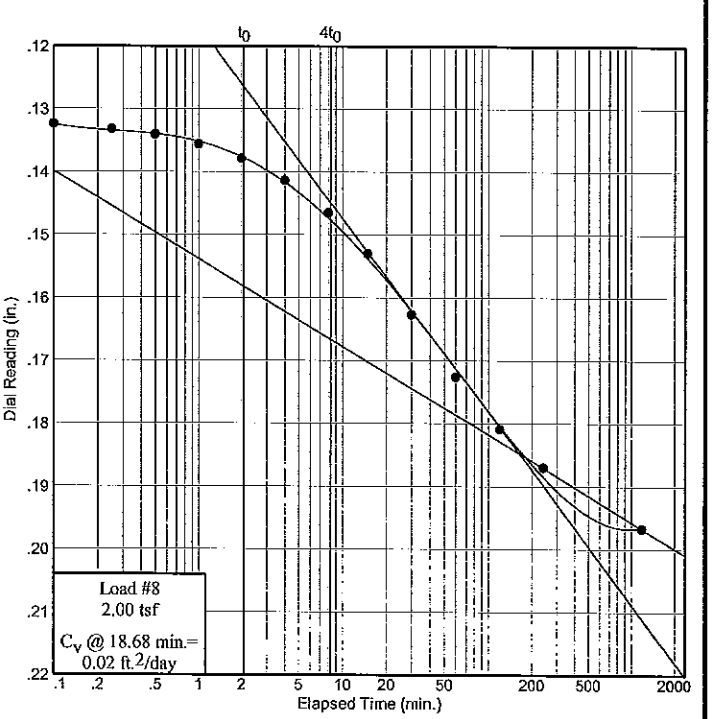
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-9 Sample No.: 19 Elev./Depth: 36-38









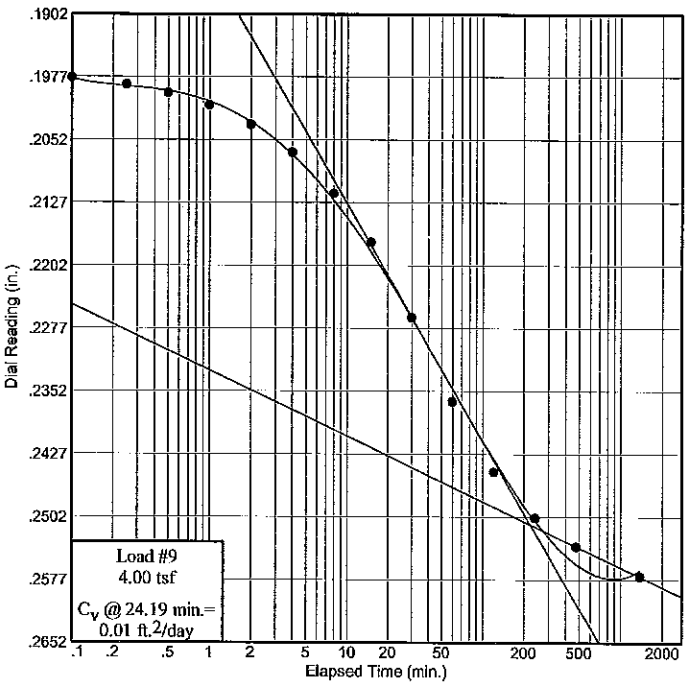
Dial Reading vs. Time

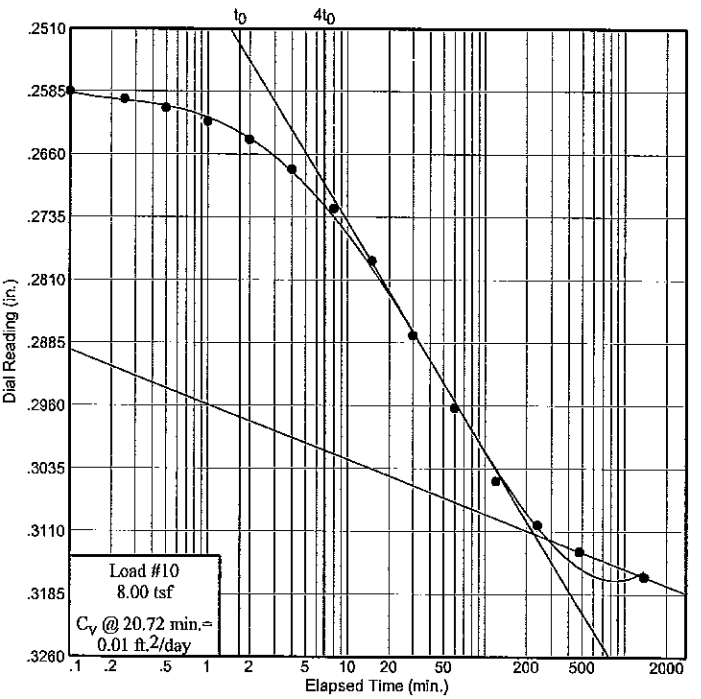
Southern Earth Sciences, Inc.

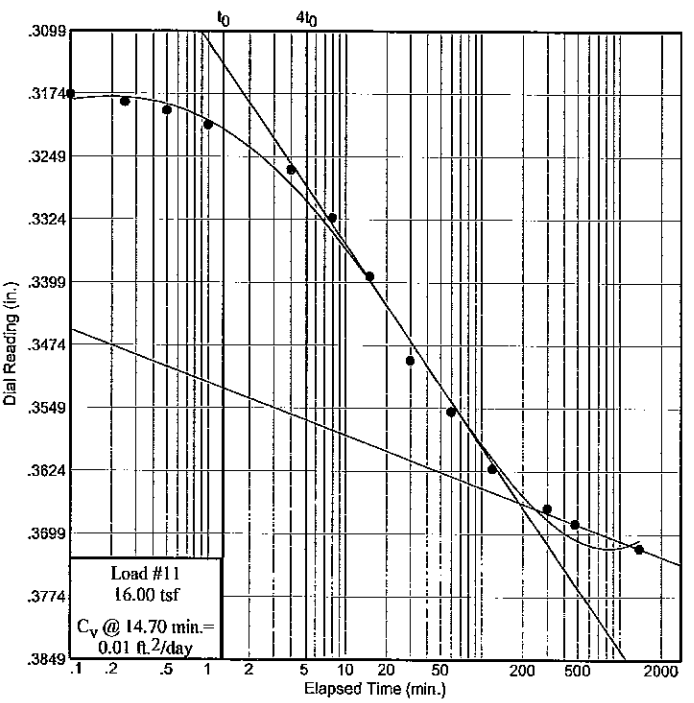
Dial Reading vs. Time

Project No.: B09-012
Project: BAYOU DUPONT

Source: B-9 Sample No.: 19 Elev./Depth: 36-38







Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-9
Sample No.: 19
Elev. or Depth: 36-38 **Sample Length(in./cm.):**
Location:
Description: SO G CL W/ SI STRKS, CH
Liquid Limit: 86 **Plasticity Index:** 52
USCS: (CH) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST	AFTER TEST
Wet w+t =	129.05 g.	**Consolidometer #** = 1	**Wet w+t** = 111.00 g.
Dry w+t =	97.05 g.		**Dry w+t** = 81.12 g.
Tare Wt. =	37.94 g.	**Spec. Gravity** = 2.80	**Tare Wt.** = .00 g.
Height =	1.00 in.	**Height** = 1.00 in.	
Diameter =	2.50 in.	**Diameter** = 2.50 in.	
Weight =	132.50 g.	**Defl. Table** = Unit No. 10 Old 2.5in	
Moisture =	54.1 %	**Ht. Solids** = 0.3817 in.	**Moisture** = 36.8 %
Wet Den. =	102.8 pcf	**Dry Wt.** = 85.96 g.*	**Dry Wt.** = 81.12 g.
Dry Den. =	66.7 pcf	**Void Ratio** = 1.620	**Void Ratio** = 0.883
		Saturation = 93.6 %	

*** Initial dry weight used in calculations**

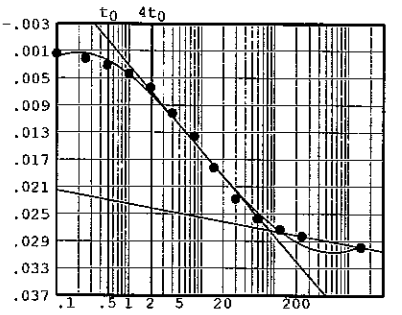
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				1.620	
0.25	0.03010	0.00020	0.09	0.002	1.542	3.0 Comprs.
0.50	0.06560	0.00040	0.02	0.003	1.449	6.5 Comprs.
1.00	0.12480	0.00080	0.02	0.010	1.295	12.4 Comprs.
0.50	0.11650	0.00080	0.11		1.317	11.6 Comprs.
0.25	0.10470	0.00080	0.04		1.348	10.4 Comprs.
0.50	0.11220	0.00080	0.09	0.000	1.328	11.1 Comprs.
1.00	0.13230	0.00100	0.06	0.005	1.276	13.1 Comprs.
2.00	0.19800	0.00130	0.02	0.016	1.105	19.7 Comprs.
4.00	0.25930	0.00200	0.01	0.010	0.946	25.7 Comprs.
8.00	0.31940	0.00300	0.01	0.009	0.791	31.6 Comprs.
16.00	0.37570	0.00410	0.01	0.009	0.646	37.2 Comprs.
2.00	0.34200	0.00150			0.728	34.0 Comprs.
0.25	0.28210	0.00060			0.883	28.1 Comprs.

C_c = 0.48 P_c = 0.25 tsf C_r = 0.12

Pressure: 0.25 tsf **TEST READINGS** **Load No. 1**

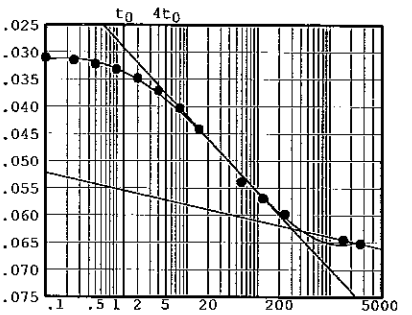
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	60.00	0.02590
2	0.10	0.00160	12	120.00	0.02750
3	0.25	0.00230	13	240.00	0.02850
4	0.50	0.00330	14	1500.00	0.03010
5	1.00	0.00460			
6	2.00	0.00660			
7	4.00	0.01040			
8	8.00	0.01380			
9	15.00	0.01840			
10	30.00	0.02300			



Void Ratio = 1.542 **Compression** = 3.0 %
D_0 = -0.00256 D_{50} = 0.01242 D_{100} = 0.02741
C_v at 5.5 min. = 0.09 ft.^{2}/day C_α = 0.002

Pressure: 0.50 tsf **TEST READINGS** **Load No. 2**

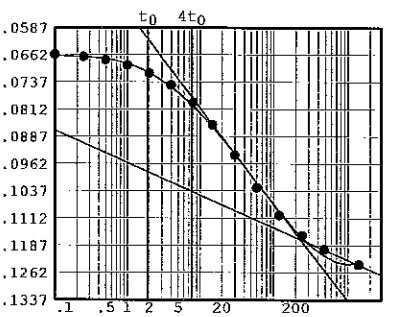
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.03010	11	120.00	0.05730
2	0.10	0.03140	12	240.00	0.06020
3	0.25	0.03190	13	1560.00	0.06490
4	0.50	0.03260	14	2700.00	0.06560
5	1.00	0.03360			
6	2.00	0.03520			
7	4.00	0.03750			
8	8.00	0.04070			
9	15.00	0.04460			
10	60.00	0.05430			



Void Ratio = 1.449 **Compression** = 6.5 %
D_0 = 0.02855 D_{50} = 0.04548 D_{100} = 0.06240
C_v at 18.5 min. = 0.02 ft.^{2}/day C_α = 0.003

Pressure: 1.00 tsf **TEST READINGS** **Load No. 3**

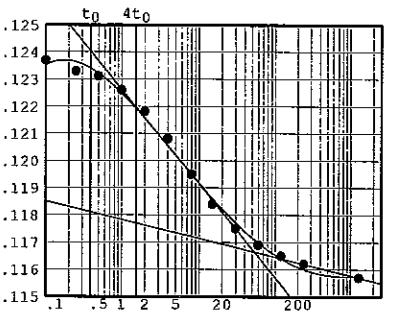
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.06560	11	60.00	0.10360
2	0.10	0.06700	12	120.00	0.11120
3	0.25	0.06760	13	246.00	0.11680
4	0.50	0.06850	14	480.00	0.12060
5	1.00	0.06990	15	1420.00	0.12480
6	2.00	0.07210			
7	4.00	0.07540			
8	8.00	0.08020			
9	15.00	0.08630			
10	30.00	0.09460			



Void Ratio = 1.295 **Compression** = 12.4 %
D_0 = 0.06205 D_{50} = 0.08951 D_{100} = 0.11697
C_v at 20.8 min. = 0.02 ft.^{2}/day C_α = 0.010

Pressure: 0.50 tsf **TEST READINGS** **Load No. 4**

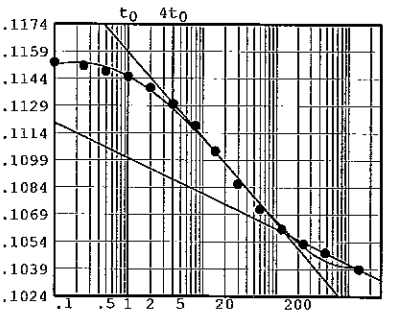
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.12480	11	60.00	0.11770
2	0.10	0.12450	12	120.00	0.11730
3	0.25	0.12410	13	240.00	0.11700
4	0.50	0.12390	14	1290.00	0.11650
5	1.00	0.12340			
6	2.00	0.12260			
7	4.00	0.12160			
8	8.00	0.12030			
9	15.00	0.11920			
10	30.00	0.11830			



Void Ratio = 1.317 **Compression =** 11.6 %
D_0 = 0.12491 **D_{50} =** 0.12078 **D_{100} =** 0.11664
C_v at 3.4 min. = 0.11 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 5**

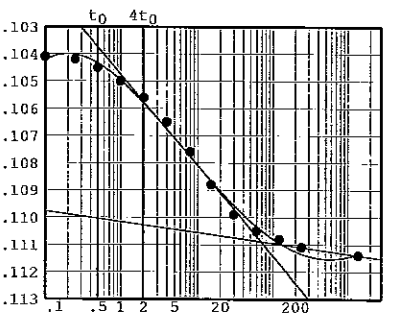
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.11650	11	60.00	0.10800
2	0.10	0.11610	12	120.00	0.10690
3	0.25	0.11590	13	240.00	0.10610
4	0.50	0.11560	14	480.00	0.10560
5	1.00	0.11530	15	1390.00	0.10470
6	2.00	0.11470			
7	4.00	0.11380			
8	8.00	0.11260			
9	15.00	0.11120			
10	30.00	0.10940			



Void Ratio = 1.348 **Compression =** 10.4 %
D_0 = 0.11630 **D_{50} =** 0.11109 **D_{100} =** 0.10588
C_v at 10.2 min. = 0.04 ft.^{2}/day

Pressure: 0.50 tsf **TEST READINGS** **Load No. 6**

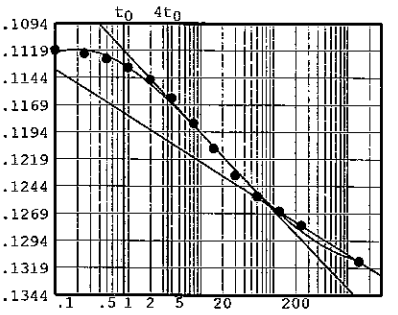
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.10470	11	60.00	0.11130
2	0.10	0.10490	12	120.00	0.11160
3	0.25	0.10500	13	240.00	0.11190
4	0.50	0.10530	14	1380.00	0.11220
5	1.00	0.10580			
6	2.00	0.10640			
7	4.00	0.10730			
8	8.00	0.10840			
9	15.00	0.10960			
10	30.00	0.11070			



Void Ratio = 1.328 **Compression =** 11.1 %
D_0 = 0.10288 **D_{50} =** 0.10688 **D_{100} =** 0.11089
C_v at 4.4 min. = 0.09 ft.^{2}/day **C_α =** 0.000

Pressure: 1.00 tsf **TEST READINGS** **Load No. 7**

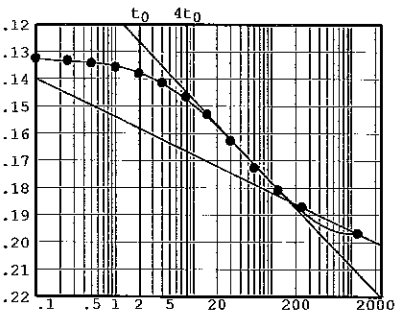
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.11220	11	60.00	0.12630
2	0.10	0.11290	12	120.00	0.12770
3	0.25	0.11320	13	240.00	0.12900
4	0.50	0.11370	14	1440.00	0.13230
5	1.00	0.11450			
6	2.00	0.11560			
7	4.00	0.11730			
8	8.00	0.11960			
9	15.00	0.12190			
10	30.00	0.12440			



Void Ratio = 1.276 **Compression** = 13.1 %
D_0 = 0.11005 D_{50} = 0.11807 D_{100} = 0.12610
C_v at 6.3 min. = 0.06 ft.^{2}/day C_α = 0.005

Pressure: 2.00 tsf **TEST READINGS** **Load No. 8**

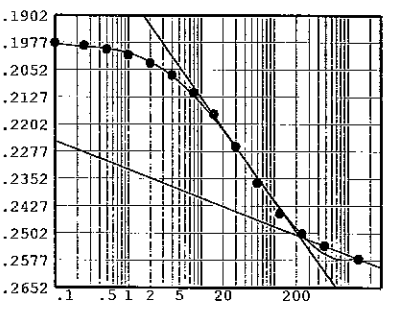
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.13230	11	60.00	0.17390
2	0.10	0.13370	12	120.00	0.18220
3	0.25	0.13450	13	240.00	0.18830
4	0.50	0.13540	14	1190.00	0.19800
5	1.00	0.13690			
6	2.00	0.13920			
7	4.00	0.14270			
8	8.00	0.14780			
9	15.00	0.15430			
10	30.00	0.16400			



Void Ratio = 1.105 **Compression** = 19.7 %
D_0 = 0.12794 D_{50} = 0.15632 D_{100} = 0.18471
C_v at 18.7 min. = 0.02 ft.^{2}/day C_α = 0.016

Pressure: 4.00 tsf **TEST READINGS** **Load No. 9**

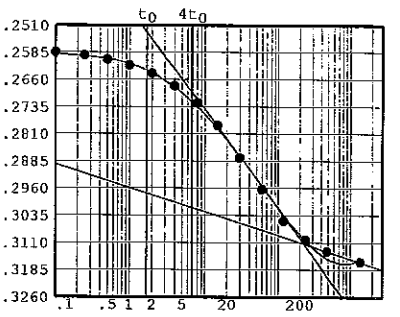
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.19800	11	60.00	0.23840
2	0.10	0.19980	12	120.00	0.24680
3	0.25	0.20060	13	240.00	0.25230
4	0.50	0.20160	14	480.00	0.25570
5	1.00	0.20310	15	1380.00	0.25930
6	2.00	0.20540			
7	4.00	0.20870			
8	8.00	0.21360			
9	15.00	0.21940			
10	30.00	0.22840			



Void Ratio = 0.946 **Compression** = 25.7 %
D_0 = 0.19670 D_{50} = 0.22389 D_{100} = 0.25108
C_v at 24.2 min. = 0.01 ft.^{2}/day C_α = 0.010

Pressure: 8.00 tsf **TEST READINGS** **Load No. 10**

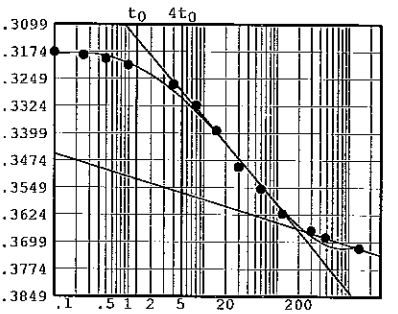
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.25930	11	60.00	0.29930
2	0.10	0.26150	12	120.00	0.30800
3	0.25	0.26240	13	240.00	0.31320
4	0.50	0.26350	14	480.00	0.31640
5	1.00	0.26510	15	1380.00	0.31940
6	2.00	0.26730			
7	4.00	0.27080			
8	8.00	0.27550			
9	15.00	0.28170			
10	30.00	0.29060			



Void Ratio = 0.791 **Compression =** 31.6 %
D_0 = 0.25475 D_{50} = 0.28301 D_{100} = 0.31126
C_v **at 20.7 min. =** 0.01 ft.^{2}/day C_α = 0.009

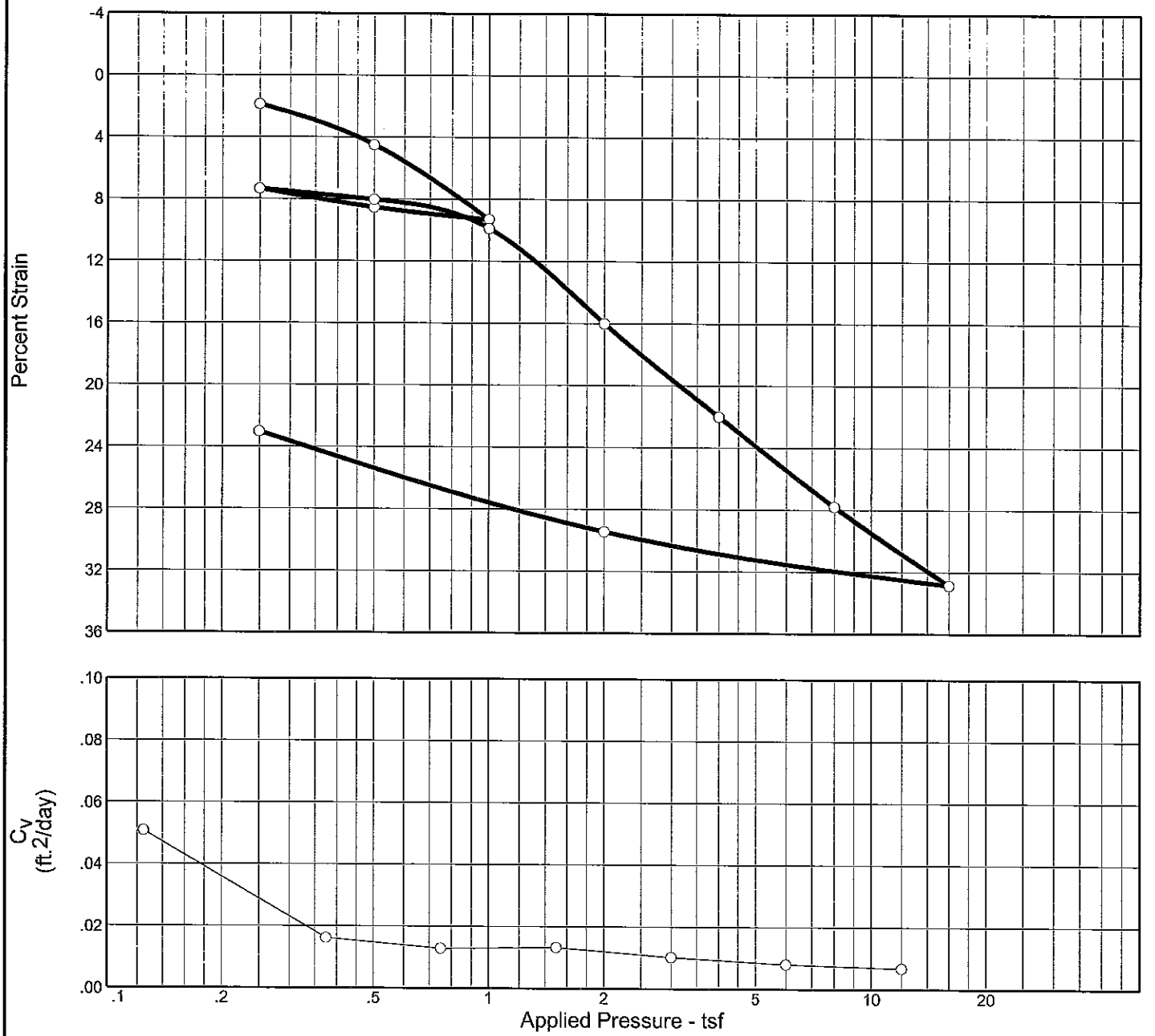
Pressure: 16.00 tsf **TEST READINGS** **Load No. 11**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.31940	11	120.00	0.36620
2	0.10	0.32160	12	300.00	0.37090
3	0.25	0.32250	13	480.00	0.37280
4	0.50	0.32350	14	1386.00	0.37570
5	1.00	0.32520			
6	4.00	0.33060			
7	8.00	0.33630			
8	15.00	0.34330			
9	30.00	0.35330			
10	60.00	0.35940			



Void Ratio = 0.646 **Compression =** 37.2 %
D_0 = 0.31298 D_{50} = 0.33956 D_{100} = 0.36614
C_v **at 14.7 min. =** 0.01 ft.^{2}/day C_α = 0.009

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
96.6 %	52.0 %	69.7	76	49	2.80	(CH)		1.508

MATERIAL DESCRIPTION

SO G CL W/ SI, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-9 **Sample No.:** 28 **Elev./Depth:** 54-56

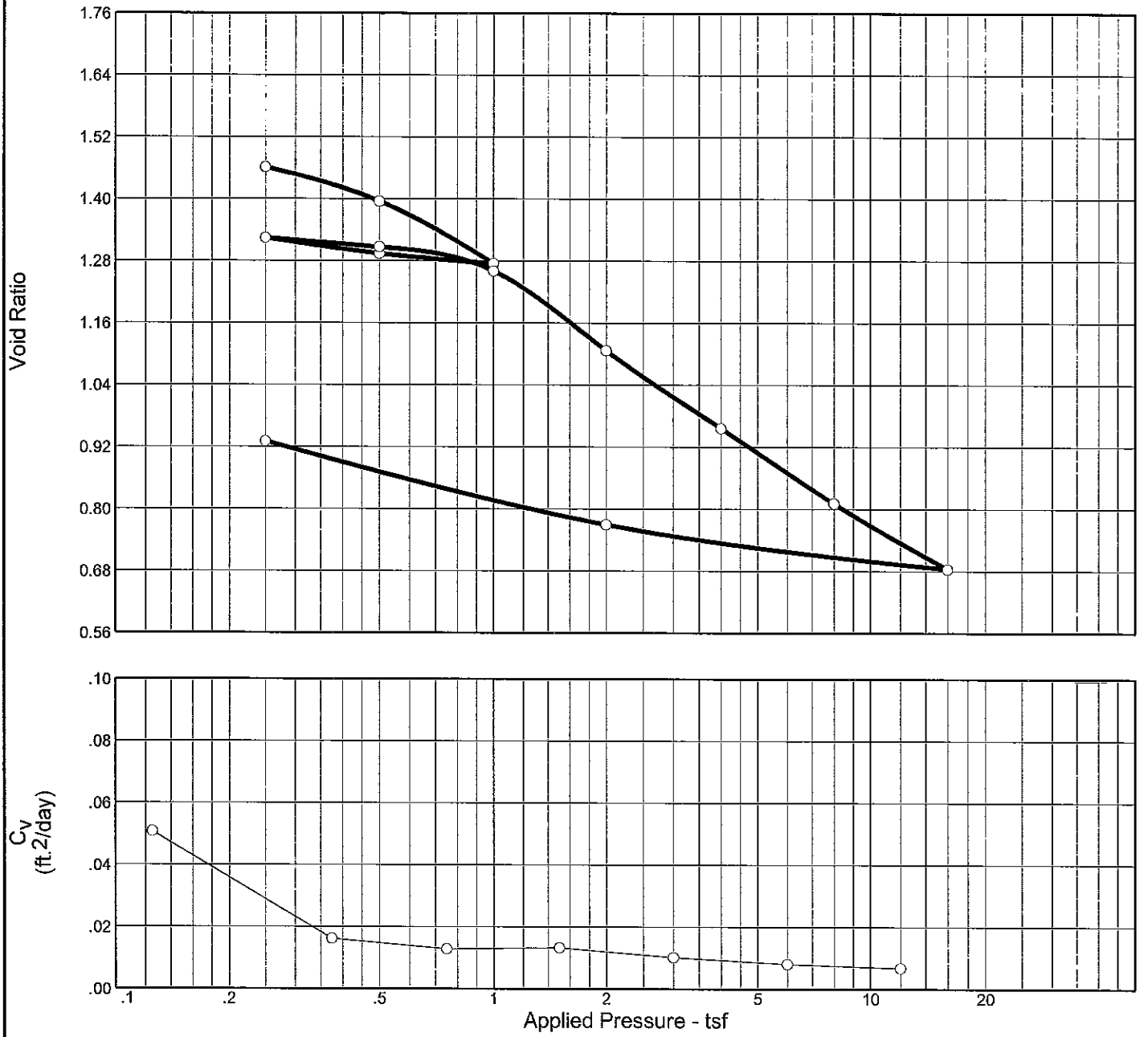
CONSOLIDATION/SWELL TEST REPORT

Southern Earth Sciences, Inc.

Remarks:

ASTM D2435

CONSOLIDATION/SWELL TEST REPORT



Natural		Dry Dens. (pcf)	LL	PI	Sp. Gr.	USCS	AASHTO	Initial Void Ratio
Saturation	Moisture							
96.6 %	52.0 %	69.7	76	49	2.80	(CH)		1.508

MATERIAL DESCRIPTION

SO G CL W/ SI, CH

Project No. B09-012 **Client:** URS

Project: BAYOU DUPONT

Source: B-9 **Sample No.:** 28 **Elev./Depth:** 54-56

CONSOLIDATION/SWELL TEST REPORT

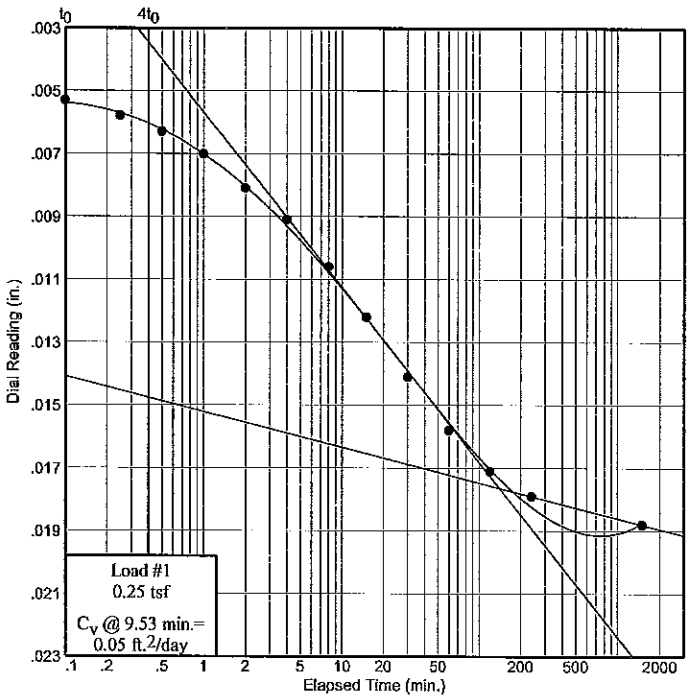
Remarks:
ASTM D2435

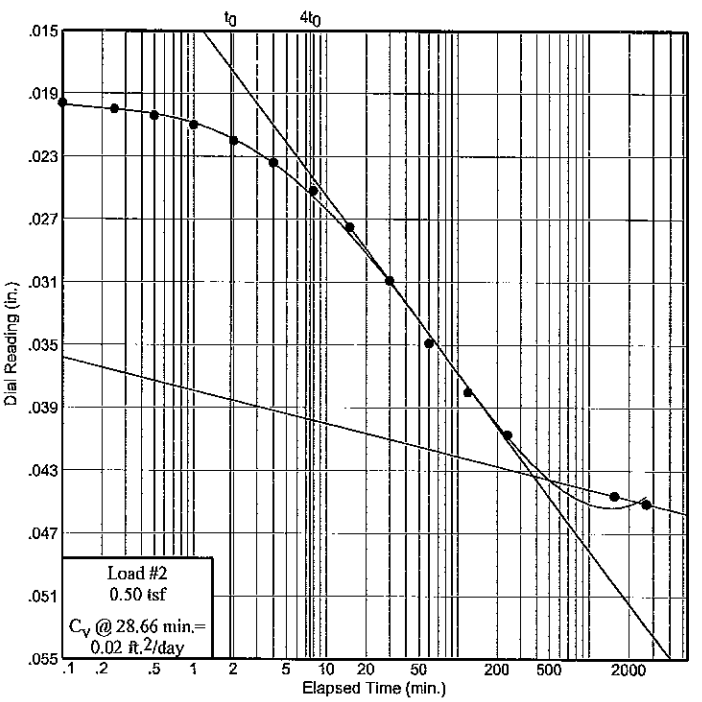
Southern Earth Sciences, Inc.

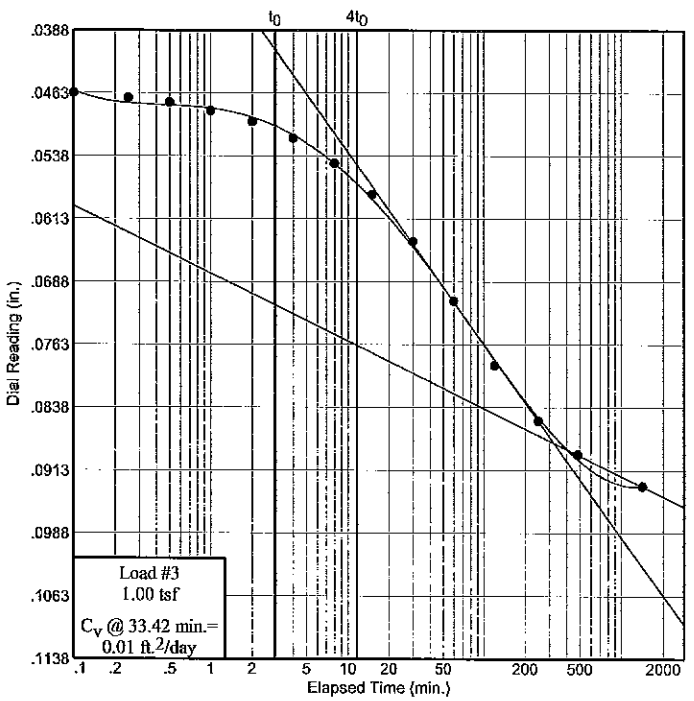
Dial Reading vs. Time

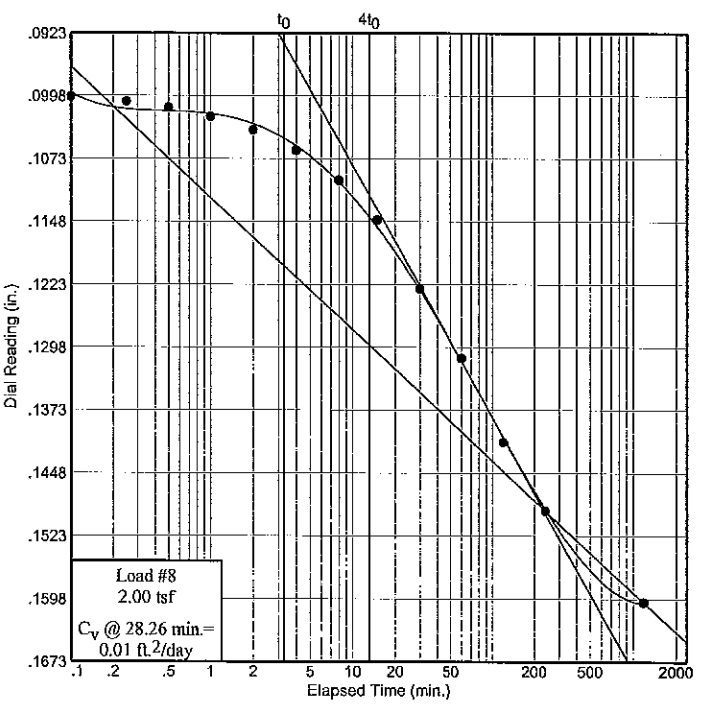
Project No.: B09-012
Project: BAYOU DUPONT

Source: B-9 Sample No.: 28 Elev./Depth: 54-56









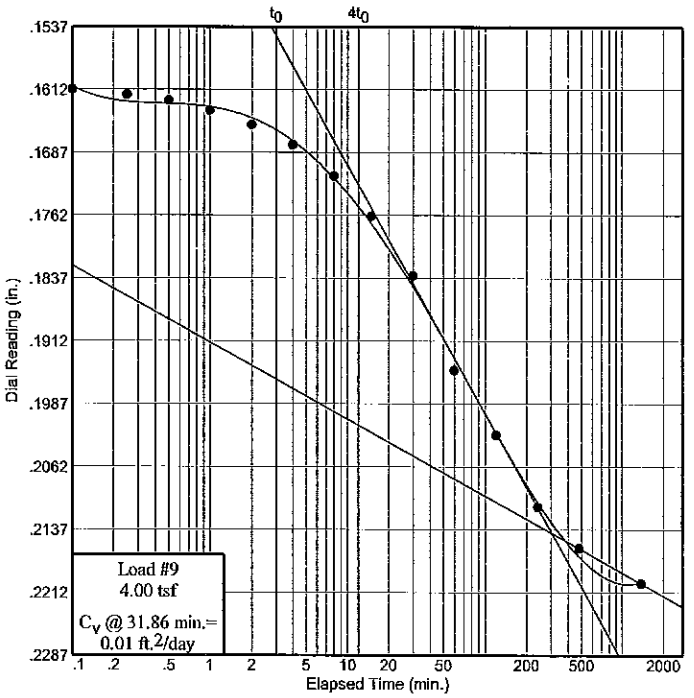
Dial Reading vs. Time

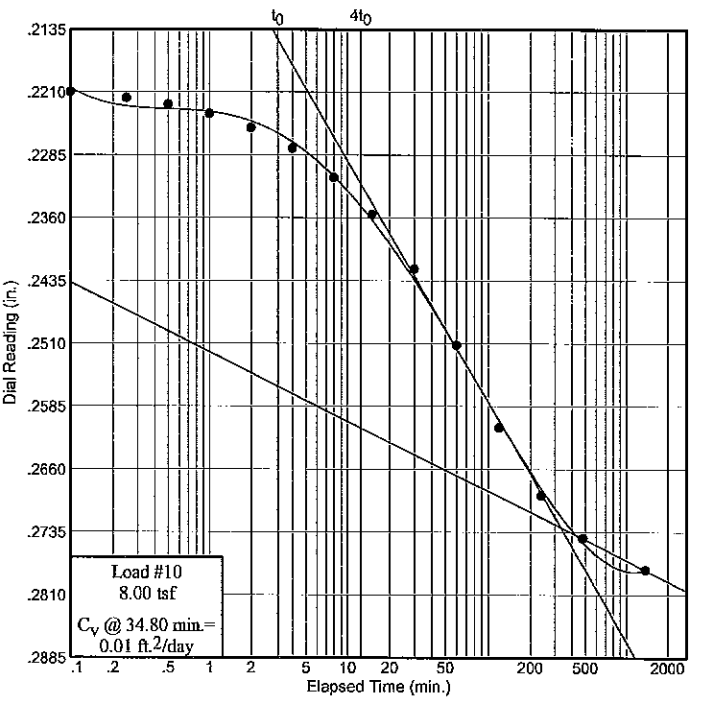
Southern Earth Sciences, Inc.

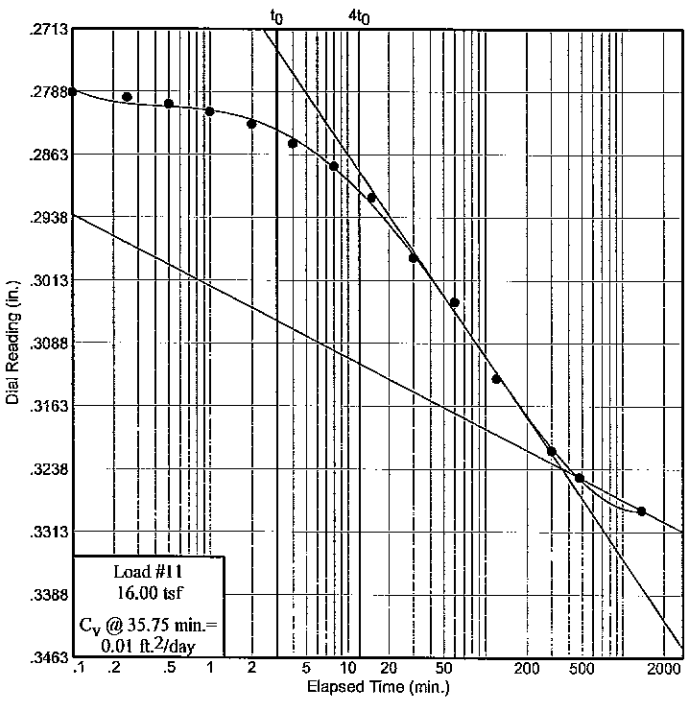
Dial Reading vs. Time

Project No.: B09-012
Project: BAYOU DUPONT

Source: B-9 Sample No.: 28 Elev./Depth: 54-56







Dial Reading vs. Time

Southern Earth Sciences, Inc.

CONSOLIDATION TEST DATA

Client: URS
Project: BAYOU DUPONT
Project Number: B09-012

Sample Data

Source: B-9
Sample No.: 28
Elev. or Depth: 54-56 **Sample Length(in./cm.):**
Location:
Description: SO G CL W/ SI, CH
Liquid Limit: 76 **Plasticity Index:** 49
USCS: (CH) **AASHTO:** **Figure No.:**
Testing Remarks: ASTM D2435

Test Specimen Data

TOTAL SAMPLE		BEFORE TEST		AFTER TEST	
Wet w+t =	117.97 g.	Consolidometer # =	1	Wet w+t =	120.45 g.
Dry w+t =	90.67 g.			Dry w+t =	87.93 g.
Tare Wt. =	38.19 g.	Spec. Gravity =	2.80	Tare Wt. =	.00 g.
Height =	1.00 in.	Height =	1.00 in.		
Diameter =	2.50 in.	Diameter =	2.50 in.		
Weight =	136.51 g.	Defl. Table =	Unit No. 9 Old 2.5in		
Moisture =	52.0 %	Ht. Solids =	0.3987 in.	Moisture =	37.0 %
Wet Den. =	105.9 pcf	Dry Wt. =	89.80 g.*	Dry Wt. =	87.93 g.
Dry Den. =	69.7 pcf	Void Ratio =	1.508	Void Ratio =	0.931
		Saturation =	96.6 %		

*** Initial dry weight used in calculations**

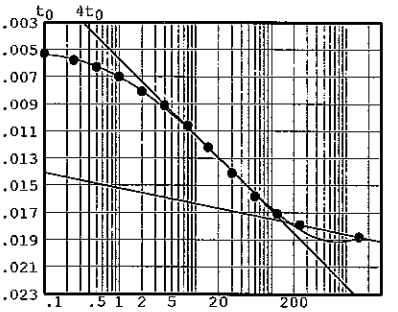
End-of-Load Summary

Pressure (tsf)	Final Dial (in.)	Machine Defl. (in.)	C_v (ft.^{2}/day)	C_α	Void Ratio	% Compression /Swell
start	0.00000				1.508	
0.25	0.01910	0.00030	0.05	0.001	1.461	1.9 Comprs.
0.50	0.04560	0.00050	0.02	0.002	1.395	4.5 Comprs.
1.00	0.09400	0.00080	0.01	0.008	1.274	9.3 Comprs.
0.50	0.08620	0.00080	0.05		1.294	8.5 Comprs.
0.25	0.07430	0.00050	0.02		1.324	7.3 Comprs.
0.50	0.08110	0.00070	0.05	0.001	1.307	8.0 Comprs.
1.00	0.09980	0.00090	0.02	0.004	1.260	9.9 Comprs.
2.00	0.16140	0.00120	0.01	0.017	1.106	16.0 Comprs.
4.00	0.22180	0.00170	0.01	0.011	0.956	22.0 Comprs.
8.00	0.28060	0.00260	0.01	0.011	0.811	27.8 Comprs.
16.00	0.33230	0.00360	0.01	0.012	0.684	32.9 Comprs.
2.00	0.29600	0.00150			0.770	29.5 Comprs.
0.25	0.23090	0.00060			0.931	23.0 Comprs.

C_c = 0.42 P_c = 0.25 tsf C_r = 0.11

Pressure: 0.25 tsf **TEST READINGS** **Load No. 1**

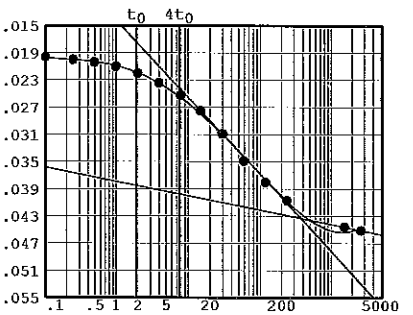
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.00000	11	60.00	0.01610
2	0.10	0.00560	12	120.00	0.01740
3	0.25	0.00610	13	240.00	0.01820
4	0.50	0.00660	14	1500.00	0.01910
5	1.00	0.00730			
6	2.00	0.00840			
7	4.00	0.00940			
8	8.00	0.01090			
9	15.00	0.01250			
10	30.00	0.01440			



Void Ratio = 1.461 **Compression =** 1.9 %
D_0 = 0.00471 D_{50} = 0.01117 D_{100} = 0.01764
C_v **at 9.5 min.** = 0.05 ft.^{2}/day C_α = 0.001

Pressure: 0.50 tsf **TEST READINGS** **Load No. 2**

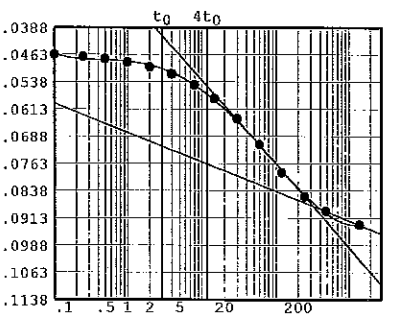
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.01910	11	60.00	0.03540
2	0.10	0.02010	12	120.00	0.03850
3	0.25	0.02050	13	240.00	0.04120
4	0.50	0.02090	14	1560.00	0.04510
5	1.00	0.02150	15	2700.00	0.04560
6	2.00	0.02250			
7	4.00	0.02390			
8	8.00	0.02570			
9	15.00	0.02800			
10	30.00	0.03140			



Void Ratio = 1.395 **Compression =** 4.5 %
D_0 = 0.01820 D_{50} = 0.03075 D_{100} = 0.04331
C_v **at 28.7 min.** = 0.02 ft.^{2}/day C_α = 0.002

Pressure: 1.00 tsf **TEST READINGS** **Load No. 3**

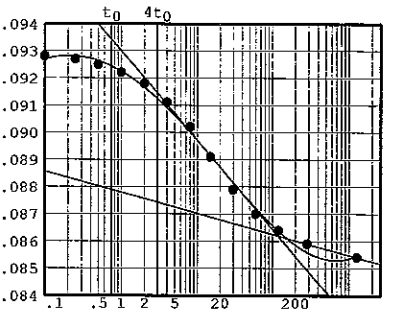
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.04560	11	60.00	0.07190
2	0.10	0.04710	12	120.00	0.07960
3	0.25	0.04770	13	248.00	0.08620
4	0.50	0.04820	14	480.00	0.09020
5	1.00	0.04920	15	1420.00	0.09400
6	2.00	0.05050			
7	4.00	0.05250			
8	8.00	0.05550			
9	15.00	0.05920			
10	30.00	0.06480			



Void Ratio = 1.274 **Compression =** 9.3 %
D_0 = 0.04325 D_{50} = 0.06563 D_{100} = 0.08801
C_v **at 33.4 min.** = 0.01 ft.^{2}/day C_α = 0.008

Pressure: 0.50 tsf **TEST READINGS** **Load No. 4**

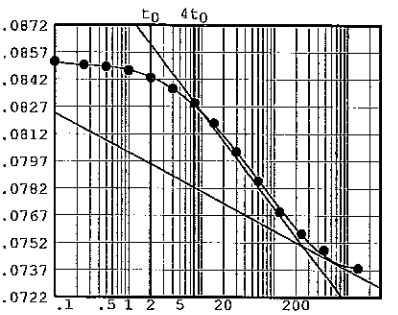
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.09400	11	60.00	0.08780
2	0.10	0.09360	12	120.00	0.08720
3	0.25	0.09350	13	290.00	0.08670
4	0.50	0.09330	14	1290.00	0.08620
5	1.00	0.09300			
6	2.00	0.09260			
7	4.00	0.09190			
8	8.00	0.09100			
9	15.00	0.08990			
10	30.00	0.08870			



Void Ratio = 1.294 **Compression** = 8.5 %
D_0 = 0.09364 D_{50} = 0.08992 D_{100} = 0.08620
C_v **at 8.6 min.** = 0.05 ft.^{2}/day

Pressure: 0.25 tsf **TEST READINGS** **Load No. 5**

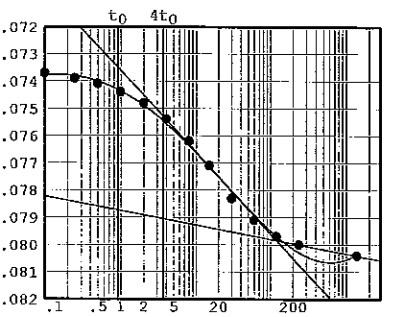
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.08620	11	60.00	0.07910
2	0.10	0.08570	12	120.00	0.07740
3	0.25	0.08550	13	240.00	0.07620
4	0.50	0.08540	14	480.00	0.07530
5	1.00	0.08520	15	1390.00	0.07430
6	2.00	0.08480			
7	4.00	0.08420			
8	8.00	0.08340			
9	15.00	0.08230			
10	30.00	0.08070			



Void Ratio = 1.324 **Compression** = 7.3 %
D_0 = 0.08553 D_{50} = 0.08027 D_{100} = 0.07500
C_v **at 24.8 min.** = 0.02 ft.^{2}/day

Pressure: 0.50 tsf **TEST READINGS** **Load No. 6**

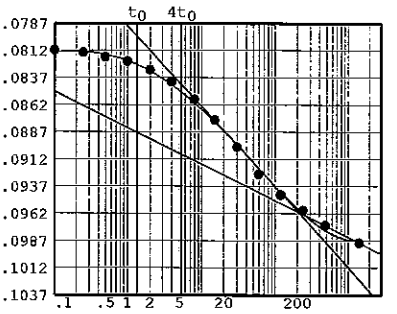
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.07430	11	60.00	0.07980
2	0.10	0.07440	12	120.00	0.08040
3	0.25	0.07460	13	240.00	0.08070
4	0.50	0.07480	14	1380.00	0.08110
5	1.00	0.07510			
6	2.00	0.07550			
7	4.00	0.07610			
8	8.00	0.07690			
9	15.00	0.07780			
10	30.00	0.07900			



Void Ratio = 1.307 **Compression** = 8.0 %
D_0 = 0.07315 D_{50} = 0.07650 D_{100} = 0.07984
C_v **at 9.1 min.** = 0.05 ft.^{2}/day C_α = 0.001

Pressure: 1.00 tsf **TEST READINGS** **Load No. 7**

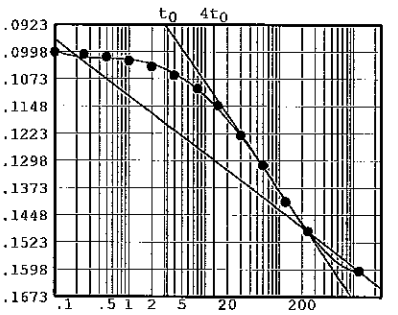
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.08110	11	60.00	0.09350
2	0.10	0.08210	12	120.00	0.09540
3	0.25	0.08230	13	240.00	0.09680
4	0.50	0.08270	14	480.00	0.09820
5	1.00	0.08310	15	1440.00	0.09980
6	2.00	0.08390			
7	4.00	0.08500			
8	8.00	0.08660			
9	15.00	0.08850			
10	30.00	0.09100			



Void Ratio = 1.260 **Compression** = 9.9 %
D_0 = 0.07995 D_{50} = 0.08802 D_{100} = 0.09609
C_v at 16.5 min. = 0.02 ft.^{2}/day C_α = 0.004

Pressure: 2.00 tsf **TEST READINGS** **Load No. 8**

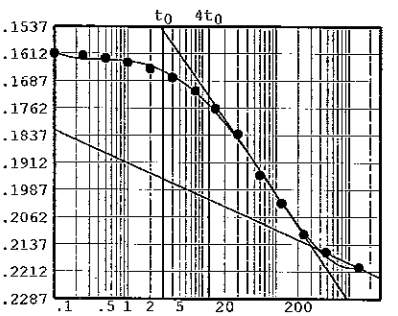
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.09980	11	60.00	0.13230
2	0.10	0.10110	12	120.00	0.14230
3	0.25	0.10170	13	240.00	0.15050
4	0.50	0.10240	14	1190.00	0.16140
5	1.00	0.10350			
6	2.00	0.10510			
7	4.00	0.10750			
8	8.00	0.11110			
9	15.00	0.11580			
10	30.00	0.12400			



Void Ratio = 1.106 **Compression** = 16.0 %
D_0 = 0.09547 D_{50} = 0.12222 D_{100} = 0.14897
C_v at 28.3 min. = 0.01 ft.^{2}/day C_α = 0.017

Pressure: 4.00 tsf **TEST READINGS** **Load No. 9**

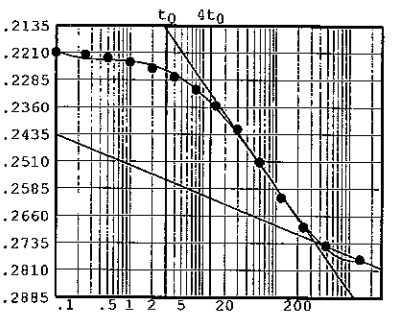
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.16140	11	60.00	0.19640
2	0.10	0.16290	12	120.00	0.20410
3	0.25	0.16350	13	240.00	0.21270
4	0.50	0.16420	14	480.00	0.21760
5	1.00	0.16540	15	1380.00	0.22180
6	2.00	0.16710			
7	4.00	0.16950			
8	8.00	0.17320			
9	15.00	0.17800			
10	30.00	0.18510			



Void Ratio = 0.956 **Compression** = 22.0 %
D_0 = 0.15682 D_{50} = 0.18544 D_{100} = 0.21407
C_v at 31.9 min. = 0.01 ft.^{2}/day C_α = 0.011

Pressure: 8.00 tsf **TEST READINGS** **Load No. 10**

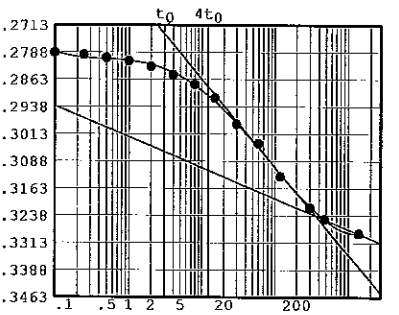
No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.22180	11	60.00	0.25380
2	0.10	0.22360	12	120.00	0.26360
3	0.25	0.22430	13	240.00	0.27170
4	0.50	0.22510	14	480.00	0.27680
5	1.00	0.22620	15	1380.00	0.28060
6	2.00	0.22790			
7	4.00	0.23030			
8	8.00	0.23380			
9	15.00	0.23820			
10	30.00	0.24470			



Void Ratio = 0.811 **Compression** = 27.8 %
D_0 = 0.21719 D_{50} = 0.24503 D_{100} = 0.27287
C_v at 34.8 min. = 0.01 ft.^{2}/day C_α = 0.011

Pressure: 16.00 tsf **TEST READINGS** **Load No. 11**

No.	Elapsed Time	Dial Reading	No.	Elapsed Time	Dial Reading
1	0.00	0.28060	11	60.00	0.30750
2	0.10	0.28250	12	120.00	0.31660
3	0.25	0.28310	13	300.00	0.32520
4	0.50	0.28390	14	480.00	0.32840
5	1.00	0.28480	15	1380.00	0.33230
6	2.00	0.28630			
7	4.00	0.28860			
8	8.00	0.29130			
9	15.00	0.29500			
10	30.00	0.30220			



Void Ratio = 0.684 **Compression** = 32.9 %
D_0 = 0.27599 D_{50} = 0.29985 D_{100} = 0.32370
C_v at 35.8 min. = 0.01 ft.^{2}/day C_α = 0.012