

## Attachment: Cone of Influence

### Calculations I. Required information

$\text{USDWdepth} = 760 \text{ feet}$	depth to the base of the lowermost USDW (feet)
$\text{GWdepth} = 0 \text{ feet}$	depth to the top of groundwater (feet). Zero feet means ground water at surface
$\text{Porosity} = 0.08$	porosity of the injection interval (fraction)
$\text{Pstatic} = 3567.15 \text{ psi}$	measured static pressure in the injection interval at the start of the permitted injection period (psi). Note this static pressure should be depth adjusted to the top of the injection interval
$\text{InjIntervalDepth} = 8239 \text{ feet}$	depth to the top of the injection interval (feet).
$h = 245 \text{ feet}$	net thickness of the injection interval (feet)
$\text{viscosity} = 1.14 \text{ cp}$	viscosity of the native injection interval fluid (cp)
$\text{brineSG} = 1.05$	specific gravity of the native injection interval fluid (dimensionless)
$ct = 6 \times 10^{-6} \text{ psi}^{-1}$	total system compressibility for the injection interval ( $\text{psi}^{-1}$ )
$k = 2.7 \text{ md}$	effective permeability of the injection interval to the injectate (md)
$r_w = 0.3 \text{ feet}$	radius of the individual injection wellbore (feet)
$r = 1320 \text{ feet}$	radius where to calculate the pressure rise. At the well $r = r_w$ and $r_w$ is determined from the individual injection wellbore (feet)
$\text{FWgrad} = 0.433 \text{ psi/feet}$	fresh water density as a pressure gradient (psi/feet)
$\text{APmudwt} = 9.5 \text{ lb/gal}$	mud density in abandoned wellbores (lb/gal)
$\text{FWwt} = 8.33 \text{ lb/gal}$	fresh water density (lb/gal)
$\text{Tpermit} = 87,600 \text{ hours}$	permit life (hours)
$\text{Qpermit} = 700 \text{ barrels/day}$	permit injection rate (barrels/day)
$B = 1.0 \text{ RB/STB}$	formation volume factor for injectate (reservoir bbls/surface stock tank bbls, $r_{vb}/\text{stb}$ ). Usually assumed to be 1

## **II. Calculate the allowable pressure rise above static pressure in an abandoned well**

Note: Make two calculations as needed depending if area wells are mud-filled or brine-filled:

1. Assume a mud filled borehole using the minimum mud weight determined for wells in the area
2. Assume a brine-filled borehole using the density of the native injection interval fluid

This calculation assumes no mud fallback in a well and no mud gel strength. It represents the amount of pressure change needed to cause upward movement of a full column of mud in an abandoned well.

$$\begin{aligned}\text{AllowPressRiseAtAP} &= [(\text{InjIntervalDepth}) * (\text{APmudwt}) * (\text{FWgrad}/\text{FWwt})] - \text{Pstatic} \\ &= [8239 * 9.5 * (.433/8.33)] - 3567.15 \\ &= 501.4 \text{ psi}\end{aligned}$$

## **III. Calculate the cone of influence (COI) using dimensionless variables (Methodology taken from Appendix C of Society of Petroleum Engineers Monograph 5)**

Note: Allowable pressure rise is determined first and then used to calculate the radial distance at which it occurs.

Dimensionless pressure, Pd:

$$\begin{aligned}\text{Pd} &= (\text{AllowPressRiseAtAP} * k * h) / (141.2 * Q_{\text{permit}} * B * \text{viscosity}) \\ &= (501.4 * 2.7 * 245) / (141.2 * 700 * 1 * 1.14) \\ &= 2.944\end{aligned}$$

Dimensionless time, td:

$$\begin{aligned}\text{td} &= 0.0002637 * k * [T_{\text{permit}} / (c_t * \text{porosity} * \text{viscosity} * r_w^2)] \\ &= 0.0002637 * 2.7 * [87600 / (6 * 10^{-6} * 0.08 * 1.14 * 0.3^2)] \\ &= 1.266 * 10^9\end{aligned}$$

Dimensionless radius, rd:

$$\begin{aligned}\text{rd} &= (\text{td} / e^{[(2 * \text{Pd}) - 0.80907]})^{0.5} \\ &= (1.266 * 10^9 / e^{[(2 * 2.944) - 0.80907]})^{0.5} \\ &= 2.808 * 10^3\end{aligned}$$

Calculate the radial distance of the cone of influence, COIradius:

$$\begin{aligned}\text{COIradius} &= \text{rd} * r_w \\ &= 2.808 * 10^3 * 0.3 \\ &= 842 \text{ feet}\end{aligned}$$

**IV. Projected pressure increase at a distance r away from the injector**

Note: The radius r is known and the pressure rise is calculated

Dimensionless time,  $t_d$ : Same as before except r is the radial distance from the injection well where pressure rise is to be calculated. This example assumed 1320'

$$\begin{aligned} t_d &= 0.0002637 * k * [T_{\text{permit}} / (c_t * \text{porosity} * \text{viscosity} * r_w^2)] \\ &= 0.0002637 * 2.7 * [87600 / (6 \times 10^{-6} * 0.08 * 1.14 * 0.3^2)] \\ &= 1.266 \times 10^9 \end{aligned}$$

Dimensionless radius,  $r_d$ : Different equation since r is a known radial distance

$$\begin{aligned} r_d &= r / r_w \quad (\text{At the well } r_d = 1 \text{ because } r = r_w) \\ &= 1320 / 0.3 \\ &= 4400 \end{aligned}$$

Dimensionless pressure,  $P_d$ : Different equation to calculate the pressure buildup at known radial distance, r

$$\begin{aligned} P_d &= 0.5 * [\ln(t_d / r_d^2) + 0.80907] \\ &= 0.5 * [\ln(1.266 \times 10^9 / 4400^2) + 0.80907] \\ &= 2.5 \end{aligned}$$

$$\begin{aligned} \text{PressureRise} &= 141.2 * Q * B * \text{viscosity} * P_d / (k * h) \\ &= 141.2 * 700 * 1 * 1.14 * 2.5 / (2.7 * 245) \\ &= 426 \text{ psi} \end{aligned}$$